

# EXHIBIT A

Case nos. 6:20-cv-00634 and 6:20-cv-00636

**Demaray LLC v Intel Corp.**  
**Demaray LLC v Samsung Electronics Co. Ltd., et al.**

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*Markman* Hearing

August 17, 2021

- 1) “pulsed DC power” / “pulsed DC power supply”
- 2) “narrow band rejection filter”
- 3) “preamble” / “insulating substrate”
- 4) “metallic mode” / “poison mode”
- 5) “reconditioning the target”
- 6) “substantially constant”

# “pulsed DC power”

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'657 Patent, Claim 1

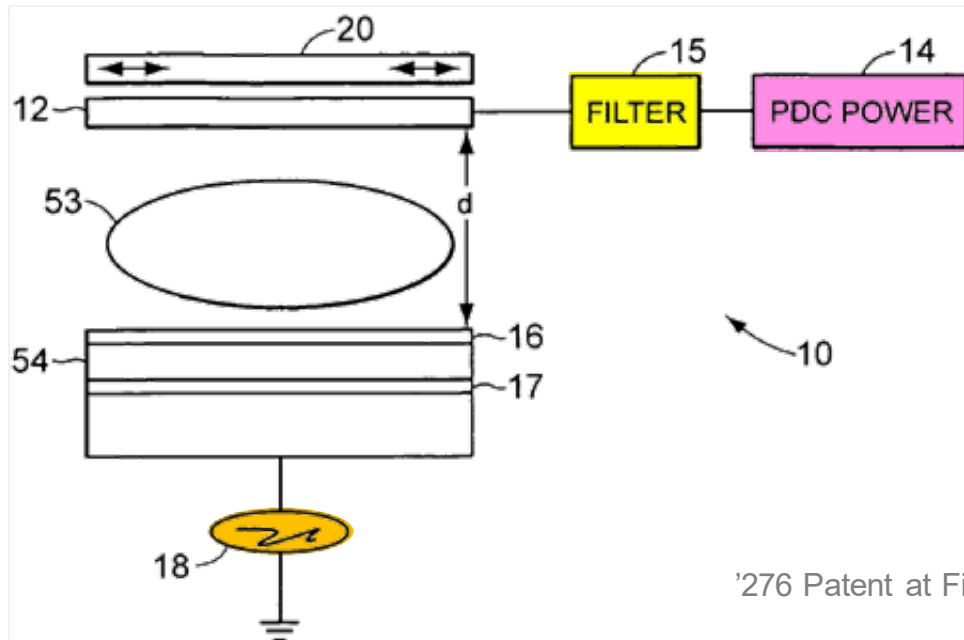
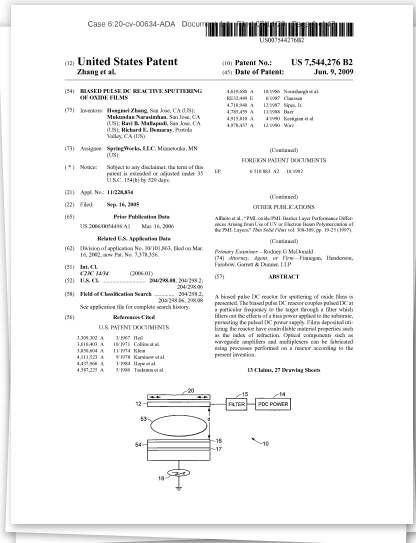
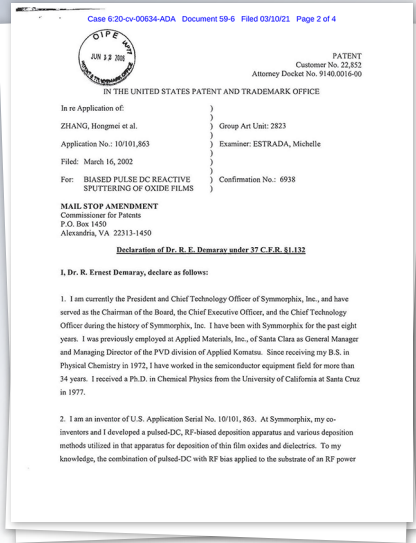
'276 Patent, Claims 1 and 6



# Patentee's Claimed Invention

4. My co-inventors and I developed the **band-rejection filter** described in the specification and claimed in U.S. Application Serial No. 10/101, 863 to overcome the problem of catastrophic failure of the **pulsed-DC power supply** output electrometer circuit during operation. We discovered that a **band-rejection filter**, which is a filter that passes all of the frequencies of the square wave power supply except within a **narrow band** centered on the RF frequency of the **RF bias**, protected the **pulsed-DC power supply** from the RF energy while not distorting the pulses generated by the **pulsed-DC power supply** applied to the target.

Dkt. 59-6 (06/07/2006 Dr. Demaray Declaration), ¶ 4



'276 Patent at Fig. 1A

## Claim Term

## Tentative Construction

“**pulsed** DC power” (’657 patent, claim 1)

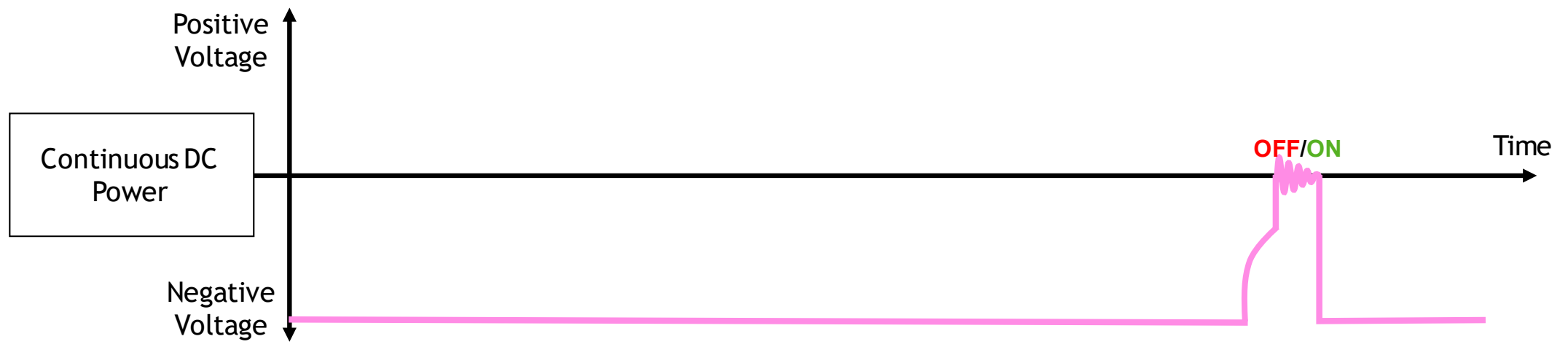
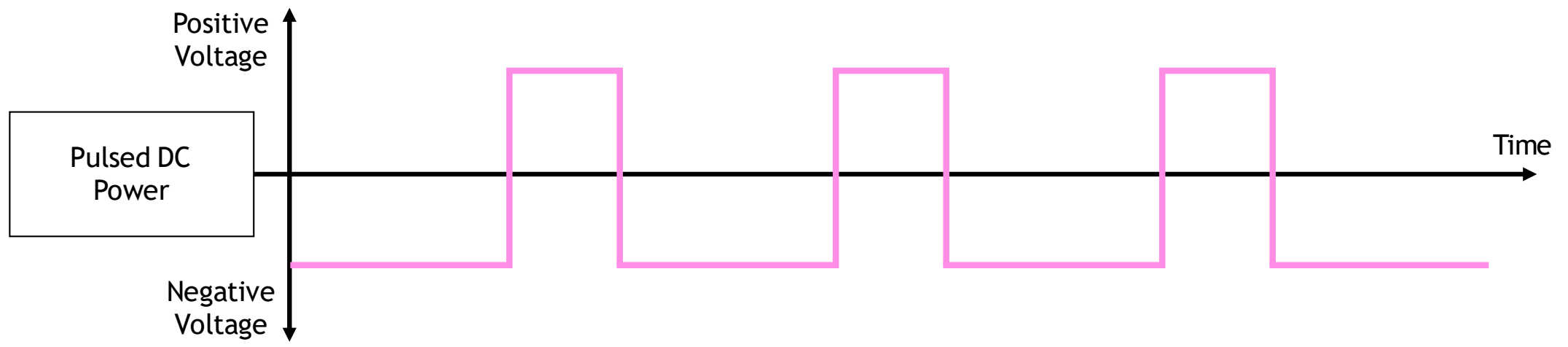
“direct current power that **oscillates between positive and negative voltages**”

“**pulsed** DC power supply” (’276 patent, claims 1, 6)

“supply for providing **pulsed** DC power”

**Fine-Tuned Dispute:** does the Court’s construction, which requires “oscillat[ing] between positive and negative voltages” encompass continuous DC power with arc suppression?

**Fine-Tuned Construction #1:** “direct current power that oscillates between **predetermined** positive and negative voltages”





# Tentative Construction Effectively Removes “Pulsed” from Claims

Claim Term	Court’s Tentative Construction
“ <b>pulsed</b> DC power” (’657 patent, claim 1)	“direct current power that <b>oscillates between positive and negative voltages</b> ”

## ’657 Patent, Claim 1

1. A method for depositing a film on an insulating substrate, comprising:

...

that ~~oscillates between positive and negative voltages~~

providing **pulsed DC power** to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;

...

# Tentative Construction Effectively Removes “Pulsed” from Claims

Claim Term	Court’s Tentative Construction
“ <b>pulsed</b> DC power” (’657 patent, claim 1)	“direct current power that <b>oscillates between positive and negative voltages</b> ”

## Unasserted Parent: ’356 Patent, Claim 1

1. A method of depositing an insulating oxide film on a substrate, comprising:

...

~~that **oscillates between positive and negative voltages**~~

applying **pulsed DC power** to the target such that a voltage on the target oscillates between positive and negative voltages...

...

# Tentative Construction Effectively Removes “Pulsed” from Claims

Claim Term	Court’s Tentative Construction
“ <b>pulsed</b> DC power” (’657 patent, claim 1)	“direct current power that <b>oscillates between positive and negative voltages</b> ”
“ <b>pulsed</b> DC power supply” (’276 patent, claims 1, 6)	“supply for providing <b>pulsed</b> DC power”

## ’276 Patent, Claim 1

1. A reactor according to the present invention, comprising:

...

that ~~oscillates between positive and negative voltages~~

the **pulsed DC power supply** providing alternating negative and positive voltages to the target;

...



## Demaray's Own Presentation

### Prosecution History: Express Definition

Applicants have explicitly defined pulsed DC power to refer to power that oscillates between positive and negative voltages. (See, application, par. [0053]). As described in the specification, the positive voltage period allows an insulating layer deposited on the target to discharge, resulting in an arc free deposition process. (See, application, par. [0053]). However, a second definition of "pulsed DC power" was also in use at the time, and the second definition is apparently the definition utilized in Smolanoff. In this second definition, which is also referred to as unipolar pulsed DC, the DC power supplied to the target is grounded on occasion, either periodically or when an impending discharge is detected. The DC power can be shunted to ground so that the voltage on the target was brought from a high negative voltage to near ground voltage until the arc condition was dissipated, while the negative voltage power supply was protected from the discharge. This process was also referred to as "pulsed DC power," but, in Smolanoff, the target remains at a negative voltage throughout the deposition.<sup>2</sup>

Ex. 3 ('356 FH) at DEMINT0001305

Applicants have explicitly defined pulsed DC power to refer to power that oscillates between positive and negative voltages. (See, application, par. [0053]). As described in the specification, the positive voltage period allows an insulating layer deposited on the target to discharge, resulting in an arc free deposition process. (See, application, par. [0053]). However, a second definition of "pulsed DC power" was also in use at the time, and the second definition is apparently the definition utilized in Smolanoff. In this second definition, which is also referred to as unipolar pulsed DC, the DC power supplied to the target is grounded on occasion, either periodically or when an impending discharge is detected. The DC power can be shunted to ground so that the voltage on the target was brought from a high negative voltage to near ground voltage until the arc condition was dissipated, while the negative voltage power supply was protected from the discharge. This process was also referred to as "pulsed DC power," but, in Smolanoff, the target remains at a negative voltage throughout the deposition.<sup>2</sup>



I. Smolanoff does not teach “applying pulsed DC power to the target . . . such that the target voltage oscillates between positive and negative voltages,” as is recited in claims 21 and 43.

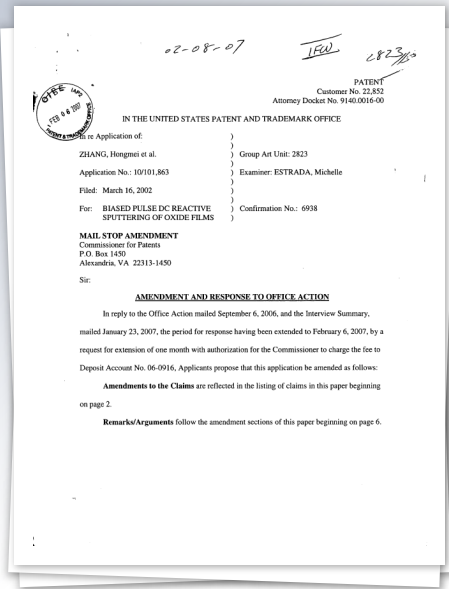
Smolanoff teaches that “[t]he target power supply 21 is usually a source of constant or pulsed DC power and is connected between the cathode assembly 17 and some element such as the chamber wall 13 which is at ground potential and serves as the system anode.” (Smolanoff, col. 5, lines 51-54). Additionally, Smolanoff teaches that “[p]ower from the steady or pulsed DC power supply 21 and/or RF generator 24 produces a negative potential on the target 16.” (Smolanoff, col. 5, line 66, through col. 6, line 1).

## Demaray’s Own Presentation

### Prosecution History: Express Definition

Applicants have explicitly defined pulsed DC power to refer to power that oscillates between positive and negative voltages. (See, application, par. [0053]). As described in the specification, the positive voltage period allows an insulating layer deposited on the target to discharge, resulting in an arc free deposition process. (See, application, par. [0053]). However, a second definition of “pulsed DC power” was also in use at the time, and the second definition is apparently the definition utilized in Smolanoff. In this second definition, which is also referred to as unipolar pulsed DC, the DC power supplied to the target is grounded on occasion, either periodically or when an impending discharge is detected. The DC power can be shunted to ground so that the voltage on the target was brought from a high negative voltage to near ground voltage until the arc condition was dissipated, while the negative voltage power supply was protected from the discharge. This process was also referred to as “pulsed DC power,” but, in Smolanoff, the target remains at a negative voltage throughout the deposition.<sup>2</sup>

The process of pulsed DC power as claimed in claims 21 and 43, where “the target voltage oscillates between positive and negative voltages,” then, differs from the teachings of Smolanoff at least in that Smolanoff teaches that the target remains at a negative potential. Such pulses occur only, generally, when an impending discharge from the target is sensed and may not be periodic. Therefore, Smolanoff does not teach “that the target voltage oscillates between positive and negative voltages,” as is recited in claims 21 and 43.



21. (Currently amended): A method of depositing [[a]] an oxide film on a substrate, comprising:  
 conditioning a target;  
 preparing the substrate;  
 adjusting an RF bias power to the substrate;  
 setting a process gas flow; and  
applying pulsed DC power to the target through a filter such that the target voltage oscillates between positive and negative voltages to create a plasma and deposit the oxide film,

43. (Currently amended): A method of depositing [[a]] an oxide film on a substrate, comprising:  
 preparing the substrate;  
 adjusting an RF bias power to the substrate;  
 setting a process gas flow; and  
applying pulsed DC power to a target through a band rejection filter at a frequency of the bias power such that the target voltage oscillates between positive and negative voltages and an oxide film is deposited on the substrate.

**SUPPLEMENTAL PRELIMINARY AMENDMENT**

15. (Currently amended) A reactor according to the present invention, comprising:

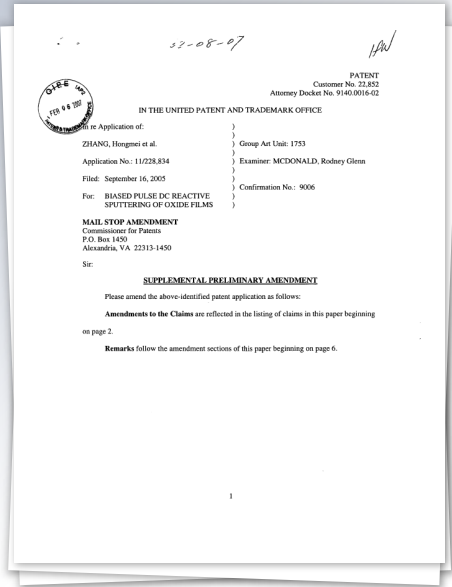
a target area for receiving a target;

a substrate area opposite the target area for receiving a substrate;

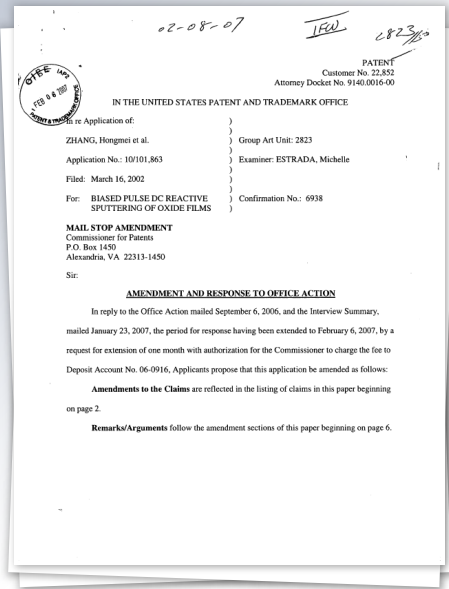
a pulsed DC power supply coupled to the target area, **the pulsed DC power supply providing alternating negative and positive voltages to the target; and**

**[(a)] an RF bias power supply coupled to the substrate; and**

a narrow band-rejection filter that rejects at a frequency of the RF bias power supply coupled between the pulsed DC power supply and the target area.



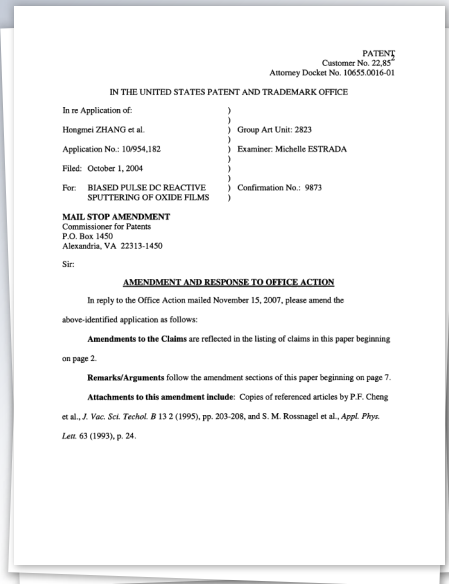
supported in the specification. **Claim 15 has been amended to recite that “the pulsed DC power supply providing alternating negative and positive voltages to the target,” which is disclosed, for example, in paragraph [0053] of the specification.** Claim 15 has also been amended to recite “a



During the interview, the inventors described to the Examiner the development of the invention, including the development of applicant's pulsed-DC processing technology, and the teachings of the cited references. In particular, the Smolanoff reference was discussed with respect to independent claims 21 and 43. Applicants discussed amending the claims to further clarify the distinctions between the claimed invention and the teachings of Smolanoff and other cited art. Those amendments are reflected in the amended claims above and in the newly added claims. The distinctions between the claimed invention and the cited prior art is further

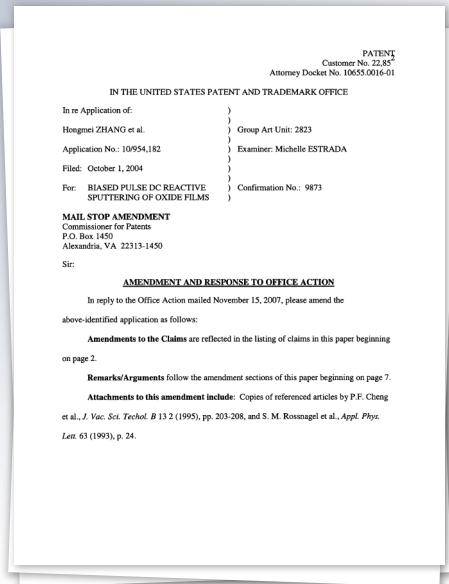
Some embodiments of pulsed DC processing, as defined in the present application, can substantially eliminate this problem. As discussed, for example, in paragraph [0053] of Applicant's application, pulsed DC sputtering refers to a sputtering technique where the pulsed DC power supply oscillates between positive and negative potentials, driving the voltage of the target alternately to positive and negative potentials. Claims 21 and 43 of the present application have been amended to explicitly recite that "the target voltage oscillates between positive and negative voltages." New claim 51 also recites that "the target voltage oscillates between positive and negative voltages." The claims have also been amended to recite that the deposited films are





**Claim 62 (Currently amended): A method of depositing a film on [[a]] an insulating substrate, comprising:**  
**providing a process gas between a conductive target and [[a]] the substrate;**  
**providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;**

Smolanoff never teaches that the target can be positive and, in accordance with the teachings of Smolanoff, the target voltage must always be negative. **Therefore, Smolanoff teaches away from “providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages” as is recited in claim 62.** Additionally, Smolanoff then teaches away from the combination “providing pulsed DC power to the target through a narrow band rejection filter such that the voltage on the target alternates between positive and negative voltages” and “providing an RF bias that corresponds to the narrow band rejection filter to the substrate,” as is recited in claim 62.



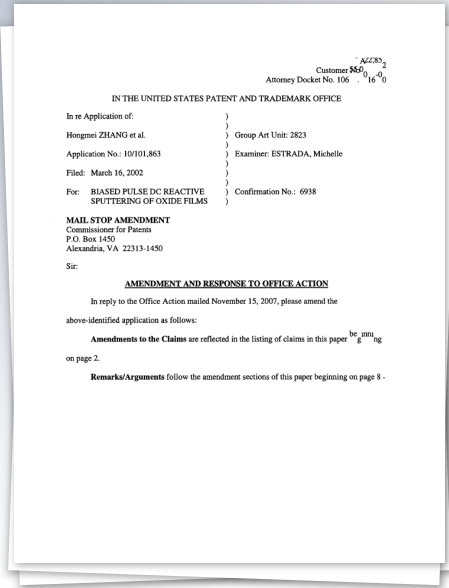
**Claim 62 (Currently amended): A method of depositing a film on [[a]] an insulating substrate, comprising:  
providing a process gas between a conductive target and [[a]] the substrate;  
providing pulsed DC power to the target through a narrow band rejection filter such that  
the target alternates between positive and negative voltages;**

(Office Action, page 3). However, as explained during the interview, that is not the case. **The narrow band rejection filter allows the combination of pulsed-dc power to the target (where the target voltage is oscillated between positive and negative voltages) and an RF bias on the substrate.** A filter that blocks too many of the constituent frequencies of the pulsed DC waveform results in the target voltage not attaining a positive voltage. A filter that does not block the RF bias voltage can result in failure of the DC power supply. Smolanoff does not teach the “narrow band rejection filtering” recited in each of claims 62 and 85.

Dkt. 60-5, Dec. 18, 2007  
Amendment ('657 patent  
app.), 972-73, 979,

# Patentee Again Distinguishes from DC Power Supply

Case 6:20-cv-00636-ADA Document 176-1 Filed 03/03/22 Page 19 of 148



RF bias applied to the substrate, as is recited in claims 21, 43, and 51. Additionally, Fu does not teach the elements for which it is relied or itself teach the combination of pulsed-DC power and RF bias recited in the claims.

Fu teaches high density, magnetic field enhanced ionized metal vapor deposition of conducting films. (See Fu, abstract). Fu, however, teaches utilization of a DC power supply (Fu, col. 1, lines 30-32) in combination with an RF bias applied to the substrate (Fu, col. 2, lines 36-41). Therefore, Fu fails to teach “adjusting an RF bias power to the substrate” in combination with “applying pulsed DC power to the target such that a voltage on the target oscillates between positive and negative voltages to create a plasma and deposit the oxide film” as is recited in

Dkt. 60-5 (Dec. 18, 2007  
Amendment ('657 patent app.), 977,

# Demaray's Own Presentation

## Prosecution History: Express Definition

Applicants have explicitly defined pulsed DC power to refer to power that oscillates between positive and negative voltages. (See, application, par. [0053]). As described in the specification, the positive voltage period allows an insulating layer deposited on the target to discharge, resulting in an arc free deposition process. (See, application, par. [0053]). However, a second definition of "pulsed DC power" was also in use at the time, and the second definition is apparently the definition utilized in Smolanoff. In this second definition, which is also referred to as unipolar pulsed DC, the DC power supplied to the target is grounded on occasion, either periodically or when an impending discharge is detected. The DC power can be shunted to ground so that the voltage on the target was brought from a high negative voltage to near ground voltage until the arc condition was dissipated, while the negative voltage power supply was protected from the discharge. This process was also referred to as "pulsed DC power," but, in Smolanoff, the target remains at a negative voltage throughout the deposition.<sup>2</sup>

Ex. 3 ('356 FH) at DEMINT0001305

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## Demaray's Own Presentation

### Specification: Consistent With Claim Language



For pulsed reactive dc magnetron sputtering, as performed by apparatus 10, the polarity of the power supplied to target 12 by power supply 14 oscillates between negative and positive potentials. During the positive period, the insulating layer on the surface of target 12 is discharged and arcing is prevented. To obtain arc free deposition, the pulsing frequency exceeds a critical frequency that depend on target material, cathode current and reverse time. High quality oxide films can be made using reactive pulse DC magnetron sputtering in apparatus 10.

Ex. 1 ('657 Patent), 5:36-45

24

For pulsed reactive dc magnetron sputtering, as performed by apparatus 10, the polarity of the power supplied to target 12 by power supply 14 oscillates between negative and positive potentials. During the positive period, the insulating layer on the surface of target 12 is discharged and arcing is prevented. To obtain arc free deposition, the pulsing frequency exceeds a critical frequency that depend on target material, cathode current and reverse time. High quality oxide films can be made using reactive pulse DC magnetron sputtering in apparatus 10.

