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|  | First Named Inventor Jean | Jean-Claude ARTONNE |
|  | Art Unit |  |
|  | Examiner Name |  |
|  | Attorney Docket Number | 688266-21RX |


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|  | 1 |  | 128145 |  | 2000-10-03 |  | Nagaoka |  |  |  |  |
|  | 2 |  | 686957 |  | 1997-11-11 |  | Baker |  |  |  |  |
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|  | 4 | 6031670 |  |  | 2000-02-29 |  | Inoue |  |  |  |  |
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|  | Art Unit |  |
|  | Examiner Name |  |
|  | Attorney Docket Number | 688266-21RX |



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| :---: | :---: | :---: |
|  | Filing Date |  |
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|  | Art Unit |  |
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Please see 37 CFR 1.97 and 1.98 to make the appropriate selection(s):

That each item of information contained in the information disclosure statement was first cited in any communication from a foreign patent office in a counterpart foreign application not more than three months prior to the filing of the information disclosure statement. See 37 CFR 1.97(e)(1).

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## SIGNATURE

A signature of the applicant or representative is required in accordance with CFR 1.33, 10.18. Please see CFR 1.4(d) for the form of the signature.

| Signature | /Stephen E. Murray/ | Date (YYYY-MM-DD) | 2014-11-26 |
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| Name/Print | Stephen E. Murray | Registration Number | 63,206 |

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| Application Number: | 90013410 |
| International Application Number: |  |
| Confirmation Number: | 4682 |
| Title of Invention: | METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE |
| First Named Inventor/Applicant Name: | Jean-Claude ARTONNE |
| Customer Number: | 00570 |
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| Attorney Docket Number: | 688266-21RX |
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| 15 | Reexam Miscellaneous Incoming Letter | Appendix_C.PDF | 1650458 | no | 6 |
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| 19 | Other Reference-Patent/App/Search documents | 00680289.PDF | 1231557 | no | 19 |
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| 20 | Copy of patent for which reexamination is requested | 00677943.PDF | 1432481 | no | 25 |
|  |  |  | ea7cr209ce517529975337ctcda7b961855 |  |  |
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| 21 | Transmittal Letter | 00680646.PDF | 80215 | no | 2 |
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| 22 | Receipt of Original Ex Parte Reexam Request | 00680645.PDF | 129414 | no | 12 |
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| 24 | Information Disclosure Statement (IDS)Form (SB08) Form (SB08) | 00675157.PDF | 612428 | no | 4 |
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## EXHIBIT 7a


（54）［発明の名称】
魚眼レンズカメラ装䓢及びその画像歪み補正方法区び画像抽出方法
（57）【要約】
【課題】 魚眼レンズカメラ装置及びその画像歪み補正方法及び画像抽出方法に関し，魚眼レンズカメラを任意 の設置アングルで取り付けた場合の魚眼レンズ画像の歪 み補正の画像変形処理を高速化し，又，人物像等の移動 する像を精度よく検出して抽出し，モニタテレビ等に高精度で表示きせる。
【解决手段】 魚眼レンズ1－1，CCD撮像装置1－ 2 で撮影した画像を映像メモリ1－3に記憶きせ，画像補正処理部1－4は，魚眼レンズカメラか設置角を補正 する座標変換と，魚眼レンズ画像の歪みを補正する座標変換とを組み合わせて演算する構成を備え，等面積射影 の魚眼レンズ像を高速に写像変換する。更に魚眼レンズ画像内の領域に対応した重み付けを行って，人物像等の特徵量を抽出し，表示エリアな抽出する構成を備えてい る。


## 【特許請求の範囲】

【請求頂1】魚眼レンズカメラにより撮影された画像 の歪みを補正する画像補正処理部を備えた魚眼レンズ力 メラ装置において，
前記画像補正処理部は，魚眼レンズカメラの設置角を補正する座標変換と，魚眼レンズ画像の歪みを補正する座摽変換とを組み合わせて演算する構成を有することを特顀とする魚眼レンズカメラ装置。
【請求項2】前記画像補正処理部は，等面積写像の魚眼レンズ画像の歪みを補正する座標変換を演算する構成 を有することを特徴とする請求項1記載の魚眼レンズカ メラ装置。
【請求頂3】魚眼レンズカメラにより撮影きれた画像 の歪みを補正する画像補正処理部を備えた魚眼レンズカ メラ装置にむろいて，
魚眼レンズ画像の歪み補正のための，表示画像の中心位置，魚眼レンズ画像の縦横比，魚眼レンズ画像エリアの半径等のパラメータを，撮像された魚眼レンズ画像自体 から抽出し，該パラメータにより魚眼レンズ画像の歪み捕正を行う構成を備えたことを特徴とする魚眼レンズカ メラ装置。
【請求頂4】 魚眼レンズカメラにより撮影した画像か ら，移動する像を抽する魚眼レンズカメラ装置におろ て，
魚眼レンズ画像内の相互の位置関係を利用して領域を統合し，像の変化した領域を抽出する構成を備えたことを特徴とする魚眼レンズカメラ装置。
【請求頂5】 魚眼レンズカメラにより撮影した两像か ら，移動する像を抽出する魚眼レンズカメラ装惪におい て，
魚眼レンズ画像をパノラマ状の横長映像に変換し，その映像のフレーム間差分の信号又はフレーム間差分とフレ ーム内差分とを結合した信号を抽出し，該信号により領域抽出を行い，複数の移動像の領域抽出を同時に行う構成を備えたことを特徴とする魚眼レンズカメラ装置。
【請求項6】 魚眼レンズカメラにより撮影した画像か ら，移動する像を抽出する魚眼レンズカメラ装置にあい て，
フレーム間差分の信号又はフレーム間差分とフレーム内差分とを結合した信号等の特徴量の抽出演算を魚眼レン ズ画像の映像をもとに行い，特徴検出領域に対する領域抽出処理において，極座標と直交座標とのアドレス変換 を行って魚眼レンズ画像の映像内を走查し，円形の魚眼 レンズ画像の映像の中から複数の移動像の領域抽出を行 ら構成を備えたことを特徴とする魚眼レンズカメラ装置。
【請求項7】 魚眼レンズカメラにより撮影した画像か ら，移動する像を抽出する魚眼レンズカメラ装置にあい て，
魚眼レンズ画像の映像の中から得られる複数の人物像の

領域について，各人物像の形状を正規化し，各像の形状内の色情報を記億し，個々の像の色情報をもとに移動す る複数の人物像を個別に追尾する映像を作成する構成を備えたことを特徴とする魚眼レンズカメラ装置。
【請求項8】魚眼レンズカメラにより撮影した画像か ら，移動する像を抽出する魚眼レン゙ズカメラ装置におい て，
魚眼レンズ画像の中心部分と周辺部分との歪みの大きさ に応じて異なる重み倸数を乗じた特徵量をもとに領域抽出を行う構成を備えたことを特銜とする魚眼レンズカメ ラ装置。
【請求項9】前記重み係数として，更に魚眼レンズ画像の映像内の領域に対応して異なる値を与え，非抽出領域をマスクして領域抽出を行う構成を備えたことを特徴 とする請求項8記載の魚眼レンズカメラ装置。
【請求項10】魚眼レンズカメラにより撮影きれた画像の歪みの補正において，
魚眼レンズカメラの設置角を補正する座標変換と，魚眼 レンズ画像の歪みを補正する座標変換とを組み合かせて演算する過程を含むことを特徵とする魚眼レンズカメラ の画像歪み補正方法。
【請求項11】前記魚眼レンズカメラの画像歪み補正 において，等面積写像の魚眼レンズ画像の歪みを補正す る座標変換を演算する過程を含むことを特徴とする請求項10記載の魚眼レンズカメラの画像歪み補正方法。
【請求項12】魚眼レンズカメラにより撮影された画像の歪みの補正において，
魚眼レンズ画像の歪み補正のための，表示画像の中心位惪，魚眼レンズ画像の熦横比，魚眼レンズ画像エリアの半径等のパラメータを，撮像された魚眼レンズ画像自体 から抽出し，該パラメータにより魚眼レンズ画像の歪み捕正を行う過程を含むことを特顀とする魚眼レンズカメ ラの画像歪み補正方法。
【請求項13】魚眼レンズカメラにより撮影した画像 から，移動する像を抽出する画像抽出方法において，
魚眼レンズ画像内の相互の位置関倸を利用して領域を統合し，像の変化した領域を抽出する過程を含むてこを特徵とする魚眼レンズカメラの画像抽出方法。
【請求項14】魚眼レンズカメラにより撮影した画像 から，移動する像を抽出する画像抽出方法において，
魚眼レンズ画像をパノラマ状の横長映像に変換し，その映像のフレーム間差分の信号又はフレーム間差分とフレ一ム内差分とを結合した信号を抽出し，該信号により領域抽出を行い，複数の移動像の領域抽出を同時に行う過程を含むことを特徴とする魚眼レンズカメラの画像抽出方法。
【請求項15】魚眼レンズカメラにより撮影した画像 から，移動する像を抽出する画像抽出方法において， フレーム間差分の信号又はフレーム間差分とフレーム内差分をを結合した信号等の特徴量の抽出演算を魚眼レン

ス画像の映像をもとに行い，特徴検出領域に対する領域抽出処理において，極座標と直交座標とのアドレス変換 を行って魚眼レンズ画像の映像内を走査し，円形の魚眼 レンズ画像の映像の中から複数の移動像の領域抽出を行 う過程を含むことを特徴とする魚眼レンズカメラの画像抽出方法。
【請求項16】魚眼レンズカメラにより撮影した画像 から，移動する像を抽出する画像抽出方法において，
魚眼レンズ画像の映像の中から得られる複数の人物像の領域について，各人物像の形状を正規化し，各像の形状内の色情報を記億し，個々の像の色情報をもとに移動す る複数の人物像を個別に追尾する映像を作成する過程を含むことを特徴とする魚眼レンズカメラの画像抽出方法。
【請求項17】魚眼レンズカメラにより撮影した画像 から，移動する像を抽出する画像抽出方法において，
魚眼レンズ画像の中心部分と周辺部分との歪みの大きさ に応じて異なる重み係数を乗じた特徴量をもとに領域抽出を行う過程を含むことを特徴とする魚眼レンズカメラ の画像抽出方法。
【請求項 18 】前記重み係数として，更に魚眼レンズ画像の映像内の領域に対応して異なる値を与え，非抽出領域をマスクして領域抽出を行う過程を含むことを特徴 とする請求項17記載の魚眼レンズカメラの画像抽出方法。
【発明の詳細な説明】
【0001】
【発明の属する技術分野】本発明しむ，魚眼レンズカメラ装置及びその画像歪み補正方法及び画像抽出方法に関
し，特に，魚眼レンズカメラにより画像を取り迏み，そ の一部の画像を切り出してモニタテレビに表示するテレ ビ会議システム又は遠隔監視システム等における魚眼レ ンズカメラ装置及びその画像歪み補正方法及び画像抽出方法に関する。
【0002】魚眼レンズは約180度の画角を有し，広範囲の画像を映し出すことができるが，その画像はたる型に歪曲し，特に周辺部は歪みが著しい。本発明は，魚眼レンズの撮像範囲が広範囲であることを利用し，1台 の魚眼レンズカメラで取り迏んだ画像の中から，注目す る画像の部分を切り出し，画像の歪みを補正してモニタ テレビ画面に表示するものである。
【0003】更に，本発明む，魚眼レンズカメラで映し取った映像の中から，人物の侵入等の動きを伴う像を検出し，その像のモニタ表示領域（切り出し領域）を自動的に決定してその移動像を追尾させるまのであり，遠隔監視システムやテレビ会議システムのカメラ装置に好適 に用いられるものである。
【0004】
【従来の技術】図 13 は従来の魚眼レンズカメラ装置の
構成及びそれを用いた遠隔監視システム及びテレビ会議

システムを示す図である。図の（a）は魚眼レンズカメ ラ装置の構成を示し，図の（b）は魚眼レンズカメラ装置を用いた遠隔監視ジステムを示し，図の（c）は魚眼 レンズカメラ装置を用いたテレビ会議システムを示す。【0005】同図において，13－10ほ魚眼レンズカ メラ装置，13－1は魚眼レンズ，13－2はCCD撮像装置，13－3は映像メモリ（フレームメモリ），1 3－4は画像補正処理回路，13－5は補正映像（NT SC）出力回路である。
【0006】魚眼レンズ13－1は約180度の画角で対象物を光学的に映し出し，CCD撮像装置13－2は光学的な映像から電気的な画像信号を生成し，映像义モ リ（フレームメモリ）13－3はその画像信号をフレー ム単位に記憶する。
【0007】画像補正処理回路13－4は，モニタ表示 する領域について，魚眼レンズの歪んだ画像を補正して元の像に戻し，補正映像（NTSC）出力回路 $13-5$ は，補正された画像信号をNTSC方式等の通常のテレ ビ映像信号として出力する。
【0008】魚眼レンズは画角が広いため，そのレンズ を用いたカメラ装置により広範囲のエリアの映像を取り込む遠隔監視システムやテレビ会議システムを構成する ことができる。図の（b），（c）に示すように，魚眼 レンズカメラ装置13－10に符号化装置13－20を取付け，又は符号化装置付きの魚眼レンズカメラ装置1 3－30により，映像信号を公衆回線13－40を介し て伝送し，復号化装置13－50を介してモニタテレビ画面13－60等に表示することにより，それらのシス テムを構成することができる。但し，魚眼レンズは画角 が広い分，映像の歪みが大きくその歪みを補正してモニ タテレビ西面13－60等に表示しなけらばならない。【OOO9】図14は従来の魚眼レンズカメラ画像の歪 み補正の説明図である。同図において，14－1は仮想 の画像フレーム，14－2は仮想の半球面，14－3は魚眼レンズ撮像画面である。又，x，y，z 軸で示する次元空間の原点○に魚眼レンズが置かれ，且つ，魚眼レ ンズは z 軸の方向に向けて置かれているものとする。
【0010】又，仮想の半球面14－2は，魚眼レンズ が正射影方式のレンズでその焦点距離が f であるとする と，半径f の仮想的な半球の球面であり，その平面部は $\mathrm{x}-\mathrm{y}$ 平面上に置かれ，その中心は原点○の位惪に置か れる。
【OO11】仮想の画像フレーム14－1は，魚眼レン ズの值置（原点）から撮影対象物へ向かう視線方向ベク トルDOV（Direction Of View）と直交する仮想的な平面上のフレームで，所定の大きさの枠を持ち，後に説明するように，この枠内の映像が魚眼 レンズ画像から切り出されてモニタテレビ画面に表示さ れることとなる。即ち，モニタテレビ等の表示フレーム の枠と同じ大きさの枠を持つ。

【OO12】又，画像フレーム14－1は，そのフレー ム内に視線方向ベクトルDOVと交差する点を原点とす る 2 次元座標軸（ $\mathrm{P}, ~ \mathrm{q}$ ）を持ち，仅想画像フレーム 1 4－1内の点はこの座標の成分（ $\mathrm{p}, \mathrm{q}$ ）によって表さ れる。
【0013】魚眼レンズによって映し出きれる像（魚眼 レンズ画像）は，レンズの射影方式（projection fomu 1a）によっていくつかのタイプに分けられるが，以下，正射影（orthographic projection）方式の魚眼レンズ について説明する。
【0014】魚眼レンズの置かれた位置（原点○）から前記仮想の半球面14－2を通して見える像を，そのま ま該仮想の半球面14－2に貼り付けたと仮定する。そ して，その半球面14－2上に貼り付けた3次元空間の像を，図のx暒及びy軸からなる2次元空間の平面上 に，該平面に垂直に（ $z$ 方向から原点方向に）押し潰し て貼り付けた像が，正射影方式の魚眼レンズの画像であ る。
【0 0 1 5 】なお，実際には，魚眼レンズの画像は上下左右逆転した位置に像を結ぶが，像の歪曲の相対的な䦎係は変わらないので，説明を簡略化するため前述したよ うに結像するものとする。
【0016】前記半球面14－2上の像を垂直に押し潰 した2次元空間の平面が魚眼レンズ撮像画面14－3で あり，該魚眼レンズ撮像画面14－3の円の内側の画像 が魚眼レンズで撮影された画像である。外側の四角の枠 は，CCD撮像装置から得られる全体の撮像画面の外枠 である。
【0017】魚眼レンズの画像は歪曲しているため，魚眼レンズカメラで撮影した像を表示するには，その一部 を切り出して正常な画像に補正する必要がある。そこ で，表示するフレームに対応するフレームを仮想の画像 フレーム14－1として想定する。
【0018】魚眼レンズが向いているz軸の方向が，鉛直線の上方の方向であるとし，前記視線方向ベタトルD OVがて軘と成す頂点角（天頂角）をゆ，水平面の基準軸（ x 軸又は y 軸）と成す方位角を $\theta$ とする。又，焦点距㒀（魚眼レンズ两像の円の半径）をf，画像フレーム の回転角を $\omega$ ，拡大率をmとする。拡大率mは，魚眼し ンズの位置（原点O）加ら画像フレーム14－1内の原点までの距䧸をDとすると， $\mathrm{m}=\mathrm{D}$ ノ f である。
【0019】魚眼レン处画像平面14－3内の点（x， y）と画像フレーム14－1内の点（ p ，q）との対応関係は，式（1）の関係式によって表わされる。
【0020】
【数1】


【0021】式（1）の対応関係を利用して魚眼レンズ画像の歪みを補正し，元の画像を復元してモニタテレビ画面に表示させることができる。即ち，先ず前記画像つ レームを14－1を定位させ，モニタ表示する領域（切 り出し領域）を定める。この定位操作は，画像フレーム の頂点角 $\phi$ ，方位角 $\theta$ ，回転角 $\phi$ 及び拡大率 $m$ を外部か ら画像補正処理回路 13－4に入力することによって設定する。
【0022】画像補正処理回路13－4は，画像フレー ム14－1内の点（ p ，q）に対応する魚眼レンズ画像平面14－3内の点（x，y）を，前記式（1）の䦎係式により求め，その点の色情報信号を映像メモり（フレ ームメモリ）13－3から読み出して，画像フレーム1 4－1内の点（p，q）に対応するアドレスを有する出力用の映像メモリ（図示省略）に該色情報信号を書き込 む。
【0023】この映像メモリ間の色情報転送操作を，画像フレーム $14-1$ 内の全ての点（ $\mathrm{p}, \mathrm{q}$ ）について行 い，出力用の映像メモりから順次，色情報信号を補正映像（NTSC）出力回路13－5に送出することによ り，補正映像（NTSC）出力回路 $13-5$ は，原点 $O$ から仮想の画像フレーム14－1の枠を通して見た実物象の画像を，歪みなく表示することができる。（米国特許第5，185，667号明細書等参照）
【0024】
【発明が解決しようとする課題】前述の魚眼レンズ画像 の歪み補正は，対象とする魚眼レンズが正射影の像とな るときの補正であり，実際の魚眼レンボとして多く使用 されている等面積写像の像となる魚眼レンズのときは，座標変㒜の演算が更に複雑なものとなる。
【0025】角眼レンス画像の歪み禣正の演算は，表示 する画像フレームの座標点毎に座標変換の演算を行うた め膨大な演算量となり，又，画像の解像度を上げると更 に演算量が増大することになるので，座標変換の演算量 は極力少ないものとしなけらげならない。
【0026】又，前述の魚眼レンズ画像の歪み補正は，魚眼レンズカメラを机等に設置して天井方向に真上に向 ける，或いは，天井に取り付けて床方向に真下に向ける等，鉛直方向に向けて置くことを前提としているため，

魚眼レンズカメラの設置アングルを自由に選定して設置 することができない。一方，魚眼レンズカメラを壁に横向きに取り付けたり，天井の隅に斜めの角度で取り付け たりした方が，監視領域等の撮像領域を魚眼レンズ画像 のより有効な撮像エリアに取り込むことができる場合が多い。
【0027】更に，魚眼レンズカメラを使って撮影され る映像は，実際には個々の魚眼レンズカメラの特性によ り変動する。この魚眼レンズカメラカメラの特性の相違 は，魚眼レンズ画像の歪み補正による画像変換を行って も，変換後の画像に画像歪みとして残って表示されてし まう。
【0028】従来は魚眼レンズカメラの映像パラメータ である，CCD撮像装置の撮像画面における魚眼レンズ画像の左右方向のずれの補正や，CCDの撮像装置の構造等に起因する縦横比の補正については，手動で調整し なければならなかった。
【0029】又，魚眼レンズカメラを使った追尾型の遠隔監視システムにおいて，人物像等の検出とモニタ表示領域（切り出し領域）の决定を自動的に行なわなければ ならないが，単に魚眼レンズ画像のフレーム間差分によ りモニ夕表示領域（切り出し領域）を決定する方法で は，動く物が1つのみである場合の検出が限界であり，領域内に複数の物が移動する場合にその各々を追尾する映像を作成することは不可能であった。
【0030】又，魚眼レンズ画像は，その中心部と周辺部とで明るさや歪曲の大きさが違っているため，追尾の際の切り出し領域が変化するに伴い，モニタ表示される画像についても不自然になり易いという欠点があった。
【0031】本発明は，魚眼レンズカメラを任意の設置 アングルで取り付けた場合の魚眼レンズ画像の歪み補正 の画像変形処理を高速化するとともに，又，魚眼レンズ カメラで撮影した人物像等の移動方る像を精度よく検出 して抽出し，モニタテレビ等に高精度で表示させること を目的とする。
【0032】
【課題を解決するための手段】本発明の魚眼レンズカメ ラ装置は，（1）魚眼レンズカメラにより撮影きれた画像の雨みを補正する画像補正处理部を備えた魚眼レンズ カメラ装置において，前記画像補正処理部は，魚眼レン ズカメラの設置角を補正する座標変換と，魚眼レンズ画像の歪みを補正する座標変換とを竩み合わせて演算する構成を有するるのである。又，（2）前記两像補正処理部は，等面積写像の魚眼レンズ画像の歪みを補正する座標変換を演算する構成を有するものである。
【0033】又，（3）魚眼レンズカメラにより撮影さ れた画像の歪みを補正する画像補正処理部を備えた魚眼 レンズカメラ装置において，魚眼レンズ画像の歪み補正 のための，表示画像の中心位置，魚眼レンズ画像の緥横比，魚眼レンズ画像エリアの半径等のパラメータを，揖

像きれた魚眼レンズ画像自体から抽出し，該パラメータ により魚眼しンズ画像の歪み捕正を行う構成を備えたも のである。
【0034】又，（4）魚眼レンズカメラにより撮影し た画像から，移動する像を抽する魚眼レンズカメラ装置 において，魚眼レンズ画像内の相互の位置関係を利用し て領域を続合し，像の変化した領域を抽出する構成を備 えたものである。
【0035】又，（5）魚眼レンズカメラにより撮影し た画像から，移動する像を抽出する魚眼レンズカメラ装置において，魚眼レンズ画像をパノラマ状の横長映像に変換し，その映像のフレーム間差分の信号又はフレーム間差分とフレーム内差分とを結合した信号を抽出し，該信号により領域抽出を行い，複数の移動像の領域抽出を同時に行う構成を備えたものである。
【0036】又，（6）魚眼レンズカメラにより撮影し た画像から，移動する像を抽出する魚眼レンズカメラ装置において，フレーム間差分の信号又はフレーム間差分 とフレーム内差分とを結合した信号等の特徴量の抽出演算を魚眼レンズ画像の映像をもとに行い，特徴検出領域 に対する領域抽出処理において，極座標と直交座標との アドレス変換を行って魚眼レンズ画像の映像内を走査 し，円形の魚眼レンズ画像の映像の中から複数の移動像 の領域抽出を行う構成を備えたものである。
【0037】又，（7）魚眼レンズカメラにより撮影し た画像から，移動する像を抽出する魚眼レンズカメラ装置において，魚眼レンズ画像の映像の中から得られる复数の人物像の領域について，各人物像の形状を正規化 L，各像の形状内の色情報を記億し，個々の像の色情報 をもとに移動する複数の人物像を個別に追尾する映像を作成する構成を備えたものである。
【0038】又，（8）魚眼レンズカメラにより撮影し た画像から，移動する像を抽出する魚眼レンズカメラ装置において，魚眼レンズ画像の中心部分と周辺部分との歪みの大きさに応じて異むる重み係数を乗じた特徴量を もとに領域抽出を行う構成を備えたものである。又，
（9）前記重み係数として，更に魚眼レンズ画像の映像内の領域に対応して異なる値を与え，非抽出領域をマス タして領域抽出を行う構成を備えたものである。
【0039】又，本発明の魚眼レンズカメラの画像歪み補正方法は，（10）魚眼レンズカメラにより撮影きれ た画像の歪みの補正において，魚眼レンズカメラの設置角を補正する座標変換と，魚眼レンス两像の歪みを補正 する座標変換とを組み合わせて演算する過程を含むもの である。又，（11）前記魚眼レンズカメラの画像歪み補正において，等面積写像の魚眼レンズ画像の歪みを補正する座標変換を演算する過程を含むものである。
【0040】又，（12）魚眼レンズカメラにより撮影 された画像の歪みの補正において，魚眼レンズ画像の歪 み補正のための，表示画像の中心位置，魚眼レンス画像

の䋡横比，魚眼レンズ画像エリアの半径等のパラメータ を，撮像ざれた魚眼レンズ画像自体から抽出し，該パラ メータにより魚眼レンズ画像の罡み捕正を行う過程を含 むものである。
【0041】又，本発明の魚眼レンズカメラの画像抽出方法恃，（13）魚眼レンズカメラにより撮影した画像 から，移動する像を抽出する画像抽出方法において，魚眼レンズ画像内の相互の位置関係を利用して領域を統合 し，像の変化した領域を抽出する過程を含むものであ る。
【0042】又，（14）魚眼レンズカメラにより撮影 した画像から，移動する像を抽出する画像抽出方法にお いて，魚眼レンズ再像をパノラマ状の横長映像に変換 し，その映像のフレーム間差分の信号又はフレーム間差分とフレーム内差分とを結合した信号を抽出し，該信号 により領域抽出を行い，複数の移動像の領域抽出を同時 に行う過程を含むものである。
【0043】又，（15）魚眼レンズカメラにより撮影 した画像から，移動する像を抽出する画像抽出方法におう いて，フレーム間差分の信号又はフレーム間差分とフレ ーム内差分とを結合した信号等の特徴量の抽出演算を魚眼レンズ画像の映像をもとに行い，特徵検出領域に対す る領域抽出処理において，極座標と直交座標とのアドレ ス変興を行って魚眼レンズ两像の映像内を走査し，円形 の魚眼レンズ画像の映像の中から複数の移動像の領域抽出を行う過程を含せものである。
【0044】又，（16）魚眼レンズカメラにより撮影 した画像から，移動する像を抽出する画像抽出方法にお いて，魚眼レンズ画像の映像の中から得られる複数の人物像の領域について，各人物像の形状を正規化し，各像 の形状内の色情報を記億し，個々の像の色情報をもとに移動する複数の人物像を個別に逭尾する映像を作成する過程を含む゚ものである。
【0045】又，（17）魚眼レンズカメラにより摄影 した画像から，移動する像を抽出する画像抽出方法にお いて，魚眼レンズ再像の中心部分と周辺部分との歪みの大きさに応じて異なる重み係数を乗じた特徴量をもとに領域抽出を行う過程を含むものである。
【0046】又，（18）前記重み係数として，更に魚眼レンズ画像の映像内の領域に対応して異なる値を与
え，非抽出領域をマスクして領域抽出を行う過程を含む ものである。
【0047】
【発明の実施の形態】図1は，本発明の実施の形態の魚眼レンズカメラ装置の構成を示す図である。同図におい て，1－1は魚眼レンズ，1－2ほCCD撮像装置，1 －3は映像メモリ（フレームメモリ），1－4は画像補正処理部， $1-41$ は力メラ設置角補正部， $1-42$ は パン メチルト角回転補正部，1－43はズーム補正部，
1－44は映像補間作成部，1－5は補正映像（NTS

C）出力回路である。
【0048】魚眼レンズ1－1により広範囲の像を光学的に取り迏み，CCD撮像罟置1－2により光学的な像 から電気的な画像信号を生成し，映像メモり（フレーム メモリ） 1 －3はその画像信号をフレーム単位に記憶す る。
【0049】画像補正処理部1－4ほ，魚眼レンズによ る歪んだ画像を補正して元の像に戻な処理を行い，補正映像（NTSC）出力回路1－5は，補正された像の信号を通常のNTSC方式等のテレヒビ映像信号として出力 する。又，この信号を符号化装置により符号化して送信 し，遠隔地で映像表示することもできる。
【0050】画像補正処理部1－4の力メラ設置角補正部1－41は，任意の方向を向いた魚眼レンズカメラ装置の設置角を補正し，パン ノチルト角回転補正部 $1-4$ 2は，映像表示エリア（切り取りエリア）のパン・キル ト角の回転量を制御し，ズーム補正部1－43は，表示映像の拡大率を制御し，映像補問作成部 $1-44$ は，座標点の間の補間を行い，映像表示エリア（切り取りエリ ア）の画像について歪みを補正して元の像に戻す処理を行う。
【0051】図2は本発明の実施の形態の魚眼レンズカ メラで撮影される映像の説明図である。図の（a）は，魚眼レンズカメラが直上を向いた場合の魚眼レンズ两像 imgを示し，図の（b）は，表示対象の魚眼レンズ两像imgを，画像フレームfrmの平面へ写像する様子 を模式的に表し，図の（c）はy軸方向から図の（b） の球を見通した図を示している。魚眼レンズ画像 i mg が正射影方式の画像の場合，図の（a）の魚眼レンズ画像 i mglさz䡉方向から図2の（b）の球を見通した画像となる。
【0052】魚眼レンズカメラをx軸，y軸， z 軸の原点に上方に（ z 䡉方向に）向けて置いたとすると，魚眼 レンズカメラで映される映像は，先ず，原点の周りの距離Rの半経の球の内側に，映像が貼り付けられた状態を想定して解析することができる。
【0053】このように物体までの距離は無視きれて，魚眼レンズカメラによる画像imgは，特定の方角 （ $\mathrm{r}, ~ \theta, \dot{\phi}$ ）から人射された像が， 2 次元の $\mathrm{x}-\mathrm{y}$ 平面で，式（2）の写像変換式により表される点（ x ＂， y＂）へ写像されるるのとみなすことができる。式 （2）において $\theta$ は方位角，$\phi$ は頂点角（天頂角）であ り，Lは頂点角 $\phi$ で入射した像が魚眼レンズ画像上に結像したときの，原点○からの距離（像高）である。
【0054】
【数2】


【0055】即ち，魚眼レンズ画像imgは，3次元極座標（ $\mathrm{r}, \theta, \phi)$ の点から，二次元の（ $\mathrm{x}=, \mathrm{y}$＂） への写像と考えることができる。距㙜（像高）L姟魚眼 レンズの射影方式によって異なり，前述の正射影方式の場合は式（3－1），等面積射影の場合は式（3－
2），等距㒀射影の場合は式（3－3）のように表わさ れる。なぁ，fはレンズの焦点距離である。
【0056】
【数3】

$$
\left.\begin{array}{ll}
\mathrm{L}=\mathrm{f} \sin \phi & \cdots \\
\mathrm{~L}=2 \mathrm{f} \sin \frac{\phi}{2} & \cdot \\
\mathbf{L}=\mathrm{f} \phi & \cdots \cdot(3-1) \\
& \cdots
\end{array}\right) \cdot(3-3)
$$

【0057】図2の（b）において，歪み補正して表示 する画像フレームfrmの方位角を $\theta$ ，頂点角を $\phi$ とす ると，表示画像をパンノチルト操作させることは，この仮想の画像フレームfrmを，3次元座標内で回転した場合に，そこに投影される映像を表示することに一致す る。
【0058】即ち，画像フレームfrm内のラスター上 に並んだ各点の座標に対応する，魚眼レンズ画像 i mg の点の座標を特定し，その座標の点の色情報信号を，表示フレームfrmの座標の点の色情報信号に対応させる ことにより，魚眼レンズ画像imgを元の画像に変換す る補正処理を行うことができる。カメラが，直上または直下を向いている場合には，画像フレームfrmのパン の操作は方位角 $\theta$ を所定量変化させ，又，チルトの操作 は頂点角 $\phi$ を所定量変化させて，対応する魚眼レンズ画像 img内の2次元座標の色情報信号のマッピングを行 えばよい。
【0059】図3は，横方向に向けた魚眼レンズカメラ の撮影画像の説明図である。同四は魚眼レンズカメラを x軸方向に向けた場合を示している。この場合魚眼レン西西像imgは垂直面に形成されることとなる。
【0060】この場合でも前述したような歪み補正によ り，歪みのない画像を表示させることはできるが，その あま，直上の映像として魚眼レンズ画像の変換を行う と，パンノチルトの操作を行ったとき，回転方向が実際 の映像のパンノチルトの方向と違った方向に回転するこ とになる。即ち，直上の映像の場合， Z 蟿との角度 $\phi$ を愛化きせてチルトの操作を行ったが，横方向に魚眼レン ズカメラが向いている場合には角度 $\dot{な}$ 変化きせてもチ ルトの操作にはならない。
【0061】そのため，先ず，歪み補正を行う前に，魚眼レンズカメラの向き，即方，カメラ設置角について補

正を行う。この補正処理は前記カメラ設置角補正部1— 41 により行う。
【0062】図4ほ横方向を向けたた魚眼レンズカメラ画像の補正の説明図である。図るに示したように魚眼し ンズカメラが横暒のx軸の方向を向いている場合，座標采をy軸の回りに予め90度回転させ，魚眼レンズ画像面 i mgがz軸と垂直に交わる位置に回転移動させるこ とにより，パン／チルトの操作に対して，前述した直上 の画像の場合と同等の処理を行うことが可能になる。即 ち，前記角度 $\phi$ を変化きせることによりチルト操作を行 うことができ，又，前記角度 $O$ を変化させることにより パン操作を行うことができる。
【0063】図4に示した例む，魚眼レンズカメラが横方向を向いている場合であったが，魚眼レンズカメラを上，下，横，斜めの任意の方向に向いているとき，鉛直方向をz＇蟿とする座標采を（ $\left.x^{\prime}, y^{\prime}, z^{\prime}\right) ~ と$ L，画像フレームfrm上の点の座標を（ $x^{\prime}, y^{\prime}$ ， $z^{\prime}$ ）で表し，この画像フレームfrm上の点（ $\mathrm{x}^{\prime}$ ， $\left.y^{\prime}, z^{\prime}\right)$ と魚眼レンズカメラの向き（z 軸方向）と の角度を $\phi$ ，画像フレームfrm上の点（ $\mathrm{x}^{\prime}$ ， $\mathrm{y}^{\prime}$ ， $\left.\mathrm{z}^{\prime}\right)$ と x 䡉との角度を $\theta$ ，画像フレーム $\mathrm{frm上の}$ 点 （ $\mathrm{x}^{\prime}, y^{\prime}, z^{\prime}$ ）とy軸との角度をoとすると，式 （4）の回転行列の式を用いて回転座標変換を行うこと により，パン ノチルトの操作方向を実際の映像と一致さ せることができる。ここで，式（4）の回転行列の式の行列 Rx ，Rz，Ryはそれぞれx軸， y 軸， z 軸の回 りに回転を与える行列であり，行列Rxはカメラアング ルに対応した回軽を与える。
【0064】
【数 4 】

$$
\begin{align*}
& {\left[\begin{array}{l}
\mathrm{x} \\
\mathrm{y} \\
\mathrm{z}
\end{array}\right]=\mathrm{Rx} \cdot \mathrm{Ry} \cdot \mathrm{Rz} \cdot\left[\begin{array}{l}
\mathrm{x}^{\prime} \\
\mathrm{y}^{\prime} \\
\mathrm{z}^{\prime}
\end{array}\right]} \\
& \mathrm{Rx}=\left[\begin{array}{ccc}
\cos \theta & -\sin \theta & 0 \\
\sin \theta & \cos \theta & 0 \\
0 & 0 & 1
\end{array}\right]  \tag{4}\\
& \mathrm{Ry}=\left[\begin{array}{ccc}
\cos \phi & 0 & -\sin \phi \\
0 & 1 & 0 \\
\sin \phi & 0 & \cos \phi
\end{array}\right] \\
& \mathrm{Rz}=\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos \rho & -\sin \rho \\
0 & \sin \rho & \cos \rho
\end{array}\right]
\end{align*}
$$

【0065】同一の方位角及びカメラアングル（頂点角）について，前記式（4）の回転行列の式を一度計算 することにより，回転後の座標が（ x ， y ， z ）として得られる。次にこの点の 2 次元座標上の魚眼レンス画像 の点（ x ＂， $\mathrm{y}^{\prime \prime}$ ）への写像を計算するにより，画像フ

レーム上の点と魚眼レンス画像の点と対応きせることが できる。魚眼レンズカメラの設置角についての計算量の増加は，一度だけ回転行列を生成なることによる増加で あり僅がである。
【0066】3次元座標の点 $(x, y, z)$ 加ら 2 次元座標上の魚眼レンズ画像の点 P （ $\left.\mathrm{x}^{\prime \prime}, \mathrm{y}^{\prime \prime}\right)$ への写像 は，先ず，点（ $\mathrm{x}, \mathrm{y}, \mathrm{z}$ ）を極座標表現の点（ r ， $\theta, \phi)$ に変換する。この変換じ，式（5）の極座標変換の式により変換することができる。
【0067】

$$
【 0067 】
$$

$$
\left.\begin{array}{l}
\text { 【数 } 5 】 \\
\mathrm{r}=\sqrt{\mathrm{x}^{2}+\mathrm{y}^{2}+\mathrm{z}^{2}} \\
\theta=\tan ^{-1}(\mathrm{x} / \mathrm{y})=\cos ^{-1}\left(\mathrm{x} / \sqrt{\mathrm{x}^{2}+\mathrm{y}^{-2}}\right) \\
\phi=\cos ^{-1}(\mathrm{z} / \mathrm{y})=\tan ^{-1}\left(\sqrt{\mathrm{x}^{2}+\mathrm{y}^{2}} / \mathrm{z}\right)
\end{array}\right\} \cdot \cdot \cdot(5)
$$

【0071】このようにして，魚眼レンズカメラ設置角 の補正は，先ず，画像変形処理を行う前に，画像フレー ムfrmの矩形領域の座標（ $\mathrm{x}^{\prime}$ ， $\mathrm{y}^{\prime}$ ， $\mathrm{z}^{\prime}$ ）を，回転座標変換により（ $\mathrm{x}, \mathrm{y}$ ， z ）の座標に変換し，その後，該（x，y，z）座標の点を，魚眼レンズ画像の座標上の点（ $\mathrm{x}^{\prime \prime}$ ， $\mathrm{y}^{\prime \prime}$ ）へ変換する。なお， z 軸の成分 はズーム率に相当するため，基本的には（ x ， y ）から （ $\mathrm{x}^{\prime \prime}$ ， $\mathrm{y}^{\prime \prime}$ ）への 2 次元 2 次元変換となる。式（7） の式に関する座標の変換式は，座標軸回転に伴う座標変換と魚眼レンズの特性に伴った写像変換とを一度に計算 することにより，計算回数の削減が図られている。【0072】ここで，前記の演算により求めた角眼レン ズ画像の座標上の点（ $\mathrm{x}^{\prime \prime}, \mathrm{y}^{\prime \prime}$ ）を（u，v）と記 す。この座標点（u，v）を滑らかに補間するために，以下のような補間処理を行う。映像信号の 3 色の色情報


【0068】更に，等面積写像方式の魚眼レンズの場合 は，式（3－2）の式で表されるため，この式を式 （2）に代大することにより，式（6）の式が得られ る。 $\mathrm{x}^{2}+\mathrm{y}^{2}+\mathrm{z}^{2}=\mathrm{x}^{\prime 2}+\mathrm{y}^{\prime 2}+\mathrm{z}^{\prime 2}=\mathrm{r}^{2}$ であること及び式（5）更に三角関数の基本式を利用し て，式（6）の式は式（7）の式のように簡素化きれ る。
【0069】
【数6】

$$
\left.\begin{array}{l}
\mathrm{x}^{\prime \prime}=2 \mathrm{f} \sin \frac{\phi}{2} \cos \theta  \tag{6}\\
\mathrm{y}^{\mathrm{n}}=2 \mathrm{f} \sin \frac{\phi}{2} \cos \theta
\end{array}\right\} \ldots \ldots
$$

【0070】
【数7】

分を，Yu，v，Uu，v，Vu，vとし，又，点 （u，v）の座標成分u，vの小数点を切り捨てて整数化した値を 1 O ， v O とし，座標（ 1 O O ， v 0 ）の点に おける色情報信号Yo値をYuOvOとする。同様に，色情報信号U，VについてもUuOvo，VuOv0に より同様な内容を表す。更に，座標成分 $11, ~ v$ をそれぞ れ小数点を切り上げした値をu1，v1とし，それに対応した座標の色情報信号Y，U，Vの値を，それそれ Y u1v1，Uu1v1，Vu1v1と表す。そして，座標成分 $u$ ， v の小数部をそれぞれ du ， dv とする。
【0073】入力映像信号を式（8）の一次変換の式に より補間してマッピングすることにより，滑らかな画像 を表示きせることができる。
【0074】
【数8】信方成分きY，U，ひとし，

【0075】次に，魚眼レンズカメラの撮像エリアか ら，魚眼レンズカメラのパラメータである画像中心位置
（Xbase，Ybase）及び焦点距離に対応した値 fを自動抽出する手法について説明する。前記のパラメ

ータは魚眼レンズカメラ画像の歪み補正において使用さ れるパラメータである。
【0076】図5は魚眼レンズカメラのバラメータ抽出 の説明図である。同図において5－1は魚眼レンズカメ ラの撮像エリア，5－2は魚眼レンズ画像エリアであ る。円像魚眼レンズを用いたカメラの撮像エリア5－1内には，円形の魚眼レンズ画像エリア5－2が観測され る。この魚眼レンズ画像エリア5－2はカメラ撮像エリ ア5－1内の所定の位置に観測され，又，魚眼レンズ画像エリア5－2の外周は光が到達しないため非常に輝度 の低いエリアとなる。
【0077】そこで，カメラ撮像エリア5－1の全体に ついて，水平及び垂直のそれぞれの方向に関してヒスト グラムを抽出し，魚眼レンズ画像エリアの位置及びその半径を測定守ることができる。
【0078】水平方向のヒストグラム Hh （ n ）と垂直方向のヒストグラムHV（n）とに関して適度な閥値T h ，TVを設定し，撮像エリア画面の両端からヒストグ ラムを測定して最初に閾値Tv，Thを越す点を探索す る。
【0079】その点を水平，垂直それぞれに対して 2 点 ずつ抽出し，水平ヒストグラムから魚眼レンズ画像エリ アの左端X1eft及び右端Xrightの点を検出す ることができる。又，垂直ヒストグラムから魚眼レンズ画像エリアの上端Yup及び下端Ydownの点を検出 することができる。
【0080】上記魚眼レンズ画像エリアの左端X1ef t，右端 Xr ight ，Yup及び下端Ydownの飞 れぞれの位置から，水平方向の半径Rhと垂直方向の半径Rvとを式（9）により抽出することができる。又，画像中心位置（Xbase，Ybase）は式（10） により抽出することができる。
【0081】
【数9】

$$
\left.\begin{array}{l}
\mathbf{R h}=(\text { Xright }- \text { Xleft }) / 2 \\
\mathbf{R v}=(\text { Ydown }- \text { Yup }) / 2
\end{array}\right\} \cdot \cdots \cdot(9)
$$

【0082】
【数10】

$$
\left.\begin{array}{l}
\text { Xbase }=(\text { Xright }+ \text { Xleft }) / 2 \\
\text { Ybase }=(\text { Ydown }+ \text { Yup }) / 2
\end{array}\right\} \cdots(10)
$$

【0083】魚眼レンズ画像エリア5－2は基本的には円形であり，水平方向の半径Rhと垂直方向の半径R v とは等しく，Rh＝Rvとなるが，CCD等の撮像素子 の維横方向のアスペクト比の違いにより，水平方向の半径 R h と垂直方向の半径 Rv とに相違が生じる場合があ る。

【0084】魚眼レンス画像エリア5－2の半径Rは，本来，魚眼レンズの焦点距離もによって定まる値で，例 えば，正射影方式の魚眼レンズでは式（11－1）で表 され，等面積射影方式の魚眼レンズでは式（11－2） で表きれる。
【0085】
【数11】

$$
\begin{array}{ll}
\mathbf{R}=\mathrm{f} & \cdots \cdot \cdot(11-1) \\
\mathbf{R}=\sqrt{2} \mathrm{f} & \cdots \cdot \cdot(11-2)
\end{array}
$$

【0086】従って，前述の魚眼レンズ画像の座標上の点（ $\mathrm{x}^{\prime \prime}$ ， $\mathrm{y}^{\prime \prime}$ ）を求める式（6）の式の計算におい て，水平方向の半径R h と垂直方向の半径R vとに相違 が生じる場合，焦点距離f の値として同一の値を使用す ることなく，方向毎に水平方向の半径Rh又は垂直方向 の半径R v の値を，式（11－1）又は式（11－2） のRの値に代入することによりfの値を修正し，アスペ クト比の違いを考虑した魚眼レンズの歪み補正を行うこ とができる。
【0087】図6は本発明の第1の実施の形態の移動像検出装置の棤成を示す図である。同図において， $6-1$ は魚眼レンズカメラ，6－2，6－3はフレームバッフ フ， $6-4$ ， $6-5$ はフレーム間差分計算部， $6-6$ は領域重みテーブル，6－7は領域抽出部である。
【0088】魚眼レンズカメラ6－1により撮影した画像信号を第1のフレームバッファ6－2に格納し，第1 のフレームバッファ6－2に格納した画像信号を第2の フレームバッファ6－3に格納する。第2のフレームバ ッファ6－3には1フレーム前の画像信号が格納され る。
【0089】そして，第1のフレームバッファ6－2か ら出力される画像信号と第2のフレームバッファ6－3 から出力きれる画像信号とにより，そのフレーム間差分 を第1のフレーム間差分計算部6－4により計算し，移動像に対して大きな値となるフレーム間差分信号を第2 のフレーム間差分計算部6－5に出力する。
【0090】第20フレーム間差分計算部6－5は，第 1のフレーム間差分計算部6－4から出力されるフレー ム間差分信号と，領域重みテーブル6－6から出力され る領域に対応した値とにより，フレーム間差分信号に領或に応じた重み付けを行い，その信号を領域抽出部6－ 7 に出力する。
【0091】領域抽出部6－7は，領域に応じた重み付 けを持つフレーム間差分信号により，移動像の検出を行 って検出フラグ信号を出力するとともにその検出領域を抽出し，領域情報を出力する。
【0092】図7は本発明の第2の実施の形態の移動像検出装置の構成を示ず図である。同図において，7－1 は魚眼レンズカメラ，7－2，7－3はフレームバッフ 7，7－4はフレーム間差分計算部，7－5はフレーム

内差分計算部，7－6は動輪郭抽出部，7－7は領域重 みテーブル，7－8は領域抽出判定部，7－9は領域抽出部である。
【0093】魚眼レンズカメラ7－1により撮影した画像信号を第1のフレームバッファ7－2に格納し，第1 のフレームバッファ7－2に格納した画像信号を第2の フレームバッファ7－3に格納する。第2のフレームバ ッファ7－3には1フレーム前の画像信号が格納きれ る。
【0094】そして，第1のフレームバッファ7－2か ら出力される画像信号と第2のフレームバッファ7－3 から出力きれる画像信号とにより，そのフレーム間差分 をフレーム間差分計算部7－4により計算し，移動像に対して大きな値となるフレーム間差分信号を動輪郭抽出部7－6に出力多る。
【0095】フレーム内差分計算部7－5は，第1のフ レームバッファ7－2加ら出力きれる画像信号のフレー ム内の差分を計算し，像の輪郭部で大きな値となるフレ一ム内差分信号を動輪郭抽出部 $7-6$ に出力する。
【0096】動輪郭抽出部7－6は，フレーム間差分計算部 $7-4$ からのフレーム間差分信号と，フレーム内差分計算部 $7-5$ からのフレーム内差分信号とを線形結合 させ，輪郭部が強調された移動像の信号を生成し，その信号を領域抽出判定部7－8に出力する。

$$
D_{n}(x, y)=P_{n}(x, y)-P_{n-1}(x, y) \quad \cdots(12)
$$

【0101】即ち，図6に示した第1のフレーム間差分計算部6－4から出力されるフレーム間差分信号，又は図7に示した動輪郭抽出部7－6から出力されるフレー ム間差分及びフレーム内差分を線形結合させた信号を，移動像抽出のための特徵量 $\mathrm{D}_{\mathrm{n}}$（ $\mathrm{x}, \mathrm{y}$ ）をとすると，

$$
G_{n}(x, y)=W(x, y)
$$

【0102】このように魚眼レンズ画像の領域に応じて重み付けられた特徴量Gn（x，y）を用いて抽出を行 う処理により，魚眼レンズ画像エリプ内の領域毎に対応 した等価的なマスク及び強調操作を行うことができる。
【0103】図8は魚眼レンズ再像の領域に応じた重み係数W（x，y）の説明図である。同図は魚眼レンズ画像の領域内を3つの領域8－1，8－2，8－3に分割 し，を領域8－1には重み係数 0 ，領域 $8-2$ には重み係数1，領域8－3には重み係数2を割り当てた例を示 している。
【0104】魚眼レンズ画像の周辺部分では中心部分に比べて同一面積の領域が小さな領域に表示される。その ため周辺部にあける移動像検出の精度が低下するが，周辺部の重み係数 $\mathrm{W} ~(\mathrm{x}, \mathrm{y})$ を大きな値としておくこと により，周辺部における精度低下を補備することができ る。更に，通常，周辺部分に人物像が存在する確率が高 いので，周辺部分を大きな值をとし，中心部分で○に近 い値としておく。
【0105】又，魚眼レンズカメラでは撮像エリアが広

式（13）により，この特徵量 $\mathrm{D}_{\mathrm{n}}(\mathrm{x}, \mathrm{y})$ と魚眼し ンス画像の領域に応じた重み係数W（x，y）との積 G n（ $\mathrm{x}, \mathrm{y}$ ）を移動像抽出のための特徴量として用い る。
－ $\mathrm{D}_{\mathrm{n}}(\mathrm{x}, \mathrm{y}) \quad \cdots(13)$
大であるため，照明等が直接撮像エリア内に入ることが多い。このような場合でも極端な輝度の違いを，等価的 な領域マスクにより補貨して移動像の誤検出を低減ざせ ることができる。
【0106】領域域抽出部6－7，7－9は，領域対応 の重み付けがされた特徴量を，予め設定きれた閾值（T hm ）と比較することにより，人物像等の像検出判定処理を行う。この像検出判定処理を伴う領域抽出处理を魚眼レンズ画像の全画面について行う。
【0107】図9は領域抽出された人物等の像の例を示 す図である。図の（a）は魚眼レンズ画像エリアを示 し，魚眼レンズカメラが机上等に上を向けて置かれ，を のカメラの周りに4人の人物が着席している場合の魚眼 レンズ画像の例を示している。9－1乃至9－4は人物像検出エリア（A）乃至人物像検出エリア（D）であ る。図の（b）は魚眼レンズ画像の人物像の形状を示 L，人物を下側から魚眼レンズで撮影した場合には体底部が長く，頭長部の短い略台形状のような形状となり，人物像を該形状に正規化することができる。

【0097】領域抽出判定部7－8は，動輪郭抽出部7 －6から出力される輪郭部が強調された移動像の信号
と，領域重みテーブル $7-7$ から出力される領域に対応 した値とにより，移動像の信号に領域に応した重み付け を行い，その信号を領域抽出部7－9に出力する。
【0098】領域抽出部7－9は，領域に応じた重み付 けを持つ移動像の信号により，移動像の検出を行って検出フラグ信号を出力するとともにその検出領域を抽出 し，領域情報を出力する。
【0099】図6及び図7に示した本発明の実施の形態 か移動像検出㳖置は，移動像か領域抽出にむいて領域に対応して映像信号に重み付けを行い，魚眼レンズによる画像の歪みによる検出パラメータ信号への影響を低減し ている。
【0100】即ち，通常，nフレームの映像信号P n（ x ， y ）と $\mathrm{n}-1$ フレームの映像信号 $\mathrm{P}_{\mathrm{n}-1}$（ x ， y）とのフレーム間差分 $\mathrm{D}_{\mathrm{n}}$（ $\mathrm{x}, \mathrm{y}$ ）を計算する場合 に，式（12）により計算を行うが，本発明は，魚眼し シズ画像の領域に対応した特徴抽出の重み係数W（ x ， y）を格納した領域重みテーブル 6－6，7－7を備 え，この重み係数W（ x ， y ）を前記フレーム間差分 D n （x，y）に乗じた値 $G_{\mathrm{n}}(\mathrm{x}, \mathrm{y})$ を用いて移動像 の抽出処理を行う。

【0108】図の（a）に示すような魚眼レンズ画像エ リアのイメージ上をラスタースキャンし，人物像として の特徴量の大きい点を検出すると，その点から下方八略台形状のような形の像の探索を行い，その領域を切り出 す。
【0109】切り出された領域に対して大きさ及び形状 についての照合を行い，人物像の領域であるかどうかの判定を行う。同様の処理を複数の領域に対して同時に処理し，複数の人物像が検出きれたときは複数の人物像の同時切り出しを行う。
【 O 1 1 O 】 又，個々 の切り出された領域について，図 の（b）に示すような人物の頭頂部，体底部及び体高の それぞれのパラメータ及びその内側の色データを左右及 び高き方向にサンプリングすることにより，画像毎の人物像識別のためのデータバースとすることができる。
【0111】抽出された特徴量から人物像等の領域を抽出する処理に関しては，基本的に通常の力メラ映像での領域抽出のためのアルゴリズムを使用することができる が，魚眼レンズ画像施円形に歪曲して配置されているた め，座標変換を施す必要がある。
【0112】座標変換の方法として以下の二つの方式が ある。第一の方式は，魚眼レンズ画像を，360度のパ ノラマ映像として座標変換された映像へと写像変換を行 う方式である。この方式は円形の魚眼レンズ撮像エリア を矩形エリアへ変換する。
【0113】第二の方式としては，領域抽出を通常のラ スタースキャンとして走査し，走査時の座標系のみを直交座標（ $\mathrm{x}, \mathrm{y}$ ）から極座標（ $\mathrm{r}, ~ O) へ と$ 変換する方式である。即方， $\mathrm{x}=\mathrm{rcos} \theta, \mathrm{y}=\mathrm{rsin} \theta$ とし て領域抽出の処理を行う。
【 0 1 1 4 】 第一の方式は，パノラマ映像に展開するた めの大きなメモりが必要になる欠点があるが，変換後は通常の画像に対する領城抽出処理をそのまま適用するこ とができる。第二の方式は領域抽出処理時に常に座標変換を行いながら処理しなければならないが，使用するメ モリ量は原再としての魚眼レンズ画像を与えるメモリ量 のみでよくコンパクトなシステムを構築することができ る。
【0115】そして，特徴量を抽出し，上下関係等，既知の映像の相互関係を利用して領域の統合処理を行う。例えぼ，真上を向いた魚眼レンズカメラの場合は，魚眼 レンズ画像の中心を上，周辺を下とした映像の位置関係 を利用して領域を統合し，その領域が背景像から人物像 に変化した領域を抽出する。
【0116】人物の侵入等の移動像の追尾処理に関して は，切り出された略台形状の人物領域内を上下左右に前 もって決められた分割数で等分する格子点を算出し，そ の格子点での色情報信号を人物像の特徴量として保存す る。そして，この人物像の特徴量の登録処理と人物像の切り出し処理とを任意の時間間隔で繰り返し行い，複数

の人物像が魚眼レンズカメラ撮像エリア内に存在する場合でも，各人物像を個別に追尾することができる。
【 O 1 1 7 】 図 1 Oは本発明の実施の形態の人物像抽出位置決定の処理のフローチャートである。先ず，魚眼し ンズ画像内の人物像等の切り出し処理のコマンドを与え （10－1），フレームについてのループ処理（10－ 2）により，フレーム間差分による又はフレーム間差分 とフレーム内差分とによる人物像等の特徵量を抽出し
（10－3），魚眼レンズ画像内の領域に対応した重み付け処理を行い（ $10-4$ ），魚眼レンズ画面内のラス ターループ処理を行い（10－5），特徴点を検出し （10－6），略台形上のエリアについて魚眼レンズ画像の座標変換を行って特徴点を抽出の処理を行い（10 －7），特徴点があるかどうかを判定し（10－8），特徵点がある場合には，抽出点を消去し（10－9）， （ $\mathrm{x}, \mathrm{y}$ ）座標の領域の最大値と最小値とを記憶し（1 0－10），最終ラインかどうかを判定し（10－1 1），最終ラインであれで終了する（10－12）。【0118】前記特徴点があるかどうかの判定（10－ 8）において，特徴点がない場合，複数ライン連続して特徴点がないかどうかを判定し（10－13），連続し て特徴点がない場合は領域数をカウントして人物領域を記憶し（10－14），前述の最終ラインかどうかの判定し（10－11）に移る。
【0119】前記複数ライン連続して特徵点がないかど ラかめ判定（10－13）において，複数ライン連続し ていなければ前記特徴点を検出する処理（10－6）に戻る。又，前記最終ラインかどうかの判定（10－1
1）において，最終ラインでないときは前記特徰点を検出する処理（10－6）に戻る。
【0120】人物像の存在領域を抽出すると，その領域 から魚眼レンズ画像を補正して表示するためのパラメー夕を求めることができる。図11は本発明の実施の形態 の領域切り出し及び表示画面作成を行う構成の説明図で ある。同図において，11－1は領域抽出部，11－2 は領域切り出し部，11－3は魚眼レンズ画像パラメー夕決定部，11－4は表示画面作成部である。
【 0 1 2 1 】 領域抽出部 1 1－1 は，前述の図6及で図 7に示した領域抽出部6－7，7－9と同一のものであ り，特徴量により人物像等を検出し，その領域を抽出す ると，検出フラグ及び領域情報め信号を出力する。検出 フラグの信号は警報又は通知用の信号として使用するこ とができる。領域情報の信号は領域切り出し部11－2 に出力きれる。
【0122】領域切り出し部11－2は，領域情報か信号に基づいて領域を切り出し，魚眼レンズ画像パラメー夕決定部11－3は，切り出きれた全領域について魚眼 レンズ画像を補正して表示するためのパラメータを決定 L，そのバラメータの信号を画面作成部11－4に送出 する。画面作成部 $11-4$ は，パラメータの信号に基づ

いて表示画面を生成し，映像信号を出力する。
【0123】ここで，簡単化のために，真上を向いた力 メラアングルの場合の魚眼レンズ画像の前記パラメータ の決定について説明する。魚眼レンズ画像の補正のため のパラメータとしては，画像フレームの方位角 $\theta$ ，頂点角 $\phi$ 及び拡大率mが必要である。
【0124】魚眼レンズ画像の領域から，例えば，图9 の（a）の人物像検出エリア（B）9－2を抽出して表示するとする。この場合，人物像検出エリア（B）9－ 2の中心位置に関する角度 $\alpha$ 及び魚眼レンズ画像の中心 Oから人物像検出エリア（B）9－2を挟む角度（立体角）$\beta$ を計算する。又，魚眼レンズ画像の中心Oから領域最上部までの距離Lを計算する。
【0125】前記角度 $\alpha$ 及び距離Lにより，人物像検出 エリア（B）9－2を表示する画像フレームの方位角 $\theta$ と頂点角 $\phi$ の値を求めることができる。即ち，方位角 $\theta$以前記角度 $\alpha$ に等しく，$\theta=\alpha$ である。又，頂点角 $\phi$ は魚眼レンズ画像の半径Rと前記距離Lとの比から式 （3－1）乃至式（3－3）を用いて求めることができ る。又，ズーム率であるmについては，領域の左端及び右端と魚眼レンズ画像の中心○との立体角 $\beta$ により求め ることができる。これらのパラメータを元に，個々の人物の表示領域を切り出し，魚眼レンズ画像の歪曲を補正 してモニタテレビ等に映像信号を送出する。
【0126】図12は1台の魚眼レンズカメラで撮影し た画像を合成した映像を示す図である。前述したように魚眼レンズ画像から人物像をその特徴量により抽出し，抽出した画像に歪み補正の処理を行い，1台のモニタテ レビ画面を 4 分割して前記抽出した人物像を表示させた様子を模式的に示している。
【0127】
【発明の効果】以上說明したように，本発明によれば，約180度の広い画角を持つ魚眼レンズカメラにより映像を取り込さので，1台のカメラにより広範囲のエリア を監視することができ，設置力メラ台数を削減すること ができるとともに，その画像を精度よく高速に補正して表示することができる。
【0128】又，魚眼レンズカメラの設置角を補正する座標変換と，魚眼レンズ画像の歪みを補正する座標変換 とを組み合わせて演算することにより，設置角度によら ず画像補正の演算処理を高速に行うことができる。又，魚眼レンズ画像の柾み補正のためのバラメータを，摄像 きれた魚眼レンズ画像自体から抽出して魚眼レンズ画像 の歪み捕正を行うことにより，設置時の調整や経年変化 に対して，安定した歪み補正を行うことができる。
【0129】魚眼レンズ画像の中心部分と周辺部分との歪みの大きさに応じて異なる重み係数を乗じた特徴量を もとに領域抽出を行うことにより，歪みの大きい周辺部分での人物像等の検出を安定して行うことができ，更 に，重み係数として，更に魚眼レンズ画像の映像内の領

域に対応して異なる値を与えて非抽出領域をマスクする ことにより，人物像等の抽出処理における不安定要素を予め取り除くことができる。
【0130】又，魚眼レンズカメラにより取り込んだ広範囲の画像の中から，任意の部分を切り出してモニタテ レビ画面に表示するなど映像作成の自由度が大きく，遠隔監視システムやテレビ会議システムのカメラに適用す ることにより，利便性の向上を図ることができる。
【 0 1 3 1 】 更に，魚眼レンズカメラで映し取った映像 の中から，人物の侵入等の動きを伴う像を検出し，その像のモニタ表示領域（切り出し領域）を自動的に決定し て滑らかな動きで追尾する電子追尾型の遠隔監視システ ム又はテレビ会議システムを構成することができる。
【図面の簡単な説明】
【図1】本発明の実施の形態の魚眼レンズカメラ装置の構成を示す図である。
【図2】本発明の実施の形態の魚眼レンズカメラで撮影 される映像の説明図である。
【図3】横方向に向けた魚眼レンズカメラの撮影画像の説明図である。
【図4】横方向を向けた魚眼レンズカメラ画像の補正の説明図である。
【図5】魚眼レンズカメラのパラメータ抽出の説明図で亦る。
【図6】本発明の第1の実施の形態の移動像検出装置の構成を示す図である。
【図7】本発明の第2の実施の形態の移動像検出装置の構成を示す図である。
【図8】魚眼レンズ画像の領域に応じた重み係数W （ $\mathrm{x}, \mathrm{y}$ ）の説明図である。
【図9】領域抽出された人物等の像の例を示す図であ る。
【図10】本発明の実施の形態の人物像抽出位置決定の处理のフローチャートである。
【図11】本発明の実施の形態の領域切り出し及び表示画面作成を行う構成の説明网である。
【図12】1台の魚眼レンズカメラで撮影した画像を合成した映像を示す図である。
【図13】従来の魚眼レンズカメラ装置の棤成及びそれ を用いた遠隔監視システム及びテレビ会議システムを示 す図である。
【図14】従来の魚眼レンズカメラ画像の柾み補正の説明図である。
【符号の説明】

```
1-1 魚眼レンズ
1-2 CCD撮像装置
1-3 映像メモり(フレームメモリ)
1-4 画像補正処理部
1-41 カメラ設置角補正部
1-42 パン/チルト角回転補正部
```

$$
\begin{array}{ll}
1-43 & \text { ズーム補正部 } \\
1-44 & \text { 映像補間作成部 }
\end{array}
$$

【図1】



【図3】
横方凧に问けた魚腿レンズカメラの摄影画像の訜㫜図


1－5 補正映像（NTSC）出力回路

【図2】


〔図4】
横分向を向けた魚眼レンズカメラ画像の補正の説明図


【図5】
【図6】
【図7】


【図12】


1台の鮘眼レンズカメラで撮影した画像を合成しだ映像を示す図


## 【図9】

領域抽出された人物等の像の侧を示す図
（a）

（b）

【図10】


【図11】

本発明 $\Phi$ 実施の形態の
領城切り出し及び表示面面作成を行う構成 説明図


【図13】

従来の魚眼レンズカメラ装置の構咸及びそれを用いだ遠隔監視システム及びデレビ会諴システムを示す図



## 【図14】



フロントページの続き
（51）Int．C1．${ }^{6}$
識別記号
F I
HO4N 5／781 520A

## EXHIBIT 8

| [54] | WIDE-ANGLE LENS |  |
| :---: | :---: | :---: |
| [75] | Inventor: | Toshiyuki Inoue, Nagano, Japan |
| [73] | Assignee: | Sankyo Seiki Mfg. Co., Ltd., Nagano-ken, Japan |
| [*] | Notice: | This patent issued on a continued prosecution application filed under 37 CFR 1.53 (d), and is subject to the twenty year patent term provisions of 35 U.S.C. 154(a)(2). |
|  |  | This patent is subject to a terminal disclaimer. |
| [21] | Appl. No.: 08/757,192 |  |
| [22] | Filed: | Nov. 27, 1996 |
|  | Related U.S. Application Data |  |
| [63] | Continuation-in-part of application No. 08/590,725, Jan. 24, 1996, abandoned, which is a continuation of application No. $08 / 251,623$, May 31, 1994, abandoned, which is a continuation of application No. 07/738,854, Jul. 31, 1994, abandoned. |  |
| [30] | Foreign Application Priority Data |  |
| Aug. 28, 1990 |  | [JP] Japan ................................ 2-225975 |
| [51] | Int. Cl. ${ }^{7}$ | ...................................... G02B 13/18 |
| [52] | U.S. Cl. | .................... 359/717; 359/739; 359/793 |
| [58] | Field of | $\begin{array}{r} \text { earch .................................. 359/642-648, } \\ 359 / 664,670,708,713-717,744-753 \\ 793 \end{array}$ |
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## ABSTRACT

The present invention is directed toward a wide-angle lens. Because of a small quantity (two) of lens elements, the wide-angle lens facilitates size and weight reduction and permits low-cost manufacture. The lens is made from plastic, which permits further cost reduction. The lens is particularly useful when employed in CCD cameras.

15 Claims, 7 Drawing Sheets



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FIG. 4


FIG. 5



COMA ABERRATION
FIG. 7

> SPHERICAL ABERRATION

$y=0$

ASTIGMATISM


$$
y=1.74
$$


COMA ABERRATION

FIG. 8

## SPHERICAL ABERRATION



$$
y=0
$$



ASTIGMATISM

$y=1.45$


FIELD CURVATURE


$$
y=2.69
$$



FIG. 9


FIG. 10

## WIDE-ANGLE LENS

This is a continuation-in-part of application Ser. No. 08/590,725, filed Jan. 24, 1996, now abandoned, which in turn, was a continuation of application Ser. No. 08/251,623, filed May 31, 1994, now abandoned, which, in turn, was continuation of application Ser. No. 07/738,854, filed Jul. 31, 1991, now abandoned.

## BACKGROUND OF THE INVENTION

## 1. Field of the Invention

The invention relates to a wide-angle lens. More particularly, the invention relates to a wide angle lens having particular application to CCD-type cameras.
2. Background Prior Art

Lately, small-sized wide-angle lenses have become increasingly used in $1 / 2$ - and $1 / 3$-inch CCD cameras which have recently been put into use.

Five-element wide-angle lenses are a common known type of such small-sized lenses.

However, such wide-angle lenses have practical limitations in size, weight and cost because they employ as many as five lens elements.

## OBJECT OF THE INVENTION

The present invention was designed to solve the problems mentioned above. Its primary object, therefore, is to provide a novel wide-angle lens which can easily be decreased in size and weight and manufactured at a low cost.

For a better understanding of the present invention, reference is made to the following description and accompanying drawings while the scope of the invention will be pointed out in the appended claims.

## BRIEF DESCRIPTION OF THE DRAWINGS

FIGS. 1 to 5 show the lens construction of corresponding embodiments 1 to 5 .

FIGS. 6 to 10 show aberrations of embodiments $\mathbf{1}$ to $\mathbf{5}$, respectively.

## DESCRIPTION OF INVENTION AND PREFERRED EMBODIMENTS

The wide-angle lens system 20 according to the invention comprises a first lens element and a second lens element which are located on object and image (picture) sides, respectively. In the drawings, a first lens element is designated as 26 and a second lens element is designated as 28. The first lens element 26 is a meniscus type having a negative refractive power and the second lens element $\mathbf{2 8}$ is a two sided convex type having a positive refractive power, one or more of lens surfaces of lens elements 26,28 being made aspherical.

The wide-angel lens system 20 can be used in $1 / 2$ - and $1 / 3$-inch CCD cameras, for example.

The quantity of the component lens element of the wideangle lens system 20 according to the present invention is thereby reduced to two. In order to secure high performance with the small quantity of lens elements, however, they are made aspherical.

In order to make its performances more effective, the wide-angle lens according to the invention is made to satisfy the following requirements.

$$
\begin{equation*}
\left|f_{1}\right|<D \tag{1}
\end{equation*}
$$

wherein $\left(f_{1}\right)$ is the focal length of the first lens element 26 and D is the distance between the principal points of the first and second lens elements 26, 28.

When satisfying requirement (1), the wide-angle lens system 20 permits its back-focus to be made two times longer despite its short focal length.

$$
\begin{equation*}
-1.5<r_{2} /\left\{\left(n_{1}-1\right) \mathrm{f}_{1}\right\}<-0.5 \tag{2}
\end{equation*}
$$

wherein ( $r_{2}$ ) is the curvature radius of the image-side surface of the first lens element 26 and $\left(\mathrm{n}_{1}\right)$ is the refractive index of the material from which the first lens element 26 was constructed.
When satisfying requirement (2), the wide-angle lens system 20 permits astigmatism to become positively large or negatively large above the upper limit of requirement (2) or below its lower limit respectively.

$$
\begin{equation*}
-10<\mathrm{K}_{4}<-1 \tag{3}
\end{equation*}
$$

wherein $K_{4}$ is the conical reflection constant when the image-side surface of the second lens element $\mathbf{2 8}$ is aspherical.

When satisfying requirement (3), the wide-angle lens system 20 permits spherical aberration to be well corrected. Namely, spherical aberration becomes negatively large or positively large above the upper limit of requirement (3) or below its lower limit respectively.

$$
\begin{equation*}
-2<\mathrm{f}_{1} / \mathrm{f}_{2}<-1 \tag{4}
\end{equation*}
$$

wherein $\left(f_{2}\right)$ is the focal length of the second lens element 28.

When satisfying requirement (4), the wide-angle lens system 20 permits field curvature to be well corrected. Namely, field curvature becomes positive or negative above the upper limit of requirement (4) or below its lower limit respectively When not satisfying requirement (4), its lowers performance of the lens system 20.

The wide-angle lens system 20 according to the invention permits achromatism even when its first and second lens elements 26, 28 are made from the same material.

When the first and second lens elements 26, 28 are made from acryl (PMMA), the wide-angle lens system 20 permits material and manufacturing costs to be reduced further.

The invention will be more fully understood by describing five embodiments as follows.
It is assumed that the first lens surface counted from the object side (including lens surface, diaphragm and CCD cover glass) has a curvature radius $r_{i}(i=1-7)$ and a distance $\mathrm{d}_{i}(\mathrm{i}=1-5)$ is given between the (i)-th and (i+1)-th surfaces on the optical axis. Formula $j=1,2$ represent the first and second lens elements respectively, $\mathrm{j}=3$ the above mentioned cover glass, $\left(n_{j}\right)$ refractive index of the material of the lens elements and cover glass $j=1-3$.

