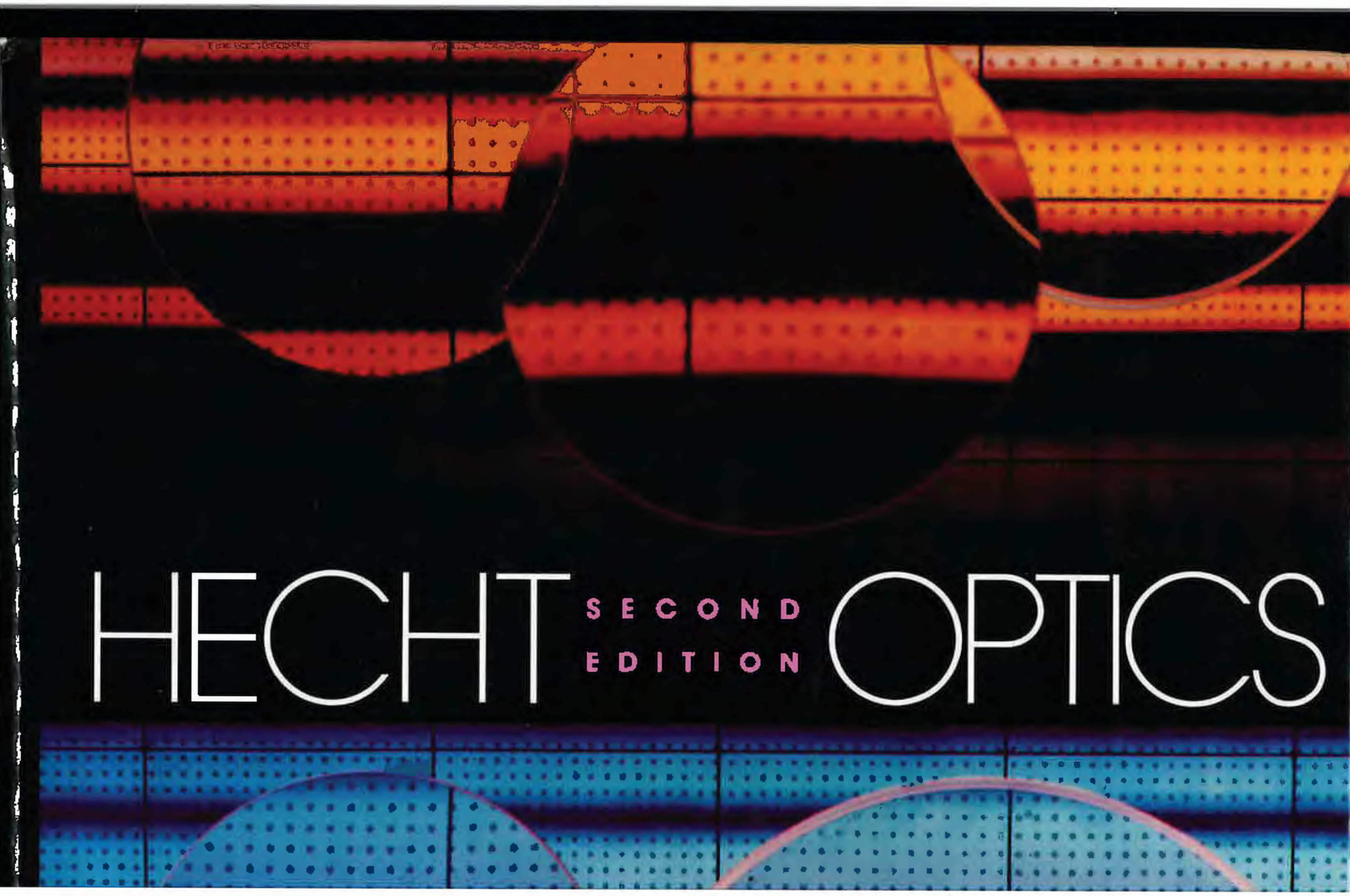
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SECOND EDITION
OPTICS

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SECOND EDITION

EUGENE HECHT
Adelphi University

With Contributions by Alfred Zajac

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To Ca, b. w. l.