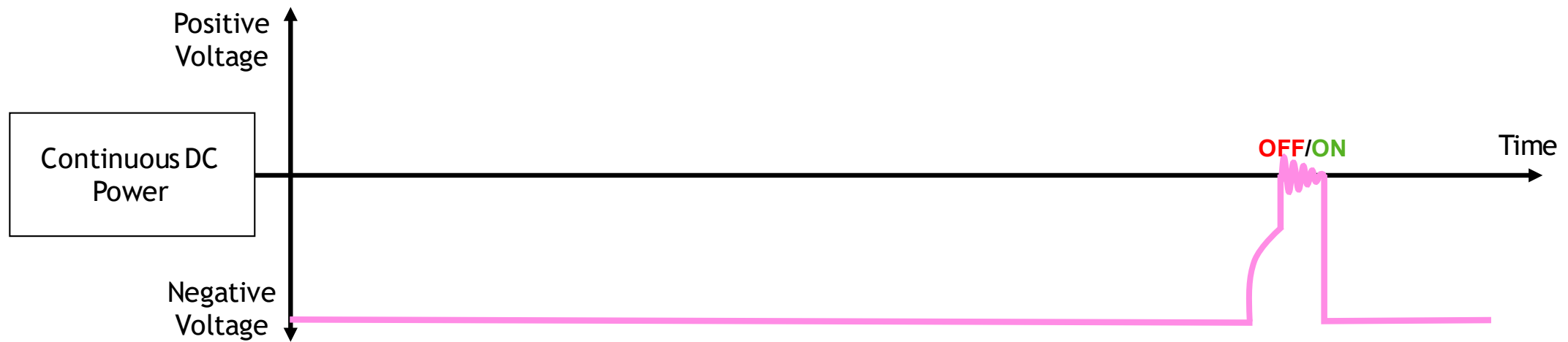
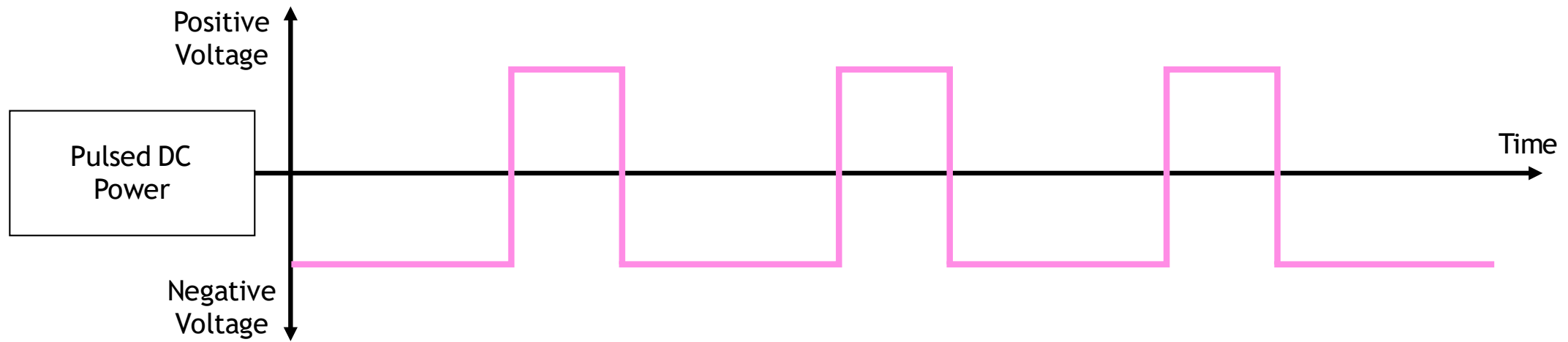
Fee Class	Number	Rate	Fee
Initial	1	\$ 9.00	\$ 9.00
Continuation	2	\$ 9.00	\$ 18.00
Divisional	3	\$ 9.00	\$ 18.00
Reissue	4	\$ 9.00	\$ 18.00
Extension of Time	5	\$ 9.00	\$ 18.00

Respectfully submitted,  
Gary J. Edwards  
Attorney for Applicant(s)  
Reg. No. 41,068

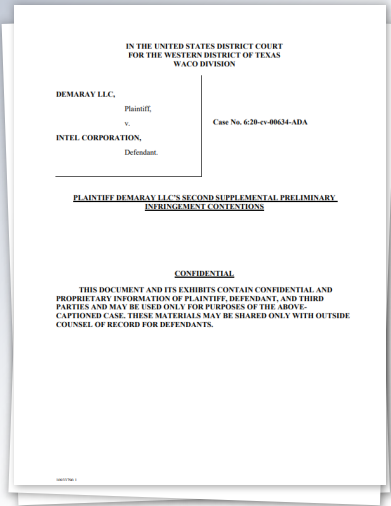
[0053]

[0051] For pulsed reactive dc magnetron sputtering, as performed by apparatus 10, the polarity of the power supplied to target 12 by power supply 14 oscillates between negative and positive potentials. During the positive period, the insulating layer on the surface of target 12 is discharged and arcing is prevented. To obtain arc free deposition, the pulsing frequency exceeds a critical frequency that depend on target material, cathode current and reverse time. High quality oxide films can be made using reactive pulse DC magnetron sputtering in apparatus 10.

# “pulsed DC power” vs. continuous DC power



# Demaray Attempts To Capture DC with Arc Suppression (Not Pulsed DC for Arc Prevention)

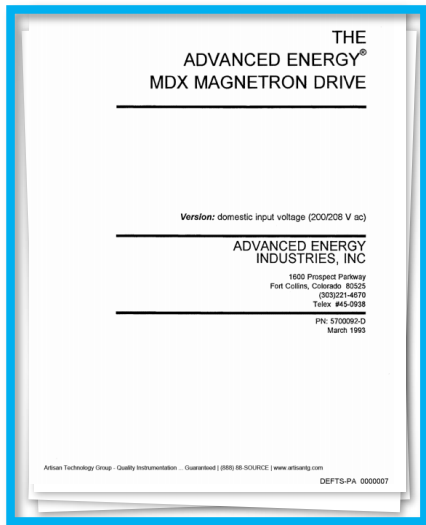


## Infringement Contentions

As another example, the Advanced Energy Pinnacle III DC power source manual describes very similar arc suppression using pulses of DC power. See, e.g., AMAT-DEM\_0000447 (“*When an arc of less than 50 μs occurs, the stored energy of the arc-out circuit is channeled into the arc and the voltage is reversed, the current passes through zero, and the arc is extinguished. Thus, the Pinnacle III unit configured with the arc-out circuitry can extinguish an arc and restore process voltage in approximately 50 μs.* This is very similar to the arc-out circuitry of the Advanced Energy Pinnacle II, MDX, and MDX-L power supplies.”); see also

04/15/2021 Plaintiff’s Second Supplemental Infringement Contentions (Intel), Exhibit A Claim Chart at 40

## Advanced Energy MDX Conventional DC Power Supply Manual (1993)



### Arc-suppression Circuitry

ARC-OUT™ provides multilevel suppression and quenching of different types of arcs. An added advantage is that ARC-OUT reduces target burn-in time and material loss. This feature also prevents energy from being dumped into hot spots by sensing a drop in impedance and immediately shutting the power off. Start-up after an arc is controlled so that the hot spots cool before power is reapplied, thus preventing repeated arcing.

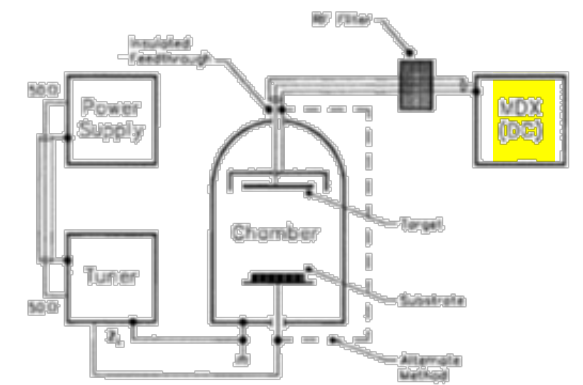


Figure 1-4. Typical configuration for dc sputtering with RF bias

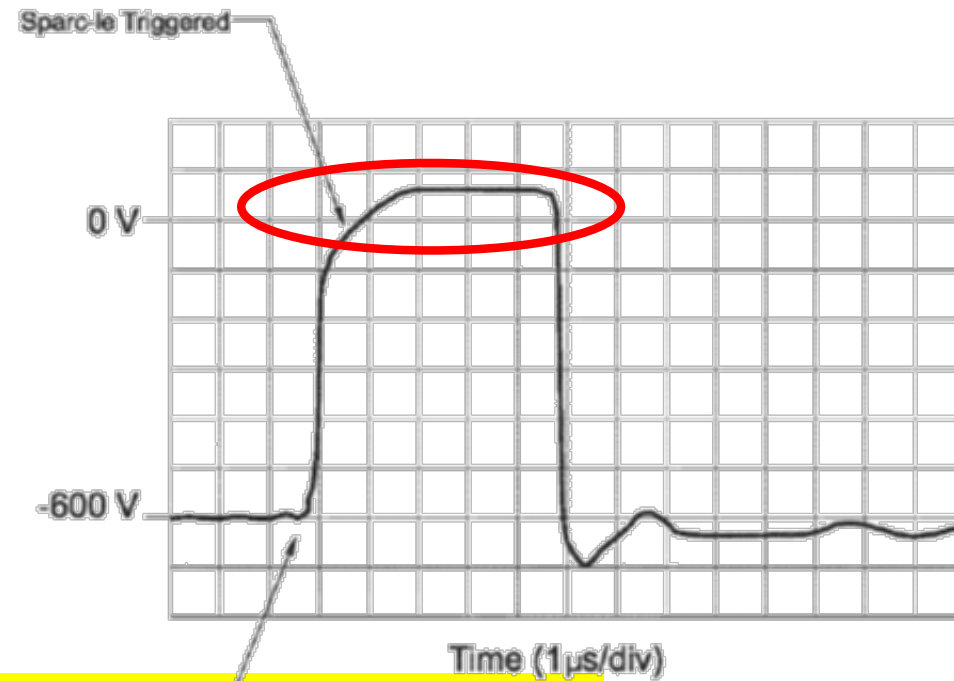
Dkt. 61-2 (The Advanced Energy MDX Magnetron Drive (1993)) at 18

# Demaray's Own Presentation

## Intrinsic Record: Pulses At Arc Detection Known



Ex. 16 at DEFTS-PA\_0003062



Arc Event  
Figure 5. SPARC-LE<sup>®</sup> waveforms, arc triggered



### Demaray's Own Presentation

Intrinsic Record: Pulses At Arc Detection Known

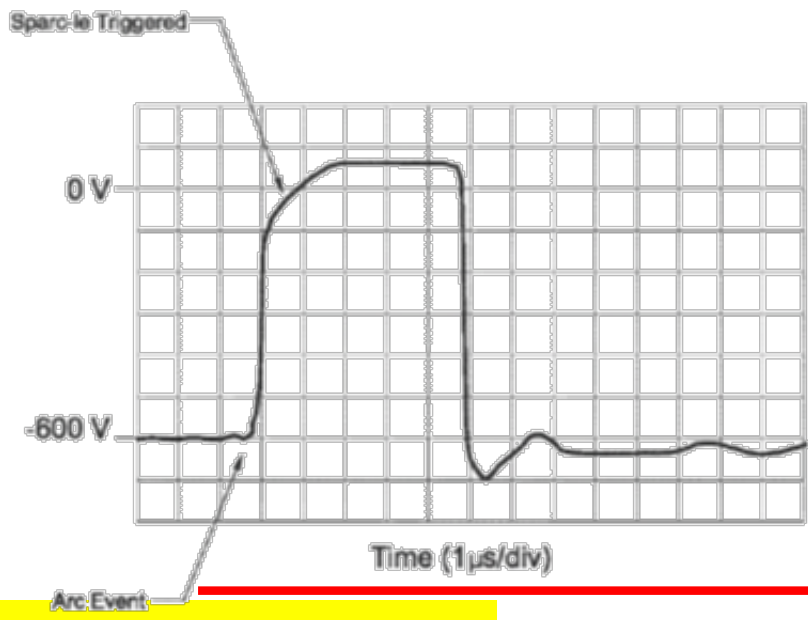
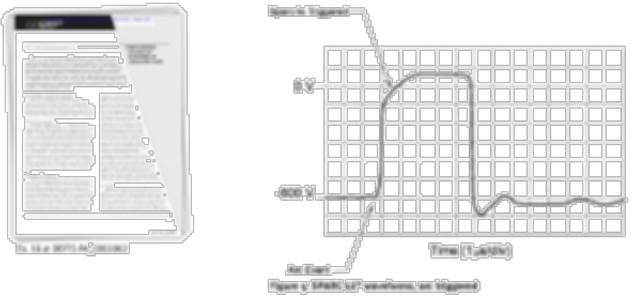


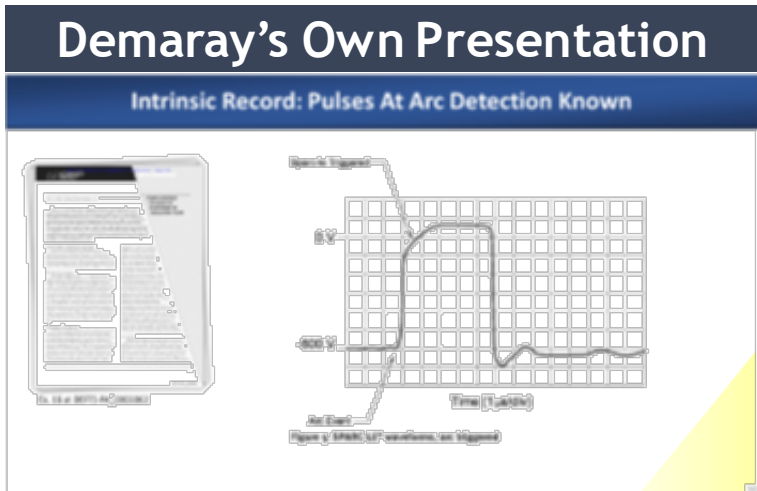
Figure 5. SPARC-LE<sup>®</sup> waveforms, arc triggered

#### Pulsed DC approaches

For the thin insulating layers formed on the target during reactive sputtering, however, there is no need to resort to radio-frequency power. Depending upon the dielectric constant of the reaction product and the current density of the arriving ions, the layers can be kept discharged with relatively low frequencies. **If the layers are kept discharged, arcing can be prevented altogether.** For Al<sub>2</sub>O<sub>3</sub>, a discharge rate of only 20 kHz is sufficient to prevent dielectric breakdown for current densities of up to 103 A/m<sup>2</sup>, and it can be shown that the rate required to prevent breakdown is not dependent upon the film thickness [4]. This fact has been taken advantage of in the use of a number of approaches to reactive sputtering.

Meanwhile, an arc detect circuit, (D), sends a signal to close the switch when an arc is sensed. This has the effect of removing the electrons from the arc and quenching it. **The voltage waveform for this case is shown in Figure 5 on page 7.**

**"Bipolar pulsed dc" supplies are also available that contain reversal-switching for a dc supply.** These units apply the full output voltage of the dc portion of the power supply to the plasma, in either a positive or negative polarity. The positive and negative pulse widths are adjustable over a considerable range (from a few ms up to 1/2 s) and variable off-times are available between the pulses. Provided the positive pulse is kept



Considerable success has been achieved by an approach that forcibly reverses the target voltage to a few tens of volts higher than the plasma potential [5,9]. This device, Advanced Energy's **Sparc-le®** unit, for which patents are pending, has a basic schematic diagram as shown in **Figure 2 on page 6.**

ADVANCED ENERGY WHITEPAPER  
 IN R. A. 3486, Advanced Energy Industries, Inc.  
**POWER SYSTEMS FOR REACTIVE SPUTTERING OF INSULATING FILMS**

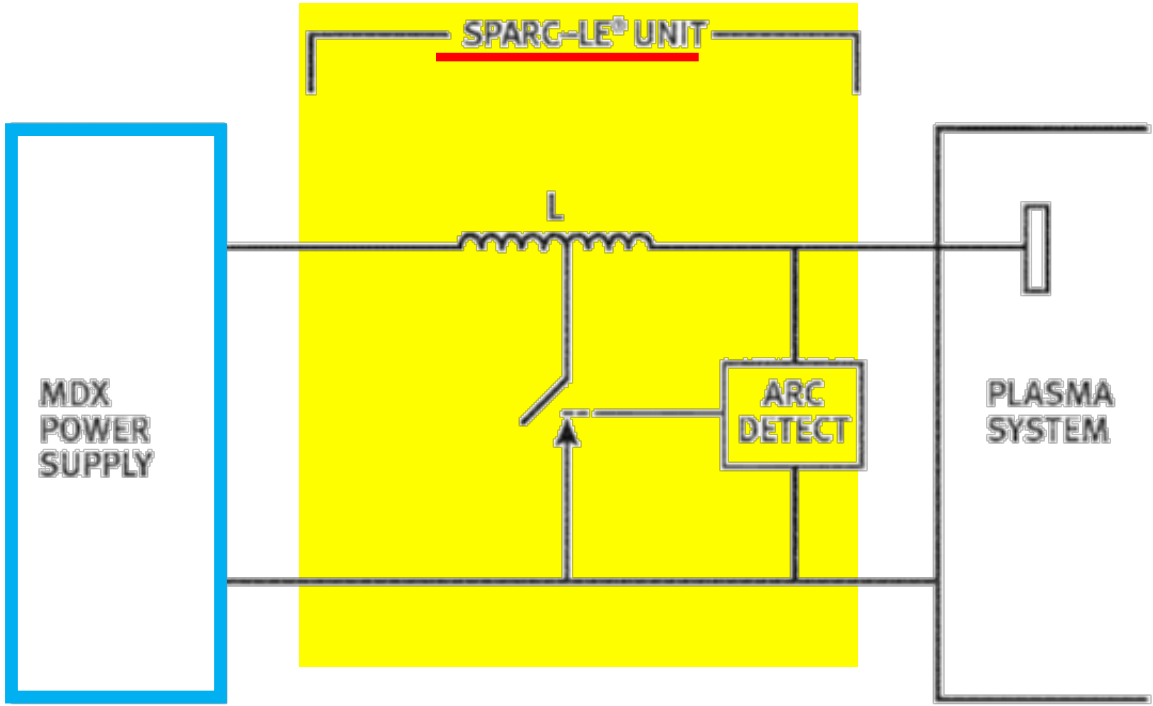
There are several approaches available for deposition of insulating films, and a number of means for arc control in such processes. In addition to the classical direct sputtering of sputtering targets by the use of substrate power, reactive sputtering using direct-current power has been frequently used because of its higher rate of deposition, and several reaction and equipment configurations have been devised for this purpose. These include single-dc sputtering from a single-target single-target sputtering using dc plus an alternating voltage component, either pulsed or sinusoidal, dual-dc sputtering using sinusoidal power and one technique using pulsed power and dual cathodes. This paper will describe the methods used and proposed for all reactive sputtering and the equipment, physical principles, and operating features of each.

**DC SPUTTERING—CONTROLLING ARC LENGTHS?**  
 Even for a fully power-reduced process, switchback to power applies here come to determine the plasma-sputtering power factor. This factor is because of the reactive-positive feature of the sputters as compared to the inertly used inert-gas types. These features result from the fact that the cathode is highly negative, shown in Figure 1 on graph.

**The Switchback Supply**  
 The supply outlined in Figure 1 is a single-phase pulse-width-modulated (PWM) inverter connected into the main power under this approach. In this design, the main voltage is inverted to produce an accelerated dc voltage by the dc inverter (C), which is followed by the switch element (S). The switch element is the heart of the power supply and produces controlled alternating voltage from an accelerated dc input and applies this voltage to the primary of transformer (T). The transformer is used not only to provide isolation from the mains, but also to increase the output voltage and current to the levels required by the load. The output of the transformer is applied to a rectifier (R), which produces dc output voltage at the switching frequency. This output is reduced by L-C filter (F). The other elements shown in Figure 1 will be described later.

**Advantages of the Approach**  
 The three principal advantages of the switchback system are all based on the high frequency of the alternating voltage caused by the switch element (S). First, the transformer (T) can be made smaller and lighter for a given power by the ratio of the mains frequency to the switching frequency. For a switching frequency of 50 kHz, this ratio is 100:1. In actual practice the transformer comes by itself by itself. But small because of the insulation and because readily available materials at the higher frequencies are more common than the materials used in main transformers. Nevertheless, it is possible to make a transformer capable of handling 5000V rms that can use only 1/10th inch of wire. Second, the energy stored in the output filter (F) can be reduced, also by the ratio of the frequency. This not only reduces the size and weight of the elements of the filter but also reduces the energy delivered into "hard" or "soft" arc arcs during processing. The third advantage is equal to reverse. The switch element (S) not only controls an alternating waveform but also controls the amount of power that reaches the output. Since it is operating at a high frequency, it can be considered as high frequency, making an effective power supply much more efficient than their respective counterparts. In most designs output power is determined by the percentage of time the switch element (S) remains on in each cycle. Also, unlike a transformer, the switch can usually used as a modulator power supplies with the control of the middle of a cycle, generally within a fraction of a microsecond. This fact, coupled with the low stored energy in the output filter (F), greatly reduces damage to the cathode or to processing under arc conditions.

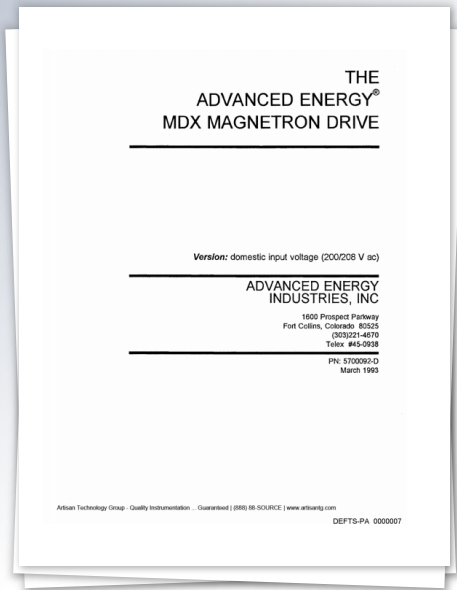
**Arc Control**  
 Should an arc appear across the output of the power supply, the entire output voltage will appear across (L) and the reactor in filter (F). This causes the current in these elements to drop or break with time. As current ceases (C) across the current now on the primary side of (T) and before the current reaches a level that would be dangerous for the switch, turn them off, stopping the current. This sequence



**Figure 2. SPARC-LE® unit simplified schematic**

Ex. 16 at DEFTS-PA\_0003062

# Conventional DC Sputtering with RF Bias (1993)



## DC Sputtering with RF Bias

In this application (see the illustration on the next page), proper installation of the RF generator and tuner is critical to proper operation of the system. Proper installation includes good, solid, RF grounding and dc installation.

An RF filter must be placed between the dc output and the chamber because 13.56 MHz can damage the typical dc magnetron power supply. There is no

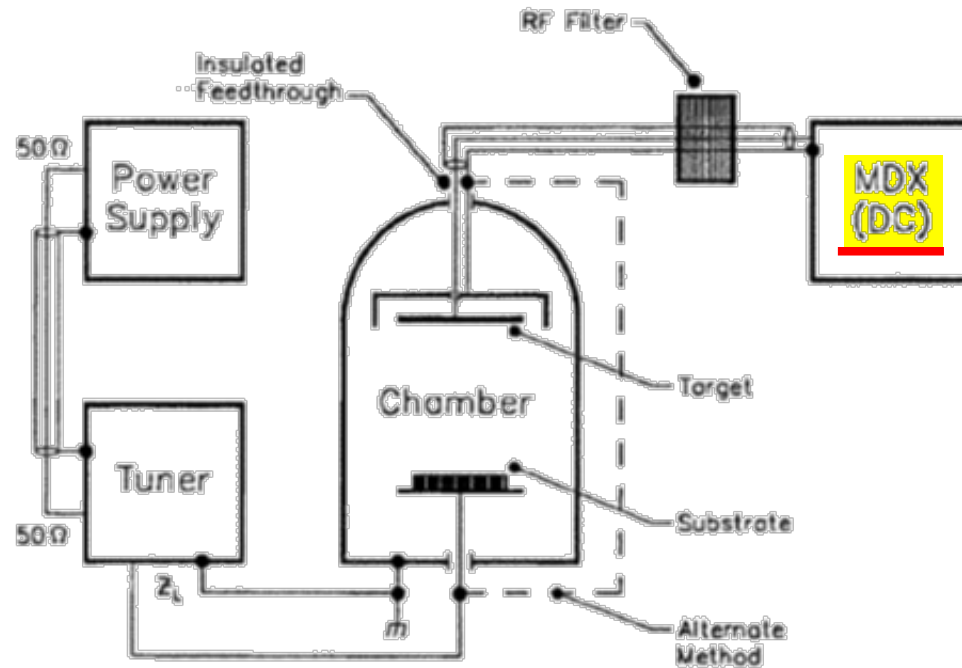
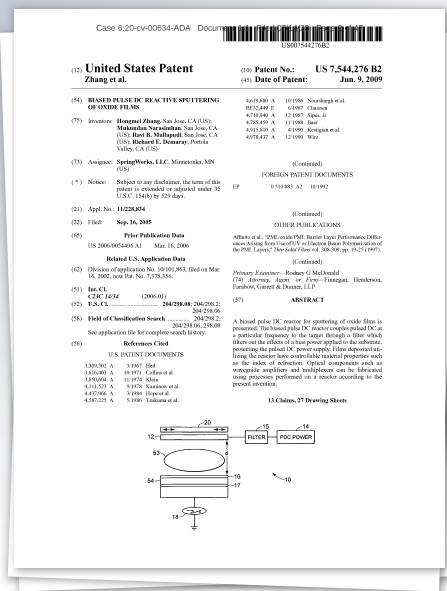


Figure 1-5. Typical configuration for dc sputtering with RF bias.

PN: 5700092-D  
March 1993

# “Pulsed DC Power” Should Not Capture Conventional Systems / Processes Denigrated by the Patentee



Reactive DC magnetron sputtering of nitrides and carbides is a widely practiced technique, but the reactive dc magnetron sputtering of nonconducting oxides is done rarely. Films such as aluminum oxide are almost impossible to deposit by conventional reactive DC magnetron sputtering due to rapid formation of insulating oxide layers on the target surface. The

'276 Patent, 4:44-49



## Claim Term

## Tentative Construction

“**pulsed** DC power” (’657 patent, claim 1)

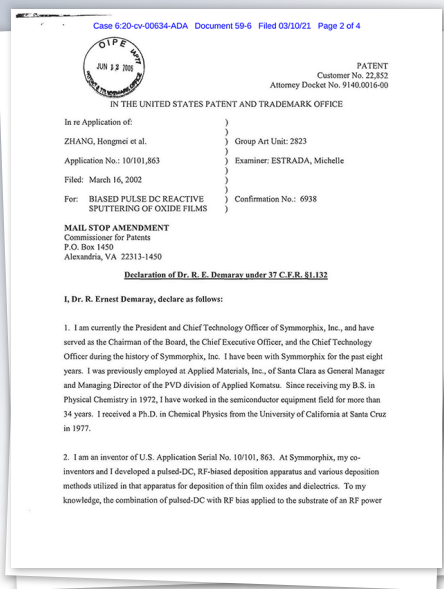
“direct current power **that oscillates between positive and negative voltages**”

“**pulsed** DC power supply” (’276 patent, claims 1, 6)

“supply for providing **pulsed** DC power”

**Fine-Tuned Construction #1:** “direct current power **that oscillates between predetermined positive and negative voltages**”

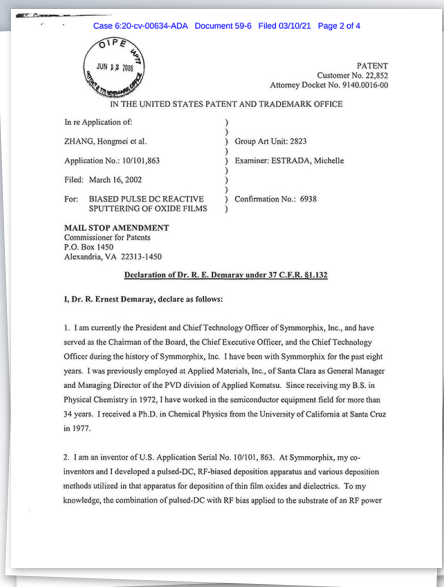
**Fine-Tuned Construction #2:** “direct current power **in a square wave form**”



## Jun. 7, 2006: Dr. Demaray's Sworn Declaration

3. During development of the deposition chambers and methods claimed in this application, we damaged a number (more than six units) of pulsed-DC power supplies due to RF bias power coupling through the plasma into the pulsed-dc power supply. **We utilized the Advanced Energy Pinnacle Plus power supply, which produced a 10 kW square wave** at a frequency of from 180 kHz to 300 KHz together with a pulse reverse time from 1.3 to 5.0  $\mu$ sec. Utilizing a band-pass filter between the pulsed-DC power supply and the plasma, however, will not protect the pulsed-DC power supply from the RF bias and will also unduly distort **the square-wave of the pulsed-DC power** signal applied to the target, which detrimentally affects the deposition conditions.