Aspherical surface of the lens elements of the wide-angle lens is obtained by revolving curve:

$$
X=\left[C Y^{2} /\left\{1+\sqrt{\left.1-(K+1) C^{2} Y^{2}\right\}}\right]+A_{4} Y^{4}+A_{6} Y^{6}\right.
$$

about the optical axis (X) with optically-axial coordinate and the coordinate orthogonal therewith given symbols $X$ and $Y$ respectively, optically-axial curvature $C$, conical reflection constant $\mathrm{K}, \mathrm{A}_{4}, \mathrm{~A}_{6}$ quarternary and hexanary aspherical coefficients, and its configuration is specified by giving conical reflectin constant $K$ ans aspherical coefficients $A_{4}$, $\mathrm{A}_{6}$.

| i | Picture size: $1 / 3$ inch (diagonal distance: 5.5 mm ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{r}_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | j | $\mathrm{n}_{\mathrm{j}}$ |
| 1 | 40.00 | 1.00 | 1 | 1.491 |
|  | 3.16 | 8.50 |  |  |
| 3 | 4.38 | 2.50 | 2 | 1.491 |
| 4 | -5.03 | 0.00 |  |  |
| 5 | (Diaphragm) | 6.22 |  |  |
| 6 | $\infty$ | 0.70 | 3 | 1.5168 |
| 7 | $\infty$ |  |  |  |

Aspherical surface: $\mathrm{r}_{4}$
$\mathrm{K}=-4.16934$
$\mathrm{A}_{4}=2.19540 \times 10^{-3}, \mathrm{~A}_{6}=2.19540 \times 10^{-3}$
$\mathrm{f}_{1}=-7.04, \mathrm{f}_{2}=5.22, \mathrm{D}=8.68, \mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1\right) \mathrm{f}_{1}\right\}=-0.91$
$\mathrm{f}_{1} / \mathrm{f}_{2}=-1.35$
The first and second lens elements $\mathbf{2 6}, \mathbf{2 8}$ were made from PMMA (acryl). The configuration of the lens and associated light paths according to the first embodiment are illustrated in FIG. 1 and the aberrations of the first embodiment are illustrated in FIG. 6. The coma aberration shown therein is obtained in connection with (d)- line.

Embodiment 2
$\mathrm{f}=5.0 \mathrm{~mm}, \mathrm{~F} / \mathrm{No}=1.8$

| i | Picture size: $1 / 2$ inch (diagonal distance: 8.0 mm ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{r}_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | j | $\mathrm{n}_{\mathrm{j}}$ |
| 1 | 100.00 | 1.00 | 1 | 1.491 |
| 2 | 4.32 | 12.00 |  |  |
| 3 | 7.32 | 3.00 | 2 | 1.491 |
| 4 | -7.05 | 0.00 |  |  |
| 5 | (Diaphragm) | 10.58 |  |  |
| 6 | $\infty$ | 0.70 | 3 | 1.5168 |
| 7 | $\infty$ |  |  |  |

Aspherical surface: $\mathrm{r}_{4}$

$$
\begin{aligned}
& \mathrm{K}=-2.70060 \\
& \mathrm{~A}_{4}=6.15920 \times 10^{-4}, \mathrm{~A}_{6}=4.25890 \times 10^{-6} \\
& \mathrm{f}_{1}=-9.21, \mathrm{f}_{2}=7.84, \mathrm{D}=13.16, \mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1 \mathrm{f}_{1}\right\}=-0.95\right. \\
& \mathrm{f}_{1} / \mathrm{f}_{2}=-1.17
\end{aligned}
$$

The first and second lens elements 26, 28 were made from PMMA (acryl). The configuration of the lens and associated light paths according to the second embodiment are illustrated in FIG. 2 and the aberrations of the second embodiment are illustrated in FIG. 7. The coma aberration shown therein is obtained in connection with (d)- line.
$\mathrm{f}=3.3 \mathrm{~mm}, \mathrm{~F} / \mathrm{No}=1.8$

35

40

45
50

Aspherical surface: $r_{3}$
$K=-1.76816$
$\mathrm{A}_{4}=2.20288 \times 10^{-5}, \mathrm{~A}_{6}=-6.86197 \times 10^{-7}$
Aspherical surface: $\mathrm{r}_{4}$

## $\mathrm{K}=-2.83668$

$\mathrm{A}_{4}=-6.15852 \times 10^{-6}, \mathrm{~A}_{6}=2.98626 \times 10^{-7}$
$\mathrm{f}_{1} / \mathrm{f}_{2}=-1.41$
The first and second lens elements 26, 28 and cover glass 32 were made from the same material (BK7). The configuration of the lens and associated light paths according to the third embodiment are illustrated in FIG. 3 and the aberrations of the third embodiment are illustrated in FIG. 8. The coma aberration shown therein is obtained in connection with (d)- line.
$\mathrm{f}=5.0 \mathrm{~mm}, \mathrm{~F} / \mathrm{No}=3.5$


## Embodiment 4

 $\qquad$
Picture size: $1 / 3$ inch (diagonal distance: 5.5 mm )

| i | $\mathrm{r}_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | j | $\mathrm{n}_{\mathrm{j}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 16.500 | 1.500 | 1 | 1.49091 |
| 2 | 2.663 | 6.000 |  |  |
| 3 | 5.050 | 2.000 | 2 | 1.49091 |
| 4 | -5.328 | 0.200 |  |  |
| 5 | (Diaphragm) | 5.875 | 3 | 1.51680 |
| 6 | $\infty$ | 4.600 | 3 |  |
| 7 | $\infty$ |  |  |  |

Aspherical surface: $r_{3}$
$\mathrm{K}=-2.27678$
$\mathrm{A}_{4}=0, \mathrm{~A}_{6}=$
Aspherical surface: $\mathrm{r}_{4}$
$\mathrm{K}=-9.5$
$\mathrm{A}_{4}=0, \mathrm{~A}_{6}=0$
$\mathrm{f}_{1}=-6.708, \mathrm{f}_{2}=5.639, \mathrm{D}=6.900, \mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1\right) \mathrm{f}_{1}\right\}=-0.809$
$\mathrm{f}_{1} / \mathrm{f}_{2}=-1.190$
The first and second lens elements $\mathbf{2 6}, \mathbf{2 8}$ were made from PMMA (acryl). The configuration of the lens and associated light paths according to the fourth embodiment are illustrated in FIG. 4 and the aberrations of the fourth embodiment are illustrated in FIG. 9. The coma aberration shown therein is obtained in connection with (d) - line.

Embodiment 5
$\mathrm{f}=5.0 \mathrm{~mm}, \mathrm{~F} / \mathrm{No}=2.5$

| i | Picture size: $1 / 3$ inch (diagonal distance: 5.5 mm ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{r}_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | j | $\mathrm{n}_{\mathrm{j}}$ |
| 1 | 21.000 | 1.500 | 1 | 1.49091 |
| 2 | 2.805 | 6.800 |  |  |
| 3 | 8.403 | 2.000 | 2 | 1.49091 |
| 4 | -4.382 | 0.00 |  |  |
| 5 | (Diaphragm) | 9.386 |  |  |
| 6 | - | 0.800 | 3 | 1.51680 |
| 7 | $\infty$ |  |  |  |

```
Aspherical surface: \(\mathrm{r}_{3}\)
    \(\mathrm{K}=-5.54774\)
    \(\mathrm{A}_{4}=0, \mathrm{~A}_{6}=0\)
Aspherical surface: \(\mathrm{r}_{4}\)
    \(\mathrm{K}=-1.2\)
    \(\mathrm{A}_{4}=0, \mathrm{~A}_{6}=0\)
    \(\mathrm{f}_{1}=-6.779, \mathrm{f}_{2}=6.095, \mathrm{D}=7.900, \mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1\right) \mathrm{f}_{1}\right\}=-0.843\)
    \(\mathrm{f}_{1} / \mathrm{f}_{2}=-1.112\)
```

The first and second lens elements 26, 28 were made from PMMA (acryl). The configuration of the lens and associated light paths according to the fifth embodiment are illustrated in FIG. 5 and the aberrations of the fifth embodiment are illustrated in FIG. 10. The coma aberration shown therein is obtained in connection with (d) - line.

FIGS. 1 through 5 show the layout of the lens elements of the wide-angle lens system of the Embodiments 1 through 5 and light paths therein. In FIGS. 1 through 5 numeral 26 is a first lens element, 28 a second lens element, 30 a diaphragm and 32 a cover glass.

As is clear from the drawings, all the embodiments show good performances.

In the aberration diagrams, consideration is given to the presence of the cover glass.

While the foregoing description and drawings represent the preferred embodiments of the present invention, it will be obvious to those skilled in the art that various changes and modifications may be made therein without departing from the true spirit and scope of the present invention.

What is claimed is:

1. A wide angle lens system comprising:
a first lens element and a second lens element which are located on the object side and image side respectively, said first lens element being of a meniscus type having a negative refractive power and said second lens element being of a two-sided convex type having a positive refractive power, at least one surface of said lens elements being aspherical, said wide angle lens system having no more than two lens elements and wherein
$\left|f_{1}\right|<D$;
$\left[-1.5<\mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1\right) \mathrm{f}_{1}\right\}<-0.5\right.$; and
$\left.-2<f_{1} / f_{2} \leqq \ldots 1\right]$
$-1.5<\mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1\right) \mathrm{f}_{1}\right\}-0.5$; and
$-2<\mathrm{f}_{1} / \mathrm{f}_{2}<-1$
where $\left(f_{1}\right)$ is the focal length of the first lens element and $D$ is the distance between a back principal point of the first lens element and a front principal point of the second lens element, where $\left(r_{2}\right)$ is the curvature radius of the image-side surface of the first lens element, where $\left(\mathrm{n}_{1}\right)$ is the refractive
index of the material of the first lens element, and where $\left(f_{2}\right)$ is the focal length of the second lens element.
2. The wide angle lens system of claim 1 , wherein

$$
-10<\mathrm{K}_{4}<-1
$$

where $\left(\mathrm{K}_{4}\right)$ is the conical reflection constant when the image-side surface of the second lens element is aspherical.
3. The wide angle lens system of claim 2 , wherein said lens elements are made of plastic.
4. The wide angle lens system of claim 3 , wherein said lens elements are made from acryl.
5. The wide angle lens system of claim 1, wherein said lens elements are made of plastic.
6. The wide angle lens system of claim 5 , wherein said lens elements are made from acryl.
7. The wide angle lens system of claim 5 , including a diaphragm and a cover glass for a CCD layer on the image side, said diaphragm being between said second lens element and said cover glass.
8. The wide angle lens system of claim 1, including a diaphragm and a cover glass for a CCD layer on the image side, said diaphragm being between said second lens element and said cover glass.
9. The wide angle lens system of claim 8 , wherein said first and second lens elements are constructed of the same material as said cover glass.
10. In a camera having a wide angle lens system, a diaphragm and a plane surface for forming an image, the improvement comprising:
that said wide angle lens system comprises:
a first lens element and a second lens element which are located on the object side and image side respectively, said first lens element being of a meniscus type having a negative refractive power and said second lens element being of a two-sided convex type having a positive refractive power, at least one surface of said lens elements being aspherical, said wide angle lens system having no more than two lens elements and wherein
$\left|f_{1}\right|<D$;
$-1.5<\mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1\right) \mathrm{f}_{1}\right\}<-0.5$; and
$-2<\mathrm{f}_{1} / \mathrm{f}_{2}<-1$
where $\left(f_{1}\right)$ is the focal length of the first lens element and $D$ is the distance between a back principal point of the first lens element and a front principal point of the second lens element, where $\left(r_{2}\right)$ is the curvature radius of the image-side surface of the first lens element, where $\left(\mathrm{n}_{1}\right)$ is the refractive index of the material of the first lens element, and where ( $\mathrm{f}_{2}$ ) is the focal length of the second lens element.
11. The camera of claim 1 wherein said camera is of the CCD type and wherein a cover glass for CCD elements is arranged on the image side, said diaphragm being disposed between said second element and said cover glass.
12. The camera of claim 11 wherein said first and second elements are constructed of the same material as said cover glass.
13. The camera of claim 1 wherein said first and second elements are made of plastic.
14. The camera of claim 10 wherein

$$
-10<\mathrm{K}_{4}<-1
$$

where $K_{4}$ is a conical reflection constant when the image-side surface of said second lens element is aspherical.
15. In a camera having a wide angle lens system, a diaphragm and a plane surface for forming an image, the improvement comprising:
that said wide angle lens system has a first lens element and a second lens element which are located on an object side and image side respectively, said first lens element being of a meniscus type having a negative refractive power and said second lens element being of a two-sided convex type having a positive refractive power, at least one surface of said lens elements being 10 aspherical wherein
$-1.5<\mathrm{r}_{2} /\left\{\left(\mathrm{n}_{1}-1\right) \mathrm{f}_{1}\right\}<-0.5$
wherein $\left(\mathrm{r}_{2}\right)$ is the curvature radius of the image side surface of the first lens element, $\left(f_{1}\right)$ is the focal length of the first lens element and $\left(\mathrm{n}_{1}\right)$ is the refractive index of the material of the first lens element.

*     *         *             *                 * 


## EXHIBIT 6a


（54）［発明の名称］画像データ変換装萓
（57）【要約】
【課題】 魚眼レンズにより得られた全周囲の撮影デ ータを，歪みを修正しつつ，一つの画像としてつなぎ目 なく表示できるように変換する。
【解決手段】魚眼レンズによる撮影により得られる円形画像データの一部分の領域に対して，前記円形画像の中心を原点とする平面直交座標系にあける前記領域上の点 （ $g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \mathrm{sin} \psi) \quad$（ $\Theta$ は $0<\Theta<\pi / 2$ を満たすパラメータ，g（ $\Theta$ ）はg （0）＝ 0 を満たし，前記 $\Theta$ の範囲で単調増加する関数，$\psi$ ね前記平面直交座標系の原点と前記円形画像上の点とを結んた線分が前記平面直交座標系における一座標軸となす角）をRを定数とする円柱座標系上の点（R， $\psi$ ， $\mathrm{R} / \mathrm{tan} \Theta)$ へ変換する。


## 【特許請求の範囲】

【請求項1】魚眼レンズによる撮影により得られる円形画像データの一部分の領域に対して，
前記円形画像の中心を原点とする平面直交座標系にあけ る前記領域上の点（ $g(\Theta) \cdot \cos \psi, g(\Theta) \cdot s$ in $\mathrm{n} \psi) \quad(\Theta は 0<\Theta<\pi / 2$ を満たすパラメー夕，$g(\Theta)$ はg（ 0$)=0$ を満たし，前記 $\Theta$ の範囲で単調増加高る関数，$\psi$ 愔前記平面直交座標系の原点と前記円形画像上の点とを結んだ線分が前記平面直交座標系 における一座標軸となす角）をRを定数とする円柱座標系上の点（ $\mathrm{R}, \psi, \mathrm{R} / \mathrm{tan} \Theta$ ）へ変換する画像デー夕変興装置。
【請求項 2】前記魚眼レンズが $\mathrm{h}=\mathrm{g}(\theta)$（ h は像
高，$\theta$ は画角）の特性を有するものである請求項 1 に記載の画像データ変換装置。
【請求項3】前記関数 $\mathrm{g}(\theta)$ が $\mathrm{g}(\theta)=2 \mathrm{f} \cdot \mathrm{ta}$ $\mathrm{n}(\theta / 2)$（ f は焦点距離）である請求項2に記載の画像データ変換装寘。
【請求項4】前記関数 $\mathrm{g}(\theta)$ が $\mathrm{g}(\theta)=\mathrm{f} \cdot \theta$（ f は焦点距離）である請求項2に記載の画像データ変換装置。
【請求項5】コンピュータに請求頂1から4のいずれか に記載の画像データ変換装置としての動作を実行させる プログラムを記録した前記コンピュータに読み取り可能 な記録媒体。
【請求項6】前記魚眼レンズと，
前記魚眼レンズより得られる像を前記画像データへ変換 する変換手段と，
請求項1から4のいずれかに記載の画像データ変換装置 と，
この画像データ変換装置により変換された前記円柱座標面上の画像データを平面に展開して表示する表示手段と より構成きれる撮像システム。
【請求項7】魯眼レンズによる撮影により得られる円形画像データの一部分の領域に対して，
前記円形画像の中心を原点と方る平面直交座標系にあけ る前記領域上の点 $(g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \mathrm{s}$ in $\psi$ ）（ $\Theta$ は $0<\Theta<\pi / 2$ を満たすパラメー夕，$g(\Theta)$ はg（ 0$)=0$ を満たし，前記 $\Theta$ の範囲で単調増加する関数，$\psi 4$ 前記平面直交座標系の原点と前記円形画像上の点とを結んだ線分が前記平面直交座標系 における一座標蟿となす角）をRを定数とする円柱座標系上の点（ $\mathrm{R}, \psi, \mathrm{R} / \mathrm{tan} \mathrm{n}$ ）へ変換する画像デー夕変換方法。
【発明の詳細な説明】
【0001】
【発明の属する技術分野】本発明待，画像データ変換装置に関し，詳しくは，魚眼レンズによる撮影により得ら れる円形の画像データを，歪みを修正しつつ広範囲に渡 る表示を行えるような平面画像データへと変換する装置

に関する。
【0002】
【従来の技術】従来，店舗内の監視カメラや交通管制用 のカメラ等でほ，周囲の状況を監視するために，前方の限られた視野を持つカメラをモータ等の駆動装置で旋回 きせることが一般的に行かれている。しかし，このよう な視野の限られたカメラを回転させるようにすると，回転駆動部が必要になるので装置が複雑となり，また，特定の対象を捕らえようとする際にカメラを回転きせる必要があり，対象が動いているようなときは回転速度の制約から対象を捕らえることができないようなことも生じ る。また，同時に複数の方向を撮影することができず，常に監視範囲に関して死角が生じるので，監視等の機能 としては十分とは言えない。
【0003】このような問題を解決なる技術として，特公表平6－501585号公報に，魚眼レンズにより前方の全方位を撮影して得られる円形の画像データを，平面画像に変換なるものが提示されている。この技術を以下に簡単に説明する。魚眼レンズにより得られる円形の画像デー夕は全方位の像を含むことができるが外周へ行 くほど像が歪む。この歪みは円形画像データを半球面上 に変換するとほぼ解消することができるが，半球面に変換した画像データでは平面的なモニターに表示すること ができない。そこで，上記技術ではきらに半球面に変換 された画像データの一部を平面に投影方ることで平面に変換して表示を可能としている。このような方法を用い ることにより，回転駆動機構が不要となって装置を簡易化でき，表示する方向の切り替えもデータ処理時間の制約だけとなるので格段に速く行うことができる。【0004】
【発明の解決しようとする課題】しかし，このように魚眼レンズで撮影した円形画像データを直接平面画像デー夕に変㒜するようにしても，歪みを十分に修正したまま半球面のすべてを一つの平面に投影することはできない ので，得られる画像は特定の方向に関するものだけとな る。従って，魚眼レンズにより全周囲の摄影をしている にもかかわらず表示画面においては死角が生じることと なる。また，死角をなくす方法として同時に複数の方向 に関して平面画像への変換を行いこれらを同時に表示す ることが考えられるが，この場合は画像同時のつなぎ目 が連続にならず，また，複数の異なる画像変換を行う必要が生じる。
【0005】本発明はこのような問題を解決するために なされたものであり，魚眼レンズにより得られた全周囲 の撮影データを，歪みを修正しつつ，一つの画像として つなざ目なく表示できるように変換することを目的とす る。
【0006】
【課題を解決するための手段】上記課題を解決するため に，本発明に係る画像データ変換装置は，魚眼レンズに

よる撮影により得られる円形画像データの一部分の領域 に対して，前記円形画像の中心を原点とする平面直交座標系における前記領域上の点（g（ $\Theta$ ）$\cdot \cos \psi$ ，g （ $\Theta$ ）－ $\sin \psi) \quad(\Theta ま 0<\Theta<\pi / 2$ を満たす パラメータ，g（ $\Theta$ ）恬g（ 0 ）＝ 0 を満たし，前記 $\Theta$ の範囲で単調增加する関数，$\psi$ は前記平面直交座標系の原点と前記円形画像上の点とを結んた線分が前記平面直交座標系における一座標軸となす角）をRを定数とする円柱座標系上の点（ $\mathrm{R}, \psi, \mathrm{R} / \mathrm{tan} \Theta$ ）へ変換－ る。たお，本発明にいう魚眼レンズには，視野角が略1 80度を有する一般的に魚眼レンズと呼ばれるもののみ ならず，それよりも小さな視野角を有する一般的に広角 レンズと呼じれるものも含まれる。
【0007】なお，変換は結果として上記関倸を満たす変換が行われれば足り変換の過程を問題としない。即 ち，上記式を直接用いる必要は必ずしもなく，変換元の画素と変換先の画素の対応を示すテーブルを用いて変換 するような場合も含まれる。また，前記平面直交座標系 および円柱座標系は互いに独立であり，座標の方向は任意に定めることができる。また，Rを定数とする円柱座標系は円筒面となるが，ここでは，これを展開して平面 として上記のような変換を行う場合も含まれる。
【0008】このようにすると，まず，$\psi$ を固定して点 （ $\mathrm{g}(\Theta) \cdot \cos \psi, \mathrm{g}(\Theta) \cdot \mathrm{sin} \psi)$ が上記円形画像データの一部分の領域に大る範囲で $\Theta$ を小さい値 から大きい値へと堷加きせていくと，円形画像データに おける中心から半径方向へ向かう線分が，Rを定数とす る円柱座標系即ち半径Rの円筒面において上方から下方 に向かう線分として変換される。このような変換がさら にみについて上記点が前記円形画像データの一部分の領域に入るように最大360度の範囲で行われるので，魚眼レンズが撮影した魚眼レンズを中心とする全周囲の画像情報を含む円形画像データの一部が，歪みを補正きれ る形でなめらかに円筒面へ変換されることとなる。円筒面に変換された画像は円筒面を展開することにより容易 に平面画像にできるので，魚眼レンズにより得られた全周囲の撮影データを歪みを修正しつつ一画像としてつな ぎ目なく表示できる。
【0009】また，前記魚眼レンズを $\mathrm{h}=\mathrm{g}(\theta)$（ h は像高，Oは画角）の特性を有するものとすると，$\Theta$ の墇加にときなう上記g（ $\Theta$ ）の増加量は，像高h の堌加量と同じとなる。従って，即ち $\Theta$ を変化させることは画角 $\theta$ を変化させることに他ならない。このようにした場合，円形画像を歪みのない仮想的な半球面へと変㒜し， さらに，中心軸がこの半球面の中心蟿と一致するように配置した前記円筒面に対して半球面の中心点から半径方向へ向かう投射光により，変換した半球面画像を投射し た画像が得られるようになる。従って，魚眼レンズの側方の全周に渡る撮影領域，即ち円形画像の外周側の画像 に関しては，ほぼ歪みのない画像へ変換されることにな

る。
【OO10】また，前記魚眼レンズの特性を示す関数g
（ $\theta$ ）をg $(\theta)=2 \mathrm{f} \cdot \mathrm{tan}(\theta / 2)$（fは焦点距離）とすると，円形画像データの外周側の画像のデー夕量が多くなるので，魚眼レンズの側方の全周に渡る撮影領域の円筒面への変換時におうる再現性を向上させる ことができる。
【0011】さらに，前記前記魚眼レンズの特性を示す関数 g （ $\theta$ ）を $\mathrm{g}(\theta)=\mathrm{f} \cdot \theta$（ f は焦点距墑）とす ると，この特性は最き一般的に使用される魚眼レンズの特性であるので，量産された安価な魚眼レンズを使用す ることができ装置のコストダウンを図ることが可能とな る。
【0012】上記の画像データ変換装置は，コンビュー夕に上記画像データ変換装置としての動作を実行させる プログラムを組み込むことでも実現することができ，こ のプログラムね前記コンピエータに読み取り可能な記録媒体に記録字ることができる。
【0013】さらに，上記課題を解決するために，本発明に係る撮像システムは，前記魚眼レンズと，前記魚眼 レンズより得られる像を前記画像データへ変換する変換手段と，請求項1から40いずれかに記載の画像データ変換装置と，この画像データ変換装置により変換された前記円柱座標面上の画像データを，当該円柱座標面を展開して平面として表示する表示手段とより糟成される。【OO14】このような構成により，この撮像システム は前述のように画像データ変換装置により歪みを修正き れてつなぎ目無く変換された円筒面上の画像を展開して平面として表示するので，一画面で魚眼レンズが摄影し た周囲の様子をすべて示すことが可能となる。なお，展開した平面には，展開した平面を適当に加工する場合も含み，例之ば，展開した平面を所定位置で切断して，各切断部分を適宜配列して表示するような場合も含む。
【0015】また，上記課題を解決するために，本発明 に係る画像データ変換方法は，魚眼レンズによる撮影に より得られる円形画像データの一部分の領域に対して，前記円形画像の中心を原点とする平面直交座標系におけ る前記領域上の点 $(\mathrm{g}(\Theta) \cdot \mathrm{cos} \psi, \mathrm{g}(\Theta) \cdot \mathrm{s}$ in $\%$ ）（ $\Theta$ は $0<\Theta<\pi / 2$ を満たすパラメー夕，$g(\Theta)$ 名 $g(0)=0$ を満たし，前記 $\Theta$ の管囲で単調増加する関数，$\psi$ は前記平面直交座標系の原点と前記円形画像上の点とを結んた線分が前記平面直交座標系 における一座標䡉となす角）をRを定数とする円柱座標系上の点（ $\mathrm{R}, ~ \psi, ~ \mathrm{R} / \mathrm{t} \mathrm{a} \mathrm{n} \Theta)$ へ変換するものであ る。この画像データ変換方法もやはり，魚眼レンズが撮影した魚眼レンズを中心とする全周囲の画像情報を含さ円形画像データの一部が，歪みを補正される形ですめら かに円筒面へ変換されるので，魚眼レンズにより得られ た全周囲の撮影データを歪みを修正しつつ，つなぎ目な く表示するようにできる。

【OO16】
【発明の実施の形態】以下に本発明の実施の形態につい て図面を参照して説明する。図1に本発明の実施の形態 に係る撮像システムの構成を示すブロッタ図を示す。こ の撮像システム㤝，カメラ部1，データ変換部2，第1画像メモリ3，第2画像メモリ4，A－Dコンバータ

$$
\mathrm{h}=2 \mathrm{f} \cdot \mathrm{tan}(\theta / 2)
$$

の特性を有するものを用いることとする。このような特性のレンズを用いると画角 $O$ の増加に対する像高hの增加量が，一般的な $\mathrm{h}=\mathrm{f} \cdot \theta$ のレンズに比べて大きくな るので画角 $\theta$ の大きな範囲つまり魚眼レンズで得られる円形画像の周辺部での情報量を多くすることができる。 このような特性を有する魚眼レンズ11により得られる円形画像はCCD 1 2により各画素のRGBごとに電気信号に変換きれてA／Dコンバータ5へと出力きれる。 ここではCCDとして例えば，1280×1024画素 のものを用いるものとする。
【0018】A Dコンバータ5はCCD 1 2 から送ら れるアメログ信号をデジタル信号へと変換して第1画像 メモリアへと出力する。第1画像メモリ3はRAMによ り構成され，送られた円形画像を表すデジタル信号に基 づき各画素ごとのRGB値を記録する。データ変換部2 は本発明に係る画像データ変換装置に相当し，後述のよ うな演算を行う演算回路により構成される。データ変換部2は第1画像メモリ3に記録された円形の画像データ を後に詳述するような変換により円筒の画像データへと変換して第2画像メモリ4へと出力する。
【0019】第2西像メモり 4 ばかはりRAMにより構成され，出力された画像データの画素ごとのRGB値を後述するような円筒面を展開した平面として記録する。 また，円筒面を展開した再像は横方向に長いので，後述 するような表示データが得られるように第2画像メモリ 4は画像データ記録する際に展開した画像を半分に分け て上下に所定閒隔を置いた画像となるように記録する。 D／Aコンバータ6は第2画像メモリ4に記録されたデ ジタル値の画像データを読み出しアナログ信号へと変換 して，画像信号としてモニター7 走査線順に送出す る。モニター7はD／Aコンバータ6より送られる画像信号に基づき第2画像メモリ4に記録されている画像を表示する。
【0020】なお，本撮像システムほカメラ部1を除い た部分は一般的なコンピュータに上記機能およひび下記動作を実現させるようなブログラムを組み込きことによっ て実現可能であり，プログラムはこのコンビュータによ り読み取り可能なフロッピーディスクのような記録媒体 に記録が可能である。また，このプログラムはインター ネット等の通信手段からも当該コンピュータに組み达む ことができる。
【0021】ここで，データ変換部2の変換方法につい て詳述する。データ変換部2は円形面上の画像データを

5，D／Aコンバータ6，モニター7より構成きれる。【OO17】カメラ部1はレンズとして魚眼レンズ11 を用いてあり，少なくともレンズの光軸方向に対して画角90度以上での撮影が可能である。ここでは，魚眼上 ンズとして，
（1）
円筒面上へと変換する。円形面上の点と円筒上の点との対応関係を図2あよび図3を用いて説明する。図2は魚眼レンズ11により撮影される全周面を仮想的に想定し た半球面 O 上任意の点 P 0 と変換する面である円筒面 Cの点P2との関係を示す図である。図2では，半球面 Oはxyz座標系において，底円（半球面の縁を構成す る円）放原点を中心として x y 平面上に位置している。 z軸は魚眼レンズ 1 1 の光軸方向と一致する。また，円筒面CはZ軲を中心䡉とする半径Rの円筒である。即 ち，円筒面CはRを定数とするr $\psi \mathrm{z}$ 円柱座標系におすけ る曲面として表すことができる。また，ここでは，円筒面C上の点をr $\psi \mathrm{z}$ 円柱座標系上の点として（ R ，$\psi$ ， $z$ ）で表す。但し，$\psi$ は， $\mathrm{x} y$ 平面に降ろした垂線と x y 平面との交点と原点とでできる線分がx軸となす角で ある。そして，原点から半球面 O 上の任意の点 P 0 を結 ぶ線分を延長した直線が円筒面Cと交わる点がP2 とな る。なお，原点から点P0とを結ぶ線分と $z$ 軸とのなす角が点P 0 に関する画角 $\theta$ となる。
【0022】図3は上述の撮影される全周面を仮想的に想定した半球面○上の任意の点P0が，魚眼レンズ11 より映きれる撮影面F上の点P1 の位置を示している。図3において撮影面F上の円形領域が魚眼レンズ11を通して光りが照射されるCCD12上の領域であり，こ の部分が変換される再像データが表示される円形面Sを形成する。図3では，XY座標系において原点をこの円形面Sの中心にとっている。なお，X軸およびY軸の方向は図2のxyz座標系のx軸およびy軸の方向と逆に なるようにしてある。これは，カメラ部1で撮影した画像は上下左右が反転するので，P0 も上下左右が反転し た位置に映ることになるため，これに対疬させるためで ある。もつとも，円筒面壮任意であるので，実際の変換 においては座標の取り方も自由である。そして，P1 の位惪り，原点から像高ho距離でかつ原点と P1 を結ん た線分とX軸とがなす角が $\downarrow$ となる位置となる。 h は上記 ${ }^{(1)}$ 式により表され，画角 $\theta$ により定まる。
【0023】データ変換部2に図3に示すP1を図2に示すP2へと変換するものである。以下に，具体的な計算について説明する。まず，パラメータを $\theta, ~ \psi と す る ~$場合を考える。この場合XY平面上におけるP1 の座標 は（h•cos $\psi$ ，h•sin $\psi$ ）であり，上記式（ $\downarrow$ りhを消去すると（ $2 \mathrm{f} \cdot \mathrm{t}$ an（ $\theta / 2$ ）•cos $\psi, 2 \mathrm{f} \cdot \tan (\theta / 2) \cdot \mathrm{sin} \psi)$ と表される。一方，P2 の座標はRは定数であり，zは図2よりz＝
$\mathrm{R} / \mathrm{tan} \theta$ の関係があるので，（ $\mathrm{R}, \psi, \mathrm{R} / \mathrm{tan}$ $\theta)$ と表される。従つて，パラメータ $\theta$ ，$\psi$ を動かし て，XY平面上における円形画像上のP1を特定でき， これに対する $\mathrm{r} \psi \mathrm{z}$ 円柱座標系上の点，即ち円筒面 C 上 の点も特定できるので，上記P1，P2 を示す式に従つ て画像データを変換することができる。但し，$\theta=0$ の場合はP2のz 座標が無限大となってしまうので，現実 には $\theta$ の値はある値以上のものを使用字ることになる。本実施の形態では $\theta$ として $\pi / 4 \leqq \theta<\pi / 2$ の範囲を使用している。
【0024】ところで，実際の変換においてはパラメー夕として，撮影きれたCCD 1 2 上の各画素位置もしく は変換される円筒面C上の変換傈の各画素位置を直接表 すものを用いる方が計算が容易である。そこで，円筒面 C上の変換後の各画素位置を直接表すパラメータとして zと $\psi$ を用いることを考える。この場合円筒面 C 上の点 P2 をパラメータz， z で表すと，（ R ，$\psi, ~ \mathrm{z}$ ）とな る。変換される円筒面Cは展開されてモニター7に表示 $\mathrm{h}=2 \mathrm{f} \cdot \mathrm{tan}(\theta / 2)=2 \mathrm{f}$ となる。図2よりsin $\theta=\mathrm{R} /\left(\mathrm{R}^{2}+\mathrm{z}^{2}\right)^{1 / 2}$ ， $\cos \theta=\mathrm{z} /\left(\mathrm{R}^{2}+\mathrm{z}^{2}\right) 1$／ 2 であるので， これらを（1）式に代入して整理すると， $\mathrm{h}=2 \mathrm{f} \cdot \mathrm{R} /$ \｛（ $\mathrm{R}^{2}+\mathrm{z}^{2}$ ） $\left.1 / 2+\mathrm{z}\right)$ \} となるので, 結果と してP1は，（2f．R•cos $\boldsymbol{f}$ ノ $\left\{\left(\mathrm{R}^{2}+\mathrm{z}^{2}\right)\right.$ $1 / 2+\mathrm{z})$ ）， $2 \mathrm{f} \cdot \mathrm{R} \cdot \mathrm{sin} \psi\left\langle\left\{\left(\mathrm{R}^{2}+\mathrm{z}\right.\right.\right.$ 2）1（2＋z））となる。従って，上述のように zをdずつ，$\psi$ を $\mathrm{d} / \mathrm{R}$ ずつ変化させて，この式より円筒面C上の各画素位置に変換される円形面S上の画素位惪を求めることができる。この場合，計算で得られる画素位置と実際のCCD 12 が撮影した画素位置とは完全 には合致しないので，最も近い画素を抽出するようにす る。具体的には，例之ば得られたX座標値およびY座標値をCCD 12 の画素ピッチdsで割り，その値を例え ぼ小数点以下を切り捨てることで得られる整数値を画素 の番号として抽出することができる。なお，この場合， CCD 1 2の各画素は，XY座標における原点を（ 0 ， 0）としてXY座標の各象限に応じてそれぞれ正負が定 まるものとする。
【0026】以上のような方法を用いてデータ変換部2 は，変換後の円笥面C上の各画素に対応する円形面S画素位惪を算出して，その画素位置における画素データを各円筒面C上の画素データとして変換していく。この結果図4に示すように円形面S上の画素データは円筒面C上の各画素データとして変換されていくことになる。な お，円形画像の各画素が円筒面のどの画素位置へ変換ざ れるかは一義的に決まるので，演算を行わずにデータ変換部2に円形画像の画素と円筒面上の画素位置との対応 を示すテーブルを設けておき，これに基づいてデータ変換を行うようにすることもできる。
【0027】続いて，以上のような構成を有する撮像シ

されることになり，各画素は䌦方向および横方向に画素 ピッチdの等間隔で並ぶことになる。図4に展開した円筒面Cと円形面Sとの関係を表す図を示す。円筒面Cの綡方向はバラメータ z と一致するので，パラメータ zに関しては画素ピッチdずつ変化きせれば円筒面Cの縦方向の画素位置に合致する。展開した円筒面の横方向の $\psi$ の変化量にともなう変化量はR• $\psi$ と表まことができる ので，円筒面Cの画素ピッチdに対応守るパラメータ $\psi$ の変化量を $\Delta \psi と す る と, ~ \Delta \psi=\mathrm{d} / \mathrm{R}$ と表すごとがで きる。従って，パラメータねに関してはd $/ \mathrm{R}$ ずつ変化 きせると円筒面Cの横方向の画素位置に合致することに なる。なお，図において円形面Sのハッチングきれてい る範囲は，$\pi / 4 \leqq \theta<\pi / 2$ に対応する円形面Sの範囲であり，円筒面Cに変換される範囲を示している。
【0025】一方，円形画像上の点P1をパラメータ Z，$\psi$ で表すことを考える。まず，上記 ${ }^{(1)}$ 式を三角関数 の倍角の公式を用いて変形すると，
$\left\{\sin \theta \succ(1+\cos \theta)\right.$ \} $\boldsymbol{D}^{\prime}$
ステムの動作について説明する。なぁ，カメラ部1は，室内において天井中央から下方に向けて取り付けられて いるものとする。また，変換する円筒面のz $\begin{gathered}\text { 範囲を } 0 ~\end{gathered}$ $<\mathrm{z} \leqq \mathrm{R}$ とする。言い換えると，$\theta$ の範囲を $\pi / 2>\theta$ $\geqq \pi$ ノ 4 に設定するものとする。図5に撮像システムの動作を表すフローチャートを示す。まず，室内の全景が カメラ部1により魚眼レンズ11を通して円形画像とし て映される。この円形画像はCCD 12 により電気信号 に変換きれ，さらに，A／Dコンバータ5により画素ご とにデジタル値に変換される。そして，これらのデータ は第1画像メモり3に記録される（s 1 O 1）。また， パラメータ $\psi, ~ \mathrm{z}$ の初期値としてそれぞれ O を入れておう く（s102）。
【0028】次に，データ変換部2によりパラメータも i を $\mathrm{d} / \mathrm{R}$ ずつ $\mathrm{i}=1 \sim \mathrm{n}(\mathrm{n}=2 \pi \mathrm{R} / \mathrm{d})$ まで増加 させ，また，パラメータzjをdずつ $\mathrm{j}=1 \sim \mathrm{~m}$（ $\mathrm{m}=$ $\mathrm{R} / \mathrm{d}$ ）まで増加させる。そして，それぞれの値ごと に，
$\mathrm{Xi}=\left[2 \mathrm{f} \cdot \mathrm{R} \cdot \cos \psi \mathrm{i} /\left\{\left(\mathrm{R}^{2}+\mathrm{z}^{2}\right)\right.\right.$
$1 / 2+\mathrm{zj}\} \cdot \mathrm{ds}]$
$\mathrm{Y} \mathrm{j}=\left[2 \mathrm{f} \cdot \mathrm{R} \cdot \mathrm{sin} \psi \mathrm{i} /\left\{\left(\mathrm{R}^{2}+\mathrm{z} \mathrm{j}^{2}\right)\right.\right.$ $1 / 2+\mathrm{zj}\} \cdot \mathrm{ds}]$
が計算きれ，この結果に基づき第1画像メモリ3に記録 されている（Xi ，Yj）番目の画素データが抽出さ
え，円筒面における（i，j）番目の画素の画素データ として第2画像メモリ4へと記録ざれる（s103～s 108）。なお，第2画像メモリ4では，図6に示すよ うな画像がモニター7に映し出されるように，円筒面上 の画素（ $\mathrm{i}, \mathrm{j}$ ）の $\mathrm{i}=1 \sim \mathrm{n} / 2, ~ \mathrm{j}=1 \sim \mathrm{~m}$ の部分 と， $\mathrm{i}=(\mathrm{n} / 2)+1 \sim \mathrm{n}, ~ \mathrm{j}=1 \sim \mathrm{~m}$ の部分とは2分をれ，後者け前者の下方に所定間隔を置いたところへ

位置するように配置きれた画像となるように記録され る。なお，図6に示されている角度を示すデキストデー夕は出め第2画像入モリ4に記録されている。
【0029】第2画像メモリ4に記録きちだ画像データ はD Aコンバータ6によって画像信号としてモニター 7ヘ出力され（s 1 09），モニター7により表示され る（ s 110 ）。上述のように画像データは2分きれて上下に配置されるように形成されているるので，図6に示す画面が表示されることになる。このように本実施の形態に係る撮像システムでは魚眼レンズで撮影した周囲 360 度の映像をすべてつなぎ目無く表示することがで き，レンズ周囲の状況を死角無く完全に監視することが できる。
【0030】ところで，上記実施の形態では，上記式『 で表きれる特性を持つ魚眼レンズを用いたが，魚眼レン ズの特性ば式（で表されるものでなくてもよい。つま り，魚眼レンズの特性を $\mathrm{h}=\mathrm{g}$（ $\theta$ ）として一般化する と P2は上記のままで，P1は（g（ $\theta$ ）•cos $\dot{\boldsymbol{*}}$ ， $\mathrm{g}(\theta) \cdot \mathrm{s} \mathrm{i} \mathrm{n} \psi)$ と表すことができるので，パラメ
 らに，上記のようにパラメータをz，ねとする場合は，図2より $\theta=\mathrm{Tan} \mathrm{n}^{-1}(\mathrm{R} / \mathrm{z})$ と表すことができ るので，P2は土上記のままでP1は（G（Tan－1
$(\mathrm{R} / \mathrm{z})$ ）cos $\psi$ ， $\mathrm{G}(\mathrm{Tan}-1$（ R ／
z））s i n $\psi$ ）と表すことができるので，上記と同様に,$~ \psi の$ 值を変えながら対応する P2，P1 か画素位置を求めることが可能である。
【0031】例えば，魚眼上ンズとして一般的によく用 いられるh＝f • $\theta$ の特性をもつものを使用する場合 は，パラメータを $\theta$ ，屼すると，P1 は（f • $\theta \cdot \mathrm{c}$ ○s $\psi$ ， $\mathrm{f} \cdot \theta \cdot \mathrm{sin} \psi)$ となり，パラメー夕をz， ねとすると，P1は（f•G（Tan－1（R／z） －cos $\psi$ ，f． G （Tan $\mathrm{n}^{-1} \quad(\mathrm{R} / \mathrm{z}) \cdot \mathrm{sin}$
 a $n^{-1}$（ $\mathrm{R} / \mathrm{z}$ ）は公知の回帰計算により求めるご とができる。
【0032】さらに，上記実施の形態におらいて魚眼レン ズ11としてh＝f• 1 の特性をもつ魚眼レンズに置き換え，他の構成部分はそのままのものを用いることも可能である。これは，上記式 $($ の特性をむつ魚眼レンズで得られる円形画像と $\mathrm{h}=\mathrm{f} \cdot \theta$ の特性をもつ魚眼レンズ円形再像とでは，半径方向の像の伸縮率が異なるが再素同士 隣接関係は変わらないので，得られる画像は Z 方向に多少の伸縮の違いがでるだけで監視用の画像として の役割を果だすことはできるからである。
【0033】このことをさらに一般化すると， $0<\Theta<$
$\pi / 2 の$ 範囲で単調増加関数となる $g(\Theta)$ を用いて， P1を（g（ $\Theta$ ）•cos $\psi$ ， $\mathrm{g}(\Theta) \cdot \mathrm{s} \mathrm{i} \mathrm{n} \psi) と$ すれだ，種々の魚眼レンズに対して，z 方向に伸縮率が異なるだけの画像が表示きたることになる。そして，関数g（ $\ominus)$ として，使用する魚眼レンズの特性に応じて最も z 方向の歪みが少なくなるようなものを用いること で，より監視用の画像として見きすいものを得ることも可能となる。
【0034】それから，上記実施の形態における撮像シ ステムは魚眼レンズ11が撮影した周囲360度すがて の画像を変換して表示するようにしたが，例えば，力入习部1を天井 $\sigma$ 壁際に設置したような場合は壁方向を除 いた 180 度部分を変換して表示すれば足り，カメラ部 1をコーナー部分に設置したような場合はコーナーを挟 を壁方向を除いた90度部分を変換して表示すれば足り る。このように，状況に応じて，変換する範囲壮任意に決めることができる。
【0035】表た，上記実施の形態における撮像システ ムでは， $0 \leqq \theta<\pi<4$ の範囲は表示きれてないが，こ の範囲はもとの円形画像における歪みが少ないので，モ ニター7に円形画像のまま変鲃せずに上記円筒面Cの画像と合わせて表示するようにしてもよい。
【図面の簡単な説明】
【図1】実施の形態に係る撮像システムの棤成を示すブ ロック図である。
【図2】魚眼レンズにより撮影された全周面を仮想的に想定した半球面上の点と変換する円筒面上の点との関係 を示す図である。
【図3】魚眼レンズにより撮影きれた全周面を仮想的に想定した半球面上の点に対応する撮影面上の点を示す図 である。
【図4】展開した円筒面を示す図である。
【図5】撮像システムの動作を示すフワーチヤートであ る。
【図6】モニターによる表示画面を示す図である。
【符号の説明】
力メラ部
2 データ変換部
3 第1画像メモリ
4 第2画像メモリ
5 A 万コンバータ
6 D ／Aコンバータ
7 モニター
11 魚眼レンズ
12 CCD
（7） $000-242773(\mathrm{P} 2000-242773 \mathrm{~A})$
［図1］


【図3】

［図2】

［図4］

［図6】



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Fターム（参考）5B057 BA02 BA11 CC02 CD16 CE10 CH01 CH11 DA16
$50022 \mathrm{AA05}$ AB68

## EXHIBIT 5



## EUROPEAN PATENT APPLICATION

(43) Date of publication: 16.08.2000 Bulletin 2000/33
(21) Application number: 00100376.3
(22) Date of filing: 07.01.2000
(84) Designated Contracting States: AT BE CH CY DE DK ES FI FR GB GR IE IT LI LU MC NL PT SE
Designated Extension States:
AL LT LV MK RO SI
(30) Priority: 12.02.1999 JP 3477099
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## (54) Arithmetic unit for image transformation

(57) An arithmetic unit for image transformation is disclosed for transforming a fisheye image obtained by using a fisheye lens (2) into a plane image for display, comprising: a first coordinate calculating unit (35) for obtaining first projection coordinates derived by projecting coordinates on the plane image onto a fisheye
image face as an imaginary object face; and a second coordinate calculating unit (36) for obtaining second projection coordinates derived by projecting the first projection coordinates obtained by the first coordinate calculating unit (35) onto the fisheye image face.

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2.16.7 (HRS)/3.6

## Description

## BACKGROUND OF THE INVENTION

## 1. Field of the Invention

[0001] The present invention relates to an arithmetic unit for image transformation and a monitoring system. More particularly, the invention relates to an arithmetic unit for image transformation for transforming an image obtained by using a fisheye lens into a plane image for display and a monitoring system having the arithmetic unit.

## 2. Description of the Related Art

[0002] An arithmetic unit for image transformation is used in, for example, a monitoring system using a monitoring camera. The operator monitors the state in a space (for example, shop) in which the monitoring camera is installed, by watching images from the monitoring camera displayed on a monitor provided for the monitoring system. When a lens attached to the camera is an ordinary standard lens, the space can be monitored only within the range of the angle of view of the standard lens. In order to monitor the entire space in which the camera is installed, it is necessary to provide a mechanism for properly changing the orientation of the camera. In case of providing such a mechanism, the cost increases and the camera has to be remote controlled. It consequently becomes hard for the operator to handle it.
[0003] There is an idea such that a fisheye lens having the wide angle of view is attached to the camera and monitoring is performed by using the fisheye lens. An image produced by the fisheye lens is, however, distorted as compared with an image obtained by using the standard lens and is very hard for the operator to watch it. A technique for transforming an image produced by the fisheye lens into a plane image is disclosed as a camera orientation system in WO92/21208.
[0004] The system transforms a circular image obtained by using the fisheye lens into an image produced by a normal image pickup lens (for example, standard lens) by an arithmetic process and a plane image seen from an arbitrary view point can be obtained. In this case, when a high speed arithmetic unit is used, plane image data can be obtained at real time rates only by software. In most of the cases, it takes long time for a communicating process, operation as a human interface, and the like in a terminal device connected to a network. It is therefore preferable to realize a part in which the same process is repeated in an image transforming process, by hardware.
[0005] Since the projecting method (stereoscopic projection, equidistant projection, orthogonal projection, or the like) of projecting a fisheye lens image onto an image pickup device (such as CCD) provided for the
camera is determined at the time of designing, by executing arithmetic computations according to mathematical expressions by hardware, the image can be transformed to a plane image.
[0006] As disclosed in WO92/21208, however, when calculations upon transformation are expressed by mathematical equations and executed according to the mathematical equations by hardware, it is necessary to realize many calculations of not only addition, subtraction, multiplication, and division, but also square root, trigonometric function, and the like by the hardware. The unit consequently cannot help becoming expensive inevitably.
[0007] The invention has been achieved in consideration of the actual condition of the conventional technique and it is an object of the invention to provide an arithmetic unit for image transformation capable of providing inexpensive hardware for transforming a fisheye image obtained by using a fisheye lens into a plane image for display.

## SUMMARY OF THE INVENTION

[0008] In order to achieve the object, an arithmetic unit for image transformation according to the invention, for transforming a fisheye image obtained by using a fisheye lens into a plane image for display, comprises:
a first coordinate calculating unit for obtaining first projection coordinates on a fisheye image face as an imaginary object face derived by projecting coordinates on the plane image; and
a second coordinate calculating unit for obtaining second projection coordinates derived by projecting the first projection coordinates obtained by the first coordinate calculating unit onto the fisheye image face.
[0009] The action of the configuration is as follows:
Step 1. The first projection coordinates on the fisheye image face as an imaginary object face obtained by projecting coordinates on the plane image are derived by the first coordinate calculating unit; and
Step 2. The second projection coordinates obtained by projecting the first coordinates onto the fisheye image face are derived.
[0010] That is, when an image is transtormed, the coordinate calculations are not performed by mathematical equations at once but are executed by stages. Consequently, the calculating unit can be constructed by combining simple arithmetic circuits and the hardware part in the arithmetic unit for image transformation can be realized at low cost.
[0011] As a preferred embodiment of the invention, a logic circuit for arithmetic operation has a pipelined
architecture in each of the first and second coordinate calculating units.
[0012] By making the logic circuit have the pipelined architecture, the coordinate transformation can be sequentially performed by stages and the circuit configuration can be partially simplified. As a result, the hardware part in the arithmetic unit for image transformation can be realized at low cost.
[0013] As another preferred embodiment of the invention, the logic circuit for arithmetic operation is limited to calculations of addition, subtraction, multiplication, and square root, and division and other function calculations are handled by referring to a lookup table.
[0014] In case of executing the calculations according to the equations by the hardware, it is necessary to realize many arithmetic operations such as addition, subtraction, multiplication, and division, and in addition, square root, trigonometric function, and the like by hardware. It is consequently necessary to use a large-scale circuit part. Especially, depending on the projecting method of the fisheye lens, there may be a case such that approximation occurs by trigonometric function or infinite polynomial. The logic circuit for arithmetic operation is consequently limited to addition, subtraction, multiplication, and square root. With respect to a part expressed by division or other function, a lookup table is referred to. Consequently, the hardware can be simplified and it can contribute to reduce the cost of the arithmetic unit for image transformation.
[0015] According to further another preferred embodiment of the invention, the second coordinate calculating unit is used to obtain the second projection coordinates by multiplying the first projection coordinates by a predetermined coefficient and the predetermined coefficient is obtained from the lookup table.
[0016] When the projecting method of the fisheye lens differs, the coefficient becomes different. Only by changing data in the lookup table, the invention can deal with a different projecting method and it is unnecessary to replace the hardware part. The cost of the hardware part in the arithmetic unit for image transformation can be therefore reduced also with respect to the point.
[0017] A monitoring system according to the invention is characterized by comprising the arithmetic unit for image transformation. According to the arithmetic unit for image transformation, the arithmetic unit can be constructed by combining simple arithmetic circuits and the cost of the hardware part in the arithmetic unit for image transformation can be reduced, so that an inexpensive monitoring system can be provided.

## BRIEF DESCRIPTION OF THE DRAWINGS

## [0018]

Fig. 1 is a diagram showing setting of a coordinate system;
Fig. 2 is a diagram for explaining a correction coef-
ficient $k_{1}$;
Fig. 3 is a diagram for explaining a procedure of transforming coordinates by hardware; and
Fig. 4 is a block diagram of circuits mounted on a
jecting position on the image pickup face ( $p$, q coordinates) of a point ( $u, v$ coordinates) on a plane image is obtained by arithmetic operation. By referring to luminance information at the point, data of the plane image to be obtained can be generated. Information of the view points ( $\varphi, \boldsymbol{\theta}, \boldsymbol{\alpha}$ ) and the scale factor (zoom ratio) as the size of the plane image is information inputted by the operator through a keyboard, pointing device, or the like and is obtained and set in advance as data for calculation by a higher-order arithmetic processing unit.
[0025] Necessary parameters are, as shown in Figs. 1 and $2,\left(X_{0}, Y_{0}, Z_{0}\right)$ indicative of the center (origin) of a plane image and change amounts $\partial u x, \partial v x$, $\partial u y, \partial v y, \partial u z, \partial v z$ in the respective axes of the ( $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ ) coordinates when a point is moved in the respective directions on the ( $u, v$ ) coordinate system by an amount of one pixel (corresponding to one pixel on the monitor screen).
[0026] The parameters can be easily obtained from the information of the angle information ( $\varphi, \theta, \alpha$ ) of the view point and the magnification of the image.

## (Calculating procedure for image transformation)

[0027] A calculating procedure for image transformation will now be described with reference to Fig. 3. The calculating procedure is performed by, broadly, two steps of first and second steps.

## Step 1

[0028] First, the coordinates of a point $P^{\prime}$ (first projection coordinates) on the hemispherical face as an imaginary object face, which is a projection of a point $P$ on a plane image (the $u, v$ coordinates) are obtained. [0029] When it is assumed that the ( $X, Y, Z$ ) coordinates of the point $P$ are ( $X_{1}, Y_{1}, Z_{1}$ ) and the ( $u, v$ ) coordinates are ( $u_{1}, v_{1}$ ), the following are given.

$$
\begin{aligned}
& X_{1}=X_{0}+u_{1} \cdot \partial u x+v_{1} \cdot \partial v x \\
& Y_{1}=Y_{0}+u_{1} \cdot \partial u y+v_{1} \cdot \partial v y \\
& Z_{1}=Z_{0}+u_{1} \cdot \partial u z+v_{1} \cdot \partial v z
\end{aligned}
$$

[0030] As clearly shown in Fig. 2, the point $\mathrm{P}^{\prime}$ is on the line connecting $O$ and $P$. When a coefficient is set to $\mathrm{k}_{1}$, the following relation is satisfied.

$$
\left(X_{2}, Y_{2}, Z_{2}\right)=k_{1} \cdot\left(X_{1}, Y_{1}, Z_{1}\right)
$$

[0031] The distance between the origin of the ( $\mathrm{X}, \mathrm{Y}$, $Z$ ) coordinate system and the point $P^{\prime}$ expressed by the coordinates $\left(X_{2}, Y_{2}, Z_{2}\right)$ is 1 . The distance between the origin ( $X_{0}, Y_{0}, Z_{0}$ ) of the ( $u, v$ ) coordinate system and the point $P^{\prime}$ expressed by the coordinates $\left(X_{2}, Y_{2}, Z_{2}\right)$ is 1. The distance $L$ from the origin of the $(u, v)$ coordinate system to the point $P$ is obtained as follows.

$$
L=\left(u^{2}+v^{2}\right)^{0.5}
$$

[0032]
When the distance $L$ is determined, $k_{1}$ is constant. Consequently, a table of $k_{1}$ with respect to the distance $L$ is formed as a lookup table and multiplication by $\mathrm{k}_{1}$ obtained from the lookup table is executed, thereby enabling ( $\mathrm{X}_{2}, \mathrm{Y}_{2}, \mathrm{Z}_{2}$ ) to be obtained as follows (refer to Fig. 3).

$$
\begin{aligned}
& X_{2}=k_{1} \cdot X_{1} \\
& Y_{2}=k_{1} \cdot Y_{1} \\
& Z_{2}=k_{1} \cdot Z_{1}
\end{aligned}
$$

In this manner, the first projection coordinates on the hemispherical face are determined.

## Step 2

[0033] As a second step of the calculation, a procedure of obtaining second projection coordinates $w\left(p_{1}\right.$, $q_{1}$ ) on a fisheye image face from the first projection coordinates ( $\mathrm{X}_{2}, \mathrm{Y}_{2}, \mathrm{Z}_{2}$ ) determined (refer to Fig. 1 with respect to w ) will be explained.
[0034] As described above, since the point $P^{\prime}$ is on the surface of the hemisphere of radius of 1 , the zenithal angle $\left(\theta_{1}\right)$ is unconditionally determined from the value of $Z_{2}$ (refer to Fig. 1 with respect to $\theta_{1}$ ). The following equation (1) is therefore derived.

$$
\begin{equation*}
\theta_{1}=\cos ^{-1}\left(Z_{2}\right) \tag{1}
\end{equation*}
$$

[0035] Since the azimuth of the point $w$ on the image pickup face and that of the point $\mathrm{P}^{\prime}$ on the hemispherical face are the same, the following equation (2) is satisfied.

$$
\begin{equation*}
\left(p_{1}, q_{1}\right)=k_{2} \cdot\left(X_{2}, Y_{2}\right) \tag{2}
\end{equation*}
$$

[0036] Since the height (h) from the origin on the fisheye image face (origin of the p, q coordinate system) to the point $w$ is expressed as a function of $\theta_{1}$ according to the fisheye image projecting method, the following equation (3) is satisfied.

$$
\begin{equation*}
h=F\left(\theta_{1}\right) \tag{3}
\end{equation*}
$$

[0037] Some examples of specific functions of $F\left(\theta_{1}\right)$ according to the projecting method will be shown. When it is assumed that the focal distance of the fisheye lens is $f$, the following relations are established.
equidistant projection: $\mathbf{h}=\mathrm{f} \cdot \boldsymbol{\theta}$
stereoscopic projection: $\mathbf{h}=2 \mathrm{f} \cdot \tan (\theta / 2)$
[0038] When the equation (1) is substituted for the
equation (3), the following equation (4) is given. h can be expressed as a function determined by $\mathrm{Z}_{2}$.

$$
\begin{equation*}
h=F\left(\cos ^{-1}\left(Z_{2}\right)\right) \tag{4}
\end{equation*}
$$

[0039] With respect to the distance $r$ from the origin of the $(X, Y, Z)$ coordinate system to the point $Q$ obtained by projecting the point $P^{\prime}$ onto the ( $\mathrm{X}, \mathrm{Y}$ ) plane, since the point $P^{\prime}$ is a point on the surface of the hemisphere of radius of 1 , the following equation (5) is satisfied.

$$
\begin{equation*}
r=\left(1-Z_{2}^{2}\right)^{0.5} \tag{5}
\end{equation*}
$$

[0040] The following equation (6) is therefore given from the equations (4) and (5).

$$
\begin{align*}
& k_{2}=h / r \\
& =F\left(\cos ^{-1}\left(Z_{2}\right)\right) /\left(1-Z_{2}{ }^{2}\right)^{0.5}(6) \tag{6}
\end{align*}
$$

[0041] That is, the coefficient $k_{2}$ of the equation (2) can be derived as a function of $Z_{2}$. With respect to the coefficient $k_{2}$, a lookup table for obtaining the coefficient $k_{2}$ from the value of $Z_{2}$ in accordance with the equation (3) is generated. By using the value, second projection coordinates $\left(p_{1}, q_{1}\right)$ on the image pickup face are obtained as follows.

$$
\begin{aligned}
& p_{1}=k_{2} \cdot X_{2} \\
& q_{1}=k_{2} \cdot Y_{2}
\end{aligned}
$$

[0042] As described above, in the first step for image transformation, calculation is limited to addition, subtraction, multiplication, and square root, and the other functions are obtained from the lookup table. The calculation in the second step is limited to multiplication and the other calculation of functions and the like is handled by referring to the lookup table. By executing the calculations in accordance with the steps, a simple arithmetic circuit (logic circuit such as an adder) can have a pipelined architecture. The circuit scale of the part of the complicated function calculation is suppressed by using the lookup table. Further, by changing the table for obtaining $k_{2}$ in the second step, a fisheye lens of a different projecting method can be dealt with easily, moreover, by the same arithmetic circuit.

## (Example of circuit configuration)

[0043] A specific circuit block configuration will now be described with reference to Fig. 4. The configuration relates to an example of a substrate which is configured for a computer system having a PCl (Peripheral Component Interconnect) bus.
[0044] A fisheye lens 2 is attached to a CCD camera 1 and image information obtained by the CCD cam-
era 1 is sent to a PCl bus substrate 3 and subjected to processes for image transformation. The PCI bus substrate 3 comprises: a camera interface 30 for obtaining fisheye image data from a CCD provided for the CCD camera 1; a frame memory 31 for storing fisheye image data of one frame; an interpolation computing unit 32 for executing an interpolating computation on the basis of the calculation result of an operation part 40; an FIFO memory 33 ; a capture control unit 34 for controlling capture of the fisheye image data to the frame memory 31; the operation part 40 (part surrounded by a broken line) having the configuration which characterizes the invention; and a PCI bus interface 39 for sending plane image data obtained by the coordinate transformation.
[0045] The operation part 40 comprises a first coordinate calculating unit 35, a second coordinate calculating unit 36, a first lookup table 37 connected to the first coordinate calculating unit 35, and a second lookup table 38 connected to the second coordinate calculating unit 36. Further description will be given in relation to the coordinate transforming procedure. The first coordinate calculating unit 35 is a part of executing the calculation of the first step shown in Fig. 3 and can obtain the first projection coordinates $\left(X_{2}, Y_{2}, Z_{2}\right)$ on the hemispherical face from the ( $u, v$ ) coordinates in the plane image. The first lookup table 37 is a table for obtaining the correction coefficient $k_{1}$ from the distance $L$.
[0046] The second coordinate calculating unit 36 is a part of executing the calculation of the second step in Fig. 3 and can obtain the second projection coordinates ( $p_{1}, q_{1}$ ) on the fisheye image face from the first projection coordinates $\left(X_{2}, Y_{2}, Z_{2}\right)$ derived by the first coordinate calculating unit 35 . The second lookup table 38 is a table for obtaining the correction coefficient $k_{2}$.

## (Description of circuit operation)

[0047] The operation of the circuit shown in Fig. 4 will now be described.
[0048] Fisheye image data obtained by the CCD camera 1 is written into the frame memory 31 via the camera interface 30 . Since the coordinates ( $p, q$ ) on the image pickup face corresponding to the coordinates ( $u$, $v$ ) on the display screen are obtained in the operation part 40, image data corresponding to the coordinates ( $p, q$ ) sequentially designated by the operation part 40 is read from the frame memory 31 and is sent to the interpolation computing unit 32.
[0049] Strictly, the position of a pixel on the fisheye image does not coincide with a pixel on the plane image to be displayed on the monitor. Plural data of pixels nearby is consequently read from the frame memory 31 and interpolation is performed by obtaining a weighted mean of the data, thereby enabling a natural plane image to be obtained.
[0050] The interpolated image data is subjected to speed adjustment by the FIFO memory and resultant data is transferred to a memory on the host computer
side via the PCI bus interface 39. In case of the example of the configuration of Fig. 4, since the processes such as coordinate calculation and interpolating calculation can be executed by a middle-scale FPGA (or gate array), the hardware can be constructed relatively cheap.

## Claims

1. An arithmetic unit for image transformation for transforming a fisheye image obtained by using a fisheye lens (2) into a plane image for display, characterized by comprising:

- a first coordinate calculating unit (35) for obtaining first projection coordinates derived by projecting coordinates on the plane image onto a fisheye image face as an imaginary object face; and
- a second coordinate calculating unit (36) for obtaining second projection coordinates derived by projecting the first projection coordinates obtained by the first coordinate calculating unit (35) onto the fisheye image face.

2. The arithmetic unit according to claim 1, characterized in that a logic circuit for arithmetic operation has a pipelined architecture in each of the first and second coordinate calculating units $(35,36)$.
3. The arithmetic unit according to claim 2 , characterized in that the logic circuit for arithmetic operation is limited to calculations of addition, subtraction, multiplication, and square root, and division and other function calculations are handled by referring to a lookup table $(37,38)$.
4. The arithmetic unit according to claim 3, characterized in that the second coordinate calculating unit (36) is used to obtain the second projection coordinates by multiplying the first projection coordinates by a predetermined coefficient ( k 1 ) and the predetermined coefficient ( $\mathbf{k}$ ) is obtained from a lookup table (38).
5. A monitoring system comprising

- a CCD camera (1) to which a fisheye lens (2) is attached and
- a Peripheral Component Interconnect (PCI) bus substrate (3) having an arithmetic unit for image transformation for transforming a fisheye image obtained by using the fisheye lens (2) into a plane image for display, characterized in that the arithmetic unit for image transformation comprises:
- a first coordinate calculating unit (35) for obtaining first projection coordinates derived by
projecting coordinates on the plane image onto a fisheye image face as an imaginary object face; and
- a second coordinate calculating unit (36) for obtaining second projection coordinates derived by projecting the first projection coordinates obtained by the first coordinate calculating unit (35) onto the fisheye image face.

6. The monitoring system according to claim 5 , characterized in that a logic circuit for arithmetic operation has a pipelined architecture in each of the first and second coordinate calculating units $(35,36)$.
7. The monitoring system according to claim 6, characterized in that the logic circuit for arithmetic operation is limited to calculations of addition, subtraction, multiplication, and square root, and division and other function calculations are performed by referring to a lookup table $(37,38)$.
8. The monitoring system according to claim 7, characterized in that the second coordinate calculating unit (36) is used to obtain the second projection coordinates by multiplying the first projection coordinates by a predetermined coefficient (k1) and the predetermined coefficient (k1) is obtained from a lookup table (38).

## FIG. 1



FIG. 2


FIG． 3
（Step 1）

（Step 1）


FIG. 4


## EXHIBIT 4

Assignee:
Filed: Louis, Mo.
Nov. 4, 1974
U.S. Cl.

350/189; 350/181
[51]
Field of Search B29D 13/18; G02B 13/08 .. 3 350/189, 192, 198, 175, 350/181

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## [57]

## ABSTRACT

A non-linear lens possesses distortion characteristics which are such that objects along the optical axis of the lens occupy disproportionately large areas of the image cast by the lens, whereas objects near the periphery of the field of view occupy a disproportionately small area of the image. The distortion characteristics approximate the formula $\mathrm{H}=\sin ^{1 / 3} \theta$ where H is height measured from the optical axis and $\theta$ is the angle measured from the optical axis. The image cast by the lens falls on the vidicon of a television camera where it is scanned and transmitted to a projector. Since the lens enlarges objects in the vicinity of the optical axis, those objects are transmitted with much greater detail than objects in the peripheral region of the view. The transmitted image is reproduced at a projector and the reproduced image is rectified through another lens having identical distortion characteristics. This lens casts the rectified image on a spherical screen. The final image which appears on the screen possesses a high degree of acuity in the region of the optical axis and substantially less acuity in peripheral regions. The resolution throughout the entire field of the reproduced image corresponds quite closely to the resolution characteristics of the human eye.

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10 Claims, 7 Drawing Figures
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FIG.I


FIG. 2


FIG. 3


FIG. 4


FIG. 6


FIG. 7

## NON-LINEAR LENS

The Government has rights in this invention pursuant to Contract Number N00014-73-C-0154 awarded by the Department of the Navy.

## BACKGROUND OF THE INVENTION

The present invention relates in general to lenses and more particularly to a lens having non-linear distortion characteristics.
The typical remote viewing system utilizes a television camera at the remote location, some type of projector at the observer location, and a television transmitting system linking the two. These viewing systems fall far short of duplicating the visual characteristis of the human eye in that they have extremely limited fields of view or else poor resolution in a large field of view.

In particular, for any fixed angular resolution (measured in minutes of arc) and frame rate (usually 30 Hz or frames/sec.) a definite relationship exists between field of view and bandwidth for transmitting that field of view. For example, commercial television, which utilizes a 525 line raster traced 30 times per second, operates on a bandwidth of 3.93 MHz . To match the resolution of the human eye, which is one minute of arc along its foveal or optical axis, the field of view for commercial television must be restricted to less than $10^{\circ}$ (see FIG. 1). On the other hand, if the field of view is increased to about $180^{\circ}$, which is the field of view for the human eye, the bandwidth must be increased to 1000 Mhz to maintain one minute of arc resolution over the entire field. This demands a raster of 10,000 lines and is far in excess of the capabilities of current television systems.

Indeed, the most advanced television currently available utilizes an 875 line system and requires a bandwidth of 10.9 Mhz . This provides a field of view of about $20^{\circ}$ with one minute arc resolution throughout the entire field, which is far less than the $180^{\circ}$ field of view possessed by the human eye.

From the foregoing, it is clear that present television viewing systems present a dilemma. If the field of view is sufficient to encompass all possible locations of interest, resolution is so low that detection or clear observation is impossible. On the other hand, if the resolution is adequate to insure that the objects will be seen clearly, the field of view is quite limited and many objects of interest are located outside of the field of view.

In a sense the human eye provides a solution for the foregoing dilemma. The human eye possesses high optical acuity along and in the vicinity of its foveal or optical axis, but the acuity diminishes outwardly therefrom. In other words, the eye distinguishes fine detail directly in front of it, but not to the sides. This characteristic is not derived from the shape of the eye lens, but instead results from the fact that most of the optical fibers for the eye are concentrated in the vicinity of the optical axis. Hence, only along the optical axis does the eye possess one minute of arc resolution. The resolution becomes progressively less toward the periphery of the field of vision (see FIG. 2). Nevertheless, the resolution in the peripheral area is sufficient to detect the presence of many objects in that area as well as much movement in that area. Of course, when the eye detects anything of interest in the peripheral areas, the head or
eye is immediately moved to bring the foveal axis to the thing of interest and thereby provide a clearer image of it.

## SUMMARY OF THE INVENTION

One of the principal objects of the present invention is to provide a lens having non-linear distortion characteristics which are such that objects located along and near the optical axis of the lens occupy a disproportionately large area of the image produced by the lens. Another object is to provide a lens of the type stated which closely approximates the resolution characteristics of the human eye over a wide field of view. A further object is to provide a lens of the type stated which is ideally suited for use in remote viewing systems in that it provides a wide field of view with maximum acuity along the optical axis. These and other objects and advantages will become apparent hereinafter.

The present invention is embodied in a lens which distorts a field of view such that objects in the vicinity of the optical axis occupy a disproportionately large area of the image cast by the lens and objects in the peripheral region of the field of view occupy a disproportionately small area of the image. The invention also consists in the parts and in the arrangements and combinations of parts hereinafter described and claimed.

## DESCRIPTION OF THE DRAWINGS

In the accompanying drawings which form part of the specification and wherein like numerals and letters refer to like parts wherever they occur:
FIG. 1 is a graph showing the relationship between field of view, angular resolution, and bandwidth for transmitting a picture of a remote location by television;
FIG. 2 is a graph showing relative acuity of the human eye throughout the field of view for the eye;
FIG. 3 is a graph showing the distortion characteristics of the lens of the present invention in terms of normalized image height and field of view and comparing such distortion characteristics with the distortion characteristics of a fisheye lens and a conventional camera lens;
FIG. 4 is a graphic representation of the non-linear distortion characteristics and showing how equal increments on the image plane correspond to unequal increments in the field of view;

FIG. 5 is a schematic perspective view of the remote viewing system in which the non-linear lens may be utilized;

FIG. 6 is a sectional view of the non-linear lens; and
FIG. 7 is an enlarged sectional view of the second and third lens groupings for the non-linear lens.