Preface

The creation of this second edition was guided primarily by two distinct imperatives: to incorporate the pedagogical insights gained in the classroom over the past dozen years, and to bring the book in step with the fast-moving edge of optical technology. Accordingly, several sections have been reorganized, some condensed, others extended, and the exposition updated and improved throughout. In the process I have added a number of graphs, drawings and photographs, as well as a good deal of new textual material—always with the motivation of enlivening and clarifying the treatment.

As well as the very many small but significant refinements that are incorporated in this second edition, there are also some substantive improvements in methodology and emphasis. For example, atomic processes associated with radiation and absorption are considered earlier and in more detail. The central role of scattering in optics (e.g., in reflection, refraction, and dispersion) can thereafter be understood more intuitively (Chapter 3). Huygens's principle, which is so useful and yet so contrived, then takes on a physical significance that is far more satisfying. Accordingly, several of the original classic derivations (those associated with the propagation of light and its interaction with material interfaces) have been recast, and additional ones have been included as well (e.g., internal reflection as viewed from the perspective of atomic scattering, p. 106, Fig. 4.35).

With the realization that a picture is indeed worth a thousand words, new illustrations have been added to the discussion of geometrical optics (Chapters 5 and 6), primarily to facilitate a better understanding of ray tracing and image formation. Not surprisingly, the discussion of fiberoptics has been considerably extended to include the remarkable developments of the last decade. The introduction to Fourier methods (Chapter 7) has been strengthened, in part, so that these ideas can be applied more naturally in the remaining exposition. Often unduly troublesome, the notion of waves leading and lagging one another is given additional attention as it relates to polarization (Chapter 8). The ramifications of the limited coherence of a typical light source are now examined, if only briefly, during the study of interference (Chapter 9). Using a new set of wavefront diagrams (e.g., Figs. 10.6, 10.10, 10.19) the plane-wave Fourier-component representation of diffraction (Chapter 10) is unobtrusively introduced early on. Enlarged and refined, the discussion of Fourier optics (Chapter 11) now contains a simpler, more pictorial representation that complements the formal mathematical treatment (there are 25 new diagrams in Chapter 11 alone). The intention is to make this material increasingly accessible to an ever wider readership. Much of the treatment of coherence theory (Chapter 12) has been reworked and reillustrated to produce a simpler, more accessible version. The discussions of lasers and holography (Chapter 14) have also been appropriately extended and brought up to date.

The natural tendency in a textbook is to isolate the principle ideas, focusing exclusively on each of them in turn: Thus there are the traditional chapters on interference, diffraction, polarization, and so forth. The first edition more or less followed that approach, while at the same time underscoring conceptual interrelationships and the unity of the entire subject—after all, optics, like all of physics, is the study of the interaction of matter and energy. This second edition subtly moves a bit further toward a holistic approach. The text now introduces many of the unifying ideas, albeit on a simple level, as soon as is appropriate. For example, the concept of interference is used qualitatively to understand propagation phenomena (p. 63) long before it's studied formally in Chapter 9. Among other benefits, this technique of presenting advanced concepts in simplified form early in the exposition allows the student to develop an integrated perspective.

Responding to requests from users, I have considerably increased the amount of material devoted to the analysis and solution of problems. The book now contains an abundance of problems, roughly twice the number that appeared in the first edition. Moreover, a portion of these are specifically designed to develop needed analytical skills. Because a balance was maintained, with as many "easy" problems added as hard ones, the exercises should better serve the needs of the student reader. This is especially true because, as in the first edition, the complete solutions to many of the problems (those without asterisks) can be found at the back of the book.

Over the years many people have been kind enough to share their thoughts about the book with me and I take this opportunity to express my appreciation to them all. In particular I thank Professors R. G. Wilson of Illinois Wesleyan University, B. Gottschalk of Harvard University, E. W. Jenkins of The University of Arizona, W. M. Becker of Purdue University, L. R. Wilcox of S.U.N.Y. Stony Brook, R. Talaga of the University of Maryland, R. A. Llewellyn of the University of Central Florida, R. Schiller of Stevens Institute of Technology, S. P. Almeida of Virginia Polytechnic Institute and State University, G. Indebetouw of Virginia Polytechnic Institute and State University, and J. Higbie of the University of Queensland. Wherever possible I have incorporated photographs and suggestions by students and encourage their continued participation. Anyone wishing to exchange ideas should write to the author c/o Physics Department, Adelphi University, Garden City, N.Y. 11530.