Dkt. 59-6 (06/07/2006 Dr. Demaray Declaration), ¶ 3  
also at Dkt. 59-5 ('356 File History, part 6/7), 1134 (¶ 3)

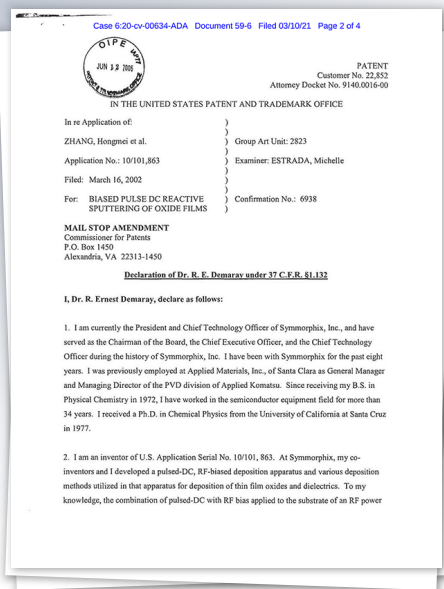


## Jun. 7, 2006: Dr. Demaray's Sworn Declaration

4. My co-inventors and I developed the band-rejection filter described in the specification and claimed in U.S. Application Serial No. 10/101, 863 to overcome the problem of catastrophic failure of the pulsed-DC power supply output electrometer circuit during operation. We discovered that a band-rejection filter, which is a filter that passes all of the frequencies of the square wave power supply except within a narrow band centered on the RF frequency of the RF bias, protected the pulsed-DC power supply from the RF energy while not distorting the pulses generated by the pulsed-DC power supply applied to the target.

3

Dkt. 59-6 (06/07/2006 Dr. Demaray Declaration), ¶ 4  
also at Dkt. 59-5 ('356 File History, part 6/7), 1134 (¶ 4)

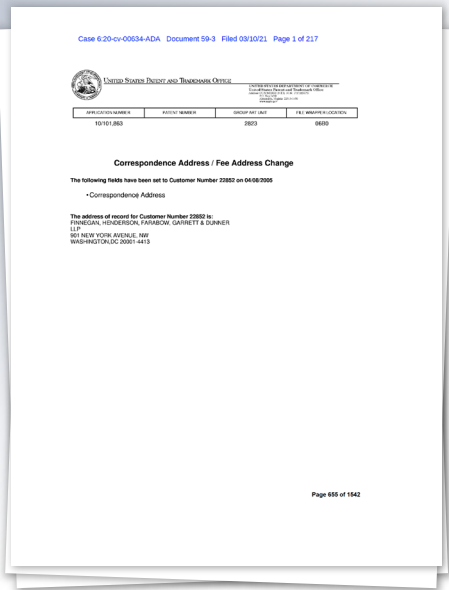


## Jun. 7, 2006: Dr. Demaray's Sworn Declaration

8. Fukui describes a band-pass filter (specifically a low pass filter) coupled between the pulsed-dc power supply and the filter. Again, a band-pass filter does not protect the pulsed-DC power supply, as is required, and will distort the pulsed-DC square wave. Further, Fukui indicates that “[t]he band-pass filter 27 serves to adjust the circuit impedance to have an infinite value so that no RF waves are superposed on a dc power from the dc power supply 28.” (Fukui, col. 6, lines 33-36). This is quite the opposite of what occurs in our applications, where the RF signal is superimposed on the pulsed DC power signal in the plasma, to which the substrate is exposed. Therefore, Fukui does not teach a band-rejection filter at the frequency of the RF bias.

Dkt. 59-6 (Dr. Demaray Declaration), ¶ 8;  
also at Dkt. 59-5 ('356 File History, part 6/7), 1135 (¶ 8)





# Jun. 12, 2006: Patentee’s Response

The Examiner relies on Fukui for this element. However, Fukui does not teach a “band rejection filter at a frequency of the bias power.” As stated in Fukui,

[a]lso connected to the first electrode 20 is a dc power supply 28 through a band-pass filter 27 such as a low-pass filter for adjustment of impedance. The band-pass filter 27 serves to adjust the circuit impedance to have an infinite value so that no RF waves are superposed on a dc power from the dc power supply 28.

(Fukui, col. 6, lines 31-36). Fukui teaches a band pass filter, specifically a low-pass filter, which

would not protect the DC power supply from RF and which would unreasonably distort the

5

pulsed-dc shape. Further, there is no indication that the band-pass filter of Fukui is related to the

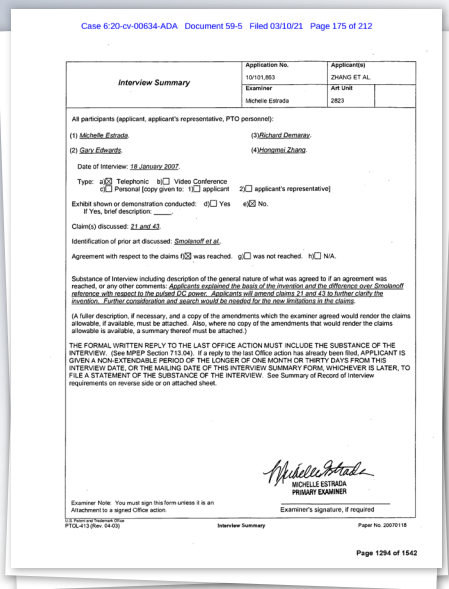
frequency of the bias power supply. A band pass filter, below at or above the frequency of the RF bias, will not protect the pulsed DC power supply from catastrophic failure as a result of the

RF power. Further, a band pass filter does not allow the broad frequency range required for the

6

square wave of the pulsed-DC supply to reach the substrate.

Dkt. 59-5 ('356 File History, part 6/7), 1131



## Jan. 23, 2007: Interview with Patent Office

When explaining the “**basis of the invention**,” the Patentee emphasized the “pulsed DC” square wave form:

- All participants (applicant, applicant's representative, PTO personnel):
- (1) Michelle Estrada.
  - (2) Gary Edwards.
  - (3) Richard Demaray.
  - (4) Hongmei Zhang.

Named inventors

Substance of Interview including description of the general nature of what was agreed to if an agreement was reached, or any other comments: Applicants explained the basis of the invention and the difference over Smolanoff reference with respect to the pulsed DC power. Applicants will amend claims 21 and 43 to further clarify the invention. Further consideration and search would be needed for the new limitations in the claims.

Dkt. 59-5 ('356 File History, part 6/7, 01/23/2007 Interview Summary), 1294

## Feb. 6, 2007: Patentee's Summary of the Same Interview

Case 6:20-cv-00634-ADA Document 59-5 Filed 03/10/21 Page 175 of 212

Interview Summary	Application No.	Applicant
	13115183	ZHANG ET AL
	Examiner	SHI YAN
	Michelle Estrada	2823

All participants (applicant, applicant's representative, PTO personnel):  
(1) Michelle Estrada (2) Richard Demeter  
(3) Gary Edwards (4) Xunmei Zhang

Date of interview: 18 January 2007

Type:  Telephonic  Video Conference  
 Personal (copy given to: 1) applicant  applicant's representative

Exhibit shown or demonstration conducted:  Yes  No  
If Yes, brief description: \_\_\_\_\_

Claim(s) discussed: 21 and 43

Identification of prior art discussed: Smolanoff et al.

Agreement with respect to the claims:  was reached  was not reached  N/A.

Substance of interview including description of the general nature of what was agreed to if an agreement was reached, or any other comments: Applicants explained the basis of the invention and the difference over Smolanoff reference with respect to the pulsed DC power. Applicants will amend claims 21 and 43 to further clarify the invention. Further consideration and search would be needed for the new limitations in the claims.

[A fuller description, if necessary, and a copy of the amendments which the examiner agreed would render the claims allowable, if available, must be attached. Also, where no copy of the amendments that would render the claims allowable is available, a summary thereof must be attached.]

THE FORMAL WRITTEN REPLY TO THE LAST OFFICE ACTION MUST INCLUDE THE SUBSTANCE OF THE INTERVIEW. (See MPEP Section 713.04). If a reply to the last Office action has already been filed, APPLICANT IS GIVEN A NON-EXTENSIBLE PERIOD OF THE LENGTH OF ONE MONTH OR THIRTY DAYS FROM THIS INTERVIEW DATE, OR THE MAILING DATE OF THIS INTERVIEW SUMMARY FORM, WHICHEVER IS LATER, TO FILE A STATEMENT OF THE SUBSTANCE OF THE INTERVIEW. See Summary of Record of interview requirements on reverse side or on attached sheet.

Examiner Note: You must sign this form unless it is an Attachment to a signed Office action.

Michelle Estrada  
MICHELLE ESTRADA  
PRIMARY EXAMINER

Page No. 20070116  
Page 1284 of 1542

During the interview, the inventors described to the Examiner the development of the

invention, including the development of applicant's pulsed-DC processing technology, and the

teachings of the cited references. In particular, the Smolanoff reference was discussed with

• • •

therefore the benefits of using pulsed DC power are lost. Applicants discovered that a narrow

band rejection filter, an embodiment of which is described in the specification at paragraph

[0056], both protects **7** DC power supply from the RF bias power and passes the pulsed DC

frequencies which form **the square pulse of the pulsed DC power** to the target so that the benefits

of pulsed DC deposition with RF bias can be realized. The elimination of a narrow band of

frequencies about a single frequency in a narrow band rejection filter has a small effect on **the**

**8** **square shape of the pulsed DC pulse.** However, elimination of either all higher frequencies or all

lower frequencies from the single frequency effectively destroys **the shape of the square pulse** **9**

and eliminates control of both the magnitude and duration of the positive portion of the pulse.

Dkt. 59-5 ('356 File History, part 6/7, 02/06/2007 Applicant's Response), 1301-03

# “Benefits” Not “Realized” Without Square Wave of “pulsed DC power”

Case 6:20-cv-00634-ADA Document 59-5 Filed 03/02/21 Page 1 of 212

US Form PTO/SDS-1, Revision 09-2004  
INFORMATION DISCLOSURE  
STATEMENT BY APPLICANT

Applicant's Name: [Redacted]  
Inventor's Name: [Redacted]  
Applicant's Address: [Redacted]  
Inventor's Address: [Redacted]

U.S. PATENTS AND PUBLISHED U.S. PATENT APPLICATIONS

Serial No.	Pub. No.	Pub. Date	Pub. Title	Pub. Title	Pub. Title

FOREIGN PATENT DOCUMENTS

Serial No.	Pub. No.	Pub. Date	Pub. Title	Pub. Title	Pub. Title

NON-PATENT LITERATURE DOCUMENTS

Serial No.	Pub. No.	Pub. Date	Pub. Title	Pub. Title	Pub. Title

Signature: *Michael J. [Redacted]*  
Date: 3/16/06

EXPRESS MAIL LABEL NO. EV 8081002 US

Page 1120 of 1542

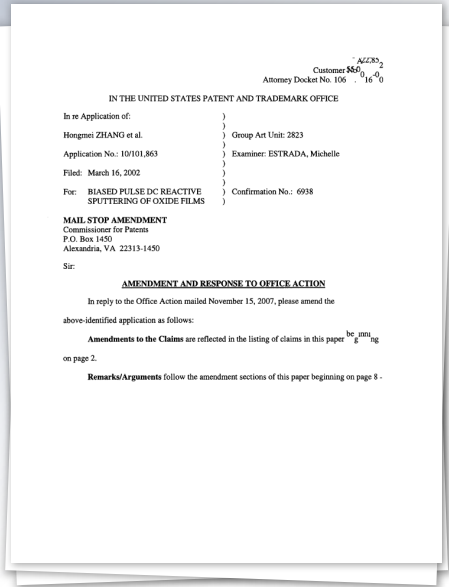
## Feb. 6, 2007: Patentee's Response

Although it is true that “the filter is going to work at certain frequencies,” as suggested by the Examiner, the recited “band rejection filter” works at the frequency of the RF bias supply and blocks only a narrow band of frequencies around the frequency of the RF bias supply. This allows the square wave pulse of the DC power, which is formed of all frequencies both higher and lower than the biased frequency, to be transmitted through the filter to the target. Otherwise, the pulse that would reach the target is distorted so that the benefits of the pulsed DC power are not realized. Therefore, utilization of a band rejection filter at the frequency of the bias power is neither taught nor obvious from the teachings of Smolanoff. Furthermore, use of a band rejection filter at the frequency of the bias power places a distinct limitation on the claim.

10

Dkt. 59-5 ('356 File History, part 6/7, 02/06/2007 Applicant's Response), 1307





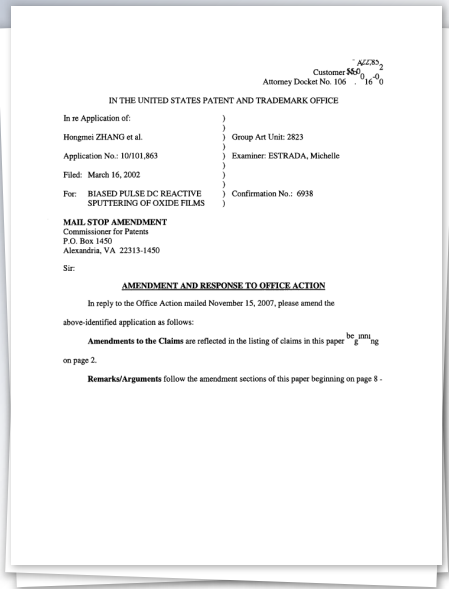
# Dec. 11, 2007: Another Interview With Patent Office

## Examiner's Interview

Applicant thanks the Examiner for meeting with us on December 11, 2007 (the “Interview”). In attendance at the Interview were Examiner Michelle Estrada, Inventor R. Ernest Demaray, and Applicant’s representative Gary J. Edwards. During the interview, all of the claims were discussed as well as the art that has been cited against the claims. Agreement with respect to the claims was reached. In this Amendment, the claims have been amended as discussed during the interview. The Examiner indicated in the Interview Summary that the proposed language for the claims “would overcome the rejection on record.”

Dkt. 59-5 ('356 File History, 012/18/2007 Applicant's Response), 1454

Dkt. 60-5 ('657 File History, 12/18/2007 Applicant's Response), 975



# Dec. 18, 2007: Patentee's Response

Interview, that is not the case. **The filter allows the combination of pulsed-DC power to the**

**target (where the target voltage is oscillated between positive and negative voltages) and an RF**

**bias on the substrate. A filter that blocks too many of the constituent frequencies of the pulsed**

**11 DC waveform results in the target voltage not attaining a positive voltage. A filter that does not**

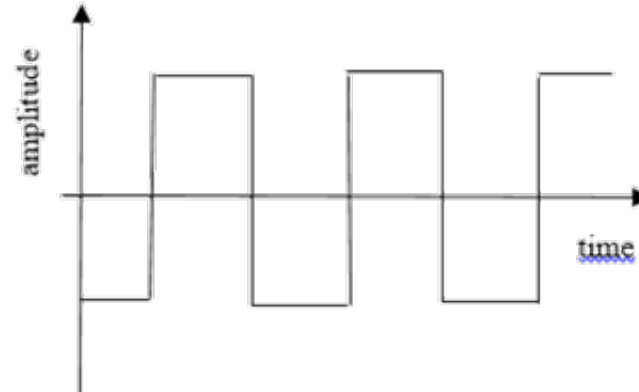
**block the RF bias voltage can result in failure of the DC power supply. Smolanoff does not**

**teach the "narrow band rejection filtering" recited in each of claims 21, 43, and 51.**

Dkt. 59-5 ('356 File History, 012/18/2007 Applicant's Response), 1456-57

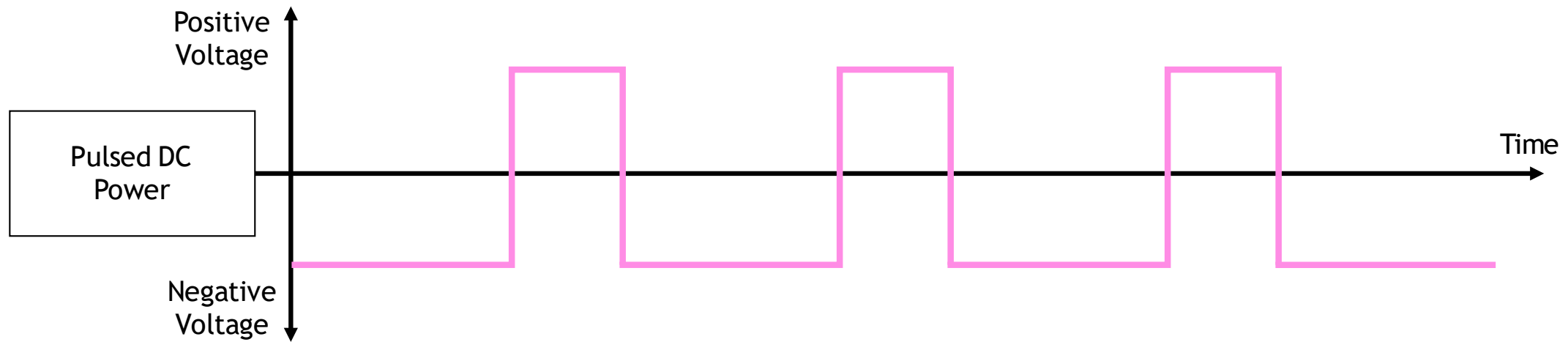


43. DC (direct current) has a unidirectional flow of electrical charge (by contrast, AC (alternating current) takes sinusoidal form). Pulsed DC power can go from positive (or negative) to zero. Alternatively, pulsed DC power can go from positive or negative passing through zero. **In the claims, in order to provide both positive and negative voltage to help reduce arcing, the pulse would have to pass through zero. See, e.g., '657 Patent at 5:30-39. Pulsed DC power passing through zero could thus roughly approximate the following schematic waveform:**



**This schematic waveform is often called a “square wave.”** As practiced in the industry, however, “pulsed DC power” is not restricted to power in the form of a square wave.

Dkt. 46–1 at ¶43



**Fine-Tuned Construction #1:** “direct current power **that oscillates between predetermined positive and negative voltages**”

**Fine-Tuned Construction #2:** “direct current power **in a square wave form**”

# “narrow band rejection filter”

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'657 Patent, Claim 1

'276 Patent, Claims 1 and 6

# “narrow band rejection filter” (NBRF)

## Demaray’s Proposal

Plain and ordinary meaning, or  
“filter which rejects a narrow band of frequencies”

## Defendants’ Proposal

“filter which rejects a narrow band of frequencies (but passes [substantially] all frequencies outside of the narrow band)”

**Court’s Tentative Construction:** Plain and ordinary meaning

**Court’s Tentative Construction:** Plain and ordinary meaning

**The dispute fine-tuned:** is the plain and ordinary meaning of NBRF:

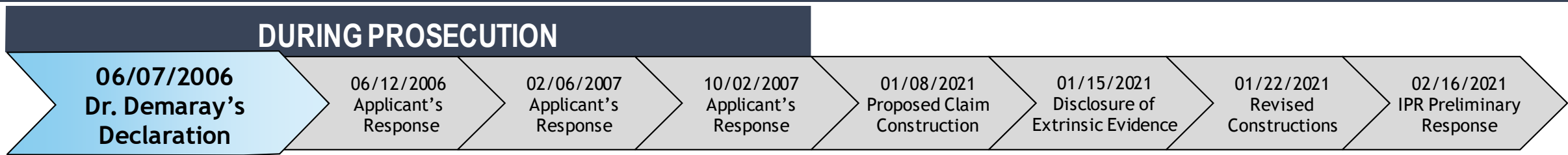
(1) a “filter that passes all of the frequencies of the power supply except within a narrow band”

**OR**

(2) a “filter which rejects a narrow band of frequencies but that is also engineered to do other things as well (such as reject at frequencies outside the narrow band)”



# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band

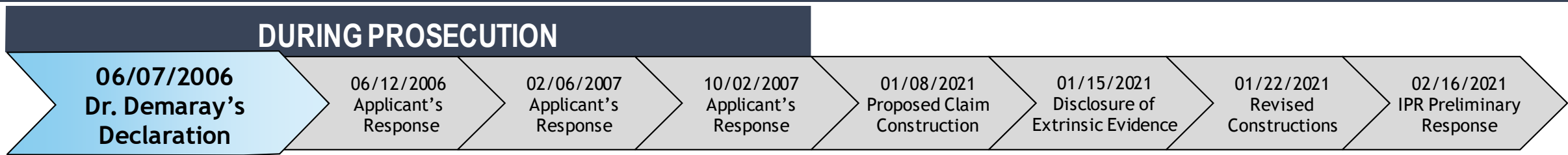


4. My co-inventors and I developed the band-rejection filter described in the specification and claimed in U.S. Application Serial No. 10/101, 863 to overcome the problem of catastrophic failure of the pulsed-DC power supply output electrometer circuit during operation. We discovered that a band-rejection filter, which is a filter that passes all of the frequencies of the square wave power supply except within a narrow band centered on the RF frequency of the RF bias, protected the pulsed-DC power supply from the RF energy while not distorting the pulses generated by the pulsed-DC power supply applied to the target.

Dkt. 59-6 (Declaration), ¶ 4



# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band



4. My co-inventors and I developed the band-rejection filter described in the specification and claimed in U.S. Application Serial No. 10/101, 863 to overcome the problem of catastrophic failure of the pulsed-DC power supply output electrometer circuit during operation. We discovered that a band-rejection filter, which is a filter that passes all of the frequencies of the square wave power supply except within a narrow band centered on the RF frequency of the RF bias, protected the pulsed-DC power supply from the RF energy while not distorting the pulses generated by the pulsed-DC power supply applied to the target.

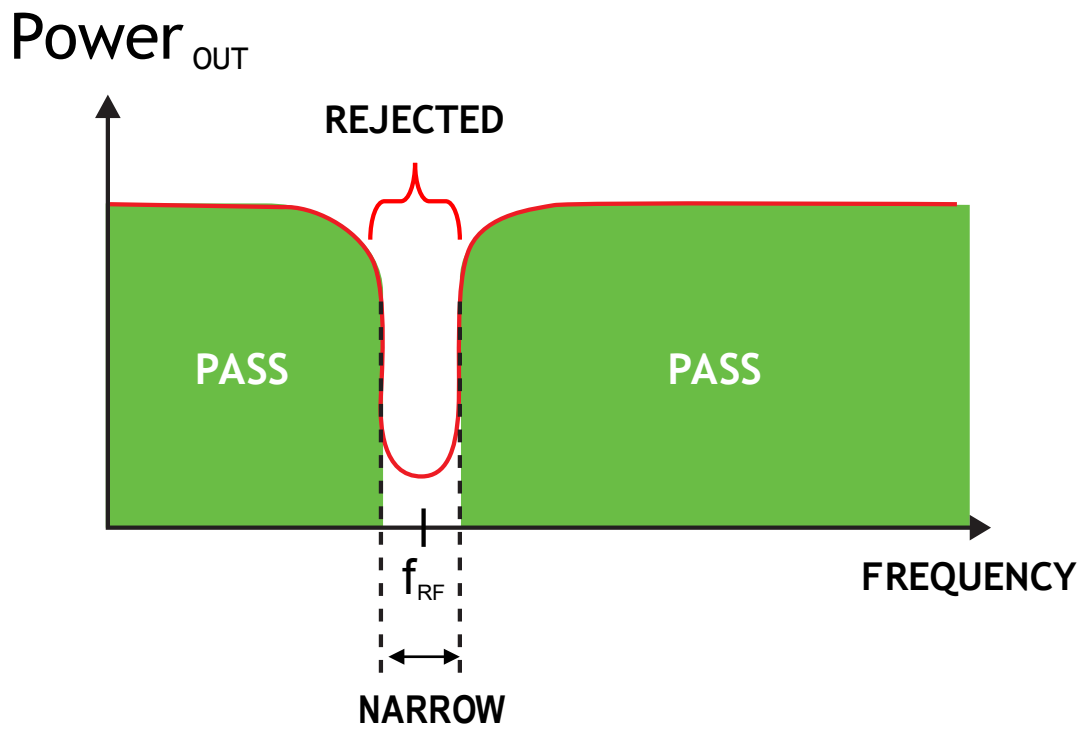
Dkt. 59-6 (Declaration), ¶ 4

# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band

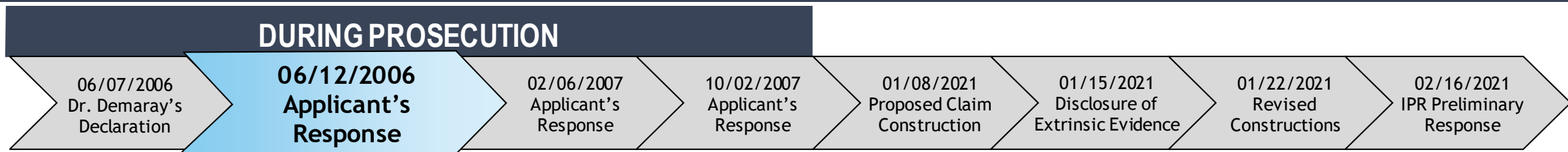
## Demaray's Definition

2MHz). The inventors explained during prosecution that the claimed filter "is a filter that passes all of the frequencies of the [] power supply except within a narrow band centered on the RF frequency of the RF bias..." Ex. 1052 at 1130-31, 1134.

Dkt. 58-3 (IPR2021-00103, 02/16/2021 Demaray's Preliminary Response), 24

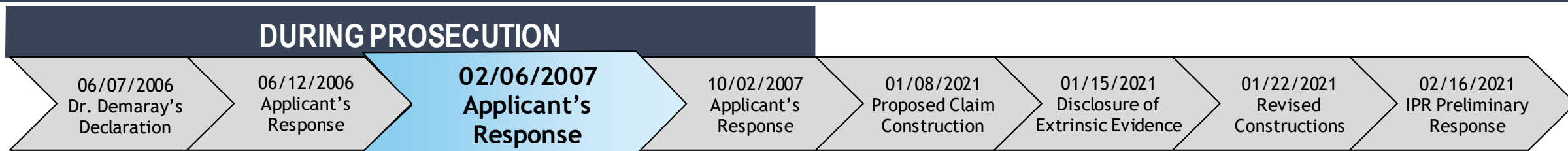


# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band



of the bias power,” as is recited in claim 21. (See, Office Action, page 5). As stated in the Declaration of Ernest Demaray filed with this amendment under 37 C.F.R. §1.132, the filter protecting the pulsed DC power supply from the RF power of the bias is an aspect of the claimed invention. **The filter must pass the pulsed DC signal without unduly affecting the shape of that signal while rejecting the RF power. Therefore, the filter passes all frequencies except for the frequency of the bias power itself.** As stated in the Declaration of Ernest Demaray, other filter designs resulted in a distortion of the pulsed DC signal or in leakage of RF power back to the pulsed DC power supply -- resulting in the catastrophic failure of the power supply.