## DETAILED DESCRIPTION

The lens of the present invention (FIGS. 6 and 7) provides non-linear image distortion characteristics over an extremely wide field of view which approaches $160^{\circ}$. This is in contrast to so-called fisheye lenses which provide linear distortion characteristics. In paticular, with a linear or fisheye lens the image height is directly proportional to the field angle (FIG. 3). The relationship is defined by the formula $H=K \theta$ where $H$ is the image height from the optical axis, $K$ is a constant, and $\theta$ is the angle measured from the optical axis. Thus, with a linear lens an object occupying twice the angle as another object, when measured from the optical axis, will cast an image twice as high as the other
object. On the other hand, with a non-linear lens of the present invention the image height is equal to a variable function of the field angle (FIG. 3). The relationship is approximated by the formula $\mathrm{H}=\sin ^{1 / 3} \theta$. Thus, objects centered along the optical axis of the non-linear lens $L$ cast a much larger image than objects located near the periphery of the field of view with the size diminishing as the angle from the optical axis increases. The result of the distortion is that objects along the optical axis occupy a disproportionately large share of the image cast by the lens when compared with other objects closer to the periphery of the field of view for the lens. In effect, the center of the non-linear lens is a telephoto lens, while the periphery of the lens amounts to a wide angle lens with the annular region between the center and periphery varying from telephoto to wide angle. Naturally, the image produced is quite distorted. The typical camera lens is represented by the formula $\mathbf{H}=\mathrm{K}$ $\tan \theta$ (FIG. 3) and is non-linear, but in a sense opposite from that of the lens of the present invention.
The non-linear transfer characteristics of the lens may be illustrated by breaking the image into equal angular increments (FIG. 4) and comparing each image increment with the corresponding increment it represents in the actual field of view. Clearly, equal angular increments on the image side of the lens represent unequal increments on the object side of the lens. More specifically, near the optical axis relatively small arcs on the object side are converted to large arcs on the image side, thus enlarging the image. At about $25^{\circ}$ from the optical axis arcs on the object side equal the arcs on the image side and this portion of the lens may be considered linear. Objects from about $25^{\circ}$ to $80^{\circ}$ (lens periphery) occupy arcs much larger than they cast on the image side with the variance in arcs becoming greater as the object approaches the periphery of the field. Hence, objects within $25^{\circ}$ of the optical axis for the lens are magnified with the magnification being substantial along the lens axis, whereas objects in the annular region located beyond $25^{\circ}$ are reduced in size, with the reduction becoming progressively greater as the maximum field angle for the lens is approached.
To appreciate the lens requires an understanding of the remote viewing system in which it is utilized. That viewing system basically comprises (FIG. 5) a television camera at the remote location, a projector at the observer location, and a transmission system linking the camera and projector in both directions. Both the camera and projector are fitted with non-linear lenses having identical distortion characteristics. However, the projector lens is mounted just the reverse of the camera lens so that it rectifies the distortion created by the camera lens. The camera is supported on a gimballed mount and is therefore capable of swinging both vertical and horizontal angles with respect to fixed coordinates at the remote location. A suitable servo mechanism bridges the gimballed mount to control the position of the camera. The projector is likewise supported on a gimballed mount which permits it to swing both vertical and horizontal angles with respect to fixed coordinates at the observer location. Another servo mechanism bridges the gimballed mount of the projector, and this servo is slaved to the camera through the transmission system such that a change in elevation or azimuth of the camera with respect to its fixed coordinates results in a corresponding change in elevation and azimuth of the projector with respect to its fixed coordinates.

The projector projects the transmitted image through its non-linear lens which casts the image upon a spherical screen surrounding the projector. The observer views the screen from the position of the projector.
Positioned on the projector is an oculometer which views the observer's eye through a transparent beamsplitter, and in effect tracks the observer's eye, producing error signals whenever the foveal axis of the eye deviates from the optical axis of the projector lens. In other words, error signals are produced when the foveal axis of the eye and the optical axis of the projector lens intersect the screen at different locations. These signals are converted into elevation and azimuth commands which are transmitted to the servo system for the camera through the transmission system. The commands cause the camera to change elevation and azimuth, and the movement is such that the corresponding movement of the projector reduces the error and brings the foveal axis of the camera back toward coincidence with the optical axis of the lens, at least at the screen Thus, the oculometer controls the position of the camera and the camera controls the position of the projector, so in effect the camera and projector are both slaved to the observer's eye through the oculometer. The oculometer and servo mechanisms for the camera and projector should all respond fast enough to bring the optical axis of the projector lens into coincidence with, or at least within 2 percent of, the foveal axis for the eye within 0.2 seconds. This is about as rapidly as the eye can fixate and perceive when changing from one object of interest to another, so the lag in the projector is barely discernible, if at all. A suitable oculometer is marketed by Honeywell Inc., Radiation Center, Boston, Mass.
Referring again to the television camera at the remote location, the camera lens casts the distorted image of all objects in the field of view on the vidicon of the camera, and this vidicon is scanned in the usual manner, that is with a beam which traces a raster pattern at uniform velocity. The conventional commercial television system of 525 lines per scan and 30 scans per second may be employed. This requires a bandwidth of 3.93 MHz (FIG. 1). The beam in effect picks the image off of the camera vidicon. Since the objects along the optical ax is are magnified and occupy a disproportionately large area of the vidicon, they are picked off the vidicon in great detail. On the other hand, objects in the peripheral region of the field of view are reduced in size and occupy relatively little area on the vidicon. Hence, they are picked off of the vidicon with substantially less detail. The picture is transmitted accordingly. The magnification along and near the optical axis is great enough to enable the beam to extract one minute of arc detail, which is all an eye with $20-20$ vision can perceive along its foveal axis. The beam extracts greater angles of arc detail away from the optical axis and hence poorer resolution is available in this area. In this regard, it will be recalled that to extract one minute arc detail over a full $180^{\circ}$ requires a 10,000 line vidicon or in other words a bandwidth of 1000 MHz which is far in excess of present television capabilities.

The distorted image cast upon the vidicon of the camera is reproduced by the light valve of the projector and this image likewise has at least one minute of arc resolution along the optical axis with the resolution diminishing toward the periphery of the image so that only much larger angles of arc are discernible beyond the optical axis. The image so produced is rectified by
the projector lens which casts it upon the spherical screen. The resulting screen image constitutes a faithful reproduction of the scene which lies within the field of view for the camera lens. The projector lens in no way affects the resolution of the image it transmits and as a result the image appearing on the screen shows detail as close as one minute of arc at the optical axis for the lens and the area immediately surrounding it, but in the remaining area such detail is not available. In other words, the resolution in the other areas is somewhat less. Hence, the projected image is very sharp and clear on the screen at the optical axis, that is directly in front of the projector, and then turns somewhat fuzzy or blurred in the surrounding area particularly at the maximum angle of $80^{\circ}$ from the optical axis.

The variance in clarity or in resolution of the final image cast upon the screen closely resembles the optical characteristics of the eye (FIG. 2). In this connection, it will be recalled that most of the optical sensing elements for the human eye are concentrated along the foveal axis.

As previously mentioned, the oculometer tracks the eye position and causes the camera to change position in response to eye movement while the projector undergoes corresponding movement as a result of being slaved to the camera. Consequently, the foveal or optical axis of the eye is always directed at the center of the projected image, that is the portion along the optical axis for the projector lens. This is the portion having the one minute of arc resolution. Since the resolution of the eye falls off with the angle from the foveal axis, little is lost by having the resolution of the projected image diminish with the angle from the optical axis. The resolution in the surrounding area of the picture is still good enough to permit the eye, as a result of the built-in peripheral vision, to detect movement and objects of interest, and if whatever is detected appears interesting enough, the viewer will turn his eye toward it. This, of course, causes the camera and projector to change position so that the formerly blurred area of the image to which the eye is turned lies along the optical axis of the camera and projector lenses and is projected with high resolution.

The non-linear lens (FIGS. 6 and 7) has three lens sets or groupings A, B and C. Its aperture ratio is 5.6 and it forms a 0.358 F diameter image where F is the focal length along the optical axis $Z$. The first lens grouping $A$ is considerably larger than the other grouping $B$ and $C$ and is contained in the large end of a tapered lens housing. The other lens groupings $\mathbf{B}$ and C are contained within a subhousing which fits into the small end of the tapered main housing. The first lens grouping is a triplet and provides the mapping function, that is the unique distortion which is essentially defined by the formula $\mathrm{H}-\sin ^{1 / 3} \theta$. The second grouping B , which has four elements, contains the aperture stop and forms an image of the scene as distorted by the first grouping A . The third grouping C is a single element which functions as a fieid flatener, that is it makes the image cast by the second grouping B planar.
The first lens grouping A (FIG. 6) consists of three lens elements $a, b$, and $c$ with no air gaps between adjacent elements. The outside lens element $a$ has a nonspherical surface $R_{1}$ exposed outwardly and a spherical surface $R_{2}$ presented inwardly against a matching surface $\mathbf{R}_{2}$ on the intermediate element $b$. The opposite surface $R_{3}$ of the intermediate element $b$ is non-spherical and abuts a matching surface $\mathrm{R}_{3}$ on the inside ele-
ment $c$. The inside element $c$ also has a spherical surface $R_{4}$ which faces the tapered interior of the housing 2 and is presented toward the second lens grouping B. Along the optical axis Z for the lens, the element $a$ has a thickness $t_{1}$, the element $b$ a thickness $t_{2}$, and the element $c$ a thickness $t_{3}$. Index matching oil couples the matching surfaces $\mathrm{R}_{2}$ of the lens elements $a$ and $b$ and the matching surfaces $\mathrm{R}_{3}$ of the lens elements $b$ and $c$. The outside and inside lens elements $a$ and $c$ are formed from type SK16 glass, whereas the intermediate lens element is formed from type F2 glass. The index of refraction for SK16 glass is 1.62041 and for F2 glass is 1.62004. The Abbe number for SK 16 is 60.27 and for F 2 is 36.25 .
Turning now to the second lens grouping $B$, it consists of four lens elements, namely, a convex-concave lens element $d$, a double convex lens element $e$, a double concave lens element $f$, and a double convex lens element $g$, all arranged in that order from the first lens grouping A. The innermost lens element $d$ has spherical surfaces $R_{5}$ and $R_{6}$ and a thickness $t_{5}$, along the optical axis Z . The next lens element $e$ has spherical surfaces $\mathbf{R}_{7}$ and $\mathbf{R}_{8}$ and a thickness $t_{7}$ along the optical axis $\mathbf{Z}$. Next, is the double concave lens element $f$ having spherical surfaces $R_{9}$ and $R_{10}$ and a thickness $t_{10}$ along the optical axis. Z. The surface $\mathbf{R}_{10}$ of the element $f$ corresponds to and is against a matching surface $\mathrm{R}_{10}$ on the lens element $g$ which has another spherical surface $\mathrm{R}_{11}$ presented toward the third lens grouping C . The surfaces $\mathrm{R}_{6}$ and $\mathrm{R}_{7}$ of the lens elements $d$ and $e$, respectively, are separated by an air gap $t_{6}$ measured along the axis $Z$ of the lens, while the surfaces $R_{6}$ and $R_{9}$ of the lens elements $e$ and $f$, respectively, are separated by an air gap $\mathrm{t}_{8}$ measured along the optical axis Z . The matching surfaces $\mathbf{R}_{10}$ of the lens element $f$ and $g$ are cemented. The lens elements $d$ and $f$ are formed from type F2 glass, while the lens elements $e$ and $g$ are formed from type SK 16 glass.
The third lens grouping $\mathbf{C}$ contains a single lens element $h$ having a non-spherical and non-planar surface $\mathrm{R}_{12}$ which is presented toward the second lens group $B$ and a spherical surface $R_{13}$ exposed outwardly. The lens element $h$ has a thickness $t_{12}$ along the optical axis Z and is made from the type SK16 glass.
The first and second lens groupings A and B are separated by an air gap $t_{4}$ which is measured from the surface $R_{4}$ to the surface $R_{5}$ along the axis $Z$ of the lens. The second and third lens groupings $B$ and $C$ are separated by an air gap $t_{11}$ which is the distance between the surfaces $\mathrm{R}_{11}$ and $\mathrm{R}_{12}$ measured along the optical axis Z .

The distorted image formed by the non-linear lens exists in an image plane $p$ located beyond the third lens grouping $C$. The vidicon of the television camera should be at this plane $p$.
The surfaces $\mathbf{R}_{2}, \mathbf{R}_{4}, \mathbf{R}_{5}, \mathbf{R}_{6}, \mathbf{R}_{7}, \mathbf{R}_{8}, \mathbf{R}_{8}, \mathbf{R}_{10}, \mathbf{R}_{11}$ and $R_{13}$ are all spherical and have their centers of curvature along the optical axis $Z$ of the lens. The surfaces $R_{1}, R_{3}$, and $R_{12}$, while being curved, are not spherical. The radii of curvature for the surfaces $R_{1}$ through $R_{13}$ follow:

-continued
0.280 F

$$
\begin{array}{ll}
<R_{10} & <0.285 F \\
<-R_{11} & <0.572 F
\end{array}
$$

$$
\begin{array}{ll}
<-R_{11} & <0.572 F \\
-\mathbf{R}_{12} & : 0.314 F
\end{array}
$$

$: 0.314 F$
$<0.4173 F$
(at optical axis only)
where $F$ is the focal length of the lens along its optical axis $Z$. Note, that since the surfaces $R_{1}, R_{3}$ and $R_{13}$ are not spherical, the radii of curvature listed above for those surfaces represents only radii along the optical axis $Z$ of the lens.
The thicknesses of the various lens elements measured along the optical axis Z follow:
$0.199 \mathrm{~F}<t_{1}<0.202 \mathrm{~F}$
$0.399 \mathrm{~F}<t_{2}<0.402 \mathrm{~F}$
$0.399 \mathrm{~F}<t_{3}<0.402 \mathrm{~F}$
$0.047 \mathrm{~F}<t_{5}<0.049 \mathrm{~F}$
$0.186 \mathrm{~F}<t_{7}<0.189 \mathrm{~F}$
$0.019 \mathrm{~F}<t_{9}<0.022 \mathrm{~F}$
$0.06 \mathrm{~F}<t_{10}<0.07 \mathrm{~F}$
$0.08 \mathrm{~F}<t_{12}<0.09 \mathrm{~F}$
The thicknesses of the air gaps measured along the optical axis $Z$ follow:
$3.248 \mathrm{~F}<t_{4}<3.251 \mathrm{~F}$
$0.0004 \mathrm{~F}<t_{6}<0.0014 \mathrm{~F}$
$0.266 \mathrm{~F}<t_{11}<0.267 \mathrm{~F}$
$0.037 \mathrm{~F}<t_{8}<0.041 \mathrm{~F}$
As previously noted, the surfaces $R_{1}, R_{3}$, and $R_{13}$ are neither spherical nor planar. Furthermore, not one of them fits any single known mathematical formula. They are defined in terms of splines, that is each surface is broken up into increments or intervals which are defined separately. The surfaces $R_{1}, R_{3}$ and $R_{13}$ are considered spline surfaces and are defined by the following cubic spline equation:

$$
\begin{aligned}
S(\rho)= & M_{i-1} \frac{\left(\rho_{i}-\rho\right)^{3}}{6 h_{i}}+M_{1} \frac{\left(\rho-\rho_{i-1}\right)^{3}}{6 h_{i}} \\
& +\left(x_{i-1}-\frac{M_{i-1} h_{1}^{2}}{6}\right) \frac{\left(\rho_{i}-\rho\right)}{h_{i}}+\left(x_{i}-\frac{M_{i} h_{i}^{2}}{6}\right)\left(\rho-\rho_{i-1}\right)
\end{aligned}
$$

where
$\rho_{i-1}=$ The value of the spline surface height at the start of the ith interval.
$\rho_{i}=$ The value of the spline surface height at the end of the ith interval.
$X_{i-1}=$ The value of the spline surface sag at the start of the ith interval.
$X_{1}=$ The value of the spline surface sag at the end of the ith interval.
$h_{i}=\rho_{i}-\rho_{i-1}=$ The length of the ith interval.
$\mathbf{M}_{i-1}=$ The value of the slope derivative at the start of the ith interval.
$\mathbf{M}_{i}=$ The value of the slope derivative at the end of the ith interval.
$\rho=$ The spline surface height (independent variable)
$S(\rho)=$ The spline surface sag as a function of height (dependent variable)
The slope of a spline surface element at a particular height ( $\rho$ ) is given by

$$
\text { Slope }=\mathrm{d} \mathrm{~S}(\rho) / \mathrm{d} \rho
$$

The values of spline surface sag (X), spline surface height ( $\rho$ ), and slope derivative ( $M$ ) for various spline intervals $0,1,2$, etc. follow:

|  |  | $\begin{gathered} \text { Surface } \\ R_{1} \end{gathered}$ | $\begin{gathered} \text { Surface } \\ \mathrm{R}_{3} \\ \hline \end{gathered}$ | Surface $\mathrm{R}_{12}$ |
| :---: | :---: | :---: | :---: | :---: |
| 5 | $\mathbf{X}(0)$ | 0.0000000 | 0.0000000 | 0.0000000 |
|  | $\mathbf{X}(1)$ | 0.2108668 | 0.1795877 | -0.0029324 |
|  | $\mathbf{X}(2)$ | 0.8554116 | 0.7202623 | -0.0041130 |
|  | $\mathrm{X}(3)$ | 1.7838662 | 1.4361922 | -0.0004761 |
|  | $\mathbf{X}(4)$ | 1.9775600 | 1.6027882 | 0.0065340 |
|  | $\mathbf{X}(5)$ | - | - | 0.0100000 |
|  | $\mathbf{X}(6)$ |  | - | 0.0100000 |
| 10 | $\boldsymbol{\rho}(0)$ | 0.0000000 | 0.0000000 | 0.0000000 |
|  | $\rho(1)$ | 1.0780200 | 0.7222734 | 0.0825000 |
|  | $\rho(2)$ | 2.1560400 | 1.4444546 | 0.1650000 |
|  | $p$ (3) | 3.2340801 | 2.1668202 | 0.2475000 |
|  | $\rho(4)$ | 3.6360801 | 2.4760010 | 0.3300000 |
|  | $p(5)$ | - | - | 0.4010000 |
|  | $\rho(6)$ |  |  | 0.5000000 |
|  | $\mathrm{M}(0)$ | 0.3644990 | 0.6859612 | $-1.5916510$ |
| 15 | M(1) | 0.3596961 | 0.6935749 | 0.5983017 |
|  | M(2) | 0.4358774 | 0.6937277 | 0.7436587 |
|  | M(3) | -0.6375478 | -1.4543979 | 0.6856855 |
|  | M(4) | $-2.1376087$ | $\bigcirc 0.6921574$ | -0.5200549 |
|  | $\mathrm{M}(5)$ | - | - | 0.0000000 |
|  | M(6) | - | - | 0.0000000 |

What is claimed is:

1. A non-linear lens comprising first lens means for distorting a scene in the field of view for the lens such 25 that objects in the vicinity of the optical axis are given substantially greater prominence than objects in the peripheral region of the field of view, and second lens means for forming a real image of the scene as distorted by the first lens means, whereby objects in the vicinity 0 of the optical axis will occupy a disproportionately large area of the real image and objects in peripheral regions of the scene will occupy a disproportionately small area of the real image.
2. A lens according to claim 1 wherein the field of 35 view is at least approximately $160^{\circ}$.
3. A non-linear lens according to claim 1 and further characterized by third lens means for causing the real image formed by the second lens means to lie in a plane.
4. A non-linear lens according to claim 1 wherein the distortion in the real image approximates the formula

$$
H=\sin ^{1 / 3} \theta
$$

45
where $H$ is the distance in the image measured from the optical axis and $\theta$ is the angle measured from the optical axis.
5. A non-linear lens according to claim 1 wherein the first lens means comprises a plurality of individual lens elements and the second lens means includes a plurality of different lens elements.
6. A non-linear lens comprising a first lens grouping - for distorting a scene in the field of view for the lens such that objects in the vicinity of the optical axis are 5 given greater prominence than objects in the peripheral region of the field of view, the first lens grouping including first, second, and third lens elements, the first lens element having surfaces $R_{1}$ and $R_{2}$, the second lens element having surfaces $R_{2}$ and $R_{3}$, and the third lens 0 element having surfaces $R_{3}$ and $R_{4}$, the surface $R_{2}$ of the first lens element matching the surface $R_{2}$ of the second lens element and being substantially in contact therewith, the surface $R_{3}$ of the second lens element matching the surface $R_{3}$ of the third lens element and 5 being substantially in contact therewith, the surfaces $\mathbf{R}_{1}$ and $R_{3}$ being curved at the optical axis and being nonspherical beyond the optical axis, the surfaces $R_{2}$ and $\mathbf{R}_{\mathbf{4}}$ being spherical substantially throughout, the radii of
the surfaces along the optical axis being substantially as follows:

|  | $\mathrm{R}_{1}:$ |  | 1.37 | F |
| :--- | ---: | :--- | :--- | :--- |
| 1.4 F | $<\mathrm{R}_{2}$ | $<$ | 1.5 | F |
|  | 1.091 F | $\mathrm{R}_{3}:$ |  | 0.729 |
|  | $<\mathrm{R}_{\mathbf{4}}$ | $<$ | 1.092 | F |

where $F$ is the focal length of the lens along the optical axis of the lens; and a second lens grouping for forming a real image of the scene as distorted by the first grouping, whereby objects in the vicinity of the optical axis will occupy a disproportionately large area of the real image and objects in peripheral regions of the scene will occupy a disproportionately small area of the real image.
7. A lens according to claim 6 wherein the first, second, and third lens elements have thicknesses $t_{1}, t_{2}$ and $\mathbf{t}_{3}$, respectively, along the optical axis of the lens and the thicknesses are as follows:
$0.199 \mathrm{~F}<t_{1}<0.202 \mathrm{~F}$
$0.399 \mathrm{~F}<t_{2}<0.402 \mathrm{~F}$
$0.399 \mathrm{~F}<t_{3}<0.402 \mathrm{~F}$.
8. A non-linear lens according to claim 6 wherein the non-spherical surfaces $\mathrm{R}_{1}$ and $\mathrm{R}_{3}$ are defined by the cubic spline equation

$$
\begin{aligned}
S(\rho)= & M_{i-1} \frac{(\rho-\rho)^{3}}{6 h_{i}}+M_{i} \frac{\left(\rho-\rho_{i-1}\right)^{3}}{6 h_{i}} \\
& +\left(x_{i-1}-\frac{M_{i-1} h_{i}^{2}}{6}\right) \frac{\left(\rho_{i}-\rho\right)}{h_{i}}+\left(x_{1}-\frac{M_{i} h_{1}^{2}}{6}\right)\left(\rho-\rho_{i-1}\right)
\end{aligned}
$$

where
$\mathrm{i}-1=$ The value of the spline surface height at the start of the ith interval.
$\mathrm{i}=$ The value of the spline surface height at the end of the ith interval.
$\mathrm{X}_{i-1}=$ The value of the spline surface sag at the start of the ith interval.
$X_{i}=$ The value of the spline surface sag at the end of the ith interval.
$\mathrm{h}_{i}=\rho_{i}-\rho_{i-1}=$ The length of the ith interval.
$\mathbf{M}_{i-1}=$ The value of the slope derivative at the start of the ith interval.
$\mathrm{M}_{i}=$ The value of the slope derivative at the end of the ith interval.
$\rho=$ The spline surface height (independent variable)
$\mathbf{S}(\rho)=$ The spline surface sag as a function of height (dependent variable); and wherein the value for X at spline intervals $\mathbf{0}, \mathbf{1}, \mathbf{2}$, etc. is

|  | Surface | Surface |
| :---: | :---: | :---: |
|  | $R_{1}$ | $R_{3}$ |
| $\mathbf{X}(0)$ | 0.000000 | 0.0000000 |
| $\mathbf{X}(1)$ | 0.2108668 | 0.1795877 |
| $\mathbf{X}(2)$ | 0.855416 | 0.7202623 |
| $\mathbf{X}(3)$ | 1.7838662 | 1.4361922 |
| $\mathbf{X ( 4 )}$ | 1.9775600 | $1.6027882 ;$ |

3.251 F .
and

$$
0.0004 \mathrm{~F}<t_{6}<0.0014 \mathrm{~F}
$$

$0.08 \mathrm{~F}<t_{12}<0.09 \mathrm{~F}$;
and wherein the spaces separating the lens elements

$$
0.037 \mathrm{~F}<t_{8}<0.041 \mathrm{~F}
$$

$$
0.037 \mathrm{~F}<t_{8}<0.041 \mathrm{~F}
$$ the surface $\mathbf{R}_{4}$ in the first lens grouping and the surface $\mathrm{R}_{5}$ in the second lens grouping are separated by a distance $t_{4}$ which is greater than 3.248 F and less than

10. A non-linear lens according to claim 9 wherein * * * * *
0.0000000
0.7222734
1.4444546
2.1668202
2.4760010
and wherein the value for M at spline intervals $\mathbf{0}, \mathbf{1}, \mathbf{2}$, etc. is

| $M(0)$ | 0.3644990 | 0.6859612 |
| :--- | :--- | ---: |
| $M(1)$ | 0.3596961 | 0.6935749 |
| $M(2)$ | 0.4358774 | 0.6937277 |
| $M(3)$ | -0.6375478 | -1.4543979 |
| $M(4)$ | -2.1376087 | -0.6921574. |

9. A non-linear lens according to claim 6 wherein the second lens grouping comprises a convex-concave first lens element, a double convex second lens element, a double concave third lens element, and a double convex fourth lens element, arranged in that order from the first lens grouping, the first lens element having a thickness $t_{5}$ along the optical axis and spherical surfaces $R_{5}$ and $R_{6}$, the second lens element having a thickness $t_{7}$ and spherical surfaces $\mathrm{R}_{7}$ and $\mathrm{R}_{8}$, the third lens element having a thickness $t 9$ and spherical surfaces $\mathbf{R}_{9}$ and $\mathrm{R}_{10}$, and the fourth lens element having a thickness $t_{10}$ and spherical surfaces $R_{10}$ and $R_{11}$, the surface $\mathrm{R}_{10}$ of the third lens element matching the surface $\mathbf{R}_{10}$ of the fourth lens element and being substantially in contact therewith, the surfaces $R_{6}$ and $R_{7}$ being separated by a distance $t_{6}$ along the optical axis and the surfaces $\mathrm{R}_{8}$ and $\mathrm{R}_{9}$ being separated by a distance $t_{8}$ along the optical axis; wherein the radii of curvature for the surfaces are:

$$
\begin{aligned}
& 1.091 \mathrm{~F}<\mathrm{R}_{4}<1.092 \mathrm{~F} \\
& 0.2373 \mathrm{~F}<\mathrm{R}_{5}<0.2376 \mathrm{~F} \\
& 0.272 \mathrm{~F}<\mathrm{R}_{6}<0.237 \mathrm{~F} \\
& 0.3936 \mathrm{~F}<\mathrm{R}_{7}<0.3940 \mathrm{~F} \\
& 0.334 \mathrm{~F}<\mathrm{R}_{8}<0.335 \mathrm{~F} \\
& 0.268 \mathrm{~F}<\mathrm{R}_{9}<0.227 \mathrm{~F} \\
& 0.280 \mathrm{~F}<\mathrm{R}_{10}<0.285 \mathrm{~F} \\
& 0.571 \mathrm{~F}<\mathrm{R}_{11}<0.572 \mathrm{~F} ;
\end{aligned}
$$

wherein the thicknesses of the lens elements along the optical axis are
$0.047 \mathrm{~F}<t_{5}<0.049 \mathrm{~F}$
$0.186 \mathrm{~F}<t_{7}<0.189 \mathrm{~F}$
$0.019 \mathrm{~F}<t_{9}<0.022 \mathrm{~F}$
$0.06 \mathrm{~F}<t_{10}<0.07 \mathrm{~F}$

## EXHIBIT 3

United States Patent
Baker
[11] Patent Number: $\mathbf{5 , 6 8 6 , 9 5 7}$
Date of Patent:
[54] TELECONFERENCLNG IMAGING SYSTEM WITH AUTOMATIC CAMERA STEERING
Inventor: Robert G. Baker, Delray Beach, Fla.

Assignee: International Business Machines
Corporation, Armonk, N.Y.
[21] Appl. No.: 496,742
Filed: Jun. 30, 1995
Related U.S. Application Data
[63] Continuation-in-part of Ser. No. 281,331, Jul. 27, 1994, Pat. No. 5,508,734.
[51] Int. Cl. ${ }^{6}$ $\qquad$ H04N 7/18
U.S. Cl.
[58] Field of Search $\qquad$ 348/214; 348/580 348/15, 214, 36 348/53, 580 ; H04N 7/18
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Primary Examiner-Howard W. Britton
Attorney, Agent, or Firm-Richard A. Tomlin; John C. Black; Malin, Haley, DiMaggio \& Crosby, P.A. [57]

## ABSTRACT

An automatic, voice-directional video camera image steering system specifically for use for teleconferencing that electronically selects segmented images from a selected panoramic video scene typically around a conference table so that the participant in the conference currently speaking will be the selected segmented image in the proper viewing aspect ratio, eliminating the need for manual camera movement or automated mechanical camera movement. The system includes an audio detection circuit from an array of microphones that can instantaneously determine the direction of a particular speaker and provide directional signals to a video camera and lens system that provides a panoramic display that can electronically select portions of that image and, through warping techniques, remove any distortion from the most significant portions of the image which lie from the horizon up to approximately 30 degrees in a hemispheric viewing area.

14 Claims, 7 Drawing Sheets









## 1

## TELECONFERENCING IMAGING SYSTEM WITH AUTOMATIC CAMERA STEERING

This application is a continuation-in-part of U.S. patent application Ser. No. 281,331 filed Jul. 27, 1994 U.S. Pat. No. 5,508,734.

## BACKGROUND OF THE INVENTION

## 1. Field of the Invention

This invention relates to a video conferencing system that has automatic, voice-directional camera image steering, and specifically to a teleconferencing system that employs automatic video image selection of the current participant speaking electronically selected from a panoramic video scene.

## 2. Description of the Prior Art

Teleconferencing provides for the exchange of video and audio information between remotely separated participants. Typically, a first group of participants is arranged around a conference table or seated strategically in a conference room and telecommunicating with a second group of participants similarly situated at a remote location. One or more video cameras at each location creates video images of the participants through manual manipulation of each video camera, normally directed at the participant speaking at the moment. Microphones at each location provide for sound transmission signals. The video image and audio voice signals are then transmitted to the remote location. The video image is projected onto a large screen or other type of video display which also would include audio outputs for providing the sounds.

Manual manipulation of each video camera at each conference site is required to change the direction of each camera to different participants as speakers change, unless a large overall view of all the participants is maintained. Such a process is labor intensive. Also image content and perspective, dependent on the location of the video camera relative to the participants, contributes to the quality of the final visual display available to the participants watching the display screen. The quality of the image and the scene content all contribute to the overall effectiveness of the telecommunication process. In particular, in a setting such as a conference table in a conference room, a hemispheric or panoramic viewpoint would be much more efficient for video image capture of surrounding selected participants. With a hemispheric scene, certain efficiencies are gained by eliminating large areas that are unused scene content while concentrating on a band of hemispheric areas populated by the teleconferencing participants. Therefore, it is believed that hemispheric or panoramic electronic imaging would be greatly beneficial to a teleconferencing environment, especially when controlled with audio directional processors. The selected video image is taken from a desired segment of a hemispherical view in the correct video aspect ratio. A centralized panoramic image capture system which already has a distorted picture of the hemisphere bounded by the plane of the table upward selects a portion of the scene and warps the image to correspond to a normal aspect ratio view of the person speaking. The signal can be converted to whatever display format is desired for transmission to a remote location. The present invention has incorporated, in one automated system, audio beam steering and electronically selectable subviews of a much larger panoramic scene. The video/subviews can be converted to an NTSC display format for transmission to a remote location for video display.

The collection, storage, and display of large areas of visual information can be an expensive and difficult process
to achieve accurately. With the recent increased emphasis on multimedia applications, various methods and apparatuses have been developed to manage visual data. A unique class of multimedia data sets is that of hemispheric visual data. Known multimedia methods and apparatuses attempt to combine various multimedia imaging data, such as still and motion (or video) images, with audio content using storage media such as photographic film, computer diskettes, compact discs (CDs), and interactive CDs. These are used in traditional multimedia applications in various fields, such as entertainment and education. Teleconferencing is an application where automated electronic selection of scene content would result in greatly improved usability. Non-multimedia applications also exist that would employ hemi spheric visual data, such as in security, surveillance, unmanned exploration, and fire and police situations. However, as will be described below, the known methods and apparatuses have certain limitations in capturing and manipulating valuable information and hemispheric scenes in a rapid (i.e., real-time) and cost effective manner.

One well known multimedia technique is used at theme parks, wherein visual information from a scene is displayed on a screen or collection of screens that covers almost 360 degrees field of view. Such a technique unfortunately results in the consumption of vast quantities of film collected from multiple cameras, requires specially designed carriages to carry and support the cameras during filming of the scene, and necessitates synchronization of shots during capture and display. The technique is also limited in that the visual image cannot be obtained with a single camera nor manipulated for display, e.g., pan, tilt, zoom, etc., after initial acquisition. Hence, this technique, while providing entertainment, is unable to fulfill critical technical requirements of many functional applications.

Other known techniques for capturing and storing visual information about a large field of view (FOV) are described in U.S. Pat. Nos. 4,125,862; 4,442,453; and $5,185,667$. In U.S. Pat. No. $4,125,862$, a system is disclosed that converts signal information from a scene into digital form, stores the data of the digitized scene serially in two-dimensional format, and reads out the data by repetitive scan in a direction orthogonally related to the direction in which the data was stored. U.S. Pat. No. 4,442,453 discloses a system in which a landscape is photographed and stored on firm. The film is then developed, with display accomplished by scanning with electro-optical sensors at "near real-time" rates. These techniques, however, do not provide instant visual image display, do not cover the field of view required for desired applications (hemispheric or 180 degrees field-of-view), do not generate visual image data in the format provided by the techniques of this invention, and are also not easily manipulated for further display, e.g., pan, tilt, etc.

The technique disclosed in U.S. Pat. No. 5,185,667 overcomes some of the above-identified drawbacks in that it is able to capture a near-hemispheric field of view, correct the image using high speed circuitry to form a normal image, and electronically manipulate and display the image at real-time rates.

For many hemispheric visual applications, however, even U.S. Pat. No. $5,185,667$ has limitations in obtaining sufficient information of critical and useful details. This is particularly true when the camera is oriented with the central axis of the lens perpendicular to the plane bounding the hemisphere of acquisition (i.e. lens pointing straight up). In such applications, the majority of critical detail in a scene is contained in areas of the field along the horizon and little or no useful details are contained in central areas of the field
located closer to the axis of the lens (the horizon being defined as the plane parallel to the image or camera plane and perpendicular to the optical axis of the imaging system). For example, in surveillance, the imaging system is aimed upward and the majority of the critical detail in the scene includes people, buildings, trees, etc., most of which are located within only a few degrees along the horizon (i.e., this is the peripheral content). Also, in this example, although the sky makes up the larger central are of the view, it contains little or no useful information requiring higher relative resolution.

To obtain sufficient detail on the critical objects in the scene, the technique should differentiate between the relevant visual information along the horizon and the remaining visual information in the scene in order to provide greater resolution in areas of higher importance. U.S. Pat. No. $5,185,667$ does not differentiate between this relevant visual information contained along the horizon and the remaining visual information in this scene. Thus, it fails to yield a sufficient quality representation of the critical detail of the scene for projected applications.

Instead, techniques described above concentrate on obtaining, storing, and displaying the entire visual information in the scene, even when portions of this information are not necessary or useful. To obtain the near-hemispheric visual information, such techniques require specific lens types to map image information in the field of view to an image plane (where either a photographic film or electronic detector or imager is placed). Known examples of U.S. Pat. No. $5,185,667$ and U.S. Pat. No. $4,442,453$ respectively use a fish-eye lens and a general wide-angle lens. As these lenses map information of a large field without differentiation between the central and peripheral areas, information from the periphery will be less fully represented in the image plane than from the central area of acquisition.

In U.S. Pat. No. 4,170,400, Bach et al. describes a wide-angle optical system employing a fiber optic bundle that has differing geometric shapes at the imaging ends. Although this is useful in itself for collecting and repositioning image data, bending of light is a natural characteristic of optical fibers and not exclusive to that patent. Further, U.S. Pat. No. 4,170,400 employs a portion of a spherical mirror to gather optical information, rendering a very reduced subset of the periphery in the final imaging result. This configuration is significantly different from the multi-element lens combination described in the present invention.

Imperfections in the image representation of any field inherently result from the nature of creating an image with any spherical glass (or plastic) medium such as a lens. The magnitude of these imperfections increases proportionally to the distance a point in the field is from the axis perpendicular to the optical imaging system. As the angle between the optical axis and a point in the field increases, aberrations of the corresponding image increase proportional to this angle cubed. Hence, aberrations are more highly exaggerated in the peripheral areas with respect to more central areas of a hemispheric image.

Although the lens types above achieve a view of a large field, the valuable content from the peripheral areas lacks in potential image quality (resolution) mapping because the imaging device and system does not differentiate between these areas and the central areas of less valuable detail. Often, the difference between the imaging capabilities between the two areas is compensated for by using only the central portion of a lens to capture the scene ("stopping the
lens down"). This works in effect to reduce the image quality of both areas such that the difference in error is a lesser percentage of the smallest area even the central area can resolve. Simultaneously, this compensation technique further degrades the performance of the lens by limiting the amount of light which is allowed to enter the lens, and thus reducing the overall intensity of the image.

More typically, the peripheral content imaged by a conventional lens is so degraded in comparison with the central area that the lens allows for only a minimal area of the periphery to be recorded by the film or electronic imager. As a result of these "off-axis" aberrations inherent to large field, the relevant information of the horizon in the scene can be underutilized or worse yet, lost.

Another limitation in U.S. Pat. No. 5,185,667 is its organization for recording only views already corrected for perspective. The nature of that methodology is that the specific view of interest must be selected and transformed prior to the recording process. The result is that no additional selection of views can be accomplished after the storage process, reducing system flexibility from the user's perspective.

Hence, there is a demand in the industry for single camera imaging systems that efficiently capture, store, and display valuable visual information within a hemispheric field of view containing particularly peripheral content, and that allow electronic manipulation and selective display of the image post-acquisition while minimizing distortion effects.

Such a system finds advantageous application in a teleconferencing environment in accordance with the present invention.

Limited control of video cameras is disclosed in the prior art. U.S. Pat. No. 4,980,761 issued to Natori, Sep. 25, 1990 describes an image processing system that rotates a camera for a teleconference system. A control unit outputs a drive signal based on an audio signal to control the movement of the image until the image controlling unit receives an operational completion signal. In this case, the rotational movement of the camera, moving the video image from one participant to another participant, alleviates having to view the camera movement. Once the camera stops skewing, the picture will then provide the proper aspect ratio. A plurality of microphones are provided to each attendant. A sound control unit then determines with a speaker detection unit which participant is speaking. U.S. Pat. No. $4,965,819$ shows a video conferencing system for courtroom and other applications in which case each system includes a local module that includes a loud speaker, a video camera, a video monitoring unit and a microphone for each local conferee. U.S. Pat. No. 5,206,721 issued to Ashida, Apr. 27, 1993, shows a television conference system that allows for automatically mechanically moving and directing a camera towards a speaking participant. In this system a microphone is provided for each participant and is recognized by the control system. Image slew is corrected to avoid camera image motion. Areview of these systems thus shows that the automation provided is very expensive and in every case requires individualized equipment for each participant.

Limited audio direction finding for multiple microphone arrays is known in the prior art. For example, a self steering digital microphone array defined by W. Kellerman of Bell Labs at ICASSP in 1991 created a teleconference in which a unique steering algorithm was used to determine direction of sound taking into account the acoustical environment in which the system was located. Also a two stage algorithm for determining talker location from linear microphone array
data was developed by H. Silverman and S. Kirkman at Brown University and disclosed in April, 1992. The filtered cross correlation of the system is introduced as the locating algorithm.

A "telepresence" concept from BellCorp briefly described in IEEE Network Magazine in March, 1992 suggests a spherical camera for use in the teleconference system. However, the entire image is sent in composite form for the remote users to select from at the other end. The present invention is quite different and includes automated pointing and control including incorporation in one automated system of both audio beam steering and selectable subviews of a much larger panoramic scene.

## SUMMARY OF THE INVENTION

The present invention comprises a video conferencing, voice-directional video imaging system for automatic electronic video image manipulation of a selected, directional signal of a hemispheric conference scene transmitted to a remote conference site. The system employs three separate subsystems for voicedirected, electronic image manipulation suitable for automated teleconferencing imaging in a desirable video aspect ratio.

The audio beam, voice pickup and directing subsystem includes a plurality of microphones strategically positioned near a predetermined central location, such as on a conference table. The microphone array is arranged to receive and transmit the voices of participants, while simultaneously determining the direction of a participant speaking relative to the second subsystem, which is a hemispheric imaging system used with a video camera. The third subsystem is a personal computer or controller circuits in conjunction with the hemispheric imaging system which ultimately provides automatic image selection of the participant speaking that is ultimately transmitted as a video signal to the remote video display at the remote teleconference location.

The hemispheric electronic image manipulator subsystem includes a video camera having a capture lens in accordance with the invention that allows for useful electronic manipulation of a segmented portion of a hemispheric scene. In a conference table setting, as viewed from the center of the conference table, participants are arranged around the table in the lower segment of the hemisphere, with the plane of the table top forming the base of the hemisphere. The electronic image is warped to provide a desired subview in proper aspect ratio in the audio selected direction.

The present invention provides a new and useful voicedirectional visual imaging system that emphasizes the peripheral content of a hemispheric field of view using a single video camera. The invention allows user-selected portions of a hemispheric scene to be electronically manipulated, transmitted, and displayed remotely from the video camera in real-time and in a cost-effective manner.

The visual imaging system of the present invention involves a video image having a lens with enhanced peripheral content imaging capabilities. The lens provides an enhanced view of the valuable information in the scene's periphery by imaging the field of view to the image plane such that the ratio of the size of the smallest detail contained within the periphery of the scene to the size of the smallest resolving pixel of an image device is increased. For this to be accomplished, the peripheral content must map to a larger percentage of a given image detector area and, simultaneously, the mapped image of the central area of the scene must be minimized by the lens so that it does not interfere with the peripheral content now covering a wider
annulus in the image plane. Information in the image plane is then detected by the video camera. The detected information of the entire hemispheric scene is then stored as a single image in memory using traditional methods.

When a portion of the scene is to be displayed, the image information relating to the relevant portion of the scene is instantaneously retrieved from memory. A transform processor subsystem electronically manipulates the scene for display as a perspective-correct image on a display device, such as a teleconference display screen or monitor, as if the particular portion of the scene had been viewed directly with the video camera pointed in that direction. The transform processor subsystem compensates for the distortion or difference in magnification between the central and peripheral areas of the scene caused by the lens by applying appropriate correction criteria to bring the selected portion of the scene into standard viewing format. The transform processor subsystem can also more fully compensate for any aberrations of the enhanced peripheral image because of the image's improved resolution as it covers a larger portion of the image device (increased number of pixels used to detect and measure the smallest detail in the periphery image). More pixels equates to more measurement data, hence more accurate data collection.

The stored image can also be manipulated by the transform processor subsystem to display an operator-selected portion of the image through particular movements, such as pan, zoom, up/down, tilt, rotation, etc.

By emphasizing the peripheral content of a scene, the visual imaging system can use a single camera to capture the relevant visual information within a panoramic field of view existing along the horizon, while being able to conventionally store and easily display the scene, or portions thereof, in real-time. Using a single optical system and camera is not only cost-effective, but keeps all hemispheric visual data automatically time-synchronized.

In the present invention, at a conference table view point, with participants seated around a conference table, hemispheric scene content is ideally suited for segmented subviews of participants, especially when directionally electronically manipulated by voice actuation. The video image should be of the current speaker.

One advantage of the present invention is that the unique visual imaging system lens can capture information from a hemispheric scene by emphasizing the peripheral portion of the hemispheric field of view and thus provide greater resolution with existing imaging devices for the relevant visual information in the scene. As an example, if an ordinary fisheye lens focuses the lowest 15 degrees up from the horizon on ten percent of the imager at the imaging plane and the peripheral-enhancing lens focuses that same 15 degrees on fifty percent of the imager, there is a five-fold increase in resolution using the same imaging device. Depending on the application and exact formulation of the lens equations, there will be at least a five times increase in resolving power by this lens/imager combination.

The third subsystem of the present invention comprises a control apparatus such as a personal computer or other collection of electronic circuits, connected to the imagery system to allow flexible operation delivering options and defaults, including an override of the automated video image manipulation. A minimal control program is the software of the host controller to provide the options that may be necessary for individual teleconferences. An example would be to delay switching time segments between speakers, or perhaps the use of alternate cameras that may include a dual display.

In operation, at a particular teleconferencing site, participants will be arranged at a conference table or in a conference room with an array of microphones, each of which will pick up the normal speaking voice of each participant. The array of microphones is directly connected to an audio direction processor. The hemispheric lens system in conjunction with the video camera is attached to view warping logic as explained above and to the controller, or a personal computer. The video and audio signals are then transmitted through a transmission medium in an NTSC or other format to the remote teleconferencing site for remote display.

Sound from the participant speaking that is processed in the audio direction processor determines the direction of the participant speaking relative to the panoramic video camera and lens. Once the particular speaker direction is determined, the panoramic image of a specific hemispherical region of interest, such as the participant's face, is processed to provide a normal video aspect ratio view for the remote participants using the system.

It is a principal object and advantage of this invention to provide a video conferencing system that automatically directs a video image to the participant that is speaking while providing a hemispherical video imaging subview that can be electronically manipulated in the direction of the speaker selected from a panoramic scene.

It is another principal advantage of this invention to provide an automatic teleconferencing system that saves transmission time, reduces coincident cost by eliminating or reducing manual operation of a video camera, and does not detract from the concentration of the subject during the conference.

And yet another advantage of this invention is to provide an automatic video camera with electronic image manipulation for video conferencing equipment that has no moving mechanical parts or physical mechanisms which improves the reliability of the system and reduces maintenance costs and service costs.

In accordance with these and other objects which will become apparent hereinafter, the instant invention will now be described with particular reference to the accompanying drawings.

## BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic illustration of the visual imaging system organization and components of the parent application.

FIG. 1A is a schematic illustration of the automated video conferencing system organization and components.

FIGS. 2A, 2B, and 2C show a cross sectional diagram indicating the field input and output rays and the resulting relative field coverage a lens typically provides in the image plane for detection by an imager device.

FIGS. 3AA, 3 AB , and 3 AC show a cross sectional diagram indicating the field input and output rays and the resulting field coverage that optical system Example I, constructed according to the principles of the present invention, provides in the image plane for detection by an imaging device or substrate.

FIGS. 3BA, 3BB show a cross sectional diagram indicating the field input and output rays and the resulting field coverage that optical system Example II of this present invention provides in the image plane for detection by an imaging device or substrate.

FIG. 4 is a schematic representation of the mapping locations on the imaging device.

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FIG. 5 is a schematic block diagram of the panoramic transform processor subsystem for use with the teleconferencing system of the present invention.

FIGS. 6A and 6B are a schematic diagram showing how multiple transform processor subsystems can be tied into the same distorted image to provide multiple different view perspectives to different users from the same source image as described in the parent application.

## DESCRIPTION OF THE PREFERRED EMBODIMENTS

The invention will be defined initially with a brief description of the principles thereof.

## Principles of the Present Invention

As described in the parent U.S. patent application, the imaging invention stems from the realization by the inventors that in many of the technical hemispheric field applications, where the image detector is parallel to the plane of the horizon, much of the relevant visual information in the scene (e.g., trees, mountains, people, etc.) is found only in a small angle with respect to the horizon. Although the length of the arc from the horizon containing the relevant 25 information varies depending upon the particular application, the inventors have determined that in many situations, almost all the relevant visual information is contained within about 10 to 45 degrees with respect to the horizon. This determination is especially true with respect to the teleconference environment which is normally centered around a conference table or conference room.

To maximize data collection and resolution for analysis and/or display of the relevant visual information located in this portion of the hemispheric scene, it is desirable to maximize the dedication of the available image detection area to this peripheral field portion. To accommodate this, it is necessary that the "central" portion of the scene (from 45 to 90 degrees with respect to the horizon) cover only the remaining areas of the imager plane so as not to interfere with light from the periphery.

In many cases, since the "central" area contains less detailed information, such as a solid white ceiling or a clear or lightly clouded sky, it is allowable to maximize completely the dedication of the available image detection area to the peripheral field portion by reducing the portion of the imager device representing the "central" area to near zero. Of course, in certain instances, it is desirable to analyze this less detailed information, but this portion of the scene can be minimized to some extent without significant degradation of such visual information. As will be described herein in more detail, the present invention provides two manners (Example I and Example II) for capturing, storing, and selectively displaying the critical visual information in a scene for many important applications.

## System Organization and Components

Referring now to the drawings, and initially to FIG. 1, the visual imaging system of the parent invention includes a still image or moving picture camera 10, having a lens, indicated generally at 14, designed to capture and enhance the peripheral content of a hemispheric scene. The captured scene can be stored onto an assortment of media, e.g., photographic film 16, electronic storage 18, or other conventional storage means. Electronic storage 18 is preferred because of the ease of electronic manipulation thereof. Additionally, photographic film 16 requires an image scanner 20 or other
capture-and-conversion method to change the image into electronic format before electronic manipulation can be performed. A video camera 11 in FIG. 1 A is used for the teleconferencing system to capture the image.

The stored electronic image data is then selectively accessed by a transform processor engine 22 and can be electronically manipulated according to user-defined criteria, such as pan, up/down, zoom, etc. The transform processor 22 corrects the image for display on a conventional display device 28 such as a video monitor or a video projection display system in a normal viewer format or on head-mounted displays $\mathbf{3 0}$, in which integrated orientationsensing devices can be used to manipulate the user controls.

Referring to FIG. 1A, the audio directive component of the teleconferencing system for the present invention is comprised of four microphones spaced apart which would be arranged concentrically about the lens and camera on a conference room table so that all of the participants in the conference will have audio access to the microphones for transmission of sound. The primary purpose of the invention is to provide automated camera steering of the video camera 11 scenes based on which particular participant is currently speaking. Therefore, the audio energy from a particular participant speaking will be the basis for directing the video camera imaging as discussed below. The microphones 21, 23,25 , and 27 are connected to a speaker detection circuit 29. The audio generated signals from the microphones are transferred to a mixer and sampling circuit in audio direction processor 19. In one particular embodiment, each microphone input would be sampled to determine which has the largest amplitude of signals or which one has signals, to determine the specific direction for steering the video carmera. Once the audio detection circuits and sampling circuits have determined which microphone is the microphone being used by the current speaker, this signal information is conveyed to the audio direction processor 19 which is correlated between the location of a particular microphone in use and the video imaging system providing the segmented image discussed below. Thus, using the microphone array and audio circuitry, a signal can be arrived at from the audio direction processor to the imaging system to give relevance of which direction or which segment of the panoramic image should be selected as a function of the current participant speaking. Determining the direction of the source of acoustical waves from an array of sensors such as an array microphone is known. Audio speaker detection circuitry is disclosed in U.S. Pat. No. 5,206,721 cited above. Additional discussion on the broad concepts can be found in Array Signal Processing: Concepts and Techniques, authored by Don H. Johnson and Dan E. Dudgeon, chapter 4, Beamforming, published by PIR Prentice-Hall, 1993, and Multidimensional Digital Signal Processing, authored by Dan E. Dudgeon and Russell M. Mersereau, chapter 6, Processing Signals Carried by Propagating Waves, published by Prentice-Hall, Inc., 1984. In the present system, the number of participants can substantially exceed the number of microphones. The video imaging system, which will ultimately provide images of the participant speaking for the teleconferencing, then receives the audio direction processor signal as an input to select the specific imaging segment as described below.

## I Image Acquisition

A. Camera

As described in the parent application, the camera 10 for the visual imaging system is an optical device that is capable of receiving a focused image from a lens and transforming that image into an electronic signal or into hard copy storage
such as photographic film. Various types of cameras for wide-angle viewing are known to those in the art, such as 35 mm cameras, 8 mm cameras, NTSC, RS170, and HDTVtype cameras. The present invention is designed to be compatible with most commercially available twodimensional cameras, with scaling of the lens geometries. It also has the technological capability to be applied to threedimensional cameras. The camera can be mounted and supported in a conventional manner.

FIG. 1A shows a teleconferencing system in accordance with the present invention, including an NSTC video camera 11 using the capture lens 13 , view-warping logic 15, and PC or master controller 17, which receives input from four microphones 21, 23, 25, and 27 disposed apart around a central audio connector 29 , the output of which is connected to the audio direction processor 19. By detecting the differences in audio signal amplitude obtained from each microphone, the audio direction processor can determine the closest microphone to the current participant speaking. It is also possible, by normal audio beam steering techniques, to select points between microphones, such that the number of participants can far exceed the number of microphones. The video camera 11 lens viewing angle segment based as a panoramic view can then be electronically changed through the view-warping logic and the PC or master controller 17 to automatically shift the segmented scene content in the direction of the person speaking at the time. Note that the video camera 11 will be physically located in a central area, preferably in the center of the conference table, whereby a panoramic view of the participants at the conference table or in a conference room can be obtained so that the relative bearing from a central camera location to a particular participant can be established relative to the panoramic scene desired and the particular amount of scene content to accurately represent and provide the proper video aspect ratio of a particular speaker while that person is speaking.
B. Lens With Enhanced Peripheral Content

The fundamental principle behind the enhanced peripheral content lens is the selective magnification of the periphery and the focusing of more of that content on the imaging plane. This recognizes the current limitations of imaging devices and film with regard to resolution. As such, the more of the peripheral content that can be focused on the imaging plane surface, the more points of data that can be resolved with a given density of imaging device or material. Therefore, for this new class of selective magnification lenses, the surface area of the imaging plane reserved for peripheral content will be large relative to the central content and roughly similar for all lenses in this class, regardless of whether the lens is designed for $1-10$ degree peripheral emphasis or 1-45 degree peripheral emphasis. However, it should be noted that the lens with 1-10 degree emphasis will have much better resolution for the same objects than the lens with 1-45 degree emphasis.
The lens 13 in FIG. 1A for video camera 11 provides a collection of data for enhanced digital processing of the peripheral portion of a given field of view. The lens uniquely achieves this by filling the greater available area of an imager device with the peripheral areas rather than the central areas of the captured scene.

A periphery-enhancing optical system suitable for achieving the goals of the present invention can be configured in various ways to present an image of the field free of detrimental values of critical aberrations. Two examples or embodiments are preferred. Example I in FIGS. 3AA-3AC,m preferably is a multi-medium system comprising a wide-angle multi-element optical lens and a fiber optic
imager device. Example II preferably is a combination system comprised of multiple refractive optical elements, one of which is of gradient index material, hemispherical in shape. The inventors define that other configurations relying on binary optics could also be utilized to accomplish similar results.

The system of Example I is best suited for applications where the capture of the minimal information contained in the central area is irrelevant. A coordinated fiber bundle array, either rigid or flexible, carefully aligned and assembled by methods known to those skilled in the art, is used to capture a peripheral annulus of the wide field image provided by the multi-element wide field lens. (REF. Journal of the Optical Society of America, 1964; lens designs presented by Miyamota. Also see U.S. Pat. No. 4,256,373 by M. Horimoto for additional wide-field lenses.) The multielement wide field lens therefore, although covering the same field as standard wide field lenses, is required to provide a larger image of the entire field. This can be accomplished by those skilled in the art by scaling a standard lens to a larger focal length until the desired image size is reached. (REF. Chapter 5.4, "Scaling a Design" of Modern Lens Design, Warren J. Smith, McGraw-Hill inc., copyright 1992.)

The fibers, arranged in a specific mechanical manner, deliver the information in a geometrically annular shape from the peripheral image area to either the rectangular or circular shape of a specific imaging device. Specific configurations can be devised for desired peripheral coverage (up to 10 degrees through 45 degrees) and matched to required image detector plane geometry. (REF. Sect. 13, Fiber Optics, Handbook of Optics, McGraw-Hill Inc., 1978.) Referring to FIGS. 3AA-3AC for a desired angle $\theta$ (theta), a standard wide-field lens design is scaled in "f f ," the length of the square camera imaging device ( $2 r^{\prime}$ ) is met. In the "Camera/Imager Interface" portion of the figure, the equation for fiber bundle radius $r^{\prime}$ as related to the imager is:

$$
\text { Area at imager }=(\mathrm{pi}) r_{y}^{2} y^{\prime}-(\mathrm{pi}) r_{x}^{2}=(\mathrm{pi})\left(\mathrm{r}^{2}, y_{r}^{2} r_{x}^{2}\right)
$$

Imager length $=2 \mathrm{r}^{\prime}$, where $\mathrm{r}^{\prime}=$ square $\operatorname{mot}\left[\mathrm{r}^{2} y_{y^{\prime}}-\mathrm{r}_{x^{\prime}}\right.$ ]
A configuration in the form of Example $I$ achieves an image in which the peripheral portion ( $0-45$ degrees with respect to the horizon) of the field of view preferably encompasses between approximately $90 \%$ to $100 \%$ of the entire usable area of the imager device, rather than the $35 \%$ or less that is typical with commercially available wideangle, fish-eye, or other conventional lenses. A configuration in the form of Example II achieves an image in which the peripheral portion preferably encompasses between $50 \%$ to $70 \%$ of the usable area of the imaging device surface.

The system of Example III is best suited for applications where all information contained in the field of view is relevant, although to differing degrees. The combination system of Example $I$ relies on the principal use of a Bravais System where a hemispherical lens or a combination of lenslets magnify an object to an image, wherein the object and image lie in the same plane. In this case, the hemispherical lens is made of gradient index material such that points impinging the image plane incur different factors of magnification depending on what index of refraction and what portion of the hemispherical curve or lenslets they pass through. This concept is used in combination with a multielement refractive lens that is designed to capture a wide field of view and also compensate for the color aberration induced by insertion of the hemispherical lens. This color compensation can be designed by those skilled in the art by
using a computer optimization routine. (REF. Mercado et al. and U.S. Pat. No. 5,210,646 on "Color Corrected Optical Systems and Method of Selecting Optical Materials Thereof." Also see Chapter 9 of the Users Manual for "Three Color Optimization" using Kidger Optics Optical Design Program v.4.71, copyright Kidger Optics 1983-1989.) By use of the hemispherical gradient index unit with a wide field multi-element lens, the portion of the camera dedicated to the periphery is increased, thereby increasing the relative resolution of information detectable by the imaging device sensing elements. With the gradient index hemisphere, index values decrease from the center, such that:

$$
\mathrm{n}_{1}<\mathrm{n}_{2}<\mathrm{n}_{3}<\mathrm{n}_{4}
$$

The operation of the optical systems is schematically illustrated in FIGS. 2A-2C and 3BA-3BB. The arc $X$ represents the field of view of the "center" portion of the "peripheral" field. The areas $X$ ' and $Y$ ' represent the subtended peripheral angles of incidence. Arc $Z$ and area $Z^{\prime}$ represent areas outside the normal imaging range of the lens. (No actual demarcation lines would exist in actual use; this is merely for exemplary purposes.)

FIGS. 2A-2C represents a typical wide-angle type lens, while FIGS. 3BA-3BB represents a lens constructed according to the principles of the present invention. As should be apparent from comparing FIGS. 2A-2C and 3BA-3BB, a typical wide-angle type lens has a fairly significant portion of the imaging surface dedicated to the central field of the lens; while the lens constructed according to the present invention has a fairly significant portion of the imaging surface dedicated to the peripheral field, and consequently less of the surface dedicated to the central field.

The portion of the imaging surface used for the peripheral portion of the scene (as compared with the central portion of the scene) can vary depending upon the particular prescription of lens specified, which is selected to capture items of interest for a given application. For example, if the imaging system is used to capture a panorama of an outdoor scene, the relevant visual information may be contained within 10 degrees of the horizon. The lens of the present invention can thus be designed to enhance only the field of view within 10 degrees of the horizon. On the other hand, if the imaging system is being used to capture a room scene within a building, the relevant visual information may include objects on walls and thus be contained within about 45 degrees from the horizon. A peripheral enhancing lens can thus also be designed to enhance the field of view up to 45 degrees from the horizon. Of course, the enhanced portion of the field of view depends upon the needs of the particular application, with the enhanced portion preferably falling somewhere between these two extremes. In any case, the principles of the present invention can be applied to these types of situations with equal success, with any appropriate corrections being made with the image transform processors, as will be described herein in more detail.
As illustrated in FIGS. 3AA-3AC, a preferred form of the Example I form of optical system comprises a standard wide field lens and a coordinated fiber array. The focal length of the wide field lens is scaled in order to match the peripheral field of view desired. The coordinated fiber array consists of an annular input face that collects the image projected from the standard wide field lens. The fiber bundle array then redirects the information from the peripheral view to its output end by total internal reflection. Fibers capable of 3 micron accuracy, covering the area of the annual region, are coordinated into a rectangular or circular shape at their output, depending on the geometry of the corresponding
imaging device. The size of output is also matched to the camera imaging device used.

Of course, these system configurations and parameters are only exemplary in nature and other configurations and parameters of the present invention could be used to provide enhanced peripheral imaging capabilities, as should be apparent to those skilled in the art.
C. Imager Device

With the present invention, a video camera 11 receives the optical image from the lens and fiber optic array.

It should be apparent from the above discussion that when the imager device is used with a lens constructed according to the principles of the present invention, the imager device will collect more information along the horizon than it will from the central area of the hemispheric scene. With only a given limited resolution of either film emulsions or CCD pixel density, the lens focuses more useful information at the imaging plane. The peripheral portion of the scene will therefore have a higher relative resolution in the resultant transformed image than the central portion. Thus, the details of any objects along the horizon will be more highly accentuated. Further, any distortion (e.g., spherical aberration) that occurs in the peripheral region of the lens will be imaged onto a larger surface area and can thus be more easily and fully compensated for. Also, as imaging device resolution improvements are made over time, peripheral enhancing lenses and configurations will continue to yield improved visual renditions.

The image mapped onto the imager device can be described by a series of concentric circles, as schematically illustrated in FIG. 4. As an example, each circle on the imager device can be described by radii of arbitrary units, e.g., 2, 5, 9, 14, etc. The radii of the circles depends on the magnification of the different regions of the hemisphere, with the blocks in the outer circles having a greater area as the magnification of the peripheral region increases. In an arbitrarily selected illustration case, each concentric circle represents 18 degrees field of view from the horizontal plane, with the outer circumference of the outermost circle being level with the horizon. The inventors have determined that the arc subtending the two outer circles (i.e., 36 degrees from the horizon) contains the relevant information in many hemispheric scenes for many applications (although again, this value can be varied depending upon the particular application).

Calculating the total circular area of the entire image circle yields 1257 units squared. The are of the three inner circles is 254 units squared. Therefore, the two outer circles contain about $80 \%$ of the usable area on the imaging device. Note that the image blocks corresponding to the horizon are spread across more area on the imager device than those in the central area of the image. Thus, the image blocks of the imager device are dominated by objects along the horizon, and those are the area of interest. This correlates to greater resolution for the peripheral areas of the scene.

The panoramic image provided by the imager is ideally suited for teleconferencing. For example, with the image lens apparatus mounted in the center of a conference table, from the plane of the table, a hemispheric view is presented. If the participants of the conference are seated around the table and the microphone array located conveniently on the table, the important image information, i.e. the participants, are found with the imager along a 10 to 30 degree or 45 degree segment of the horizon, by far the bulk of the images of interest. Therefore, using the present invention with audio detection to determine the direction of the current speaker, the desired image segments can be electronically manipu-
lated between speakers automatically controlled by the direction of the current speaker's voice from the array disposed at or near the center of the conference table. Camera steering and image segment selection among participants speaking is undetectable by the participants, providing for minimal distractions and maximum concentration by the participants of the conference.

## II. Image Storage

The image received on the imager device is passed on to the system components for storage and/or transmission to a remote teleconferencing site. For photographic processes, a storage device might be film; while for electronic processes, the storage device might be electronic storage in the form of random access memories, a conventional diskette or hard file, or video recording tape. The entire display of the scene (along with any secondary documentation) can be stored as a single image on the storage device.
As should be apparent from the configuration of the imager device in FIG. 4, the image is stored or transmitted in a "warped" form. The warped image is caused not only by the wide-angle nature of the lens (i.e. the "keystoning" effect), but also by the enhanced peripheral field of view of the lens (i.e., magnification along the periphery). The underlying concept is that a partial slice of the scene can be reproduced with the proper aspect ratio for the human visual system (i.e., as a perspective corrected view).

Looking at FIG. 5, the stored image will be loaded into the source image buffer 40 if it has been stored in electronic form on the host system, an example of which would be a personal computer or controller. Alternatively, the image can be brought in for processing without going through storage for real-time teleconferencing transmission. As one option, an analog signal from a video camera 11 (FIG. 1A) can connect into an NTSC-to-digital converter 42. This converts the image from analog information into a digital bit map (i.e., into "pixels"). The source image is then loaded into the source image frame buffer 40. However, as indicated previously, any type of camera can be used to provide the electronic input to buffer 40. The buffer preferably operates with sufficient speed so that real-time viewing is possible. III. Image Retrieval/Display

Referring to FIG. 1A, the video camera 11 image can be selectively accessed and transformed for display at the source location or at a remote teleconference location. In order to recreate a proper display of the scene in two dimensions for perspective-correct viewing, processor logic in transform processor engine 22 is utilized (see FIG. 1). The transform processors may be made of collections of smallscale, medium-scale, large-scale, or very-large-scale integrated (VLSI) circuits, examples of which are image re-sampling sequencers, commercially available from Raytheon Semiconductors (formerly TRW LSI Products, Inc., LaJolla, Calif.), which are marketed under the mark/ designation TMC2301 and TMC2302.

In FIG. 5, the re-sampling sequencers control the address sequencing of the pixels in the source image buffer 40 through a multiply-accumulate unit 46, and from there into the warped image buffer 48. The sequencers control the filtering or remapping of two-dimensional images from a set of Cartesian coordinates ( $\mathrm{x}, \mathrm{y}$ ) as defined within each sector "unit" (A1, B1, etc.) onto a newly transformed set of coordinates ( $\mathrm{u}, \mathrm{v}$ ). The "fish-eye" type of transformations described in U.S. Pat. No. 5,185,667 are based on nonconstant second-order derivatives. A different set of secondorder derivatives employed for the transforms associated with the sequencers can also handle three-dimensional images by re-sampling them from a set of Cartesian coor-
dinates ( $\mathrm{x}, \mathrm{y}, \mathrm{z}$ ) into a new, transformed set ( $u, \mathrm{v}, \mathrm{w}$ ). Typically, these sequencers can support nearest-neighbor, bilinear interpolation or convolution re-sampling, and can operate at speeds allowing real-time operation. Alternate electronic solutions can be constructed using VLSI or applicationspecific integrated circuits.
Re-mapped pixel locations (i.e., interpolation "kernels") of more than one pixel in the bit map requires an external interpolation coefficient look-up table 50 and the multiply/ accumulate unit 46 as shown in FIG. 5. A table "walk" is typically performed on each source pixel, thus providing a smoother image by summing the products of the original lens image data with the appropriate interpolation coefficients. By capturing the hemispheric lens image data into source image buffer 40 , the warp engine can be programmed to perform a perspective correction, much like an inverse keystoning effect. The re-mapping of the pixel locations is matched to the differential magnification of the particular periphery-enhancing lens used.

Direct access to the interpolation coefficient look-up table 50 and to the transformation parameters is also often desirable to allow dynamic modification of the interpolation algorithm. Thus, a local interpolation coefficient buffer 52 to update the varying transform parameters is included to allow for real-time still and motion image transformations.

The row and column warping engines $58 a, 58 b$ of the transform processor 22 supply addresses to the source image buffer 40. The addresses are determined by the interpolation algorithm chosen. The multiply-accumulate unit 46 takes the pixels supplied by the source image buffer 40 under warping engine control and multiplies the pixels together using combinational logic with weighting factors dependent on the algorithm. Compensation for aberration (e.g., spherical aberration) can also be made at this point. Finally, the composed interpolated pixels are sent to the warped image buffer 48. The address location within the warped image buffer is again determined by the warping. The algorithm parameters from lookup table 50 are input to the registers of the row and column warping engines $58 a, 58 b$, as well as into the interpolation coefficient buffer 52.

The memory controller/clock circuitry 62 provides refresh control to the source and warped image buffers 40 , 48. In addition, all clock sources are synchronized through this circuitry. The bus interface and control circuitry 56 also provide an interface to the host system bus (i.e., for MCA, ISA, etc.) and the re-mapping circuitry. This interface logic serves to load control information into the re-mapping circuitry and to provide a path to transport warped images to the system display buffer (not shown; part of host system), or store images to disk via the system bus prior to warping. An optional random access memory digital-to-analog converter (RAMDAC) 66 provides support for a local display connection if desired.

One feature of the transform processors is the valid source address flag within the transform processor engine. This allows the user to construct abutting sub-images in the ( $\mathrm{x}, \mathrm{y}$ ) plane without danger of edge interference. Thus, edge detection of the unused areas outside the circular image of FIG. 4 can alert the system to ignore these values.

The image capture function can also be accomplished with motion video devices. All types of image data are input to the source image buffer 40 for processing as desired. The NTSC digitizer 42, for example, can provide real-time data from an NTSC video camera 11 used for teleconferencing. Any similar device that converts an image to the appropriate digital format for input to the source image buffer can be employed as optional element 42 in FIG. 5. Prerecorded
distorted images generated through this invention's optical system can also be input through optional conversion block 42 to allow dynamic manipulation of previously recorded image data.

The image transformation performed on the captured digitized image from modified hemispheric coordinates to planar coordinates for display is one of a multitude of possible image transformations, any of which can be invoked in real-time for smooth merging of effects. These transformations include, but are not limited to pans, up/downs, zooms, tiles, rotations, scaling, cropping, and image shear, which can be controlled using human or computer input. Image filtering can be performed as well as edge detection in associated processes during the course of manipulation. These services can be applied to any system image loaded into the source image buffer, thus providing a host of added features beyond the simple application of the hemispheric lens and display system.

The advantage of the image transformation logic becomes apparent when describing particular applications. A security camera application can be implemented to view an entire panorama such that the security monitor will display fullmotion rate images in real-time. Source image coordinates for still images can also be sequenced, allowing perceived animation or full-motion renditions by simply reloading new source image coordinates into the wapping engines as frames are drawn from memory. Details from other stored images can be utilized to give the effect of full motion panning of the horizon within the captured image by the lens.
Finally, the transform processor subsystem can produce multiple different outputs simultaneously from individual stored or currently converted images. Referring to FIGS. 6A and 6B, with the main transform processor circuits collected into a simplified single block as shown in the lower drawing, multiple outputs are generated from a single image source, either motion or still, with individual effects for each scene as desired, allowing several scenes on different display devices or several windows on a single display. This is accomplished by incorporating several image processing subsystems within one overall system.

In all cases, by having greater resolution of the peripheral image of a scene, the details of any objects along the horizon will be enhanced. Further, aberrations occurring around the periphery of the lens (i.e., spherical aberrations) can be more fully and completely compensated for, as the aberrations are spread across a greater area on the imager device.
As described above, the present invention provides a visual imaging system that efficiently captures, stores, and displays visual information about an enhanced hemispheric field of view existing particularly along the horizon, and that allows electronic manipulation and selective display thereof even after acquisition and storage, while minimizing distortion. The present invention provides an automatic, audio directed video camera steering of segmented images selected from a hemispherical view ideally suited for teleconferencing.
The principles, embodiments, and modes of operation of the present invention have been described in the foregoing specification. The invention that is intended to be protected herein should not, however, be construed to the particular form described as it is to be regarded as illustrative rather than restrictive. Variations and changes may be made by those skilled in the art without department from the spirit of the present invention. Accordingly, the foregoing detailed description should be exemplary in nature and not limiting as to the scope and spirit of the invention as set forth in the appended claims.