I am especially grateful to Lorraine Ferrier, who oversaw the production of this second edition. She worked long hours, good naturedly bringing to bear a rare combination of skill, patience, and knowledge that made this book physically as fine as it is. Finally, I nod appreciatively to my friend Carolyn Eisen Hecht for going through all this, one more time.

Freeport, New York E.H.

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OPTICS

Second Edition

1 A BRIEF HISTORY

1.1 PROLEGOMENON

In chapters to come we will evolve a formal treatment of much of the science of optics with particular emphasis on aspects of contemporary interest. The subject embraces a vast body of knowledge accumulated over roughly three thousand years of the human scene. Before embarking on a study of the modern view of things optical, let's briefly trace the road that led us there, if for no other reason than to put it all in perspective.

The complete story has myriad subplots and characters, heroes, quasi-heroes, and an occasional villain or two. Yet from our vantage in time, we can sift out of the tangle of millennia perhaps four main themes—the optics of reflection and refraction, and the wave and quantum theories of light.

1.2 IN THE BEGINNING

The origins of optical technology date back to remote antiquity. Exodus 38:8 (ca. 1200 B.C.) recounts how Bezaleel, while preparing the ark and tabernacle, recast "the looking-glasses of the women" into a brass laver (a ceremonial basin). Early mirrors were made of polished copper, bronze, and later on of speculum, a copper alloy rich in tin. Specimens have survived from ancient Egypt—a mirror in perfect condition was unearthed along with some tools from the workers' quarters near the pyramid of Sesostris II (ca. 1900 B.C.) in the Nile valley. The Greek philosophers Pythagoras, Democritus, Empedocles, Plato, Aristotle, and others evolved several theories of the nature of light (that of the last named being quite similar to the aether theory of the nineteenth century). The rectilinear propagation of light was known, as was the law of reflection enunciated by Euclid (300 B.C.) in his book *Catoptrics*. Hero of Alexandria attempted to explain both these phenomena by asserting that light traverses the shortest allowed path between two points. The burning glass (a positive lens) was alluded to by Aristophanes in his comic play *The Clouds* (424 B.C.). The apparent bending of objects partly immersed in water is mentioned in Plato's *Republic*. Refraction was studied by Cleomedes (50 A.D.) and later by Claudius Ptolemy (130 A.D.) of Alexandria, who tabulated fairly precise measurements of the angles of incidence and refraction for several media. It is clear from the accounts of the historian Pliny (23–79 A.D.) that the Romans also possessed burning glasses. Several glass and crystal spheres, which were probably used to start fires, have been found among Roman ruins, and a planar convex lens was recovered in Pompeii. The Roman philosopher Seneca (3 B.C.–65 A.D.) pointed out that a glass globe filled with water could be used for magnifying purposes. And it is certainly possible that some Roman artisans may have used magnifying glasses to facilitate very fine detailed work.

After the fall of the Western Roman Empire (475 A.D.), which roughly marks the start of the Dark

Ages, little or no scientific progress was made in Europe for a great while. The dominance of the Greco-Roman-Christian culture in the lands embracing the Mediterranean soon gave way by conquest to the rule of Allah. Alexandria fell to the Moslems in 642 A.D., and by the end of the seventh century, the lands of Islam extended from Persia across the southern coast of the Mediterranean to Spain. The center of scholarship shifted to the Arab world, where the scientific and philosophical treasures of the past were translated and preserved. Rather than lying intact but dormant, as much of science did, optics was extended at the hands of Alhazen (ca. 1000 A.D.). He elaborated on the law of reflection, putting the angles of incidence and reflection in the same plane normal to the interface; he studied spherical and parabolic mirrors and gave a detailed description of the human eye.