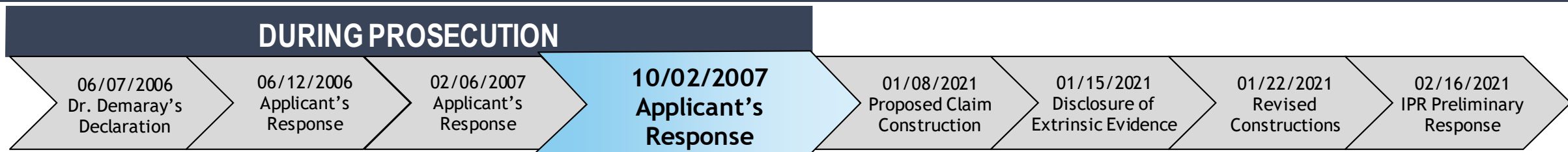
# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band



Although it is true that “the filter is going to work at certain frequencies,” as suggested by the Examiner, the recited “band rejection filter” works at the frequency of the RF bias supply and blocks only a narrow band of frequencies around the frequency of the RF bias supply. This allows the square wave pulse of the DC power, which is formed of all frequencies both higher and lower than the biased frequency, to be transmitted through the filter to the target. Otherwise,

Dkt. 59 ('356 File History, part 7/7), 1307

# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band

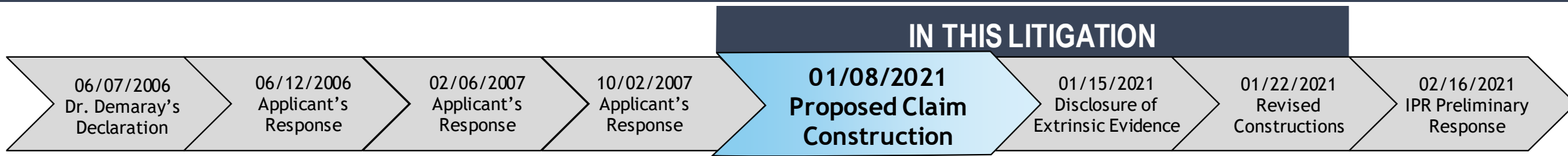


Additionally, in order for the pulsed DC power applied to the target to be useful, the pulsed DC power must include substantially all of its Fourier constituents, and therefore only a band rejection filter that filters out a specific narrow band of filters can be utilized. Further, in order that the pulsed DC power be protected from the RF bias power supply, the band rejection filter must be set to filter out the frequency of the RF bias power supply. A low pass filter, which is commonly utilized in systems such as Smolanoff, would destroy all of the low frequency components of the pulses. With a band rejection filter, all of the pulsed DC power except that within the rejected band passes to the target. Therefore, far from not mattering which

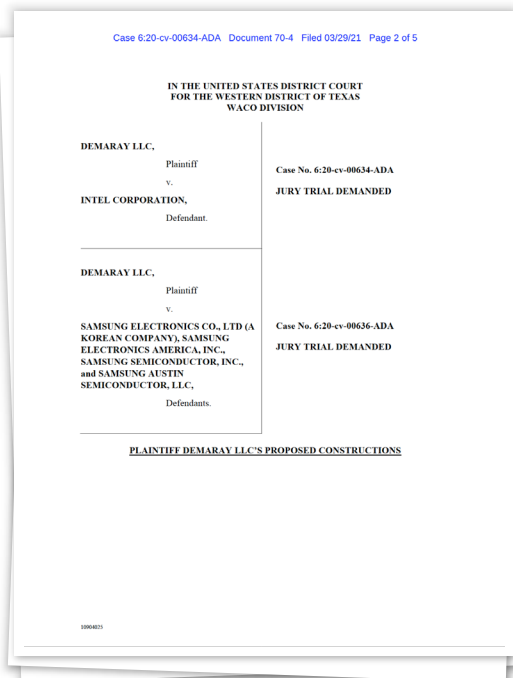
Dkt. 59 ('356 File History, part 7/7), 1386-87



# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band



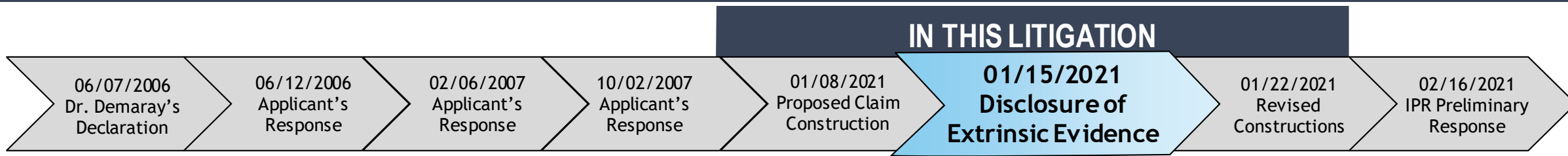
Demaray acknowledged that the NBRF “passes all of the frequencies ... except within a narrow band”



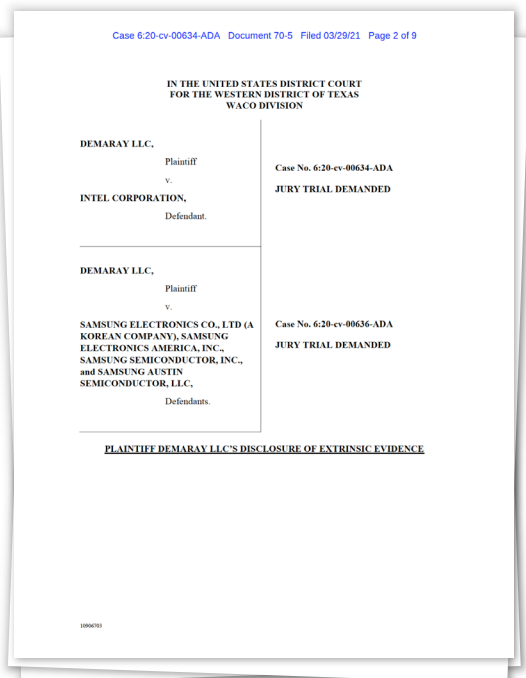
<p>“narrow band-rejection filter”</p>	<p>Plain and ordinary meaning</p> <p>or</p> <p>“filter that passes all of the frequencies of the power supply except within a narrow band”</p>
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Dkt. 70-4 (Demaray's Proposed Constructions), 3

# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band



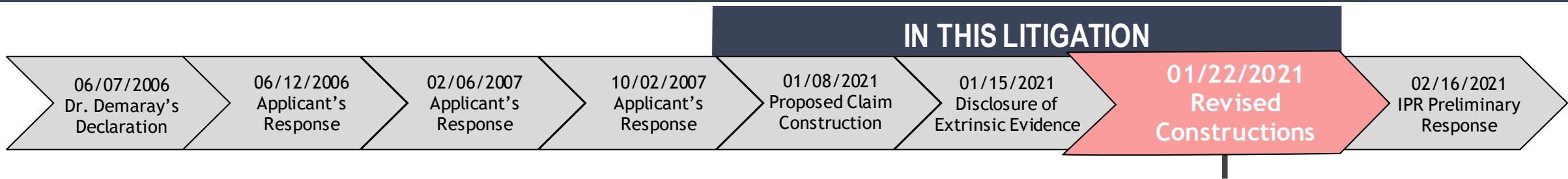
Demaray reiterated that the NBRF “passes all of the frequencies ... except within a narrow band”



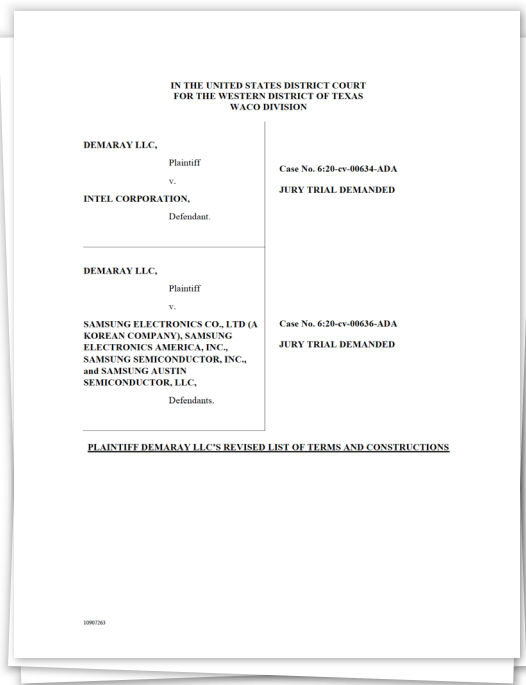
<p>“narrow band-rejection filter”</p>	<p>Plain and ordinary meaning</p> <p>or</p> <p>“filter that passes all of the frequencies of the power supply except within a narrow band”</p>
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Dkt. 70-5 (01/15/2021 Demaray's Disclosure of Extrinsic Evidence), 4

# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band



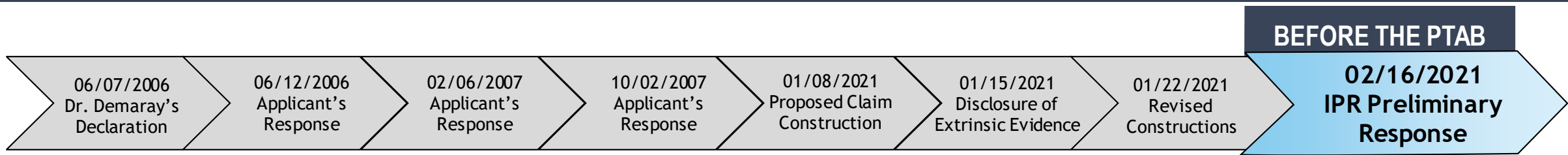
Demaray abandoned its prior position that the NBRF “passes all of the frequencies ... except within a narrow band”



“narrow band-rejection filter”	Plain and ordinary meaning
	or
	“filter which rejects a narrow band of frequencies”

(01/22/2021 Demaray's Revised Constructions), 3; Dkt. 76 (Joint Claim Construction Statement), 2

# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band

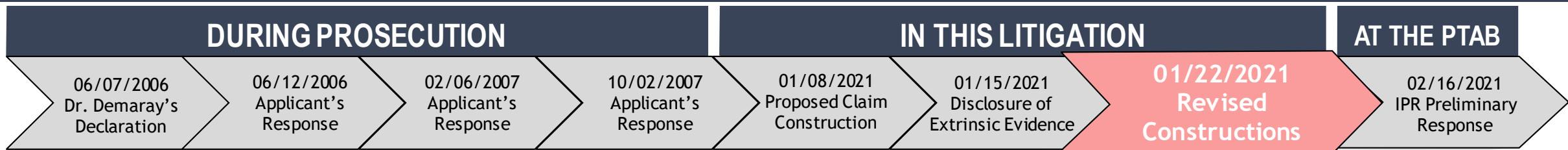


Demaray once again argued that the claimed filter “passes all of the frequencies ... except within a narrow band centered on the RF frequency of the RF bias”

In other words, even if Hirose’s filter were viewed as a narrow-band rejection filter, it is designed to operate or reject at a frequency that differs from the RF bias power supply to the substrate (*i.e.*, designed at 2.25 MHz as opposed to 2MHz of the RF power supply 15). *Id.*; Ex. 1006, 4:42-45 (RF bias power 15 is 2MHz). The inventors explained during prosecution that the claimed filter “(is) a filter that passes all of the frequencies of the [] power supply except within a narrow band centered on the RF frequency of the RF bias...” Ex. 1052 at 1130-31, 1134.

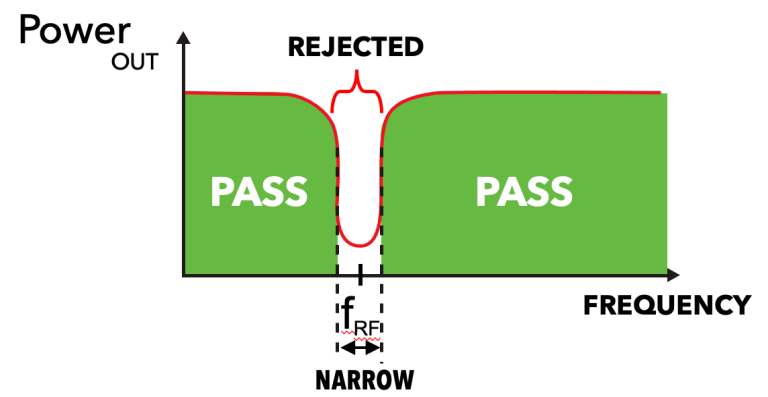
Dkt. 58-3 (IPR2021-00103, 02/16/2021 Demaray’s Preliminary Response), 24

# Demaray Has Repeatedly Defined NBRF (Just Like Defendants) As Passing All Frequencies Outside the Narrow Band



## Demaray's Definition

2MHz). The inventors explained during prosecution that the claimed filter "is a filter that passes all of the frequencies of the [ ] power supply except within a narrow band centered on the RF frequency of the RF bias..." Ex. 1052 at 1130-31, 1134. Dkt. 58-3 (IPR2021-00103, 02/16/2021 Demaray's Preliminary Response, citing to 06/07/2006 Demaray Declaration), 24



## Demaray's Litigation Proposal

Plain and ordinary meaning, or "filter which rejects a narrow band of frequencies"

(01/22/2021 Demaray's Revised Constructions), 3; Dkt. 76 (Joint Claim Construction Statement), 2



# Why Did Demaray Change its Proposal to Leave Open That the Narrow Band Rejection Filter Can Reject Other Frequencies?

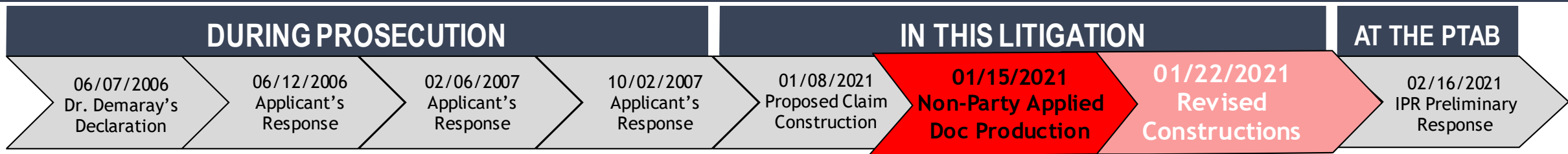


Exhibit #  
Miller 11  
02/09/21 - MP

FOR PART QUALIFICATION & CONTROL REQUIREMENTS, REFERENCE PQC ADDENDUM DOCUMENT FOR THIS ITEM REVISION. PART SPECIFICATION IS INCOMPLETE WITHOUT PQC ADDENDUM

Part Number	0190-41240
Revision	05
Title	[REDACTED]
ECO Releasing this Rev.	3026888
Original Document Author	Ken Smyth/Wenwen Liu

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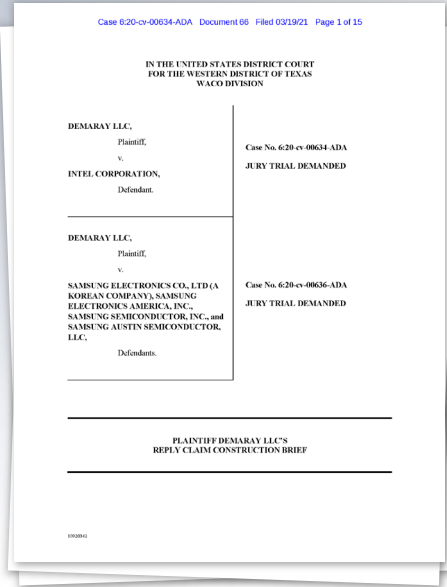
## Demaray's Litigation Proposal

Plain and ordinary meaning, or

“filter which rejects a narrow band of frequencies”

(01/22/2021 Demaray's Revised Constructions), 3;  
Dkt. 76 (Joint Claim Construction Statement), 2

# Demaray's New Arguments in Litigation



## Demaray's Litigation Argument

should address frequencies *passed* in addition to those *rejected*. Resp. 15. Rejecting and passing

frequencies are different subjects, and adding extraneous “passing” limitations would be improper.

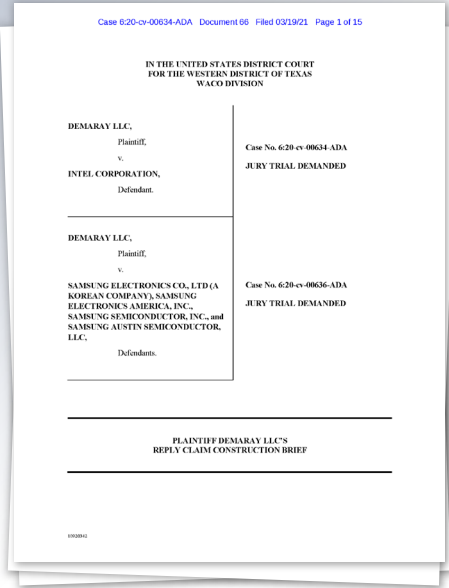
Defendants’ proposal that “[substantially] all frequencies outside of the narrow band” must be

passed is not required by the term’s plain meaning. Contextual claim language provides, for

Dkt. 66 (03/19/2021 Demaray’s Reply Br.), 7-8

# Demaray's New Arguments in Litigation Contradict Its Own Expert

Case 6:20-cv-00636-ADA Document 176-1 Filed 03/03/22 Page 57 of 148



## Demaray's Litigation Argument

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Dkt. 66 (03/19/2021 Demaray's Reply Br.), 7-8

## Demaray's Expert

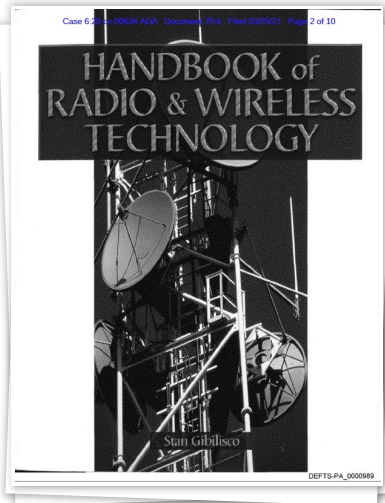
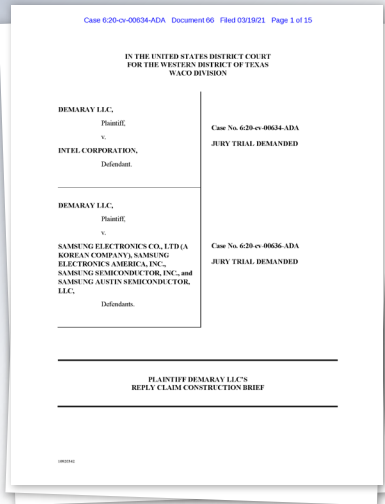
Q. And what would a POSITA then understand in terms of what that narrow band rejection filter passes? How would a POSITA describe or understand that?

A. **What it doesn't filter, it passes. That which is not filtered is passed.** You know, given—given the limitations of any circuit not being perfect.

Dkt. 58-7 (03/02/2021 Dr. Glew Depo. Tr.), 252:12-20



# Demaray's New Arguments in Litigation Contradict the Plain Meaning



## Demaray's Litigation Argument

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Dkt. 66 (03/19/2021 Demaray's Reply Br.), 7-8

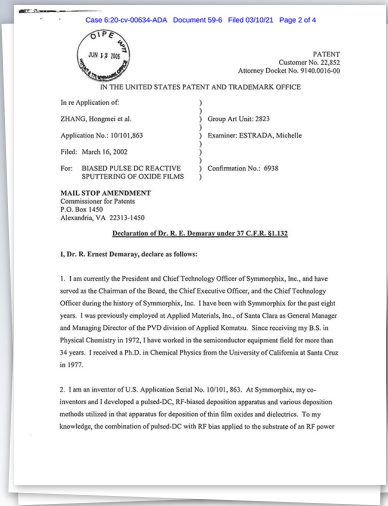
## Plain Meaning

### **Band-Rejection Filter**

**A band-rejection filter, also called a band-stop filter, is a resonant circuit designed to pass energy at all frequencies, except within a certain range.** The attenuation is greatest at the resonant frequency  $f_0$ , or between two limiting frequencies  $f_0$  and  $f_1$ . Figure 2-9E shows a simple

Dkt. 70-6 (Handbook of Radio and Wireless Technology (1999)), 63

# Demaray Cannot Sue Based on Filters it Disclaimed in Prosecution History



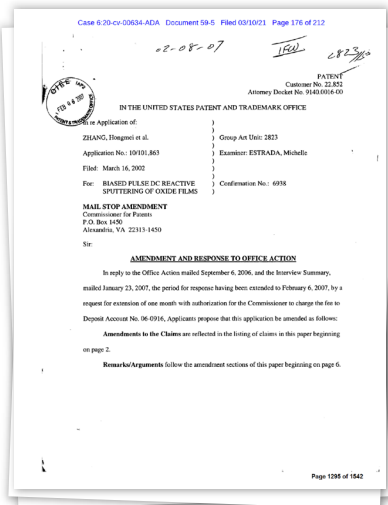
kHz to 300 KHz together with a pulse reverse time from 1.3 to 5.0  $\mu$ sec. Utilizing a band-pass filter between the pulsed-DC power supply and the plasma, however, will not protect the pulsed-DC power supply from the RF bias and will also unduly distort the square-wave of the pulsed-DC power signal applied to the target, which detrimentally affects the deposition conditions.

Disclaimed filter

1

2

Dkt. 59-6 (06/07/2006 Dr. Demaray Declaration), ¶ 3



Disclaimed filters

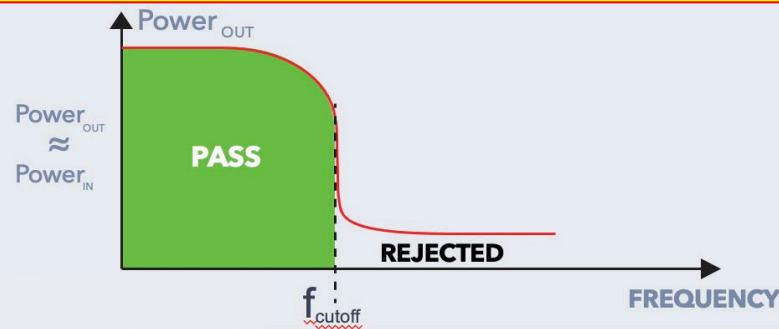
supply due to transmission of the RF power into the pulsed DC power supply. However, a conventional high or low pass filter blocks a portion of the pulsed DC frequency to the target and therefore the benefits of using pulsed DC power are lost. Applicants discovered that a narrow

Dkt. 59-5 ('356 File History, part 6/7, 02/06/2007 Applicant's Response), 1302

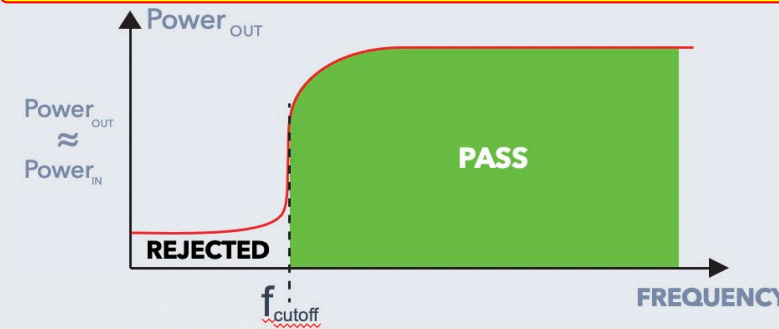


## Disclaimed Filters

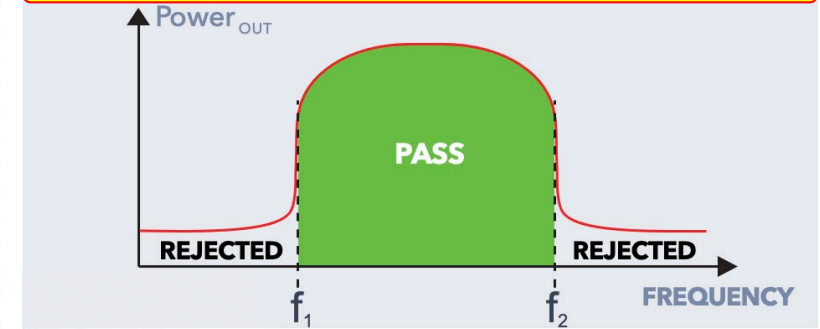
Low Pass Filter



High Pass Filter



Band Pass Filter



“A patentee may not state during prosecution that the claims do not cover a particular device and then change position and later sue a party who makes that same device for infringement.”

*Spring Window Fashions LP v. Novo Industries, L.P.*, 323 F.3d 989, 995 (Fed. Cir. 2003)

# Demaray's POM Interpretation of NBRF Rejects Frequencies Outside the Narrow Band

## Demaray's Litigation Argument

Resp. 15. The term (and Demaray's construction) defines rejection in a "narrowband," not mere broadband rejection typically seen with, *e.g.*, low-pass or high-pass filters alone. *See, e.g.*, Ex. 3 ('356 FH) at -1302 (distinguishing a narrow band rejection filter from "a conventional high or low pass filter"). That said, this is a "comprising" claim and a filter that is directed at rejecting frequencies in narrowband, but that is also engineered to do other things as well (*e.g.*, a dual-notch filter rejecting at a second frequency), certainly be encompassed by the claim term.

Dkt. 66 (03/19/2021 Demaray's Reply), 9

## Demaray's Statements During Prosecution

4. My co-inventors and I developed the band-rejection filter described in the specification and claimed in U.S. Application Serial No. 10/101, 863 to overcome the problem of catastrophic failure of the pulsed-DC power supply output electrometer circuit during operation. We discovered that a band-rejection filter, which is a filter that passes all of the frequencies of the square wave power supply except within a narrow band centered on the RF frequency of the RF bias, protected the pulsed-DC power supply from the RF energy while not distorting the pulses generated by the pulsed-DC power supply applied to the target.