What is claimed is:

1. An automatic audio controlled video camera steering system for electronic imaging and manipulation of a hemispheric field of view, comprising:
at least two microphones;
audio detection circuitry connected to said microphones for determining which of said microphones is receiving audio energy;
means for generating a signal representing the direction of the received audio energy based on signals from the microphones;
a video camera for receiving optical images of the field of view and for producing video image output signals;
an optical system associated with said video camera for producing the optical images from a hemispheric field of view for optical conveyance to said video camera, said optical system having a configuration that emphasizes the peripheral content of the panoramic field of view (when the central lens axis is oriented vertically) as compared to the central content of a hemispheric field of view, this being accomplished through differential magnification;
an imager device associated with said camera for receiving the optical images from said lens and for providing digitized output signals;
input image memory for receiving the digitized output signals from said imager device and for storing the digitized output signals;
an image transform processor or set of circuits for selectively accessing and processing the digitized output signals from said input image memory according to user defined criteria;
output image memory for receiving the processed signals from the image transform processor, and
means connected to said output image memory from said hemispheric field of yiew for selecting a particular segmentized image from the hemispheric field of view representative of the direction from the camera of the microphone array determined to be receiving sound wave energy;
an output display connected to said output image memory for displaying the signals in said output image memory according to the user defined criteria.
2. The system as in claim 1, wherein said optical system has a configuration that images the peripheral portion of the hemispheric scene onto at least $50 \%-90 \%$ of the usable surface area of the imaging device, when used in an electronic image capture apparatus.
3. The system as in claim 2 , wherein said optical system includes a color aberrated wide field lens and a gradient index hemispheric lens.
4. The system as in claim 2 , wherein said optical system has a configuration which emphasizes the field of view from 1 to 45 degrees up from the horizon in a hemispherical captured image, the lens representing one of many configurations that may selectively emphasize some subset of the aforesaid 1 to 45 degrees covered.
5. The system as in claim 4, wherein said optical system 60 includes a wide field multi-element lens and a coordinated fiber array geometrically fabricated with an annular input end and a rectangular output end.
6. The system as in claim 4, wherein said optical system includes a wide field multi-element lens and a coordinated fiber array geometrically fabricated with an annular input end and a circular output end.
7. A teleconferencing system for electronic manipulation of a hemispheric scene, comprising:
a plurality of microphones;
means connected to the output of said microphones for determining the amplitude levels of audio signals from the microphones;
means for detecting and comparing the audio signals from said microphones to determine the direction of a particular speaker;
means for providing an output signal representing the direction of a speaker at a given time;
a camera imaging system for receiving optical images of the field of view and for producing output video signals corresponding to the optical images;
an optical system associated with said camera imaging system for producing the optical images from a field of view for optical conveyance to said camera imaging system;
an imager device associated with said camera for receiving the optical images from said lens and for providing digitized output signals;
input image memory for receiving the digitized output signals from said imaging device and for storing the digitized output signals;
an image transform processor for selectively accessing and processing the digitized output signals from said input image memory according to user-defined criteria;
means connected to said image transform proces sor from said microphone direction means to provide the image segment of a hemispheric scene to be selected representing the direction of the speaker based on the audio signals from that array of microphones;
output image memory for receiving the processed signals from the image transform processor means;
an output display device connected to said output image memory for displaying the signals in said output image memory according to user-defined criteria;
wherein the improvement comprises said optical systems having a configuration that emphasizes the peripheral content of field of view of a hemispheric scene as compared to the central content, such that said imager device receives magnified optical images of the peripheral portion of the hemispheric field of view.
8. A teleconferencing method for electronically capturing, storing, and manipulating a hemispheric field of view, having a plurality of individual human speakers, comprising the steps of:
providing a plurality of microphones connected to a microphone audio detection circuit that can provide an output signal that determines which microphone is in use at a given point in time, indicative of the direction of the human speaker;
providing an optical system having a configuration that enhances the peripheral portion of the field of view in the direction of the human speaker;
capturing the hemispheric field of view with the periphery-enhancing optical system and imaging the field of view onto an imager device by enhancing the peripheral field of view;
storing the captured image as a single image;
selectively accessing a portion of the stored image according to user-defined criteria;
transforming the stored image so that the stored image can be displayed as a perspective-correct image;
selecting from a portion of the field of view a specific image segment representative of the direction of the speaker;
displaying the perspective-correct image in a user-defined format.
9. The method as in claim 8, wherein said transforming step comprises manipulating the peripheral-enhanced image into a perspective-correct image.
10. The method as in claim 8, wherein said peripheryenhancing optical system selectively magnifies visual content within an arc of between 10 and 45 degrees up from the horizon in a hemispheric field of view onto the imager device.
11. The method as in claim 8, wherein the storage step comprises storing the captured image in electronic storage.
12. A method for electronically manipulating a hemispheric scene having an enhanced peripheral field of view stored as an image on a video camera, comprising the steps of:
providing a plurality of microphones connected to an audio detection circuit that determines the direction of a given speaker;
converting the image on a video camera into electronic output signals;
selectively accessing a portion of the output signals according to user-defined criteria;
transforming the accessed portion of the output signals by manipulating the peripheral-enhanced field of view so that the stored image can be displayed as a perspectivecorrect image in a direction based on audio signals from said audio detection circuit;
selecting a particular image segment as a function of speaker direction for display;
displaying the perspective-correct image in the userdefined format.
13. A videoconferencing imaging system having automatic camera steering comprising:
plurality of microphones disposed in a common plane strategically positioned relative to each other and relative to conference participants to be captured on video for remote video and audio transmission of each participant's image and spoken word;
microphone output circuit connected to each of said microphones;
audio detection processor having an input connected to said microphone output circuit;
conference platform for arranging participants in individual locations about said conference platform;
video camera including a hemispheric lens mounted strategically in a predetermined location on said confer-
ence platform capable of presenting a hemispheric view to said video camera from said platform;
video image view warping logic circuit connected to the output of said video camera and said output of said audio direction processor, said video image view warping logic circuit having a video output of specific regions of interest based on said hemispheric lens image and having an audio output;
a computer processor or other controller circuits having input connected to said view warping logic circuit for controlling the desired specific region of interest as a function of audio directed processor input related to the participant speaking to create a normal aspect ratio view based on the participants using the system; and
video and audio transmission medium connected to the output of said view warping logic circuit for transmitting said audio and video signals to said remote video conference.
14. A videoconferencing image system having automatic camera steering as in claim 13, including:
said video image view warping logic circuit including a source image buffer connected to the input from the video camera lens;
a row (X) warp engine having an output connected to said source image buffer;
column ( $Y$ ) warp engine, said row warp engine and said column warp engine connected to panoramic image transformation parameter look up table and said computer control output;
interpolation coefficient buffer connected to the output of said row (X) warp engine and said column (Y) warp engine;
multiply accumulation unit connected to the output of said source image buffer and said interpolation coefficient buffer for receiving coefficient data;
memory control device connected to the output of said panoramic image transformation parameter look up table and said computer controller;
warped image buffer connected to the output of said column ( $Y$ ) warp engine and said memory control and having a warp data output connected to said transmission medium whereby the selection of a normal aspect ratio view containing specific regions of interest selected by the determination of the participant speaking is based on the participant's direction, as determined by the audio direction processor.

## EXHIBIT 2

United States Patent
[19]
Nagaoka
[11] Patent Number:
6,128,145
Date of Patent:

IMAGE PICK-UP DEVICE, IMAGE DISPLAY DEVICE AND INFORMATION RECORDING MEDIUM COMPRISING A FISHEYE LENS

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[21] Appl. No.: 09/300,972
[22] Filed: Apr. 28, 1999
[30] Foreign Application Priority Data
Nov. 25, 1998 [JP] Japan $\qquad$ 10-350751
[51] Int. Cl. ${ }^{7}$ $\qquad$ G02B 13/04
[52]
U.S. Cl. $\qquad$ 359/749; 359/672
[58]
] Field of Search $\qquad$ 359/749, 750-753, 359/680-682, 672-675

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## ABSTRACT

An image is picked up by a camera comprising a fisheye lens having a relationship of $h=n \cdot f \cdot \tan (\theta / m)$, wherein $h$ is the height of an image of a subject at a certain point, $f$ is the focal distance of the fisheye lens, $\theta$ is a field angle, $m$ has a value of $1.6 \leqq m \leqq 3$, and $n$ has a value of $m-0.4 \leqq n \leqq m+0.4$, and the image data of which is output from the camera, is converted into a plane image by an image data processing unit, and this converted image is then output to a monitor unit. Preferably, $n$ and $m$ both equal 2.

14 Claims, 9 Drawing Sheets



FIG. 1


FIG.3A
FIELD ANGLE $\theta\left({ }^{\circ}\right)$


FIG.3B


FIG.4A


FIG.4B


FIG.4C


FIG.4D

FIG. 5


FIG. 6


FIG. 7
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FIG.8A


FIG.9A

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FIG. 8 B


FIG.9B


FIG. 10

## IMAGE PICK-UP DEVICE, IMAGE DISPLAY DEVICE AND INFORMATION RECORDING MEDIUM COMPRISING A FISHEYE LENS

## BACKGROUND OF THE INVENTION

The present invention relates to an image pick-up device comprising a fisheye lens, an image display device and an information recording medium, all of which can obtain a high-quality converted image when an image picked up by the fisheye lens is converted into a plane image.

A monitoring system using a camera which enables product examination at a plant or construction work at a construction site to be monitored from a remote place has recently been developed. In this monitoring system, depending on what is monitored, capability of monitoring a wide range at a limited number of cameras is desired. To realize this, the development of a monitoring system comprising a fisheye lens which can pick up an image of all the directions of the field of view around the optical axis at a field angle of at least $90^{\circ}$ in each direction with respect to the optical axis is under way.

Use of this fisheye lens makes it possible to obtain an image of all the space with a single camera. That is, the space is regarded as a single sphere, a camera is installed at the center of the sphere, an image of half of the sphere is picked up by the fisheye lens, the camera is turned at an angle of $180^{\circ}$ from that position, an image of the other half of the sphere in the opposite direction is picked up, and the two images are combined together to obtain an image of all the directions of the field of view in the space of $360^{\circ}$, that is, the sphere. This image is converted into a plane image.

As the monitoring system comprising a fisheye lens of the prior art, there is a system disclosed by Japanese Patent Application Laid-open No. Hei6-501585 (to be referred to as "prior art" hereinafter), for example. Although this prior art makes it possible to pick up an image of all the directions of the field of view, the lens used in the prior art is a fisheye lens having a relationship of $h=f \cdot \theta$ (wherein $h$ is the height of an image of a subject at a certain point obtained by the fisheye lens, $f$ is the focal distance of the fisheye lens and $\theta$ is a field angle). This is obvious from the fact that Nikon's $8-\mathrm{mm} \mathrm{f} / 2.8$ lens is used as the fisheye lens in the above Japanese Patent Application Laid-open No. Hei6-501585. Conventional fisheye lenses generally have a relationship of $\mathrm{h}=\mathrm{f} \cdot \theta$ and Nikon's $8-\mathrm{mm} \mathrm{f} / 2.8$ fisheye lens has the above relationship of $h=f \cdot \theta$.

The method of picking up an image by a fisheye lens having this relationship of $\mathrm{h}=\mathrm{f} \cdot \theta$ and converting the image into a plane image is called "equidistant projection". Since an image picked up by a fisheye lens having the above characteristics has a small volume of image data on its peripheral portion (field angle of around $90^{\circ}$ with respect to the optical axis of the fisheye lens), when the image is converted into a plane image, there are many missing portions of image data on the peripheral portion of the image and the missing portions must be interpolated. In addition, the image picked up by the fisheye lens having the above characteristics involves such a problem that the peripheral portion of the image is distorted.

An object of the present invention is to provide an image pick-up device comprising a fisheye lens, an image display device and an information recording medium, which minimize missing portions of image data by extracting a large volume of image data at a field angle of around $90^{\circ}$ with respect to the optical axis of the fisheye lens to reduce interpolating of the missing portions and can obtain a natural
plane image when images of all the directions of the field of view around the optical axis are picked up at a field angle of at least $90^{\circ}$ with respect to the optical axis and are converted into plane images.

Various other objects, advantages and features of the present invention will become readily apparent to those of ordinary skill in the art, and the novel features will be particularly pointed out in the appended claims.

## SUMMARY OF THE INVENTION

To attain the above object, according to a first aspect of the present invention, there is provided an image pick-up device comprising a fisheye lens for picking up an image of all the directions of the field of view around the optical axis of the fisheye lens at a field angle of at least $90^{\circ}$ in each direction with respect to the optical axis, wherein the fisheye lens has a relationship of $h=n f \cdot \tan (\theta / \mathrm{m})$ (wherein $h$ is the height of an image of a subject at a certain point obtained by the fisheye lens, $f$ is the focal distance of the fisheye lens, $1.6 \leqq \mathrm{~m} \leqq 3, \mathrm{~m}-0.4 \leqq \mathrm{n} \leqq \mathrm{m}+0.4$, and $\theta$ is a field angle).

According to a second aspect of the present invention, the fisheye lens is constructed by a master lens provided on an existing image pick-up device and by an attachment lens to be attached to the master lens.

Further, according to a third aspect of the present invention, there is provided an image display device comprising an image data processing unit for converting an image obtained by the image pick-up device of the first or second aspect of the present invention into a plane image and a display unit for displaying the converted plane image.

According to a fourth aspect of the present invention, there is provided an information recording medium that records a program having at least the step of converting an image obtained by a fisheye lens having a relationship of $\mathrm{h}=\mathrm{nf} \cdot \tan (\theta / \mathrm{m}$ ) (wherein h is the height of an image of a subject at a certain point, f is the focal distance of the fisheye lens, $\theta$ is a field angle, $1.6 \leqq m<3$. and $\mathrm{m}-0.4 \leqq \mathrm{n} \leqq \mathrm{m}+0.4$ ) into a plane image, the step of displaying a predetermined portion of the converted plane image on a display unit and the step of changing continuously the predetermined portion with instruction means.

One of the fisheye lens used in the present invention has the relationship of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 2)$. Compared with an ordinary fisheye lens having a relationship of $\mathrm{h}=\mathrm{f} \cdot \theta$, an image at a peripheral portion (field angle of around $90^{\circ}$ with respect to the optical axis of the fisheye lens) is enlarged and missing portions of image data on the peripheral portion can be minimized with the fisheye lens in accordance with the present invention. With this, when a picked-up image is to be converted into a plane image, the interpolating of image data can be reduced, thereby making it possible to obtain a more natural plane image.

The fisheye lens according to the present invention may be constructed by attaching an attachment lens to a master lens provided on an existing camera so that the fisheye lens can be attached to almost all the existing cameras. In addition, only the attachment lens is newly produced, thereby making it possible to reduce costs.

Further, the image display device for displaying a plane image converted from an image picked up by the image pick-up device having the above fisheye lens on a display unit makes the displayed image easy to be seen, thereby improving the value of the device. When the information recording medium recording the above steps is read by a computer and the program is executed, a more natural plane image can be displayed on the display unit and the displayed
portion can be freely shifted within the range of the image picked up by the image pick-up device.

## BRIEF DESCRIPTION OF THE DRAWINGS

The following detailed description, given by way of example and not intended to limit the present invention solely thereto, will best be appreciated in conjunction with the accompanying drawings, wherein like reference numerals denote like elements and parts, in which:

FIG. 1 is a schematic structural diagram of an image processing system using an image pick-up device comprising a fisheye lens according to the present invention;

FIG. 2 are a structural diagram of the fisheye lens shown in FIG. 1 and a corresponding diagram schematically showing lens intervals (lens intervals and lens thicknesses);

FIG. 3(A) is a diagram showing the relationship between field angle $\theta$ and image height $h$ with respect to fisheye lenses having relationships of $\mathrm{h}=\mathrm{f} \cdot \theta, \mathrm{h}=2 \mathrm{f} \cdot \sin (\theta / 2), \mathrm{h}=\mathrm{f} \cdot \sin$ $\theta, \mathrm{h}=\mathrm{f} \cdot \tan \theta, \mathrm{h}=3 \mathrm{f} \cdot \tan (\theta / 3), \mathrm{h}=2 \mathrm{f} \cdot(\tan \theta / 1.6)$ and one of the fisheye lenses of the present invention having a relationship of $h=2 f \cdot \tan (\theta / 2)$;

FIG. 3(B) is a diagram showing the relationship between field angle $\theta$ and image height $h$ with respect to fisheye lenses having relationships of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 1.6), \mathrm{h}=2.4 \mathrm{f} \cdot \tan (\theta /$ 2), $\mathrm{h}=3.4 \mathrm{f} \cdot \tan (\theta / 3), \mathrm{h}=1.2 \mathrm{f} \cdot \tan (\theta / 1.6), \mathrm{h}=1.6 \mathrm{f} \cdot \tan (\theta / 2)$ and $\mathrm{h}=\mathrm{f} \cdot \theta$.

FIGS. 4(A) to 4(D) are views illustrating, in concentric circles each centering around the optical axis of each fisheye lens shown in FIG. 3, changes of image heights when the field angle is changed in $10^{\circ}$ with respect to the optical axis of each fisheye lens;

FIG. 5 is a diagram for explaining a method of polarcoordinate converting a hemispherical image obtained by a fisheye lens;

FIG. 6 is a diagram for explaining a method of obtaining the position of an image formation point on the surface of CCD image pick-up elements in the polar coordinate conversion of FIG. 5;

FIG. 7 is a flow chart for explaining the steps of processing an image using the image processing system of FIG. 1;

FIGS. 8(A) and 8(B) are diagrams showing another application example of the image pick-up device of the present invention, wherein FIG. 8(A) is a schematic diagram showing the side thereof and FIG. 8(B) is a diagram when seen from a direction indicated by an arrow B in FIG. 8(A);

FIGS. 9 (A) and 9 (B) are diagrams showing still another application example of the image pick-up device of the present invention, wherein FIG. 9(A) is a schematic diagram showing the side thereof and FIG. $9(B)$ is a diagram when seen from a direction indicated by an arrow B in FIG. 9(A); and

FIG. 10 is a diagram showing another example of an image processing system utilizing the image pick-up device comprising a fisheye lens of the present invention.

## DETAILED DESCRIPTION OF CERTAIN PREFERRED EMBODIMENTS

Preferred embodiments of the present invention will be described hereinafter with reference to FIGS. 1 to $\mathbf{1 0}$.

FIG. 1 schematically shows an image processing system utilizing an image pick-up device comprising a fisheye lens of the present invention. This image processing system comprises a camera (such as a video camera) 2 that is an image pick-up device equipped with a fisheye lens 1 , an
image data processing unit $\mathbf{3}$ for processing image data from the camera 2 , and a monitor unit 4 for displaying an image processed by the image data processing unit 3 . The image data processing unit $\mathbf{3}$ has a CPU, memory means and the like and performs various processing using image data output from the camera 2. In the case of the present invention, the image data processing unit 3 also converts an image picked up by the fisheye lens 1 into a plane image.

As shown in FIG. 2, the fisheye lens 1 used in this embodiment roughly consists of a lens unit (called master lens unit) $\mathbf{1 0}$ provided on the camera $\mathbf{2}$ and a lens unit (called attachment lens unit) 20 that can be attached to and detached from the master lens unit $\mathbf{1 0}$. The fisheye lens 1 of the present invention functions as a fisheye lens when the attachment lens unit $\mathbf{2 0}$ is attached to the master lens unit $\mathbf{1 0}$.
The attachment lens unit $\mathbf{2 0}$ consists of a first lens 21, a second lens 22, a third lens 23, a fourth lens 24 and a plate 25. The master lens unit 10 consists of a fifth lens 11, a sixth lens 12, a seventh lens 13, an eighth lens $\mathbf{1 4}$, a ninth lens 15 and a diaphragm 26 interposed between the sixth lens 12 and the seventh lens 13 .

The curvature R (diameter of the curved surface of the lens) of each lens and interval $D$ (lens thickness or lens interval) in this embodiment are as follows. That is, beginning with the curvature R1 of the left curved surface of the first lens 21 on the leftmost side of FIG. 2, in turn, the curvatures R1 and R2 of the first lens 21 are 40.0 mm and 9.0 mm , the curvatures R3 and R4 of the second lens 22 are -26.0 mm and 80.0 mm , the curvatures R5 and R6 of the third lens 23 are -36.0 mm and $\mathbf{- 2 0 . 0} \mathrm{mm}$, and the curvatures R7 and R8 of the fourth lens 24 are -81.0 mm and -27.0 mm , respectively.

Further, the curvatures R9 and R10 of the fifth lens 11 are 14.0 mm and 68.0 mm , the curvatures R11 and R12 of the sixth lens 12 are 9.0 mm and 3.0 mm , the curvatures R13 and R14 of the seventh lens 13 are 0.0 mm and -8.0 mm , the curvatures R15 and R16 of the eighth lens 14 are 10.0 mm and -6.0 mm , and the curvatures R17 and R18 of the ninth

Meanwhile, the thickness D1 of the first lens 21 on the leftmost side of FIG. 2 is 1.2 mm , the interval D $\mathbf{2}$ between the first lens 21 and the second lens 22 is 10.00 mm , and the thickness D3 of the second lens 22 is 1.2 mm . The interval D4 between the second lens 22 and the third lens 23 is 14.0 mm , the thickness D5 of the third lens 23 is 2.0 mm , the interval D6 between the third lens 23 and the fourth lens 24 is 3.0 mm , and the thickness D7 of the fourth lens 24 is 5.0 mm .
Further, the interval D8 between the fourth lens 24 and the fifth lens $\mathbf{1 1}$ is 7.0 mm , the thickness $\mathbf{D 9}$ of the fifth lens $\mathbf{1 1}$ is 2.0 mm , the interval D10 between the fifth lens $\mathbf{1 1}$ and the sixth lens 12 is 0.3 mm , and the thickness D11 of the sixth lens $\mathbf{1 2}$ is 0.8 mm The seventh lens 13, the eighth lens 14 and the ninth lens 15 can be moved in the direction of the optical axis to change magnification, and the intervals between adjacent lenses to be described hereinafter are maximum values thereof. The interval D12 between the diaphragm 26 and the seventh lens 13 is 4.0 mm , the thickness D13 of the seventh lens 13 is 1.0 mm , the interval D14 of the seventh lens 13 and the eighth lens 14 is 1.0 mm , and the thickness D15 of the eighth lens 14 is 4.0 mm .

The interval D16 between the eighth lens 14 and the ninth lens 15 is 2.0 mm , and the thickness D17 of the ninth lens is 4.0 mm . Parallel plates $\mathbf{1 6}$ and 17 are arranged on the right side in FIG. 2 of the ninth lens 15.
In this arrangement, light incident upon the first lens 21 passes through the first to fourth lenses 21 to 24 , further
through the fifth to ninth lenses $\mathbf{1 1}$ to $\mathbf{1 5}$ and is input into CCD image pick-up elements $\mathbf{3 0}$ in the camera 2 . In this attachment lens unit 20, parallel rays input into the first lens 21 are output from the fourth lens 24 as parallel rays. Therefore, this attachment lens unit 20 can be attached to almost all the cameras. The width of the parallel pencil of rays output from the fourth lens 24 of the attachment lens unit 20 (shown by " $w$ " in the figure) is set to $1 / 2$ or less the effective diameter of the master lens 10 of the camera to which the attachment lens unit 20 is attached. In FIG. 2, the spherical surface 40 at the front of the first lens 21 represents a virtual subject surface of the picked up image.

As described above, the present invention is characterized in that a desired fisheye lens $\mathbf{1}$ constructed by the master lens unit 10 and the attachment lens unit $\mathbf{2 0}$ and has a relationship of $h=2 f \cdot \tan (\theta / 2)$ (where in $h$ is the height of an image of a subject at a certain position, $f$ is the focal distance of the fisheye lens and $\theta$ is a field angle). It is noted that although the preferred embodiment of the present invention has the above-indicated relationship, the present invention also embodies fisheye lenses having the relationship of $h=n \cdot f \cdot t a n$ $(\theta / \mathrm{m})$, where m has the value of $1.6 \leqq m \leqq 3$, and n has the value of $\mathrm{m}-0.4 \leqq \mathrm{n} \leqq \mathrm{m}+0.4$. Also, the present invention contemplates such a relationship when m equals $n$. Also, the relationship $\mathrm{h}=1.2 \mathrm{f} \cdot \tan (\theta / \mathrm{m}), \mathrm{m} \geqq 1.6$ also is embodied by the present invention. However, for purposes of discussion herein, $m$ and $n$ both equal to 2 .

The fisheye lens that has been generally used in the prior art has a relationship of $h=f \cdot \theta$ as described above. These functions are used to map a spherical image as a polarcoordinate converted image. The relationship, other than that, may be $\mathrm{h}=2 \mathrm{f} \cdot \sin (\theta / 2), \mathrm{h}=2 \mathrm{f}=\cdot \sin \theta$ or $\mathrm{h}=\mathrm{f} \cdot \tan \theta$.

FIG. 3(A) is a diagram showing relationships between field angle $\theta$ and image height $h$ when fisheye lenses having relationships of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 2), \mathrm{h}=\mathrm{f} \cdot \theta, \mathrm{h}=\mathrm{f} \cdot \sin (\theta / 2), \mathrm{h}=\mathrm{f} \cdot \sin \theta$ and $h=f \cdot \tan \theta$, etc. are used. Here, $\theta=90^{\circ}$ shows a field angle with respect to the optical axis (the field angle of the optical axis is $0^{\circ}$ ).

In FIG. 3(A), a curve C1 shows the relationship between field angle $\theta$ and image height $h$ when the fisheye lens of the present invention having the relationship of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 2)$ is used, and a curve C2 shows the relationship between field angle $\theta$ and image height $h$ when a fisheye lens having the relationship of $\mathrm{h}=\mathrm{f} \cdot \theta$ is used. A curve C3 shows the relationship between field angle $\theta$ and image height $h$ when a fisheye lens having the relationship of $\mathrm{h}=2 \mathrm{f} \cdot \sin (\theta / 2)$ is used, a curve C 4 shows the relationship between field angle $\theta$ and image height $h$ when a fisheye lens having the relationship of $\mathrm{h}=2 \mathrm{f} \cdot \sin \theta$ is used, and a curve C5 shows the relationship between field angle $\theta$ and image height $h$ when a fisheye lens having the relationship of $h=f \cdot \tan \theta$ is used. A curve C1' shows the relationship of $h=3 f \cdot \tan (\theta / 3)$ and a curve $C^{\prime \prime}$ shows the relationship of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 1.6)$.

FIG. 3(B), is a diagram showing the relationship between field angle $\theta$ and image height when fisheye lenses having relationships of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 1.6), \mathrm{h}=2.4 \mathrm{f} \cdot \tan (\theta / 2), \mathrm{h}=3.4 \mathrm{f} \cdot \tan$ $(\theta / 3), \mathrm{h}=1.2 \mathrm{f} \cdot \tan (\theta / 1.6), \mathrm{h}=1.6 \mathrm{f} \cdot \tan (\theta / 2)$ and $\mathrm{h}=\mathrm{f} \cdot \theta$. All of these fisheye lenses, except $h=f \cdot \theta$, are embodied by the present invention.

As is evident from FIG. 3, an increase in image height $h$ at a field angle $\theta$ of about $90^{\circ}$ is largest when the fisheye lens having the relationship of $\mathbf{h}=\mathbf{f} \cdot \tan \theta$ is used and is second largest when the fisheye lens having the relationship of $h=2 f \cdot \tan (\theta / 2)$ is used. Changes in image height $h$ with respect to changes in field angle $\theta$ become linear when the fisheye lens having the relationship of $h=f \cdot \theta$ is used and
further an increase in image height $h$ tends to be smaller as the field angle becomes closer to $90^{\circ}$ when the fisheye lenses having the relationships of $\mathrm{h}=2 \mathrm{f} \cdot \sin (\theta / 2)$ and $\mathrm{h}=\mathrm{f} \cdot \sin \theta$ are used.

An increase in image height becomes larger toward the peripheral portion (field angle of $90^{\circ}$ ) when the fisheye lens having the relationship of $\mathrm{h}=\mathrm{f} \cdot \tan \theta$ is used and more image data can be obtained. However, at a field angle $\theta$ of $90^{\circ}$, tan $\theta$ becomes infinite. Since the fisheye lens is required to obtain an image of all the directions of the field of view around the optical axis at a field angle of at least $90^{\circ}$ with respect to the optical axis, it can be said that the fisheye lens having the relationship of $h=f \cdot \tan \theta$ is not suitable.

Therefore, the fisheye lenses having relationships of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 2), \mathrm{h}=\mathrm{f} \cdot \theta, \mathrm{h}=2 \mathrm{f} \cdot \sin (\theta / 2)$ and $\mathrm{h}=\mathrm{f} \cdot \sin \theta$ may be used. FIGS. 4(A) to 4(D) show, in concentric circles each centering around the optical axis of each fisheye lens, image heights $h$ when the field angle $\theta$ is changed in $10^{\circ}$ with respect to the optical axis of each fisheye lens. FIG. 4(A) shows the image height in the fisheye lens having the relationship of $h=2 f \cdot \tan (\theta / 2)$, FIG. $4(B)$ shows the image height in the fisheye lens having the relationship of $h=f \cdot \theta$, FIG. 4(C) shows the image height in the fisheye lens having the relationship of $h=2 f \cdot \sin (\theta / 2)$, and FIG. 4(D) shows the image height in the fisheye lens having the relationship of $h=f \cdot \sin \theta$. In FIGS. 4(A) to 4(D), ho represents the height of an image Mo near the optical axis of each fisheye lens and he represents the height of an image Me at a field angle of around $90^{\circ}$.

As is understood from FIGS. 4(A) to 4(D), image height at a field angle of around $90^{\circ}$ when the fisheye lens having the relationship of $h=2 f \cdot \sin (\theta / 2)$ or the fisheye lens having the relationship of $h=f \cdot \sin \theta$ is used is smaller than image height near the optical axis and only a small volume of image data can be obtained. The image height he of an image Me at a peripheral portion of the fisheye lens that has been generally used and has the relationship of $h=f \cdot \theta$ is the same as the image height ho of an image Mo near the optical axis and the image is distorted.

From these facts, it can be said that the fisheye lenses having relationships of $\mathrm{h}=2 \mathrm{f} \cdot \sin (\theta / 2)$ and $\mathrm{h}=\mathrm{f} \cdot \sin \theta$ are not preferred in view that how large volume of data can be obtained at a field angle of $90^{\circ}$ or therearound. Even with the fisheye lens that has been generally used and has the relationship of $\mathrm{h}=\mathrm{f} \cdot \theta$ is not satisfactory.
In contrast to that, the image height he of the image Me at a peripheral portion of the fisheye lens 1 having the relationship of $\mathbf{h}=2 f \cdot \tan (\theta / 2)$ in accordance with the present invention is enlarged and larger than the image height ho of the image Mo near the optical axis, a larger volume of image data can be obtained in comparison with the conventional fisheye lens, and the obtained image is not distorted.
When a single spherical image obtained by combining two hemispherical images of all the directions of the field of view around the optical axis of the fisheye lens 1 , which are picked up at a field angle of $90^{\circ}$ with respect to the optical axis is converted into a plane image by the image data processing unit 3 , it is necessary to interpolate missing image data on the peripheral portion (field angle of around $90^{\circ}$ with respect to the optical axis) of the image. According to the present invention, since an image at the peripheral portion is enlarged and a large volume of data on the peripheral portion can be extracted, the volume of image data to be interpolated can be greatly reduced, when compared with the conventional system.

An image of all the directions of the field of view around the optical axis is picked up at a field angle of at least $90^{\circ}$
with respect to the optical axis and is polar-coordinate converted into a plane image in the following manner.

An X, Y and Z coordinate system as shown in FIG. 5 is imagined in subject space. At this point, the optical axis of the fisheye lens 1 is made $Z$ axis. The coordinates of a certain point $p$ are represented as (X1, Y1, Z1) and the elevation angle of the point $p$ from the origin $O$ of the coordinates with respect to the XZ plane is represented by $\theta$. The elevation angle of the point $p$ from the position of $\mathbf{Z 1}$ on the Z axis with respect to the XZ plane is represented by $\emptyset$.

When an $x$ and $y$ coordinate system having the optical axis ( Z axis) as an origin $o$ is imagined on the surface of CCD image pick-up elements 30 as shown in FIG. 6 and the focal distance of the fisheye lens 1 is represented by $f$, the image formation point ( $p^{\prime}$ ) for the point $p$ is located as shown in FIG. 6. In FIG. 6, $\pi$ is added to $\varnothing$ because an image formed at the point $\mathbf{p}^{\prime}$ is inverted vertically and horizontally with respect to the image of the subject surface (point $p$ ). The optical axis in FIG. 6 is present in a direction perpendicular to the paper from the origin $o$ of the $x$ and $y$ coordinates.

The position of the point $\mathrm{p}^{\prime}$ is expressed as polar coordinates with a length (h) between the origin o and the point $\mathrm{p}^{\prime}$ and an angle $\varphi+\pi$ formed by op' and the x axis. When the polar coordinates are expressed on the $x$ and $y$ rectangular coordinates, the position ( $\mathrm{x} 1, \mathrm{y} 1$ ) on the x and y rectangular coordinates are expressed as follows.

```
x1=h\cdot\operatorname{cos}(\varnothing+\pi)
y1=h}\cdot\operatorname{sin}(\emptyset+\pi
```

In addition, the image height $h$ of the point $p^{\prime}$ is represented by $h=2 f \cdot \tan (\theta / 2)$, hence, when $h=2 f \cdot \tan (\theta / 2)$ is substituted into the above expressions (1) and (2), the coordinates ( x 1 , y1) of the image formation point $p^{\prime}$ on the surface of the CCD image pick-up elements $\mathbf{3 0}$ are as follows.

```
xI=2f
y=2f}\cdot\operatorname{tan}(0/2)\cdot\operatorname{sin}(\varphi+\pi
```

As a result, they are expressed as follows.

$$
\begin{align*}
& x=-2 \mathrm{f} \cdot \tan (\theta / 2) \cdot \cos \emptyset  \tag{5}\\
& y=-2 \mathrm{f} \cdot \tan (\theta / 2) \cdot \sin \emptyset \tag{6}
\end{align*}
$$

In the above expressions, $\theta$ and $\varnothing$ are defined as follows.

$$
\begin{aligned}
& \theta=\tan ^{-1}\left(\sqrt{\mathrm{X} 1^{2+Y 1^{2}}} / \mathrm{Z} 1\right) \\
& \phi=\tan ^{-1}(\mathrm{Y} 1 / \mathrm{X} 1)
\end{aligned}
$$

Thus, the position of the point $\mathrm{p}^{\prime}$ on the surface of CCD image pick-up elements $\mathbf{3 0}$ can be obtained for the point $p$ on the surface of the subject.

Thereafter, a description is subsequently given, with reference to FIG. 7, of steps required when the sphere (all directions) is photographed by the camera 2 comprising the fisheye lens 1 and an image thereof is displayed on the monitor unit 4 that is the display unit.

First, a hemisphere in one direction is photographed by the camera 2 comprising the fisheye lens 1 (step $\mathbf{S 1}$ ). Thereby, an image of the hemisphere is formed on the surface of the CCD image pick-up elements $\mathbf{3 0}$ as a polarcoordinate converted image. Thereafter, the camera 2 is turned at an angle of $180^{\circ}$ to photograph the other hemisphere in the opposite direction (step S2). Thereby, an image of the other hemisphere is formed on the surface of the CCD image pick-up elements $\mathbf{3 0}$ as a polar-coordinate converted image.

The above two images are then combined together and the combined image is converted into a plane image by the image data processing unit 3 (step S 3 ). At this point, an area corresponding to a connection portion between these hemispheres must be corrected. Since the polar-coordinate converted image obtained by the fisheye lens 1 has a large volume of information on a peripheral portion, the processing of combining these images is easy. Thereafter, a predetermined portion of the thus obtained plane image is extracted and displayed on the monitor unit 4 (step S4).

A user shifts the screen with instruction means such as a mouse when the user likes to change the displayed predetermined portion. This shifting can be made continuously in any direction of $360^{\circ}$ around the portion displayed on the monitor unit 4 (step $\mathrm{S5}$ ).

The above steps are for picking up an image of a sphere in all the directions of $360^{\circ}$. When only a single hemisphere is photographed, the same steps are taken. However, step S2 is unnecessary and the processing of combining two images in step $\mathbf{~} \mathbf{3}$ is also unnecessary.

In the present invention, since the volume of information on the peripheral portion of an image obtained by the fisheye lens $\mathbf{1}$ is large, that is, an image at the peripheral portion is enlarged, it is convenient when the present invention is used for the examination of a product. For example, when the inner surface $\mathbf{5 2}$ of a cylindrical body $\mathbf{5 1}$ is photographed at the condition that the optical axis of the fisheye lens 1 of the present invention is aligned with the central axis of the cylindrical body 51 as shown in FIGS. 8(A) and 8(B), a peripheral portion of an image can be extracted as an image having a larger volume of information than a central portion in the present invention. Therefore, it is easy to find that a scratch has been generated in the inner surface 52. Consequently, this can be used for the examination of a pipe-like body such as a water pipe or gas pipe and further for the monitoring of a crack that has been generated in the wall surface of a tunnel or the like.
It can also be used for the examination of the connection condition of a small part such as an IC. That is, when a part 71 is fixed to a substrate $\mathbf{7 4}$ by a solder $\mathbf{7 3}$ on its both sides 72 and 72 shown in FIGS. 9(A) and 9(B), the soldering state of the part must be checked from its side direction in the prior art. However, when another part 75 is existent in a side direction, the solder 73 on the part 75 side cannot be seen through a camera, thereby making automatic examination difficult. On the other hand, even when the fisheye lens 1 is installed right over the part 71 as shown in FIG. 9(A), the side direction of the part 71 can be sufficiently photographed by the camera 2 comprising the fisheye lens $\mathbf{1}$ of the present invention, thereby enabling automatic examination with the camera 2.

Although each foregoing embodiment is an example of a preferred embodiment of the invention, it is to be understood that the invention is not limited thereto and that various changes and modifications may be made in the invention without departing from the spirit and scope thereof. For example, the fisheye lens may be constructed by the attachment lens unit 20 alone without the master lens $\mathbf{1 0}$, or contrariwise may be constructed by an integrated unit of the master lens unit $\mathbf{1 0}$ and the attachment lens unit 20. Also, the construction and numerical values of the fisheye lens 1 shown in the above embodiment are just examples and a fisheye lens having other construction and numerical values may be used.

Further, as the system comprising the fisheye lens 1 of the present invention, an image processing system 81 shown in FIG. 10 may be used. This image processing system 81 is mainly constructed with a camera 2 equipped with a fisheye lens 1 and an image data processing unit/monitor 5 connected to the camera 2 by a cable. The image data processing unit/monitor 5 is a personal computer equipped with a monitor, and a key board $5 a$ and a mouse $5 b$ are connected to the computer as instruction means.

Also, this image data processing unit/monitor 5 has a hard disk (not shown) in that the contents of an information recording medium (floppy disk) 6 recording a program for executing the steps S3, S4 and S5 shown in FIG. 7 are to be installed. By installing this program in the image data processing unit/monitor 5 , the image data processing unit/ monitor 5 carries out the same function as the image data processing unit 3 which has been described in the foregoing.

Image pick-up data may be transferred from the camera 2 to the image data processing unit/monitor 5 by a memory card such as a flash card or wireless communication such as infrared communication, besides a cable. Further, the program may be installed not from the floppy disk 6 but other recording medium such as a CD-ROM, or transferred from other storage unit over a network. When the program is transferred over a network, the storage unit of a transmitter or the hard disk (storage unit) of the image data processing unit/monitor 5 serves as the information recording medium of the present invention.

As having been described above, in the image pick-up device comprising the fisheye lens according to the first aspect of the present invention, the fisheye lens has the relationship of $h=n f \cdot \tan (\theta / m)$ (wherein $h$ is an image height, $f$ is a focal distance, and $\theta$ is a field angle). With this, compared with the ordinary fisheye lens having the relationship of $h=f \cdot \theta$ (wherein $h$ is an image height, $f$ is a focal distance, and $\theta$ is a field angle), an image at a peripheral portion (field angle of around $90^{\circ}$ with respect to the optical axis of the fisheye lens) is enlarged and the volume of information is large, thereby making it possible to minimize the missing portions of image data on the peripheral portion. When the picked-up image is to be converted into a plane image, interpolating of image data can be thereby minimized and a more natural plane image can be obtained.

Also, according to the second aspect of the present invention, by attaching the attachment lens different from the master lens provided on the existing image pick-up device (camera) to the master lens, the fisheye lens is constructed by this master lens and the attachment lens. Therefore, the fisheye lens can be attached to almost all the existing image pick-up devices (cameras) and further, only the attachment lens is newly produced, thereby reducing costs.

Further, according to the third aspect of the present invention, the image display device can convert a spherical image into a plane image with ease and can display a more natural plane image. In addition, according to the fourth aspect of the present invention, when the program recorded in the information recording medium is read and executed by a computer, a more natural plane image can be formed.

Therefore, it is intended that the appended claims be interpreted as including the embodiments described herein, the alternatives mentioned above, and all equivalents thereto.

What is claimed is:

1. An image pick-up device, comprising:
a fisheye lens for picking up an image of all directions of a field of view around an optical axis of said fisheye lens at a field angle of at least $90^{\circ}$ in each direction with respect to the optical axis,
the fisheye lens having a relationship of $h=n \cdot f \cdot \tan (\theta / m), h$ being a height of an image of a subject at a predetermined point obtained by the fisheye lens, $f$ being a focal distance of the fisheye lens, $\theta$ being a field angle, $m$ having a value of $1.6 \leqq \mathrm{~m}<3$, and n having a value of $\mathrm{m}-0.4<\mathrm{n} \leqq \mathrm{m}+0.4$.
2. The image pick-up device of claim 1 , wherein $m$ and $n$ are substantially equal.
3. The image pick-up device of claim 1, wherein m and $n$ both substantially equal 2 .
4. The image pick-up device of claim 1, wherein $m$ and $n$ both equal 2 such that the fisheye lens has a relationship of $\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta) / 2)$.
5. The image pick-up device of claim 1, wherein the fisheye lens is constructed by a master lens provided on an existing image pick-up device and an attachment lens to be attached to the master lens.
6. An image display device, comprising:
an image data processing unit for converting an image obtained by the image pick-up device of claim 1 into a plane image; and
a display unit for displaying the converted plane image.
7. The image display device of claim 6, wherein said image data processing unit receives the image picked up by said fisheye lens.
8. The image display device of claim 6 , wherein $m$ and $n$ are substantially equal.
9. The image display device of claim 6, wherein $m$ and $n$ both substantially equal 2 .
10. The image display device of claim 6, wherein $m$ and n both equal 2 such that the fisheye lens has a relationship of $h=2 f \cdot \tan (\theta / 2)$.
11. An information recording medium having recorded thereon a program including at least the steps of:
converting into a plane image an image obtained by a fisheye lens for picking up an image of all directions of a field of view around an optical axis of said fisheye lens at a field angle of at least $90^{\circ}$ in each direction with respect to the optical axis, said fisheye lens having a relationship of $h=n \cdot f \cdot \tan (\theta / m)$, $h$ being a height of an image of a subject at a predetermined point obtained by the fisheye lens, $f$ being a focal distance of the fisheye lens, $\theta$ being a field angle, $m$ having a value of $1.6 \leqq m \leqq 3$, and $n$ having a value of $m-0.4 \leqq n \leqq m+0.4$;
displaying a predetermined portion of the converted plane image on a display unit; and
changing continuously the predetermined portion with instruction means.
12. The information recording medium of claim 11, wherein $m$ and $n$ are substantially equal.
13. The information recording medium of claim 11, wherein $m$ and $n$ both substantially equal 2 .
14. The information recording medium of claim 11, wherein $m$ and $n$ both equal 2 such that the fisheye lens has a relationship of $h=2 f \cdot \tan (\theta / 2)$.

*     *         *             *                 * 


## APPENDIX H

## Appendix H

## Claim Analysis Chart of U.S. Patent $\mathrm{N} 0.6,844,990$ B2 ("the ' 990 patent")

Detailed Explanation of Pertinency of Baker, Shiota, and Enami

The ' 990 Patent

| 15. The method according to claim 10 , further comprising: | Baker and Shiota disclose the elements of claim 10 , as described in Appendix F. |
| :---: | :---: |
| determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the nonlinear distribution function, and | Enami discloses determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the non-linear distribution function. (Enami translation at paras. [0058], [0084]-[0085]). Enami discloses allocating to each image point of the display window the color of an image point that is the closest on the initial image. (Enami translation at paras [0072][0074]). Enami discloses a coordinate of a point of the fisheye lens image img corresponding to a coordinate of each point arranged on a raster in the image frame frm is specified, and a color information signal of the point having the coordinate is made to correspond to a color information signal of a point having a coordinate of the display frame frm, and thus it is possible to perform a correction process of transforming the fisheye lens image img to an original image. (Enami translation at para. [0058]). |
| allocating to each image point of the display window the color of an image point that is the closest on the initial image. | Enami discloses: "Here, the point ( $x$ ", $y$ ") on the coordinates of the fisheye lens image obtained through the above-described operation is indicated by (u, v). In order to smoothly interpolate this coordinate point (u, v), the following interpolation process is performed. Color information signal components of three colors of a picture signal are indicated by $Y, U$, and $V$, those components of the point ( $u$, v) are indicated by $\mathrm{Yu}, \mathrm{V}, \mathrm{Uu}$, $v$, and Vu , v , values which become an integer by omitting decimal points of the coordinate components $u$ and $v$ of the point $(\mathrm{u}, \mathrm{v})$ are indicated by u 0 and v 0 , and a value of the color information signal Y in a point having the coordinate $(\mathrm{u} 0, \mathrm{vO})$ is indicated by YuO vO . Similarly, the same content is indicated by UuOvO and VuOvO for the color information signals U and V . In addition, values obtained by rounding up decimal points of the coordinate components $u$ and $v$ are respectively indicated by ul and v , and values of the color information signals $\mathrm{Y}, \mathrm{U}$ and V having a coordinate corresponding thereto are respectively indicated by Yulvl, Uulvl, and Vulvl. Further, decimal parts of the coordinate components $u$ and $v$ are respectively indicated by du and dv." |

## Appendix H

|  | (Enami translation at para. [0072]). |
| :---: | :---: |
| 16. The method according to claim 15 , wherein the projection of the image points of the display window onto the initial image comprises: projecting the image points of the display window onto a sphere or a sphere portion, | Enami discloses mapping from a three-dimensional coordinate point $(x, y, z)$ to a point $P\left(x^{\prime \prime}, y^{\prime \prime}\right)$ of the fisheye lens image on the twodimensional coordinates which is first performed by transforming the point $(x, y, z)$ into a point $(r, \cdot, \cdot)$ expressed in polar coordinates. This transform can be performed using a polar coordinate transform expression of Equation (5). (Enami translation at para. [0066]). <br> Shiota discloses "transforming a fisheye image obtained using a fisheye lens (2) into a plane image for display comprising: a first coordinate calculating unit (35) for obtaining first projection coordinates derived by projecting coordinates on the plane image onto a fisheye face as an imaginary object face." (Shiota at Abstract). |
| determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and | Enami discloses this transform can be performed using a polar coordinate transform expression of Equation (5). (Enami translation at para. [0067]). <br> Shiota discloses "Necessary parameters are, as shown in Figs. 1 and 2, ( $\mathrm{XO}, \mathrm{YO}, \mathrm{ZO}$ ) indicative of the center (origin) of a plane image and change amounts $\bullet u x, \bullet v x, \cdot u y, \cdot v y, \bullet u z, \bullet v z$ in the respective axes of the $(X, Y$, Z) coordinates when a point is moved in the respective directions on the (u, v) coordinate system by an amount of one pixel (corresponding to one pixel on the monitor screen). (Shiota at para. [0025]). "The parameters can be easily obtained from the information of the angle information ( $\cdot$, $\cdot \cdot \cdot$ ) of the view point and the magnification of the image." (Shiota at para. [0026]). Since point P' "is on the surface of the hemisphere of radius of 1 , the zenithal angle $(\cdot 1)$ is unconditionally determined..." (Shiota at para. [0034]). |
| projecting onto the initial image each image point projected onto the sphere or the sphere portion, | Enami discloses a fisheye lens of an equal area mapping formula which is expressed by Equation (3-2), and this equation is assigned to Equation (2) so as to obtain an expression of Equation (6). The expression of Equation (5) is simplified as in an expression of Equation (7) using a relation of $x 2$ $+y^{2}+z_{2}=x^{\prime} 2+y^{\prime} 2+z^{\prime 2}=r 2$, Equation (5), and further a basic expression of a trigonometric function. (Enami translation at paras. [0068], [0070]). |

## Appendix H

|  | Shiota discloses "First, the coordinates of a point $P^{\prime}$ (first projection coordinates) on the hemispherical face as an imaginary object face, which is a projection of a point $P$ on a plane image (the $u, v$ coordinates) are obtained." (Shiota at para. [0028]). |
| :---: | :---: |
| the projection being performed by means of the nonlinear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion. | Enami discloses that the projection is performed by means of the nonlinear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion. The field angle is defined according to the horizontal and vertical extents in the image area while the center is defined to be the image center position. Further, a fisheye lens of an equal area mapping formula is expressed by an expression of Equation (3-2), and this equation is assigned to Equation (2) so as to obtain an expression of Equation (6). (Enami translation at para. [0068]). <br> Shiota discloses as a second step of the calculation, "a procedure of obtaining second projection coordinates $\mathrm{w}(\mathrm{pl}, \mathrm{q} 1$, ) on a fisheye image face from the first projection coordinates (X2, Y2, Z2) determined (refer to FIG. 1 with respect to w) will be explained." (Shiota at para. [0033]). An example of a specific function of $\mathrm{F}(1)$ according to the projecting method is the stereographic projection, which has the non-linear distribution function: $2 \mathrm{ff} \tan \cdot \cdot / 2$ ). (Shiota at para. [0037]). |

## APPENDIX G

## Appendix G

## Claim Analysis Chart of U.S. Patent $\mathrm{N} 0.6,844,990$ B2 ("the ' 990 patent")

Detailed Explanation of Pertinency of Nagaoka, Shiota, and Enami

The ${ }^{6} 990$ Patent

| 15. The method according to claim 10 , further comprising: | Nagaoka and Shiota disclose the elements of claim 10 , as described in Appendix D. |
| :---: | :---: |
| determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the nonlinear distribution function, and | Enami discloses determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the non-linear distribution function. (Enami translation at paras. [0058], [0084]-[0085]). Enami discloses allocating to each image point of the display window the color of an image point that is the closest on the initial image. (Enami translation at paras [0072][0074]). Enami discloses a coordinate of a point of the fisheye lens image img corresponding to a coordinate of each point arranged on a raster in the image frame frm is specified, and a color information signal of the point having the coordinate is made to correspond to a color information signal of a point having a coordinate of the display frame frm, and thus it is possible to perform a correction process of transforming the fisheye lens image img to an original image. (Enami translation at para. [0058]). |
| allocating to each image point of the display window the color of an image point that is the closest on the initial image. | Enami discloses: "Here, the point ( $x$ ", $y^{\prime \prime}$ ) on the coordinates of the fisheye lens image obtained through the above-described operation is indicated by (u, v). In order to smoothly interpolate this coordinate point (u, v), the following interpolation process is performed. Color information signal components of three colors of a picture signal are indicated by $\mathrm{Y}, \mathrm{U}$, and V , those components of the point $(u, v)$ are indicated by $\mathrm{Yu}, \mathrm{V}, \mathrm{Uu}, \mathrm{v}$, and Vu , v , values which become an integer by omitting decimal points of the coordinate components $u$ and $v$ of the point $(\mathrm{u}, \mathrm{v})$ are indicated by u 0 and v 0 , and a value of the color information signal Y in a point having the coordinate $(\mathrm{u} 0, \mathrm{v} 0)$ is indicated by YuO vO . Similarly, the same content is indicated by $\mathrm{UuOVO}_{\mathrm{V}}$ and VuOvO for the color information signals U and V . In addition, values obtained by rounding up decimal points of the coordinate components $u$ and $v$ are respectively indicated by ul and vl , and values of the color information signals $\mathrm{Y}, \mathrm{U}$ and V having a coordinate corresponding thereto are respectively indicated by Yulvl, Uulvl, and Vulvl. Further, decimal parts of the coordinate components $u$ and $v$ are respectively indicated by du and dv." |

## Appendix G

|  | (Enami translation at para. [0072]). |
| :---: | :---: |
| 16. The method according to claim 15 , wherein the projection of the image points of the display window onto the initial image comprises: projecting the image points of the display window onto a sphere or a sphere portion, | Enami discloses mapping from a three-dimensional coordinate point $(x, y, z)$ to a point $P\left(x^{\prime \prime}, y^{\prime \prime}\right)$ of the fisheye lens image on the twodimensional coordinates which is first performed by transforming the point $(x, y, z)$ into a point $(r, \cdot, \cdot)$ expressed in polar coordinates. This transform can be performed using a polar coordinate transform expression of Equation (5). (Enami translation at para. [0066]). <br> Shiota discloses "transforming a fisheye image obtained using a fisheye lens (2) into a plane image for display comprising: a first coordinate calculating unit (35) for obtaining first projection coordinates derived by projecting coordinates on the plane image onto a fisheye face as an imaginary object face." (Shiota at Abstract). |
| determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and | Enami discloses this transform can be performed using a polar coordinate transform expression of Equation (5). (Enami translation at para. [0067]). <br> Shiota discloses "Necessary parameters are, as shown in Figs. 1 and 2, $(\mathrm{XO}, \mathrm{YO}, \mathrm{ZO})$ indicative of the center (origin) of a plane image and change amounts $\bullet u x, \bullet v x, \cdot u y, \bullet v y, \bullet u z, \bullet v z$ in the respective axes of the $(X, Y$, Z) coordinates when a point is moved in the respective directions on the (u, v) coordinate system by an amount of one pixel (corresponding to one pixel on the monitor screen). (Shiota at para. [0025]). "The parameters can be easily obtained from the information of the angle information ( $\cdot$, $\cdot, \cdot$ ) of the view point and the magnification of the image." (Shiota at para. [0026]). Since point $P$ ' "is on the surface of the hemisphere of radius of 1 , the zenithal angle $(\cdot 1)$ is unconditionally determined..." (Shiota at para. [0034]). |
| projecting onto the initial image each image point projected onto the sphere or the sphere portion, | Enami discloses a fisheye lens of an equal area mapping formula which is expressed by Equation (3-2), and this equation is assigned to Equation (2) so as to obtain an expression of Equation (6). The expression of Equation (5) is simplified as in an expression of Equation (7) using a relation of $\times 2$ $+y_{2}+z 2=x^{\prime 2}+y^{\prime} 2+z^{\prime 2}=r 2$, Equation (5), and further a basic expression of a trigonometric function. (Enami translation at paras. [0068], [0070]). |

## Appendix G

|  | Shiota discloses "First, the coordinates of a point $P^{\prime}$ (first projection coordinates) on the hemispherical face as an imaginary object face, which is a projection of a point $P$ on a plane image (the $u, v$ coordinates) are obtained." (Shiota at para. [0028]). |
| :---: | :---: |
| the projection being performed by means of the nonlinear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion. | Enami discloses that the projection is performed by means of the nonlinear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion. The field angle is defined according to the horizontal and vertical extents in the image area while the center is defined to be the image center position. Further, a fisheye lens of an equal area mapping formula is expressed by an expression of Equation (3-2), and this equation is assigned to Equation (2) so as to obtain an expression of Equation (6). (Enami translation at para. [0068]). <br> Shiota discloses as a second step of the calculation, "a procedure of obtaining second projection coordinates $\mathrm{w}(\mathrm{pl}, \mathrm{q} 1$, ) on a fisheye image face from the first projection coordinates (X2, Y2, Z2) determined (refer to FIG. 1 with respect to w) will be explained." (Shiota at para. [0033]). An example of a specific function of $\mathrm{F}(1)$ according to the projecting method is the stereographic projection, which has the non-linear distribution function: $2 \mathrm{ff} \tan \cdot \cdot / 2$ ). (Shiota at para. [0037]). |

## APPENDIX F

## Appendix F

# Claim Analvsis Chart of U.S. Patent N0. $6,844,990$ B2 ("the "900 patent") 

Detailed Explanation of Pertinency of Baker and Shiota

The '990 Patent
Prior Art

| 10. A method for displaying an initial panoramic image obtained in accordance with the method according to claim 1, the method for displaying comprising: | Baker discloses the elements of claim 1, as described in Appendix B. |
| :---: | :---: |
| correcting the non-linearity of the initial image, performed by means of a reciprocal function of the nonlinear distribution function of the objective lens or by means of the non-linear distribution function. | Baker discloses a "transform processor 22" which "corrects the image for display on a conventional display device 28 " by "compensate[ing] for the distortion or difference in magnification between the central and peripheral areas of the scene caused by the lens by applying appropriate correction criteria to bring the selected portion of the scene into standard viewing format." (Baker at col. 6, Ins. 5-24; col. 9, Ins. 5-13). Baker does not disclose details on the specific corrections applied by the transform processor 22. <br> Shiota discloses correcting the non-linearity of an initial image performed by using a non-linear distribution function. (Shiota at paras. [0030][0032]). "An image is transformed as follows. The projecting position on the image pickup face ( $p, q$ coordinates) of a point ( $u, v$ coordinates) on a plane image is obtained by arithmetic operation." (Shiota at para. [0024]). In one embodiment, a non-linear distribution function $(\mathrm{h}=2 \mathrm{f} \cdot \tan (/ 2))$ is used to compute the coefficient $\mathrm{k} 2 . \mathrm{k} 2=\mathrm{h} / \mathrm{r}$, where h is defined by the lens function and $r$ is the distance from the origin. (Shiota at paras. [0037]-[0042]). The coefficient $k 2$ is used to obtain the image points that will be displayed. (Shiota at paras. [0031]-[0035]). As the coefficient k 2 used to correct the image is computed using the non-linear distribution function, Shiota discloses "correcting the non-linearity of the initial image, performed ... by means of the non-linear distribution function." |
| 11. The method according to claim 10 , wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises. | Shiota discloses a stereoscopic projection having a relationship $\mathrm{h}=2 \mathrm{f} \cdot \tan (12)$, which produces an image having an expanded portion. (Shiota at para. [0037]). Shiota further discloses that the position of a pixel on the fisheye image will not necessarily map to a pixel on the plane image and hence nearby pixels would be used for interpolation. (Shiota at |

## Appendix F

|  | para. [0049]). Because Shiota has an expanded portion, one of ordinary <br> skill in the art would have known that the number of image points in a <br> corrected digital image would be larger than the number of points in the <br> initial image. Considering a region in the initial image that is to be <br> expanded, each initial image point will represent the projection of <br> multiple spatial points according to the lens system. Hence, during the <br> expansion process, the image points will be mapped to one or more points <br> in the corrected digital image. Shiota discloses this step of transforming <br> the initial image into a corrected digital image where the number of image <br> points is higher than the number of pixels of the image sensor. |
| :--- | :--- |

## APPENDIX E

## Appendix E

## Claim Analysis Chart of U.S. Patent No. $6,844,990$ B2 ("the ' 990 patent")

## Detailed Explanation of Pertinency of Nagaoka and Matsui

The ' 990 Patent
Prior Art

| 10. A method for displaying an initial panoramic image obtained in accordance with the method according to claim 1, the method for displaying comprising: | Nagaoka discloses the elements of claim 1, as described in Appendix A. |
| :---: | :---: |
| correcting the non-linearity of the initial image, performed by means of a reciprocal function of the nonlinear distribution function of the objective lens or by means of the non-linear distribution function. | Nagaoka discloses that the obtained image is "converted into a plane image by the image data processing unit 3" (Nagaoka at col. 8, Ins. 2-3), but does not disclose the specific correction applied by the image data processing unit. <br> Matsui discloses correcting the non-linearity of an initial image, performed by the non-linear distribution function. (Matsui translation at paras. [0025], [0030]-[0031]. Matsui discloses a data image conversion device, in which image data obtained with a fish-eye lens is corrected to remove distortion so that it may be displayed. (Matsui translation at para. [0001]). Matsui discloses that this correction can be performed using the non-linear lens distribution function $h=2 f \cdot \tan (/ 2)=2 f \cdot\{\sin /(1+$ $\cos )\}$, or more generally using the formula $\mathrm{h}=\mathrm{g}()$. (Shiota at paras. [0025], [0030]). Matsui further discloses the calculation of pixel positions on the circular surface from the pixel positions actually captured by the CCD utilizing the non-linear distribution function $\mathrm{h}=2 \mathrm{f} \cdot \tan (12)$. (Shiota at para. [0025]). A data converter 2, that calculates the circular surface $S$ pixel position corresponding to each pixel on the postconversion cylindrical surface $C$, then converts the pixel data of the pixel positions as respective pixel data on the cylindrical surface C. "As a result, as shown in Fig. 4, the pixel data on the circular surface $S$ is converted as respective pixel data on the cylindrical surface C." (Matsui translation at para. [0026]). "The data converter 2 converts Pl shown in Fig. 3 into P2 shown in Fig. 2." (Matsui translation at para. [0023]). Matsui therefore discloses "correcting the non-linearity of the initial image, performed ... by means of the non-linear distribution function." |

## APPENDIX D

## Appendix D

# Claim Analysis Chart of U.S. Patent N0. $6,844,990$ B2 ("the "900 patent") 

Detailed Explanation of Pertinency of Nagaoka and Shiota

The ' 990 Patent
Prior Art
$\left.\left.\begin{array}{|l|l|}\hline \hline \begin{array}{l}\text { 10. A method for displaying an initial panoramic image } \\ \text { obtained in accordance with the method according to } \\ \text { claim 1, the method for displaying comprising: }\end{array} & \begin{array}{l}\text { Nagaoka discloses the elements of claim l, as described in Appendix A. } \\ \text { correcting the non-linearity of the initial image, } \\ \text { performed by means of a reciprocal function of the non- } \\ \text { linear distribution function of the objective lens or by } \\ \text { means of the non-linear distribution function. }\end{array} \\ \begin{array}{l}\text { Nagaoka discloses that the obtained image is "converted into a plane } \\ \text { image by the image data processing unit 3" (Nagaoka at col. 8, Ins. 2-3), } \\ \text { but does not disclose the specific correction applied by the image data } \\ \text { processing unit. } \\ \text { Shiota discloses correcting the non-linearity of an initial image performed }\end{array} \\ \text { by using a non-linear distribution function. (Shiota at paras. [0030]- } \\ \text { [0032]). "An image is transformed as follows. The projecting position on } \\ \text { the image pickup face (p, q coordinates) of a point (u, v coordinates) on a } \\ \text { plane image is obtained by arithmetic operation." (Shiota at para. }\end{array} \right\rvert\, \begin{array}{l}\text { [0024]). In one embodiment, a non-linear distribution function } \\ \text { (h=2ftan( /2)) is used to compute the coefficient k2. k2 = h/r, where h is } \\ \text { defined by the lens function and r is the distance from the origin. (Shiota }\end{array}\right\}$

## Appendix D

|  | expanded, each initial image point will represent the projection of <br> multiple spatial points according to the lens system. Hence, during the <br> expansion process, the image points will be mapped to one or more points <br> in the corrected digital image. Shiota discloses this step of transforming <br> the initial image into a corrected digital image where the number of image <br> points is higher than the number of pixels of the image sensor. |
| :--- | :--- |

## APPENDIX J

## Appendix J

## Claim Analysis Chart of U.S. Patent $\mathrm{N} 0.6,844,990$ B2 ("the ' 990 patent")

> Detailed Explanation of Pertinency of Baker and Inoue

The 990 Patent Prior Art

| 25. The panoramic objective lens according to claim 22, |
| :--- | :--- |
| comprising polymethacrylate lenses. | | Baker discloses the elements of claim 22, as described in Appendix B. |
| :--- |
|  |
| Inoue discloses making wide angle ennses from PMMA (Inoue at col. 2, <br> Ins. 42-44), which the '990 Patent equates to polymetharylate ( 990 <br> Patent at col. 16, Ins. 31-43). |

## APPENDIX I

## Appendix I

## Claim Analysis Chart of U.S. Patent $\mathrm{N} 0.6,844,990$ B2 ("the ' 990 patent")

> Detailed Explanation of Pertinency of Nagaoka and Inoue

The '990 Patent
Prior Art

| 25. The panoramic objective lens according to claim 22, <br> comprising polymethacrylate lenses. | Nagaoka discloses the elements of claim 22, as described in Appendix A. |
| :--- | :--- |
|  | Inoue discloses making wide angle lenses from PMMA (Inoue at col. 2, <br> lns. 42-44), which the '990 Patent equates to polymethacrylate ('990 <br> Patent at col. 16, Ins. 31-43). |

APPENDIX C

## Appendix C

## Claim Analysis Chart of U.S. Patent N0. $6,844,990$ B2 ("the "900 patent")

> Detailed Explanation of Pertinency of Fisher

The ${ }^{6} 990$ Patent
Prior Art

| 1. A method for capturing a digital panoramic image, | Fig. 6 of Fisher depicts a non-linear panoramic objective lens. (Col. 5, Ins. 44-45). Additionally, "[t]he distorted image formed by the non-linear lens exists in an image plane p located beyond the third lens grouping C. The vidicon of the television camera should be at this plane p." (Abstract; col. 6, Ins. 51-54; col. 4, Ins. 35-45). |
| :---: | :---: |
| by projecting a panorama onto an image sensor by means of a panoramic objective lens, | Fisher discloses projecting a panorama onto an image sensor by means of a panoramic objective lens. (Fig. 3; col. 3, Ins. 48-49). Fisher also discloses "The image cast by the lens falls on the vidicon of a television camera where it is scanned and transmitted to a projector." (Abstract; col. 4, lns. 35-45). |
| the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, | Fisher discloses "The present invention relates in general to lenses and more particularly to a lens having non-linear distortion characteristics." (Col. 1, Ins. 9-11). "One of the principal objects of the present invention is to provide a lens having non-linear distortion characteristics." (Col. 2, lns. 6-8). |
| the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, | Fig. 3 of Fisher shows a "NON-LINEAR LENS" where the image height is equal to a variable function of the field angle. Fig. 3 shows "the distortion characteristics of the lens of the present invention in terms of normalized image height and field of view and comparing such distortion characteristics with the distortion characteristics of a linear fisheye lens and a conventional camera lens." (Col. 2, Ins. 38-43). The relationship is approximated by the formula $\mathrm{H}=\sin ^{1 / 3}$. (Col. 3, Ins. 1-4). As shown in Fig. 3, Fisher discloses a non-linear lens having a distribution function whose maximum divergence is much greater than $10 \%$ compared to a linear distribution function (fisheye lens). |

## Appendix C


Appendix C

|  | Image [i.e., the image is compressed at the edges]." (Col. 2, Ins. 19-24). |
| :---: | :---: |
| 6. The method according to claim 1 , wherein the objective lens comprises a set of lenses forming an apodizer. | As described in the " 990 Patent, an "apodizer" is an optical system which provides a non-linear distribution of image points relative to the field angle of the object points. (Col. 16, Ins. 1-4). As shown in Figs. 4 and 6 of Fisher, the lens system controls the angular distribution of the objective lens to obtain non-linearity, and therefore includes an "apodizer" as defined in the ' 990 Patent. |
| 7. The method according to claim 6 , wherein the set of lenses forming an apodizer comprises at least one aspherical lens. | Fisher discloses that the lens surfaces R1 and R3 shown in Fig. 6 are non-spherical (aspherical): "The first lens grouping A(FIG. 6) consists of three lens elements $a, b$, and $c$ with no air gaps between adjacent elements. The outside lens element a has a non-spherical surface R1 exposed outwardly and a spherical surface R2 presented inwardly against a matching surface R 2 on the intermediate element $b$. The opposite sufface $R 3$ of the intermediate element $b$ is non-spherical and abuts a matching surface R3 on the inside element c." (Col. 5, ln. 61-col. 6, ln. 1). |
| 17. A panoramic objective lens comprising: | Fig. 6 of Fisher depicts a non-linear panoramic objective lens. (Col. 5, Ins. 44-45). |
| optical means for projecting a panorama into an image plane of the objective lens, | Fisher discloses projecting a panorama onto an image sensor by means of a panoramic objective lens. (Fig. 3; col. 3, Ins. 48-49). Fisher also discloses "The image cast by the lens falls on the vidicon of a television camera where it is scanned and transmitted to a projector." (Abstract; col. 4, Ins. 35-45). |
| the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama, | Fisher discloses "The present invention relates in general to lenses and more particularly to a lens having non-linear distortion characteristics." (Col. 1, Ins. 9-11). "One of the principal objects of the present invention is to provide a lens having non-linear distortion characteristics." (COL. 2, lns. 6-8). |
| the distribution function having a maximum divergence of at least. + -. $10 \%$ compared to a linear distribution function, | Fig. 3 of Fisher shows a "NON-LINEAR LEN"" where the image height is equal to a variable function of the field angle. Fig. 3 shows "the distortion characteristics of the lens of the present invention in terms of normalized image height and field of view and comparing such distortion characteristics with the distortion characteristics of a linear fisheye lens |

## Appendix C

|  | and a conventional camera lens." (Col. 2, Ins. 38-43). The relationship is <br> approximated by the formula H=sin <br> Fig. 3, Fisher discloses a non-linear lens having a distribution function <br> whose maximum divergence is much greater than $10 \%$ compared to a <br> linear distribution function (fisheye lens). |
| :--- | :--- |

## Appendix C

| 19. The panoramic objective lens according to claim 17 , wherein the lens expands the center of an image and compresses the edges of the image. | Fisher discloses that the "present invention is embodied in a lens which distorts a field of view such that objects in the vicinity of the optical axis occupy a disproportionately large area of the image cast by the lens [i.e., the image is expanded at the center] and objects in the peripheral region of the field of view occupy a disproportionately small area of the Image [i.e., the image is compressed at the edges]." (Col. 2, Ins. 19-24). |
| :---: | :---: |
| 22. The panoramic objective lens according to claim 17 , further comprising a set of lenses forming an apodizer. | As described in the " 990 Patent, an "apodizer" is an optical system which provides a non-linear distribution of image points relative to the field angle of the object points. (Col. 16, Ins. 1-4). As shown in Figs. 4 and 6 of Fisher, the lens system controls the angular distribution of the objective lens to obtain non-linearity, and therefore includes an "apodizer" as defined in the ' 990 Patent. |
| 23. The panoramic objective lens according to claim 22, wherein the set of lenses forming an apodizer comprises at least one aspherical lens. | Fisher discloses that the lens surfaces R1 and R3 shown in Fig. 6 are non-spherical (aspherical): "The first lens grouping A(FIG. 6) consists of three lens elements $a, b$, and $c$ with no air gaps between adjacent elements. The outside lens element a has a non-spherical surface R1 exposed outwardly and a spherical surface R2 presented inwardly against a matching surface $R 2$ on the intermediate element $b$. The opposite surface R 3 of the intermediate element $b$ is non-spherical and abuts a matching surface R3 on the inside element c." (Col. 5, ln. 61-col. $6, \ln .1)$. |