By the latter part of the thirteenth century, Europe was only beginning to rouse from its intellectual stupor. Alhazen's work was translated into Latin, and it had a great effect on the writings of Robert Grosseteste (1175–1253), Bishop of Lincoln, and on the Polish mathematician Vitello (or Witelo), both of whom were influential in rekindling the study of optics. Their works were known to the Franciscan Roger Bacon (1215–1294), who is considered by many to be the first scientist in the modern sense. He seems to have initiated the idea of using lenses for correcting vision and even hinted at the possibility of combining lenses to form a telescope. Bacon also had some understanding of the way in which rays traverse a lens. After his death, optics again languished. Even so, by the mid-1300s, European paintings were depicting monks wearing eyeglasses. And alchemists had come up with a liquid amalgam of tin and mercury that was rubbed onto the back of glass plates to make mirrors. Leonardo da Vinci (1452–1519) described the *camera obscura*, later popularized by the work of Giovanni Battista Della Porta (1535–1615), who discussed multiple mirrors and combinations of positive and negative lenses in his *Magia naturalis* (1589).

This, for the most part, modest array of events constitutes what might be called the first period of optics. It was undoubtedly a beginning—but on the whole a dull one. It was more a time for learning how to play the game than actually scoring points. The whirlwind of accomplishment and excitement was to come later, in the seventeenth century.

1.3 FROM THE SEVENTEENTH CENTURY

It is not clear who actually invented the refracting telescope, but records in the archives at The Hague show that on October 2, 1608, Hans Lippershey (1587–1619), a Dutch spectacle maker, applied for a patent on the device. Galileo Galilei (1564–1642), in Padua, heard about the invention and within several months had built his own instrument, grinding the lenses by hand. The compound microscope was invented at just about the same time, possibly by the Dutchman Zacharias Janssen (1588–1632). The microscope's concave eyepiece was replaced with a convex lens by Francisco Fontana (1580–1656) of Naples, and a similar change in the telescope was introduced by Johannes Kepler (1571–1630). In 1611, Kepler published his *Dioptrice*. He had discovered total internal reflection and arrived at the small angle approximation to the law of refraction, in which case the incident and transmission angles are proportional. He evolved a treatment of first-order optics for thin-lens systems and in his book describes the detailed operation of both the Keplerian (positive eyepiece) and Galilean (negative eyepiece) telescopes. Willebrord Snell (1591–1626), professor at Leyden, empirically discovered the long-hidden *law of refraction* in 1621—this was one of the great moments in optics. By learning precisely how rays of light are redirected on traversing a boundary between two media, Snell in one swoop swung open the door to modern applied optics. René Descartes (1596–1650) was the first to publish the now familiar formulation of the law of refraction in terms of sines. Descartes deduced the law using a model in which light was viewed as a pressure transmitted by an elastic medium; as he put it in his *La Dioptrique* (1637)

> . . . recall the nature that I have attributed to light, when I said that it is nothing other than a certain motion or an action conceived in a very subtle matter, which fills the pores of all other bodies. . . .

The universe was a plenum. Pierre de Fermat (1601–1665), taking exception to Descartes's assumptions, rederived the law of reflection from his own *principle of least time* (1657). Departing from Hero's shortest-path statement, Fermat maintained that light propagates from one point to another along the route taking the least time, even if it has to vary from the shortest actual path to do it.

Figure 1.1 Johannes Kepler (1571–1630).

The phenomenon of diffraction, i.e., the deviation from rectilinear propagation that occurs when light advances beyond an obstruction, was first noted by Professor Francesco Maria Grimaldi (1618–1663) at the Jesuit College in Bologna. He had observed bands of light within the shadow of a rod illuminated by a small source. Robert Hooke (1635–1703), curator of experiments for the Royal Society, London, later also observed diffraction effects. He was the first to study the colored interference patterns generated by thin films (*Micrographia*, 1665) and correctly concluded that they were due to an interaction between the light reflected from the front and back surfaces. He proposed the idea that light was a rapid vibratory motion of the medium propagating at a very great speed. Moreover "every pulse or vibration of the luminous body will generate a sphere"—this was the beginning of the wave theory. Within a year of Galileo's death, Isaac Newton (1642–1727) was born. The thrust of Newton's scientific effort is clear from his own description of his work in optics as *experimental philosophy*. It was his intent to build on direct observation and avoid speculative hypotheses. Thus he remained ambivalent for a long while about the actual nature of light. Was it corpuscular—a stream of particles, as some maintained? Or was light a wave in an all-pervading medium, the aether? At the age of 23, he began his now famous experiments on dispersion.