Dkt. 59-6 (06/07/2006 Dr. Demaray's Declaration) at ¶ 4; *see also* Dkt. 59-5 (06/12/2006 Applicant's Response), 1130-1131; Dkt. 59-6 (02/06/2007 Applicant's Response), 1307; Dkt. 59 (10/02/2007 Applicant's Response), 1386-87; Dkt. 70-4 (01/08/2021 Demaray's Proposed Constructions), 3; Dkt. 70 (01/15/2021 Demaray's Disclosure of Extrinsic Evidence), 4; Dkt. 58-3 (02/16/2021 Demaray's IPR Preliminary Response), 24

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Dkt. 66 (03/19/2021 Demaray's Reply), 9

## Demaray's Proposal

~~Plain and ordinary meaning, or~~

"filter which rejects a narrow band of frequencies **but that is also engineered to do other things as well (such as reject at frequencies outside the narrow band)**"

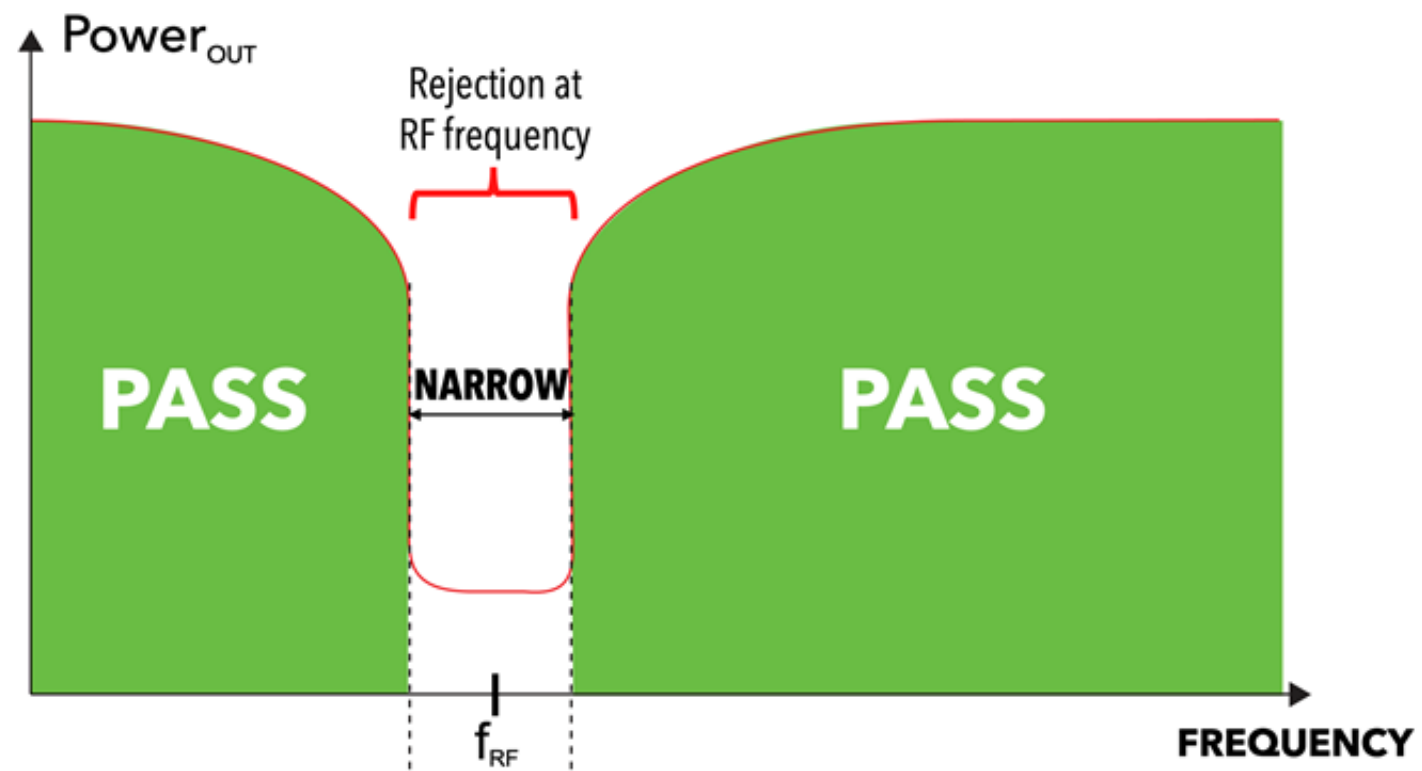
# Demaray's POM Interpretation of NBRF Rejects Frequencies Outside the Narrow Band

## Demaray's Original Proposal

## Demaray's POM Interpretation

“filter that passes all of the frequencies of the power supply except within a narrow band”

“filter which rejects a narrow band of frequencies but that is also engineered to do other things as well (such as reject at frequencies outside the narrow band)”





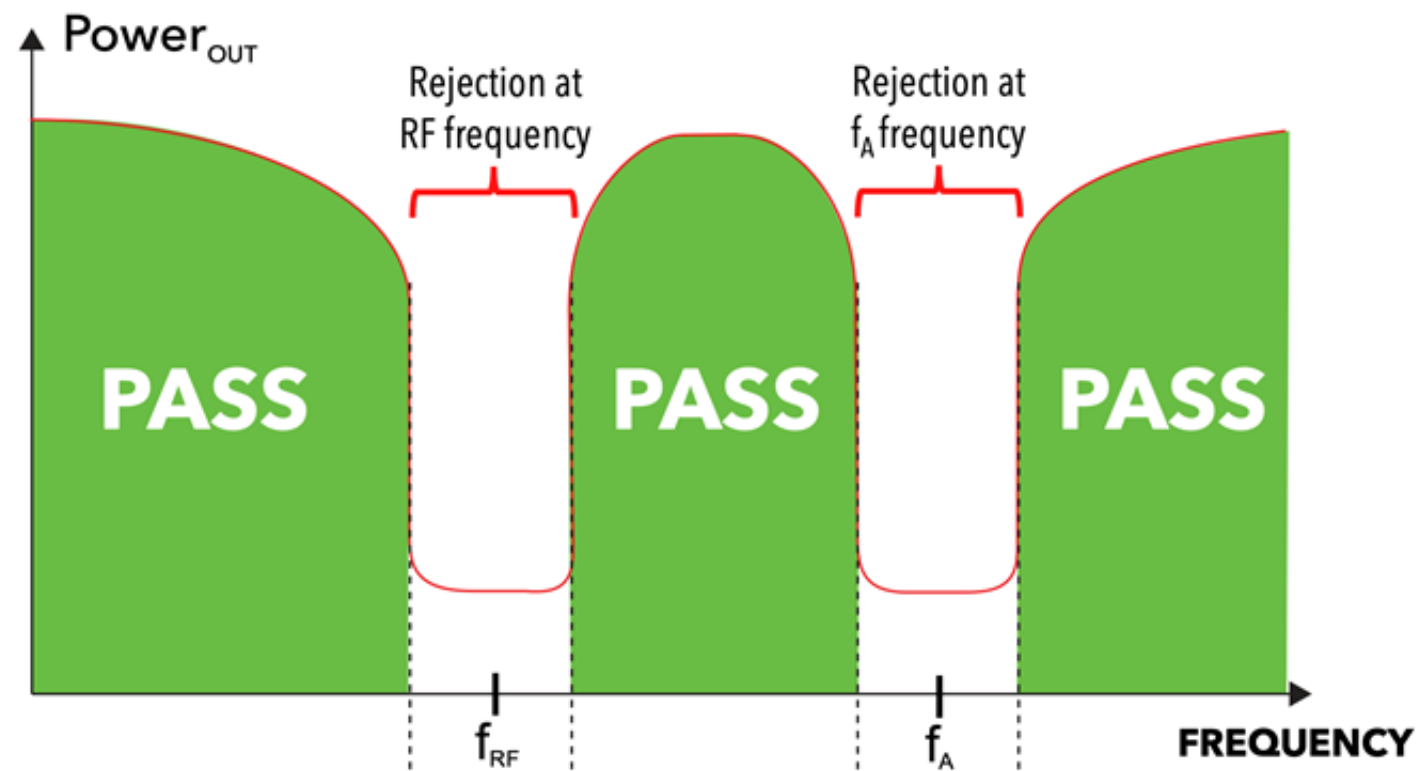
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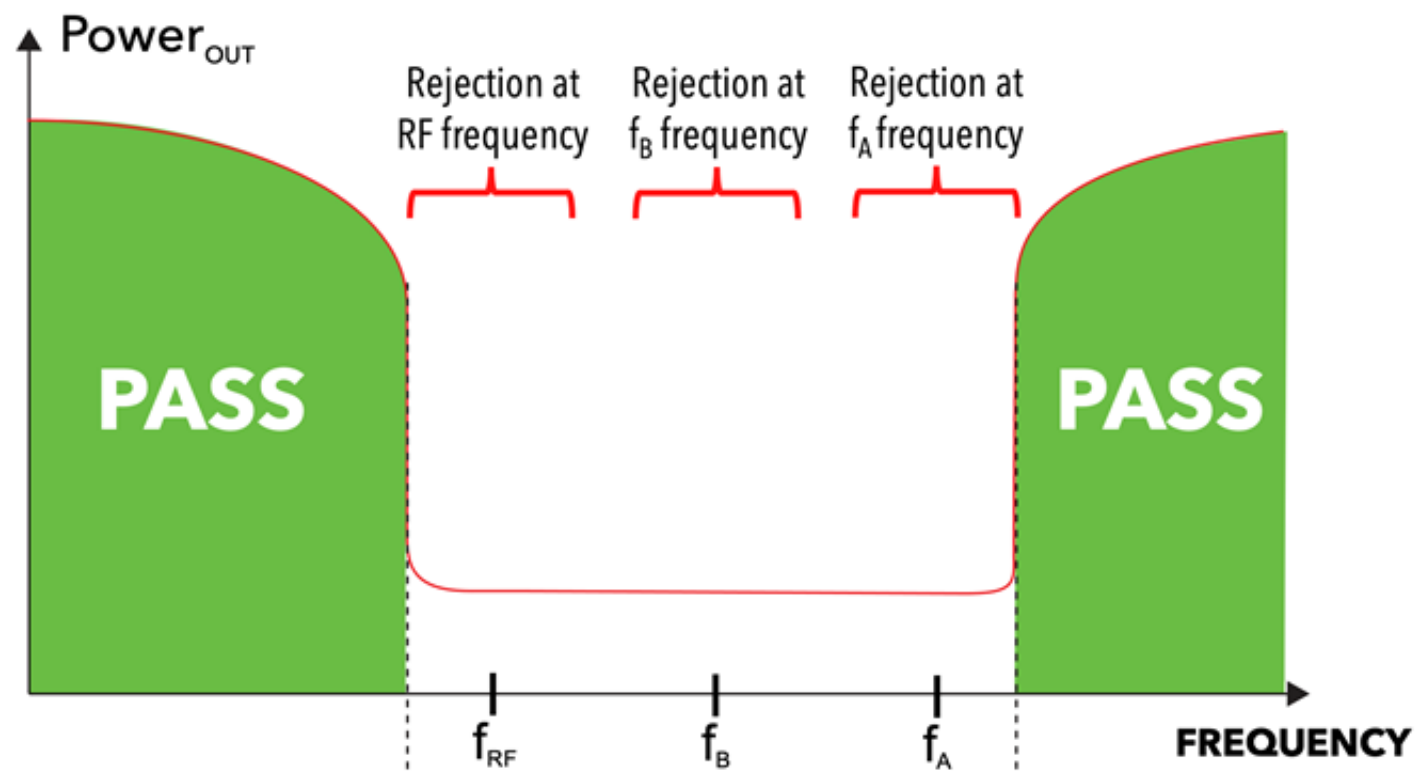
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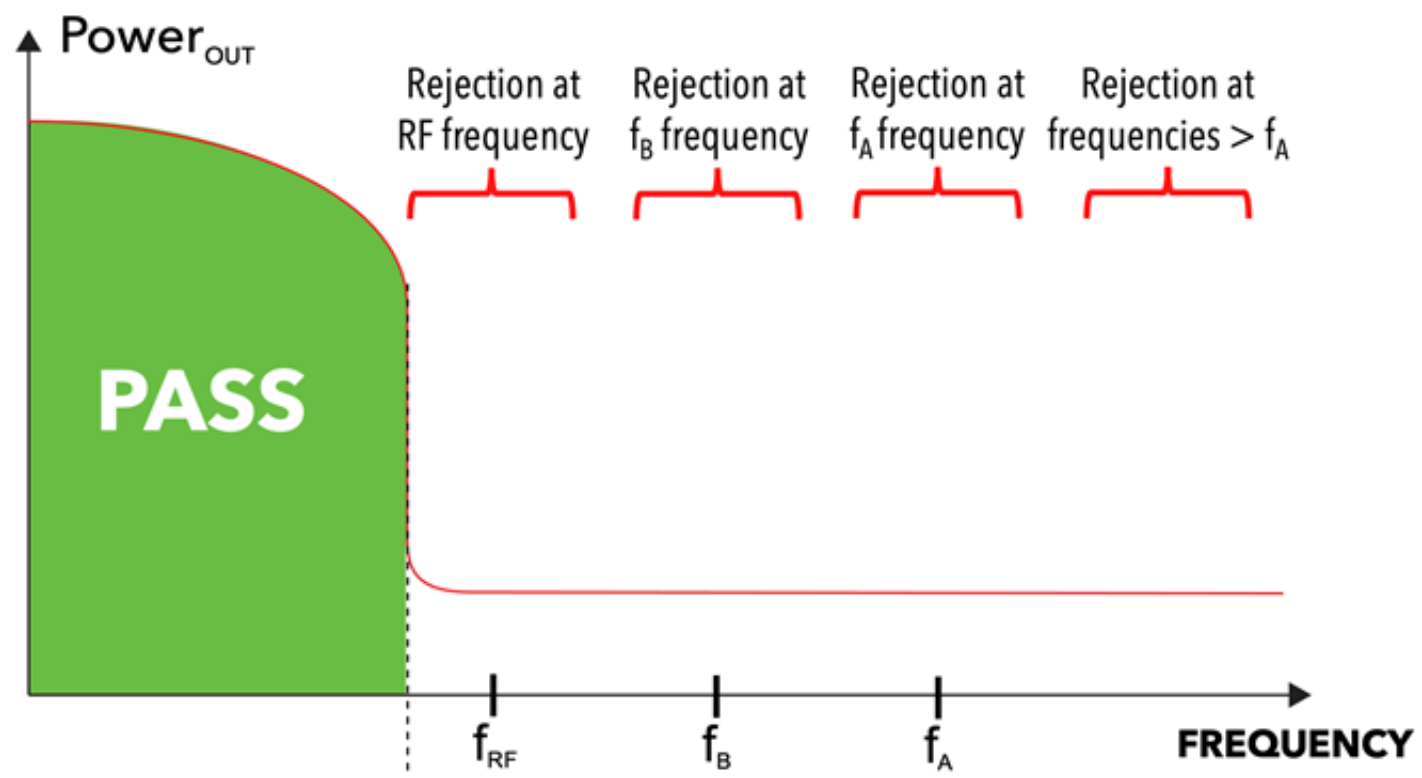
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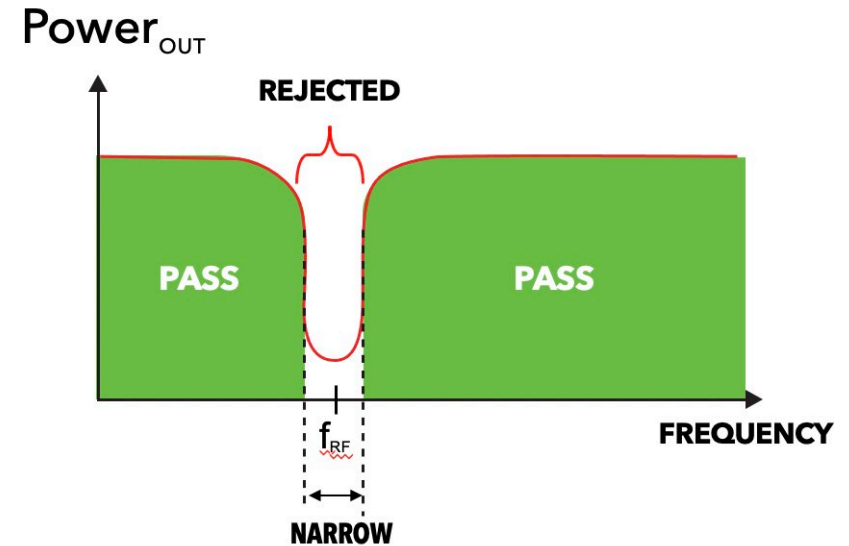
# Demaray's POM Interpretation of NBRF Seeks to Recapture Disclaimed Filters

## Demaray's Definition

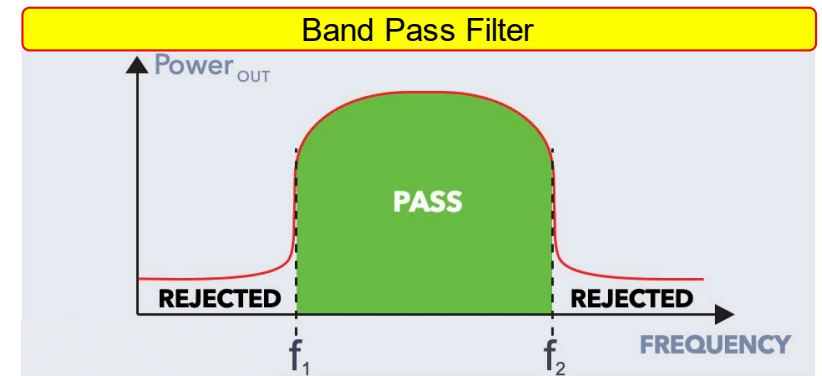
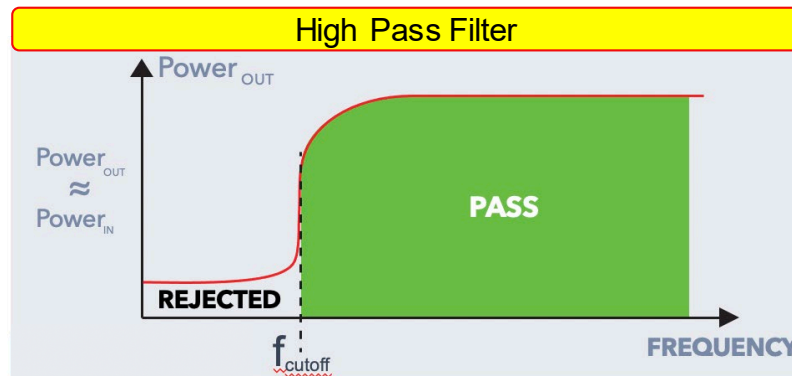
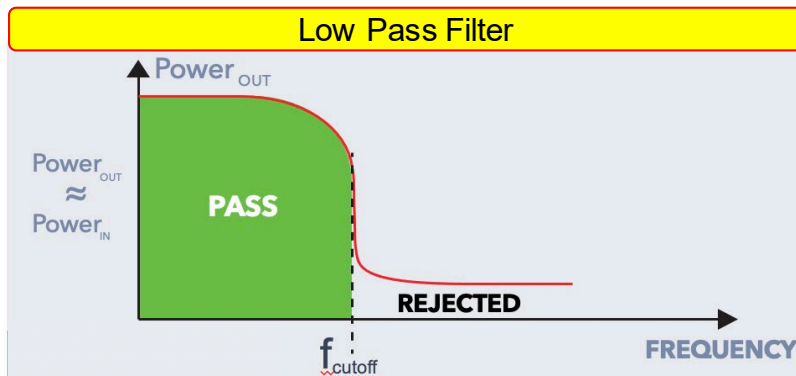
2MHz). The inventors explained during prosecution that the claimed filter "is a filter that passes all of the frequencies of the [ ] power supply except within a narrow band centered on the RF frequency of the RF bias...." Ex. 1052 at 1130-31, 1134.

Dkt. 58-3 (IPR2021-00103, 02/16/2021 Demaray's Preliminary Response), 24

## Claimed NBRF



## Disclaimed Filters



# Demaray’s POM Interpretation of NBRF Rejects Frequencies Outside the Narrow Band

Demaray’s alleged basis for broadening the claim limitation is contrary to law

pass filter”). That said, this is a “comprising” claim and a filter that is directed at rejecting

frequencies in narrowband, but that is also engineered to do other things as well (e.g., a dual-notch

filter rejecting at a second frequency), certainly be encompassed by the claim term.

Dkt. 66 (03/19/2021 Demaray’s Reply), 9



“Comprising, while permitting additional elements not required by a claim, does not remove the limitations that are present.”

*Power Mosfet Techs. L.L.C. v. Siemens AG*, 378 F.3d 1396, 1409 (Fed. Cir. 2004) (internal quotes omitted)



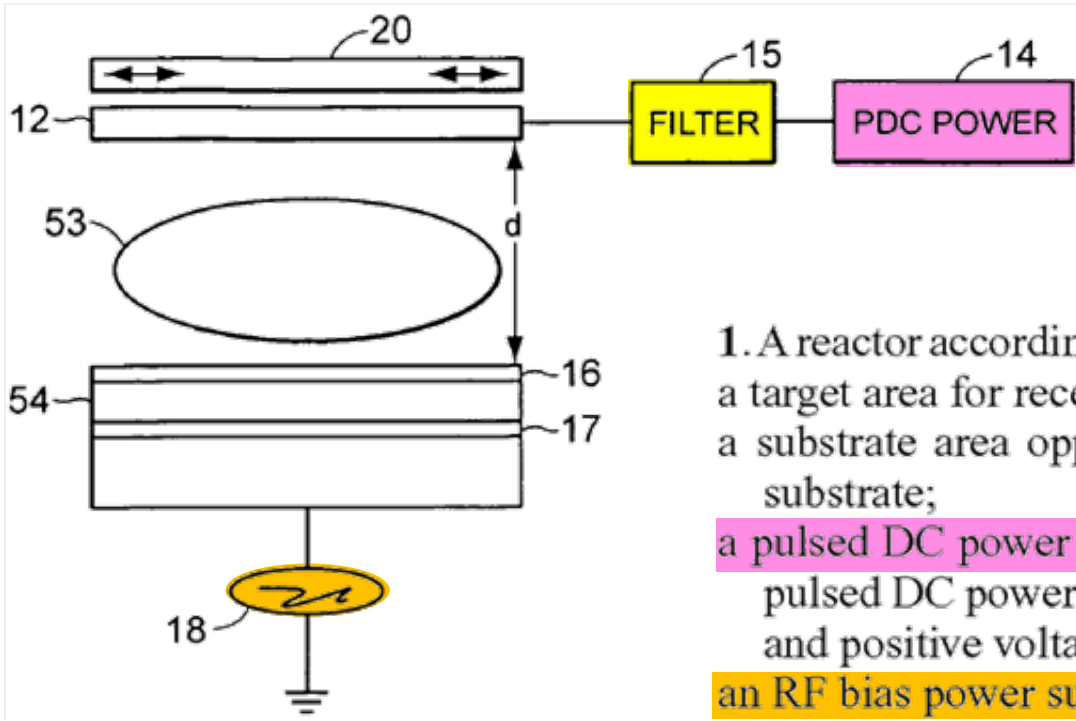
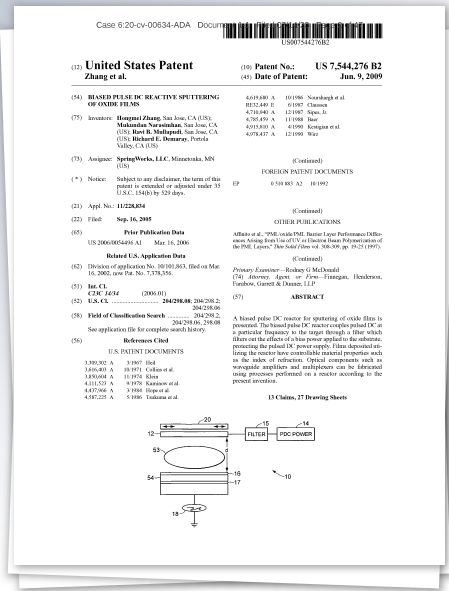
“[C]omprising is not a weasel word with which to abrogate claim limitations.”

*Dippin’Dots, Inc. v. Mosey*, 476 F.3d 1337, 1343 (Fed. Cir. 2007) (internal quotes omitted)



# NBRF Must Pass All Frequencies Outside the Narrow Band to Not Distort the Shape of the "pulsed DC power"

## Three Key Interrelated Elements of Alleged Invention



1. A reactor according to the present invention, comprising:
  - a target area for receiving a target;
  - a substrate area opposite the target area for receiving a substrate;
  - a pulsed DC power supply coupled to the target area, the pulsed DC power supply providing alternating negative and positive voltages to the target;
  - an RF bias power supply coupled to the substrate; and
  - a narrow band-rejection filter that rejects at a frequency of the RE bias power supply coupled between the pulsed DC power supply and the target area.

# NBRF Must Pass All Frequencies Outside the Narrow Band to Not Distort the Shape of the “pulsed DC power”

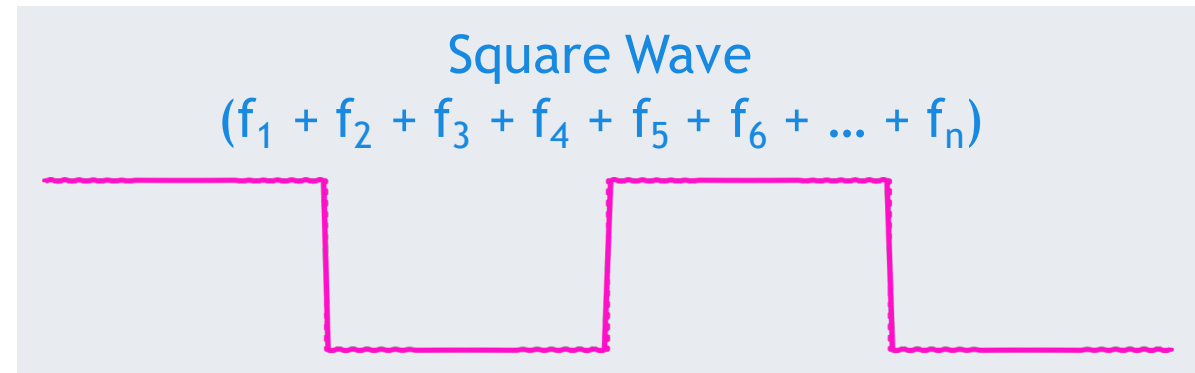
## Applicant’s Response

Although it is true that “the filter is going to work at certain frequencies,” as suggested by the Examiner, the recited “band rejection filter” works at the frequency of the RF bias supply and blocks only a narrow band of frequencies around the frequency of the RF bias supply. This allows the square wave pulse of the DC power, which is formed of all frequencies both higher and lower than the biased frequency, to be transmitted through the filter to the target. Otherwise, the pulse that would reach the target is distorted so that the benefits of the pulsed DC power are not realized. Therefore, utilization of a band rejection filter at the frequency of the bias power is neither taught nor obvious from the teachings of Smolanoff. Furthermore, use of a band rejection filter at the frequency of the bias power places a distinct limitation on the claim.

Dkt. 59-5 ('356 File History, part 6/7, Applicant’s Response), 1307

Given that:

- The pulse wave is “formed of all frequencies both higher and lower than the [RF] bias[] frequency”



# NBRF Must Pass All Frequencies Outside the Narrow Band to Not Distort the Shape of the “pulsed DC power”

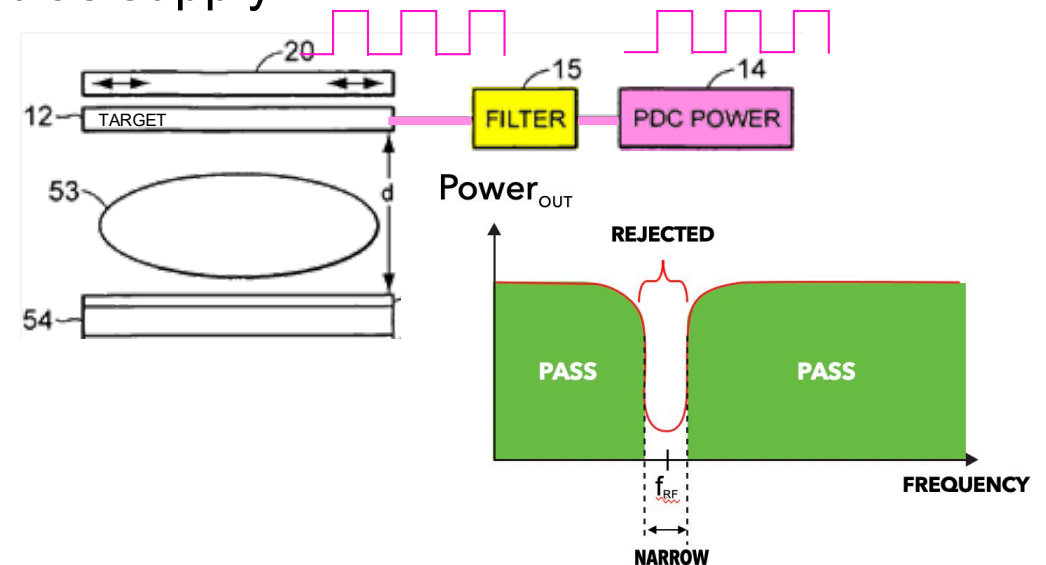
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Dkt. 59-5 (’356 File History, part 6/7, Applicant’s Response), 1307

Given that:

- The pulse wave is “formed of all frequencies both higher and lower than the [RF] bias[] frequency”
- The NBRF “blocks only a narrow band of frequencies around the frequency of the RF bias supply”



# NBRF Must Pass All Frequencies Outside the Narrow Band to Not Distort the Shape of the “pulsed DC power”

## Applicant’s Response

Although it is true that “the filter is going to work at certain frequencies,” as suggested by the Examiner, the recited “band rejection filter” works at the frequency of the RF bias supply and blocks only a narrow band of frequencies around the frequency of the RF bias supply. This allows the square wave pulse of the DC power, which is formed of all frequencies both higher and lower than the biased frequency, to be transmitted through the filter to the target. **Otherwise, the pulse that would reach the target is distorted so that the benefits of the pulsed DC power are not realized.** Therefore, utilization of a band rejection filter at the frequency of the bias power is neither taught nor obvious from the teachings of Smolanoff. Furthermore, use of a band rejection filter at the frequency of the bias power places a distinct limitation on the claim.

Dkt. 59-5 (’356 File History, part 6/7, Applicant’s Response), 1307

Given that:

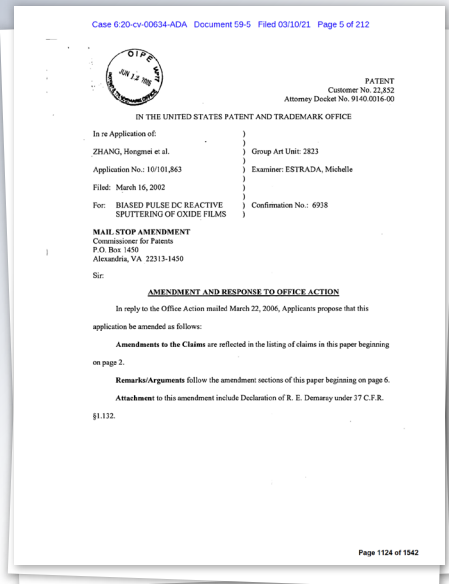
- a. The pulse wave is “formed of all frequencies both higher and lower than the [RF] bias[] frequency”
- b. The NBRF “blocks only a narrow band of frequencies around the frequency of the RF bias supply”

The result is:

- c. The pulsed DC is **not** “distorted so that the **benefits** of the pulsed DC power are [] **realized**”

# NBRF Must Pass All Frequencies Outside the Narrow Band to Not Distort the Shape of the “pulsed DC power”

## Applicant’s Response



of the bias power,” as is recited in claim 21. (See, Office Action, page 5). As stated in the Declaration of Ernest Demeray filed with this amendment under 37 C.F.R. §1.132, the filter protecting the pulsed DC power supply from the RF power of the bias is an aspect of the claimed invention. **The filter must pass the pulsed DC signal without unduly affecting the shape of that signal while rejecting the RF power. Therefore, the filter passes all frequencies except for the frequency of the bias power itself.** As stated in the Declaration of Ernest Demeray, other filter designs resulted in a distortion of the pulsed DC signal or in leakage of RF power back to the pulsed DC power supply -- resulting in the catastrophic failure of the power supply.