## APPENDIX B

## Appendix B

## Claim Analvsis Chart of U.S. Patent No. $6,844,990$ B2 ("the "900 patent")

Detailed Explanation of Pertinency of Baker

The '990 Patent
Prior Art

| 1. A method for capturing a digital panoramic image, | Baker discloses "the visual imaging system can use a single camera to capture the relevant visual information within a panoramic field of view existing along the horizon," (col. 6, lns. 29-32), and that the "captured scene can be stored onto an assortment of media, e.g., photographic film 16, electronic storage 18 , or other conventional storage means." (Col. 2, Ins. 35-39; col. 8, Ins. 62-65; col. 10, Ins. 55-57; col. 14, Ins. 32-36). |
| :---: | :---: |
| by projecting a panorama onto an image sensor by means of a panoramic objective lens, | Baker discloses projecting a panorama onto an image sensor by means of a panoramic objective lens, and that a "CCD" may be used for digital storage. (Col. 13, Ins. 14-17). |
| the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, | Fig. 2 A of Baker depicts a lens having a typical linear distribution function of image points, while Fig. 3BA of Baker depicts a lens having a non-linear distribution function of image points, relative to the field angle of the object points of the panorama. (Col. 12, Ins. 23-25). <br> Baker further discloses the "fundamental principle behind the enhanced peripheral content lens is the selective magnification of the periphery and the focusing of more of that content on the imaging plane." (Fig. 3BA; col. 10, Ins. 38-41). Baker further discloses a non-linear "lens, indicated generally at 14 , designed to capture and enhance the peripheral content of a hemispheric scene." (Col. 8, lns. 60-62). "To maximize data collection and resolution for analysis and or display of the relevant visual information located in this portion of the hemispheric scene, it is desirable to maximize the dedication of the available image detection area to this peripheral field portion." (Col. 8, Ins. 32-36). |
| the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, | Baker discloses a panoramic objective lens with a distribution function having a maximum divergence of at least $\pm 10 \%$ compared to a linear distribution function. "[l]f an ordinary fisheye lens focuses the lowest 15 degrees up from the horizon on ten percent of the imager at the imaging plane and the peripheral-enhancing lens focuses that same 15 degrees on fifty percent of the imager, there is a five-fold increase in resolution using the same imaging device. Depending on the application and exact formulation of the lens equations, there will be at least a five times |

## Appendix B

|  | increase in resolving power by this lens / mager combination." (Col. 6, Ins. 48-56). <br> Using a normalized height of 1 at $90^{\circ}$, one can calculate the height $h$ at $75^{\circ}$ for the circumstance in which $50 \%$ of the imager is occupied by the lowest $15^{\circ}$. That is, half of the area of the entire circular image is equal to the area of a circle with height $h$ at $75^{\circ}$, or $(1)^{2} / 2=h^{2}$, which gives a height $h$ of about 0.707 . This is a divergence of greater than $10 \%$ compared to a linear distribution function, which would have a height $h$ at $75^{\circ}$ of about 0.833. |
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| such that the panoramic image obtained has at least one substantially expanded zone and at least one substantially compressed zone. | Baker discloses "The lens uniquely achieves this by filling the greater available area of an imager device with the peripheral areas rather than the central areas of the captured scene." (Col. 10, Ins. 57-60). "[T]he lens constructed according to the present invention has a fairly significant portion of the imaging surface dedicated to the peripheral field, and consequuntly less of the surface dedicated to the central field." (Col. 12, Ins. 29-32). The panoramic image obtained from the linear objective lens is shown in Fig. 2B of Baker below, and the panoramic image obtained from the non-linear objective lens is shown in Fig 3BB of Baker below: <br> fig. 20 <br> Fig. $30 D$ <br> Comparing the image in Fig. 2B (linear image) to the image in Fig. 3BB (non-linear image) shows how zone $X$ ' has been substantially compressed and zone $Y$ ' has been substantially expanded. Thus, the panoramic image obtained from the non-linear objective lens (Fig. 3BB) depicts a substantially expanded zone $Y$ ' and a substantially compressed zone $X$ ' compared to the panoramic image obtained from the linear objective lens (Fig. 2B). (Col. 12, Ins. 29-32). |

Appendix B

| 2. The method according to claim 1 , wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point. | Fig. 3BA of Baker shows that the distribution function of the lens depicted in Fig. 3BA is symmetrical with respect to the optical axis of the lens, as the height of an image point relative to the center of the image varies according to the field angle. |
| :---: | :---: |
| 4. The method according to claim 1 , wherein the objective lens expands the edges of the image and compresses the center of the image. | "The lens uniquely achieves this by filling the greater available area of an imager device with the peripheral areas rather than the central areas of the captured scene." (Col. 10, Ins. 57-60). "The lens constructed according to the present invention has a fairly significant portion of the imaging surface dedicated to the peripheral field, and consequently less of the surface dedicated to the central field." (Col. 12, lns, 29-32). See also Fig. 3BB of Baker as compared to Fig. 2 thereof, which shows the expansion of the periphery of the image and compression of the center. |
| 6. The method according to claim 1 , wherein the objective lens comprises a set of lenses forming an apodizer. | As described in the '990 Patent, an "apodizer" is an optical system which provides a non-linear distribution of image points relative to the field angle of the object points. (Col. 16, lns. 1-4). The hemispherical lens elements at bottom of Fig. 3BA comprise an "apodizer," as defined in the ' 990 Patent, as they control the angular distribution of the panoramic objective lens to obtain the desired nonlinearity. |
| 17. A panoramic objective lens comprising: | Baker discloses "the visual imaging system can use a single camera to capture the relevant visual information within a panoramic field of view existing along the horizon." (COI. 6, Ins. 29-32). |
| optical means for projecting a panorama into an image plane of the objective lens, | Baker discloses projecting a panorama onto an image sensor by means of a panoramic objective lens, and that a "CCD" may be used for digital storage. (Col. 13, Ins. 14-17). |
| the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama, | Fig. 2 A of Baker depicts a lens having a typical linear distribution function of image points, while Fig. 3BA of Baker depicts a lens having a non-linear distribution function of image points, relative to the field angle of the object points of the panorama. (Col. 12, Ins. 23-25). <br> Baker further discloses the "fundamental principle behind the enhanced peripheral content lens is the selective magnification of the periphery and |

## Appendix B

|  | the focusing of more of that content on the imaging plane." (Fig. 3BA; col. 10, Ins. 38-41). Baker further discloses a non-linear "lens, indicated generally at 14 , designed to capture and enhance the peripheral content of a hemispheric scene." (Col. 8, Ins. 60-62). "To maximize data collection and resolution for analysis and/or display of the relevant visual information located in this portion of the hemispheric scene, it is desirable to maximize the dedication of the available image detection area to this peripheral field portion." (Col. 8, Ins. 32-36). |
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| the distribution function having a maximum divergence of at least.t-. $10 \%$ compared to a linear distribution function, | Baker discloses a panoramic objective lens with a distribution function having a maximum divergence of at least $\pm 10 \%$ compared to a linear distribution function. "[I]f an ordinary fisheye lens focuses the lowest 15 degrees up from the horizon on ten percent of the imager at the imaging plane and the peripheral-enhancing lens focuses that same 15 degrees on fifty percent of the imager, there is a five-fold increase in resolution using the same imaging device. Depending on the application and exact formulation of the lens equations, there will be at least a five times increase in resolving power by this lens imager combination." (Col. 6, Ins. 48-56). <br> Using a normalized height of 1 at $90^{\circ}$, one can calculate the height $h$ at $75^{\circ}$ for the circumstance in which $50 \%$ of the imager is occupied by the lowest $15^{\circ}$. That is, half of the area of the entire circular image is equal to the area of a circle with height $h$ at $75^{\circ}$, or $(1)^{2} / 2=h^{2}$, which gives a height $h$ of about 0.707 . This is a divergence of greater than $10 \%$ compared to a linear distribution function, which would have a height $h$ at $75^{\circ}$ of about 0.833. |
| such that a panoramic image obtained by means of the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone. | Baker discloses "The lens uniquely achieves this by filling the greater available area of an imager device with the peripheral areas rather than the central areas of the captured scene." (Col. 10, Ins. 57-60). "[T]he lens constructed according to the present invention has a fairly significant portion of the imaging surface dedicated to the peripheral field, and consequently less of the surface dedicated to the central field." (Col. 12, Ins. 29-32). The panoramic image obtained from the linear objective lens is shown in Fig. 2B of Baker below, and the panoramic image obtained from the non-linear objective lens is shown in Fig 3BB of Baker below: |

## Appendix B

|  | Comparing the image in Fig. 2B (linear image) to the image in Fig. 3BB <br> (non-linear image) shows how zone X' has been substantially compressed <br> and zone Y' has been substantially expanded. Thus, the panoramic image |
| :--- | :--- |
| obtained from the non-linear objective lenss (Fig. 3BB) depicts a |  |
| substantially expanded zone Y' and a substantially compressed zone X' |  |
| compared to the panoramic image obtained from the linear objective lens |  |
| (Fig. 2B). (Col. 12, Ins. 29-32). |  |

## Appendix B

|  | elements at bottom of Fig. 3BA comprise an "apodizer," as defined in the <br> 'g90 Patent, as they control the angular distribution of the panoramic <br> objective lens to obtain the desired nonlinearity. |
| :--- | :--- |

## APPENDIX A

## Appendix A

## Claim Analysis Chart of U.S. Patent $\mathrm{N} 0.6,844,990$ B2 ("the ' 990 patent")

Detailed Explanation of Pertinency of Nagaoka

The ${ }^{6} 990$ Patent
Prior Art

| 1. A method for capturing a digital panoramic image, | Nagaoka discloses a panoramic objective lens and a method for capturing a digital panoramic image: "...an image processing system utilizing an image pickup device comprising a fisheye lens..." (Col. 3, Ins. 63-65). Nagaoka further discloses a panoramic objective lens: "an image of half of the sphere is picked up by the fisheye lens." (Col. 1, Ins. 23-31). Digital image data can be stored, e.g., on a flashcard. (Col. 9, lns. 18-21). |
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| by projecting a panorama onto an image sensor by means of a panoramic objective lens, | Nagaoka discloses that the panorama is projected onto a CCD image sensor by a panoramic objective lens. (Fig. 2; col. 4, ln. 66-col. 5, ln. 2). |
| the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, | Nagaoka discloses several panoramic (fisheye) lenses each having an image point distribution function that is not linear relative to the field angle of object points of the panorama. Specifically, Nagaoka discloses examples of such non-linear lenses have the functions $h=1.2 f \cdot \tan (/ 1.6)$ and h=1.6f $\tan (12)$. (Figs. 3A and 3B). |
| the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, | Each of the above recited non-linear distribution functions lenses has a maximum divergence of at least $\pm 10 \%$ compared to the linear distribution function. (Figs. 3 A and 3 B ). Using a normalized image height (height $=$ 1 at $90^{\circ}$ ), the function $h=1.2 \mathrm{f} \tan (/ 1.6)$ gives $h$ of about 0.36 at $45^{\circ}$, which is about $18 \%$ divergence from the linear distribution function $f$ (which would be 0.45 at $45^{\circ}$ ). Similarly, the function $h=1.6 f \cdot \tan (12)$ gives a divergence at $45^{\circ}$ of about $16 \%$. |
| such that the panoramic image obtained has at least one substantially expanded zone and at least one substantially compressed zone. | The lenses having the functions $\mathrm{h}=1.2 \mathrm{f} \cdot \tan (/ 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \cdot \tan (/ 2)$ project a substantially expanded zone near the periphery (evidenced from Fig. 3B, which shows a slope for these two functions exceeding the slope of the linear distribution function ( f ) starting at about $60^{\circ}$ ) and a substantially compressed zone near the center (evidenced from Fig. 3B, which shows a slope for these two functions that is less than the slope of the linear distribution function (f) prior to about $60^{\circ}$ ). |
| 2. The method according to claim 1 , wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to | Fig. 2 of Nagaoka shows a lens having a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens. In the lenses having functions $\mathrm{h}=1.2 \mathrm{f} \cdot \tan (/ 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \cdot \tan (12)$ the nonlinear distribution function is symmetrical relative to the optical axis and |

Appendix A

| the center of the image varying according to the field angle of the corresponding object point. | the positions of points relative to the center of the image are based on the field angle of the corresponding object point. See also Figs. 4A-4D, showing the intent to have symmetry about the optical axis $\left(0^{\circ}\right)$ and variance of position according to field angle. |
| :---: | :---: |
| 4. The method according to claim 1 , wherein the objective lens expands the edges of the image and compresses the center of the image. | As described above with respect to claim 1, Fig. 3B shows that the functions $\mathrm{h}=1.2 \mathrm{f} \cdot \tan (/ 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \cdot \tan (12)$ have a shallower slope as compared to the linear distribution function closer the center of the image, and a steeper slope relative to the linear distribution function near the periphery, evidencing an expanded edge of the image and a compressed center. |
| 6. The method according to claim 1 , wherein the objective lens comprises a set of lenses forming an apodizer. | As described in the " 990 Patent, an "apodizer" is an optical system which provides a non-linear distribution of image points relative to the field angle of the object points. (Col. 16, Ins. 1-4). As shown in Fig. 2 of Nagaoka, the lens system controls the angular distribution of the panoramic objective lens to obtain a non-linear distribution function, and therefore includes an "apodizer" as defined in the " 990 Patent. |
| 17. A panoramic objective lens comprising: | Nagaoka discloses a panoramic objective lens and a method for capturing a digital panoramic image: "...an image processing system utilizing an image pickup device comprising a fisheye lens..." (Col. 3, Ins. 63-65). Nagaoka further discloses a panoramic objective lens: "an image of half of the sphere is picked up by the fisheye lens." (Col. 1, Ins. 23-31). |
| optical means for projecting a panorama into an image plane of the objective lens, | Nagaoka discloses that the panorama is projected onto a CCD image sensor by a panoramic objective lens. (Fig. 2; col. 4, ln. 66-col. 5, ln. 2). |
| the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama, | Nagaoka discloses several panoramic (fisheye) lenses each having an image point distribution function that is not linear relative to the field angle of object points of the panorama. Specifically, Nagaoka discloses examples of such non-linear lenses have the functions $h=1.2 f \cdot \tan (11.6)$ and h=1.6f $\tan (/ 2)$. (Figs. 3A and 3B). |
| the distribution function having a maximum divergence of at least.t-. $10 \%$ compared to a linear distribution function, | Each of the above recited non-linear distribution functions lenses has a maximum divergence of at least $\pm 10 \%$ compared to the linear distribution function. (Figs. 3A and 3B). Using a normalized image height (height $=$ 1 at $90^{\circ}$ ), the function $h=1.2 \mathrm{f} \tan (/ 1.6)$ gives $h$ of about 0.36 at $45^{\circ}$, which is about $18 \%$ divergence from the linear distribution function f |

## Appendix A

|  | (which would be 0.45 at $45^{\circ}$ ). Similarly, the function $h=1.6 f \cdot \tan (/ 2)$ gives a divergence at $45^{\circ}$ of about $16 \%$. |
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| such that a panoramic image obtained by means of the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone. | The lenses having the functions $\mathrm{h}=1.2 \mathrm{f} \tan (11.6)$ and $\mathrm{h}=1.6 \mathrm{f} \tan (/ 2)$ project a substantially expanded zone near the periphery (evidenced from Fig. 3B, which shows a slope for these two functions exceeding the slope of the linear distribution function $(\mathrm{f})$ starting at about $60^{\circ}$ ) and a substantially compressed zone near the center (evidenced from Fig. 3B, which shows a slope for these two functions that is less than the slope of the linear distribution function ( f ) prior to about $60^{\circ}$ ). |
| 18. The panoramic objective lens according to claim 17 , having a non-IInar distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of an image obtained varying according to the field angle of the corresponding object point. | Fig. 2 of Nagaoka shows a lens having a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens. In the lenses having functions $\mathrm{h}=1.2 \mathrm{f} \cdot \tan (/ 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \cdot \tan (/ 2)$ the nonlinear distribution function is symmetrical relative to the optical axis and the positions of points relative to the center of the image are based on the field angle of the corresponding object point. See also Figs. 4A-4D, showing the intent to have symmetry about the optical axis $\left(0^{\circ}\right)$ and variance of position according to field angle. |
| 20. The panoramic objective lens according to claim 17 , wherein the lens expands the edges of an image and compresses the center of the image. | As described above with respect to claim 1, Fig. 3B shows that the functions $\mathrm{h}=1.2 \mathrm{f} \tan (/ 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \tan (12)$ have a shallower slope as compared to the linear distribution function closer the center of the image, and a steeper slope relative to the linear distribution function near the periphery, evidencing an expanded edge of the image and a compressed center. |
| 22. The panoramic objective lens according to claim 17 , further comprising a set of lenses forming an apodizer. | As described in the " 990 Patent, an "apodizer" is an optical system which provides a non-linear distribution of image points relative to the field angle of the object points. (Col. 16, Ins. 1-4). As shown in Fig. 2 of Nagaoka, the lens system controls the angular distribution of the panoramic objective lens to obtain a non-linear distribution function, and therefore includes an "apodizer" as defined in the "990 Patent. |

## EXHIBIT 7b

## CERTIFICATION

I, Takayoshi Hongo, Toranomon East Bldg., No. 7-13, Nishi-Shimbashi 1-chome, Minato-ku, Tokyo, Japan, do hereby certify that $I$ am conversant with the English and Japanese languages and am a competent translator thereof, and I further certify that to the best of my knowledge and belief the attached English translation is a true and accurate translation made by me of the Japanese Unexamined Patent Application Publication JP 11-261868 published on September 24, 1999.

Signed this on the 20 th day of March, 2014

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## EXHIBIT 6b

# VERIFICATION OF TRANSLATION 

I, Karen McGillicuddy
of 1950 Roland Clarke Place
Reston, VA 20191
declare that I am well acquainted with both the Japanese and English languages, and that the attached is an accurate translation, to the best of my knowledge and ability, of Japanese Patent Laid-open Publication No. 2000-242773, published September 8, 2000.


## (12) Laid-Open Patent Publication (A)

(19) Japan Patent Office (JP)
(11) Patent Application Publication No.

2000-242773
(P2000-242773A)
(43) Published September 8, 2000

| (51) | Int. Cl. ${ }^{6}$ ID No. | F1 |  | Theme Code (Ref.) |
| :---: | :---: | :---: | :---: | :---: |
|  | G06T 3/00 | G06F 15/66 | 360 | 5 B 057 |
|  | // H04N 5/225 | H04N 5/225 | C | 5 C 022 |

Request for Examination Requested No. of Claims: 7 OL (Total of 8 page(s))
(21) Application No. H11-41002
(71) Applicant 594066648
Yugen Kaisha FIT
(22) Application Date February 19, 1999

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Okayama-shi, Okayama-ken cont'd on last page

## (54) [TITLE OF INVENTION] <br> IMAGE DATA CONVERSION DEVICE

## (57) [ABSTRACT]

[PROBLEM] To convert image capture data of a full surrounding area obtained by a fish-eye lens such that distortion can be corrected and the image capture data can be displayed as a seamless single image.
[MEANS FOR SOLVING THE PROBLEM] With respect to a region for a portion of circular image data obtained by image capture using a fish-eye lens, a point $(g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \sin \psi)$ in the region on a planar Cartesian coordinate system whose origin point is a center of the circular image (where $\Theta$ is a parameter fulfilling $0<\Theta<\pi / 2 ; g(\Theta)$ is a function fulfilling $g(0)=0$ and monotonically increasing in the range of $\Theta$; and $\psi$ is an angle formed by a line segment and a coordinate axis on the planar Cartesian coordinate system, the line segment linking the origin point of the planar Cartesian coordinate system and
 the point on the circular image) is converted into a point ( $R, \psi, R / \tan \Theta$ ) on a cylindrical coordinate system where R is a constant.

## [SCOPE OF THE CLAIMS]

[CLAIM 1] An image data conversion device wherein, with respect to a region for a portion of circular image data obtained by image capture using a fish-eye lens, a point $(g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \sin \psi)$ in the region on a planar Cartesian coordinate system whose origin point is a center of the circular image (where $\Theta$ is a parameter fulfilling $0<\Theta<\pi / 2 ; \mathrm{g}(\Theta)$ is a function fulfilling $g(0)=0$ and monotonically increasing in the range of $\Theta$; and $\psi$ is an angle formed by a line segment and a coordinate axis on the planar Cartesian coordinate system, the line segment linking the origin point of the planar Cartesian coordinate system and the point on the circular image) is converted into a point $(\mathrm{R}, \psi, \mathrm{R} / \tan \Theta)$ on a cylindrical coordinate system where R is a constant.
[CLAIM 2] The image data conversion device according to claim 1, wherein the fish-eye lens has a property in which $\mathrm{h}=\mathrm{g}(\theta)$ ( h being an image height and $\theta$ being a field angle).
[CLAIM 3] The image data conversion device according to claim 2, wherein the function $g(\theta)$ is $g(\theta)=2 f \cdot \tan (\theta / 2)$ ( $f$ being a focal distance).
[CLAIM 4] The image data conversion device according to claim 2, wherein the function $g(\theta)$ is $g(\theta)=f \cdot \theta$ ( $f$ being a focal distance).
[CLAIM 5] A computer-readable storage medium storing a program executing operations of the image data conversion device according to any one of claims 1 to 4 on the computer.
[CLAIM 6] An image capture system comprising:
the fish-eye lens;
a conversion means converting an image obtained by the fish-eye lens into the image data;
the image data conversion device according to any one of claims 1 to 4 ; and a display means displaying the image data on the cylindrical coordinate plane by projecting the image data onto a plane, the image data on the cylindrical coordinate plane having been converted by the image data conversion device.
[CLAIM 7] An image data conversion method wherein, with respect to a region for a portion of circular image data obtained by image capture using a fish-eye lens, a point $(g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \sin \psi)$ in the region on a planar Cartesian coordinate system whose origin point is a center of the circular image (where $\Theta$ is a parameter fulfilling $0<\Theta<\pi / 2$; $\mathrm{g}(\Theta)$ is a function fulfilling $g(0)=0$ and monotonically increasing in the range of $\Theta$; and $\psi$ is an angle formed by a line segment and a coordinate axis on the planar Cartesian coordinate system, the line segment linking the origin point of the planar Cartesian coordinate system and the point
$\{130504902051422 . D O C\} 2$
on the circular image) is converted into a point $(\mathrm{R}, \psi, \mathrm{R} / \tan \Theta)$ on a cylindrical coordinate system where R is a constant.

## [DETAILED DESCRIPTION OF THE INVENTION]

[0001]
[Technical Field of the Invention] The present invention relates to an image data conversion device and, specifically, relates to a device converting image data having a circular shape and obtained by image capture with a fish-eye lens into planar image data in which distortion is corrected and wide area display is possible.
[0002]
[Prior Art] Conventionally, in an in-store surveillance camera, a traffic regulating camera, and the like, in order to monitor a status of a surrounding area, a camera having a field of view that is limited to a forward view is typically rotated by a drive device such as a motor. However, when such a camera having a limited field of view is rotated, a rotation driver becomes necessary, and thus the device becomes complex. In addition, the camera must be rotated when a specific target is to be captured and so when the target is moving, it may not be possible to capture the target due to limitations of rotation speed. Furthermore, a plurality of directions cannot be imaged simultaneously, constantly resulting in blind spots in a monitored area, and therefore such a camera cannot be said to be sufficient for a monitoring function and the like.

10003] Japanese Patent Publication No. H06-501585 suggests, as a technology resolving such problems, converting image data having a circular shape into a planar image, the image data being obtained by capturing an image of all orientations forward of a fish-eye lens. A simple description of the technology follows. The circular image data obtained by the fisheye lens can include an image of all orientations, but the image becomes more distorted further toward an outer periphery. This distortion can be largely removed when the circular image data is translated onto a hemisphere surface, but image data translated to the hemisphere surface cannot be displayed on a planar monitor. In the above technology, the portion of the image data translated to the hemisphere surface is further projected onto a planar surface, thereby enabling the image data to be displayed by conversion into a plane. By using such a method, a device can be simplified by making a rotation drive mechanism unnecessary, and switching a display direction simply becomes a matter of control during data processing, and thus can also be sped up remarkably.
[0004]
[Problem to Be Solved by the Invention] However, even when circular image data obtained in this way by the fish-eye lens is configured to be converted directly into planar image data, an entire hemisphere surface cannot be projected onto a single planar surface with adequate distortion correction, and therefore the image obtained relates only to a specific direction. Accordingly, blind spots occur on a display screen even though the full surrounding area is captured by the fish-eye lens. In addition, as a method to eliminate blind spots, a method performing planar image conversion for a plurality of directions simultaneously and performing simultaneous display can be considered. However, in such a case, seams between images are not continuous and a plurality of different image conversions must be performed.
[0005] In order to resolve these problems, the present invention has as an object to convert image capture data of a full surrounding area obtained by a fish-eye lens such that distortion can be corrected and the image capture data can be displayed as a seamless single image.
[0006]
[Means for Solving the Problems] In order to resolve the above-noted problems, with respect to a region for a portion of circular image data obtained by image capture using a fish-eye lens, an image data conversion device according to the present invention converts a point $(g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \sin \psi)$ in the region on a planar Cartesian coordinate system whose origin point is a center of the circular image (where $\Theta$ is a parameter fulfilling $0<\Theta<\pi / 2$; $g(\Theta)$ is a function fulfilling $g(0)=0$ and monotonically increasing in the range of $\Theta$; and $\psi$ is an angle formed by a line segment and a coordinate axis on the planar Cartesian coordinate system, the line segment linking the origin point of the planar Cartesian coordinate system and the point on the circular image) into a point $(\mathrm{R}, \psi, \mathrm{R} / \tan \Theta)$ on a cylindrical coordinate system where R is a constant. Moreover, what is referred to as a fish-eye lens in the present invention includes not only what is typically called a fish-eye lens, having a viewing angle of substantially $180^{\circ}$, but also includes what is typically called a wide-angle lens, having a narrower viewing angle.
[0007] Moreover, the conversion is sufficient when a conversion is performed that, as a result, satisfies the above-noted relationship and the process of the conversion is not discussed. In other words, the above-noted formula need not be applied directly, and cases are also included where conversion is performed using a table showing correspondence between pre-conversion pixels and post-conversion pixels. In addition, the planar Cartesian coordinate system and the cylindrical coordinate system are mutually independent and directions of the coordinates can be defined as desired. In addition, the cylindrical coordinate
\{J305049 02051422.DOC\}4
system where $R$ is a constant forms a cylindrical surface. However, herein, cases are also included where the above-described conversion is performed by projecting the image as a plane.
[0008] When configured in this way, first, when $\psi$ is fixed and $\Theta$ is increased from a small value to a large value within a range where the point $(g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \sin \psi)$ is in the region for the portion of the circular image data, a line segment oriented in a radial direction from the center of the circular image data is converted into the cylindrical coordinate system where $R$ is a constant (i.e., as a line segment oriented from up to down on a cylindrical surface of radius R ). This conversion is further performed for $\psi$ in a maximum range of $360^{\circ}$ such that the above-noted point is in the region for the portion of the circular image data. Therefore, the portion of the circular image data is smoothly converted into a cylindrical surface in a form where distortion is corrected, the portion of the circular image data including image data for a full surrounding area centered on the fish-eye lens and captured by the fish-eye lens. The image converted into a cylindrical surface can be readily made into a planar image by projecting the cylindrical surface. Therefore, distortion of the image capture data of the full surrounding area obtained by the fish-eye lens can be corrected and the image capture data can be displayed as a seamless single image.
[0009] In addition, when the fish-eye lens has a property in which $\mathrm{h}=\mathrm{g}(\theta)$ (h being an image height and $\theta$ being a field angle), an amount that $g(\Theta)$ increases accompanying an increase of $\Theta$ is the same as the amount that the image height $h$ increases. Accordingly, in other words, changing $\Theta$ is the same as changing the field angle $\theta$. In such a case, the circular image is converted into an ideal, undistorted hemisphere surface and, moreover, an image can be obtained in which a converted hemisphere surface image is projected with respect to the cylindrical surface using light projected from a center point of the hemisphere surface and oriented in a radial direction, the cylindrical surface being positioned such that a center axis matches the center axis of the hemisphere surface. Accordingly, an image capture region spanning the entire area on the sides of the fish-eye lens (i.e., an image on an outer peripheral side of the circular image) is converted into an image with almost no distortion. [0010] In addition, when the function $g(\theta)$ indicating a property of the fish-eye lens is $g(\theta)$ $=2 \mathrm{f} \cdot \tan (\theta / 2)$ (where f is a focal distance), an amount of data for the image on the outer peripheral side of the circular image data is greater. Therefore, reproducibility during conversion into a cylindrical surface of an image capture area spanning the entire area on the sides of the fish-eye lens can be improved.
[0011] Moreover, when the function $g(\theta)$ indicating a property of the fish-eye lens is $g(\theta)=$ $\mathrm{f} \cdot \theta$ (where f is a focal distance), the property is that of the most typically used fish-eye lens. Therefore, a low-cost, mass-produced fish-eye lens can be used and cost of the device can be reduced.
[0012] The image data conversion device can also be achieved by installing a program executing the operations of the image data conversion device onto a computer, and the program can be stored on a storage medium readable by the computer.
[0013] Moreover, in order to resolve the above problems, an image capture system according to the present invention includes the fish-eye lens; a conversion means converting an image obtained by the fish-eye lens into the image data; the image data conversion device according to any one of claims 1 to 4 ; and a display means displaying the image data on the cylindrical coordinate plane as a plane by projecting the cylindrical coordinate plane, the image data on the cylindrical coordinate plane having been converted by the image data conversion device.
[0014] According to such a configuration, the image capture system, as described above, displays the image on the cylindrical surface by projecting the image as a plane, the image data conversion device having corrected distortion of the image and converted the image to remove seams. Therefore, a situation of a surrounding area captured by the fish-eye lens can be entirely shown on one screen. Moreover, the projected plane also includes cases where the projected plane is processed as appropriate, e.g., a case where the projected plane is cut at a predetermined position and each cut section is arrayed as appropriate for display.
[0015] Also, in order to resolve the above-noted problems, with respect to a region for a portion of circular image data obtained by image capture using a fish-eye lens, an image data conversion method according to the present invention converts a point $(g(\Theta) \cdot \cos \psi$, $g(\Theta) \cdot \sin \psi)$ in the region on a planar Cartesian coordinate system whose origin point is a center of the circular image (where $\Theta$ is a parameter fulfilling $0<\Theta<\pi / 2 ; g(\Theta)$ is a function fulfilling $g(0)=0$ and monotonically increasing in the range of $\Theta$; and $\psi$ is an angle formed by a line segment and a coordinate axis on the planar Cartesian coordinate system, the line segment linking the origin point of the planar Cartesian coordinate system and the point on the circular image) into a point ( $\mathrm{R}, \psi, \mathrm{R} / \tan \Theta$ ) on a cylindrical coordinate system where R is a constant. The image data conversion method also smoothly converts the portion of the circular image data into a cylindrical surface in a form where distortion is corrected, the portion of the circular image data including image data for a full surrounding area centered on the fish-eye lens and captured by the fish-eye lens. Therefore, distortion can be corrected
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and the image capture data for the full surrounding area obtained by the fish-eye lens can be displayed seamlessly.
[0016]
[Mode for Carrying out the Invention] Hereafter, a description of an embodiment of the present invention is given with reference to the drawings. Fig. 1 shows a block diagram illustrating a configuration of an image capture system according to the embodiment of the present invention. The image capture system is configured with a camera portion 1 , a data converter 2, a first image memory 3 , a second image memory 4 , an $\mathrm{A} / \mathrm{D}$ converter 5 , a $\mathrm{D} / \mathrm{A}$ converter 6, and a monitor 7.
[0017] The camera portion 1 uses a fish-eye lens 11 as a lens and is capable of image capture at a field angle of $90^{\circ}$ or more at least with respect to an optical axis of the lens. Herein, a fish-eye lens is used having a property wherein

$$
\begin{equation*}
\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 2) \tag{1}
\end{equation*}
$$

When a lens having such a property is used, an amount that an image height $h$ increases relative to an increase in the field angle $\theta$ becomes greater in comparison to a typical lens where $h=f \cdot \theta$. Therefore, an amount of information can be greater for a range having a large field angle $\theta$ (i.e., a periphery of a circular image obtained by the fish-eye lens). The circular image obtained by the fish-eye lens 11 having this property is converted into an electronic signal by a CCD 12 for each RGB value of each pixel and is output to the A/D converter 5 . Herein, the CCD is, for example, a CCD using $1280 \times 1024$ pixels.
[0018] The A/D converter 5 converts an analog signal transmitted from the CCD 12 into a digital signal and outputs the signal to the first image memory 3. The first image memory 3 is configured with a RAM and stores RGB values for each pixel based on the digital signal representing the transmitted circular image. The data converter 2 is equivalent to an image data conversion device according to the present invention and is configured with an arithmetic circuit performing calculations described below. The data converter 2 converts the circular image data stored in the first image memory 3 into cylindrical image data using a conversion described in detail hereafter, then outputs the image data to the second image memory 4.
[0019] The second image memory 4 is again configured with a RAM, and the RGB values for each pixel of the output image data are stored as a plane, described hereafter, onto which the cylindrical surface is projected. In addition, the image onto which the cylindrical surface is projected is long in a width direction. Therefore, in order to obtain the display data
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described below, when storing image data, the second image memory 4 stores the projected image such that the image is divided into halves and placed at a predetermined vertical interval. The D/A converter 6 reads the image data having digital values stored in the second image memory 4 and converts the image data into an analog signal, then transmits the analog signal as an image signal in order of scan lines of the monitor 7. The monitor 7 displays the image stored in the second image memory 4 based on the image signal transmitted by the D/A converter 6 .
[0020] Moreover, portions of the present image capture system except the camera portion 1 can be achieved by installing a program to accomplish the above-noted functions and the below-noted operations on a typical computer. The program can be stored on a storage medium such as a floppy disk that is readable by the computer. In addition, the program can be installed on the computer through a communication means such as the Internet.
[0021] At this point, a conversion method of the data converter 2 is described in detail. The data converter 2 converts the image data on the circular surface onto a cylindrical surface. A correspondence relationship between points on the circular surface and points on the cylindrical surface is described with reference to Figs. 2 and 3. Fig. 2 is a view showing a relationship between a desired point $P 0$ on a hemisphere surface $O$, which supposes an ideal full circumferential surface captured by the fish-eye lens 11 , and a point P 2 on the cylindrical surface C, which is the converted surface. In Fig. 2, in an xyz coordinate system, the hemisphere surface $O$ has a base circle (a circle configuring an edge of the hemisphere surface) positioned on an $x y$ plane and centered on the origin point. A $z$ axis coincides with the optical axis of the fish-eye lens 11. Furthermore, the cylindrical surface C is a cylinder of radius R axially centered on the z axis. In other words, the cylindrical surface C can be represented as a curved surface in an r $\psi z$ cylindrical coordinate system where R is constant. In addition, herein, points on the cylindrical surface C are represented by $(\mathrm{R}, \psi, \mathrm{z})$ as points on the r $\psi z$ cylindrical coordinate system. However, $\psi$ is an angle formed by a line segment and an x axis, the line segment being created by the origin point and a point of intersection between a vertical line down to the xy plane and the xy plane. Also, P2 is a point where a straight line extension of a line segment linking the origin point with the desired point P 0 on the hemisphere surface $O$ intersects with the cylindrical surface $C$. Moreover, an angle formed by the z axis and the line segment linking the origin point with the point P 0 has a field angle $\theta$ with respect to the point P 0 .
[0022] The desired point P 0 on the hemisphere surface O , which supposes the above-noted ideally captured full circumferential surface, indicates a position of a point P1 on a captured
image surface $F$ captured by the fish-eye lens 11 in Fig. 3. A circular region on the captured image surface F in Fig. 3 is a region on the CCD 12 bombarded by light through the fish-eye lens 11, and forms a circular surface S displaying converted image data. In Fig. 3, an origin point on an $X Y$ coordinate system is occupied by the center of the circular surface $S$.

Moreover, directions of the X axis and the Y axis are configured to be opposite from the x axis and the y axis of the xyz coordinate system of Fig. 2. This is in order to handle P0 also being shown in a position inverted top to bottom and left to right because the image captured by the camera portion 1 is inverted top to bottom and left to right. However, the cylindrical surface is arbitrary, and so in an actual conversion there is also liberty in how coordinates are handled. In addition, the position of P 1 is a position at an image height h distance from the origin point where an angle formed by the X axis and a line segment linking the origin point with Pl is $\psi . \mathrm{h}$ is expressed by the above noted formula 1 and is defined by the field angle $\theta$.
[0023] The data converter 2 converts P1 shown in Fig. 3 into P2 shown in Fig. 2. Hereafter, a description is given of a concrete calculation. First, a case is considered where parameters are set to $\theta$ and $\psi$. In this case, the coordinates of P 1 on the XY plane are ( $\mathrm{h} \cdot \cos \psi, \mathrm{h} \cdot \sin \psi$ ) and, when $h$ is substituted out using the above-noted formula 1 , are represented by $(2 f \cdot \tan (\theta / 2) \cdot \cos \psi, 2 \mathrm{f} \cdot \tan (\theta / 2) \cdot \sin \psi)$. Meanwhile, for the coordinates of $\mathrm{P} 2, \mathrm{R}$ is a constant, and $z$ has a relationship according to Fig. 2 in which $z=R / \tan \theta$, and thus the coordinates of P 2 are represented by $(\mathrm{R}, \psi, \mathrm{R} / \tan \theta)$. Accordingly, the parameters $\theta$ and $\psi$ can be moved to specify P 1 on the circular image on the XY plane, and a point on the $\mathrm{r} \psi \mathrm{z}$ cylindrical coordinate system (that is, the point on the cylindrical surface $C$ ) can also be specified with respect thereto. Therefore, the image data can be converted according to a formula that indicates P1 and P2. However, in a case where $\theta=0$, the $z$ coordinate of P2 becomes infinitely large, and therefore in reality a value of $\theta$ is used which is a certain value or more. In the present embodiment, a range of $\pi / 4 \leq \theta<\pi / 2$ is used for $\theta$.
[0024] In an actual conversion, calculation is facilitated by using data directly representing a position of each pixel in the captured CCD 12 or a post-conversion position of each pixel on the converted cylindrical surface $C$ as the parameters. Use of $x$ and $\psi$ as parameters directly representing the post-conversion position of each pixel on the cylindrical surface C is considered. In such a case, when the point P 2 on the cylindrical surface C is represented with the parameters $z$ and $\psi$, the coordinates are ( $\mathrm{R}, \psi, z$ ). The converted cylindrical surface C is projected and displayed on the monitor 7 , and each pixel is aligned at equal intervals of a pixel pitch d in a longitudinal direction and a lateral direction. Fig. 4 illustrates a view representing a relationship between the projected cylindrical surface C and the circular
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surface $S$. The longitudinal direction of the cylindrical surface $C$ coincides with the parameter $z$. Therefore, when a change is made to the parameter $z$ in units of the pixel pitch d, the changes coincide with the longitudinal direction pixel positions of the cylindrical surface $C$. An amount of change accompanying an amount of change in $\psi$ in the lateral direction of the projected cylindrical surface can be represented by $\mathrm{R} \cdot \psi$. Therefore, when the amount of change of the parameter $\psi$ corresponding to the pixel pitch d of the cylindrical surface C is $\Delta \psi$, the amount of change can be represented as $\Delta \psi=\mathrm{d} / \mathrm{R}$. Accordingly, when a change is made to the parameter $\psi$ in units of $d / R$, the change coincides with the lateral direction pixel positions of the cylindrical surface $C$. Moreover, a range where the circular surface $S$ has hatching in the drawings is a range of the circular surface $S$ corresponding to $\pi / 4 \leq \theta<\pi / 2$ and indicates the range converted into the cylindrical surface $C$.
[0025] Meanwhile, representing the point P1 on the circular image using the parameters $z$ and $\psi$ is considered. First, when transforming the above-noted formula (1) using a doubleangle formula for a trigonometric function,

$$
\mathrm{h}=2 \mathrm{f} \cdot \tan (\theta / 2)=2 \mathrm{f} \cdot\{\sin \theta /(1+\cos \theta)\}
$$

results. Fig. 2 shows that $\sin \theta=R /\left(R^{2}+z^{2}\right)^{1 / 2}, \cos \theta=z /\left(R^{2}+z^{2}\right)^{1 / 2}$, and therefore when these are substituted into the formula 1 and simplified, $\left.h=2 f \cdot R /\left\{\left(R^{2}+z^{2}\right)^{1 / 2}+z\right)\right\}$ results. Therefore, as a result, P 1 is $\left.\left.\left(2 \mathrm{f} \cdot \mathrm{R} \cdot \cos \psi /\left\{\left(\mathrm{R}^{2}+\mathrm{z}^{2}\right)^{1 / 2}+\mathrm{z}\right)\right\}, 2 \mathrm{f} \cdot \mathrm{R} \cdot \sin \psi /\left\{\left(\mathrm{R}^{2}+\mathrm{z}^{2}\right)^{1 / 2}+\mathrm{z}\right)\right\}\right)$. Accordingly, as noted above, changes are made to $z$ in units of $d$, and changes are made to $\psi$ in units of $d / R$, then the pixel positions on the circular surface $S$, in which each pixel position on the cylindrical surface $C$ is converted by the formula, can be found. In such a case, the pixel positions obtained by calculation and the pixel positions actually captured by the CCD 12 fail to coincide completely, and therefore the nearest pixel is extracted. Specifically, obtained X coordinate values and Y coordinate values are, for example, divided by a pixel pitch ds of the CCD 12 and those values at or below a decimal point, for example, are discarded. Thereby, the obtained integer value can be extracted as a number for the pixel. Moreover, in such a case, where the origin point of the XY coordinates is (0, 0), each pixel of the CCD 12 is respectively defined with a positive or negative in accordance with each quadrant of the $X Y$ coordinates.
[0026] Using the above method, the data converter 2 calculates the circular surface $S$ pixel position corresponding to each pixel on the post-conversion cylindrical surface $C$, then converts the pixel data of the pixel positions as respective pixel data on the cylindrical surface $C$. As a result, as shown in Fig. 4, the pixel data on the circular surface $S$ is converted
as respective pixel data on the cylindrical surface $C$. Moreover, an unambiguous determination is made as to which pixel position of the cylindrical surface each pixel of the circular image is transformed into. Therefore, the data converter 2 can be provided with a table showing a correspondence between the pixels of the circular image and the pixel positions on the cylindrical surface without performing calculations, and the data conversion can be performed based on this.
[0027] Next, a description is given of operations of the image capture system having the above-noted configuration. Moreover, the camera portion 1 is mounted inside a room, oriented downward from a center of a ceiling. Further, a range of $z$ of the converted cylindrical surface is $0<z \leq R$. In other words, the range of $\theta$ is defined as $\pi / 2>\theta \geq \pi / 4$.

Fig. 5 is a flowchart illustrating operations of the image capture system. First, a panoramic view of the room is captured by the camera portion 1 as a circular image through the fish-eye lens 11. The circular image is converted to an electrical signal by the CCD 12, then is further converted to digital values for each pixel by the $A / D$ converter 5 . Then, this data is stored in the first image memory 3 (s101). Furthermore, 0 is input for each of the parameters $\psi$ and $z$ as an initial value ( s 102 ).
[0028] Next, using the data converter 2, a parameter $\psi i$ is increased in units of $d / R$ until i $=1 \sim \mathrm{n}(\mathrm{n}=2 \pi \mathrm{R} / \mathrm{d})$, and a parameter $z \mathrm{j}$ is increased in units of d until $\mathrm{j}=1 \sim \mathrm{~m}(\mathrm{~m}=\mathrm{R} / \mathrm{d})$.
Then, for each of the values,
$\mathrm{Xi}=\left[2 \mathrm{f} \cdot \mathrm{R} \cdot \cos \psi \mathrm{i} /\left\{\left(\mathrm{R}^{2}+\mathrm{zj}^{2}\right)^{1 / 2}+\mathrm{zj}\right\} \cdot \mathrm{ds}\right]$
$Y j=\left[2 f \cdot R \cdot \sin \psi i /\left\{\left(R^{2}+z j^{2}\right)^{1 / 2}+z j\right\} \cdot d s\right]$
is calculated and, based on the results, ( $\mathrm{Xi}, \mathrm{Yj}$ ) order pixel data stored in the first image memory 3 is extracted and stored in the second image memory 4 as pixel data of the ( $\mathrm{i}, \mathrm{j}$ ) order pixel in the cylindrical surface (s103-s108). Moreover, in the second image memory 4, in order to display the image as shown in Fig. 6 on the monitor 7, the pixels ( $i, j$ ) on the cylindrical surface are divided into two parts, one part in which $\mathrm{i}=1 \sim \mathrm{n} / 2$ and $\mathrm{j}=1 \sim \mathrm{~m}$ and one part in which $\mathrm{i}=(\mathrm{n} / 2)+1 \sim \mathrm{n}$ and $\mathrm{j}=1 \sim \mathrm{~m}$, and are stored so as to obtain an image in which the latter part is positioned so as to be a predetermined interval below the former part. Moreover, text data indicating the angle, shown in Fig. 6, is pre-stored in the second image memory 4.
[0029] The image data stored in the second image memory 4 is output to the monitor 7 as an image signal by the $\mathrm{D} / \mathrm{A}$ converter 6 ( s 109 ) and is displayed by the monitor 7 ( s 110 ). The image data is divided into two parts and formed so as to be positioned vertically, as noted above, and thus a screen shown in Fig. 6 is displayed. In this way, in the image capture

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$$

system according to the present embodiment, footage of an environment in $360^{\circ}$ captured by the fish-eye lens can be fully and seamlessly displayed, and a status of the environment of the lens can be fully monitored without blind spots.
[0030] In the above-described embodiment, a fish-eye lens was used having a property represented by the above formula 1. However, the fish-eye lens may also have a property not represented in formula 1. Specifically, when the property of the fish-eye lens is generalized to $\mathrm{h}=\mathrm{g}(\theta), \mathrm{P} 2$ remains as described above and P 1 can be represented with $(\mathrm{g}(\theta) \cdot \cos \psi$, $g(\theta) \cdot \sin \psi)$. Therefore, in a case where the parameters are $\theta$ and $\psi$, it is sufficient to use the same. Moreover, in a case where the parameters are z and $\psi$, as described above, it is possible to use the expression $\theta=\operatorname{Tan}^{-1}(\mathrm{R} / \mathrm{z})$, per Fig. 2. Therefore, P 2 remains as described above and Pl can be represented with $\left(\mathrm{G}\left(\operatorname{Tan}^{-1}(\mathrm{R} / \mathrm{Z})\right)\right) \cdot \cos \psi, G\left(\operatorname{Tan}^{-1}(\mathrm{R} /\right.$ $z)) \cdot \sin \psi)$. Therefore, similar to the above, corresponding P2 and P1 pixel positions can be found while changing the values of $z$ and $\psi$.
[0031] For example, in a case where a commonly used fish-eye lens having a property in which $h=f \cdot \theta$ is used as the fish-eye lens, it is sufficient to make similar conversions as above in which, when the parameters are $\theta$ and $\psi, \mathrm{P} 1$ is $(f \cdot \theta \cdot \cos \psi, f \cdot \theta \cdot \sin \psi)$, and when the parameters are $z$ and $\psi, P 1$ is $\left.\left(f \cdot G\left(\operatorname{Tan}^{-1}(R / z)\right)\right) \cdot \cos \psi, f \cdot G\left(\operatorname{Tan}^{-1}(R / z)\right) \cdot \sin \psi\right)$. Moreover, $\operatorname{Tan}^{-1}(\mathrm{R} / \mathrm{z})$ can be found using a known regression calculation.
[0032] Moreover, a fish-eye lens having a property in which $h=f \cdot \theta$ can be swapped for the fish-eye lens 11 in the above-described embodiment, while other components remain the same. This is because, although a rate of expansion and contraction of an image in a radial direction differs between the circular image obtained by the fish-eye lens having the property according to the above-noted formula 1 and the fish-eye lens circular image having the property $h=f \cdot \theta$, an adjacency relationship between the images does not change, and therefore the obtained image can fulfill a role as a surveillance image with only minor differences of expansion and contraction appearing in the $z$ direction.

10033] Even more generally, using a monotonically increasing function $g(\Theta)$ in a range where $0<\Theta<\pi / 2$, when P1 is $(g(\Theta) \cdot \cos \psi, g(\Theta) \cdot \sin \psi)$, images are displayed for various kinds of fish-eye lenses, the images differing only in the rate of expansion and contraction in the $z$ direction. In addition, by using, as the function $g(\Theta)$, a function having a least amount of $z$-direction distortion in response to the property of the fish-eye lens being used, a surveillance image that is easier to see can be obtained.
[0034] Further, the image capture system in the above-described embodiment is configured to convert and display an image for all of a $360^{\circ}$ environment captured by the fish-eye lens
$\{30504902051422 . D O C\} 12$
11. However, in a case where the camera portion 1 is installed where a wall meets the ceiling, for example, converting and displaying a $180^{\circ}$ portion excluding the wall direction is sufficient, and in a case where the camera portion 1 is installed in a corner, converting and displaying a $90^{\circ}$ portion excluding the wall directions that enclose the comer is sufficient. In this way, depending on a situation, a range for conversion can be determined as desired.
[0035] In addition, in the image capture system of the above-noted embodiment, the range of $0 \leq \theta<\pi / 4$ is not displayed. However, because this range has a small amount of distortion in the original circular image, the range may also be configured to be matched with the image of the cylindrical surface C and displayed on the monitor 7 as the circular image, without performing conversion.

## [BRIEF DESCRIPTION OF THE DRAWINGS]

[FIG. 1] is a block diagram illustrating a configuration of an image capture system according to an embodiment.
[FIG. 2] is a view showing a relationship between a point on a hemisphere surface, which supposes an ideal full circumferential surface captured by a fish-eye lens, and a point on a converted cylindrical surface.
[FIG. 3] is a view showing a point on a captured image surface corresponding to a point on a hemisphere surface, which supposes an ideal full circumferential surface captured by the fisheye lens.
[FIG. 4] is a view illustrating a projected cylindrical surface.
[FIG. 5] is a flowchart illustrating operations of the image capture system.
[FIG. 6] is a view illustrating a display screen using a monitor.

## [DESCRIPTION OF REFERENCE NUMERALS]

1 Camera portion
2 Data converter
3 First image memory
4 Second image memory
5 A/D converter
6 D/A converter
7 Monitor
11 Fish-eye lens
12 CCD
\{J305049 02051422.DOC \} 13

Fig. 1


Fig. 2

$\{330504902051422$. DOC $\} 14$

Fig. 3


Fig. 4

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Fig. 5


Fig. 6


Continued from front page
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F terms (ref.) 5B057 BA02 BA11 CC02 CD16 CE10
CH01 CH11 DA16
5C022 AA05 AB68

## EXHIBIT 1

${ }^{(12)}$ United States Patent
Artonne et al.
(10) Patent No.: US 6,844,990 B2
(45) Date of Patent:
(54) METHOD FOR CAPTURING AND

DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE
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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.
(21)

Appl. No.: 10/706,513
Filed: Nov. 12, 2003
Prior Publication Data
US 2004/0136092 A1 Jul. 15, 2004

## Related U.S. Application Data

(63) Continuation of application No. PCT/FR02/01588, filed on May 10, 2002.
(30) Foreign Application Priority Data

May 11, 2001 (FR)
. 0106261


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ABSTRACT
A method for capturing a digital panoramic image includes projecting a panorama onto an image sensor by means of a panoramic objective lens. The panoramic objective lens has a distribution function of the image points that is not linear relative to the field angle of the object points of the panorama, such that at least one zone of the image obtained is expanded while at least another zone of the image is compressed. When a panoramic image obtained is then displayed, correcting the non-linearity of the initial image is required and is performed by means of a reciprocal function of the non-linear distribution function of the objective lens or by means of the non-linear distribution function.

26 Claims, 11 Drawing Sheets



Fig. 2




Fig. 7A


Fig. 7B


Fig. 8


Fig. 9


Fig. 10


Fig. 11

Fig. 12

> S1-Acquisition

- Taking a panoramic image by means of a still digital camera or a digital video camera equipped with a panoramic lens having a non-linear distribution function Fd

S2 - Transfer of the image file into a computer

- Transfer of the image file (image disk) into a microcomputer
- Storage in the auxiliary storage (optional)


## S3-Linearisation of the image disk

- Transfer of the image points of the initial image disk into a second virtual image disk comprising more image points than the initial image disk, by means of the function $\mathrm{Fd}^{-1}$

Obtaining a linear image disk
S4-Digitisation

- Transfer of the image points of the second image disk into a system of axes OXYZ in spherical coordinates Obtaining a panoramic image in a hemisphere


## S5 - Interactive display

- Determination of the image points of an image sector to be displayed
- Display of the image sector on a display window
- Detection of the user's actions on a screen pointer or any other control means,
- Detection of the user's actions on keys for image enlargement,
- Modification of the sector displayed (sliding the image sector displayed on the surface of the hemisphere and/or shrinking/expanding the image sector displayed)


Fig. 14

> S1 - Acquisition

- Taking a panoramic image by means of a still digital camera or a digital video camera equipped with a panoramic lens having a non-linear distribution function Fd

S2 - Transfer of the image file into a computer

- Transfer of the image file (image disk) into a microcomputer
- Storage in the auxiliary storage (optional)

S3' - Interactive display with implicit correction of the
non-linearity of the initial image
A - Determination of the colour of the points $E(i, j)$ of an image sector to be displayed using the points $\mathrm{p}(\mathrm{pu}, \mathrm{pv})$ of the image disk:

1. determination of the coordinates $\mathrm{Ex}, \mathrm{Ey}, \mathrm{Ez}$ in the coordinate system OXYZ of each point $E(i, j)$ of the sector to be displayed,
2- determination of the coordinates $\mathrm{Px}, \mathrm{Py}, \mathrm{Pz}$ of points P of the hemisphere corresponding to the points $\mathrm{E}(\mathrm{i}, \mathrm{j})$,
3- calculation of the coordinates, in the coordinate system O'UV of the image disk, of the points $\mathrm{p}(\mathrm{pu}, \mathrm{pv})$ corresponding to the points $P$ of the hemisphere, by means of the function Fd,

B - Presentation of the image sector in a display window,
C - Detection of the user's actions on a screen pointer or any other control means, D - Detection of the user's actions on enlargement keys, E - Modification of the image sector displayed (moving and/or shrinking/expanding the image sector)


Fig. 15


Fig. 16


Fig. 17


## METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE

## CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation of International Application No. PCT/FR02/01588, filed May 10, 2002 the disclosure of which is incorporated herein by reference.

## BACKGROUND OF THE INVENTION

The present invention relates to obtaining digital panoramic images and displaying panoramic images on computer screens.

FIG. 1 represents a classical device allowing a digital panoramic image to be produced and presented on a computer screen. The device comprises a digital camera 1 equipped with a panoramic objective lens 2 of the "fish-eye" type, having an angular aperture on the order of $180^{\circ}$. The camera 1 is connected to a computer 5 , such as a microcomputer for example, equipped with a screen 6. The connection to the microcomputer 5 may be permanent, when, for example, the camera 1 is a digital video camera, or temporary, when, for example, the camera 1 is a still digital camera equipped with an image memory, the connection then being carried out at the time the image files are to be transferred into the microcomputer.

FIG. 2 schematically represents the appearance of a panoramic image 3 obtained by means of the panoramic objective lens 2 . The round appearance of the image is characteristic of the axial symmetry of panoramic objective lenses and the image has dark edges 4 that will subsequently be removed. This digital panoramic image is delivered by the camera 1 in the form of a computer file containing image points coded RGBA arranged in a two-dimensional table, " $R$ " being the red pixel of an image point, " $G$ " the green pixel, "B" the blue pixel, and "A" the Alpha parameter or transparency. The parameters R, G, B, A are generally being coded on 8 bits.

The image file is transferred into the microcomputer 5 which transforms the initial image into a three-dimensional digital image, then presents the user with a sector of the three-dimensional image in a display window 7 occupying all or part of the screen 6 .

FIG. 3 schematically shows classical steps of transforming the two-dimensional panoramic image into a panoramic image offering a realistic perspective effect. After removing the black edges of the image, the microcomputer has a set of image points forming an image disk 10 of center $O$ and axes OX and OY. The image points of the image disk are transferred into a three-dimensional space defined by an orthogonal coordinate system of axes $O^{\prime} X^{\prime} Y^{\prime} Z$, the axis $O^{\prime} Z$ being perpendicular to the plane of the image disk. The transfer is performed by a mathematical function implemented by an algorithm executed by the microcomputer, and leads to obtaining a set of image points referenced in the coordinate system $O^{\prime} X^{\prime} Y^{\prime} Z$. These image points are for example coded in spherical coordinates RGBA $(\phi, \theta)$, $\phi$ being the latitude and $\theta$ the longitude of an image point. The angles $\phi$ and $\theta$ are coded in 4 to 8 bytes (IEEE standard). These image points form a hemisphere 11 when the panoramic objective lens used has an aperture of $180^{\circ}$, otherwise a portion of a hemisphere. The microcomputer thus has a virtual image in the shape of a hemisphere one sector $\mathbf{1 2}$ of which, corresponding to the display window 7 , is presented on the screen (FIG. 1) considering that the observer is on the
central point $\mathrm{O}^{\prime}$ of the system of axes $\mathrm{O}^{\prime} \mathrm{X}^{\prime} \mathrm{Y}^{\prime} \mathrm{Z}$, which defines with the center $\mathrm{O}^{\prime \prime}$ of the image sector 12, a direction $\mathrm{O}^{\prime} \mathrm{O}^{\prime \prime}$ called "viewing direction".
In order to avoid the image sector displayed $\mathbf{1 2}$ having geometrical distortions unpleasant for the observer, the classical panoramic objective lenses must have a distribution function of the image points according to the field angle of the object points of a panorama that is as linear as possible. Therefore, if two points $\mathrm{A}^{\prime}, \mathrm{B}^{\prime}$, situated on the same meridian of the hemisphere 11, and the corresponding points $\mathrm{A}, \mathrm{B}$ on the image disk 10 are considered, the ratio between the angles ( $A^{\prime} O^{\prime} Z$ ) and ( $B^{\prime} O^{\prime} Z$ ) must be equal to the ratio between the distances $O A$ and $O B$ on the image disk.

Due to this property of linearity of a classical panoramic objective lens, image points corresponding to object points having an identical field angle form concentric circles C10, C20 . . C90 on the image disk 10, as represented in FIG. 4A. Classically, "field angle of an object point" means the angle of an incident light ray passing through the object point considered and through the center of the panorama photographed, relative to the optical axis of the objective lens. The field angle of an object point can be between 0 and $90^{\circ}$ for an objective lens having an aperture of $180^{\circ}$. Therefore, the circle C 10 is formed by the image points corresponding to object points having a field angle of $10^{\circ}$, the circle C 20 is formed by image points corresponding to object points having a field angle of $20^{\circ}$, etc., the circle C 90 being formed by the image points having a field angle of $90^{\circ}$.

FIG. 4B represents the shape of the distribution function Fdc of a classical panoramic objective lens, which determines the relative distance dr of an image point in relation to the center of the image disk according to the field angle ax of the corresponding object point. The relative distance dr is between 0 and 1 and is equal to the distance of the image point in relation to the center of the image divided by the radius of the image disk. The ideal form of the function Fde is a straight line of gradient K :

## $d r=F d c(\alpha)=K \alpha$

in which the constant $K$ is equal to 0.111 degree $^{-1}\left(1 / 90^{\circ}\right)$.
This technique of displaying a digital panoramic image sector on a computer screen has various advantages, particularly the possibility of "exploring" the panoramic image by sliding the image sector presented on the screen to the left, the right, upwards or downwards, until the limits of the panoramic image are reached. This technique also allows complete rotations of the image to be carried out when two complementary digital images have been taken and supplied to the microcomputer, the latter thus reconstituting a complete panoramic sphere by assembling two hemispheres. Another advantage provided by presenting a panoramic image on screen is to enable the observer to make enlargements or zooms on parts of the image. The zooms are performed digitally, by shrinking the image sector displayed and expanding the distribution of the image points on the pixels of the screen.

Various examples of interactive panoramic images can be found on the Web. Reference could be made in particular to the central site "http://www.panoguide.com" ("The Guide to Panoramas and Panoramic Photography") which gives a full overview of all the products available to the public to produce these images. Software programs allowing digital panoramic photographs to be transformed into interactive panoramic images are offered to the public in the form of downloadable programs or CD-ROMs available in stores.

Despite the various advantages that this technique for displaying digital images offers, the digital enlargements have the disadvantage of being limited by the resolution of the image sensor used when taking the initial image and the resolution of an image sensor is generally much lower than that of a classical photograph. Therefore, when the enlargement increases, the granulosity of the image appears as the limits of the resolution of the image sensor are being reached.

To overcome this disadvantage, it is well known to proceed with pixel interpolations so as to delay the apparition of the blocks of color which betray the limits of the resolution of the sensor. However, this method only improves the appearance of the enlarged image sector and does not in any way increase the definition. Another obvious solution is to provide an image sensor with a high resolution, higher than the resolution required to present an image sector without enlargement, so that there is a remaining margin of definition for zooms. However, this solution is expensive as the cost price of an image sensor rapidly rises with the number of pixels per unit of area.

Some attempts have been made to improve the quality of the enlargements, by changing the optical properties of the panoramic objective lenses themselves. Thus, U.S. Pat. No. $5,710,661$ teaches capturing a panoramic image with two over locking objective lenses using a set of mirrors. A first set of mirrors provides an overall view, and a mobile central mirror provides a detailed view on a determined zone of the panorama. However, this solution does not offer the same flexibility as digital zooms, particularly when the image is not displayed in real time, as the observer no longer has the possibility of choosing the image portion that he wants to enlarge once the photograph has been taken.

## BRIEF SUMMARY OF THE INVENTION

Therefore, the present invention comprises a method allowing the physical limits of image sensors to be circumvented and the definition offered by digital enlargements concerning certain parts of a digital panoramic image to be improved, without the need to increase the number of pixels per unit of area of an image sensor or to provide an overlooking optical enlargement system in a panoramic objective lens.

The present invention is based on the observation that, in several applications, only certain zones of a panoramic image are of a practical interest and are likely to be expanded by the observer by means of a digital zoom. Thus, in applications such as video surveillance, videoconferencing, visio-conferencing, a panoramic camera can be installed against a wall or on the ceiling and there is generally no reason to make enlargements on the zones of the panoramic image corresponding to the wall or the ceiling. Similarly, as part of a videoconference performed by means of a panoramic camera, the most interesting zone is generally situated at a specific place situated towards the center of the image (in the case of individual use) or on the edges of the image (in the case of collective use or visioconferencing). Furthermore, when used for recreation and leisure, most panoramic images comprise parts that are less interesting than others, such as the parts representing the sky or a ceiling for example, the most useful part generally being in the vicinity of the center of the image.

Therefore, the present invention is based on the premise that a panoramic image has some zones that are not very useful and that can tolerate a reasonable definition to the benefit of other zones of the image.

On the basis of this premise, the idea of the present invention is to produce panoramic photographs by means of e to the fangle of object points of the panorama, the distribution function having a maximum divergence of at least $\pm 10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least one substantially compressed zone.

According to one embodiment, the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.

According to one embodiment, the objective lens expands the center of the image and compresses the edges of the image.

According to one embodiment, the objective lens expands the edges of the image and compresses the center of the image.
5 According to one embodiment, the objective lens compresses the center of the image and the edges of the image, and expands an intermediate zone of the image located between the center and the edges of the image.

According to one embodiment, the objective lens com-
According to one embodiment, the set of lenses forming an apodizer comprises at least one aspherical lens.

According to one embodiment, the set of lenses forming 45

According to one embodiment, the objective lens comprises a set of mirrors comprising at least one distorting mirror.

The present invention also relates to a method for dis50 playing an initial panoramic image obtained in accordance with the method described above, comprising a step of correcting the non-linearity of the initial image, performed by means of a reciprocal function of the non-linear distribution function of the objective lens or by means of the 5 non-linear distribution function.

According to one embodiment, the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.

According to one embodiment, the method comprises a step of calculating the size of the corrected image, by means of the reciprocal function of the distribution function, so that the resolution of the corrected image is equivalent to the 65 most expanded zone of the initial image, and a step of scanning each image point of the corrected image, searching for the position of a twin point of the image point on the
initial image and allocating the color of the twin point to the image point of the corrected image.

According to one embodiment, the initial image and the corrected image comprise an image disk.

According to one embodiment, the method comprises a step of transferring the image points of the corrected image into a three-dimensional space and a step of presenting one sector of the three-dimensional image obtained on a display means.

According to one embodiment, the method comprises a step of determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the non-linear distribution function, and allocating to each image point of the display window the color of an image point that is the closest on the initial image.

According to one embodiment, the projection of the image points of the display window onto the initial image comprises a step of projecting the image points of the display window onto a sphere or a sphere portion, a step of determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and a step of projecting onto the initial image each image point projected onto the sphere or the sphere portion, the projection being performed by means of the non-linear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion.

The present invention also relates to a panoramic objective lens comprising optical means for projecting a panorama into an image plane of the objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $\pm 10 \%$ compared to a linear distribution function, such that a panoramic image obtained by means of the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone.

According to one embodiment, the panoramic objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of an image obtained varying according to the field angle of the corresponding object point.

According to one embodiment, the panoramic objective lens expands the center of an image and compresses the edges of the image.

According to one embodiment, the panoramic objective lens expands the edges of an image and compresses the center of the image.

According to one embodiment, the panoramic objective lens compresses the center of an image and the edges of the image, and expands an intermediate zone of the image located between the center and the edges of the image.

According to one embodiment, the panoramic objective lens comprises a set of lenses forming an apodizer.

According to one embodiment, the set of lenses forming an apodizer comprises at least one aspherical lens.

According to one embodiment, the set of lenses forming an apodizer comprises at least one diffractive lens.

According to one embodiment, the panoramic objective lens comprises polymethacrylate lenses.

According to one embodiment, the panoramic objective lens comprises a set of mirrors comprising at least one distorting mirror.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

The foregoing summary, as well as the following detailed description of preferred embodiments of the invention, will be better understood when read in conjunction with the appended drawings. For the purpose of illustrating the invention, there are shown in the drawings embodiments which are presently preferred. It should be understood, however, that the invention is not limited to the precise arrangements and instrumentalities shown.

In the drawings:
FIG. 1 described above represents a system for displaying a digital panoramic image on a screen;

FIG. 2 described above represents a panoramic image before it is processed by a computer;

FIG. 3 described above shows a classical method for transforming a two-dimensional panoramic image into a three-dimensional digital panoramic image;

FIGS. 4A and 4B described above show the linearity of a classical panoramic objective lens;

FIGS. 5 and 6 show one aspect of the method according to the present invention and respectively represent a distribution of image points obtained with a classical panoramic objective lens and a distribution of image points obtained with a non-linear panoramic objective lens according to the present invention;

FIGS. 7A and 7B show a first example of non-linearity of 30 a panoramic objective lens according to the present invention;

FIG. 8 shows a second example of non-linearity of a panoramic objective lens according to the present invention;

FIG. 9 shows a third example of non-linearity of a 35 panoramic objective lens according to the present invention;

FIG. 10 represents a system for displaying a digital panoramic image by means of which a method for correcting the panoramic image according to the present invention is implemented;

FIG. 11 schematically shows a first embodiment of the correction method according to the present invention;

FIG. 12 is a flow chart describing a method for displaying a panoramic image incorporating the first correction method 45 according to the present invention;

FIG. 13 schematically shows a second embodiment of the correction method according to the present invention;

FIG. 14 is a flow chart describing a method for displaying a panoramic image incorporating the second correction 50 method according to the present invention;

FIG. 15 is a cross-section of a first embodiment of a non-linear panoramic objective lens according to the present invention;

FIG. 16 is an exploded cross-section of a system of lenses present in the panoramic objective lens in FIG. 15;

FIG. 17 is a side view of a lens present in the panoramic objective lens in FIG. 15; and

FIG. $\mathbf{1 8}$ is the diagram of a second embodiment of a 60 non-linear panoramic objective lens according to the present invention.

DETAILED DESCRIPTION OF THE

## INVENTION

5 A-Compression/Expansion of an Initial Image
FIG. 5 schematically represents a classical system for taking panoramic shots, comprising a panoramic objective lens $\mathbf{1 5}$
of optical axis OZ and a digital image sensor $\mathbf{1 7}$ arranged in the image plane of the objective lens 15. Here, four object points $\mathrm{a}, \mathrm{b}, \mathrm{c}, \mathrm{d}$ will be considered that belong to a panorama PM located opposite the objective lens and respectively having angles of incidence $\alpha 1, \alpha 2,-\alpha 2,-\alpha 1$. As explained in the preamble, the field angle of an object point is the angle that an incident light ray passing through the object point considered and through the center of the panorama PM, marked by a point "p" on FIG. 5, has relative to the optical axis OZ of the objective lens. In this example, the angle $\alpha 1$ is equal to two times the angle $\alpha 2$. On the image sensor 17, image points $\mathrm{a}^{\prime}, \mathrm{b}^{\prime}, \mathrm{c}^{\prime}, \mathrm{d}^{\prime}$ corresponding to the object points $\mathrm{a}, \mathrm{b}, \mathrm{c}, \mathrm{d}$ are located at distances from the center of the image respectively equal to $\mathrm{d} 1, \mathrm{~d} 2,-\mathrm{d} 2,-\mathrm{d} 1$. As the distribution of the image points according to the field angle of the object points is linear with a classical panoramic objective lens, the distances d 1 and d 2 are linked by the following relation:

## $d 1 / \alpha 1=d 2 / \alpha 2$

As the angle $\alpha 1$ is here equal to $2 \alpha 2$, it follows that:

$$
\mathrm{d} 1=2 \mathrm{~d} 2
$$

As is well known by those skilled in the art, the term "linearity" here refers to a ratio of proportionality between the distance of an image point measured relative to the center of the image and the field angle of the corresponding object point. The notion of "linearity" in the field of panoramic objective lenses is therefore different from that prevailing in the field of paraxial optics (in the vicinity of the optical axis) when the conditions of Gauss are met.

FIG. 6 represents a system for taking shots of the same type as above, but in which the classical panoramic objective lens $\mathbf{1 5}$ is replaced by an objective lens $\mathbf{1 8}$ according to the present invention, the image sensor 17 being arranged in the image plane of the objective lens 15 . The projection onto the image sensor 17 of the object points $a, b, c, d$ having angles of incidence $\alpha 1, \alpha 2,-\alpha 2$ and $-\alpha 1$ relative to the axis OZ of the objective lens and to the center " $p$ " of the panorama are considered again. On the image sensor 17 , the corresponding image points $a^{\prime \prime}, b^{\prime \prime}, c^{\prime \prime}, d^{\prime \prime}$ are located at distances from the center of the image respectively equal to $\mathrm{d} 1^{\prime}, \mathrm{d} 2^{\prime},-\mathrm{d} 2^{\prime},-\mathrm{d} 1^{\prime}$.

According to the present invention, the objective lens $\mathbf{1 8}$ has a distribution function of the image points that is not linear. The ratio of the distances $\mathrm{d} 1^{\prime}, \mathrm{d} 2^{\prime},-\mathrm{d} 2^{\prime},-\mathrm{d} 1^{\prime}$ are not equal to the ratio of the angles of incidence $\alpha 1, \alpha 2,-\alpha 2$, $-\alpha 1$. In the example represented, the distance $d 2^{\prime}$ is clearly greater than $\mathrm{d}^{1} / 2$, such that the central part of the panoramic image projected onto the image sensor 17 , which corresponds to a solid angle $2 \alpha 2$ centered on the optical axis OZ , occupies a greater area on the image sensor 17 than the area it occupies in FIG. 5 with the classical panoramic objective lens (hatched zone). This central part of the panoramic image is therefore projected onto the image sensor with expansion of its area, in relation to the area the central part would occupy if the objective lens were linear. The result is that the number of pixels of the image sensor covered by this part of the image is greater than in previous practices and that the definition obtained is improved. On the other hand, the part of the image delimited by two circles respectively passing through the points $\mathrm{a}^{\prime \prime}, \mathrm{d}^{\prime \prime}$ and through the points $\mathrm{b}^{\prime \prime}$, $\mathrm{c}^{\prime \prime}$ is compressed relative to the corresponding part in FIG. $\mathbf{5}$, and the definition on the edges of the image is less than that obtained with a classical linear objective lens, to the benefit of the central part of the image.