> I procured me a triangular glass prism to try therewith the celebrated phenomena of colours.

Newton concluded that white light was composed of a mixture of a whole range of independent colors. He maintained that the corpuscles of light associated with the various colors excited the aether into characteristic

Figure 1.2 René Descartes (1596–1650).

Figure 1.3 Sir Isaac Newton (1642–1727).

vibrations. Furthermore, the sensation of red corresponded to the longest vibration of the aether, and violet to the shortest. Even though his work shows a curious propensity for simultaneously embracing both the wave and emission (corpuscular) theories, he did become more committed to the latter as he grew older. Perhaps his main reason for rejecting the wave theory as it stood then was the blatant problem of explaining rectilinear propagation in terms of waves that spread out in all directions.

After some all-too-limited experiments, Newton gave up trying to remove chromatic aberration from refracting telescope lenses. Erroneously concluding that it could not be done, he turned to the design of reflectors. Sir Isaac's first reflecting telescope, completed in 1668, was only 6 inches long and 1 inch in diameter, but it magnified some 30 times.

At about the same time that Sir Isaac was emphasizing the emission theory in England, Christiaan Huygens (1629–1695), on the continent, was greatly extending the wave theory. Unlike Descartes, Hooke, and Newton, Huygens correctly concluded that light effectively slowed down on entering more dense media. He was able to derive the laws of reflection and refraction and even explained the double refraction of calcite, using his wave theory. And it was while working with calcite that he discovered the phenomenon of *polarization.*

> As there are two different refractions, I conceived also that there are two different emanations of the waves of light. . . .

Thus light was either a stream of particles or a rapid undulation of aethereal matter. In any case, it was generally agreed that its speed of propagation was exceedingly large. Indeed, many believed that light propagated instantaneously, a notion that went back at least as far as Aristotle. The fact that it was finite was determined by the Dane Ole Christensen Römer (1644–1710). Jupiter's nearest moon, Io, has an orbit about that planet that is nearly in the plane of Jupiter's own orbit around the Sun. Römer made a careful study of the eclipses of Io as it moved through the shadow behind Jupiter. In 1676 he predicted that on November 9th Io would emerge from the dark some 10 minutes later than would have been expected on the basis of its yearly averaged motion. Precisely on schedule, Io performed as predicted, a phenomenon Römer correctly explained as arising from the finite speed of light. He was able to determine that light took about 22 minutes to traverse the diameter of the Earth's orbit around the Sun—a distance of about 186 million miles. Huygens and Newton, among others, were quite convinced of the validity of Römer's work. Independently estimating the Earth's orbital diameter, they assigned values to c equivalent to 2.3×10^8 m/s and 2.4×10^8 m/s, respectively. Still others, especially Hooke, remained skeptical, arguing that any speed so incredibly high actually had to be infinite.*

Figure 1.4 Christiaan Huygens (1629–1695).

The great weight of Newton's opinion hung like a shroud over the wave theory during the eighteenth century, all but stifling its advocates. There were too many content with dogma and too few nonconformist enough to follow their own experimental philosophy, as surely Newton would have had them do. Despite this, the prominent mathematician Leonhard Euler (1707–1783) was a devotee of the wave theory, even if an unheeded one. Euler proposed that the undesirable color effects seen in a lens were absent in the eye (which is an erroneous assumption) because the different media present negated dispersion. He suggested that achromatic lenses might be constructed in a similar way. Enthused by this work, Samuel Klingenstjerna (1698–1765), a professor at Upsala, reperformed Newton's experiments on achromatism and determined them to be in error. Klingenstjerna was in communication with a London optician, John Dollond (1706–1761), who was observing similar results. Dollond finally, in 1758, combined two elements, one of crown and the other of flint glass, to form a single achromatic lens. This was an accomplishment of very great practical importance. Incidentally, Dollond's invention was actually preceded by the unpublished work of the amateur scientist Chester Moor Hall (1703–1771) of Moor Hall in Essex.