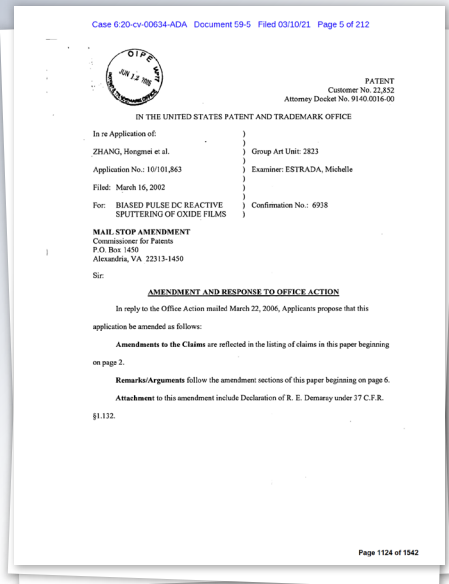
Dkt. 59-5 ('356 File History, part 6/7, 06/12/2006 Applicant’s Response), 1130-31

Passing all frequencies outside the narrow band is a “must”



# NBRF Must Pass All Frequencies Outside the Narrow Band to Not Distort the Shape of the “pulsed DC power”

## Applicant’s Response



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Dkt. 59-5 ('356 File History, part 6/7, 06/12/2006 Applicant’s Response), 1130-31

# NBRF Must Pass All Frequencies Outside the Narrow Band to Not Distort the Shape of the “pulsed DC power”

## Applicant’s Response

Additionally, in order for the pulsed DC power applied to the target to be useful, the

pulsed DC power must include substantially all of its Fourier constituents, and therefore only a

band rejection filter that filters out a specific narrow band of filters can be utilized. Further, in

order that the pulsed DC power be protected from the RF bias power supply, the band rejection

filter must be set to filter out the frequency of the RF bias power supply. A low pass filter,

which is commonly utilized in systems such as Smolanoff, would destroy all of the low

frequency components of the pulses. With a band rejection filter, all of the pulsed DC power

except that within the rejected band passes to the target. Therefore, far from not mattering which

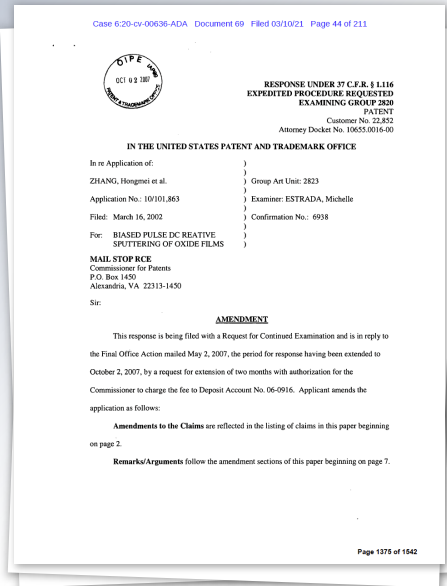
filter is used, as the Examiner opines, it is extremely important that the filter be a band rejection

filter that filters out the frequency of the RF bias power, as is recited in claims 21, 43, and 51.

For at least this reason, claims 21, 43, and 51 are allowable over the combination of Smolanoff

and Fu.

Dkt. 59 ('356 File History, part 7/7, 10/02/2007 Applicant’s Response), 1386-87

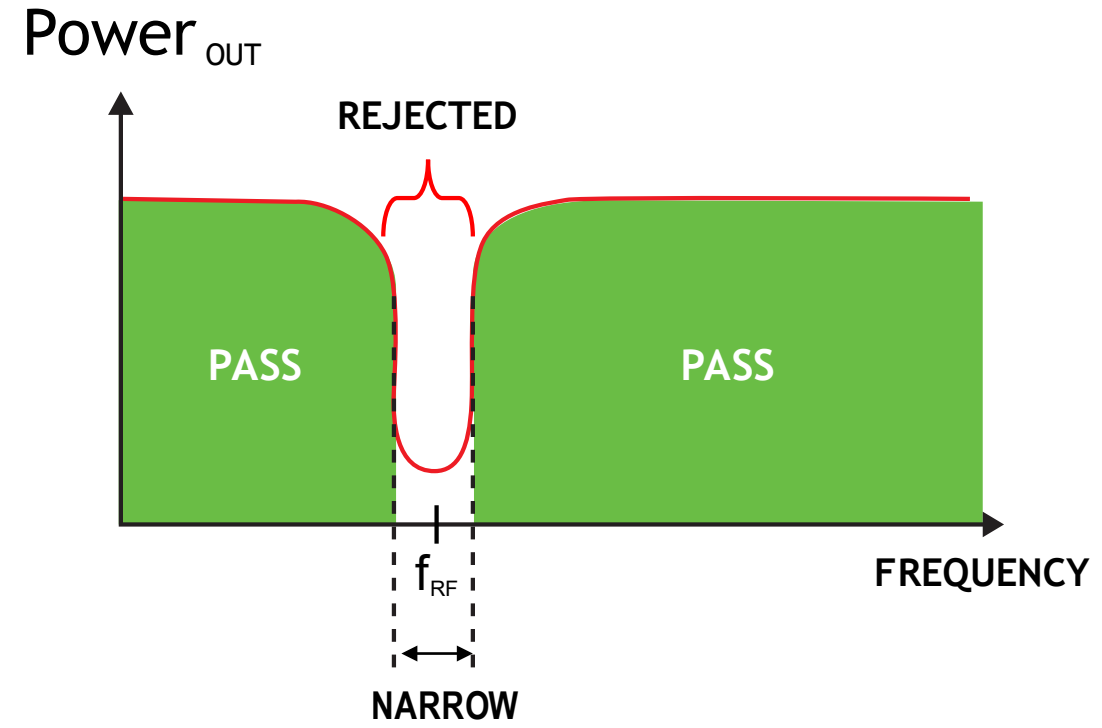


# NBRF Defined to Pass All Frequencies Outside the Narrow Band

## Demaray's Definition

2MHz). The inventors explained during prosecution that the claimed filter "is a filter that passes all of the frequencies of the [ ] power supply except within a narrow band centered on the RF frequency of the RF bias..." Ex. 1052 at 1130-31, 1134.

Dkt. 58-3 (IPR2021-00103, 02/16/2021 Demaray's Preliminary Response), *citing to 06/07/06 Demaray Declaration*, 24



**“A method of depositing a film on an insulating substrate, comprising”**

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'657 Patent, Claim 1 Preamble

# The Meaning of “substrate”

Limitation	Court’s Preliminary Construction	Demaray’s Proposal
“substrate”	Plain-and-ordinary meaning, which includes, but is not limited to a wafer coated with an insulator	Plain and ordinary meaning OR <b><u>“material that provides the surface on which something is deposited or inscribed, for example a silicon wafer used to manufacture integrated circuits”</u></b>



**Court’s Tentative Construction:** Plain and ordinary meaning, which includes, but is not limited to a wafer coated with an insulator

**The dispute fine-tuned:** Can the plain and ordinary meaning of “substrate” as used in the claimed “insulating substrate” be any “material that provides the surface on which something is deposited or inscribed”?

In other words, can an “insulating substrate” be any type of substrate having one thin film that is insulating?

# Asserted Claim Requires “an insulating substrate”

1. A method of depositing a film on an insulating substrate, comprising:  
providing a process gas between a conductive target and the substrate;  
providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;  
providing an RF bias at a frequency that corresponds to the narrow band rejection filter to the substrate;  
providing a magnetic field to the target; and  
reconditioning the target;  
wherein preconditioning the target includes reactive sputtering in the metallic mode and then reactive sputtering in the poison mode.

'657 Patent, Claim 1

# Non-Asserted Claim Requires Any Type of “substrate”

“an *insulating film* on a substrate”

2. A method of depositing an insulating film on a substrate, comprising:

- providing a process gas between a target and a substrate;
- providing pulsed DC power to the target through a narrow band rejection filter such that the voltage on the target alternates between positive and negative voltages;
- providing an RF bias that corresponds to the narrow band rejection filter to the substrate; and
- providing a magnetic field to the target;

wherein an oxide material is deposited on the substrate, and the insulating film is formed by reactive sputtering in a mode between a metallic mode and a poison mode.

'657 Patent, Claim 2

## [Any Type of] Substrate

Substrate 16 can be a solid, smooth surface. Typically, substrate 16 can be a silicon wafer or a silicon wafer coated with a layer of silicon oxide formed by a chemical vapor deposition process or by a thermal oxidation process. Alternatively, substrate 16 can be a glass, such as Corning 1737 (Corning Inc., Elmira, N.Y.), a glass-like material, quartz, a metal, a metal oxide, or a plastic material. Substrate 16 can

'657 Patent, 7:62-8:1

silicon substrate

glass substrate

metal substrate

# Asserted Claim Requires “an insulating substrate” — Not Any Type of “substrate”

## Asserted Claim

“an *insulating substrate*”

1. A method of depositing a film on **an insulating substrate**, comprising:

- providing a process gas between a conductive target and **the substrate**;
- providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;
- providing an RF bias at a frequency that corresponds to the narrow band rejection filter to **the substrate**;
- providing a magnetic field to the target; and
- reconditioning the target;

wherein reconditioning the target includes reactive sputtering in the metallic mode and then reactive sputtering in the poison mode.

'657 Patent, Claim 1

## Non-Asserted Claim

“an *insulating film on a substrate*”

2. A method of depositing **an insulating film on a substrate**, comprising:

- providing a process gas between a target and **a substrate**;
- providing pulsed DC power to the target through a narrow band rejection filter such that the voltage on the target alternates between positive and negative voltages;
- providing an RF bias that corresponds to the narrow band rejection filter to **the substrate**; and
- providing a magnetic field to the target;

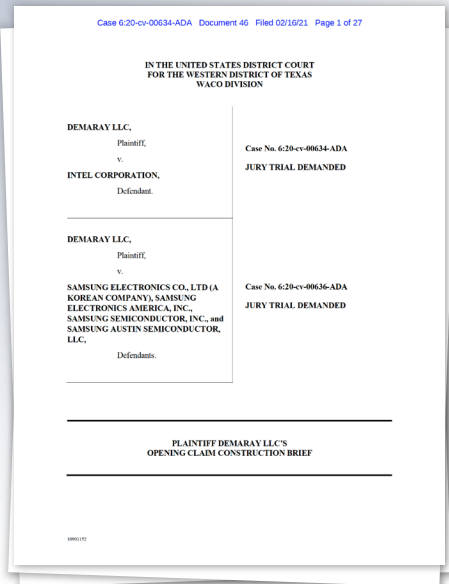
wherein an oxide material is deposited on **the substrate**, and **the insulating film** is formed by reactive sputtering in a mode between a metallic mode and a poison mode.

'657 Patent, Claim 2



**“In the absence of any evidence to the contrary, *we must presume that the use of these different terms in the claims connotes different meanings.*”**

# Demaray Replaces “insulating substrate” With Any Type of “substrate”



Defendants’ position disregards the patents’ teaching that the claimed methods can be used

with “any type” of substrate. Ex. 1, 2:61–62. Defendants’ position also contradicts numerous

Dkt. 46 (Demaray’s Opening Brief), 6



# Demaray's POM of "substrate": Improperly Allows "insulating substrate" to Encompass Any Type of "Substrate" Having One Insulating Layer of Material

**"insulating [Court's construction of 'substrate']"**

**insulating [plain and ordinary meaning, which includes, but is not limited to a wafer coated with an insulator]**

**INSERTING DEMARAY'S POM:**

**insulating [material that provides the surface on which something is deposited or inscribed, which includes, but is not limited to a wafer coated with an insulator]**

**CONDUCTING METAL SUBSTRATE**



Parties agree this is a "substrate"

# Demaray's POM of "substrate": Improperly Allows "insulating substrate" to Encompass Any Type of "Substrate" Having One Insulating Layer of Material

"insulating [Demaray's 'substrate' POM]"

**insulating [material that provides the surface on which something is deposited or inscribed, which includes, but is not limited to a wafer coated with an insulator]**

CONDUCTING METAL SUBSTRATE

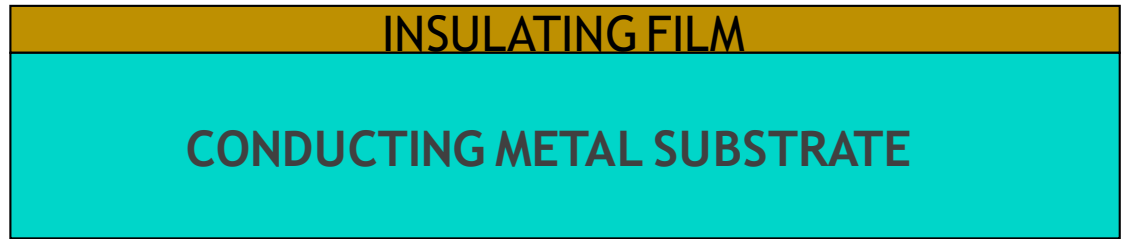


Parties agree this is a "substrate"

# Demaray's POM of "substrate": Improperly Allows "insulating substrate" to Encompass Any Type of "Substrate" Having One Insulating Layer of Material

"insulating [Demaray's 'substrate' POM]"

**insulating [material that provides the surface on which something is deposited or inscribed, which includes, but is not limited to a wafer coated with an insulator]**

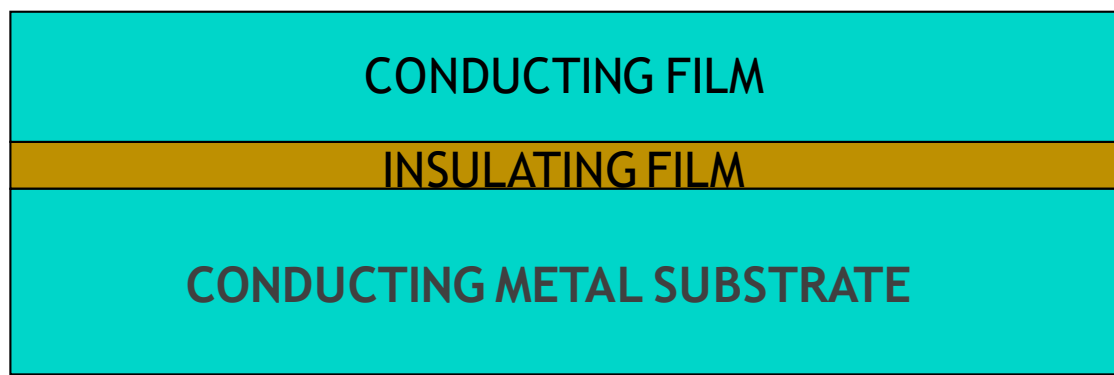


**insulating substrate  
according to Demaray**

# Demaray's POM of "substrate": Improperly Allows "insulating substrate" to Encompass Any Type of "Substrate" Having One Insulating Layer of Material

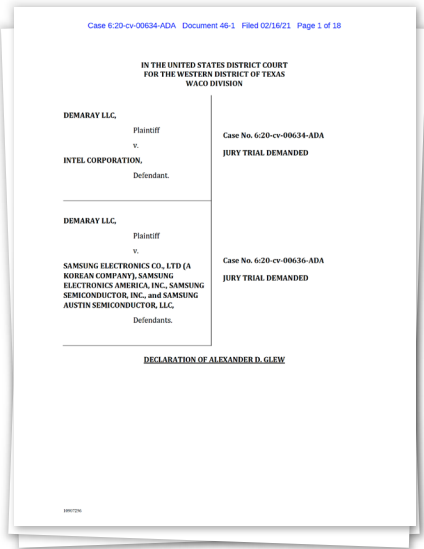
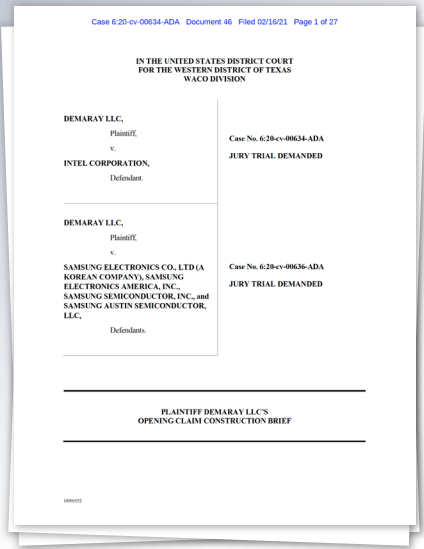
"insulating [Demaray's 'substrate' POM]"

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insulating substrate according to Demaray

# Demaray Replaces “insulating substrate” With Any Type of “substrate”



Defendants’ position disregards the patents’ teaching that the claimed methods can be used

with “any type” of substrate. Ex. 1, 2:61–62. Defendants’ position also contradicts numerous

■ ■ ■

(cls. 41 & 81: “wherein the substrate includes a transistor structure.”). Thus, any construction that suggests the substrate must be monolithic or entirely non-conductive is contrary to both the intrinsic record and the technology at issue. Glew, ¶¶ 35-37.

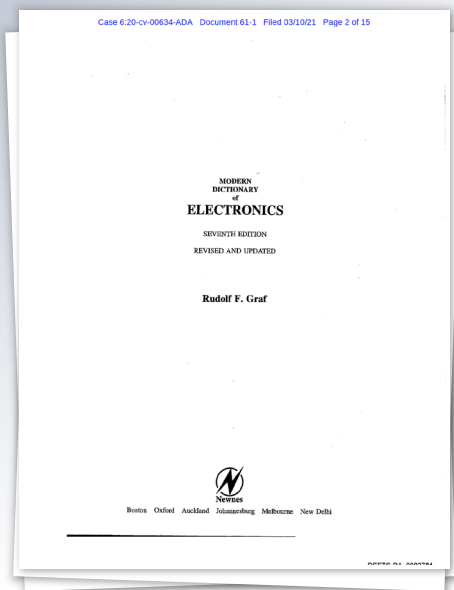
Dkt. 46 (Demaray’s Opening Brief), 6

37. In addition, as discussed above, pure silicon is an insulating material. In semiconductor manufacturing, the silicon is doped to create a lower resistance semiconductor material. The doped silicon wafer contains striations of layers that exhibit differing degrees of insulating properties and conductive properties resulting from the doping. A POSITA would thus consider silicon wafers used in the industry to be insulating substrates to the extent they are not considered monolithic.

Dkt. 46–1 (Glew Declaration), ¶ 37

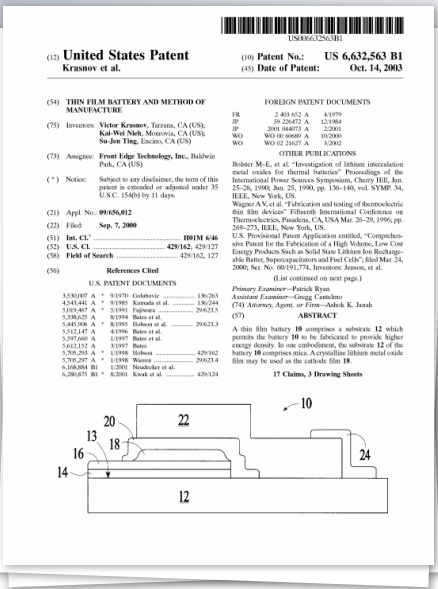


# Silicon is a Semiconducting Material



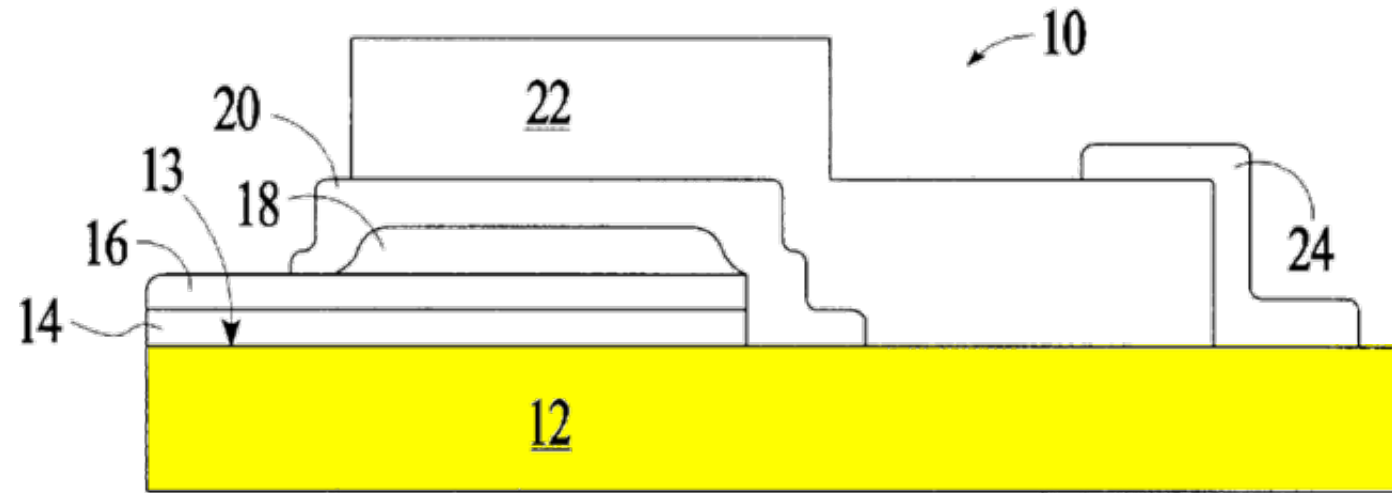
**semiconductor**— 1. A class of materials, such as silicon and germanium, whose electrical properties lie between those of conductors (such as copper and aluminum) and insulators (such as glass and rubber), in which the electrical charge carrier concentration increases with increasing temperature over some temperature range.

Dkt. 61-1 (Modern Dictionary of Electronics (1999)), 2796.



## Intrinsic Evidence

present invention is illustrated in FIG. 1. The battery 10 is formed on a substrate 12 which can be an insulator, a semiconductor, or a conductor. The substrate 12 should also have sufficient mechanical strength to support the thin films during processing or operational temperatures. For example, the substrate 12 can comprise silicon dioxide, aluminum oxide, titanium, or a polymer.



U.S. Pat. 6,632,563, 2:46-48, Fig. 1  
(cited on face of Patents-in-Suit)

# Demaray's POM of "substrate": Improperly Allows "insulating substrate" to Encompass Any Type of "Substrate" Having One Insulating Layer of Material

"insulating [Demaray's 'substrate' POM]"

***insulating [material that provides the surface on which something is deposited or inscribed, which includes, but is not limited to a wafer coated with an insulator]***

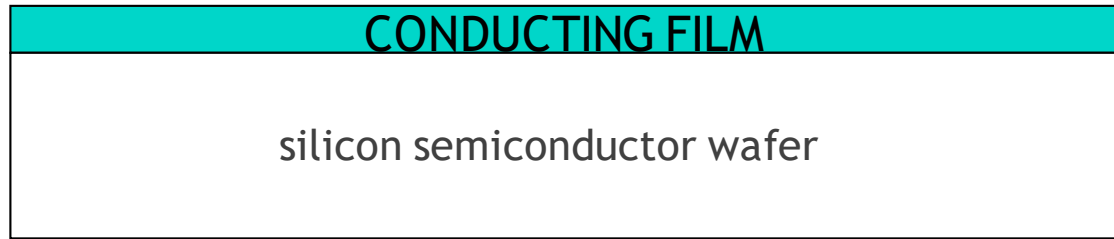
silicon semiconductor wafer

***insulating substrate according to Demaray***

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"insulating [Demaray's 'substrate' POM]"

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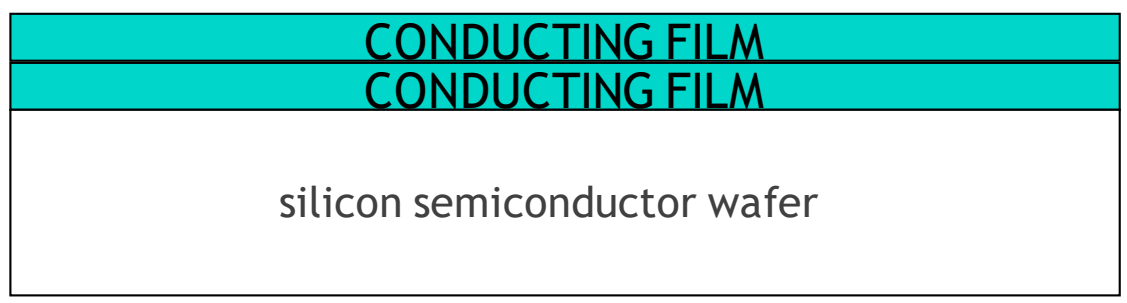


**insulating substrate  
according to Demaray**

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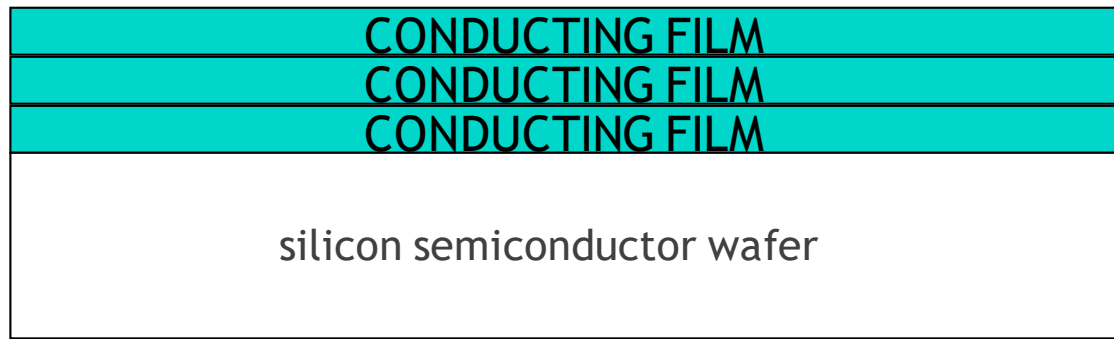
**insulating substrate  
according to Demaray**



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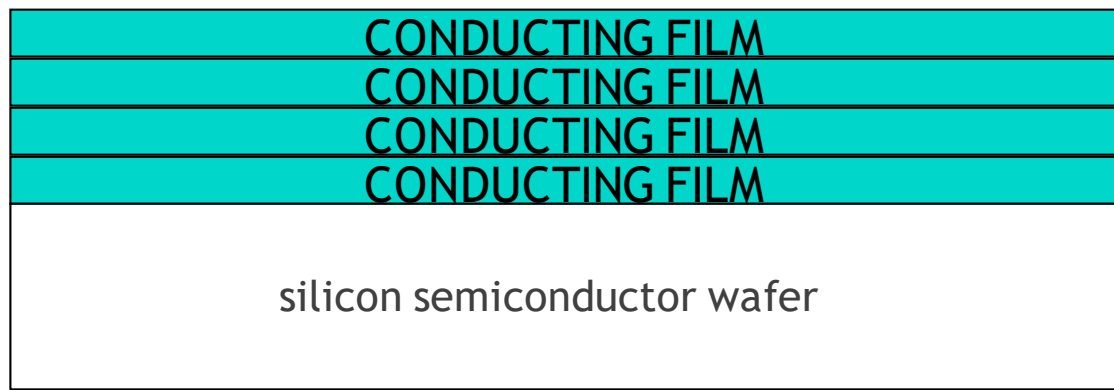