By applying the principle according to the present invention, which involves expanding one part of the image
and compressing another part of the image, the part to be expanded and the part to be compressed can be chosen according to the intended application, by producing several types of non-linear objective lenses and by choosing an objective lens suited to the intended application. Depending on the intended application, the most useful part of a panoramic image may be located in the center of the image, on the edge of the image, in an intermediate zone situated between the center and the edge of the image, etc.

FIGS. 7A-7B, 8 and 9 show three examples of non-linear distribution functions according to the present invention.

The distribution function shown in FIGS. 7A and 7B corresponds to the example in FIG. 6, that is a panoramic objective lens that expands the image in the center. FIG. 7A represents equidistant concentric circles $\mathrm{C} 10, \mathrm{C} 20, \ldots, \mathrm{C} 90$ present on an image disk, each circle being formed by image points corresponding to object points having the same field angle. The circle C10 is formed by the image points corresponding to object points having a field angle of $10^{\circ}$, the circle C20 is formed by image points corresponding to object points having a field angle of $20^{\circ}$, etc. By comparing FIG. 7A with FIG. 4A described in the preamble, it appears that the circles C10 and C20 are further from the center of the image and further from each other than the circles C10 and C20 obtained with a classical objective lens, while the circles C30 to C90 are closer to each other. This panoramic image thus has an expanded zone in the center and a compressed zone on the edge of the image disk.

FIG. 4B represents the curve of the corresponding distribution function Fd1. The classical linear distribution function, expressed by $\mathrm{Fdc}=\mathrm{K} \alpha$ and in the form of a straight line of gradient $\mathbf{K}$, is also represented as a guide mark (the constant K being equal to $1 / 90$ for an objective lens having an aperture of $180^{\circ}$, i.e., a gradient of 0.111 per degree). The field angle $\alpha$ of the object points is represented on the X -axis and is between 0 and $90^{\circ}$. The relative distance dr of an image point in relation to the center of the image disk is represented on the Y -axis and is between 0 and 1 . The curve of the function Fd1 has a higher gradient than the straight line Fdc for angles $\alpha$ of between 0 and $20^{\circ}$, then a lesser gradient after $20^{\circ}$ and up to $90^{\circ}$. A high gradient means an expansion of the image and a low gradient means a compression of the image.

As demonstrated in this example, the curve Fd1 has a point of maximum divergence $\operatorname{Pd}$ at the angle $\alpha=20^{\circ}$. "Point of maximum divergence" refers to the image point $\operatorname{Pd}(\alpha)$ at which the greatest gap in relative distance dr in relation to a corresponding point $\operatorname{Pdl}(\alpha)$ on the linear distribution straight line K $\alpha$ can be observed. In this example, the point $\operatorname{Pd}\left(\alpha=20^{\circ}\right)$ has a relative distance dr equal to 0.5 relative to the center of the image while the corresponding point $\operatorname{Pdl}\left(\alpha=20^{\circ}\right)$ on the linear curve Fdc has a relative distance dr of 0.222 . The maximum divergence DIVmax of the distribution function $\mathrm{Fd} \mathbf{1}$ according to the present invention can be calculated by a formula of the type:

$$
D V V_{\max } \%=[[d r(P d)-d r(P d T) \backslash \backslash d r(P d \mathbf{1})]]^{* 100}
$$

i.e.:
$D V V_{\max } \%_{\%}=\left[\left[d r(P d)-K^{*} \alpha(P d)\right]\left[K^{*} \alpha(P d)\right]\right]^{*} 100$
In which $\operatorname{dr}(\mathrm{Pd})$ is the relative distance in relation to the center of the point of maximum divergence $\mathrm{Pd}, \mathrm{dr}(\mathrm{Pdl})$ is the relative distance in relation to the center of the corresponding point on the linear distribution straight line Fdc, $\alpha(\mathrm{Pd})$ being the abscissa of the point Pd, i.e., the field angle of the corresponding object point.

In the example considered here, the maximum divergence is therefore equal to $+125 \%$. This value of maximum divergence according to the present invention is clearly higher than that due to the possible design errors or manufacturing errors of a classical panoramic objective lens, which is of a few percent. Generally speaking, a non-linear objective lens according to the present invention has a maximum divergence on the order of $10 \%$ at least, to obtain an expansion of the useful parts of the image which results in a clear increase in the number of pixels of the image sensor covered by the useful parts and a substantial improvement in the definition obtained.

An average rate TX of expansion or compression of one part of the image contained between two circles passing through points $\mathrm{Pd} \mathbf{1}$ and $\mathrm{Pd} \mathbf{2}$ is also defined. The rate TX is the ratio between the area delimited by the two circles passing through the points $\mathrm{Pd} \mathbf{1}, \mathrm{Pd} 2$ and the area delimited by two circles passing through points Pdl1, Pd12 of the same abscissa belonging to the linear distribution function Fdc. The rate TX can be determined by a formula of the type:

$$
\begin{array}{ll} 
& T X=\left[d r(P d \mathbf{1})^{2}-d r(P d \mathbf{2})^{2}\right]\left[(d r(P d \mathbf{1}))^{2}-(d r(P d \mathbf{2}))^{2}\right] \\
\text { i.e.: } & \\
& T X=\left[d r(P d 1)^{2}-d r(P d \mathbf{2})^{2}\right]\left[K^{2}\left[(\alpha(P d \mathbf{1}))^{2}-(\alpha(P d \mathbf{2}))^{2}\right]\right]
\end{array}
$$

A rate TX higher than 1 indicates an expansion of the part of image considered while a rate TX lower than 1 indicates a compression of the part of image considered. In the example of function Fd 1 considered here, the average rate of expansion/compression TX of the central part of the image, delimited by the circle C20, is equal to 5.07 , i.e., an average expansion by a factor 5 of the central part of the image and consequently a $500 \%$ improvement of the definition obtained for a constant number of pixels of the image sensor.

FIG. 8 represents another example of distribution function Fd 2 according to the present invention, here having a point of maximum divergence $\operatorname{Pd}$ at the angle $\alpha=70^{\circ}$, and having a relative distance in relation to the center of the image of 0.3 . The maximum divergence of the curve Fd 2 is $-61.4 \%$ here, and the average rate of expansion/compression TX of the central part of the image delimited by the circle C70 (not represented) is 0.5 , i.e., an average compression by a factor of 0.15 of the central part of the image. The expanded part of the image here is thus located here on the edge of the image, between the circle C70 and the circle C90, and has an average rate of expansion/compression of 2.3. Thus, an image disk obtained with a panoramic objective lens having a distribution function conforming to the function Fd 2 , has a high definition zone on its edges, that lend themselves well to digital enlargements, and a low definition zone in its central part.

FIG. 9 represents a third example of distribution function Fd 3 according to the present invention, having a first point of maximum divergence $\operatorname{Pd} 1\left(\alpha=30^{\circ}, \mathrm{dr}=0,1\right)$ and a second point of maximum divergence $\operatorname{Pd} 2\left(\alpha=70^{\circ}, \mathrm{dr}=0,9\right)$. Thus, two maximum divergences can be seen, one negative and equal to $-70 \%$, and the other positive and equal to $15.8 \%$. A compressed image zone can also be seen between the center O of the image and the circle C 30 passing through the point Pd 1 , an expanded image zone between the circle C30 and the circle C70 passing through the point Pd 2 , and a compressed image zone between the circle C70 and the circle C90 forming the edge of the image disk. The average rates of expansion/compression TX( $\mathbf{0}, \mathrm{C} 30)$, TX(C30, C70), TX(C70, C90) for each of these zones are respectively equal to $0.09,1.6$ and 0.48 . An image disk obtained with a
panoramic objective lens having a distribution function conforming to the function Fd 3 , has a high definition zone in its intermediate part, which lends itself well to digital enlargements, and two low definition zones in its central part and on its edges.
B-Correction of the Non-linearity of the Initial Image
A first aspect of the present invention was described above, according to which a non-linear distribution of image points onto a digital image was provided to improve the definition of the image in expanded zones, by increasing the number of pixels of the image sensor covered by the expanded zones. Before describing examples of embodiments of non-linear panoramic objective lenses according to the present invention, a second aspect of the present invention will be described which involves correcting the nonlinearity of the image disk obtained in order to present the observer with an image free from optical distortion.

This second aspect of the present invention is implemented at the stage of the processing of the initial image by computer, to present an interactive panoramic image on a screen. The means for implementing the method of the present invention are shown in FIG. 10 and are classical in themselves. A digital camera 20 can be equipped with a non-linear panoramic objective lens 21 and connected to a microcomputer 22 comprising a screen 23 . The digital images IMi taken by means of the camera $\mathbf{2 0}$ are transferred to the microcomputer to be processed and displayed on the screen 23, in a display window 24 . A processing program comprising an algorithm for transforming and displaying the images is first loaded into the microcomputer, by means of a CD-ROM 25 or by downloading via the Internet for example. The camera 20 can be a still digital camera or a digital video camera and the connection to the microcomputer can be permanent or otherwise. In the case of a video camera, the microcomputer receives a flow of images that it processes in real time to display them on the screen.

In this context, the correction method according to the present invention can be performed according to two embodiments. A first embodiment involves correcting the initial image by means of a function $\mathrm{Fd}^{-1}$ that is the reciprocal function of the distribution function Fd according to the present invention. As the distribution function Fd is known and determined at the time the non-linear objective lens is designed, it is easy to deduce the reciprocal function $\mathrm{Fd}^{-1}$ therefrom. This correction step allows a corrected image to be obtained in which the non-linearity due to the objective lens according to the present invention is removed. The corrected image is equivalent to an image taken by means of a classical panoramic objective lens and can then be processed by any classical display software program available in stores, provided for transferring the image points of an image disk into a three-dimensional space and for interactively displaying a sector of the image obtained.

The second alternative of the method involves using the distribution function Fd in an image display algorithm working backwards, that is defining in real time the color of the pixels of a display window using the image points of the image disk.

## First Embodiment of the Correction Method

FIG. 11 shows the first embodiment of the method according to the present invention. Here it is assumed that there is an initial image Img1 comprising a non-linear image disk ID1 of radius R1, having for example an expansion zone in the center (circles C10 and C20). The initial image Img1 is transformed into a corrected image Img2 comprising a linear image disk ID2 of radius R2. The radius R2 of the image
disk ID2 is higher than the radius R1 of the initial image disk ID1 and the image disk ID2 has a resolution equal or substantially equal to the resolution offered by the zone of the image disk Img1 in which the greatest density of information (i.e. the zone in which the image is the most 5 expanded) is to be found. Here, the zone with the greatest density of information is the central part of the image delimited by the circle C20.

The main steps of this method are the following:
initially, the size R2 of the linearized image disk ID2 is calculated by means of the reciprocal function $\mathrm{Fd}^{-1}$, considering on the initial image disk ID1 the place in which the image is the most expanded, so that the corrected image Img2 has a resolution equal or substantially equal to the resolution offered by the zone of the image $\operatorname{Img} 1$ in which the greatest density of information is to be found,
then each pixel of the image to be calculated Img2 is scanned, and the position of its twin point on the image Img1 is searched for, and then
the color of the corresponding point on the initial image
Img1 is allocated to the point of the new image Img2.
This method is implemented by means of an algorithm described below (algorithm 1), in which:

A is the angular aperture of the objective lens,
$D$ is the distance of an image point relative to the center of the initial image disk ID1,
R1 is the size in pixels of the radius of the initial image disk ID1 (i.e. the number of pixels betwreen the center and the edge of the image disk),
$\mathrm{R} \mathbf{2}$ is the size in pixels of the radius of the linearized image disk ID2,
I and $\mathbf{J}$ are the coordinates of an image point in the image produced, the coordinate point $(\mathbf{0}, \mathbf{0})$ being in the center of the image,
U and V are the coordinates of a twin point in the original image, the coordinate point $(\mathbf{0}, 0)$ being in the center of the image,
"Current_angle" and "Previous_angle" are iterative parameters,
DAM is the minimum angular difference between two object points corresponding to two adjacent image points on the initial image disk ID1 (i.e., the maximum resolution of the image disk ID1 expressed in angular difference), and
Fdlin ${ }^{-1}$ is the reciprocal function of a distribution function of a classical linear objective lens, of the type: Fdlin $(\alpha)=K \alpha$, with $K=2 / A$, i.e. $K=1 / 90$ with an objective lens having an angular aperture of $180^{\circ}$.

| Algorithm 1 |
| :---: |
| [finding DAM] |
| 1/ DAM $=$ A/2 |
| 2/ Current angle $=0$ |
| 3/ For D = 1 to R1 [with increments of 1] |
| 4/ Previous_angle $=$ Current angle |
| 5/ Current_angle $=\mathrm{Fd}^{-1}(\mathrm{D} / \mathrm{R} 1)$ |
| 6) If DAM > (Current angle - Previous angle) then |
| 7/ DAM = (Current_angle - Previous_angle) |
| 8/ End if |
| $9 /$ End for |
| [determining the radius R 2 of the disk ID2] |
| 10/ $\mathrm{R} 2=(\mathrm{A} / 2) / \mathrm{DAM}$ | pointsally, this method involves projecting the image DW on mage sector corresponding to a display window method does not require calculating a corrected image disk, 65 contrary to the previous embodiment.

The image points of the display window DW are referenced $E(i, j)$ in the coordinate system of the display window,
expressed in line coordinates $i$ and in column coordinates $j$. The points $\mathrm{E}(\mathrm{i}, \mathrm{j})$ are first projected onto a sphere portion HS of center O and of axes $\mathrm{OX}, \mathrm{OY}, \mathrm{OZ}$, to obtain image points $\mathrm{P}(\mathrm{px}, \mathrm{py}, \mathrm{pz})$ belonging to the sphere portion. This sphere portion covers a solid angle that corresponds to the aperture of the objective lens used. The example considered until now was of a panoramic objective lens having an aperture of $180^{\circ}$ and the sphere portion HS considered here is therefore a hemisphere. The image points P thus determined are then projected onto the image disk Img1 by means of the nonlinear distribution function Fd according to the present invention, which first requires calculating the field angle $\alpha$ of the points P in relation to the center O of the hemisphere. The center $O$ of the hemisphere is the virtual equivalent of the center " $p$ " of the panorama, having been used as the reference, in the description above, to determine the angles of incidence a of the object points and the shape of the function Fd. The projection of the image points $P$ onto the image disk ID1 allows image points $p(p u, p v)$ to be obtained on the image disk, in a coordinate system of center $\mathrm{O}^{\prime}$ (corresponding to the center of the image disk) and of axes $\mathrm{O}^{\prime} \mathrm{U}$ and $\mathrm{O}^{\prime} \mathrm{V}$. The axis OZ in the system of the hemisphere HS is perpendicular to the plane of the image disk ID1 and passes through the center $O^{\prime}$ of the image disk, such that the axes $\mathrm{O}^{\prime} \mathrm{Z}$ and $\mathrm{OZ}^{2}$ are merged.
As it will be clear to those skilled in the art, the correction of the non-linearity of the image disk is implicit here since the image points $p(p u, p v)$ corresponding to the image points $E(i, j)$ of the display window DW are "retrieved" from the image disk ID1, by means of the function Fd.

The method according to the present invention is implemented by means of an algorithm described below (algorithm 2), in which:
$i$ and $j$ are the coordinates of a point $E(i, j)$ of the display window,
Imax and Jmax are the number of columns and the number of lines of the display window, corresponding to the dimensions in number of pixels of the display window,
Ex, Ey and Ez are the Cartesian coordinates of a point $E(i, j)$ of the display window DW in the coordinate system OXYZ,
$\mathrm{Px}, \mathrm{Py}$ and Pz are the Cartesian coordinates of a point P on the hemisphere HS,
pu and $p v$ are the Cartesian coordinates of an image point $p$ of the image disk in the coordinate system $\mathrm{O}^{\prime} \mathrm{UV}$, L is the size of the image disk, in number of pixels,
M is the center of the display window DW,
the "viewing direction" is the direction materialised by the point O and the center of the display window M , the display window forming the base of a pyramid of vision of the observer the top of which is the point $O$ (observer's position),
$\theta 0$ and $\phi 0$ are the longitudes and latitudes corresponding to the viewing direction from the point O towards the center M of the display window,
Screen_Pixel $[i, j]$ is the color (RGBA) of a point $E(i, j)$ of the display window DW,
Image_Pixel[i,j] is the color of the point $\mathrm{P}(\mathrm{i}, \mathrm{j})$ of the hemisphere HS corresponding to the image disk, the coordinate point $(0,0)$ being situated in the center of the image disk,
$R$ is the radius of the hemisphere HS (arbitrary value chosen so as to improve the accuracy of the calculations, R is for example chosen to be equal to 10,000),
$\alpha$ is the angle in relation to the center $O$ of an image point " P situated on the hemisphere (represents the field angle at the moment the shot of the corresponding object point is taken),
aux1, aux2are intermediate variables,
"Zoom" is a variable defining the enlargement, having a default value equal to $R$, and
" $V$ " is the square root function.
$\mathrm{Ez}=\mathrm{Zoom}^{*} \cos (\phi 0)+\mathrm{j}^{*} \sin (\phi 0)$
$\mathrm{Ez}=\mathrm{Zoom}$
aux1 $=\mathrm{Ez}$
aux $=E z$
$\mathrm{Ez}=\mathrm{Ez}^{*} \cos (\theta 0)-\mathrm{i}^{*} \sin (\theta 0)$
$E z=E z^{*} \cos (\theta 0)-i^{*} \sin (\theta 0)$
$E x=i^{*} \cos (\theta 0)+a u x 1^{*} \sin (\theta 0)$
[calculation of the coordinates of the point P corresponding to the point E ]
8/ $\quad \mathrm{aux} 2=\mathrm{R} / v\left(E x^{*} \mathrm{Ex}+\mathrm{Ey}^{*} \mathrm{Ey}+\mathrm{Ez}^{*} \mathrm{Ez}\right)$
$\mathrm{P}_{\mathrm{x}}=\mathrm{Ex}^{*}$ aux 2
$\mathrm{Py}=E y^{*} \mathrm{aux}^{2}$
$\mathrm{Py}=\mathrm{Ey}$ *aux 2
$\mathrm{Pz}=\mathrm{Ez}^{*}$ aux 2
$\mathrm{Pz}=E z^{*}$ aux 2
[calculation of the coordinates of the point p corresponding
to the point P , in the coordinate system
(OUV), by means of the function Fd ]
$\mathrm{X}=\mathrm{Px} / \mathrm{R}$
$\mathrm{Y}=\mathrm{Py} / \mathrm{R}$
$\mathrm{r}=\mathrm{V}\left(\mathrm{X}^{*} \mathrm{X}+\mathrm{Y} * \mathrm{Y}\right)$
$\alpha=\operatorname{arcsine}(\mathrm{r})$
$\alpha=\operatorname{arcsine}(\mathrm{r})$
$\mathrm{U}=\mathrm{X} / \mathrm{r}$
$\mathrm{U}=\mathrm{X} / \mathrm{r}$
$\mathrm{V}=\mathrm{Y} / \mathrm{r}$
$\mathrm{pu}=\mathrm{L}^{*} \mathrm{U}^{*} \mathrm{Fd}(\alpha)$
$\mathrm{pv}=\mathrm{L}^{*} \mathrm{~V}^{*} \mathrm{Fd}(\alpha)$
Screen_Pixel[i,j] = Image_Pixel[pu,pv]
end for
end for

A request for enlargement (zoom) by the user results in the algorithm modifying the "Zoom" parameter. When the "Zoom" parameter is equal to the radius R of the hemisphere, the display window DW is tangential to the hemisphere (FIG. 13). When the parameter "Zoom" is higher than $R$, the window DW moves away from the hemisphere (along the axis given by the viewing position 0 M ), which corresponds to a shrinking of the pyramid of vision and an enlargement of the image sector presented in the window DW. The enlargement of the image sector presented to the observer is therefore equal to the ratio of the "Zoom" parameter by the radius R.

When the steps 18 and 19 have been performed with a "Zoom" parameter higher than R, a gain in definition is obtained in the zones in which the image has been expanded at the time the shot is taken as there are still. While the resolution limit is not reached, two adjacent pixels on the image disk which correspond to two adjacent pixels of the display window. In the compressed zones of the image, the search for the closest pixel by means of the relations $L^{*} U^{*} \operatorname{Fd}(\alpha)$ and $L^{*} V^{*} \operatorname{Fd}(\alpha)$ results, on the other hand, in the algorithm finding the same image pixel for several adjacent pixels of the display window on the image disk. However, these compressed image zones, benefiting from a lesser definition on the image disk, are considered secondary for the intended application, in accordance with the premise on which the present invention is based.

Generally speaking, any other projection method can be used, the essential step according to the present invention being that of finding the field angle a of the object points on the hemisphere, in relation to the center of the hemisphere, so as to use the distribution function Fd in the calculations.

It will be understood that the algorithm $\mathbf{2}$ is applicable when there are two complementary image disks, one corresponding to a front photograph and the other to a rear photograph of a panorama at $360^{\circ}$, the second photograph being taken by rotating the panoramic objective lens by $180^{\circ}$ around an axis passing through the center of the panorama. In this case, two hemispheres and two image points called "Front_Image_Pixel" and "Rear_Image_Pixel" are defined:

Front_Image_Pixel[i, $]$ : color of a point $\mathrm{E}(\mathrm{i}, \mathrm{j})$ on the hemisphere corresponding to the front photo, the coordinate point $(0,0)$, being situated in the center of the image disk,
Rear_Image_Pixel[i,j]: color of a point E(i,j) on the hemisphere corresponding to the rear photo, the coordinate point $(0,0)$ being situated in the center of the image disk.
The steps 18 and following of the algorithm 2 are therefore modified as follows:

18) $\mathrm{pu}=\mathrm{L} * \mathrm{U} * \mathrm{Fd}(\alpha)$<br>$\mathrm{pv}=\mathrm{L}^{*} \mathrm{~V}^{*} \mathrm{Fd}(\alpha)$<br>$\mathrm{pv}=\mathrm{L}$ If $\mathrm{Pz}>=0$ then<br>Screen_Pixel[i,i] = Front_Image_Pixel[pu,pv]<br>If not Screen Pixel[i,j] = Rear_Image_Pixel[L-pu,pv]<br>End if<br>end for<br>end for

FIG. 14 is a flow chart giving a general overview of the steps of a method for capturing and interactively presenting a panoramic image on a screen. This flow chart is described in table 2 in the Appendix, that is an integral part of the description. The acquisition S1 and transfer S2 steps described above are again included. The step S 2 is followed by an interactive display step $\mathrm{S} \mathbf{3}^{\prime}$ performed in accordance with the method that has just been described, implicitly incorporating a correction of the non-linearity of the image disk through the use of the distribution function Fd to find the points corresponding to the pixels of the display window on the image disk.

## II-EXAMPLES OF EMBODIMENTS OF A NON-LINEAR PANORAMIC OBJECTIVE LENS ACCORDING TO THE PRESENT INVENTION

Here, one object of the present invention is to provide a panoramic objective lens having a non-linear distribution function Fd, that is simple in structure and with a low cost price. Below, two examples of embodiments of non-linear panoramic objective lenses according to the present invention will be described, the first being a direct-type objective lens and the second of indirect type, that is using mirrors.

## First Embodiment

Apodizers are optical systems well known by those skilled in the art, used to change the energy distribution (amount of light) of a source of light at the pupil. They are particularly used to level out the energy in a laser beam or even, in the field of photography, to limit the diffraction of light through the lenses. Using an apodizer as a filter is also well known, to cover the aperture of an optical instrument in order to remove the secondary rings of a diffraction pattern. When it is desirable to separate the images of two neighbouring pin-point sources, these secondary rings are a nuisance and reduce the resolution. "Apodization" can thus be performed, that is these secondary rings can be removed by placing an adequate filter in the plane of the pupil.

Here, the idea of the present invention is to use an apodizer for a different purpose: the principle of the apodizer is used to control the angular distribution of a panoramic objective lens and to obtain the non-linearity sought.

FIG. 15 represents, by a cross-section, an example of an embodiment of a non-linear objective lens $\mathbf{3 0}$ according to the present invention. The distribution function Fd obtained by means of the objective lens $\mathbf{3 0}$ is the function Fd described above in relation with FIG. 7B, the objective lens 30 thus expanding the image in the center.

The objective lens $\mathbf{3 0}$ comprises a system of lenses that is also represented in FIG. 16 by an exploded view. A divergent optical group formed by lenses L1, L2, L3, and a convergent optical group formed by lenses L4, L5, L6, L7 can be distinguished. A diaphragm D1 is arranged between the lenses L6 and L7.

Parts B1 to B4 and parts I3 to I6 are provided to hold the lenses. The part B1 forms the body of the objective lens and comprises a cylindrical cavity in which the lenses L2 to L6 are arranged. The part B2 is screwed onto the body B1 and allows the front lens L1 to be fastened against the front of the part B1, the back of the lens L1 being in contact with the front of the lens L2. The parts B3 and B4 are fastened with screws (not represented) against the rear part of the body B1. The part B3 holds the diaphragm D1 and comprises a cavity 5 for receiving the back lens L7. The part B4 presses the lens L7 into the part B3 and comprises a rear sleeve F1 equipped with a thread allowing an image sensor to be fastened, such as a CCD sensor for example. The parts 13 to I6 are dividers allowing the distances between the lenses L 2 to L 6 inside the body B1 to be adjusted with precision.

The divergent optical group L1, L2, L3 defines the field angle of the objective lens 30 , here of $180^{\circ}$. The front lens L 1 is a divergent meniscus in PMMA with an aspherical front and a concave back. It must be said that PMMA or polymethacrylate is organic glass with a low cost price, belonging to the category of plastics. The lens L2 is of the planoconcave type and is made of borosilicate BK7 (standard optical mineral glass). Its front (plane side) is pressed against a flat part of the back of the lens L1, which extends at the periphery of the concave part (useful part) of the back of the lens L1. The lens L3 is also of the planoconcave type and is in BK7. Its concave side is oriented towards the front, opposite the back of the lens $\mathrm{L} \mathbf{2}$.

The convergent optical group L4, L5, L6, L7 forms an 5 apodizer within the meaning of the present invention and determines the non-linear distribution function Fd, which is obtained here by means of a-spherical lenses and a diffractive lens.

The lens L4 is of the planoconcave type and is in PMMA. Its concave front is a-spherical. The lens L5 is of the planoconvex type and is in BK7, its plane side being oriented towards the front. The lens L6 is a meniscus in PMMA having a concave and aspherical front and a diffractive convex back. This diffractive back has a diffraction grating made up of circular diffractive zones centered on the optical axis of the lens, the profile of which is represented in FIG. 17. Finally, the back lens L7 is of the biconvex type and is in BK7. The back lens L7 focuses the luminous flux onto the image plane, at the spot provided for the image sensor.

The aspherical fronts of the lenses L1, L4 and L6 are determined by means of a formula of the type:

$$
z(r)=\left[\left(C^{*} r^{2}\right) /\left(1+\sqrt{ }\left(1-(1+k)^{*} C^{2 *} r^{2}\right)\right]+A_{1} r^{2}+A_{2} r^{6}+A^{4} r^{8}+A_{5} r^{10}\right.
$$

in which:
" $k$ " is a conicity constant,
" $\mathbf{A 1}$ ", " $\mathbf{A} 2$ ", " $\mathbf{A} \mathbf{3}$ ", " $\mathbf{A 4}$ ", " $\mathbf{A 5}$ " are constants for adjusting the coefficient of conicity according to the position,
" $z$ " is the shape of the surface,
" $r$ " is the radius at the center, and
"C" is the radius of curvature.
The diffractive back of the lens L6 allows the number of lenses required to produce the objective lens $\mathbf{3 0}$ to be reduced. In the present embodiment, it avoids for example providing at least three supplementary complex lenses. It is determined by means of a formula of the type:

$$
\phi(r)=\alpha 1(r / R 0)^{2}+\alpha 2(r / R 0)^{4}
$$

in which:
" $r$ " is the distance in relation to the center of the lens of a point considered, located on the surface of the lens,
$\alpha 1$ and $\alpha 2$ are constants defining the phase shift of the wave surface,
" R 0 " is a constant allowing r to be normalized, and
" $\phi$ " is the phase shift introduced by the diffractive surface at the point considered.
The lenses in PMMA L1, L4 and L6 are manufactured using a method called "diamond turning" well known by those skilled in the art, which involves milling the surface of the lenses along a mesh of points.

The solid angle of propagation of the light rays in each lens is marked on FIG. 15 by black lines. The light rays pass through the optical group L1, L2, L3, pass through the apodizer L4, L5, L6, L7 while being stopped down by D1.

The determination of the parameters defining the aspherical sides mentioned above, the formula of the diffraction grating of the lens L6, the calculation of the diameters of the lenses and of the distances between the lenses, are within the understanding of those skilled in the art using the classical computer-aided lens design tools.

## Second Embodiment

FIG. 18 schematically represents a non-linear objective lens 40 using a distorting mirror. The objective lens 40 comprises, at input, a divergent optical group consisting, for example, of the three lenses L1, L2, L3 described above, defining the field angle of the objective lens. Opposite the optical group a plane mirror M1 is located which reflects the luminous beam onto a distorting mirror M2 of aspherical concave shape. The beam reflected by the mirror M2 is sent onto an image sensor 43.

In this embodiment, the irregularities of sphericity that the concave part of the mirror has determined the angular distribution function Fd sought for the intended application (distortion in the center, on the edges . . . ). The result obtained is equivalent to that of the optical system described above. Obtaining the distribution function Fd is within the understanding of those skilled in the art using computeraided lens design tools which allow, in addition to designing lenses, reflecting surfaces to be designed and focused.

One alternative of this embodiment involves providing several distorting mirrors so as to combine distortions or simplify complex distortions by characterising a type of distortion per mirror, which has the advantage of facilitating the engineering work.

Yet another alternative involves using one or more deformable mirrors to produce a so-called "adaptive" optical system. Deformable mirrors comprise a layer of piezoelectric micro-pistons covered by a reflecting layer. Each piezoelectric piston is activated individually, so that the distortions of the mirror can be controlled at several points to obtain the desired shape. This device can be driven by an
integrated circuit comprising several configurations of the micro-pistons in its memory, to obtain a distribution function Fd that is adjustable according to the intended use, which avoids providing several objective lenses.

Generally speaking, adaptive optics are in themselves known by those skilled in the art and used in high-precision telescopes to correct the optical defects of the lenses or atmospheric distortions. Deformable mirrors also exist in the field of optical disks, if reference is made for example to the U.S. Pat. Nos. 5,880,896 and 5,745,278.

Therefore, means that are in themselves known are also used for different purposes, not to correct a lens but to obtain, on the contrary, a non-linear angular distribution function.

It will be understood that various other alternatives of the present invention may be made. In particular, although the description above was of non-linear panoramic objective lenses with axial symmetry relative to the optical axis, in which the position of an image point only varies with the field angle relative to this axis of the corresponding object point (which gives a distribution of points in concentric circles, as seen above), the framework of the present invention also covers providing objective lenses the non-linearity of which is not symmetrical relative to the optical axis, such that the expanded parts of the image may, in this case, not be set on the center of the image.

It will be appreciated by those skilled in the art that changes could be made to the embodiments described above without departing from the broad inventive concept thereof. It is understood, therefore, that this invention is not limited to the particular embodiments disclosed, but it is intended to cover modifications within the spirit and scope of the present invention as defined by the appended claims.

> APPENDIX (Forming an Integral Part of the Description)

TABLE 1
S1-Acquisition
Taking a panoramic image by means of a still digital camera or a digital video camera equipped with a panoramic objective lens having a non-linear distribution function Fd $\mathbf{S 2 - T r a n s f e r ~ o f ~ t h e ~ i m a g e ~ f i l e ~ i n t o ~ a ~ c o m p u t e r ~}$
Transfer of the image file (image disk) into a microcomputer Storage in the auxiliary storage (optional) S3-Linearisation of the image disk
Transfer of the image points of the initial image disk into a second virtual image disk comprising more image points than the initial image disk, by means of the function $\mathrm{Fd}^{-1}$ $\Rightarrow$ Obtaining a linear image disk S4-Digitization
Transfer of the image points of the second image disk into a system of axes OXYZ in spherical coordinates $\Rightarrow$ Obtaining a panoramic image in a hemisphere
S5 - Interactive display

Determination of the image points of an image sector to be displayed
Display of the image sector on a display window
Detection of the user's actions on a screen pointer or any
other control means,
Detection of the user's actions on keys for image enlargement, Modification of the sector displayed (sliding the image sector displayed on the surface of the hemisphere and/or shrinking/expanding the image sector displayed)

TABLE 2

## S1-Acquisition

Taking a panoramic image by means of a still digital camera or a digital video camera equipped with a panoramic objective lens having a non-linear distribution function Fd

S2 - Transfer of the image file into a computer
Transfer of the image file (image disk) into a microcomputer
Storage in the auxiliary storage (optional)
S3' - Interactive display with implicit correction
of the non-linearity of the initial image

A - Determination of the color of the points $E(i, j)$ of an image sector
to be displayed using the points $\mathrm{p}(\mathrm{pu}, \mathrm{pv})$ of the image disk:
1 - determination of the coordinates Ex, Ey, Ez in the coordinate
system OXYZ of each point $E(i, j)$ of the sector to be displayed,
2 - determination of the coordinates $\mathrm{Px}, \mathrm{Py}, \mathrm{Pz}$ of points P of the hemisphere corresponding to the points $\mathrm{E}(\mathrm{i}, \mathrm{j})$,
3 - calculation of the coordinates, in the coordinate system O'UV
of the image disk, of points $\mathrm{p}(\mathrm{pu}, \mathrm{pv})$ corresponding to the points P
of the hemisphere, by means of the function Fd ,
B - Presentation of the image sector in a display window,
C - Detection of the user's actions on a screen pointer or any
other control means,
D - Detection of the user's actions on enlargement keys,
E - Modification of the inage sector displayed (moving and/or shrinking/expanding the image sector)

We claim:

1. A method for capturing a digital panoramic image, by projecting a panorama onto an image sensor by means of a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $\pm 10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least one substantially compressed zone.
2. The method according to claim 1 , wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
3. The method according to claim 1 , wherein the objective lens expands the center of the image and compresses the edges of the image.
4. The method according to claim 1 , wherein the objective lens expands the edges of the image and compresses the center of the image.
5. The method according to claim 1 , wherein the objective lens compresses the center of the image and the edges of the image and expands an intermediate zone of the image located between the center and the edges of the image.
6. The method according to claim 1, wherein the objective lens comprises a set of lenses forming an apodizer.
7. The method according to claim 6, wherein the set of lenses forming an apodizer comprises at least one aspherical 55 lens.
8. The method according to claim 6, wherein the set of lenses forming an apodizer comprises at least one diffractive lens.
9. The method according to claim 1, wherein the objective lens comprises a set of mirrors including at least one distorting mirror.
10. A method for displaying an initial panoramic image obtained in accordance with the method according to claim 1 , the method for displaying comprising:
correcting the non-linearity of the initial image, per-
formed by means of a reciprocal function of the non-
linear distribution function of the objective lens or by means of the non-linear distribution function.
11. The method according to claim 10 , wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.
12. The method according to claim 11, further comprising:
calculating the size of the corrected image, by means of the reciprocal function of the distribution function, so that the resolution of the corrected image is equivalent to the most expanded zone of the initial image, and
scanning each image point of the corrected image, searching for the position of a twin point of the image point on the initial image and allocating the color of the twin point to the image point of the corrected image.
13. The method according to claim 11 , wherein the initial image and the corrected image comprise an image disk.
14. The method according to claim 11, further comprising:
transferring the image points of the corrected image into a three-dimensional space, and
presenting one sector of the three-dimensional image obtained on a display means.
15. The method according to claim 10 , further comprising:
determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the nonlinear distribution function, and
allocating to each image point of the display window the color of an image point that is the closest on the initial image.
16. The method according to claim 15 , wherein the projection of the image points of the display window onto the initial image comprises:
projecting the image points of the display window onto a sphere or a sphere portion,
determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and
projecting onto the initial image each image point projected onto the sphere or the sphere portion, the projection being performed by means of the non-linear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion.
17. A panoramic objective lens comprising:
optical means for projecting a panorama into an image plane of the objective lens, the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $\pm 10 \%$ compared to a linear distribution function, such that a panoramic image obtained by means of the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone.
18. The panoramic objective lens according to claim 17, having a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of an image obtained varying according to the field angle of the corresponding object point.
19. The panoramic objective lens according to claim 17 , wherein the lens expands the center of an image and compresses the edges of the image.
20. The panoramic objective lens according to claim 17, wherein the lens expands the edges of an image and com- 5 presses the center of the image.
21. The panoramic objective lens according to claim 17 , wherein the lens compresses the center of the image and the edges of the image, and expands an intermediate zone of the image located between the center and the edges of the 10 image.
22. The panoramic objective lens according to claim 17 , further comprising a set of lenses forming an apodizer.
23. The panoramic objective lens according to claim 22 wherein the set of lenses forming an apodizer comprises at least one aspherical lens.
24. The panoramic objective lens according to claim 22, 5 wherein the set of lenses forming an apodizer comprises at least one diffractive lens.
25. The panoramic objective lens according to claim 22, comprising polymethacrylate lenses.
26. The panoramic objective lens according to claim 17, 0 comprising a set of mirrors comprising at least one distorting mirror.

# UNITED STATES PATENT AND TRADEMARK OFFICE CERTIFICATE OF CORRECTION 

PATENT NO. : 6,844,990 B2
Page 1 of 1
DATED
: January 18, 2005
INVENTOR(S) : Jean-Claude Artonne et al.

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Column 2,
Line 34, "ax" should be replaced with -- $\alpha-$-;
Column 13,
Line 17, "a" should be replaced with -- $\alpha-$-;
Column 14,
Line 65 , "a" should be replaced with -- $\alpha-$-;
Column 16,
Line 62, the formula should read:
$\cdots z(r)=\left[\left(C^{*} r^{2}\right) /\left(1+\sqrt{(1-(1+k) *} C^{2}+r^{2}\right)\right]+A_{1} r^{2}+A_{2} r^{4}+A_{3} r^{6}+A_{4} r^{8}+A_{55} r^{10} \cdots$.

Signed and Sealed this
Twenty-fourth Day of May, 2005


JON W. DUDAS
Director of the United States Patent and Trademark Office

## (Also referred to as FORM PTO-1465) <br> REQUEST FOR EX PARTE REEXAMINATION TRANSMITTAL FORM

Address to:
Mail Stop Ex Parte Reexam
Commissioner for Patents
P.O. Box 1450

Alexandria, VA 22313-1450

## Attorney Docket No.: <br> $\square$

Date: November 26, 2014
1.

This is a request for ex parte reexamination pursuant to 37 CFR 1.510 of patent number
$\qquad$ issued $\qquad$
$\qquad$ . The request is made by:
patent owner. third party requester.
2.
$x$ The name and address of the person requesting reexamination is:

```
6115187 Canada Inc.
2020 University Street
Suite 2320
Montreal, Quebec H3A 2A5
CANADA
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3. Requester claims $\square$ small entity (37 CFR 1.27) or micro entity status (37 CFR 1.29) - only a patent owner requester can claim micro entity status.
4. 


a. A check in the amount of $\$$ $\qquad$ is enclosed to cover the reexamination fee, 37 CFR 1.20(c)(1);b. The Director is hereby authorized to charge the fee as set forth in 37 CFR 1.20(c)(1) to Deposit Account No. $\qquad$ ;c. Payment by credit card. Form PTO-2038 is attached; or

X
d. Payment made via EFS-Web.
5.Any refund should be made by $\square$ check or $\square$ credit to Deposit Account No. $\qquad$ . 37 CFR 1.26 (c). If payment is made by credit card, refund must be to credit card account.
6. X A copy of the patent to be reexamined having a double column format on one side of a separate paper is enclosed. 37 CFR 1.510(b)(4).
7. $\qquad$ CD-ROM or CD-R in duplicate, Computer Program (Appendix) or large table
7. $\square$
$\square$ Landscape Table on CD
8.Nucleotide and/or Amino Acid Sequence Submission
If applicable, items a. - c. are required.
a. $\square$ Computer Readable Form (CRF)
b. Specification Sequence Listing on:
i. $\square$ CD-ROM (2 copies) or CD-R (2 copies); or
ii. $\square$ paper
c. $\square$ Statements verifying identity of above copies
9. $x$ A copy of any disclaimer, certificate of correction or reexamination certificate issued in the patent is included.
10. $x$ Reexamination of claim(s) $\qquad$ $1-4,6-7,10-11,15-20,22-23$, and 25 is requested.
11. x A copy of every patent or printed publication relied upon is submitted herewith including a listing thereof on Form PTO/SB/08, PTO-1449, or equivalent.
12. x An English language translation of all necessary and pertinent non-English language patents and/or printed publications is included.
13. x The attached detailed request includes at least the following items:
a. A statement identifying each substantial new question of patentability based on prior patents and printed publications. 37 CFR $1.510(b)(1)$.
b. An identification of every claim for which reexamination is requested, and a detailed explanation of the pertinency and manner of applying the cited art to every claim for which reexamination is requested. 37 CFR 1.510(b)(2).
14. x A proposed amendment is included (only where the patent owner is the requester). 37 CFR 1.510(e).
15.a. It is certified that a copy of this request (if filed by other than the patent owner) has been served in its entirety on the patent owner as provided in 37 CFR 1.33(c). The name and address of the party served and the date of service are:
$\square$Date of Service: $\qquad$ ; or
b. A duplicate copy is enclosed since service on patent owner was not possible. An explanation of the efforts made to serve patent owner is attached. See MPEP § 2220.
16. Correspondence Address: Direct all communication about the reexamination to:



WARNING: Information on this form may become public. Credit card information should not be included on this form. Provide credit card information and authorization on PTO-2038.

| /Stephen E. Murray/ |
| :---: |
| Authorized Signature |
| Stephen E. Murray |
| Typed/Printed Name |


| $\frac{\text { November 26, } 2014}{\text { Date }}$ |  |
| :---: | :---: |
| $\frac{63,206}{\text { Registration No. }}$ | $\boxed{x}$ For Patent Owner Requester |
|  | $\square$ For Third Party Requester |

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Patent of:
Jean-Claude ARTONNE et al.
Patent No.: 6,844,990 B2
Issue Date: January 18, 2005

For: METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION<br>DIGITAL PANORAMIC IMAGE

## REQUEST BY PATENT OWNER FOR EX PARTE REEXAMINATION OF U.S. PATENT NO. $\mathbf{6 , 8 4 4 , 9 9 0}$

6115187 Canada Inc. ("Immervision") hereby respectfully requests ex parte reexamination under 35 U.S.C. § 302 and 37 C.F.R. § 1.510 of claims 1-4, 6-7, 10-11, 15-20, 2223, and 25 of U.S. Patent No. 6,844,990 B2 ("the '990 patent") filed on November 12, 2003 by Jean-Claude Artonne, et al. and assigned to Immervision. The ' 990 patent is a continuation of International Patent Application No. PCT/FR02/01588, filed on May 10, 2002, which claims priority to French Patent Application No. FR 01-06261, filed on May 11, 2001. The '990 patent was issued on January 18, 2005 and is still in force. A copy of the '990 patent is attached hereto as Exhibit 1.

Payment of the fee for reexamination is included herewith. If any additional fee is due, please charge such fee to Deposit Account No. 50-1017.

Ex Parte Reexamination of U.S. Patent No. 6,844,990
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## I. Identification of Prior Art

The following patents and publications form the basis of the current request for ex parte reexamination:

1. U.S. Patent No. 6,128, 145 of Nagaokal ("Nagaoka"): Nagaoka issued on October 3, 2000, more than one year before the earliest priority date (May 10, 2002) of the ' 990 patent. Thus, Nagaoka qualifies as prior art to the ' 990 patent under 35 U.S.C. §§ 102(b) and 103(a). ${ }^{2}$
2. U.S. Patent No. 5,686,957 of Baker" ("Baker"): Baker issued on November 11, 1997, more than one year before the earliest priority date (May 10, 2002) of the ' 990 patent. Thus, Baker qualifies as prior art to the ' 990 patent under 35 U.S.C. §§ 102(b) and 103(a).
3. U.S. Patent No. 3,953,111 of Fisher, et al. ${ }^{4}$ ("Fisher"): Fisher issued on April 27, 1976, more than one year before the earliest priority date (May 10, 2002) of the ' 990 patent. Thus, Fisher qualifies as prior art to the ' 990 patent under 35 U.S.C. §§ 102(b) and 103(a).
4. European Patent Publication No. EP 1028389 A2 ("Shiota"): Shiota was published on August 16, 2000, more than one year before the earliest priority date (May 10, 2002) of the '990 patent. Thus, Shiota qualifies as prior art to the '990 patent under §§ 102(b) and 103(a).
5. Japanese Patent Publication No. JP 2000-242773 ("Matsui"): Matsui was published on September 8, 2000, more than one year before the earliest priority date (May 10, 2002) of the '990 patent. Thus, Matsui qualifies as prior art to the '990 patent under §§ 102(b) and 103(a).
[^5]Ex Parte Reexamination of U.S. Patent No. 6,844,990
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6. Japanese Patent Publication No. JP H11-2618687 ("Enami"): Enami was published on September 24, 1999, more than one year before the earliest priority date (May 10, 2002) of the '990 patent. Thus, Enami qualifies as prior art to the '990 patent under $\S \S 102(\mathrm{~b})$ and 103(a).
7. U.S. Patent No. 6,031,670 of Inoue ${ }^{8}$ ("Inoue"): Inoue issued on February 29, 2000, more than one year before the earliest priority date (May 10, 2002) of the '990 patent. Thus, Inoue qualifies as prior art to the '990 patent under 35 U.S.C. $\S \S 102(\mathrm{~b})$ and 103(a).

## II. Identification of Claims for Which Reexamination is Requested

Reexamination is requested of claims $1-4,6-7,10-11,15-20,22-23$, and 25 of the ' 990 patent in view of the prior art patents and printed publications listed below:

1. Reexamination of claims $1-2,4,6,17-18,20$, and 22 is requested in view of Nagaoka.
2. Reexamination of claims $1-2,4,6,17-18,20$, and 22 is requested in view of Baker.
3. Reexamination of claims 1-3, 6-7, 17-19, and 22-23 is requested in view of Fisher.
4. Reexamination of claims 10-11 is requested in view of Nagaoka in view of Shiota.
5. Reexamination of claim 10 is requested in view of Nagaoka in view of Matsui.
6. Reexamination of claims $10-11$ is requested in view of Baker in view of Shiota.
7. Reexamination of claims 15-16 is requested in view of Nagaoka in view of Shiota and in further view of Enami.
8. Reexamination of claims 15-16 is requested in view of Baker in view of Shiota and in further view of Enami.
9. Reexamination of claim 25 is requested in view of Nagaoka in view of Inoue.
10. Reexamination of claim 25 is requested in view of Baker in view of Inoue.
[^6]Ex Parte Reexamination of U.S. Patent No. 6,844,990
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## III. Showing of Each Substantial New Question of Patentability

## A. Nagaoka

Nagaoka was not of record in the file of the ' 990 patent, although its European equivalent (EP 1004 915) was cited to the Examiner. Nagaoka discloses a monitoring system utilizing a fisheye lens 1 in conjunction with a camera 2 for image capture. The fisheye lens 1 may include one of several "non-linear" image point distribution functions, including ones having a maximum divergence from a linear distribution function of more than $10 \%$, such as $h=1.2 \mathrm{f}$ $\tan (/ 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \tan (/ 2)$. These equations give the fisheye lens 1 an "expanded" zone near the periphery of the image and a "compressed zone" near the center of the image. (Nagaoka at Figs. 2, 3A-3B, 4A; col. 3, ln. 63-col. 4, ln. 15; col. 5, lns. 13-27). Because Nagaoka provides subject matter of claims $1-2,4,6,17-18,20$, and 22 of the ' 990 patent, and the Examiner appears to have overlooked relevant portions of the disclosure of Nagaoka's European equivalent, the teachings of Nagaoka raise a substantial new question of patentability with respect to claims 1-2, $4,6,17-18,20$, and 22.

## B. Baker

Baker was not of record in the file of the ' 990 patent, although its European equivalent (EP 0695 085) was cited to the Examiner. Baker discloses a camera 10 having a lens 14 designed to capture and enhance peripheral content of a hemispheric scene, thereby compressing the center and expanding the periphery of the image. An example provided by Baker states that the lens would focus the lowest fifteen (15) degrees up from the horizon on fifty (50) percent of the imager area, which is greater than a $10 \%$ divergence from a linear distribution function. (Baker at Figs. 1, 3BA, 3BB; col. 6, lns. 48-56; col. 8, In. 58-col. 9, In. 4). Because Baker provides subject matter of claims $1-2,4,6,17-18,20$, and 22 of the ' 990 patent, and the Examiner appears to have overlooked relevant portions of the disclosure of Baker's European equivalent, the teachings of Baker raise a substantial new question of patentability with respect to claims 1-2, 4, 6, 17-18, 20, and 22.

Ex Parte Reexamination of U.S. Patent No. 6,844,990
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## C. Fisher

Fisher was of record in the file of the ' 990 patent, but the Examiner appears to have overlooked certain aspects of the disclosure in Fisher that are relevant to various claims of the '990 patent. Fisher discloses a non-linear panoramic objective lens having three lens groupings A, B, C. The first grouping A provides a mapping function having a formula of $\mathrm{H}=\sin ^{1 / 3}$, which expands the center of the image and compresses the periphery thereof. (Fisher at Figs. 3, 6; col. 3, lns. 8-12; col. 5, lns. 52-60). Because Fisher provides subject matter of claims 1-3, 6-7, 17-19, and 22-23 of the ' 990 patent, and the Examiner appears to have overlooked relevant portions of the disclosure of Fisher, the teachings of Fisher raise a substantial new question of patentability with respect to claims 1-3, 6-7, 17-19, and 22-23.

## D. Nagaoka and Shiota

As described above, Nagaoka itself was not of record in the file of the ' 990 patent, although a European equivalent was considered by the Examiner.

Shiota was not of record in the file of the '990 patent. Shiota discloses an arithmetic unit that transforms an image captured by a fisheye lens into a plane image for display. Points $\mathrm{X}_{2}, \mathrm{Y}_{2}$ on a plane are mapped to projection coordinates $\mathrm{p} 1, \mathrm{q} 1$ on an image pickup surface using an equation relying on $\mathrm{k}_{2}$, which is derived using the distribution function (e.g., F() ). (Shiota at Fig. 1; paras. [0001], [0022], [0028]-[0041]).

Because the teachings of Nagaoka and Shiota, taken together, provide subject matter of claims 10-11 of the '990 patent, and because the Examiner did not have the benefit of examining Shiota in combination with the European equivalent of Nagaoka, Nagaoka and Shiota present a substantial new question of patentability with respect to claims 10-11.

## E. Nagaoka and Matsui

As described above, Nagaoka itself was not of record in the file of the ' 990 patent, although a European equivalent was considered by the Examiner.

Matsui was not of record in the file of the ' 990 patent. Matsui discloses conversion of image data captured using a fisheye lens onto a converted cylindrical surface. The position on

Ex Parte Reexamination of U.S. Patent No. 6,844,990
Proposed Amendment
the captured image can be mapped with a point on the cylindrical surface using the distribution function, which in the example of Matsui is given as $\mathrm{h}=2 \mathrm{f} \tan (/ 2)$. (Matsui at Figs. 2-4, 6; translation at Abstract; para. [0025]).

Because the teachings of Nagaoka and Matsui, taken together, provide subject matter of claim 10 of the ' 990 patent, and because the Examiner did not have the benefit of examining Matsui in combination with the European equivalent of Nagaoka, Nagaoka and Matsui present a substantial new question of patentability with respect to claim 10 .

## F. Baker and Shiota

As described above, Baker itself was not of record in the file of the ' 990 patent, although a European equivalent was considered by the Examiner. As further described above, Shiota was not of record in the file of the ' 990 patent.

Because the teachings of Baker and Shiota, taken together, provide subject matter of claims 10-11 of the ' 990 patent, and because the Examiner did not have the benefit of examining Shiota in combination with the European equivalent of Baker, Baker and Shiota present a substantial new question of patentability with respect to claims 10-11.

## G. Nagaoka, Shiota, and Enami

As described above, Nagaoka itself was not of record in the file of the '990 patent, although a European equivalent was considered by the Examiner. As further described above, Shiota was not of record in the file of the ' 990 patent.

Enami was also not of record in the file of the ' 990 patent. Enami discloses a fisheye lens apparatus and an image distortion correction method. The correction method includes extracting color information from the original image through projection using the distribution function and assigning the appropriate colors on the display point. (Enami at Figs. 2-4; translation at paras. [0072]-[0074], [0084]-[0085]).

Because the teachings of Nagaoka, Shiota, and Enami, taken together, provide subject matter of claims 15-16 of the ' 990 patent, and because the Examiner did not have the benefit of

Ex Parte Reexamination of U.S. Patent No. 6,844,990
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examining Enami in combination with the European equivalent of Nagaoka, Nagaoka, Shiota, and Enami present a substantial new question of patentability with respect to claims 15-16.

## H. Baker, Shiota, and Enami

As described above, Baker itself was not of record in the file of the '990 patent, although a European equivalent was considered by the Examiner. As further described above, neither Shiota nor Enami was of record in the file of the '990 patent.

Because the teachings of Baker, Shiota, and Enami, taken together, provide subject matter of claims 15-16 of the ' 990 patent, and because the Examiner did not have the benefit of examining Enami in combination with the European equivalent of Baker, Baker, Shiota, and Enami present a substantial new question of patentability with respect to claims 15-16.

## I. Nagaoka and Inoue

As described above, Nagaoka itself was not of record in the file of the ' 990 patent, although a European equivalent was considered by the Examiner.

Inoue was not of record in the file of the ' 990 patent. Inoue discloses a wide angle lens that may be made from PMMA. (Inoue at col. 2, Ins. 42-44).

Because the teachings of Nagaoka and Inoue, taken together, provide subject matter of claim 25 of the '990 patent, and because the Examiner did not have the benefit of examining Inoue in combination with the European equivalent of Nagaoka, Nagaoka and Inoue present a substantial new question of patentability with respect to claim 25 .

## J. Baker and Inoue

As described above, Baker itself was not of record in the file of the ' 990 patent, although a European equivalent was considered by the Examiner. As further described above, Inoue was not of record in the file of the ' 990 patent.

Because the teachings of Baker and Inoue, taken together, provide subject matter of claim 25 of the ' 990 patent, and because the Examiner did not have the benefit of examining Inoue in
combination with the European equivalent of Baker, Baker and Inoue present a substantial new question of patentability with respect to claim 25.

## IV. Detailed Explanation under 37 CFR § 1.510(b) of Pertinence and Manner of Applying Cited Prior Art to Every Claim for which Reexamination is Requested

A. Nagaoka

Each element of claims 1-2, 4, 6, 17-18, 20, and 22 is set forth in the attached "Detailed Explanation of Pertinency of Nagaoka and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix A) with an explanation as to how Nagaoka is pertinent to the recited features of each of claims 1-2, 4, 6, 17-18, 20, and 22.
B. Baker

Each element of claims 1-2, 4, 6, 17-18, 20, and 22 is set forth in the attached "Detailed Explanation of Pertinency of Baker and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix B) with an explanation as to how Baker is pertinent to the recited features of each of claims 1-2, 4, 6, 17-18, 20, and 22.
C. Fisher

Each element of claims 1-3, 6-7, 17-19, and 22-23 is set forth in the attached "Detailed Explanation of Pertinency of Fisher and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix C) with an explanation as to how Baker is pertinent to the recited features of each of claims 1-3, 6-7, 17-19, and 22-23.

## D. Nagaoka and Shiota

Nagaoka teaches a monitoring system with a fisheye lens having a non-linear distribution function which expands the peripheral edges of the captured image. A person of ordinary skill in the art would recognize the need to correct the image captured by Nagaoka. Shiota, in the same field of endeavor, teaches a method of transforming a captured image into a plane image for display using the non-linear distribution function. Thus, one of ordinary skill in the art would have had reason to consult Shiota for a method of de-warping the image captured by the fisheye lens of Nagaoka for presentation to a user.

Ex Parte Reexamination of U.S. Patent No. 6,844,990
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Each element of claims 10-11 is set forth in the attached "Detailed Explanation of Pertinency of Nagaoka and Shiota and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix D) with an explanation as to how Nagaoka and Shiota are pertinent to the recited features of each of claims 10-11.

## E. Nagaoka and Matsui

Nagaoka teaches a monitoring system with a fisheye lens having a non-linear distribution function which expands the peripheral edges of the captured image. A person of ordinary skill in the art would recognize the need to correct the image captured by Nagaoka. Matsui, in the same field of endeavor, teaches a method of transforming a captured image into a plane image for display using the non-linear distribution function. Thus, one of ordinary skill in the art would have had reason to consult Matsui for a method of de-warping the image captured by the fisheye lens of Nagaoka for presentation to a user.

Each element of claim 10 is set forth in the attached "Detailed Explanation of Pertinency of Nagaoka and Matsui and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix E) with an explanation as to how Nagaoka and Matsui are pertinent to the recited features of claim 10.

## F. Baker and Shiota

Baker teaches a camera with a lens for capturing a hemispheric scene, emphasizing the periphery of the image. A person of ordinary skill in the art would recognize the need to correct the image captured by Baker. Shiota, in the same field of endeavor, teaches a method of transforming a captured image into a plane image for display using the non-linear distribution function. Thus, one of ordinary skill in the art would have had reason to consult Shiota for a method of de-warping the image captured by the panoramic lens of Baker for presentation to a user.

Each element of claims 10-11 is set forth in the attached "Detailed Explanation of Pertinency of Baker and Shiota and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2"

Ex Parte Reexamination of U.S. Patent No. 6,844,990
Proposed Amendment
(Appendix F) with an explanation as to how Baker and Shiota are pertinent to the recited features of each of claims 10-11.

## G. Nagaoka, Shiota, and Enami

Nagaoka and Shiota, taken together, teach a monitoring system with a fisheye lens having a non-linear distribution function which expands the peripheral edges of the captured image, and which corrects the captured image for display to a user by utilizing the non-linear distribution function. Enami is in the same field of endeavor and teaches color allocation during the image correction process. One of ordinary skill in the art would have had reason to further modify Nagaoka in order to ensure that mapped coordinates were assigned the appropriate color value and provide a more accurate corrected image.

Each element of claims 15-16 is set forth in the attached "Detailed Explanation of Pertinency of Nagaoka, Shiota, and Enami and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix G) with an explanation as to how Nagaoka, Shiota, and Enami are pertinent to the recited features of each of claims 15-16.

## H. Baker, Shiota, and Enami

Baker and Shiota, taken together, teach a camera with a lens having a non-linear distribution function which expands the peripheral edges of the captured hemispheric image, and which corrects the captured image for display to a user by utilizing the non-linear distribution function. Enami is in the same field of endeavor and teaches color allocation during the image correction process. One of ordinary skill in the art would have had reason to further modify Baker in order to ensure that mapped coordinates were assigned the appropriate color value and provide a more accurate corrected image.

Each element of claims 15-16 is set forth in the attached "Detailed Explanation of Pertinency of Baker, Shiota, and Enami and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix H) with an explanation as to how Baker, Shiota, and Enami are pertinent to the recited features of each of claims 15-16.

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## I. Nagaoka and Inoue

Nagaoka teaches a monitoring system with a fisheye lens having a non-linear distribution function which expands the peripheral edges of the captured image. Inoue, in the same field of endeavor, teaches that material and manufacturing costs may be reduced using PMMA to manufacture the wide angle lens. (Inoue at col. 2, lns. 42-44). The ' 990 patent equates PMMA and polymethacrylate. One of ordinary skill in the art would have had reason to manufacture the fisheye lens of Nagaoka out of polymethacrylate, based on Inoue.

Each element of claim 25 is set forth in the attached "Detailed Explanation of Pertinency of Nagaoka and Inoue and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix I) with an explanation as to how Nagaoka and Inoue are pertinent to the recited features of claim 25.

## J. Baker and Inoue

Baker teaches a camera with a lens for capturing a hemispheric scene, emphasizing the periphery of the image. Inoue, in the same field of endeavor, teaches that material and manufacturing costs may be reduced using PMMA to manufacture the wide angle lens. (Inoue at col. 2, lns. 42-44). The '990 patent equates PMMA and polymethacrylate. One of ordinary skill in the art would have had reason to manufacture the fisheye lens of Baker out of polymethacrylate, based on Inoue.

Each element of claim 25 is set forth in the attached "Detailed Explanation of Pertinency of Baker and Inoue and Claim Analysis Chart for U.S. Patent No. 6,844,990 B2" (Appendix J) with an explanation as to how Baker and Inoue are pertinent to the recited features of claim 25.

## V. Notification of Existence of Prior or Concurrent Proceedings and Decisions Thereon Under 37 C.F.R. § $\mathbf{1 . 5 6 5 ( a )}$

The ' 990 patent was previously asserted in a case entitled Immervision, Inc. v. Vivotek, Inc., et al., Civil Action No. 2:13-cv-01117, filed in the United States District Court for the District of Nevada. The case was dismissed pursuant to a settlement between the parties on September 27, 2013.

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The ' 990 patent was also previously asserted in a case entitled 6115187 Canada, Inc. d/b/a Immervision, Inc. v. CBC. Co., Ltd., et al., Civil Action No. 13-cv-1139, filed in the United States District Court for the District of Delaware. The case was dismissed pursuant to a settlement between the parties on August 5, 2014.

A petition for inter partes review of the ' 990 patent was filed on September 3, 2014, the record for which is electronically available through the Patent Review Processing System (PRPS) under Case No. IPR2014-01438. The proceeding was dismissed on November 26, 2014, prior to institution, pursuant to a joint motion to terminate as a result of a settlement between the parties.

There are presently no ongoing proceedings involving the ' 990 patent.

## VI. Conclusion

In view of the foregoing and related Exhibits $1-8 \mathrm{~b}$ and Appendices A-J, ex parte reexamination of claims $1-4,6-7,10-11,15-20,22-23$, and 25 of the ' 990 patent is respectfully requested.

Dated: November 26, 2014

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## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Patent of:
Jean-Claude ARTONNE et al.
Patent No.: 6,844,990 B2
Issue Date: January 18, 2005
For: METHOD FOR CAPTURING AND
DISPLAYING A VARIABLE RESOLUTION
DIGITAL PANORAMIC IMAGE

## PROPOSED AMENDMENT UNDER 37 C.F.R. $\$ \$$ 1.510(e) AND 1.530

This proposed amendment is being submitted pursuant to 37 C.F.R. $\S \S 1.510(\mathrm{e})$ and 1.530 in connection with the concurrently filed request for ex parte reexamination of the aboveidentified patent.

Prior to reexamination, please amend the above-identified U.S. patent as follows:
Amendments to and Listing of Claims Subject to Reexamination begin on page 2 of this paper.

Remarks/Arguments begin on page 10 of this paper.

## AMENDMENTS TO AND LISTING OF CLAIMS SUBJECT TO REEXAMINATION

The following listing of claims subject to reexamination replaces all prior versions, and listings, of claims subject to reexamination.

1. (Cancelled).
2. (Amended) The method according to claim [1] 27, wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
3. (Amended) The method according to claim [1] 27, wherein the objective lens expands the center of the image and compresses the edges of the image.
4. (Amended) The method according to claim [1] 27, wherein the objective lens expands the edges of the image and compresses the center of the image.
5. (Not Subject to Reexamination).

6-7. (Cancelled).

8-9. (Not Subject to Reexamination).
10. (Amended) A method for displaying an initial panoramic image obtained in accordance with the method according to claim 1, the method for displaying comprising: correcting the non-linearity of the initial image, performed by means of a reciprocal function of the non-linear distribution function of the objective lens [or by means of the non-linear distribution function].

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11. (Original) The method according to claim 10, wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.

## 12-14. (Not Subject to Reexamination).

15. (Amended) The method according to claim [10] 27, further comprising: determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the non-linear distribution function, and
allocating to each image point of the display window the color of an image point that is the closest on the initial image.
16. (Original) The method according to claim 15, wherein the projection of the image points of the display window onto the initial image comprises:
projecting the image points of the display window onto a sphere or a sphere portion, determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and
projecting onto the initial image each image point projected onto the sphere or the sphere portion, the projection being performed by means of the non-linear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion.
17. (Original) A panoramic objective lens comprising: optical means for projecting a panorama into an image plane of the objective lens, the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that a panoramic image obtained by means of the objective lens

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comprises at least one substantially expanded zone and at least one substantially compressed zone.
18. (Original) The panoramic objective lens according to claim 17, having a nonlinear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of an image obtained varying according to the field angle of the corresponding object point.
19. (Original) The panoramic objective lens according to claim 17, wherein the lens expands the center of an image and compresses the edges of the image.
20. (Original) The panoramic objective lens according to claim 17, wherein the lens expands the edges of an image and compresses the center of the image.
21. (Not Subject to Reexamination).
22. (Cancelled).
23. (Original) The panoramic objective lens according to claim 22, wherein the set of lenses forming an apodizer comprises at least one aspherical lens.
24. (Not Subject to Reexamination).
25. (Original) The panoramic objective lens according to claim 22, comprising polymethacrylate lenses.
26. (Not Subject to Reexamination).

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27. (New) A method for displaying a digital panoramic image, the method comprising:
obtaining a digital panoramic image by projecting a panorama onto an image sensor using a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to a field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one expanded zone and at least one compressed zone; and
displaying the obtained panoramic image by correcting the non-linearity of the initial image, performed by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function and a size L of the obtained image.
28. (New) The method according to claim 27, wherein the objective lens compresses the center of the image and the edges of the image and expands an intermediate zone of the image located between the center and the edges of the image.
29. (New) The method according to claim 27, wherein the objective lens comprises a set of lenses forming an apodizer.
30. (New) The method according to claim 29, wherein the set of lenses forming an apodizer comprises at least one aspherical lens.
31. (New) The method according to claim 27, wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.
32. (New) A panoramic objective lens comprising:
a set of lenses configured to project a panorama into an image plane of the objective lens, the panoramic objective lens having an image point distribution function that is not linear

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relative to a field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that a panoramic image obtained using the objective lens comprises at least one expanded zone and at least one compressed zone,
wherein the panoramic image obtained by the objective lens is configured to be corrected by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function, and a size L of the obtained image.
33. (New) The lens according to claim 32, wherein the objective lens has a nonlinear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
34. (New) The lens according to claim 32 , wherein the objective lens expands the center of the image and compresses the edges of the image.
35. (New) The lens according to claim 32 , wherein the objective lens expands the edges of the image and compresses the center of the image.
36. (New) The lens according to claim 32 , wherein the objective lens compresses the center of the image and the edges of the image and expands an intermediate zone of the image located between the center and the edges of the image.
37. (New) The lens according to claim 32, wherein the set of lenses comprises at least one aspherical lens.
38. (New) A method for capturing a digital panoramic image, by projecting a panorama onto an image sensor using a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object

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points of the panorama, the distribution function having a maximum divergence of at least $10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one expanded zone and at least two compressed zones.
39. (New) The method according to claim 38, wherein the objective lens has a nonlinear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
40. (New) A method for displaying an initial panoramic image obtained in accordance with the method according to claim 38 , the method for displaying comprising: correcting the non-linearity of the initial image, performed using a reciprocal function of the non-linear distribution function of the objective lens or using the non-linear distribution function.
41. (New) The method according to claim 40 , wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.
42. (New) The method according to claim 41, further comprising:
calculating the size of the corrected image, using the reciprocal function of the distribution function, so that the resolution of the corrected image is equivalent to the most expanded zone of the initial image, and
scanning each image point of the corrected image, searching for the position of a twin point of the image point on the initial image and allocating the color of the twin point to the image point of the corrected image.
43. (New) The method according to claim 41, wherein the initial image and the corrected image comprise an image disk.

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44. (New) The method according to claim 41, further comprising:
transferring the image points of the corrected image into a three-dimensional space, and presenting one sector of the three-dimensional image obtained on a display.
45. (New) The method according to claim 40, further comprising:
determining the color of image points of a display window, by projecting the image points of the display window onto the initial image using the non-linear distribution function, and
allocating to each image point of the display window the color of an image point that is the closest on the initial image.
46. (New) The method according to claim 45, wherein the projection of the image points of the display window onto the initial image comprises:
projecting the image points of the display window onto a sphere or a sphere portion, determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and
projecting onto the initial image each image point projected onto the sphere or the sphere portion, the projection being performed using the non-linear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion.
47. (New) The method according to claim 38, wherein the objective lens compresses at least one zone near the center and at least one zone near the edge, and expands at least one intermediate zone of the image between the center and the edge of the image.
48. (New) A method for capturing a digital panoramic image, by projecting a panorama onto an image sensor by means of a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least

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$+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one expanded zone and at least one compressed zone, wherein the objective lens has a nonlinear distribution function that is not symmetrical relative to the optical axis of the objective lens.

## REMARKS

Reexamination of claims 1-4, 6-7, 10-11, 15-20, 22-23, and 25 of U.S. Patent No. $6,844,990$ ("the ' 990 Patent") has been requested. By virtue of the present proposed amendment, claims 27-48 have been added. Claims 1, 6-7, and 22 have been cancelled. Claim 10 has been amended to clarify the invention. Claims 2-4 and 15 have been amended for formalities only.

Status of Patent Claims pursuant to 37 C.F.R. § 1.530(e):

$$
\begin{aligned}
& 1,6-7 \text {, and } 22 \text { - cancelled; } \\
& 2-4,10-11,15-20,23 \text {, and } 25 \text { - pending (reexamination requested); } \\
& 5,8-9,12-14,21,24 \text {, and } 26 \text { - not subject to reexamination; and } \\
& 27-48-\text { added (new). }
\end{aligned}
$$

No new matter has been added by the claim amendments and the amendments do not enlarge the scope of the original claims. Claim 10 was amended solely to remove one of the alternatives for correcting the non-linearity of the initial image. Claims 2-4 and 15 were amended to depend from new claim 27. Support for the new claims is provided in the chart below:

| New <br> Claim | Support Citations in '990 patent |
| :---: | :--- |
| 27 | Original claim 1; col. 12, ln. 59-col. 14, ln. 35 |
| 28 | Original claim 5 |
| 29 | Original claim 6 |
| 30 | Original claim 7 |
| 31 | Original claim 11 |
| 32 | Original claim 17; col. 12, $\ln .59-c o l . ~ 14, ~ l n . ~ 35 ; ~$ <br> col. 16, ln. 1-col. 17, ln.34; Figs. 15-16 |
| 33 | Original claim 2 |
| 34 | Original claim 3 |
| 35 | Original claim 4 |
| 36 | Original claim 5 |
| 37 | Original claim 7; col. 16, lns. 31-61 |
| 38 | Original claims 1 and 5; col. 9, ln. 53-col. 10, $\ln$. <br> $5 ; ~ F i g . ~ 9 ~$ |
| 39 | Original claim 2 |
| 40 | Original claim 10 |


| New <br> Claim | Support Citations in '990 patent |
| :---: | :--- |
| 41 | Original claim 11 |
| 42 | Original claim 12 |
| 43 | Original claim 13 |
| 44 | Original claim 14 |
| 45 | Original claim 15 |
| 46 | Original claim 16 |
| 47 | Original claim 5 |
| 48 | Original claim 1; col. 18, Ins. 17-28 |

Accordingly, entry of the proposed amendments to the claims is respectfully requested.

## Claim 10

Claim 10 has been amended to remove "or by means of the non-linear distribution function." Thus, the only method remaining in claim 10 for correcting the non-linearity of the initial image is "by means of a reciprocal function of the non-linear distribution function of the objective lens." As described below, claim 10, as amended, would not have been obvious over the combinations of Nagaoka and Shiota, Nagaoka and Matsui, and Baker and Shiota proposed in the reexamination request

Neither Nagaoka nor Baker teaches a specific method for correcting the images captured by their respective panoramic lenses. Shiota discloses image correction through mapping of coordinates onto the image. The projection process includes the use of the non-linear distribution function of the lens to obtain certain coordinates. (Shiota at paras. [0001], [0022], [0028]-[0041]). However, in all instances, Shiota utilizes the non-linear distribution function itself, and does not teach the use of a reciprocal function of the non-linear distribution function as a way to correct the non-linearity of the initial image.

Matsui similarly discloses image correction by virtue of using the distribution function $h$ $=\mathrm{g}($ ), which can be non-linear (see e.g., $\mathrm{h}=2 \mathrm{f} \cdot \tan (/ 2)$ ), to calculate points $\mathrm{P} 1, \mathrm{P} 2$ in projecting the image onto a cylindrical surface C. (Matsui at paragraphs [0023], [0025], [0030]-[0031]). Matsui, like Shiota, does not disclose using a reciprocal function of the non-linear distribution function to correct the original image. It has previously been suggested that paragraphs [0030]-

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[0031] of Matsui teach this feature, but this assertion is incorrect. These paragraphs teach the use of the inverse tangent function when is unknown. However, the distribution function itself is still used to obtain P1 and P2, but with a formula substituted in for . (Matsui at paras. [0030][0031]). A reciprocal of $\mathrm{g}(\mathrm{)}$ is not taught by Matsui for use in image correction.

When combining two or more references to establish a prima facie case of obviousness, the references together must teach or suggest all of the claim elements. In re Royka, 490 F.2d 981, 985 (C.C.P.A. 1974). Furthermore, "[a]ll words in a claim must be considered in judging the patentability of that claim against the prior art." In re Wilson 424 F.2d 1382, 1385 (CCPA 1970); M.P.E.P. § 2143.03. Accordingly, claim 10, as amended, would not have been obvious over any combination of Nagaoka and Shiota, Nagaoka and Matsui, or Baker and Shiota, because none of the combinations teaches or suggests correcting the non-linearity of the initial image by means of a reciprocal function of the non-linear distribution function of the objective lens. For at least this reason, Patent Owner submits that amended claim 10 is patentable over the cited references.

## New Claims

Claims 27-48 are believed to be patentable over the references cited in the reexamination request for at least the following reasons.

## Claims 2-4, 15, 16, and 27-37

Claim 27 recites that the non-linearity of the initial image is corrected by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function and a size $L$ of the obtained image. For example, the initial image may be in the form of an image disk having a size L , which may be provided in the number of pixels. Image points $p(p u, p v)$ corresponding to image points $E(i, j)$ of, for example, a display window, can be obtained using equations that multiply, among other things, the size of the image disk L with the non-linear distribution function at an angle $\square$ (e.g., $\mathrm{pu}=\mathrm{L} * \mathrm{U}^{*} \mathrm{Fd}(\square)$ and $\mathrm{pv}=$ L*V*Fd( $)$ ). Claim 32 contains a similar recitation.

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The references all fail to teach or suggest this feature of claims 27 or 32 . As described above with respect to claim 10, Nagaoka, Baker, and Fisher do not describe any specific method for correcting the image. As for Shiota, the second projection points $\mathrm{p}_{1}$ and $\mathrm{q}_{1}$ are obtained using a coefficient $\mathrm{k}_{2}$, which is equal to the distribution function divided by a distance r from the origin of the image disk to a point Q on the image disk. The coefficient $\mathrm{k}_{2}$ is then multiplied by corresponding coordinates $\mathrm{X}_{2}, \mathrm{Y}_{2}$ on a hemisphere. (Shiota at Fig. 1; paras. [0033]-[0041]). The size of the image disk is not utilized to correct the image.

In Matsui, coordinates of a point P1 are obtained by multiplying the distribution function by $\cos \square$ and $\sin \square$, where $\square$ represents an angle in the plane of the image disk of a point on the image disk. (Matsui at Figs 2-3; translation at paras. [0025], [0030]-[0031]). The size of the image disk is not taken into account for image correction. Enami also does not use the size of the image disk to correct the initial image. (Enami translation at paras. [0065]-[0074]). Inoue does not disclose any image correction techniques.

None of the other references teaches the use of the size of the image disk in correcting the non-linearity of the initial image. Accordingly, claims 27 and 32 are believed to be patentable over the references cited in the reexamination request. Claims 28-31 are dependent on claim 27, and claims 33-37 are dependent on claim 32. Thus, claims 28-31 and 33-37 are believed to be patentable over the references cited in the reexamination request due at least to their dependence on claim 38.

Moreover, based on the proposed amendments, claims 2-4 and 15-16 all depend from new claim 27, and are therefore believed to be patentable over the references cited in the reexamination request due at least to their dependence on claim 27.

## Claims 38-47

Claim 38 recites that the panoramic image obtained using a panoramic objective lens has at least one expanded zone and at least two compressed zones. For example, Fig. 9 of the '990 patent shows a non-linear distribution function having a compressed zone between $0^{\circ}$ and $30^{\circ}$, an

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expanded zone between $30^{\circ}$ and $70^{\circ}$, and another compressed zone between $70^{\circ}$ and $90^{\circ}$. None of the cited references discloses this feature.

In Nagaoka, only two of the illustrated distribution functions have both an expanded zone and a compressed zone ( $\mathrm{h}=1.6 \mathrm{f} \tan (/ 2$ ) and $\mathrm{h}=1.2 \mathrm{f} \tan (/ 1.6)$ ). (See Nagaoka at Figs. 3A, 3B). This is demonstrated through the comparison of the slope at different angles compared with the linear distribution function $(\mathrm{h}=\mathrm{f})$. That is, shallower slopes indicate compression and steeper slopes indicate expansion. None of the distribution functions shown in Nagaoka have two compressed zones in addition to an expanded zone.

In Baker, no specific distribution function is given, but Baker's stated purpose is to compress the center of the image while expanding the periphery. (Baker at col. 8, lns. 32-62). Fig. 3BB shows only two zones in the image, one compressed ( $\mathrm{X}^{\prime}$ ) and the other expanded ( $\mathrm{Y}^{\prime}$ ). Thus, Baker does not teach the image having at least two compressed zones in addition to an expanded zone.

Fisher uses the distribution function of $\mathrm{H}=\sin ^{1 / 3}$, which is plotted in Fig. 3 along with the linear distribution function. As can be seen from Fig. 3, Fisher's lens will create an expanded zone in the center, and one compressed zone starting at around $30^{\circ}$ and extending to the edge. This is in accordance with Fisher's goal, which is to have objects near the optical axis of the lens occupy a disproportionately large area of the image sensor. (Fisher at col. 2, lns. 19-24).

None of the other references teaches a distribution function that creates an image having at least two compressed zones and at least one expanded zone either. Accordingly, claim 38 is believed to be patentable over the references cited in the reexamination request. Claims 39-47 are dependent on claim 38, and are also believed to be patentable over the references cited in the reexamination request due at least to their dependence on claim 38 .

## Claim 48

Claim 48 recites that the objective lens has a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens. That is, the position of an image

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point may vary not only with the field angle of the corresponding object point relative to the optical axis, but also with the angle of the corresponding object point in the image plane. Thus, image points would not be distributed in concentric circles, as with symmetric distribution functions.

None of the main references teaches a non-symmetrical distribution function. In Nagaoka, for example, all of the images show concentric circular distributions of image points, indicating symmetric distribution functions. (Nagaoka at Figs. 4A-4D). Baker similarly shows a concentric circular distribution of image points. (Baker at Fig. 3BB). Fig. 4 of Fisher also implies that the variations in image height are due only to field angle. (Fisher at Fig. 4). None of the other references cited in the reexamination teaches or suggests a non-symmetrical distribution function either. Accordingly, claim 48 is believed to be patentable over the references cited in the reexamination request.

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|  | FILING OR 371(c) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SERIAL NUMBER |  |  |  |  |
| $90 / 013,410$ | $11 / 26 / 2014$ | CLASS | GROUP ART UNIT | ATTORNEY <br> DOCKET NO. |
|  | RULE | 359 | 3992 | $688266-21$ RX |

AIA (First Inventor to File): YES

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** CONTINUING DATA
This application is a REX of 10/706,513 11/12/2003 PAT 6844990 which is a CON of PCT/FR02/01588 05/10/2002
** FOREIGN APPLICATIONS
FRANCE 0106261 05/11/2001

| Foreign Priority claimed $\square_{\text {yes }} \square_{\text {no }}$ <br> 35 USC 119 (a-d) conditions  <br> met  <br> Verified and <br> Acknowledged $\square_{\text {yes }}$ <br> Allowance $\quad$Met after <br> Examiner's Signature | STATE OR COUNTRY | SHEETS DRAWING | $\begin{gathered} \text { TOTAL } \\ \text { CLAIMS } \\ 26 \end{gathered}$ | INDEPENDEN CLAIMS 2 |
| :---: | :---: | :---: | :---: | :---: |

## ADDRESS

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TITLE
METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE

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Page 2 of 2


## Patent Assignment Abstract of Title



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Alexandria, Yíginia 22313-1450
REEXAM CONTROL NUMBER
90/013,410

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| 90/013,410 | 11/26/2014 | 6844990 |
|  |  | CONFIRMATION NO. 4682 |
| 570 |  | REEXAMINATION REQUEST |
| PANITCH SCHWARZE BELISARIO \& NADEL LLP |  | NOTICE |
| ONE COMMERCE SQUARE |  |  |
| 2005 MARKET STREET, SUITE 2200 |  |  |
| PHILADELPHIA, PA 19103 |  |  |

Date Mailed: 12/02/2014

## NOTICE OF REEXAMINATION REQUEST FILING DATE

(Patent Owner Requester)
Requester is hereby notified that the filing date of the request for reexamination is $11 / 26 / 2014$, the date the required fee of $\$ 2,520$ was received. (See CFR 1.510(d)).
A decision on the request for reexamination will be mailed within three months from the filing date of the request for reexamination. (See 37 CFR 1.515(a)).

Pursuant to 37 CFR 1.33(c), future correspondence in this reexamination proceeding will be with the latest attorney or agent of the record in the patent file.

The paragraphs checked below are part of this communication:
$\qquad$ 1. The party receiving the courtesy copy is the latest attorney or agent of record in the patent file.
__ 2. The person named to receive the correspondence in this proceeding has not been made the latest attorney or agent of record in the patent file because:
$\qquad$ A. Requester's claim of ownership of the patent is not verified by the record.
$\qquad$ B. The request papers are not signed with a real or apparent binding signature.
C. The mere naming of a correspondence addressee does not result in that person being appointed as the latest attorney or agent of record in the patent file.
3. Addressee is the latest attorney or agent of record in the patent file.
4. Other $\qquad$
/rbell/
Legal Instruments Examiner
Central Reexamination Unit 571-272-7705; FAX No. 571-273-9900

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Date Mailed: 12/02/2014

## NOTICE OF ASSIGNMENT OF REEXAMINATION REQUEST

The above-identified request for reexamination has been assigned to Art Unit 3992. All future correspondence to the proceeding should be identified by the control number listed above and directed to the assigned Art Unit.

A copy of this Notice is being sent to the latest attorney or agent of record in the patent file or to all owners of record. (See 37 CFR 1.33(c)). If the addressee is not, or does not represent, the current owner, he or she is required to forward all communications regarding this proceeding to the current owner(s). An attorney or agent receiving this communication who does not represent the current owner(s) may wish to seek to withdraw pursuant to 37 CFR 1.36 in order to avoid receiving future communications. If the address of the current owner(s) is unknown, this communication should be returned within the request to withdraw pursuant to Section 1.36.

## /rbell/

Legal Instruments Examiner
Central Reexamination Unit 571-272-7705; FAX No. 571-273-9900

## Litigation Search Report CRU 3999

Reexam Control No. 90/013,410

| TO: Examiner |
| :--- |
| Location: CRU |
| Art Unit: 3992 |
| Date: $12 / 04 / 14$ |
| Case Serial Number: $90 / 013,410$ |

From: Tredelle Jackson
Location: CRU 3999
MDE 4B21
Phone: (571) 272-2783
Tredelle.Jackson@uspto.gov

## Search Notes

Litigation Search for U.S. Patent Number 6,844,990.
Sources:
Status (OPEN) IPR2014-01438 Panasonic System Networks Co., Ltd. Vs. 6115187 CANADA INC.
Status (CLOSED) 1:13cv1139 Immervision Inc. V. Cbc Co. Ltd. Et Al
Status (CLOSED) 2:13cv1117 Immervision, Inc. V. Vivotek, Inc.

1) I performed a KeyCite Search in Westlaw, which retrieves all history on the patent including any litigation.
2) I performed a search on the patent in Lexis CourtLink for any open dockets or closed cases.
3) I performed a search in Lexis in the Federal Courts and Administrative Materials databases for any cases found.
4) I performed a search in Lexis in the IP Journal and Periodicals database for any articles on the patent.
5) I performed a search in Lexis in the news databases for any articles about the patent or any articles about litigation on this patent.

## KEYCITE

C US PAT 6844990 METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE, Assignee: 6115187 Canada Inc. (Jan 18, 2005)

History

## Direct History

=> I METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE, US PAT 6844990, 2005 WL 109751 (U.S. PTO Utility Jan I8, 2005)

## Patent Family

2 PANORAMIC DIGITAL IMAGE PROCESSING SYSTEM USES WIDE ANGLE LENS CAUSING IMAGE DISTORTION, AND DIGITAL PROCESSING COUNTERACTING DISTORTION, Derwent World Patents Legal 2003-148422

## Patent Status Files

.. AIA Trial Proceedings Filed before The Patent Trial and Appeal Board, (OG DATE: Oct 28, 2014)
.. Patent Suit(See LitAlert Entries),
.. Patent Suit(See LitAlert Entries),
.. Certificate of Correction, (OG DATE: Jun 14, 2005)

## Docket Summaries

7 IMMERVISION INC. v. CBC CO. LTD. ET AL, (D.DEL. Jun 25, 2013) (NO. 1:13CV0I139), ( 35 USC 27I PATENT INFRINGEMENT)
8 IMMERVISION, INC. v. VIVOTEK, INC. ET AL, (D.NEV. Jun 25, 2013) (NO. 2:13CV01117), (35 USC I45 PATENT INFRINGEMENT)

## Litigation Alert

9 Derwent LitAlert P2013-35-01 (Jun 25, 2013) Action Taken: NOTICE TO COUNSEL PURSUANT TO LOCAL RULE IA 10-2 COUNSEL FREDERICK A TECCE, JOHN D. SIMMONS, STEPHEN E MURRAY TO COMPLY WITH COMPLETION AND ELECTRONIC FILING OF THE DESIGNATION OF LOCAL COUNSEL AND VERIFIED PETITION
10 Derwent LitAlert P2013-26-137 (Jun 25, 2013) Action Taken: CAUSE - 35 USC 271 - COMPLAINT FOR PATENT INFRINGEMENT
11 Derwent LitAlert P2013-26-140 (Jun 25, 2013) Action Taken: CAUSE-35 USC 145-COM-

Prior Art (Coverage Begins 1976)

| C | I2 DEFORMABLE MIRROR, US PAT 5880896Assignee: Sharp Kabushiki Kaisha, (U.S. PTO Utility 1999) |
| :---: | :---: |
| C | 13 INNOVATIVE DEFORMABLE MIRROR ACTUATOR CONFIGURATION, US PAT 5745278Assignee: Raytheon Optical Systems, Inc., (U.S. PTO Utility 1998) |
| C | 14 INTEGRATED PANORAMIC AND HIGH RESOLUTION SENSOR OPTICS, US PAT 5710661 Assignee: Hughes Electronics, (U.S. PTO Utility 1998) |
| C | 15 NON-LINEAR LENS, US PAT 3953111 Assignee: McDonnell Douglas Corporation, (U.S. PTO Utility 1976) |
| C | 16 OMNIRAMIC OPTICAL SYSTEM HAVING CENTRAL COVERAGE MEANS WHICH IS ASSOCIA TED WITH A CAMERA, PROJECTOR, OR SIMILAR ARTICLE, US PAT 6333826 (U.S. PTO Utility 2001) |
| C | 17 SOLID CATADIOPTRIC OMNIDIRECTIONAL OPTICAL SYSTEM HAVING CENTRAL COVERAGE MEANS WHICH IS ASSOCIATED WITH A CAMERA, PROJECTOR, MEDICAL INSTRUMENT, OR SIMILAR ARTICLE, US PAT 6449103 (U.S. PTO Utility 2002) |
| C | 18 WIDE-ANGLE LENS, US PAT 6031670Assignee: Sankyo Seiki Mfg. Co., Ltd., (U.S. PTO Utility 2000) |

# United States Patent Trial and Appeals Board 

US Patent Trial and Appeals Board - Alexandria
(Alexandria)
IPR2014-01438
Panasonic System Networks Co., Ltd. Vs. 6115187 CANADA INC.
This case was retrieved from the court on Wednesday, November 12, 2014

| Header |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Case Number: IPR2014-01438 |  |  |  |  |  |
| Date Filed: 09/03/2014 |  |  |  |  |  |
| Date Full Case Retrieved: $11 / 12 / 2014$ |  |  |  |  |  |
| Status: Open |  |  |  |  |  |
| Misc: Civil |  |  |  |  |  |
| [Summary][Participants][Proceedings] |  |  |  |  |  |
| Summary |  |  |  |  |  |
| Court Case Status: Pending |  |  |  |  |  |
| Case Type: IPR: Inter partes review |  |  |  |  |  |
| Technical Center Number: 2800 |  |  |  |  |  |
| Patent Application Number: 10706513 |  |  |  |  |  |
| Patent Number: 6844990 |  |  |  |  |  |
| Participants |  |  |  |  |  |
| Litigants |  |  |  |  |  |
| Panasonic System Networks Co., Ltd. |  |  |  |  |  |
| Petitioner |  |  |  |  |  |
| 6115187 Canada Inc. |  |  |  |  |  |
| PatentOwner |  |  |  |  |  |
| Proceedings |  |  |  |  |  |
| File Date | Details | Document Type | $\begin{aligned} & \text { Paper/Exhibit } \\ & \text { No. } \end{aligned}$ | Filed By | Public? |
| 09/03/2014 | Power of Attorney | Power of Attorney | 1 | Petitioner | Yes |
| 09/03/2014 | IPR Petition | Petition | 2 | Petitioner | Yes |
| 09/03/2014 | U.S. Patent No. 6,844,990 | Exhibit | 1001 | Petitioner | Yes |
| 09/03/2014 | U.S. Patent No. 5,686,957 | Exhibit | 1002 | Petitioner | Yes |
| 09/03/2014 | U.S. Patent No. 6,128,145 | Exhibit | 1003 | Petitioner | Yes |


| 09/03/2014 | U.S. Patent No. 3,953,111 | Exhibit | 1004 | Petitioner | Yes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 09/03/2014 | Ep 1386480 B1 | Exhibit | 1005 | Petitioner | Yes |
| 09/03/2014 | EP 1386480 B1 Amendment of May 6, 2010 | Exhibit | 1006 | Petitioner | Yes |
| 09/03/2014 | U.S. Patent No. 6,031,670 | Exhibit | 1007 | Petitioner | Yes |
| 09/03/2014 | European Patent Publication EP 1028389 A2 | Exhibit | 1008 | Petitioner | Yes |
| 09/03/2014 | Japanese Patent Publication P2000-242773A | Exhibit | 1009 | Petitioner | Yes |
| 09/03/2014 | English translation of Matsui with verification | Exhibit | 1010 | Petitioner | Yes |
| 09/03/2014 | Japanese Unexamined <br> Patent Application <br> Publication 11-261868 | Exhibit | 1011 | Petitioner | Yes |
| 09/03/2014 | English translation of Enami | Exhibit | 1012 | Petitioner | Yes |
| 09/03/2014 | Declaration of Jack Feinberg, Ph.D. | Exhibit | 1013 | Petitioner | Yes |
| 09/03/2014 | Declaration of Shishir K: Shah, Ph.D. | Exhibit | 1014 | Petitioner | Yes |
| 09/11/2014 | Notice of Filing Date Accorded to Petition and Defective Petition | Notice of Filing Date Accorded to Petition | 3 | Board | Yes |
| 09/16/2014 | Response to Notice | Reply | 4 | Petitioner | Yes |
| 09/16/2014 | Amended Petition | Reply | 5 | Petitioner | Yes |
| 09/23/2014 | Notice of Accepting Corrected Petition | Notice | 6 | Board | Yes |
| 09/24/2014 | Power of Attorney | Power of Attorney | 7 | Potential <br> Patent Owner | Yes |
| 09/24/2014 | Related Matters | Notice | 8 | Potential Patent Owner | Yes |

[^7]
## US District Court Civil Docket

## U.S. District - Delaware <br> (Wilmington)

## 1:13cv1139

Immervision Inc. v. Cbc Co. Ltd. et al

This case was retrieved from the court on Friday, August 16, 2013