* A. Wróblewski, *Am. J. Phys.* **53** (7), July 1985, p. 620.

1.4 THE NINETEENTH CENTURY

The wave theory of light was reborn at the hands of Dr. Thomas Young (1773–1829), one of the truly great minds of the century. On November 12, 1801, July 1, 1802, and November 24, 1803, he read papers before the Royal Society extolling the wave theory and adding to it a new fundamental concept, the so-called *principle of interference:*

> When two undulations, from different origins, coincide either perfectly or very nearly in direction, their joint effect is a combination of the motions belonging to each.

He was able to explain the colored fringes of thin films and determined wavelengths of various colors using Newton's data. Even though Young, time and again, maintained that his conceptions had their very origins in the research of Newton, he was severely attacked. In a series of articles, probably written by Lord Brougham, in the *Edinburgh Review*, Young's papers were said to be "destitute of every species of merit"—and that's going pretty far. Under the pall of Newton's presumed infallibility, the pedants of England were not prepared for the wisdom of Young, who in turn became disheartened.

Augustin Jean Fresnel (1788–1827), born in Broglie, Normandy, began his brilliant revival of the wave theory in France, unaware of the efforts of Young some 13 years earlier. Fresnel synthesized the concepts of Huygens's wave description and the interference principle. The mode of propagation of a primary wave was viewed as a succession of stimulated spherical secondary wavelets, which overlapped and interfered to reform the advancing primary wave as it would appear an instant later. In Fresnel's words:

> The vibrations of a luminous wave in any one of its points may be considered as the sum of the elementary movements conveyed to it at the same moment, from the separate action of all the portions of the unobstructed wave considered in any one of its anterior positions.

These waves were presumed to be longitudinal in analogy with sound waves in air. Dominique François Jean Arago (1786–1853) was an early convert to Fresnel's wave theory, and they became fast friends and sometime collaborators. Under criticism from such renowned men and proponents of the emission hypothesis as Pierre Simon de Laplace (1749–1827) and Jean-Baptiste Biot (1774–1862), Fresnel's theory took on a mathematical emphasis. He was able to calculate the diffraction patterns arising from various obstacles and apertures and satisfactorily accounted for rectilinear propagation in homogeneous isotropic media, thus dispelling Newton's main objection to the undulatory theory. When finally apprised of Young's priority to the interference principle, a somewhat disappointed Fresnel nonetheless wrote to Young telling him that he was consoled by finding himself in such good company—the two great men became allies.

Figure 1.5 Augustin Jean Fresnel (1788–1827).

Huygens was aware of the phenomenon of polarization arising in calcite crystals, as was Newton. Indeed, the latter in his *Opticks* stated,

> Every Ray of Light has therefore two opposite Sides....

He further developed this concept of lateral asymmetry even though avoiding any interpretation in terms of the hypothetical nature of light. Yet it was not until 1808 that Étienne Louis Malus (1775–1812) discovered that this two-sidedness of light became apparent upon reflection as well; it was not inherent to crystalline media. Fresnel and Arago then conducted a series of experiments to determine the effect of polarization on interference, but the results were utterly inexplicable within the framework of their longitudinal wave picture—this was a dark hour indeed. For several years Young, Arago, and Fresnel wrestled with the problem until finally Young suggested that the aethereal vibration might be *transverse* as is a wave on a string. The two-sidedness of light was then simply a manifestation of the two orthogonal vibrations of the aether, transverse to the ray direction. Fresnel went on to evolve a mechanistic description of aether oscillations, which led to his now famous formulas for the amplitude of reflected and transmitted light. By 1825 the emission (or corpuscular) theory had only a few tenacious advocates.