**insulating substrate  
according to Demaray**

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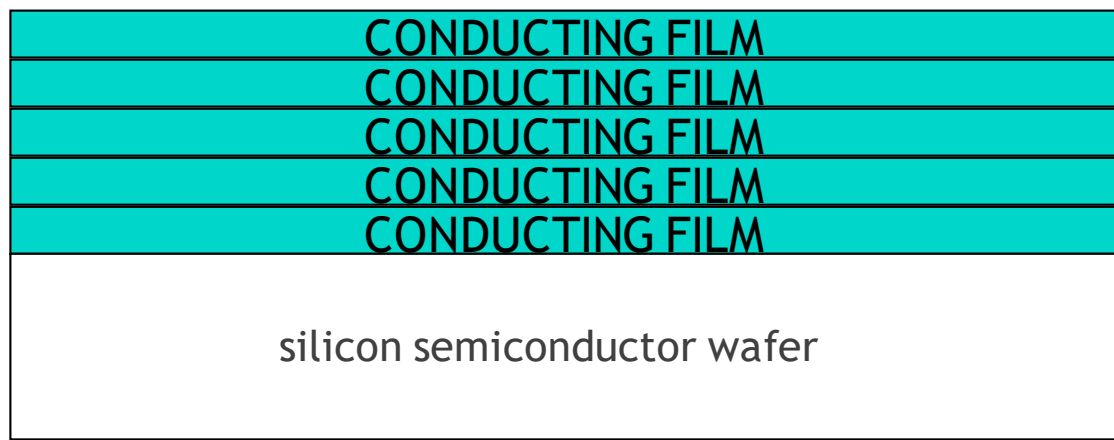


**insulating substrate according to Demaray**

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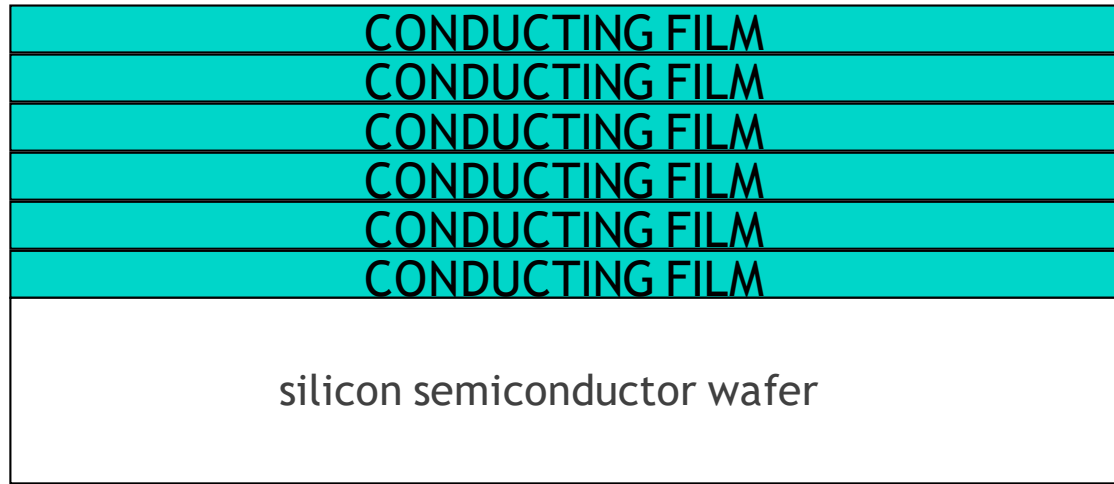


**insulating substrate according to Demaray**

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**insulating substrate  
according to Demaray**

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"insulating [Demaray's 'substrate' POM]"

**insulating [material that provides the surface on which something is deposited or inscribed, which includes, but is not limited to a wafer coated with an insulator]**

INSULATING GLASS SUBSTRATE



Parties agree this is an "insulating substrate"



# Demaray's POM of "substrate": Improperly Allows "insulating substrate" to Encompass Any Type of "Substrate" Having One Insulating Layer of Material

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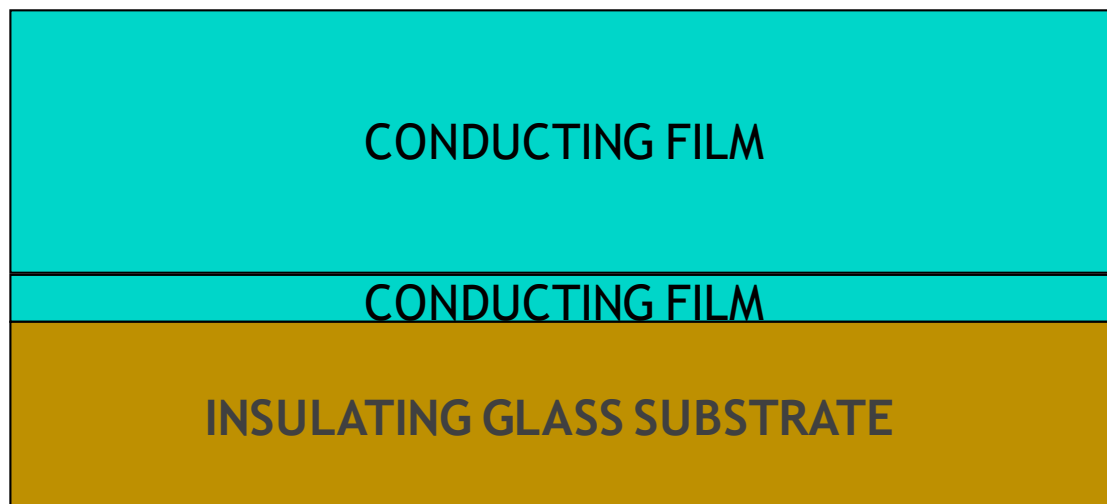


**insulating substrate  
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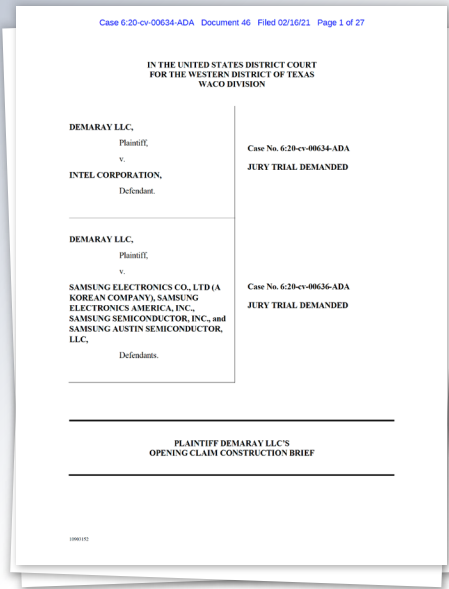
**insulating [material that provides the surface on which something is deposited or inscribed, which includes, but is not limited to a wafer coated with an insulator]**



**insulating substrate  
according to Demaray**

# Demaray Mischaracterizes Claim 1 and the Specification

Case 6:20-cv-00636-ADA Document 176-1 Filed 03/03/21 Page 102 of 148



Defendants' position disregards the patents' teaching that the claimed methods can be used

with "any type" of substrate. Ex. 1, 2:61–62. Defendants' position also contradicts numerous preferred embodiments involving substrates that include layers of insulating materials that have been deposited on top of other materials—as well as materials containing conductive elements such as traces and transistors—that are also part of the "substrate." In these preferred

Dkt. 46 (02/16/2021 Demaray's Opening Br.), 6



# Demaray's Citations Support the POM of "substrate" is "base material, including but not limited to a wafer coated with an insulator"

## Demaray's Own Presentation

Can Be Wafer And/Or Prior Layer(s)



in the '341 application. The Er—Yb (0.8/0.8) co-doped Alumino-Silicate film was deposited onto a 6 inch wafer of substrate 16 which includes a 10 μm thick thermal oxide substrate, which can be purchased from companies such as Silicon Quest International, Santa Clara, CA. Target 12 was

Substrate 16 can be a solid, smooth surface. Typically, substrate 16 can be a silicon wafer or a silicon wafer coated with a layer of silicon oxide formed by a chemical vapor deposition process or by a thermal oxidation process. Alternatively, substrate 16 can be a glass, such as Corning 1737 (Corning Inc., Elmira, N.Y.), a glass-like material, quartz, a metal, a metal oxide, or a plastic material.

Ex. 1 ('657 Pat.), 7:62-8:1

tion. In one example, substrate 16 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 16 with the thermal oxide layer can

Ex. 1 ('657 Pat.), 18:55-57

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'657 Patent at 18:7-12

Demaray's Presentation, Slide 10

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Ex. 1 ('657 Pat.), 7:62-8:1

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Ex. 1 ('657 Pat.), 18:55-57

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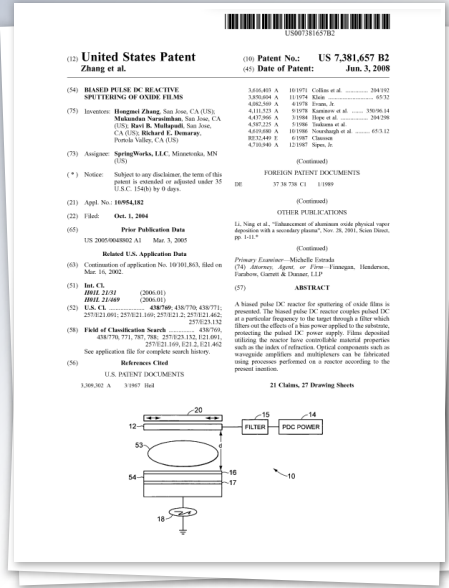
Demaray's Presentation, Slide 10

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'657 Patent at 18:7-12



# Demaray's Citations Support the POM of "substrate" is "base material, including but not limited to a wafer coated with an insulator"



## EXAMPLE 2

A waveguide amplifier can be deposited according to the present invention. An embodiment of target 12 having composition 57.4 cat. % Si, 41.0 cat. % Al, 0.8 cat. % Er 0.8 cat. % Yb (the "0.8/0.8 target") can be formed as disclosed in the '341 application. The Er—Yb (0.8/0.8) co-doped Alumino-Silicate film was deposited onto a 6 inch wafer of substrate 16 which includes a 10 μm thick thermal oxide substrate, which can be purchased from companies such as Silicon Quest International, Santa Clara, CA. Target 12 was first cleaned by sputtering with Ar (80 sccm) only in the metallic mode. Target 12 was then conditioned in poison mode by flowing 60 sccm of Argon and 40 sccm of oxygen respectively. The power supplied to target 12 during conditioning was kept at about 6 kW.

An active core film was then deposited on substrate 16. The thickness of the deposited film is approximately 1.2 μm. The deposition parameters are shown in Table 2.

A straight waveguide pattern can then formed by standard photolithography techniques. The active core was etched using reactive ion etch followed by striping and cleaning. Next, a 10 μm top cladding layer is deposited using a similar deposition process according to the present invention. An embodiment of target 12 with composition 92 cat. % Si and 8 cat. % Al as shown in FIG. 9 to form the top cladding layer. The index difference between the top cladding layer and the active layer is about 3.7%. The amplifier is then annealed at 725° C. for about 30 min (see FIG. 6, for example).

Substrate 16

Active core film deposited

Cladding layer deposited over active core film

# Demaray's Citations Support the POM of "substrate" is "base material, including but not limited to a wafer coated with an insulator"

## Demaray's Own Presentation

Can Be Wafer And/Or Prior Layer(s)



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Ex. 1 ('657 Pat.), 18:7-12

Substrate 16 can be a solid, smooth surface. Typically, substrate 16 can be a silicon wafer or a silicon wafer coated with a layer of silicon oxide formed by a chemical vapor deposition process or by a thermal oxidation process. Alternatively, substrate 16 can be a glass, such as Corning 1737 (Corning Inc., Elmira, N.Y.), a glass-like material, quartz, a metal, a metal oxide, or a plastic material.

Ex. 1 ('657 Pat.), 7:62-8:1

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Ex. 1 ('657 Pat.), 18:55-57

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Demaray's Presentation, Slide 10

tion. In one example, substrate 16 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 16 with the thermal oxide layer can

'657 Patent at 18:55-57

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## Demaray's Own Presentation

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Ex. 1 ('657 Pat.), 7:62-8:1

tion. In one example, substrate 16 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 16 with the thermal oxide layer can

Ex. 1 ('657 Pat.), 18:55-61

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Demaray's Presentation, Slide 10

tion. In one example, substrate 16 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 16 with the thermal oxide layer can be purchased from companies such as Silicon Quest International, Santa Clara, Calif. A layer of active core material is then deposited on substrate 16 with a Shadow Mask as described in the '492 application. Use of a shadow mask

'657 Patent at 18:55-61



# Demaray's Citations Support the POM of "substrate" is "base material, including but not limited to a wafer coated with an insulator"

## EXAMPLE 3

This example describes production of a dual core Erbium/Yttrium co-doped amplifier according to the present invention. In one example, substrate 16 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 16 with the thermal oxide layer can be purchased from companies such as Silicon Quest International, Santa Clara, Calif. A layer of active core material is then deposited on substrate 16 with a Shadow Mask as described in the '492 application. Use of a shadow mask results in a vertical taper on each side of a finished waveguide which greatly enhances the coupling of light into and out of the waveguide.

Substrate 16

Active layer deposited on substrate 16

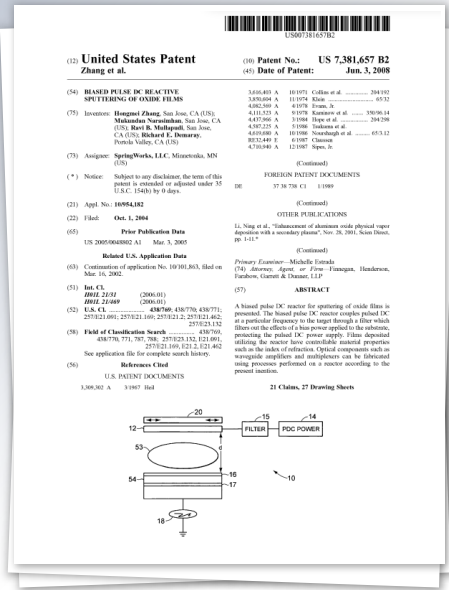
Passive layer deposited over active layer

Upper cladding layer deposited over passive layer

A passive layer of aluminasilicate is then deposited over the active layer. A passive layer of about 4.25 μm thickness can be deposited with an embodiment of target 12 having composition of Si/Al of about 87 cat. % Si and about 13 cat. % Al. The passive layer and active layer are then patterned by standard lithography techniques to form a core that has a width of about 5.0 μm for the active core and tapering to about 3.5 μm at the top of the passive core with an effective length of about 9.3 cm.

Upper cladding layer is then deposited from a Si/Al target of 92 cat. % Si and 8 cat. % Al. Deposition of the upper cladding layer is shown in FIG. 9. In some embodiments, the upper cladding layer can be deposited with a non-biased process. The thickness of the upper cladding layer can be about 10 μm. The amplifier formed by this process is then annealed at 725° C. for about 30 min.

'657 Patent at 18:50–19:21



### EXAMPLE 2

A waveguide amplifier can be deposited according to the present invention. An embodiment of target 12 having composition 57.4 cat. % Si, 41.0 cat. % Al, 0.8 cat. % Er (0.8 cat. % Yb (the "0.8/0.8 target") can be formed as disclosed in the '341 application. The Er–Yb (0.8/0.8) co-doped Aluminosilicate film was deposited onto a 6 inch wafer of substrate 16 which includes a 10 μm thick thermal oxide substrate, which can be purchased from companies such as Silicon Quest International, Santa Clara, CA. Target 12 was first cleaned by sputtering with Ar (80 sccm) only in the metallic mode. Target 12 was then conditioned in poison mode by flowing 60 sccm of Argon and 40 sccm of oxygen respectively. The power applied to target 12 during conditioning was kept at about 6 kW.

An active core film was then deposited on substrate 16. The thickness of the deposited film is approximately 1.2 μm. The deposition parameters are shown in Table 2.

A straight waveguide pattern can then formed by standard photolithography techniques. The active core was etched using reactive ion etch followed by stripping and cleaning. Upper or top cladding layer is then deposited using a non-biased process according to the present invention. An embodiment of target 12 with composition 92 cat. % Si and 8 cat. % Al as shown in FIG. 9 to form the top-cladding layer. The index difference between the top cladding layer and the active layer is about 3.7%. The amplifier is then annealed at 725° C. for about 30 min (see FIG. 6, for example).

# Demaray's Citations Support the POM of "substrate" is "base material, including but not limited to a wafer coated with an insulator"

## Demaray's Own Presentation

Can Be Wafer And/Or Prior Layer(s)



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Ex. 1

Ex. 1 ('657 Pat.), 18:55-57

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Demaray's Presentation, Slide 10

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'657 Patent at 7:62-8:1

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Demaray's Presentation, Slide 10

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'657 Patent at 7:62-8:1



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'657 Patent at 7:62-8:1

Demaray's Presentation, Slide 10

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Can Be Wafer And/Or Prior Layer(s)



in the '341 application. The Er-Yb (0.8/0.8) co-doped Almino-Silicate film was deposited onto a 6 inch wafer of substrate 16 which includes a 10 μm thick thermal oxide substrate, which can be purchased from companies such as Silicon Quest International, Santa Clara, CA. Target 12 was

Substrate 16 can be a solid, smooth surface. Typically, substrate 16 can be a silicon wafer or a silicon wafer coated with a layer of silicon oxide formed by a chemical vapor deposition process or by a thermal oxidation process. Alternatively, substrate 16 can be a glass, such as Corning 1737 (Corning Inc., Elmira, N.Y.), a glass-like material, quartz, a metal, a metal oxide, or a plastic material.

tion. In one example, substrate 16 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 16 with the thermal oxide layer can

Ex. 1

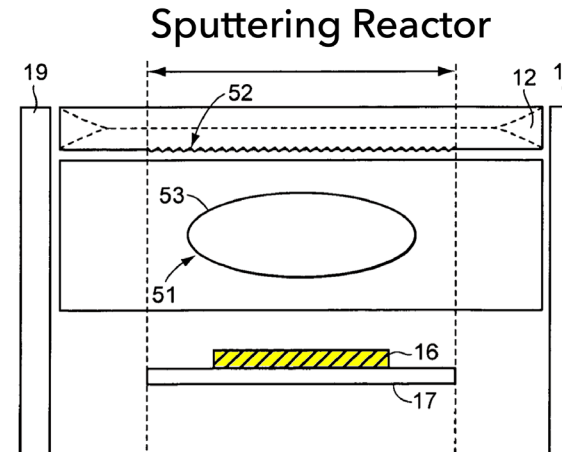
Ex. 1 ('657 Pat.), 18:55-57

10

Demaray's Presentation, Slide 10

Substrate 16 can be a solid, smooth surface. Typically, substrate 16 can be a silicon wafer or a silicon wafer coated with a layer of silicon oxide formed by a chemical vapor deposition process or by a thermal oxidation process. Alternatively, substrate 16 can be a glass, such as Corning 1737 (Corning Inc., Elmira, N.Y.), a glass-like material, quartz, a metal, a metal oxide, or a plastic material.

'657 Patent at 7:62-8:1



- 12. target
- 16. substrate
- 17. carrier sheet
- 19. ground shield
- 51. region
- 52. central target region
- 53. plasma

'657 Patent, Fig. 1B

# The Specification Confirms “substrate” is the “base material, including but not limited to a wafer coated with an insulator”

## EXAMPLE 4

Another example of production of a waveguide amplifier is described here. Again, substrate 16 can be a Si wafer with about a 15 μm thick thermal oxide as can be purchased from Silicon Quest International, Santa Clara, Calif. The embodi-

Substrate 16

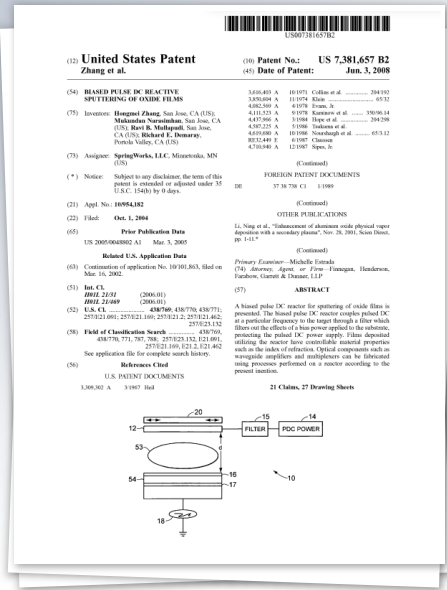
The active core film was deposited onto a 6 inch thermal oxide wafer, which has been previously discussed, from the 1.5/0 target. The thermal oxide thickness was about 10 μm as described in previous examples. The active core is deposited to a thickness of about 1.2 μm with a deposition time of approximately 1 hr. The process condition are as listed in Table 4 below.

Active core film deposited

A straight waveguide pattern can then be formed by a standard photolithography procedure. The active core was etched using reactive ion etch followed by striping and cleaning. Finally, a 10 μm top cladding layer is deposited using a similar process. A target having composition 92 cat. % Si and 8 cat. % Al with deposition parameters as described in FIG. 9 was used to deposit the top cladding. The difference between the index of refraction between the core and the cladding is then about 3.7%.

Cladding film deposited over core film

'657 Patent at 19:39–20:17



A waveguide amplifier can be deposited according to the present invention. An embodiment of target 12 having composition 57.4 cat. % Si, 41.0 cat. % Al, 0.8 cat. % Er, 0.8 cat. % Yb (the “0.8/0.8 target”) can be formed as disclosed in the ‘341 application. The Er–Yb (0.8/0.8) co-doped Aluminosilicate film was deposited onto a 6 inch wafer of substrate 16 which includes a 10 μm thick thermal oxide substrate, which can be purchased from companies such as Silicon Quest International, Santa Clara, CA. Target 12 was first cleaned by sputtering with Ar (80 sccm) only in the metallic mode. Target 12 was then conditioned in poison mode by flowing 60 sccm of Argon and 40 sccm of oxygen respectively. The power supplied to target 12 during conditioning was kept at about 6 kW.

An active core film was then deposited on substrate 16. The thickness of the deposited film is approximately 1.2 μm. The deposition parameters are shown in Table 2.

A straight waveguide pattern can then formed by standard photolithography techniques. The active core was etched using reactive ion etch followed by striping and cleaning. Next, a 10 μm top cladding layer is deposited using a similar process. A target having composition 92 cat. % Si and 8 cat. % Al as shown in FIG. 9 to form the top-cladding layer. The index difference between the top cladding layer and the active layer is about 3.7%. The amplifier is then annealed at 725° C. for about 30 min (see FIG. 4, for example).

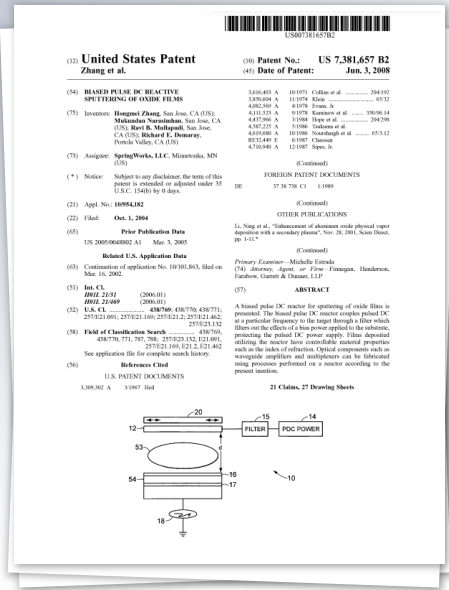
This example describes production of a dual core Erbium/Ytterbium co-doped amplifier according to the present invention. In one example, substrate 16 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 16 with the thermal oxide layer can be purchased from companies such as Silicon Quest International, Santa Clara, Calif. A layer of active core material is then deposited on substrate 16 with a Shadow Mask as described in the ‘452 application. Use of a shadow mask results in a vertical taper on each side of a finished waveguide which greatly enhances the coupling of light into and out of the waveguide.

A passive layer of aluminosilicate is then deposited over the active layer. A passive layer of about 4.25 μm thickness can be deposited with an embodiment of target 12 having composition of Si/Al of about 87 cat. % Si and about 13 cat. % Al. The passive layer and active layer are then patterned by standard lithography techniques to form a core that has a width of about 5.0 μm for the active core and tapering to about 3.5 μm at the top of the passive core with an effective length of about 6.3 cm.

Upper cladding layer is then deposited from a Si/Al target of 92 cat. % Si and 8 cat. % Al. Deposition of the upper cladding layer is shown in FIG. 9. In some embodiments, the upper cladding layer can be deposited with a non-biased process. The thickness of the upper cladding layer can be about 10 μm. The amplifier formed by this process is then annealed at 725° C. for about 30 min.



# The Specification Confirms “substrate” is the “base material, including but not limited to a wafer coated with an insulator”



## EXAMPLE 6

A waveguide amplifier was fabricated using this material in the similar fashion as described in examples 2-4. The active core was first deposited on substrate 16, which includes a 10 μm thermal oxide layer, using the following deposition parameters: target power 5 KW, pulsing frequency 120 KHz, bias 100 W, reverse time 2.3 us, Argon and Oxygen flow are 60 sccm and 30 sccm respectively. The active core thickness is deposited to a thickness about 1.2 μm, which takes approximately 1 hr. All wafers are pre-heated at about 350° C. for 30 min before deposition. A straight waveguide pattern is then formed by standard photolithography procedure. The active core was etched using reactive ion etch following by striping and cleaning. Next, a 10 μm top cladding layer is deposited using similar process. The “92/8” (92 cat. % Si and 8 cat. % Al) metallic target was used to deposit top clad according to deposition parameters shown in FIG. 9, resulting in a 4% index difference between active core and cladding. The wave guide was then annealed at 800° C. for about 30 min.

Substrate 16

Active core deposited

Cladding layer deposited over active core

'657 Patent at 20:62–21:55

### EXAMPLE 2

A waveguide amplifier can be deposited according to the present invention. An embodiment of target 12 having composition 57.4 cat. % Si, 41.0 cat. % Al, 0.8 cat. % Ir 0.8 cat. % Yb (the “0.8/0.8 target”) can be formed as disclosed in the ‘341 application. The Er–Yb (0.8/0.8) co-sputtered Aluminum-Silicate film was deposited onto a 6 inch wafer of substrate 18 which includes a 10 μm thick thermal oxide substrate, which can be purchased from companies such as Silicon Quest International, Santa Clara, CA. Target 12 was first cleaned by sputtering with Ar (80 sccm) only in the metallic mode. Target 12 was then conditioned in poison mode by flowing 60 sccm of Argon and 40 sccm of oxygen respectively. The power supplied to target 12 during conditioning was kept at about 6.5 KW.

An active core film was then deposited on substrate 18. The thickness of the deposited film is approximately 1.2 μm. The deposition parameters are shown in Table 2.

A straight waveguide pattern can then be formed by standard photolithography techniques. The active core was etched using reactive ion etch followed by striping and cleaning. Next, a 10 μm top cladding layer is deposited using a similar process according to the present invention. An embodiment of target 12 with composition 92 cat. % Si and 8 cat. % Al as shown in FIG. 9 to form the top-cladding layer. The index difference between the top cladding layer and the active layer is about 3.7%. The amplifier is then annealed at 725° C. for about 30 min (see FIG. 6, for example).

### EXAMPLE 3

This example describes production of a dual core Erbium/Yttrium co-doped amplifier according to the present invention. In one example, substrate 18 is a silicon substrate with an undercladding layer of thermally oxidized SiO<sub>2</sub> of about 15 μm thick. Substrate 18 with the thermal oxide layer can be purchased from companies such as Silicon Quest International, Santa Clara, Calif. A layer of active core material is then deposited on substrate 18 with a Shadow Mask as described in the ‘452 application. Use of a shadow mask results in a vertical taper on each side of a finished waveguide which greatly enhances the coupling of light into and out of the waveguide.