```
            Date Filed: 06/25/2013
            Assigned To: Judge Sue L. Robinson
            Referred To: Judge Sherry R. Fallon
Nature of suit: Patent (830)
            Cause: Patent Infringement
        Lead Docket: None
Other Docket: None
                            None
                            None
                                    None
                                    None
    Jurisdiction: Federal Question
```




6115187 Canada Inc. doing business as ImmerVision Inc. Plaintiff

Cbc Co. Ltd. Defendant

Cbc (America) Corporation Defendant

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doing business as
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Counter Defendant
Cbc (America) Corporation
Counter Claimant

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Cbc Co. Ltd.
Counter Claimant

Immervision Inc.
[Term: 03/11/2014]
Counter Defendant

```
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302-777-0338
Fax: 302-421-5870
Email:Mfarnan@farnanlaw.Com
```

| Date | \# | Proceeding Text | Source |
| :---: | :---: | :---: | :---: |
| 06/25/2013 | 1 | COMPLAINT filed with Jury Demand against CBC (America) Corporation, CBC Co. Ltd. - Magistrate Consent Notice to Pltf. ( Filing fee $\$ 400$, receipt number 311-1317132.) - filed by ImmerVision Inc.. (Attachments: \# 1 Exhibit A, \# 2 Exhibit B, \# 3 Exhibit C, \# 4 Civil Cover Sheet)(dmp, ) (Entered: 06/26/2013) |  |
| 06/25/2013 | 2 | Notice, Consent and Referral forms re: U.S. Magistrate Judge jurisdiction. (dmp, ) (Entered: 06/26/2013) |  |
| 06/25/2013 | 3 | Report to the Commissioner of Patents and Trademarks for Patent/Trademark Number(s) US 6,844,900 B2; (dmp, ) (Entered: 06/26/2013) |  |
| 06/25/2013 |  | No Summons Issued. (dmp, ) (Entered: 06/26/2013) |  |
| 07/03/2013 |  | Case Assigned to Judge Sue L. Robinson. Please include the initials of the Judge (SLR) after the case number on all documents filed. (rjb) (Entered: 07/03/2013) |  |
| 10/15/2013 | 4 | WAIVER OF SERVICE returned executed by ImmerVision Inc.: For CBC Co. Ltd. waiver sent on 10/14/2013, answer due 1/13/2014. (Farnan, Joseph) (Entered: 10/15/2013) | Events <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 10/15/2013 | 5 | WAIVER OF SERVICE returned executed by ImmerVision Inc.: For CBC (America) Corporation waiver sent on 10/14/2013, answer due 12/13/2013. (Farnan, Joseph) (Entered: $10 / 15 / 2013)$ | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 12/10/2013 | 6 | MOTION for Extension of Time to Respond to Complaint Unopposed - filed by ImmerVision Inc.. (Attachments: \# 1 Text of Proposed Order)(Farnan, Michael) (Entered: 12/10/2013) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 12/12/2013 | -- | SO ORDERED, re 6 MOTION for Extension of Time to Respond to Complaint - Unopposed filed by ImmerVision Inc., Set/Reset Answer Deadlines: CBC (America) Corporation answer due $1 / 13 / 2014$. CBC Co. Ltd answer due $1 / 13 / 2014$. Signed by Judge Sue L. Robinson on 12/12/2013. (fms) (Entered: 12/12/2013) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 01/13/2014 | 7 | ANSWER to 1 Complaint, with Jury Demand, COUNTERCLAIM against ImmerVision Inc. by CBC (America) Corporation, CBC Co. Ltd..(Wilson, Samantha) (Entered: 01/13/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 01/13/2014 | 8 | Disclosure Statement pursuant to Rule 7.1: No Parents or Affiliates Listed filed by CBC Co. Ltd.. (Wilson, Samantha) (Entered: 01/13/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 01/13/2014 | 9 | Disclosure. Statement pursuant to Rule 7.1: identifying Corporate Parent CBC Co. Ltd. for CBC (America) Corporation, CBC (America) Corporation filed by CBC (America) Corporation. (Wilson, Samantha) (Entered: 01/13/2014) | Events <br> <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 01/13/2014 | 10 | MOTION for Pro Hac Vice Appearance of Attorney Nick G. Saros, Miwa Shoda, Kristopher R. Kiel and Yusuf Esat - filed by CBC (America) Corporation, CBC Co. Ltd.. (Sharp, Melanie) (Entered: 01/13/2014) | Events <br> <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 01/14/2014 | -- | SO ORDERED, re 10 MOTION for Pro Hac Vice Appearance of | Events |


|  | Attorney Nick G. Saros, Miwa Shoda, Kristopher R. Kiel and <br> Yusuf Esat filed by CBC (America) Corporation, CBC Co. Ltd. <br> Signed by Judge Sue L. Robinson on 1/14/2014. (fms) (Entered: | <br>since\&nbsplast <br> <br>full\&nbspupdate |
| :--- | :--- | :--- | :--- | :--- |
|  | 01/14/2014) |  |


|  |  | Construction Reply Brief due by $2 / 19 / 2015$. Claim Construction Surreply Brief due by $3 / 5 / 2015$. A Final Pretrial Conference is set for 2/10/2016 at 04:30 PM in Courtroom 4B before Judge Sue L. Robinson. A Jury Trial is set for 3/7/2016 at 09:00 AM in Courtroom 4B before Judge Sue L. Robinson. Signed by Judge Sue L. Robinson on 3/10/2014. (nmfn) (Entered: 03/10/2014) |  |
| :---: | :---: | :---: | :---: |
| 03/11/2014 | -- | SO ORDERED, re 16 Stipulation To Amend Caption. Signed by Judge Sue L. Robinson on 3/11/2014. (fms) (Entered: 03/11/2014) | Events <br> <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 03/12/2014 | 19 | ORDER Setting Mediation Conferences: A Mediation Conference is set for 4/15/2014 and 4/16/2014 at 10:00 AM in Courtroom 6C before Judge Sherry R. Fallon. Signed by Judge Sherry R. Fallon on 3/12/2014. (lih) (Entered: 03/12/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 03/17/2014 | 20 | NOTICE OF SERVICE of Plaintiff ImmerVision's Initial Disclosures Pursuant to Federal Rule 26(a)(1)(A) filed by 6115187 Canada Inc..(Farnan, Michael) (Entered: 03/17/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 03/17/2014 | 21 | NOTICE OF SERVICE of Defendants' Rule 26(a)(1) Initial Disclosures filed by CBC (America) Corporation, CBC Co. Ltd.. (Sharp, Melanie) (Entered: 03/17/2014) | Events <br> <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 03/17/2014 | 22 | NOTICE of Withdrawal of Kristopher R. Kiel as Counsel for Defendants CBC Co., Ltd and CBC (America) Corporation by CBC (America) Corporation, CBC Co. Ltd. (Wilson, Samantha) (Entered: 03/17/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 03/24/2014 | 23 | Letter to Counsel from Judge Robinson regarding changes to the way the Court processes patent cases. (nmfn) (Entered: $03 / 24 / 2014)$ | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 03/26/2014 | 24 | Order Setting Patent Scheduling Conference: An In-Person Scheduling Conference is set for 4/21/2014 at 01:00 PM in Courtroom 4B before Judge Sue L. Robinson. Signed by Judge Sue L. Robinson on 3/26/2014. (nmfn) (Entered: 03/26/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 04/09/2014 | 25 | Joint STIPULATION TO EXTEND TIME for the parties to exchange disclosures pursuant to Paragraph 3 of the Default Standard for Discovery, and for plaintiff to produce information pursuant to Paragraph 4 of same to May 9, 2014 - filed by CBC (America) Corporation, CBC Co. Ltd.. (Wilson, Samantha) (Entered: 04/09/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 04/10/2014 | -- | SO ORDERED, re 25 Joint STIPULATION TO EXTEND TIME for the parties to exchange disclosures pursuant to Paragraph 3 of the Default Standard for Discovery; and for plaintiff to produce information pursuant to Paragraph 4 of same to May 9, 2014 filed by CBC (America) Corporation, CBC Co. Ltd. Signed by Judge Sue L. Robinson on 4/10/2014. (fms) (Entered: $04 / 10 / 2014)$ | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 04/18/2014 | 26 | PROPOSED ORDER Revised Scheduling Order by 6115187 <br> Canada Inc.. (Attachments: \# 1 Letter to The Honorable Sue L. Robinson)(Farnan, Michael) (Entered: 04/18/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 04/21/2014 | -- | Reset Hearings: The In-Person Scheduling Conference has been rescheduled per request of counsel for 5/19/2014 at 04:30 PM in Courtroom 4B before Judge Sue L. Robinson. (nmfn) (Entered: 04/21/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 04/24/2014 | -- | ORAL ORDER- IT IS HEREBY ORDERED that: a Telephone Mediation Conference is set for 5/1/2014 at 12:00 PM before Judge Sherry R. Fallon. Ordered by Judge Sherry R. Fallon on 4/24/2014. (lih) (Entered: 04/24/2014) | Events <br> <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 05/09/2014 | 27 | NOTICE OF SERVICE of CBC's Disclosures Pursuant to Paragraph | Events |


|  |  | 3 of the District of Delaware Default Standard for Discovery, Including Discovery of Electronically Stored Information ("ESI") filed by CBC (America) Corporation, CBC Co. Ltd..(Sharp, Melanie) (Entered: 05/09/2014) | <br>since\&nbsplast <br> <br>full\&nbspupdate |
| :---: | :---: | :---: | :---: |
| 05/09/2014 | 28 | NOTICE OF SERVICE of (i) Plaintiff ImmerVision's Electronic Discovery Disclosures and (ii) Plaintiff ImmerVision's Initial Patent Disclosures filed by 6115187 Canada Inc..(Farnan, Michael) (Entered: 05/09/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 05/16/2014 | -- | The scheduling conference originally set for 5/19/2014 at 4:30 p.m. has been cancelled. It will be rescheduled soon. (nmfn) (Entered: 05/16/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 05/16/2014 | -- | Reset Hearings: The In-Person Scheduling Conference is rescheduled for 6/24/2014 at 04:30 PM in Courtroom 4B before Judge Sue L. Robinson. (nmfn) (Entered: 05/16/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 06/03/2014 | -- | Reset Hearings: The In-Person Scheduling Conference is rescheduled for 6/24/2014 at 03:30 PM in Courtroom 4B before Judge Sue L. Robinson. (nmfn) (Entered: 06/03/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 06/05/2014 | 29 | PROPOSED ORDER Stipulated Protective Order by 6115187 Canada Inc.. (Farnan, Michael) (Entered: 06/05/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 06/06/2014 | -- | SO ORDERED, re 29 Proposed Stipulated Protective Order filed by 6115187 Canada Inc.: Signed by Judge Sue L. Robinson on 6/6/2014. (fms) (Entered: 06/06/2014). | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 06/10/2014 | 30 | NOTICE OF SERVICE of Core Technical Documents Pursuant to Paragraph 4(b) of the D. Del. Default Standard for Discovery filed by CBC (America) Corporation, CBC Co. Ltd..(Wilson, Samantha) (Entered: 06/10/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 06/23/2014 | 31 | PROPOSED ORDER Scheduling Order by 6115187 Canada Inc.. (Attachments: \# 1 Letter to The Honorable Sue L. Robinson) (Farnan, Michael) (Entered: 06/23/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 06/24/2014 | -- | Minute Entry for proceedings held before Judge Sue L. Robinson - Scheduling Conference held on 6/24/2014. (Court Reporter V. Gunning.) Counsel to submit the final proposed scheduling order to the court. (nmfn) (Entered: 06/24/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 06/25/2014 | 32 | PROPOSED ORDER Scheduling Order by 6115187 Canada Inc.. (Attachments: \# 1 Letter to The Honorable Sue L. 'Robinson) (Farnan, Michael) (Entered: 06/25/2014) | Events <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 06/26/2014 | -- | SO ORDERED, re 32 SCHEDULING ORDER: Case referred to the Magistrate Judge for the purpose of exploring ADR. Case referred to the Magistrate Judge for discovery and all motions to dismiss, to amend, to transfer and any discovery motions permitted by a Magistrate Judge. ( Joinder of Parties due by 12/8/2014., Amended Pleadings due by 12/8/2014., Discovery due by $7 / 15 / 2015$., A Status Conference re: Expert Discovery is set for $6 / 18 / 2015$ at 04:30 PM in Courtroom 4B before Judge Sue L. Robinson, Dispositive Motions due by $8 / 21 / 2015$., An Oral Argument is set for 11/19/2015 at 01:00 PM in Courtroom 4B before Judge Sue L. Robinson., Claim Construction Opening Brief due by $1 / 15 / 2015$., Claim Construction Answering Brief due by 2/5/2015., Claim Construction Reply Brief due by 2/19/2015., Claim Construction Surreply Brief due by 3/5/2015., A Markman Hearing is set for 3/27/2015 at 09:30 AM in Courtroom 4B before Judge Sue L. Robinson., A Final Pretrial Conference is set for 2/10/2016 at 04:30 PM in Courtroom 4B before Judge Sue L. Robinson., A Jury Trial is set for 3/7/2016 at 09:00 AM in Courtroom 4B before Judge Sue L. Robinson.). Signed by Judge | Events <br>since\&nbsplast <br>full\&nbspupdate |

Sue L. Robinson on 6/26/2014. (nmfn) (Entered: 06/26/2014)

| 06/27/2014 | 33 | NOTICE OF SERVICE of Plaintiff ImmerVision's Damages Model under Paragraph 1 (c) (2) of Patent Replacement Scheduling Order filed by 6115187 Canada Inc..(Farnan, Michael) (Entered: 06/27/2014) | Events <br> <br>since\&nbsplast <br> <br>full\&nbspupdate |
| :---: | :---: | :---: | :---: |
| 07/09/2014 | 34 | STIPULATION TO EXTEND TIME for Initial Claim Chart and Initial Invalidity Contentions to 8/8/2014 and 9/8/2014 respectively filed by 6115187 Canada Inc.. (Farnan, Michael) (Entered: 07/09/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 08/05/2014 | 35 | STIPULATION of Dismissal by 6115187 Canada Inc.. (Farnan, Michael) (Entered: 08/05/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |
| 08/05/2014 | -- | CASE CLOSED per D.I. 35 . (nmfn) (Entered: 08/05/2014) | Events <br> <br>since\&nbsplast <br> <br>full\&nbspupdate |
| 08/07/2014 | 36 | Report to the Commissioner of Patents and Trademarks for Patent/Trademark Number(s) US 6,844,900 B2. (Attachments: \# 1 Stipulation)(fms) (Entered: 08/07/2014) | Events <br>since\&nbsplast <br>full\&nbspupdate |

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## US District Court Civil Docket

## U.S. District - Nevada

(Las Vegas)

## 2:13cv1117

Immervision, Inc. v. Vivotek, Inc.
This case was retrieved from the court on Friday, August 16, 2013

Date Filed: 06/25/2013
Assigned To: Judge Andrew P. Gordon Referred To: Magistrate Judge Carl W. Hoffman

Nature of suit: Patent (830)
Cause: Patent Infringement
Lead Docket: None
Other Docket: None
Jurisdiction: Federal Question

Class Code: CLOSED
Closed: 09/27/2013
Statute: 35:145
Jury Demand: Plaintiff
Demand Amount: \$0
NOS Description: Patent

Litigants
Immervision, Inc.
Plaintiff

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Vivotek, Inc.
Defendant
Vivotek USA, Inc.
Defendant
Vivotek Holdings, Inc.
Defendant

Date \#

## Proceeding Text

Source
06/25/2013 1 COMPLAINT against Vivotek, Inc. (Filing fee $\$ 400$ receipt number 0978-2866350), filed by ImmerVision, Inc.. Certificate of Interested Parties due by $7 / 5 / 2013$. Proof of service due by 10/23/2013. (Attachments: \# 1 Exhibit Ex. A to Complaint, \# 2 Exhibit Ex. B to Complaint, \# 3 Exhibit Ex. C to Complaint, \# 4 Civil Cover Sheet Civil Cover Sheet) (Ballif, Philip) (Entered: 06/25/2013)

06/25/2013 Case assigned to Judge Andrew P. Gordon and Magistrate Judge Carl W. Hoffman. Nature of Suit: 830 Patent Case (MAJ) (Entered: 06/25/2013)
06/25/2013 2 NOTICE PURSUANT TO LOCAL RULE IB 2-2: In accordance with 28 USC § 636(c) and FRCP 73, the parties in this action are provided with a link to the "AO 85 Notice of Availability, Consent, and Order of Reference - Exercise of Jurisdiction by a U.S. Magistrate Judge" form on the Court's website www.nvd.uscourts.gov. Consent forms should NOT be electronically filed. Upon consent of all parties, counsel are advised to manually file the form with the Clerk's Office. A copy of form AO 85 has been mailed to parties not receiving electronic service. (no image attached) (MAJ) (Entered: 06/25/2013)
06/25/2013 3 NOTICE TO COUNSEL PURSUANT TO LOCAL RULE IA 10-2. Counsel Frederick A. Tecce, John D. Simmons, Stephen E Murray to comply with completion and electronic filing of the Designation of Local Counsel and Verified Petition. For your convenience, click on the following link to obtain the form from the Court's website - www.nvd.uscourts.gov/Forms.aspx. Counsel is also required to register for the Court's Case Management and Electronic Case Filing (CM/ECF) system and the electronic service of pleadings. Please visit the Court's website www.nvd.uscourts.gov to register Attorney(s) upon approval of the Verified Petition. Verified Petition due by 8/9/2013.(no image attached) (MAJ) (Entered: 06/25/2013)
06/25/2013 4 AO 120 - REPORT on the filing or determination of an action regarding a patent or trademark. E-mailed to the US Patent and Trademark Office. (MAJ) (Entered: 06/25/2013)
$\left.\begin{array}{llll}07 / 02 / 2013 & 5 & \begin{array}{l}\text { CERTIFICATE of Interested Parties filed by ImmerVision, Inc. } \\ \text { that identifies all parties that have an interest in the outcome of } \\ \text { this case. Other Affiliate 9116-6271 Quebec Inc for }\end{array} & \\ \text { ImmerVision, Inc. added. . (Ballif, Philip) (Entered: 07/02/2013) }\end{array}\right)$

1. The Sports Network, June 8, 2014 Sunday 5:55 PM EST, , PGA TOUR - MEN'S PROFESSIONAL GOLF; Statistics, 1977 words, PGA Tour Statistics - Final Round Scoring Average; (Complete Through FedEx St. Jude Classic)

|  |  | Webb Simpson | 10 | 69.40 | 70.15 | 694 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 34 | Camilo Villegas | 12 | 70.33 | 70.98 | 844 |
| 35 |  | Boo Weekley | 12 | 70.33 | 71.25 | 844 |
|  | 54 | Zach Johnson | 14 | 70.71 | 70.16 | 990 |
| 55 |  | Scott Brown | 14 | 70.71 | 70.83 | 990 |
| 56 |  | Brian Davis | 14 | 70.71 | 71.47 | 990 |

2. News Bites US Markets, September 12, 2014 Friday, 916 words, CAI International decreases 1.2\% - trailing 93\% of stocks 12 September, 2014 16:00 EDT
... NYSE market of 2,071 stocks and 34 units traded today, the stock has a 6-month relative price strength of 7 indicating it is trailing $93 \%$ of the market.
... 1000) invested one year ago in CAI International is US\$844, for a capital loss of US\$156. ...
... CAP.NYSE 992990844
S\&P 500 Index 990 1,027 1,195 ...
3. News Bites - Middle East \& North Africa: Palestine, November 20, 2014 Thursday, STOCK, 322 words, Weekly: Palestine Electric in its biggest trailing week loss for 7 months
... week. - In the Palestinian market of 18 stocks traded today, the stock has a 6month relative strength of 7 indicating it is trailing $93.0 \%$ of the market. ...
... value of US $\$ 1,000$ invested two years ago is US $\$ 844$ for a capital loss of US $\$ 156$.
... PEC 947844 ..
... Al-Quds 990944 1,077 ...
4. News Bites US Markets, October 1, 2014 Wednesday, 622 words, AV Homes in 2nd daily fall, nears twenty two-month low 01 October, 2014 16:00 EDT
... last three months the stock has hit a new 52 -week low six times, pointing to a downtrend. + The Moving Average Convergence Divergence (MACD) indicator of ... ... 1000) invested one year ago in AV Homes is US $\$ 844$, for a capital loss of US $\$ 156$.
... AVHI.NASDAQ 990918844 ...
5. The Sampson Independent (Clinton, North Carolina), October 21, 2014 Tuesday, ANNOUNCEMENTS, 844 words, Community Bulletin Board, Emily Hobbs
... progress report pickup for all students and parents on Oct. 27, 6 p.m.A Senior Information Night with graduation supply ordering, scholarship information, Sampson
... by Stephen Mallatratt at The Victor R. Small House. Thursday, Nov. 6, 7:30 p.m.; Friday, Nov. 7, 7:30 p.m.; Saturday, Nov. 8, ...
... out, or delivery. FMI or to purchase a plate, call Skippy Jackson at 990-9554, Glenn Jernigan at 990-0969 or L.S. Guy at 910-267-6441. If you would like to make a ... ... Planning and Zoning Board - meets the first Tuesday of every month at 6 p.m. while training through the N.C. Department of Commerce is being held. The business
6. The Sports Network, April 7, 2013 Sunday 4:47 PM EST, , NATIONWIDE TOUR - GOLF; Statistics, 1671 words, Web.com Tour Statistics - Scoring Average; (Complete Through
```
Brasil Classic)
```

| $\ldots$. | 6 | Wes Roach |  | 2 | 68.38 | 547 |
| :--- | :--- | :--- | :---: | :---: | :---: | :--- | ...

7. Independent.co.uk, August 27, 2014 Wednesday 1:05 AM GMT, , UK POLITICS, 328 words, Authorities failing in hunt for 'most wanted' tax dodgers who owe HMRC $£ 844 \mathrm{~m}$; Campaign that publicly identified those sought has seen results, but many have fled abroad, Kunal Dutta
... year's list include Ahmed Salim Khezr, an Iranian national sentenced to six years for selling non-UK duty paid cigarettes across the UK and ...
... Others are Murugasan Natarajan, who is thought to have fled to India after receiving a six-year sentence last December for smuggling garlic - incorrectly declared as ginger - into the UK. HMRC say that the frauds have collectively cost the UK more than $£ 844$ million. The appeal provided intelligence on the alleged offenders, and the whereabouts of 16 others are now known, HMRC says, with 990 prosecutions having taken place in the last year. But authorities have punished just ...
... said: "These fugitives were involved in frauds that have collectively cost the UK more than $£ 844$ million but the success of our campaign means those on the run should know that HMRC will ...
8. Johannesburg Stock Exchange News Service, March 26, 2014 Wednesday, 2569 words, KDV - KAYDAV GROUP LIMITED - Condensed audited consolidated results for the year ended 31 December 2013
... Profit for the year $23710844 \quad 20350534$...
... equity holders of the parent $23710844 \quad 20350534$...
... Earnings $23710844 \quad 20350534$...
... Current assets 184990190 165 $011970 \ldots$
... Short-term portion of interest-bearing liabilities. 6124965 '5 $538192 \ldots$
... Total comprehensive income for the year $23710844 \quad 20350534$...
... Board distribution $\quad 37932997 \quad 29806990$...
9. Pivotal Sources, November 6, 2014 Thursday, 128 words, Skladowisko Odpadow secures contract for Refuse and waste related services, Poland

Poland, Nov. 6 -- Contract Id: 98432 Description: POLAND based Skladowisko Odpadow has secured contract ...
The contract is valued approximately 2844990 PLN, Including VAT. VAT rate (\%) 8. Country: Poland Sector: ...
November 6, 2014
10. The Sports Network, July 6, 2014 Sunday 9:25 PM EST, , NATIONWIDE TOUR - GOLF; Statistics, 1733 words, Web.com Tour Statistics - Second Round Scoring Average; (Complete Through Nova Scotia Open)

|  | 6 | Roland Thatcher |  | 12 | 68.75 | 70.27 | 825 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 48 | Cameron Percy |  | 12 | 70.33 | 70.15 | 844 |
| 49 |  | Hugo Leon | 12 |  | 70.33 | 70.68 | 844 |
| 50 |  | Brett Lederer | 12 |  | 70.33 | 71.23 | 844 |
|  | 65 | Manuel Villegas |  | 14 | 70.71 | 70.75 | 990 |

Source: Combined Source Set 4 i] - English Language News (Most recent Two Years)
Terms: $\mathbf{6 8 4 4 9 9 0}$ or 6,844,990 (Suggest Terms for My Search \| Feedback on Your Search) View: Cite
Date/Time: Thursday, December 4, 2014-4:30 PM EST
( ${ }^{(1)}$ LexisNexis ${ }^{\oplus} \begin{aligned} & \text { About LexisNexis } \\ & \text { Copyright © }\end{aligned}$ I Privacy Policy I Terms \& Conditions I Contact Us

# UNITED STATES PATENT AND TRADEMARK OFFICE GRANTED PATENT 

4963097
Get Drawing Sheet 1 of 12
Access PDF of Official Patent *
Order Patent File History / Wrapper from REEDFAX®
Link to Claims Section
October 16, 1990
Display apparatus for a group education system
INVENTOR: Anju, Shinji - Saitama, Japan (JP)
APPL-NO: 869449 (06)
FILED-DATE: April 27, 1986
GRANTED-DATE: October 16, 1990
CORE TERMS: display, seat, screen, designated, symbol, cursor, displayed, switch, electrode, classroom, correspond, column, row, assigned, actuation, terminal, seating, designatable, stored, microcomputer, array, teacher, console, actuated, memory, corner, designation, switching, seated, select

## ENGLISH-ABST:

In a group education system of the type having a teacher console and a plurality of terminals at seat positions assignable for student use, a display apparatus includes a display screen adapted to display a seating pattern which corresponds to the seating arrangement of terminals within the classroom. The displayed pattern is created by designating certain areas of the display screen to correspond to seat positions actually assigned for student use, and identifying symbols may be displayed in each of these areas. The display apparatus also includes pattern selecting keys for reordering the designated areas to correspond to a selected on of a plurality of predetermined patterns. In an information display made of the apparatus, actuation of a switch corresponding to a respective one of these areas causes the display of information related to the student occupying the corresponding seat in the classroom.

## DETDESC:

... key for causing this rearrangement, where the information and data relating to each individual student is retained unchanged, but the information is associated with different ones of the designatable image areas according to the selected pattern. Function keys PATNO 1-4 provide this function.

In FIGS. 6A and 6B the numbers shown may be considered to be identifying marks or symbols associated with the respective image areas. Alternatively, FIG. 6A and 6B may be used to illustrate the operation of function keys PATNO 1 to 4 , by identifying the pattern number of the image areas within each pattern.

Thus, for instance, suppose that pattern number 1 is the pattern that appears in FIG. 6C. It should be understood that the symbols ...

Source: Command Searching > Utility, Design and Plant Patents i

Terms: patno=6844990 (Suggest Terms for My Search)
View: SuperKWIC
Date/Time: Thursday, December 4, 2014-4:32 PM EST
(©) LexisNexis ${ }^{8}$ About LexisNexis | Privacy Policy ITerms \& Conditions I Contact Us


Please find below and/or attached an Office communication concerning this application or proceeding.
The time period for reply, if any, is set in the attached communication.

| Ex Parte Reexamination Interview <br> Summary - Pilot Program for Waiver of <br> Patent Owner's Statement | Control No.. | Patent For Which Reexamination <br> is Requested <br> 6844990 |
| :---: | :--- | :--- |
|  | $90 / 013,410$ |  | | Art Unit |
| :--- |
|  |

-- The MAILING DATE of this communication appears on the cover sheet with the correspondence address. --

All participants (USPTO official and patent owner):
(1) Tredelle D. Jackson
(2) MURRAY, STEPHEN 63206

Date of Telephonic Interview: 12/09/14.
The USPTO official requested waiver of the patent owner's statement pursuant to the pilot program for waiver of patent owner's statement in ex parte reexamination proceedings.*
$\searrow$ The patent owner agreed to waive its right to file a patent owner's statement under 35 U.S.C. 304 in the event reexamination is ordered for the above-identified patent.
$\square$ The patent owner did not agree to waive its right to file a patent owner's statement under 35 U.S.C. 304 at this time.

The patent owner is not required to file a written statement of this telephone communication under 37 CFR 1.560(b) or otherwise. However, any disagreement as to this interview summary must be brought to the immediate attention of the USPTO, and no later than one month from the mailing date of this interview summary. Extensions of time are governed by 37 CFR 1.550(c).
*For more information regarding this pilot program, see Pilot Program for Waiver of Patent Owner's Statement in Ex Parte Reexamination Proceedings, 75 Fed. Reg. 47269 (August 5, 2010), available on the USPTO Web site at http://www.uspto.gov/patents/law/notices/2010.jsp.
$\square$ USPTO personnel were unable to reach the patent owner.

The patent owner may contact the USPTO personnel at the telephone number provided below if the patent owner decides to waive the right to file a patent owner's statement under 35 U.S.C. 304.
/Tredelle. D. Jackson/
571-272-2783
Signature and telephone number of the USPTO official who contacted or attempted to contact the patent owner.
cc: Requester (if third party requester)
P.O. Box 1450
Alexandria, Vir
www.uspto.gov

| APPLICATION NO. | FLIING DATE | FIRST NAMED INVENTOR | ATTORNEY DOCKET NO. | CONFIRMATION NO. |
| :---: | :---: | :---: | :---: | :---: |
| 90/013,410 | 11/26/2014 6844990 |  | 688266-21RX | 4682 |
|  |  |  | EXAMINER |  |
| ONE COMMERCE SQUARE |  |  | LEUNG, CHRISTINA Y |  |
| 2005 MARKET STREET, SUITE 2200 |  |  |  |  |
| PHILADELPHIA, PA 19103 |  |  | ART UNTT | PAPER NUMBER |
|  |  |  | 3992 |  |
|  |  |  | MAIL DATE | DELIVERY MODE |
|  |  |  | 01/09/2015 | PAPER |

Please find below and/or attached an Office communication concerning this application or proceeding.
The time period for reply, if any, is set in the attached communication.

| Order Granting / Denying Request For | Control No. | Patent Under Reexamination |
| :---: | :--- | :--- |
|  | Examiner | 6844990 |
|  | Christina Y. Leung | 3992 |

--The MAILING DATE of this communication appears on the cover sheet with the correspondence address--

The request for ex parte reexamination filed $\underline{26}$ November 2014 has been considered and a determination has been made. An identification of the claims, the references relied upon, and the rationale supporting the determination are attached.
Attachments: a) $\square$ PTO-892
b) $\triangle \mathrm{PTO} / \mathrm{SB} / 08$,
c) $\square$ Other: $\qquad$

1. $\boxtimes$ The request for ex parte reexamination is GRANTED.

RESPONSE TIMES ARE SET AS FOLLOWS:
For Patent Owner's Statement (Optional): TWO MONTHS from the mailing date of this communication (37 CFR 1.530 (b)). EXTENSIONS OF TIME ARE GOVERNED BY 37 CFR 1.550(c).

For Requester's Reply (optional): TWO MONTHS from the date of service of any timely filed Patent Owner's Statement (37 CFR 1.535). NO EXTENSION OF THIS TIME PERIOD IS PERMITTED. If Patent Owner does not file a timely statement under 37 CFR 1.530(b), then no reply by requester is permitted.
2. $\square$ The request for ex parte reexamination is DENIED.

This decision is not appealable (35 U.S.C. 303(c)). Requester may seek review by petition to the Commissioner under 37 CFR 1.181 within ONE MONTH from the mailing date of this communication (37 CFR 1.515(c)). EXTENSION OF TIME TO FILE SUCH A PETITION UNDER 37 CFR 1.181 ARE AVAILABLE ONLY BY PETITION TO SUSPEND OR WAIVE THE REGULATIONS UNDER 37 CFR 1.183.

In due course, a refund under 37 CFR 1.26 ( $c$ ) will be made to requester:
a)by Treasury check or,
b)by credit to Deposit Account No. $\qquad$ , or
c) $\square$ by credit to a credit card account, unless otherwise notified (35 U.S.C. 303(c)).

| /Christina Y. Leung/ <br> Primary Examiner, Art Unit 3992 |  |  |
| :--- | :--- | :--- |
| cc:Requester (if third party requester) |  |  |
| U.S.Paent and Trademark oftice Office Action in Ex Parte Reexamination Part of Paper No. 20141229 <br> PTOL-471 (Rev. 08-06)   |  |  |

Art Unit: 3992

# DECISION GRANTING EX PARTE REEXAMINATION 

Decision on the Request
The present request for ex parte reexamination raises a substantial new question of patentability with respect to claims $1-4,6,7,10,11,15-20,22,23$, and 25 of United States Patent $6,844,990$ to Artonne.

## References Cited in the Request

Nagaoka (US 6,128,145 A)
Baker (US 5,686,957 A)
Fisher (US 3,953,111 A)

Shiota (EP 1028389 A2)

Matsui (JP 2000-242773)

Enami (JP H11-261868)
Inoue (US 6,031,670 A)

## Issues Raised by the Request

Issue 1

The request alleges that Nagaoka raises a substantially new question of patentability with respect to claims $1,2,4,6,17,18,20$, and 22 .

Issue 2
The request alleges that Baker raises a substantially new question of patentability with respect to claims $1,2,4,6,17,18,20$, and 22 .

## Issue 3

Art Unit: 3992

The request alleges that Fisher raises a substantially new question of patentability with respect to claims $1-3,6,7,17-19,22$, and 23 .

## Issue 4

The request alleges that Nagaoka in view of Shiota raises a substantially new question of patentability with respect to claims 10 and 11 .

## Issue 5

The request alleges that Nagaoka in view of Matsui raises a substantially new question of patentability with respect to claim 10.

## Issue 6

The request alleges that Baker in view of Shiota raises a substantially new question of patentability with respect to claims 10 and 11 .

## Issue 7

The request alleges that Nagaoka in view of Shiota and Enami raises a substantially new question of patentability with respect to claims 15 and 16 .

## Issue 8

The request alleges that Baker in view of Shiota and Enami raises a substantially new question of patentability with respect to claims 15 and 16.

## Issue 9

The request alleges that Nagaoka in view of Inoue raises a substantially new question of patentability with respect to claim 25.

Issue 10

The request alleges that Baker in view of Inoue raises a substantially new question of patentability with respect to claim 25.

## Scope of Reexamination

Since the requester did not request reexamination of claims $5,8,9,12-14,21,24$, and 26 , and did not assert the existence of a substantial new question of patentability for those claims (see 35 U.S.C. § 31 l(b)(2); see also 37 CFR 1.915 b and 1.923 ), those claims will not be reexamined. This matter was squarely addressed in Sony Computer Entertainment America lnc., et al. v. Jon W. Dudas, 85 USPQ2d 1594 (E.D. Va 2006). The District Court upheld the Office's discretion to not reexamine claims in an inter partes reexamination proceeding other than those claims for which reexamination had been specifically requested. The Court stated:
"To be sure, a party may seek, and the PTO may grant, inter partes review of each and every claim of a patent. Moreover, while the PTO in its discretion may review claims for which inter partes review was not requested, nothing in the statute compels it to do so. To ensure that the PTO considers a claim for inter partes review, $\S 311(\mathrm{~b})(2)$ requires that the party seeking reexamination demonstrate why the PTO should reexamine each and every claim for which it seeks review. Here, it is undisputed that Sony did not seek review of every claim under the ' 213 and '333 patents. Accordingly, Sony cannot now claim that the PTO wrongly failed to reexamine claims for which Sony never requested review, and its argument that AIPA compels a contrary result is unpersuasive."

The Sony decision's reasoning and statutory interpretation apply analogously to ex parte reexamination, as the same relevant statutory language applies to both inter partes and ex parte reexamination. 35 U.S.C. § 302 provides that the ex parte reexamination "request must set forth
the pertinency and manner of applying cited prior art to every claim for which reexamination is requested" (emphasis added), and 35 U.S.C. § 303 provides that "the Director will determine whether a substantial new question of patentability affecting any claim of the patent concerned is raised by the request" (emphasis added). These provisions are analogous to the language of 35 U.S.C. § $311(\mathrm{~b})(2)$ and 35 U.S.C. § 312 applied and construed in Sony, and would be construed in the same manner. As the Director can decline to reexamine non-requested claims in an inter partes reexamination proceeding, the Director can likewise do so in ex parte reexamination proceeding. See Notice of Clarification of Office Policy To Exercise Discretion in Reexamining Fewer Than All the Patent Claims (signed Oct. 5, 2006) 1311 OG 197 (Oct. 31, 2006). See also MPEP § 2240, Rev. 5, Aug. 2006.

## The Artonne Patent

Artonne is generally directed to a method for capturing a digital panoramic image. Claim 1 is representative:

1. A method for capturing a digital panoramic image, by projecting a panorama onto an image sensor by means of a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least one substantially compressed zone.

## Prosecution History

Artonne issued 18 January 2005 from application 10/706,513 filed 12 November 2003, which claims priority to application PCT/FR02/01588 filed on 10 May 2002.

12 November 2003: Applicant filed claims 1-26.
14 September 2004: Examiner allowed claims 1-26, noting that
'"The prior art fails to teach a combination of all the claimed features as presented, for example, in independent claims 1 and 17 , which include a panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least on substantially compressed zone."

## Detailed Analysis

Claims $1-4,6,7,10,11,15-20,22,23$, and 25 will be reexamined.
In view of the prosecution history, a substantial new question of patentability is raised by the evaluation of a prior art reference (or a combination of prior art references) that teaches a panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least on substantially compressed zone

## Issues 1, 4, 5, 7, and 9

The request alleges that Nagaoka alone or in view of Shiota, Matsui, Enami, and/or Inoue raise substantially new questions of patentability with respect to claims $1,2,4,6,10,11,15-18$, 20,22 , and 25.

Nagaoka, in the form of European equivalent patent EP 1004915 A1, was previously cited in an Information Disclosure Statement (IDS) during the prosecution of Artonne. However, the teachings of Nagaoka were not discussed on the record by the Examiner or the applicant. Shiota, Matsui, Enami, and Inoue were not previously cited and are new prior art.

The request provides new view of Nagaoka by alleging that Nagaoka generally teaches a panoramic objective lens (Figure 2) having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least on substantially compressed zone (e.g., lenses having functions $h=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ or 1.6 f - $\tan (\theta / 2)$. See Figures 3A-B.

Since this teaching is directly related to subject matter considered the basis for allowability of claims $1,2,4,6,10,11,15-18,20,22$, and 25 , a reasonable examiner would consider evaluation of this new view of Nagaoka important in determining the patentability of the claims. Therefore, Nagaoka as discussed on the record by the request, alone or in view of Shiota, Matsui, Enami, and/or Inoue, raises a substantial new question of patentability with respect to claims $1,2,4,6,10,11,15-18,20,22$, and 25 .

## Issues 2, 6, 8, and 10

The request alleges that Baker alone or in view of Shiota, Enami, and/or Inoue raises substantially new questions of patentability with respect to claims $1,2,4,6,10,11,15-18,20$, 22 , and 25.

Baker, in the form of European equivalent patent EP 0695085 A1, was previously cited in an IDS during the prosecution of Artonne. However, the teachings of Baker were not discussed on the record. Shiota, Enami, and Inoue were not previously cited and are new prior art.

The request provides new view of Baker by alleging that Baker generally teaches a panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama (Figures 3BA and 3BB), the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least on substantially compressed zone (column 6, lines 48-56; and column 12, lines 29-32).

Since this teaching is directly related to subject matter considered the basis for allowability of claims $1,2,4,6,10,11,15-18,20,22$, and 25 , a reasonable examiner would consider evaluation of this new view of Baker important in determining the patentability of the claims. Therefore, Baker as discussed on the record by the request, alone or in view of Shiota, Matsui, Enami, and/or Inoue, raises a substantial new question of patentability with respect to claims $1,2,4,6,10,11,15-18,20,22$, and 25.

## Issue 3

The request alleges that Fisher raises substantially new questions of patentability with respect to claims $1-3,6,7,17-19,22$, and 23 .

Fisher was previously cited in an IDS during the prosecution of Artonne. However, the teachings of Fisher were not discussed on the record. The request provides new view of Fisher by alleging that Fisher generally teaches a panoramic objective lens (Figures 3 and 6) having an

Art Unit: 3992
image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function (e.g., the function labeled "Non-Linear Lens" in Figure 3, which is $\mathrm{H}=\sin ^{1 / 3} \theta$ ), such that the panoramic image obtained has at least one substantially expanded zone and at least on substantially compressed zone (column 3, lines 4-12).

Since this teaching is directly related to subject matter considered the basis for allowability of claims $1-3,6,7,17-19,22$, and 23 , a reasonable examiner would consider evaluation of this new view of Fisher important in determining the patentability of the claims. Therefore, Fisher raises a substantial new question of patentability with respect to claims $1-3,6$, $7,17-19,22$, and 23 .

## Conclusion

Extensions of time under 37 CFR 1.136(a) will not be permitted in these proceedings because the provisions of 37 CFR 1.136 apply only to "an applicant" and not to parties in a reexamination proceeding. Additionally, 35 U.S.C. 305 requires that ex parte reexamination proceedings "will be conducted with special dispatch" (37 CFR 1.550(a)). Extensions of time in ex parte reexamination proceedings are provided for in 37 CFR 1.550 (c).

The patent owner is reminded of the continuing responsibility under 37 CFR 1.565 (a) to apprise the Office of any litigation activity, or other prior or concurrent proceeding, involving Patent No. 6,844,990 throughout the course of this reexamination proceeding. See MPEP §§ 2207, 2282 and 2286.

All correspondence relating to this ex parte reexamination proceeding should be directed:
By mail to: Mail Stop Ex Parte Reexam
Central Reexamination Unit

Art Unit: 3992

Commissioner for Patents
United States Patent \& Trademark Office
P.O. Box 1450

Alexandria, VA 22313-1450

By fax to: (571) 273-9900
Central Reexamination Unit
By hand to: Customer Service Window
Randolph Building
401 Dulany Street
Alexandria, VA 22314
Any inquiry concerning this communication should be directed to the Central
Reexamination Unit at telephone number (571) 272-7705.
/Christina Y. Leung/
Primary Examiner, Art Unit 3992

Conferees:
/D.M.H./, PE AU3992
/SUDHANSHU PATHAK/
Supervisory Patent Examiner, Art Unit 3992

| Order Granting / Denying Request For | Control No. | Patent Under Reexamination |
| :---: | :--- | :--- |
|  | Examiner | 6844990 |
|  | Christina Y. Leung | 3992 |

--The MAILING DATE of this communication appears on the cover sheet with the correspondence address--

The request for ex parte reexamination filed $\underline{26}$ November 2014 has been considered and a determination has been made. An identification of the claims, the references relied upon, and the rationale supporting the determination are attached.
Attachments: a) $\square$ PTO-892
b) $\triangle \mathrm{PTO} / \mathrm{SB} / 08$,
c) $\square$ Other: $\qquad$

1. $\boxtimes$ The request for ex parte reexamination is GRANTED.

RESPONSE TIMES ARE SET AS FOLLOWS:
For Patent Owner's Statement (Optional): TWO MONTHS from the mailing date of this communication (37 CFR 1.530 (b)). EXTENSIONS OF TIME ARE GOVERNED BY 37 CFR 1.550(c).

For Requester's Reply (optional): TWO MONTHS from the date of service of any timely filed Patent Owner's Statement (37 CFR 1.535). NO EXTENSION OF THIS TIME PERIOD IS PERMITTED. If Patent Owner does not file a timely statement under 37 CFR 1.530(b), then no reply by requester is permitted.
2. $\square$ The request for ex parte reexamination is DENIED.

This decision is not appealable (35 U.S.C. 303(c)). Requester may seek review by petition to the Commissioner under 37 CFR 1.181 within ONE MONTH from the mailing date of this communication (37 CFR 1.515(c)). EXTENSION OF TIME TO FILE SUCH A PETITION UNDER 37 CFR 1.181 ARE AVAILABLE ONLY BY PETITION TO SUSPEND OR WAIVE THE REGULATIONS UNDER 37 CFR 1.183.

In due course, a refund under 37 CFR 1.26 ( $c$ ) will be made to requester:
a)by Treasury check or,
b)by credit to Deposit Account No. $\qquad$ , or
c) $\square$ by credit to a credit card account, unless otherwise notified (35 U.S.C. 303(c)).

| /Christina Y. Leung/ <br> Primary Examiner, Art Unit 3992 |  |  |
| :--- | :--- | :--- |
| cc:Requester (if third party requester) |  |  |
| U.S.Paent and Trademark oftice Office Action in Ex Parte Reexamination Part of Paper No. 20141229 <br> PTOL-471 (Rev. 08-06)   |  |  |


| Search Notes | Application/Control No. $90013410$ | Applicant(s)/Patent Under Reexamination <br> 6844990 |
| :---: | :---: | :---: |
|  | Examiner <br> CHRISTINA Y LEUNG | Art Unit 3992 |


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| Symbol | Date | Examiner |


| CPC COMBINATION SETS - SEARCHED |  |  |
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| Symbol | Date | Examiner |


| US CLASSIFICATION SEARCHED |  |  |  |
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| Class | Subclass | Date | Examiner |
|  |  |  |  |


| SEARCH NOTES |  |  |  |
| :---: | :---: | :---: | :---: |
| Search Notes | Date | Examiner |  |
| Reviewed cited references and patented file's prosecution history. | $1-5-15$ | /CL/ |  |

INTERFERENCE SEARCH

| US Class/ | US Subclass / CPC Group | Date | Examiner |
| :---: | :---: | :---: | :---: |
| CPC Symbol |  |  |  |
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| Reexamination | Application/Control No. $90 / 013,410$ | Applicant(s)/Patent Under Reexamination $6844990$ |
| :---: | :---: | :---: |
|  | Certificate Date | Certificate Number |


| Requester Correspondence Address: $\quad$ Patent Owner $\quad \square$ Third Party |  |
| :--- | :--- |
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| PANITCH SCHWARZE BELISARIO \& NADEL LLP |  |
| ONE COMMERCE SQUARE |  |
| 2005 MARKET STREET, SUITE 2200 |  |
| PHILADELPHIA, PA 19103 |  |


| LITIGATION REVIEW $\boxtimes$ | Case Name |
| :---: | :---: | :---: |
| (examiner initials) | $\mathbf{1 - 5 - 1 5}$ <br> (date) |
| $1: 13 c v 1139$, Immervision Inc. v. Cbc Co. Ltd. et al. | Director Initials |
| $2: 13 c v 1117$, Immervision, Inc. v. Vivotek, Inc. |  |
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| COPENDING OFFICE PROCEEDINGS |  |
| :--- | :--- |
| TYPE OF PROCEEDING | NUMBER |
| $1 . \quad$ Inter partes review of 6,844,990 | IPR2014-01438 |
| 2. |  |
| 3. |  |
| 4. |  |


| INFORMATION DISCLOSURE STATEMENT BY APPLICANT <br> ( Not for submission under 37 CFR 1.99) | Application Number | 90/013,410 |
| :---: | :---: | :---: |
|  | Filing Date |  |
|  | First Named Inventor | Jean-Claude ARTONNE |
|  | Art Unit |  |
|  | Examiner Name |  |
|  | Attorney Docket Numb | er 688266-21RX |


| U.S.PATENTS Remove |  |  |  |  |  |  |  |  |  |  |  |
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| Examiner Initia\|* | $\begin{aligned} & \text { Cite } \\ & \text { No } \end{aligned}$ | Patent Number |  | Kind Code | Issue Date |  | Name of Patentee or Applicant of cited Document |  | Pages,Columns,Lines where Relevant Passages or Relevant Figures Appear |  |  |
| 10. | 1 |  | 128145 |  | 2000-10-0 |  | Nagaoka |  |  |  |  |
|  | 2 |  | 686957 |  | 1997-11-1 |  | Baker |  |  |  |  |
| ICl | 3 |  | 953111 |  | 1976-04-2 |  | Fisher, et al. |  |  |  |  |
| CL | 4 |  | 031670 |  | 2000-02-2 |  | Inoue |  |  |  |  |
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| INFORMATION DISCLOSURE STATEMENT BY APPLICANT <br> ( Not for submission under 37 CFR 1.99) | Application Number | 90/013,410 |
| :---: | :---: | :---: |
|  | Filing Date |  |
|  | First Named Inventor Jean | Jean-Claude ARTONNE |
|  | Art Unit |  |
|  | Examiner Name |  |
|  | Attorney Docket Number | 688266-21RX |


*EXAMINER: Initial if reference considered, whether or not citation is in conformance with MPEP 609. Draw line through a citation if not in conformance and not considered. Include copy of this form with next communication to applicant.
${ }^{1}$ See Kind Codes of USPTO Patent Documents at www.USPTO.GOV or MPEP 901.04. ${ }^{2}$ Enter office that issued the document, by the two-letter code (WIPO Standard ST.3). ${ }^{3}$ For Japanese patent documents, the indication of the year of the reign of the Emperor must precede the serial number of the patent document. ${ }^{4}$ Kind of document by the appropriate symbols as indicated on the document under WIPO Standard ST. 16 if possible. ${ }^{5}$ Applicant is to place a check mark here if English language translation is attached.

| INFORMATION DISCLOSURE STATEMENT BY APPLICANT <br> ( Not for submission under 37 CFR 1.99) | Application Number | 90013410 |
| :---: | :---: | :---: |
|  | Filing Date | 2014-11-26 |
|  | First Named Inventor | Jean-Claude ARTONNE |
|  | Art Unit | 3992 |
|  | Examiner Name | Christina Y. Leung |
|  | Attorney Docket Number | er ${ }^{\text {a }}$ 688266-21RX |


| U.S.PATENTS Remove |  |  |  |  |  |  |  |  |  |  |  |
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| Examiner Initial* | Cite No | Patent Number |  | Kind Code ${ }^{1}$ | Issue Date |  | Name of Patentee or Applicant of cited Document |  | Pages,Columns,Lines where Relevant Passages or Relevant Figures Appear |  |  |
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| Examiner Initial* | $\begin{array}{\|l} \text { Cite } \\ \text { No } \end{array}$ |  | reign Document mber ${ }^{3}$ | Country <br> Code² |  | Kind Code ${ }^{4}$ | Publication Date | Name of Patente Applicant of cited Document |  | Pages,Columns,Lines where Relevant Passages or Relevant Figures Appear | T5 |
|  | 1 |  |  |  |  |  |  |  |  |  | $\square$ |
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| Examiner Initials* | $\begin{array}{\|l} \text { Cite } \\ \text { No } \end{array}$ | Include name of the author (in CAPITAL LETTERS), title of the article (when appropriate), title of the item (book, magazine, journal, serial, symposium, catalog, etc), date, pages(s), volume-issue number(s), publisher, city and/or country where published. |  |  |  |  |  |  |  |  | T5 |


| INFORMATION DISCLOSURE STATEMENT BY APPLICANT <br> ( Not for submission under 37 CFR 1.99) | Application Number |  | 90013410 |
| :---: | :---: | :---: | :---: |
|  | Filing Date |  | 2014-11-26 |
|  | First Named Inventor | Jean-Claude ARTONNE |  |
|  | Art Unit |  | 3992 |
|  | Examiner Name | Christina Y. Leung |  |
|  | Attorney Docket Number |  | 688266-21RX |



| INFORMATION DISCLOSURE STATEMENT BY APPLICANT <br> ( Not for submission under 37 CFR 1.99) | Application Number |  | 90013410 |
| :---: | :---: | :---: | :---: |
|  | Filing Date |  | 2014-11-26 |
|  | First Named Inventor | Jean-Claude ARTONNE |  |
|  | Art Unit |  | 3992 |
|  | Examiner Name | Christina Y. Leung |  |
|  | Attorney Docket Number |  | 688266-21RX |

## CERTIFICATION STATEMENT

Please see 37 CFR 1.97 and 1.98 to make the appropriate selection(s):

That each item of information contained in the information disclosure statement was first cited in any communication from a foreign patent office in a counterpart foreign application not more than three months prior to the filing of the information disclosure statement. See 37 CFR 1.97(e)(1).

## OR

That no item of information contained in the information disclosure statement was cited in a communication from a foreign patent office in a counterpart foreign application, and, to the knowledge of the person signing the certification after making reasonable inquiry, no item of information contained in the information disclosure statement was known to any individual designated in 37 CFR 1.56(c) more than three months prior to the filing of the information disclosure statement. See 37 CFR 1.97(e)(2).

See attached certification statement.
The fee set forth in 37 CFR 1.17 (p) has been submitted herewith.
A certification statement is not submitted herewith.

## SIGNATURE

A signature of the applicant or representative is required in accordance with CFR $1.33,10.18$. Please see CFR 1.4(d) for the form of the signature.

| Signature | /Stephen E. Murray/ | Date (YYYY-MM-DD) | $2015-01-09$ |
| :--- | :--- | :--- | :--- |
| Name/Print | Stephen E. Murray | Registration Number | 63206 |

This collection of information is required by 37 CFR 1.97 and 1.98. The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 1 hour to complete, including gathering, preparing and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

## Privacy Act Statement

The Privacy Act of 1974 (P.L. 93-579) requires that you be given certain information in connection with your submission of the attached form related to a patent application or patent. Accordingly, pursuant to the requirements of the Act, please be advised that: (1) the general authority for the collection of this information is 35 U.S.C. 2(b)(2); (2) furnishing of the information solicited is voluntary; and (3) the principal purpose for which the information is used by the U.S. Patent and Trademark Office is to process and/or examine your submission related to a patent application or patent. If you do not furnish the requested information, the U.S. Patent and Trademark Office may not be able to process and/or examine your submission, which may result in termination of proceedings or abandonment of the application or expiration of the patent.

The information provided by you in this form will be subject to the following routine uses:

1. The information on this form will be treated confidentially to the extent allowed under the Freedom of Information Act (5 U.S.C. 552) and the Privacy Act (5 U.S.C. 552a). Records from this system of records may be disclosed to the Department of Justice to determine whether the Freedom of Information Act requires disclosure of these record s.
2. A record from this system of records may be disclosed, as a routine use, in the course of presenting evidence to a court, magistrate, or administrative tribunal, including disclosures to opposing counsel in the course of settlement negotiations.
3. A record in this system of records may be disclosed, as a routine use, to a Member of Congress submitting a request involving an individual, to whom the record pertains, when the individual has requested assistance from the Member with respect to the subject matter of the record.
4. A record in this system of records may be disclosed, as a routine use, to a contractor of the Agency having need for the information in order to perform a contract. Recipients of information shall be required to comply with the requirements of the Privacy Act of 1974, as amended, pursuant to 5 U.S.C. 552a(m).
5. A record related to an International Application filed under the Patent Cooperation Treaty in this system of records may be disclosed, as a routine use, to the International Bureau of the World Intellectual Property Organization, pursuant to the Patent Cooperation Treaty.
6. A record in this system of records may be disclosed, as a routine use, to another federal agency for purposes of National Security review (35 U.S.C. 181) and for review pursuant to the Atomic Energy Act (42 U.S.C. 218(c)).
7. A record from this system of records may be disclosed, as a routine use, to the Administrator, General Services, or his/her designee, during an inspection of records conducted by GSA as part of that agency's responsibility to recommend improvements in records management practices and programs, under authority of 44 U.S.C. 2904 and 2906. Such disclosure shall be made in accordance with the GSA regulations governing inspection of records for this purpose, and any other relevant (i.e., GSA or Commerce) directive. Such disclosure shall not be used to make determinations about individuals.
8. A record from this system of records may be disclosed, as a routine use, to the public after either publication of the application pursuant to 35 U.S.C. 122(b) or issuance of a patent pursuant to 35 U.S.C. 151. Further, a record may be disclosed, subject to the limitations of 37 CFR 1.14, as a routine use, to the public if the record was filed in an application which became abandoned or in which the proceedings were terminated and which application is referenced by either a published application, an application open to public inspections or an issued patent.
9. A record from this system of records may be disclosed, as a routine use, to a Federal, State, or local law enforcement agency, if the USPTO becomes aware of a violation or potential violation of law or regulation.

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Patent of:
Jean-Claude ARTONNE et al.

Reexamination Control No.: 90/013,410
Filing Date: November 26, 2014
For: METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE

## INFORMATION DISCLOSURE STATEMENT (IDS) UNDER 37 C.F.R. § 1.555

Enclosed is an Information Disclosure Citation Form PTO/SB/08A and/or 08B in accordance with 37 C.F.R. $\S 1.98$ listing all patents, publications, applications, and/or other information being submitted for consideration which may be material to this reexamination proceeding and/or for which there may be a duty to disclose in accordance with 37 C.F.R. § 1.56.

In accordance with M.P.E.P. § 2280, this Information Disclosure Statement is being filed within two months of the date of the order for reexamination.

The enclosed reference is an excerpt from the second edition of "Applied Photographic Optics" that is directed to design development and features of a "fisheye" lens.

The filing of this Information Disclosure Statement shall not be construed as an admission that any of the listed documents constitutes prior art, nor as an admission against interest in any manner.

No fee is believed to be due in connection with the filing of this Information Disclosure Statement. However, if any fee is due, please charge the fee to Deposit Account No. 50-1017.

It is respectfully requested that this Information Disclosure Statement and the document listed on the attached Form PTO/SB/08A and/or 08B and attached herewith be considered and acknowledged by the Examiner in connection with the above-identified reexamination, be made of record therein, and that the listed document be cited in reexamination certificate.

Dated: January 9, 2015 $\qquad$ -

Respectfully submitted,
By/Stephen E. Murray/
Stephen E. Murray
Registration No.: 63,206
PANITCH SCHWARZE BELISARIO \& NADEL LLP
One Commerce Square
2005 Market Street, Suite 2200
Philadelphia, Pennsylvania 19103
(215) 965-1307
(215) 965-1331 (Fax)
smurray@panitchlaw.com (E-Mail)

| Electronic Acknowledgement Receipt |  |
| :---: | :---: |
| EFS ID: | 21170689 |
| Application Number: | 90013410 |
| International Application Number: |  |
| Confirmation Number: | 4682 |
| Title of Invention: | METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE |
| First Named Inventor/Applicant Name: | 6844990 |
| Customer Number: | 570 |
| Filer: | Stephen Murray/Kathy Higgins |
| Filer Authorized By: | Stephen Murray |
| Attorney Docket Number: | 688266-21RX |
| Receipt Date: | 09-JAN-2015 |
| Filing Date: | 26-NOV-2014 |
| Time Stamp: | 16:09:42 |
| Application Type: | Reexam (Patent Owner) |

## Payment information:

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| :---: | :---: | :---: | :---: | :---: | :---: |
| File Listing: |  |  |  |  |  |
| Document Number | Document Description | File Name | File Size(Bytes)/ Message Digest | Multi Part /.zip | Pages (if appl.) |
| 1 | Non Patent Literature | Applied_Photographic_Optics_ -_Sidney_F_Ray.PDF | $\qquad$ | no | 6 |
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| Information: |  |  |  |  |  |
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| 3 | Transmittal Letter | 00694035.PDF | 453506 | no | 2 |
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| Total Files Size (in bytes): |  |  | 1377721 |  |  |
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| New Applications Under 35 U.S.C. 111 |  |  |  |  |  |
| If a new application is being filed and the application includes the necessary components for a filing date (see 37 CFR 1.53(b)-(d) and MPEP 506), a Filing Receipt (37 CFR 1.54) will be issued in due course and the date shown on this Acknowledgement Receipt will establish the filing date of the application. |  |  |  |  |  |
| National Stage of an International Application under 35 U.S.C. 371 |  |  |  |  |  |
| If a timely submission to enter the national stage of an international application is compliant with the conditions of 35 U.S.C. 371 and other applicable requirements a Form PCT/DO/EO/903 indicating acceptance of the application as a national stage submission under 35 U.S.C. 371 will be issued in addition to the Filing Receipt, in due course. |  |  |  |  |  |
| New International Application Filed with the USPTO as a Receiving Office |  |  |  |  |  |
| If a new international application is being filed and the international application includes the necessary components for an international filing date (see PCT Article 11 and MPEP 1810), a Notification of the International Application Number and of the International Filing Date (Form PCT/RO/105) will be issued in due course, subject to prescriptions concerning national security, and the date shown on this Acknowledgement Receipt will establish the international filing date of the application. |  |  |  |  |  |

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www uspto.gov


Please find below and/or attached an Office communication concerning this application or proceeding.
The time period for reply, if any, is set in the attached communication.

| Office Action in Ex Parte Reexamination | Control No. <br> $90 / 013,410$ | Patent Under Reexamination <br> 6844990 |  |
| :--- | :--- | :--- | :--- |
|  | Examiner <br> Christina Y. Leung | Art Unit <br> 3992 | AIA (First Inventor to <br> File) <br> No |

## -- The MAILING DATE of this communication appears on the cover sheet with the correspondence address --

a. $\boxtimes$ Responsive to the communication(s) filed on 26 November 2014.
$\square$ A declaration(s)/affidavit(s) under 37 CFR 1.130 (b) was/were filed on $\qquad$
b.This action is made FINAL.
c.A statement under 37 CFR 1.530 has not been received from the patent owner.
A shortened statutory period for response to this action is set to expire $\underline{2}$ month(s) from the mailing date of this letter. Failure to respond within the period for response will result in termination of the proceeding and issuance of an ex parte reexamination certificate in accordance with this action. 37 CFR 1.550(d). EXTENSIONS OF TIME ARE GOVERNED BY 37 CFR 1.550(c).
If the period for response specified above is less than thirty (30) days, a response within the statutory minimum of thirty (30) days will be considered timely.

Part I THE FOLLOWING ATTACHMENT(S) ARE PART OF THIS ACTION:

1. $\quad \square$ Notice of References Cited by Examiner, PTO-892.
3.Interview Summary, PTO-474.
2.Information Disclosure Statement, PTO/SB/08.
2. 

$\qquad$ —.

Part II SUMMARY OF ACTION
1a. $\boxtimes$ Claims $1-4,6,7,10,11,15-20,22,23,25$ and $27-48$ are subject to reexamination.
1b. $\boxtimes$ Claims $5,8,9,12-14,21,24$ and 26 are not subject to reexamination.
2. $\boxtimes$ Claims $1,6,7$ and 22 have been canceled in the present reexamination proceeding.
3. $\boxtimes$ Claims 10 and 11 are patentable and/or confirmed.
4. $\boxtimes$ Claims 2-4,15-20,23,25 and 27-48 are rejected.
5.
$\square$ Claims $\qquad$ are objected to.
6. $\qquad$
$\qquad$ are acceptable.
7. $\square$ The proposed drawing correction, filed on $\qquad$ has been (7a)approved (7b)disapproved.
8.
$\square$ Acknowledgment is made of the priority claim under 35 U.S.C. § 119 (a)-(d) or ( f$)$.
a)All b)Some* c) $\qquad$ None of the certified copies havebeen received.
$2 \square$not been received.

3been filed in Application No. $\qquad$ ـ.
4been filed in reexamination Control No. $\qquad$ -
5 -been received by the International Bureau in PCT application No. $\qquad$ ـ.

* See the attached detailed Office action for a list of the certified copies not received.
9.Since the proceeding appears to be in condition for issuance of an ex parte reexamination certificate except for formal matters, prosecution as to the merits is closed in accordance with the practice under Ex parte Quayle, 1935 C.D. 11, 453 O.G. 213.
10.Other: $\qquad$

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## DETAILED ACTION

## Reexamination

1. Ex parte reexamination of claims 1-4, 6, 7, 10, 11, 15-20, 22, 23, and 25 of Artonne (US $6,844,990$ B2) has been granted. Claims $5,8,9,12-14,21,24$, and 26 are not subject to reexamination in this proceeding. Patent Owner ( PO ) filed a preliminary claim amendment with the request for reexamination on 26 November 2014, canceling claims $1,6,7$, and 22 ; amending claims 2-4, 10, and 15; and adding new claims 27-48.
2. The claims currently pending in this proceeding are claims $2-4,10,11,15-20,23,25$, and 27-48.

## References and Documents Cited in this Action

Artonne (US 6,844,990 B2)

Nagaoka (US 6, 128, 145 A)
Baker (US 5,686,957 A)

Fisher (US 3,953,111 A)
Shiota (EP 1028389 A2)
Matsui (JP 2000-242773; see English-language translation filed by PO on 26 November 2014)

Enami (JP H11-261868; see English-language translation filed by PO on 26 November 2014)

Inoue (US 6,031,670 A)
PO Request (request for reexamination filed by PO on 26 November 2014)

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PO Remarks (remarks filed by PO with a preliminary amendment on 26 November 2014)

## Claim Rejections - 35 USC § 305

3. Claims $\mathbf{2 - 4}, \mathbf{1 5}, \mathbf{1 6}$, and $\mathbf{2 7 - 4 8}$ are rejected under 35 U.S.C. 305 as enlarging the scope of the claim(s) of the patent being reexamined. In 35 U.S.C. 305 , it is stated that "[n]o proposed amended or new claim enlarging the scope of a claim of the patent will be permitted in a reexamination proceeding... ." A claim presented in a reexamination "enlarges the scope" of the patent claim(s) where the claim is broader than any claim of the patent. A claim is broader in scope than the original claims if it contains within its scope any conceivable product or process which would not have infringed the original patent. A claim is broadened if it is broader in any one respect, even though it may be narrower in other respects.

Regarding independent claims 27, 38, and 48, claims 27, 38, and 48 each include steps and limitations recited in original claim 1, except claims 27 and 48 recite "such that the panoramic image obtained has at least one expanded zone and at least one compressed zone" and claim 38 recites "such that the panoramic image obtained has at least one expanded zone and at least two compressed zones." In contrast, original claim 1 recites "at least one substantially expanded zone and at least one substantially compressed zone." Claims 27,38 , and 48 are rejected under 35 U.S.C. 305 because they are broader than the original claims in at least this aspect. The claims do not require a "substantially expanded" and a "substantially compressed" zone (i.e., expanded and compressed zones that are not "substantially" expanded and compressed would be contained within its scope).

Claims 2-4, 15, 16, 28-31, and 39-47 are also rejected under 35 U.S.C. 305 for the above reason because they depend on claim 27 or 38 .

Similarly, regarding independent claim 32, claim 32 includes elements and limitations recited in original claim 17, except claim 32 recites "such that a panoramic image obtained using the objective lens comprises at least one expanded zone and at least one compressed zone." In contrast, original claim 17 recites "at least one substantially expanded zone and at least one substantially compressed zone." Claim 32 is rejected under 35 U.S.C. 305 because it is broader than the original claims in at least this aspect. The claim does not require a "substantially expanded" and a "substantially compressed" zone (i.e., expanded and compressed zones that are not "substantially" expanded and compressed would be contained within its scope).