The first terrestrial determination of the speed of light was performed by Armand Hippolyte Louis Fizeau (1819–1896) in 1849. His apparatus, consisting of a rotating toothed wheel and a distant mirror (8633 m), was set up in the suburbs of Paris from Suresnes to Montmartre. A pulse of light leaving an opening in the wheel struck the mirror and returned. By adjusting the known rotational speed of the wheel, the returning pulse could be made either to pass through an opening and be seen or to be obstructed by a tooth. Fizeau arrived at a value of the speed of light equal to 315,300 km/s. His colleague Jean Bernard Léon Foucault (1819–1868) was also involved in research on the speed of light. In 1834 Charles Wheatstone (1802–1875) had designed a rotating-mirror arrangement in order to measure the duration of an electric spark. Using this scheme, Arago had proposed to measure the speed of light in dense media but was never able to carry out the experiment. Foucault took up the work, which was later to provide material for his doctoral thesis. On May 6, 1850, he reported to the Academy of Sciences that the speed of light in water was *less* than that in air. This result was, of course, in direct conflict with Newton's formulation of the emission theory and a hard blow to its few remaining devotees.

While all of this was happening in optics, quite independently, the study of electricity and magnetism was also bearing fruit. In 1845 the master experimentalist Michael Faraday (1791–1867) established an interrelationship between electromagnetism and light when he found that the polarization direction of a beam could be altered by a strong magnetic field applied to the medium. James Clerk Maxwell (1831–1879) brilliantly summarized and extended all the empirical knowledge on the subject in a single set of mathematical equations. Beginning with this remarkably succinct and beautifully symmetrical synthesis, he was able to show, purely theoretically, that the electromagnetic field could propagate as a transverse wave in the luminiferous aether. Solving for the speed of the wave, he arrived at an expression in terms of electric and magnetic properties of the medium ($c = 1/\sqrt{\epsilon_0\mu_0}$). Upon substituting known empirically determined values for these quantities, he obtained a numerical result equal to the measured speed of light! The conclusion was inescapable—*light was "an electromagnetic disturbance in the form of waves" propagated through the aether.* Maxwell died at the age of 48, eight years too soon to see the experimental confirmation of his insights and far too soon for physics. Heinrich Rudolf Hertz (1857–1894) verified the existence of long electromagnetic waves by generating and detecting them in an extensive series of experiments published in 1888.

The acceptance of the wave theory of light seemed to necessitate an equal acceptance of the existence of an all-pervading substratum, the luminiferous aether. If there were waves, it seemed obvious that there must be a supporting medium. Quite naturally, a great deal of scientific effort went into determining the physical nature of the aether, yet it would have to possess some

Figure 1.6 James Clerk Maxwell (1831–1879).

rather strange properties. It had to be so tenuous as to allow an apparently unimpeded motion of celestial bodies. At the same time it could support the exceedingly high-frequency ($\sim 10^{15}$ Hz) oscillations of light traveling at 186,000 miles/s. That implied remarkably strong restoring forces within the aethereal substance. The speed at which a wave advances through a medium is dependent upon the characteristics of the disturbed substratum and not upon any motion of the source. This is in contrast to the behavior of a stream of particles whose speed with respect to the source is the essential parameter.

Certain aspects of the nature of aether intrude when studying the optics of moving objects, and it was this area of research, evolving quietly on its own, that ultimately led to the next great turning point. In 1725 James Bradley (1693–1762), then Savilian Professor of

Astronomy at Oxford, attempted to measure the distance to a star by observing its orientation at two different times of the year. The position of the Earth changed as it orbited around the Sun and thereby provided a large base line for triangulation on the star. To his surprise, Bradley found that the "fixed" stars displayed an apparent systematic movement related to the direction of motion of the Earth in orbit and not dependent, as had been anticipated, on the Earth's position in space. This so-called *stellar aberration* is analogous to the well-known falling-raindrop situation. A raindrop, although traveling vertically with respect to an observer at rest on the Earth, will appear to change its incident angle when the observer is in motion. Thus a corpuscular model of light could explain stellar aberration rather handily. Alternatively, the wave theory also offers a satisfactory explanation provided that it is assumed that *the aether remains totally undisturbed as the Earth plows through it.* Incidentally, Bradley, convinced of the correctness of his analysis, used the observed aberration data to arrive at an improved value of *c*, thus confirming Römer's theory of the finite speed of light.