A passive layer of aluminumsilicate is then deposited over the active layer. A passive layer of about 4.25 μm thickness can be deposited with an embodiment of target 12 having composition of Si/Al of about 87 cat. % Si and about 13 cat. % Al. The passive layer and active layer are then patterned by standard lithography techniques to form a core that has a width of about 5.0 μm for the active core and tapering to about 3.5 μm at the top of the passive core with an effective length of about 9.3 cm.

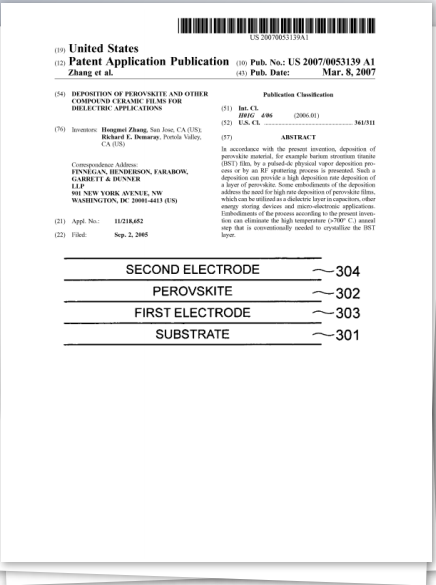
Upper cladding layer is then deposited from a Si/Al target of 92 cat. % Si and 8 cat. % Al. Deposition of the upper cladding layer is shown in FIG. 9. In some embodiments, the upper cladding layer can be deposited with a non-biased process. The thickness of the upper cladding layer can be about 10 μm. The amplifier formed by this process is then annealed at 725° C. for about 30 min.

### EXAMPLE 4

Another example of production of a waveguide amplifier is described here. Again, substrate 18 can be a Si wafer with about a 15 μm thick thermal oxide as can be purchased from Silicon Quest International, Santa Clara, Calif. The embodiment of target 12 is as described in the ‘341 application. The active core film was deposited onto a 6 inch thermal oxide wafer which has been previously discussed, from the 1.50 target. The thermal oxide thickness was about 10 μm as described in previous examples. The active core is deposited to a thickness of about 1.2 μm with a deposition time of approximately 1 hr. The process condition are as listed in Table 4 below.

A straight waveguide pattern can then be formed by a standard photolithography procedure. The active core was etched using reactive ion etch followed by striping and cleaning. Next, a 10 μm top cladding layer is deposited using a similar process. A target having composition 92 cat. % Si and 8 cat. % Al with deposition parameters as described in FIG. 9 was used to deposit the top cladding. The difference between the index of refraction between the core and the cladding is then about 3.7%.

# Intrinsic Evidence Confirms “substrate” is the “base material, including but not limited to a wafer coated with an insulator”



## Named Inventors' Other Patent Publication

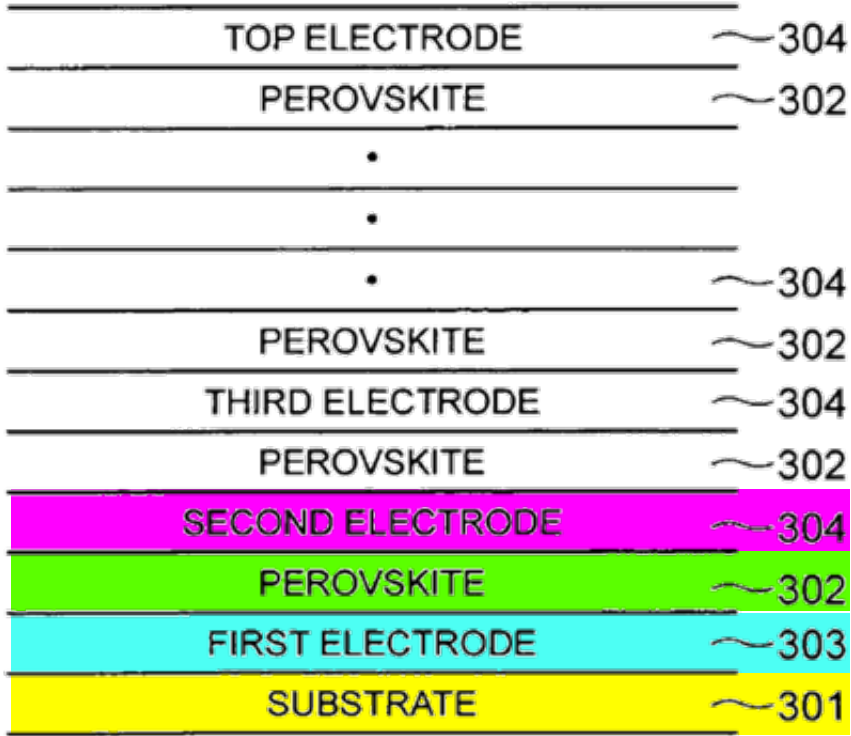


FIG. 6

[0062] FIG. 6A illustrates a parallel coupled stacking. As shown in FIG. 6A, a substrate 301, which for example can be a high temperature plastic substrate, such as polyimide, is loaded into load lock 503. Electrode layer 303, for example, can be deposited in chamber 504. A dielectric perovskite layer 302 is then deposited on electrode layer 303. Perovskite layer 302 can be about 0.1 to 1 μm and can be deposited in chamber 505 according to embodiments of the present invention. The wafer can then be moved to chamber 506 where the next electrode layer 304 of thickness of about 0.1 μm or more is deposited. A second capacitor stack can then be deposited over the first capacitor stack formed by first electrode layer 303, perovskite layer 302, and second electrode layer 304. This capacitor stack includes second perovskite layer 305 and third electrode layer 306. In some

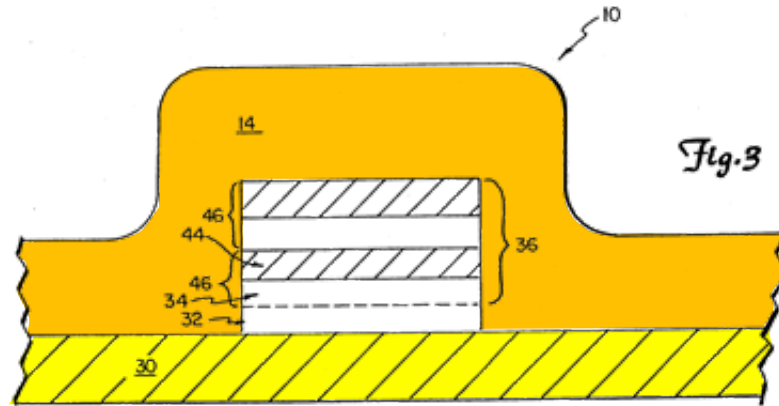
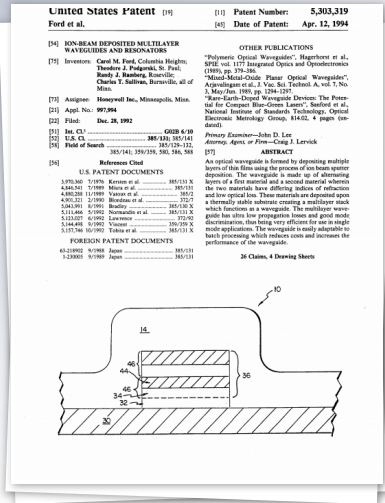
U.S. Patent Publ'n No. 2007/0053139, [0062], Fig. 6 (cited on face of Asserted Patents)





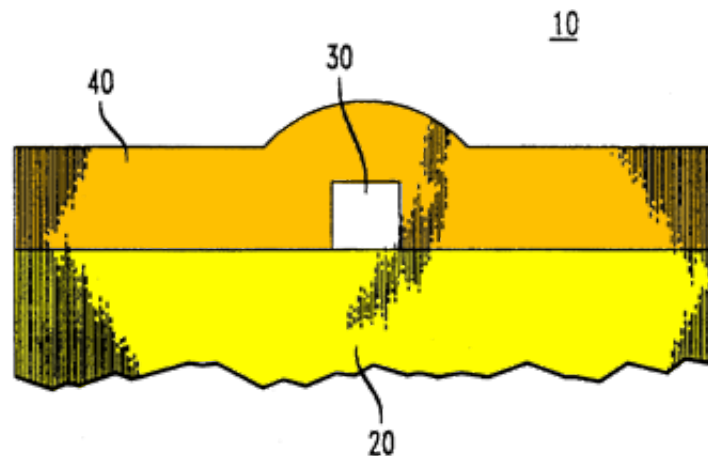
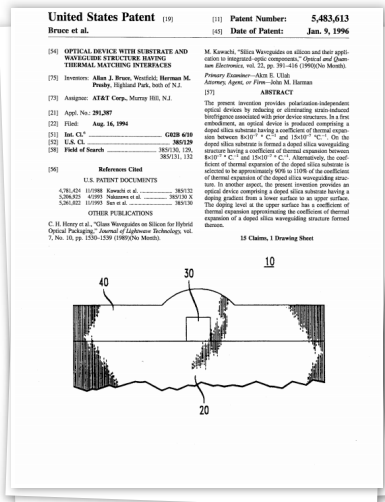


# Intrinsic Evidence Confirms “substrate” Is the “base material, including but not limited to a wafer coated with an insulator”



Waveguide 10 comprises a stack of material 12 which is attached to a substrate 30. A protective coating or upper isolation layer 14 is placed on top of both multi-layer stack 12 and substrate 30. Upper isolation layer 14 can shield the waveguide from environmental attacks such as moisture, chemical attack, etc. Furthermore,

U.S. Pat. 5,303,319 at 2:66-3:3, Fig. 3 (cited on face of Asserted Patents)



Referring to the drawings, FIG. 1 is a schematic view of an optical device 10 having a substrate 20, a waveguiding element 30, and a cladding layer 40. In conventional applications, substrate 20 is typically a silicon wafer with a thermally oxidized SiO<sub>2</sub> surface layer. The SiO<sub>2</sub> layer in such devices functions as a first cladding layer for the waveguiding element. In a first embodiment of the present invention, layer 20 is a doped silica substrate, the doped silica substrate having a coefficient of thermal expansion which approximates the coefficient of thermal expansion of the waveguiding element material layer.

U.S. Pat. 5,483,613 at 2:47-57, Fig. 1 (cited on face of Asserted Patents)

# Plain meaning of “substrate” is “base material, including but not limited to a wafer coated with an insulator”

**substrate**—Also called **base material**. 1. The supporting material on or in which the parts of an integrated circuit are attached or made. The substrate may be passive (thin film, hybrid) or active (monolithic compatible). 2. A

Dkt. 61-1 (Modern Dictionary of Electronics (1999)), 2797

## **3.2 SUBSTRATES FOR THIN FILMS APPLICATIONS**

### **3.2.1 Introduction**

The function of the **substrate** is to provide the **base onto which** thin film circuits are fabricated and various **thin film multilayers are deposited**. In addition, the substrate provides the necessary mechanical support and rigidity needed for a reliable circuit, and it has ade-

Dkt. 61 (Thin Film Technology Handbook (1997)), 2815.

# “metallic mode” / poison mode”

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'657 Patent, Claim 1

## Demaray’s Proposal

metallic mode: “mode of operation in which the surface of the target is substantially metallic”

poison mode: “mode of operation in which the rate of the thin film formation on the surface of the target equals or exceeds the rate of sputter removal of the surface of the target”

## Defendants’ Proposal

Plain and ordinary meaning

## Court’s Preliminary Construction

metallic mode: Plain-and-ordinary meaning wherein the plain-and-ordinary meaning is “mode of operation in which the surface of the target is substantially metallic” and is characterized by a small addition of reactive gas to the inert gas flow, a higher impedance magnetron discharge, an incomplete oxidation of film, and a higher voltage (as compared to poison mode)”

Demaray’s Proposal

poison mode: Plain-and-ordinary meaning wherein the plain-and-ordinary meaning is “mode of operation in which the rate of the thin film formation on the surface of the target equals or exceeds the rate of sputter removal of the surface of the target,” and is characterized by a lower voltage (as compared to **poison mode**)”

Demaray’s Proposal



1. A method of depositing a film on an insulating substrate, comprising:

- providing a process gas between a conductive target and the substrate;
- providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;
- providing an RF bias at a frequency that corresponds to the narrow band rejection filter to the substrate;
- providing a magnetic field to the target; and
- reconditioning the target;

wherein reconditioning the target includes reactive sputtering in the **metallic mode** and then reactive sputtering in the **poison mode**.

'657 Patent, Claim 1

1. A method of depositing a film on an insulating substrate, comprising:

- providing a process gas between a conductive target and the substrate;
- providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;
- providing an RF bias at a frequency that corresponds to the narrow band rejection filter to the substrate;
- providing a magnetic field to the target; and
- reconditioning the target;

wherein reconditioning the target includes reactive sputtering in the metallic mode and then reactive sputtering in the poison mode.

'657 Patent, Claim 1

# Demaray's "Metallic Mode" Proposal

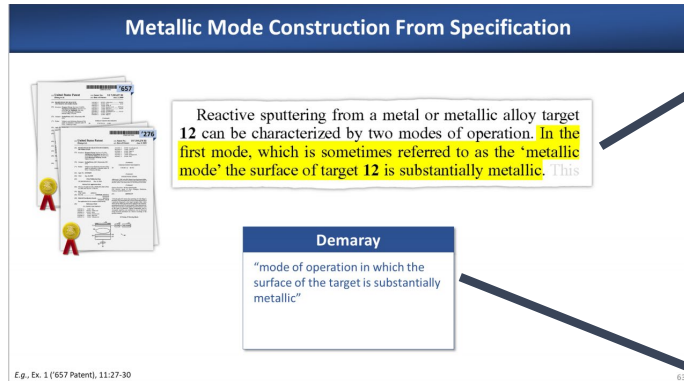
**Metallic Mode Construction From Specification**

Reactive sputtering from a metal or metallic alloy target 12 can be characterized by two modes of operation. In the first mode, which is sometimes referred to as the 'metallic mode' the surface of target 12 is substantially metallic. This

**Demaray**

"mode of operation in which the surface of the target is substantially metallic"

E.g., Ex. 1 (657 Patent), 11:27-30

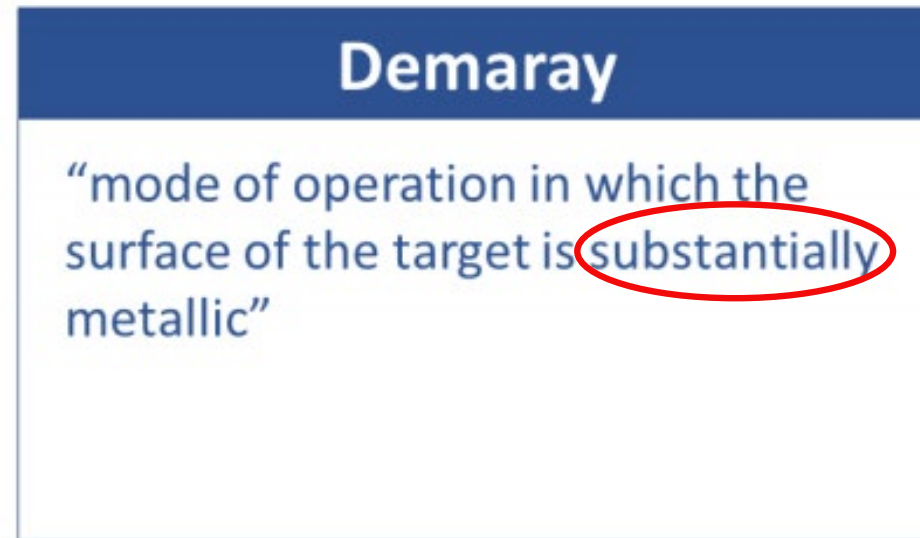


Demaray's *Markman* Slide 63

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**Demaray**

"mode of operation in which the surface of the target is substantially metallic"



?

# “reconditioning the target”

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'657 Patent, Claim 1

1. A method of depositing a film on an insulating substrate, comprising:

- providing a process gas between a conductive target and the substrate;
- providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;
- providing an RF bias at a frequency that corresponds to the narrow band rejection filter to the substrate;
- providing a magnetic field to the target; and
- reconditioning the target;

wherein reconditioning the target includes reactive sputtering in the metallic mode and then reactive sputtering in the poison mode.

'657 Patent at Claim 1



# “reconditioning the target”: The Parties’ Dispute

## Demaray’s Proposal

Plain and ordinary meaning, or  
“**cleaning and** conditioning the target”

## Defendants’ Proposal

“conditioning the target **between depositions**”

### The Parties’ Dispute:

1. Whether reconditioning includes “cleaning”?
2. Whether reconditioning occurs “between depositions”?

# Demaray's Proposal is Incorrect. Demaray Attempts to Rewrite the Claim and Renders Claim Language Void

*cleaning and*  
~~re~~conditioning the target;

*cleaning and*  
wherein ~~re~~conditioning the target includes reactive sputtering in the metallic mode and then reactive sputtering in the poison mode.

'657 Patent at Claim 1

# Demaray's Proposal Is Incorrect. Demaray's Attempt to Broaden "Reconditioning" to Include "Cleaning" Is at Odds with the Intrinsic Evidence

## Claim 1 Covers Reactive Sputtering

1. A method of depositing a film on an insulating substrate, comprising:

- providing a process gas between a conductive target and the substrate;
- providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;
- providing an RF bias at a frequency that corresponds to the narrow band rejection filter to the substrate;
- providing a magnetic field to the target; and
- reconditioning the target;

wherein reconditioning the target includes reactive sputtering in the metallic mode and then reactive sputtering in the poison mode.

'657 Patent at Claim 1

## Demaray's Evidence Relates to Non-Reactive Sputtering

260V. Before each film deposition, in step 401, target 12 is cleaned by pure Argon sputtering in the metallic mode. Then target is then conditioned in poison mode with the oxygen flow much higher than the flow required at the transition region.

'657 Patent at 17:10-15

# Demaray's Proposal Is Incorrect: Demaray's Attempt to Limit "Conditioning" to Poison Mode Is Inconsistent with the Intrinsic Evidence

## Demaray's Evidence

metallic mode. Target 12 was then conditioned in poison mode by flowing 60 sccm of Argon and 40 sccm of oxygen respectively. The power supplied to target 12 during condi-

'657 Patent at 18:13-15

## "Conditioning" Includes Both Metallic & Poison Modes

1. A method of depositing an insulating oxide film on a substrate, comprising:

conditioning a target;

preparing the substrate;

adjusting an RF bias power to the substrate;

setting a process gas flow; and

applying pulsed DC power to the target such that a voltage on the target oscillates between positive and negative voltages to create a plasma and deposit the oxide film; and

narrow band rejection filtering the DC power at a frequency of the bias power before applying the DC power to the target,

wherein conditioning the target includes sputtering with the target in a metallic mode to remove the surface of the target and then sputtering with the target in poisonous mode to prepare the surface.

Dkt. 61-11 ('356 Patent) at Claim 1;  
see also '657 Patent at 20:52-55

# Defendants' Proposal is Correct. Specification Makes Clear Reconditioning Refers to Conditioning Between Depositions

## The Problem

One of the problems encountered during the reactive sputtering from an alloy metallic target is that the film composition drifts from run to run due to the difference in sputtering yields from the elements that forms the target alloy. For example, with Ar as a sputtering gas, the sputtering yield of Aluminum is about 3-4 times that of Silicon, while sputtering yield of Alumina is only about 50% that of Silica. Therefore, during the metal burn in, more Aluminum is sputtered from the target, resulting in a Si rich target surface. When sputtering in the poison mode, more Silica will be removed from target. Thus, as deposition goes on, the composition of the film deposited on substrate 16 will drift from lower Alumina concentration to higher Alumina concentration. This results in the index of refraction of a film drifting up with subsequent depositions from a target 12, as is shown for the deposition described in Example 4 in FIG. 29. FIG. 30 shows the drift in photoluminescence pumped at 532 nm with subsequent depositions. FIG. 31 shows drift in the excited state lifetime with subsequent depositions from a target. The embodiment of target 12 utilized in FIGS. 29 through 31 is the 1.5/0 target and the deposition parameters are as described above in Example 4.



# Defendants' Proposal is Correct. Specification Makes Clear Reconditioning Refers to Conditioning Between Depositions

## The Problem

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'657 Patent at 20:30-51

## The Solution

The drift can be stabilized by recondition target 12 prior to deposition. The recondition process (or burn in) consists of both sputtering in metallic mode and then sputtering in poison mode to condition target 12. The burn in time in metallic mode needs to be as short as possible and at the same time insure no arcing during the poison mode deposition. FIG. 32 shows the much improved drift in the index of refraction and the photoluminescence when target 12 is reconditioned between subsequent depositions.

'657 Patent at 20:52-60

# Demaray's Proposal Is Incorrect. Demaray Cherry Picks Passages to Support Its Proposal

## Specification: Consistent With Claim Language



The drift can be stabilized by recondition target 12 prior to deposition. The recondition process (or burn in) consists of both sputtering in metallic mode and then sputtering in poison mode to condition target 12. The burn in time in metallic mode needs to be as short as possible and at the same time insure no arcing during the poison mode deposition. FIG. 32 shows the much improved drift in the index of refraction and the photoluminescence when target 12 is reconditioned between subsequent depositions.

260V. Before each film deposition, in step 401, target 12 is cleaned by pure Argon sputtering in the metallic mode. Then

metallic mode. Target 12 was then conditioned in poison mode by flowing 60 sccm of Argon and 40 sccm of oxygen respectively. The power supplied to target 12 during condi-

Ex. 1 ('657 Patent), 17:10-11, 18:13-15, 20:52-60

# Demaray's Proposal Is Incorrect. Demaray Cherry Picks Passages to Support Its Proposal

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'657 Patent at 20:52-60



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'657 Patent at 20:52-60

260V. Before each film deposition, in step 401, target 12 is cleaned by pure Argon sputtering in the metallic mode. Then

'657 Patent at 17:10-11



# Demaray's Proposal Is Incorrect. Demaray Cherry Picks Passages to Support Its Proposal

## Specification: Consistent With Claim Language



The drift can be stabilized by recondition target 12 prior to deposition. The recondition process (or burn in) consists of both sputtering in metallic mode and then sputtering in poison mode to condition target 12. The burn in time in metallic mode needs to be as short as possible and at the same time insure no arcing during the poison mode deposition. FIG. 32 shows the much improved drift in the index of refraction and the photoluminescence when target 12 is reconditioned between subsequent depositions.

260V. Before each film deposition, in step 401, target 12 is cleaned by pure Argon sputtering in the metallic mode. Then

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'657 Patent at 20:52-60

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'657 Patent at 17:10-11

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'657 Patent at 18:13-15

Ex. 1 ('657 Patent), 17:10-11, 18:13-15, 20:52-60

Demaray's Mark

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The pulsed DC power supplied to target 12 was about 6 kW. Whenever a brand new target was used or when the target has been expose to atmosphere, a long time of condition (for example more than 30 hrs of conditioning) may be necessary to ensure films with the best active core property (longest life time and highest photoluminescence) are deposited. Substrate 16 is then preheat at about 350° C. for about 30 min before deposition.

'657 Patent at 19:53-60

FIG. 5 shows the hysteresis curve of this particular embodiment of target 12. When target 12 under goes the transition from metallic to poison mode, the target voltage drops from an average of about 420V to an average of about 260V. Before each film deposition, in step 401, target 12 is cleaned by pure Argon sputtering in the metallic mode. Then target is then conditioned in poison mode with the oxygen flow much higher than the flow required at the transition region.

'657 Patent at 17:6-15

# “reconditioning the target”

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'657 Patent, Claim 1

1. A method of depositing a film on an insulating substrate, comprising:  
providing a process gas between a conductive target and the substrate;  
providing pulsed DC power to the target through a narrow band rejection filter such that the target alternates between positive and negative voltages;  
providing an RF bias at a frequency that corresponds to the narrow band rejection filter to the substrate;  
providing a magnetic field to the target; and  
reconditioning the target;  
wherein **reconditioning the target** includes reactive sputtering in the metallic mode and then reactive sputtering in the poison mode.

'657 Patent at Claim 1

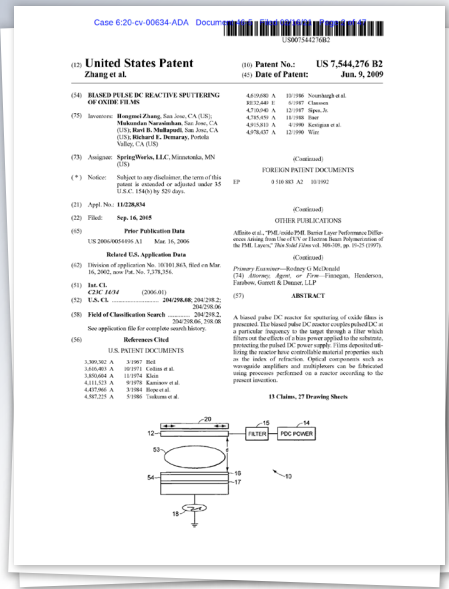
**“the temperature of the  
substrate substantially  
constant”**

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'276 Patent, Claim 10



# Claim 10 of the '276 Patent



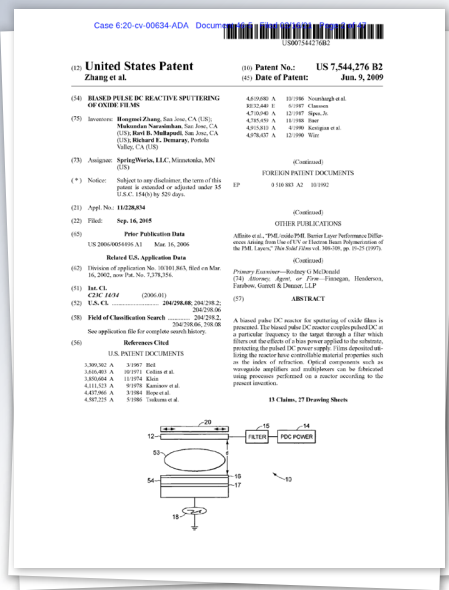
10. The reactor of claim 6, further including a temperature controller for holding the temperature of the substrate substantially constant.

'276 Patent, Claim 10

What does “substantially constant” mean in the context of this patent?

## Court’s Preliminary Construction: Plain and ordinary meaning

Claim Term	Demaray’s Proposal	Defendants’ Proposal
“the temperature of the substrate substantially constant”	Plain and ordinary meaning or “substantially constant” means “within about 10 °C”	“within about 10 °C of the set temperature”



hundred watts of RF power. The temperature of the substrate can be controlled to within about 10° C. and can vary from about -50° C. to several hundred degrees C. Process gasses

'276 Patent, 3:1-3

of the substrate. The substrate temperature can be held constant in the range of about -40° C. to about 550° C. and can be maintained at a chosen temperature to within about 10° C. by means of preheating substrate 16 and the substrate holder prior to deposition. During the course of deposition, the heat

'276 Patent, 9:19-23

# Defendants' Proposal Is Correct: Demaray's Expert Confirms the 10 °C Difference is Measured from a Temperature Sensor's Reading

## Demaray's Expert

- Q. So essentially the staying within 10 degrees is within 10 degrees of whatever you've measured the temperature at?
- A. Right. The reality is one only measures the temperature where the temperature sensor is. There might be two temperature sensors, there might be three, but, you know, they're not everywhere.
- Q. Okay. So – and based on whatever that temperature sensor is measuring, **a person of ordinary skill in the art would understand the temperature of the substrate substantially constant to be within about 10 degrees of whatever that measurement is.** Do I understand that right?
- A. **Yes.** And that is how one sets processes. Any – any parameter for a process typically has a range where you say 1,000 watts plus or minus 20 watts, or 300 degrees plus or minus 5 degrees, or something. **So there's always a process setting, so that's – one of skill in the art would understand that 10 degrees is the process setting for the temperature control. That – that defines “substantially constant.”**

# Demaray's Proposal is Incomplete

Claim Term	Demaray's Proposal
"the temperature of the substrate substantially constant"	Plain and ordinary meaning or "substantially constant" means "within about 10 °C" [ <b><i>of what?</i></b> ]



Claim Term	Defendants' Proposal
"the temperature of the substrate substantially constant"	"within about 10 °C of a set temperature"