Claims 33-37 are also rejected under 35 U.S.C. 305 for the above reason because they depend on claim 32.

## Claim Rejections - 35 USC § 112

4. The following is a quotation of the first paragraph of 35 U.S.C. 112(a):
(a) IN GENERAL.-The specification shall contain a written description of the invention, and of the manner and process of making and using it, in such full, clear, concise, and exact terms as to enable any person skilled in the art to which it pertains, or with which it is most nearly connected, to make and use the same, and shall set forth the best mode contemplated by the inventor or joint inventor of carrying out the invention.

The following is a quotation of the first paragraph of pre-AIA 35 U.S.C. 112 :

The specification shall contain a written description of the invention, and of the manner and process of making and using it, in such full, clear, concise, and exact terms as to enable any person skilled in the art to which it pertains, or with which it is most nearly connected, to make and use the same, and shall set forth the best mode contemplated by the inventor of carrying out his invention.
5. Claim 48 is rejected under 35 U.S.C. 112(a) or 35 U.S.C. 112 (pre-AIA), first paragraph, as failing to comply with the enablement requirement. The claim(s) contains subject matter
which was not described in the specification in such a way as to enable one skilled in the art to which it pertains, or with which it is most nearly connected, to make and/or use the invention.

Claim 48 recites the limitation "wherein the objective lens has a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens." In PO Remarks (page 11), PO cites column 18, lines 17-28 to support this limitation:
"In particular, although the description above was of non-linear panoramic objective lenses with axial symmetry relative to the optical axis, in which the position of an image point only varies with the field angle relative to this axis of the corresponding object point (which gives a distribution of points in concentric circles, as seen above), the framework of the present invention also covers providing objective lenses the non-linearity of which is not symmetrical relative to the optical axis, such that the expanded parts of the image may, in this case, not be set on the center of the image." (Artonne, column 18, lines 17-28)

However, although the above contends that "the framework of the present invention also covers" the limitations recited in claim 48, Artonne does not disclose or illustrate any examples of objective lenses with a non-linear distribution that is not symmetrical relative to the optical axis. The embodiments described in Figures 1-18 and throughout the specification only include objective lenses with a symmetrical non-linear distribution. There is no embodiment disclosed in Artonne having a non-symmetrical non-linear distribution. Artonne also does not describe how to make an objective lens with a non-linear distribution that is not symmetrical relative to the optical axis. Therefore, claim 48 contains subject matter which was not described in the specification in such a way as to enable one skilled in the art to which it pertains, or with which it is most nearly connected, to make and/or use the invention.

## Claim Rejections - 35 USC § 102

6. The following is a quotation of the appropriate paragraphs of pre-AIA 35 U.S.C. 102 that form the basis for the rejections under this section made in this Office action:

A person shall be entitled to a patent unless -
(a) the invention was known or used by others in this country, or patented or described in a printed publication in this or a foreign country, before the invention thereof by the applicant for a patent.
(b) the invention was patented or described in a printed publication in this or a foreign country or in public use or on sale in this country, more than one year prior to the date of application for patent in the United States.
(e) the invention was described in (1) an application for patent, published under section 122(b), by another filed in the United States before the invention by the applicant for patent or (2) a patent granted on an application for patent by another filed in the United States before the invention by the applicant for patent, except that an international application filed under the treaty defined in section 351(a) shall have the effects for purposes of this subsection of an application filed in the United States only if the international application designated the United States and was published under Article 21(2) of such treaty in the English language.
7. Claims 17, 18, and 20 are rejected under pre-AIA 35 U.S.C. 102(a) or 102(e) as being anticipated by Nagaoka.

Regarding claim 17, Nagaoka discloses a panoramic objective lens (e.g., fisheye lens 1;
Figure 2) comprising:
optical means for projecting a panorama into an image plane of the objective lens (i.e., CCD image sensor 30),
the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama (e.g., Nagaoka discloses non-linear lenses with functions $\mathrm{h}=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \bullet \tan (\theta / 2)$; Figures $3 \mathrm{~A}-\mathrm{B}$ ' column 5 , lines $34-67$; column 6, lines 1-13),
the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function (e.g., the function $\mathrm{h}=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ diverges about $18 \%$ and the function $\mathrm{h}=1.6 \mathrm{f} \bullet \tan (\theta / 2)$ diverges about $16 \%$ compared to a linear distribution function at $\theta=$ $45^{\circ}$ ),
such that a panoramic image obtained by means of the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone (Figure 3B shows the functions $\mathrm{h}=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \bullet \tan (\theta / 2)$ each having a slope less than the linear distribution function between $0^{\circ}$ and about $60^{\circ}$ and a slope greater than the linear distribution function between about $60^{\circ}$ and $90^{\circ}$, which correspond to an image with a compressed zone in the center and an a expanded zone near the periphery).

Regarding claim 18, Nagaoka discloses a non- linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of an image obtained varying according to the field angle of the corresponding object point. For example, the lenses having the functions $h=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ and $h=1.6 f \bullet \tan (\theta / 2)$ each have functions that are symmetrical relative to the optical axis (column 5 , lines 34-67; column 6, lines 1-13; see Figures 3A-B and also Figures 4A-D, which show symmetry relative to the optical axis for lenses with related non-linear distribution functions).

Regarding claim 20, Nagaoka discloses that wherein the lens expands the edges of an image and compresses the center of the image. For example, Figure 3 B shows the functions $\mathrm{h}=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \bullet \tan (\theta / 2)$ each having a slope less than the linear distribution function between $0^{\circ}$ and about $60^{\circ}$ and a slope greater than the linear distribution function between about $60^{\circ}$ and $90^{\circ}$, which correspond to an image with a compressed zone in the center and an a expanded zone near the periphery.
8. Claims 17, 18, and 20 are rejected under pre-AIA 35 U.S.C. 102(b) as being anticipated by Baker.

Regarding claim 17, Baker discloses a panoramic objective lens (e.g., the lens shown in Figures 3 BA and 3 BB ) comprising
optical means for projecting a panorama into an image plane of the objective lens (i.e., a CCD; column 13, lines 14-17),
the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama (Figures 3BA and 3BB; column 12, lines 23-25), the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function (e.g., Baker discloses, compared to a linear distribution lens that would focus "the lowest 15 percent degrees from the horizon on ten percent of the imager," a non-linear lens that focuses that 15 degrees on "fifty percent of the imager" [column 6 , lines 4856], which corresponds to a greater than $10 \%$ divergence of the image height at $75^{\circ}$ ),
such that a panoramic image obtained by means of the objective lens comprises at least zone substantially expanded zone and at least one substantially compressed zone (i.e., Baker discloses that the periphery of the image is expanded and the center of the image is compressed; column 12, lines 29-32; see also Figure 3BB compared to the linear lens image in Figure 2B).

Regarding claim 18, Baker discloses a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of an image obtained varying according to the field angle of the corresponding object point (Figure 3BB).

Regarding claim 20, Baker discloses that the lens expands the edges of an image and compresses the center of the image (Figure 3BB shows an expanded periphery and a compressed center compared to the linear lens image in Figure 2B).

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9. Claims 17-19 and 23 are rejected under pre-AIA 35 U.S.C. 102(b) as being anticipated by Fisher.

Regarding claim 17, Fisher discloses a panoramic objective lens (Figures 3 and 6) comprising:
optical means for projecting a panorama into an image plane of the objective lens (Abstract; column 3, lines 48-49; column 4, lines 35-45),
the optical means having an image point distribution function that is not linear relative to the field angle of object points of the panorama (Figure 3; column 1, lines 9-11; column 2, lines 6-8),
the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function (Figure 3 shows the function labeled "Non-Linear Lens" 3, which is $\mathrm{H}=\sin ^{1 / 3} \theta$, having a divergence of greater than $10 \%$ compared to the linear distribution function of the "Fisheye Lens"),
such that a panoramic image obtained by means of the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone (Fisher discloses that the center objects "occupy a disproportionately large share of the image cast by the lens when compared with other objects closer to the periphery of the field of view for the lens"; column 3, lines 4-12; see also Figure 4, which compares the object space to the image plane).

Regarding claim 18, Fisher discloses a non- linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of an image obtained varying according to the field angle of the corresponding object point (Figure 4; column 3, lines 21-42).

Regarding claim 19, Fisher discloses that the lens expands the center of an image and compresses the edges of the image. Specifically, Fisher discloses that the center objects "occupy a disproportionately large share of the image cast by the lens when compared with other objects closer to the periphery of the field of view for the lens" (column 3, lines 4-12; see also Figure 4 and column 3, lines 21-42).

Regarding claim 23, Fisher discloses a panoramic objective lens according to claim 17 as discussed above, and further discloses a set of lenses forming an apodizer (as recited in claim 22, which is not subject to reexamination in this proceeding), at least in the sense that Fisher discloses that the lenses provide a non-linear distribution of image points relative to the field angle of the object points (see Artonne, Figure 15 and column 16, lines 1-4, which describe lenses forming an apodizer; and Fisher, Figure 6, which shows a set of lenses providing a nonlinear distribution and thereby forming an apodizer). Further regarding claim 23, Fisher discloses that the set of lenses forming an apodizer comprises at least one aspherical lens (e.g., lens element "a" having aspherical surface R1 and lens element " $b$ " having aspherical surface R3' Figure 6; column 5, lines 61-68).

## Claim Rejections - 35 USC § 103

10. The following is a quotation of pre-AIA 35 U.S.C. 103(a) which forms the basis for all obviousness rejections set forth in this Office action:
(a) A patent may not be obtained though the invention is not identically disclosed or described as set forth in section 102 of this title, if the differences between the subject matter sought to be patented and the prior art are such that the subject matter as a whole would have been obvious at the time the invention was made to a person having ordinary skill in the art to which said subject matter pertains. Patentability shall not be negatived by the manner in which the invention was made.
11. Claim 25 is rejected under pre-AIA 35 U.S.C. 103(a) as being unpatentable over

Nagaoka in view of Inoue.

Regarding claim 25, Nagaoka discloses a panoramic objective lens according to claim 17 as discussed above, and further discloses a set of lenses forming an apodizer (as recited in claim 22 , which is not subject to reexamination in this proceeding), at least in the sense that Nagaoka discloses that the lenses provide a non-linear distribution of image points relative to the field angle of the object points (see Artonne, Figure 15 and column 16, lines 1-4, which describe lenses forming an apodizer; and Nagaoka, Figure 2, which shows a set of lenses providing a nonlinear distribution and thereby forming an apodizer).

Further regarding claim 25, Nagaoka does not specifically disclose polymethacrylate lenses. However, Inoue teaches a lens system that is related to the one disclosed by Nagaoka including polymethacrylate lenses (i.e., "PMMA"; column 2 , lines $42-44$ ). It would have been obvious to one of ordinary skill in the art to include polymethacrylate lenses as taught by Inoue in the system disclosed by Nagaoka in order to advantageously reduce the size, weight, and costs of the lens materials (Inoue, column 1, lines 28-31; column 2, lines 42-44).
12. Claim 25 is rejected under pre-AIA 35 U.S.C. 103(a) as being unpatentable over Baker in view of Inoue.

Regarding claim 25, Baker discloses a panoramic objective lens according to claim 17 as discussed above, and further discloses a set of lenses forming an apodizer (as recited in claim 22, which is not subject to reexamination in this proceeding), at least in the sense that Baker discloses that the lenses provide a non-linear distribution of image points relative to the field angle of the object points (see Artonne, Figure 15 and column 16, lines 1-4, which describe lenses forming an apodizer; and Baker, Figures 3BA and 3BB, which shows a set of lenses providing a non-linear distribution and thereby forming an apodizer).

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Further regarding claim 25, Baker does not specifically disclose polymethacrylate lenses. However, Inoue teaches a lens system that is related to the one disclosed by Baker including polymethacrylate lenses (i.e., "PMMA"; column 2, lines 42-44). It would have been obvious to one of ordinary skill in the art to include polymethacrylate lenses as taught by Inoue in the system disclosed by Baker in order to advantageously reduce the size, weight, and costs of the lens materials (Inoue, column 1, lines 28-31; column 2, lines 42-44).
13. Claim 48 is rejected under pre-AIA 35 U.S.C. 103(a) as being unpatentable over

## Nagaoka.

Regarding claim 48, as similarly discussed above with respect to claim 17, Nagaoka discloses a method for capturing a digital panoramic image, by projecting a panorama onto an image sensor by means of a panoramic objective lens (e.g., onto CCD image sensor 30 by means of fisheye lens 1; Figure 2),
the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama (e.g., Nagaoka discloses non-linear lenses with functions $h=1.2 f \bullet \tan (\theta / 1.6)$ and $h=1.6 f \bullet \tan (\theta / 2)$; Figures $3 A-B^{\prime}$ column 5 , lines 34-67; column 6, lines 1-13),
the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function (e.g., the function $\mathrm{h}=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ diverges about $18 \%$ and the function $\mathrm{h}=1.6 \mathrm{f} \bullet \tan (\theta / 2)$ diverges about $16 \%$ compared to a linear distribution function at $\theta=$ $45^{\circ}$ ),
such that the panoramic image obtained has at least one expanded zone and at least one compressed zone (Figure 3B shows the functions $\mathrm{h}=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \bullet \tan (\theta / 2)$ each
having a slope less than the linear distribution function between $0^{\circ}$ and about $60^{\circ}$ and a slope greater than the linear distribution function between about $60^{\circ}$ and $90^{\circ}$, which correspond to an image with a compressed zone in the center and an a expanded zone near the periphery).

Further regarding claim 48, Nagaoka does not specifically disclose that the objective lens has a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens. Instead, Nagaoka discloses a non- linear distribution function that is symmetrical relative to the optical axis of the objective lens. For example, the lenses having the functions $\mathrm{h}=1.2 \mathrm{f} \bullet \tan (\theta / 1.6)$ and $\mathrm{h}=1.6 \mathrm{f} \bullet \tan (\theta / 2)$ each have functions that are symmetrical relative to the optical axis (column 5, lines 34-67; column 6, lines 1-13; see Figures 3A-B and also Figures 4A-D, which show symmetry relative to the optical axis for lenses with related non-linear distribution functions). However, as well as the claim may be understood with respect to 35 U.S.C. 112, first paragraph, discussed above, the Artonne specification suggests that providing an objective lens having a non-linear distribution function that is asymmetrical instead of symmetrical would be accomplished by one of ordinary skill in the art without undue experimentation. In that case, it would have been obvious to one of ordinary skill in the art to include a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens in the system disclosed by Nagaoka in order to create a resulting image with compressed and expanded zones that do not include the entire center or entire periphery as desired by the user. The development of the lens with the asymmetrical function would have been obvious to try with a reasonable expectation of success.
14. Claim 48 is rejected under pre-AIA 35 U.S.C. 103(a) as being unpatentable over Baker.

Regarding claim 48, as similarly discussed above with respect to claim 17, Baker discloses a method for capturing a digital panoramic image, by projecting a panorama onto an image sensor by means of a panoramic objective lens (e.g., onto a CDD by means of the lens shown in Figure 3BA; column 13, lines 14-17)
the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama (Figures 3BA and 3BB; column 12, lines 23-25),
the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function (e.g., Baker discloses, compared to a linear distribution lens that would focus "the lowest 15 percent degrees from the horizon on ten percent of the imager," a non-linear lens that focuses that 15 degrees on "fifty percent of the imager" [column 6 , lines 48 56], which corresponds to a greater than $10 \%$ divergence of the image height at $75^{\circ}$ ),
such that a panoramic image obtained by means of the objective lens comprises at least zone substantially expanded zone and at least one substantially compressed zone (i.e., Baker discloses that the periphery of the image is expanded and the center of the image is compressed; column 12, lines 29-32; see also Figure 3BB compared to the linear lens image in Figure 2B).

Further regarding claim 48, Baker does not specifically disclose that the objective lens has a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens. Instead, Baker discloses a non- linear distribution function that is symmetrical relative to the optical axis of the objective lens (see Figure 3BB). However, as well as the claim may be understood with respect to 35 U.S.C. 112, first paragraph, discussed above, the Artonne specification suggests that providing an objective lens having a non-linear distribution function
that is asymmetrical instead of symmetrical would be accomplished by one of ordinary skill in the art without undue experimentation. In that case, it would have been obvious to one of ordinary skill in the art to include a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens in the system disclosed by Baker in order to create a resulting image with compressed and expanded zones that do not include the entire center or entire periphery as desired by the user. The development of the lens with the asymmetrical function would have been obvious to try with a reasonable expectation of success. 15. Claim 48 is rejected under pre-AIA 35 U.S.C. 103(a) as being unpatentable over Fisher. Regarding claim 48, as similarly discussed above with respect to claim 17, Fisher discloses a method for capturing a digital panoramic image, by projecting a panorama onto an image sensor by means of a panoramic objective lens (Figures 3 and 6; Abstract; column 3, lines 48-49; column 4, lines 35-45), the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama (Figure 3; column 1, lines 9-11; column 2 , lines 6-8),
the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function (Figure 3 shows the function labeled "Non-Linear Lens" 3, which is $H=\sin ^{1 / 3} \theta$, having a divergence of greater than $10 \%$ compared to the linear distribution function of the "Fisheye Lens"),
such that a panoramic image obtained by means of the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone (Fisher discloses that the center objects "occupy a disproportionately large share of the image cast by the lens
when compared with other objects closer to the periphery of the field of view for the lens"; column 3, lines 4-12; see also Figure 4 , which compares the object space to the image plane).

Further regarding claim 48, Fisher does not specifically disclose that the objective lens has a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens. Instead, Fisher discloses a non- linear distribution function that is symmetrical relative to the optical axis of the objective lens (Figure 4 ; column 3, lines 21-42). However, as well as the claim may be understood with respect to 35 U.S.C. 112 , first paragraph, discussed above, the Artonne specification suggests that providing an objective lens having a non-linear distribution function that is asymmetrical instead of symmetrical would be accomplished by one of ordinary skill in the art without undue experimentation. In that case, it would have been obvious to one of ordinary skill in the art to include a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens in the system disclosed by Fisher in order to create a resulting image with compressed and expanded zones that do not include the entire center or entire periphery as desired by the user. The development of the lens with the asymmetrical function would have been obvious to try with a reasonable expectation of success.

## Patentable Claims

16. Claims 10 and 11 are patentable. Claims 2-4, 15, 16, and 27-47 may contain patentable subject matter if amended to overcome the rejection under 35 U.S.C. 305 discussed above. 17. Enami generally teaches an image distortion correction method including extracting color information through projection using the distribution function and assigning appropriate colors on the display (Figures 2-4; paragraphs [0072]-[0074], [0084], and [0085]).

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18. Shiota and Matsui each generally teach correcting the non-linearity of an image captured by a lens (Shiota, Figure 1; paragraphs [0001], [00022], and [0028]-[0041]; Matsui, Figures 2-4 and 6; Abstract and paragraph [0025]).
19. However, the prior art of record, including Nagaoka, Baker, Fisher, Shiota, Matsui, Enami, and Inoue, does not specifically disclose or fairly teach a method for capturing a digital panoramic image or a panoramic objective lens including all of the elements, steps, and limitations recited in claims $2-4,10,11,15,16$, and $27-47$ (including all of the limitations of any respective parent claims), particularly including
correcting the non-linearity of the initial image, performed by means of a reciprocal function of the non-linear distribution function of the objective lens (e.g., claims 10 and 11); or displaying the obtained panoramic image by correcting the non-linearity of the initial image, performed by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function and a size L of the obtained image (e.g., claims $2-4,15,16$, and $27-31$ );
or particularly wherein
the panoramic image obtained by the objective lens is configured to be corrected by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function, and a size L of the obtained image (e.g., claims 32-37); or the panoramic image obtained has at least one expanded zone and at least two compressed zones (e.g., claims 38-47).

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## Conclusion

20. In order to ensure full consideration of any amendments, affidavits or declarations, or other documents as evidence of patentability, such documents must be submitted in response to this Office action. Submissions after the next Office action, which is intended to be a final action, will be governed by the requirements of 37 CFR 1.116 , after final rejection and 37 CFR 41.33 after appeal, which will be strictly enforced.
21. Extensions of time under 37 CFR 1.136(a) will not be permitted in these proceedings because the provisions of 37 CFR 1.136 apply only to "an applicant" and not to parties in a reexamination proceeding. Additionally, 35 U.S.C. 305 requires that reexamination proceedings "will be conducted with special dispatch" (37 CFR 1.550(a)). Extension of time in ex parte reexamination proceedings are provided for in 37 CFR 1.550(c).
22. The patent owner is reminded of the continuing responsibility under 37 CFR $1.565(\mathrm{a})$, to apprise the Office of any litigation activity, or other prior or concurrent proceeding, involving Patent No. 6,844,990 throughout the course of this reexamination proceeding. See MPEP §§ 2207, 2282 and 2286.
23. All correspondence relating to this ex parte reexamination proceeding should be directed:

By mail to: Mail Stop Ex Parte Reexam
Central Reexamination Unit
Commissioner for Patents
United States Patent \& Trademark Office
P.O. Box 1450

Alexandria, VA 22313-1450
By fax to: (571) 273-9900
Central Reexamination Unit
By hand to: Customer Service Window
Randolph Building

Art Unit: 3992
401 Dulany Street
Alexandria, VA 22314
Any inquiry concerning this communication should be directed to the Central Reexamination Unit at telephone number (571) 272-7705.
/Christina Y. Leung/
Primary Examiner, Art Unit 3992

Conferees:
/D.M.H./, PE AU3992
/JENNIFER MCNEIL/
Supervisory Patent Examiner, Art Unit 3992

| Search Notes | Application/Control No. $90013410$ | Applicant(s)/Patent Under Reexamination <br> 6844990 |
| :---: | :---: | :---: |
|  | Examiner <br> CHRISTINA Y LEUNG | Art Unit 3992 |


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| Class | Subclass | Date | Examiner |
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| SEARCH NOTES |  |  |  |
| :---: | :---: | :---: | :---: |
| Search Notes | Date | Examiner |  |
| Reviewed cited references and patented file's prosecution history. | $1-5-15$ | /CL/ |  |

INTERFERENCE SEARCH

| US Class/ | US Subclass / CPC Group | Date | Examiner |
| :---: | :---: | :---: | :---: |
| CPC Symbol |  |  |  |


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| Reexamination | Application/Control No. $90 / 013,410$ | Applicant(s)/Patent Under Reexamination <br> 6844990 |
| :---: | :---: | :---: |
|  | Certificate Date | Certificate Number |


| Requester Correspondence Address: $\quad \boxtimes$ Patent Owner | $\square$ Third Party |
| :--- | :--- |
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| PANITCH SCHWARZE BELSARIO \& NADEL LLP |  |
| ONE COMMERCE SQUARE |  |
| 2005 MARKET STREET, SUITE 220 |  |
| PHILADELPHIA, PA 19103 |  |
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| LITIGATION REVIEW $\boxtimes$ | Case Name |  |
| :---: | :---: | :---: |
| (examiner initials) | (date) |  |
| $1: 13 c v 1139$, Immervision Inc. v. Cbc Co. Ltd. et al. | Director Initials |  |
| $2: 13 \mathrm{cv} 1117$ Immervision, Inc. v. Vivotek, Inc. | JY |  |
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| COPENDING OFFICE PROCEEDINGS |  |
| :--- | :--- |
| TYPE OF PROCEEDING | NUMBER |
| $1 . \quad$ Inter partes review of 6,844,990 | IPR2014-01438 |
| 2. |  |
| 3. |  |
| 4. |  |

# IN THE UNITED STATES PATENT AND TRADEMARK OFFICE 

In re Patent of:
Jean-Claude ARTONNE et al.
Patent No. 6,844,990
Reexamination Control No.: 90/013,410
Filed: November 26, 2014

## For: METHOD FOR CAPTURING AND <br> DISPLAYING A VARIABLE RESOLUTION <br> DIGITAL PANORAMIC IMAGE

## AMENDMENT UNDER 37 C.F.R. $\& \S 1.111$ AND 1.530

The following Amendment and Remarks are being submitted in response to the Office Action dated January 29, 2015, and are being timely filed within the two month period set for reply, namely by March 29,2015 . No fee is believed to be due with this response, but if any fee is due, please charge such fee to Deposit Account No. 50-1017.

Amendments to and Listing of the Claims Subject to Reexamination begin on page 2 of this paper.

Remarks/Arguments begin on page 9 of this paper.

## AMENDMENTS TO AND LISTING OF CLAIMS SUBJECT TO REEXAMINATION

The following listing of claims subject to reexamination replaces all prior versions, and listings, of claims subject to reexamination.

1. (Cancelled).
2. (Amended) The method according to claim [1] 27, wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
3. (Amended) The method according to claim [1] 27, wherein the objective lens expands the center of the image and compresses the edges of the image.
4. (Amended) The method according to claim [1] 27, wherein the objective lens expands the edges of the image and compresses the center of the image.
5. (Not Subject to Reexamination).

6-7. (Cancelled).

8-9. (Not Subject to Reexamination).
10. (Amended) A method for displaying an initial panoramic image obtained in accordance with the method according to claim 1 , the method for displaying comprising: correcting the non-linearity of the initial image, performed by means of a reciprocal function of the non-linear distribution function of the objective lens [or by means of the non-linear distribution function].
11. (Original) The method according to claim 10, wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.

## 12-14. (Not Subject to Reexamination).

15. (Amended) The method according to claim [10] 27, further comprising:
determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the non-linear distribution function, and
allocating to each image point of the display window the color of an image point that is the closest on the initial image.
16. (Original) The method according to claim 15 , wherein the projection of the image points of the display window onto the initial image comprises:
projecting the image points of the display window onto a sphere or a sphere portion, determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and
projecting onto the initial image each image point projected onto the sphere or the sphere portion, the projection being performed by means of the non-linear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion.

17-20. (Cancelled).
21. (Not Subject to Reexamination).

22-23. (Cancelled).

Reexamination Control No. 90/013,410
Reply to Office Action of January 29, 2015
24. (Not Subject to Reexamination).
25. (Cancelled).
26. (Not Subject to Reexamination).
27. (New) A method for displaying a digital panoramic image, the method comprising:
obtaining a digital panoramic image by projecting a panorama onto an image sensor using a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to a field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least one substantially compressed zone; and
displaying the obtained panoramic image by correcting the non-linearity of the initial image, performed by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function and a size L of the obtained image.
28. (New) The method according to claim 27, wherein the objective lens compresses the center of the image and the edges of the image and expands an intermediate zone of the image located between the center and the edges of the image.
29. (New) The method according to claim 27, wherein the objective lens comprises a set of lenses forming an apodizer.
30. (New) The method according to claim 29, wherein the set of lenses forming an apodizer comprises at least one aspherical lens.

Reexamination Control No. 90/013,410
Reply to Office Action of January 29, 2015
31. (New) The method according to claim 27, wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.
32. (New) A panoramic objective lens comprising:
a set of lenses configured to project a panorama into an image plane of the objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to a field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that a panoramic image obtained using the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone,
wherein the panoramic image obtained by the objective lens is configured to be corrected by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function, and a size L of the obtained image.
33. (New) The lens according to claim 32, wherein the objective lens has a nonlinear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
34. (New) The lens according to claim 32, wherein the objective lens expands the center of the image and compresses the edges of the image.
35. (New) The lens according to claim 32, wherein the objective lens expands the edges of the image and compresses the center of the image.
36. (New) The lens according to claim 32 , wherein the objective lens compresses the center of the image and the edges of the image and expands an intermediate zone of the image located between the center and the edges of the image.
37. (New) The lens according to claim 32, wherein the set of lenses comprises at least one aspherical lens.
38. (New) A method for capturing a digital panoramic image, by projecting a panorama onto an image sensor using a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least two substantially compressed zones.
39. (New) The method according to claim 38, wherein the objective lens has a nonlinear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
40. (New) A method for displaying an initial panoramic image obtained in accordance with the method according to claim 38, the method for displaying comprising: correcting the non-linearity of the initial image, performed using a reciprocal function of the non-linear distribution function of the objective lens or using the non-linear distribution function.
41. (New) The method according to claim 40, wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.
42. (New) The method according to claim 41, further comprising: calculating the size of the corrected image, using the reciprocal function of the distribution function, so that the resolution of the corrected image is equivalent to the most expanded zone of the initial image, and
scanning each image point of the corrected image, searching for the position of a twin point of the image point on the initial image and allocating the color of the twin point to the image point of the corrected image.
43. (New) The method according to claim 41, wherein the initial image and the corrected image comprise an image disk.
44. (New) The method according to claim 41, further comprising:
transferring the image points of the corrected image into a three-dimensional space, and presenting one sector of the three-dimensional image obtained on a display.
45. (New) The method according to claim 40, further comprising:
determining the color of image points of a display window, by projecting the image points of the display window onto the initial image using the non-linear distribution function, and
allocating to each image point of the display window the color of an image point that is the closest on the initial image.
46. (New) The method according to claim 45, wherein the projection of the image points of the display window onto the initial image comprises:
projecting the image points of the display window onto a sphere or a sphere portion,
determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and
projecting onto the initial image each image point projected onto the sphere or the sphere portion, the projection being performed using the non-linear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion.

Reexamination Control No. 90/013,410
Reply to Office Action of January 29, 2015
47. (New) The method according to claim 38, wherein the objective lens compresses at least one zone near the center and at least one zone near the edge, and expands at least one intermediate zone of the image between the center and the edge of the image.
48. (Cancelled).

## REMARKS

Claims 1-4, 6-7, 10-11, 15-20, 22-23, 25, and 27-48 of U.S. Patent No. 6,844,990 ("the '990 Patent") are subject to reexamination. Claims 1, 6-7, and 22 were previously cancelled, claims 27-48 were previously added, and claims 2-4, 10, and 15 were previously amended by an amendment submitted with the request for reexamination. By virtue of the present amendment, claims $17-20,23,25$, and new claim 48 have been cancelled. Further, claims 27, 32, and 38 have been amended to add the term "substantially" to the "compressed" and "expanded" zones, as was present in original claims 1 and 17 of the ' 990 Patent.

Status of Patent Claims pursuant to 37 C.F.R. § 1.530(e):
$1,6-7,17-20,22-23,25$, and 48 - cancelled;
$2-4,10-11,15-16$, and $27-47$ - pending; and
$5,8-9,12-14,21,24$, and $26-$ not subject to reexamination.

No new matter has been added by the claim amendments and the amendments do not enlarge the scope of the original claims. The changes to claims 27,32 , and 38 are supported by original claims 1 and 17 of the ' 990 Patent, in addition to col. 4, 1ns. 11-21 and col. 5, 1ns. 29-39. Accordingly, entry of the amendments to the claims is respectfully requested.

## Patentable Subject Matter

Patent Owner wishes to thank the Examiner for the indication that claims 10 and 11 are patentable, and that claims 2-4, 15, 16, and 27-47 contain patentable subject matter if amended to overcome the formality rejections. By virtue of the present amendment, Patent Owner has amended claims 27,32 , and 38 to address the issues highlighted by the Examiner.

## Claim Rejections Under 35 U.S.C. § 305

Claims 2-4, 15, 16, and 27-48 were rejected under 35 U.S.C. § 305 as impermissibly broadening the scope of the original claims of the patent being reexamined. Specifically, independent claims $27,32,38$, and 48 omitted the term "substantially," which was present before the claimed "expanded" and "compressed zones" in original claims 1 and 17 of the '990 Patent.

The Examiner asserts that the omission of this term expands the scope of the claims beyond original claims 1 and 17. Claim 48 has been cancelled, and the rejection thereof rendered moot.

While not necessarily agreeing with the rejection as to remaining claims $2-4,15,16$, and 27-47, solely for the purpose of advancing the present reexamination proceeding, claims 27,32 , and 38 have each been amended to insert the term "substantially" prior to the claimed "expanded" and "compressed" zones. Patent Owner therefore respectfully requests withdrawal of the rejection of claims 2-4, 15, 16, and 27-47 under 35 U.S.C. § 305.

## Claim Rejection Under 35 U.S.C. § 112, first paragraph

Claim 48 was rejected under 35 U.S.C. § 112, first paragraph as lacking enablement for the feature of "wherein the objective lens has a non-linear distribution function that is not symmetrical relative to the optical axis of the objective lens." While not necessarily agreeing with the rejection, and solely for the purpose of advancing the reexamination proceeding, claim 48 has been cancelled, and the rejection thereof rendered moot. Patent Owner therefore respectfully requests withdrawal of the rejection.

## Claim Rejections Under 35 U.S.C. §§ 102 and 103(a)

## Claims 17-20, 23, and 25

Claims 17-20 and 23 were each rejected under 35 U.S.C. $\S 102$ as being anticipated by one or more of Nagaoka, Baker, and Fisher. Claim 25, which depends from claim 17, was also rejected under 35 U.S.C. § 103(a) as being obvious over the combinations of Nagaoka in view of Inoue and Baker in view of Inoue. While not necessarily agreeing with the rejections, and solely for the purpose of advancing the reexamination proceeding, claims 17-20, 23, and 25 have all been cancelled, and the rejections thereof rendered moot. Patent Owner therefore respectfully requests withdrawal of these prior art rejections.

## Claim 48

Claim 48 was separately rejected as being obvious under 35 U.S.C. § 103 over any of Nagaoka, Baker, or Fisher. As explained above, claim 48 has been cancelled, and the rejections

Reexamination Control No. 90/013,410
Reply to Office Action of January 29, 2015
thereof are therefore rendered moot. Patent Owner therefore respectfully requests withdrawal of these prior art rejections.

## CONCLUSION

In view of the foregoing Amendment and Remarks, Patent Owner respectfully submits that claims 2-4, 10-11, 15-16, and 27-47 are patentable, and issuance of a Reexamination Certificate confirming the same is earnestly solicited.

Dated: Februan 12,2015
Respectfully submitted,
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| Electronic Acknowledgement Receipt |  |
| :---: | :---: |
| EFS ID: | 21482987 |
| Application Number: | 90013410 |
| International Application Number: |  |
| Confirmation Number: | 4682 |
| Title of Invention: | METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE |
| First Named Inventor/Applicant Name: | 6844990 |
| Customer Number: | 570 |
| Filer: | Stephen Murray/Andrea Bennett |
| Filer Authorized By: | Stephen Murray |
| Attorney Docket Number: | 688266-21RX |
| Receipt Date: | 12-FEB-2015 |
| Filing Date: | 26-NOV-2014 |
| Time Stamp: | 13:36:47 |
| Application Type: | Reexam (Patent Owner) |

## Payment information:

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| File Listing: |  |  |  |  |  |
| Document Number | Document Description | File Name | File Size(Bytes)/ Message Digest | Multi Part /.zip | Pages (if appl.) |
| 1 | Amendment/Req. Reconsideration-After Non-Final Reject | Amendment.PDF | 527896 | no | 11 |
|  |  |  | 958 d 861 a 02378 e 2456 b 7 a 34993574 d 8 b 59 0 dbb 5 e |  |  |
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## New Applications Under 35 U.S.C. 111

If a new application is being filed and the application includes the necessary components for a filing date (see 37 CFR 1.53(b)-(d) and MPEP 506), a Filing Receipt (37 CFR 1.54) will be issued in due course and the date shown on this Acknowledgement Receipt will establish the filing date of the application.

## National Stage of an International Application under 35 U.S.C. 371

If a timely submission to enter the national stage of an international application is compliant with the conditions of 35 U.S.C. 371 and other applicable requirements a Form PCT/DO/EO/903 indicating acceptance of the application as a national stage submission under 35 U.S.C. 371 will be issued in addition to the Filing Receipt, in due course.

## New International Application Filed with the USPTO as a Receiving Office

If a new international application is being filed and the international application includes the necessary components for an international filing date (see PCT Article 11 and MPEP 1810), a Notification of the International Application Number and of the International Filing Date (Form PCT/RO/105) will be issued in due course, subject to prescriptions concerning national security, and the date shown on this Acknowledgement Receipt will establish the international filing date of the application

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The time period for reply, if any, is set in the attached communication.

| Notice of Intent to Issue | Control No. $90 / 013,410$ | Patent Under Reexamination 6844990 |  |
| :---: | :---: | :---: | :---: |
| Ex Parte Reexamination Certificate | Examiner <br> Christina Y. Leung | Art Unit $3992$ | AIA (First Inventor to File) Status No |

-- The MAILING DATE of this communication appears on the cover sheet with the correspondence address --

1. $\boxtimes$ Prosecution on the merits is (or remains) closed in this ex parte reexamination proceeding. This proceeding is subject to reopening at the initiative of the Office or upon petition. Cf. 37 CFR $1.313(\mathrm{a})$. A Certificate will be issued in view of
(a) $\boxtimes$ Patent owner's communication(s) filed: 12 February 2015.
(b) $\square$ Patent owner's failure to file an appropriate timely response to the Office action mailed: $\qquad$ —.
(c) $\square$ Patent owner's failure to timely file an Appeal Brief (37 CFR 41.31).
(d) $\square$ The decision on appeal by the $\square$ Board of Patent Appeals and Interferences $\square$ Court dated $\qquad$
(e) $\qquad$
$\qquad$ -.
2. The Reexamination Certificate will indicate the following:
(a) Change in the Specification: $\square$ Yes $\boxtimes$ No
(b) Change in the Drawing(s): $\square$ Yes $\boxtimes$ No
(c) Status of the Claim(s):
(1) Patent claim(s) confirmed: $\qquad$ _.
(2) Patent claim(s) amended (including dependent on amended claim(s)): 2-4,10,11,15 and 16
(3) Patent claim(s) canceled: 1,6,7,17-20,22,23 and 25.
(4) Newly presented claim(s) patentable: 27-47.
(5) Newly presented canceled claims: 48.
(6) Patent claim(s) $\square$ previously $\square$ currently disclaimed: $\qquad$
(7) Patent claim(s) not subject to reexamination: $5,8,9,12-14,21,24$ and 26.
3. $\square$ A declaration(s)/affidavit(s) under 37 CFR 1.130(b) was/were filed on $\qquad$ .
4. $\boxtimes$ Note the attached statement of reasons for patentability and/or confirmation. Any comments considered necessary by patent owner regarding reasons for patentability and/or confirmation must be submitted promptly to avoid processing delays. Such submission(s) should be labeled: "Comments On Statement of Reasons for Patentability and/or Confirmation."
5.Note attached NOTICE OF REFERENCES CITED (PTO-892).
5. $\boxtimes$ Note attached LIST OF REFERENCES CITED (PTO/SB/08 or PTO/SB/08 substitute).
6. $\square$ The drawing correction request filed on $\qquad$ is: $\square$ approveddisapproved
7. $\boxtimes$ Acknowledgment is made of the priority claim under 35 U.S.C. § 119(a)-(d) or (f).
a) $\boxtimes$ All b) $\square$ Some* $\quad$ c) $\square$ None of the certified copies have
$\square$ been received.
$\square$ not been received.
$\boxed{\square}$ been filed in Application No. 10/706,513.
$\square$ been filed in reexamination Control No. $\square$ been received by the International Bureau in PCT Application No. $\qquad$ _.

* Certified copies not received: $\qquad$ .
9.Note attached Examiner's Amendment.
10.Note attached Interview Summary (PTO-474).Other: $\qquad$
All correspondence relating to this reexamination proceeding should be directed to the Central Reexamination Unit at the mail, FAX, or hand-carry addresses given at the end of this Office action.

|  | /Christina Y. Leung/ <br> Primary Examiner, Art Unit 3992 |
| :--- | :--- | :--- |
| ce: Requester (if third party requester) <br> U.S. Patent and Trademark Office   <br> PTOL-469 (Rev. 08-13) Notice of Intent to Issue Ex Parte Reexamination Certificate Part of Paper No 20150224 |  |

# STATEMENT OF REASONS FOR PATENTABILITY AND/OR CONFIRMATION 

1. Claims 1-4, 6, 7, 10, 11, 15-20, 22, 23, and 25 of Artonne (US 6,844,990 B2) are being reexamined. Claims $1,6,7,17-20,22,23,25$, and 48 have been canceled. Claims $5,8,9,12-14$, 21,24 , and 26 are not subject to reexamination.
2. Claims 2-4, 10, 11, 15, and 16, and new claims 27-47 are patentable.
3. The following is an examiner's statement of reasons for patentability and/or confirmation of the claims found patentable in this reexamination proceeding:

Patent Owner's (PO's) amendment filed 12 February 2015 has overcome all of the rejections in the previous Office action mailed 29 January 2015. As noted in that action, the prior art of record, including Nagaoka, Baker, Fisher, Shiota, Matsui, Enami, and Inoue, does not specifically disclose or fairly teach a method for capturing a digital panoramic image or a panoramic objective lens including all of the elements, steps, and limitations recited in claims 2$4,10,11,15,16$, and 27-47 (including all of the limitations of any respective parent claims), particularly including
correcting the non-linearity of the initial image, performed by means of a reciprocal function of the non-linear distribution function of the objective lens (e.g., claims 10 and 11); or displaying the obtained panoramic image by correcting the non-linearity of the initial image, performed by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function and a size L of the obtained image (e.g., claims $2-4,15,16$, and 27-31);
or particularly wherein

Art Unit: 3992
the panoramic image obtained by the objective lens is configured to be corrected by retrieving image points on the obtained image in a coordinate system of center $\mathrm{O}^{\prime}$ using at least the non-linear distribution function, and a size $L$ of the obtained image (e.g., claims 32-37); or
the panoramic image obtained has at least one expanded zone and at least two compressed zones (e.g., claims 38-47).
4. Any comments considered necessary by PATENT OWNER regarding the above statement must be submitted promptly to avoid processing delays. Such submission by the patent owner should be labeled: "Comments on Statement of Reasons for Patentability and/or Confirmation" and will be placed in the reexamination file.
5. All correspondence relating to this ex parte reexamination proceeding should be directed:

By mail to: Mail Stop Ex Parte Reexam
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Commissioner for Patents
United States Patent \& Trademark Office
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Alexandria, VA 22313-1450

By fax to: (571) 273-9900
Central Reexamination Unit

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Randolph Building
401 Dulany Street
Alexandria, VA 22314

Any inquiry concerning this communication should be directed to the Central
Reexamination Unit at telephone number (571) 272-7705.
/Christina Y. Leung/
Primary Examiner, Art Unit 3992
Conferees:

Application/Control Number: 90/013,410
Art Unit: 3992
/Deandra M. Hughes/, Reexamination Specialist AU 3992
/Woo H. Choi/
SPRS, Art Unit 3992

| INFORMATION DISCLOSURE STATEMENT BY APPLICANT <br> ( Not for submission under 37 CFR 1.99) | Application Number |  | 90013410 |
| :---: | :---: | :---: | :---: |
|  | Filing Date |  | 2014-11-26 |
|  | First Named Inventor | Jean-Claude ARTONNE |  |
|  | Art Unit |  | 3992 |
|  | Examiner Name | Christina Y. Leung |  |
|  | Attorney Docket Number |  | 688266-21RX |


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| Examiner Initia\|* | $\begin{aligned} & \text { Cite } \\ & \text { No } \end{aligned}$ | Patent Number |  | Kind Code ${ }^{1}$ | Issue Date |  | Name of Patentee or Applicant of cited Document |  | Pages,Columns,Lines where Relevant Passages or Relevant Figures Appear |  |  |
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| INFORMATION DISCLOSURE STATEMENT BY APPLICANT <br> ( Not for submission under 37 CFR 1.99) | Application Number |  | 90013410 |
| :---: | :---: | :---: | :---: |
|  | Filing Date |  | 2014-11-26 |
|  | First Named Inventor | Jean-Claude ARTONNE |  |
|  | Art Unit |  | 3992 |
|  | Examiner Name | Christina Y. Leung |  |
|  | Attorney Docket Number |  | 688266-21RX |


| CL | $1 \quad$App <br> Editi | Applied Photographic Optics; Lenses and optical systems for photography, film, video and electronic imaging. Second Edition by Sidney F. Ray (1998) |  |  | $\square$ |
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| ${ }^{1}$ See Kind Codes of USPTO Patent Documents at www.USPTO.GOV or MPEP 901.04. ${ }^{2}$ Enter office that issued the document, by the two-letter code (WIPO Standard ST.3). ${ }^{3}$ For Japanese patent documents, the indication of the year of the reign of the Emperor must precede the serial number of the patent document. ${ }^{4}$ Kind of document by the appropriate symbols as indicated on the document under WIPO Standard ST. 16 if possible. ${ }^{5}$ Applicant is to place a check mark here i English language translation is attached. |  |  |  |  |  |

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## BIB DATA SHEET

CONFIRMATION NO. 4682

| SERIAL NUMBER 90/013,410 |  | FILING DA <br> 11/26 <br> RU | 371(c) <br> 14 | CLASS <br> 359 | GROUP AR $3992$ |  | RNEY DOCKET NO. 88266-21RX |
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| Foreign Priority claim 35 USC 119(a-d) co Verified and <br> Acknowledged | ed ditions /CHRIS LEUNG Examine | $\begin{aligned} & \boldsymbol{\nabla}_{\mathrm{Yes}} \square_{\mathrm{No}} \\ & \mathrm{Y}_{\mathrm{Yes}} \square_{\mathrm{No}} \\ & \text { gnature } \end{aligned}$ | $\square . \begin{gathered}\text { Met } \\ \text { Allow }\end{gathered}$ Tntials | STATE OR COUNTRY | SHEETS DRAWINGS | TOTAL CLAIMS 26 | INDEPENDENT CLAIMS 2 |
| PANITCH SCHWARZE BELISARIO \& NADEL LLP ONE COMMERCE SQUARE 2005 MARKET STREET, SUITE 2200 PHILADELPHIA, PA 19103 UNITED STATES |  |  |  |  |  |  |  |
| METHOD FOR CAPTURING AND DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE |  |  |  |  |  |  |  |
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| Reexamination | Application/Control No. $90 / 013,410$ | Applicant(s)/Patent Under Reexamination $6844990$ |
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| LITIGATION REVIEW $\boxtimes$ | Case Name |
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| $1: 13 \mathrm{cv} 1139$, Immervision, Inc. v. Cbc Co. Ltd. et al. | Director Initials |
| $2: 13 \mathrm{cv1117}$ Immervision, Inc. v. Vivotek, Inc. |  |
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| COPENDING OFFICE PROCEEDINGS |  |
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| $1 . \quad$ Inter partes review of 6,844,990 | IPR2014-01438 |
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| Search Notes | Application/Control No. $90013410$ | Applicant(s)/Patent Under Reexamination <br> 6844990 |
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|  | Examiner <br> CHRISTINA Y LEUNG | Art Unit <br> 3992 |


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| Reviewed cited references and patented file's prosecution history. | $2-24-15$ | /CL/ |  |

## INTERFERENCE SEARCH

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| Issue Classification | Application／Control No． $90013410$ | Applicant（s）／Patent Under Reexamination $6844990$ |
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| （Assistant Examiner） | （Date） | Total Claims Allowed： |
| ／CHRISTINA Y LEUNG／ <br> Primary Examiner．Art Unit 3992 <br> （Primary Examiner） | $02 / 25 / 2015$ | O．G．Print Claim（s） |
| O．G．Print Figure |  |  |


| Issue Classification | Application/Control No. $90013410$ | Applicant(s)/Patent Under Reexamination $6844990$ |
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|  | Examiner <br> CHRISTINA Y LEUNG | Art Unit $3992$ |



| NONE <br> (Assistant Examiner) | (Date) | Total Claims Allowed:$28$ |  |
| :---: | :---: | :---: | :---: |
| /CHRISTINA Y LEUNG/ <br> Primary Examiner.Art Unit 3992 <br> (Primary Examiner) | $02 / 25 / 2015$ <br> (Date) | O. G. Print Claim(s) $27$ | O.G. Print Figure $11$ |


| Issue Classification | Application/Control No. $90013410$ | Applicant(s)/Patent Under Reexamination $6844990$ |
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| 区 | Claims renumbered in the same order as presented by applicant |  |  |  |  |  |  | - | CPA |  | $\square \quad$ т.D. | $\square \quad$ R. |  | R.1.47 |  |
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| NONE <br> (Assistant Examiner) | (Date) | Total Claims Allowed:$28$ |  |
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| /CHRISTINA Y LEUNG/ <br> Primary Examiner.Art Unit 3992 <br> (Primary Examiner) | 02/25/2015 <br> (Date) | O.G. Print Claim(s) 27 | O.G. Print Figure $11$ |

## (12) EX PARTE REEXAMINATION CERTIFICATE (10588th) United States Patent <br> (10) Number: $\quad$ US 6,844,990 C1 <br> Artonne et al. <br> (45) Certificate Issued: May 8, 2015

(54) METHOD FOR CAPTURING AND

DISPLAYING A VARIABLE RESOLUTION DIGITAL PANORAMIC IMAGE
(75) Inventors: Jean-Claude Artonne, Montreal (CA); Christophe Moustier, Marseilles (FR); Benjamin Blanc, Montreal (CA)
(73) Assignee: 6115187 CANADA, INC., Saint

Laurent, Quebec (CA)
Reexamination Request:
No. 90/013,410, Nov. 26, 2014

## Reexamination Certificate for:

Patent No.: $\quad \mathbf{6 , 8 4 4 , 9 9 0}$
Issued: Jan. 18, 2005
Appl. No.: 10/706,513
Filed: Nov. 12, 2003
Certificate of Correction issued May 24, 2005

## Related U.S. Application Data

(63) Continuation of application No. PCT/FR02/01588, filed on May 10, 2002.

Foreign Application Priority Data
May 11, 2001
(FR) $\qquad$ 0106261
(51) Int. Cl.

G02B 13/06
H04N 5/225
(2006.01)
(2006.01)
(52) U.S. Cl.

CPC .............. H04N 5/2254 (2013.01); G02B 13/06
(2013.01)
(58) Field of Classification Search

None
See application file for complete search history.

## References Cited

To view the complete listing of prior art documents cited during the proceeding for Reexamination Control Number 90/013,410, please refer to the USPTO's public Patent Application Information Retrieval (PAIR) system under the Display References tab.

Primary Examiner - Christina Y Leung

## (57)

ABSTRACT
A method for capturing a digital panoramic image includes projecting a panorama onto an image sensor by means of a panoramic objective lens. The panoramic objective lens has a distribution function of the image points that is not linear relative to the field angle of the object points of the panorama, such that at least one zone of the image obtained is expanded while at least another zone of the image is compressed. When a panoramic image obtained is then displayed, correcting the non-linearity of the initial image is required and is performed by means of a reciprocal function of the non-linear distribution function of the objective lens or by means of the nonlinear distribution function.


EX PARTE
REEXAMINATION CERTIFICATE ISSUED UNDER 35 U.S.C. 307

## THE PATENT IS HEREBY AMENDED AS INDICATED BELOW.

Matter enclosed in heavy brackets [] appeared in the patent, but has been deleted and is no longer a part of the patent; matter printed in italics indicates additions made to the patent.

## AS A RESULT OF REEXAMINATION, IT HAS BEEN DETERMINED THAT:

Claims 1, 6, 7, 17-20, 22, $\mathbf{2 3}$ and $\mathbf{2 5}$ are cancelled.
Claims 2-4, $\mathbf{1 0}$ and $\mathbf{1 5}$ are determined to be patentable as amended.

Claims 11 and 16, dependent on an amended claim, are 20 determined to be patentable.

New claims 27-47 are added and determined to be patentable.

Claims 5, 8, 9, 12-14, 21, 24 and 26 were not reexamined.
2. The method according to claim [1] 27, wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
3. The method according to claim [1] 27, wherein the objective lens expands the center of the image and compresses the edges of the image.
4. The method according to claim [1] 27, wherein the objective lens expands the edges of the image and compresses the center of the image.
10. A method for displaying an initial panoramic image obtained in accordance with the method according to claim 1, the method for displaying comprising:
correcting the non-linearity of the initial image, performed by means of a reciprocal function of the non-linear distribution function of the objective lens [or by means of the non-linear distribution function].
15. The method according to claim [10] 27, further comprising:
determining the color of image points of a display window, by projecting the image points of the display window onto the initial image by means of the non-linear distribution function, and
allocating to each image point of the display window the color of an image point that is the closest on the initial image.
27. A method for displaying a digital panoramic image, the method comprising:
obtaining a digital panoramic image by projecting a panorama onto an image sensor using a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to a field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+-10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least one substantially compressed zone; and
displaying the obtained panoramic image by correcting the non-linearity of the initial image, performed by retriev-
ing image points on the obtained image in a coordinate system of center $O^{\prime}$ using at least the non-linear distribution function and a size $L$ of the obtained image.
28. The method according to claim 27 , wherein the objec5 tive lens compresses the center of the image and the edges of the image and expands an intermediate zone of the image located between the center and the edges of the image.
29. The method according to claim 27, wherein the objective lens comprises a set of lenses forming an apodizer.
30. The method according to claim 29 , wherein the set of lenses forming an apodizer comprises at least one aspherical lens.
31. The method according to claim 27 , wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.
32. A panoramic objective lens comprising:
a set of lenses configured to project a panorama into an image plane of the objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to a field angle of object points of the panorama, the distribution function having a maximum divergence of at least $+/-10 \%$ compared to a linear distribution function, such that a panoramic image obtained using the objective lens comprises at least one substantially expanded zone and at least one substantially compressed zone,
wherein the panoramic image obtained by the objective lens is configured to be corrected by retrieving image points on the obtained image in a coordinate system of center $O^{\prime}$ using at least the non-linear distribution function, and a size $L$ of the obtained image.
33. The lens according to claim 32, wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
34. The lens according to claim 32, wherein the objective lens expands the center of the image and compresses the edges of the image.
35. The lens according to claim 32, wherein the objective lens expands the edges of the image and compresses the center of the image.
36. The lens according to claim 32, wherein the objective lens compresses the center of the image and the edges of the image and expands an intermediate zone of the image located between the center and the edges of the image.
37. The lens according to claim 32, wherein the set oflenses comprises at least one aspherical lens.
38. A method for capturing a digital panoramic image, by projecting a panorama onto an image sensor using a panoramic objective lens, the panoramic objective lens having an image point distribution function that is not linear relative to the field angle of object points of the panorama, the distribution function having a maximum divergence of at least $10 \%$ compared to a linear distribution function, such that the panoramic image obtained has at least one substantially expanded zone and at least two substantially compressed zones.
39. The method according to claim 38 , wherein the objective lens has a non-linear distribution function that is symmetrical relative to the optical axis of the objective lens, the position of an image point relative to the center of the image varying according to the field angle of the corresponding object point.
40. A method for displaying an initial panoramic image obtained in accordance with the method according to claim 38, the method for displaying comprising:
correcting the non-linearity of the initial image, performed using a reciprocal function of the non-linear distribution 5 function of the objective lens or using the non-linear distribution function.
41. The method according to claim 40 , wherein the step of correcting comprises a step of transforming the initial image into a corrected digital image comprising a number of image points higher than the number of pixels that the image sensor comprises.
42. The method according to claim 41, further comprising:
calculating the size of the corrected image, using the reciprocal function of the distribution function, so that the resolution of the corrected image is equivalent to the most expanded zone of the initial image, and
scanning each image point of the corrected image, searching for the position of a twin point of the image point on the initial image and allocating the color of the twin 20 point to the image point of the corrected image.
43. The method according to claim 41, wherein the initial image and the corrected image comprise an image disk.
44. The method according to claim 41, further comprising:
transferring the image points of the corrected image into a 2 three-dimensional space, and
presenting one sector of the three-dimensional image obtained on a display.
45. The method according to claim 40, further comprising: determining the color of image points of a display window, by projecting the image points of the display window onto the initial image using the non-linear distribution function, and
allocating to each image point of the display window the color of an image point that is the closest on the initial image.
46. The method according to claim 45 , wherein the projection of the image points of the display window onto the initial image comprises:
projecting the image points of the display window onto $a$ sphere or a sphere portion,
determining the angle in relation to the center of the sphere or the sphere portion of each projected image point, and projecting onto the initial image each image point projected onto the sphere or the sphere portion, the projection being performed using the non-linear distribution function considering the field angle that each point to be projected has in relation to the center of the sphere or the sphere portion.
47. The method according to claim 38, wherein the objective lens compresses at least one zone near the center and at least one zone near the edge, and expands at least one intermediate zone of the image between the center and the edge of the image.


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[^5]:    ${ }^{1}$ Copy attached as Exhibit 2.
    ${ }^{2}$ All references to 35 U.S.C. $\S \S 102$ and 103 herein are with respect to pre-AIA versions thereof.
    ${ }^{3}$ Copy attached as Exhibit 3.
    ${ }^{4}$ Copy attached as Exhibit 4.
    ${ }^{5}$ Copy attached as Exhibit 5.
    ${ }^{6}$ Copy of Japanese Publication attached as Exhibit 6a, a certified English translation thereof is attached as Exhibit 6b.

[^6]:    ${ }^{7}$ Copy of Japanese Publication attached as Exhibit 7a, a certified English translation thereof is attached as Exhibit 7b.
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