In response to speculation as to whether the Earth's motion through the aether might result in an observable difference between light from terrestrial and extraterrestrial sources, Arago set out to examine the problem experimentally. He found that there were no observable differences. Light behaved just as if the Earth were at rest with respect to the aether. To explain these results, Fresnel suggested in effect that light was partially dragged along as it traversed a transparent medium in motion. Experiments by Fizeau, in which light beams passed down moving columns of water, and by Sir George Biddell Airy (1801–1892), who used a water-filled telescope in 1871 to examine stellar aberration, both seemed to confirm Fresnel's drag hypothesis. Assuming an aether at *absolute rest,* Hendrik Antoon Lorentz (1853–1928) derived a theory that encompassed Fresnel's ideas.

In 1879 in a letter to D. P. Todd of the U.S. Nautical Almanac Office, Maxwell suggested a scheme for measuring the speed at which the solar system moved with respect to the luminiferous aether. The American physicist Albert Abraham Michelson (1852–1931), then a naval instructor, took up the idea. Michelson, at the tender age of 26, had already established a favorable reputation by performing an extremely precise determination of the speed of light. A few years later, he began an experiment to measure the effect of the Earth's motion through the aether. Since the speed of light in aether is constant and the Earth, in turn, presumably moves in relation to the aether (orbital speed of 67,000 miles/h), the speed of light measured with respect to the Earth should be affected by the planet's motion. Michelson's work was begun in Berlin, but because of traffic vibrations, it was moved to Potsdam, and in 1881 he published his findings. There was no detectable motion of the Earth with respect to the aether—the aether was stationary. But the decisiveness of this surprising result was blunted somewhat when Lorentz pointed out an oversight in the calculation. Several years later Michelson, then professor of physics at Case School of Applied Science in Cleveland, Ohio, joined with Edward Williams Morely (1838–1923), a well-known professor of chemistry at Western Reserve, to redo the experiment with considerably greater precision. Amazingly enough, their results, published in 1887, once again were negative:

> It appears from all that precedes reasonably certain that if there be any relative motion between the earth and the luminiferous aether, it must be small; quite small enough entirely to refute Fresnel's explanation of aberration.

Thus, whereas an explanation of stellar aberration within the context of the wave theory required the existence of a relative motion between Earth and aether, the Michelson–Morley experiment refuted that possibility. Moreover, the findings of Fizeau and Airy necessitated the inclusion of a partial drag of light due to motion of the medium.

1.5 TWENTIETH-CENTURY OPTICS

Jules Henri Poincaré (1854–1912) was perhaps the first to grasp the significance of the experimental inability to observe any effects of motion relative to the aether. In 1899 he began to make his views known, and in 1900 he said:

> Our aether, does it really exist? I do not believe that more precise observations could ever reveal anything more than *relative* displacements.

In 1905 Albert Einstein (1879–1955) introduced his *special theory of relativity,* in which he too, quite independently, rejected the aether hypothesis.

> The introduction of a "luminiferous aether" will prove to be superfluous inasmuch as the view here to be developed will not require an "absolutely stationary space."

He further postulated:

> light is always propagated in empty space with a definite velocity *c* which is independent of the state of motion of the emitting body.

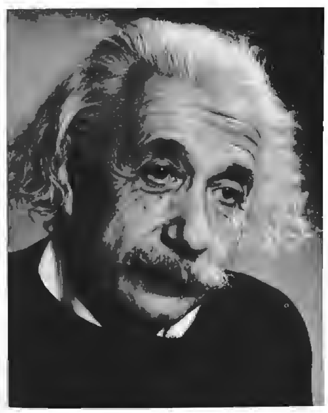


Figure 1.7 Albert Einstein (1879–1955). (Photo by Fred Stein.)

The experiments of Fizeau, Airy, and Michelson–Morley were then explained quite naturally within the framework of Einstein's relativistic kinematics.* Deprived of the aether, physicists simply had to get used to the idea that electromagnetic waves could propagate through free space—there was no alternative. Light was now envisaged as a self-sustaining wave with the conceptual emphasis passing from aether to field. The electromagnetic wave became an entity in itself.

On October 19, 1900, Max Karl Ernst Ludwig Planck (1858–1947) read a paper before the German Physical Society in which he introduced the beginnings of what was to become yet another great revolution in scientific thought—*quantum mechanics,* a theory embracing submicroscopic phenomena. In 1905, building on these ideas, Einstein proposed a new form of corpuscular theory in which he asserted that light consisted of globs or "particles" of energy. Each such quantum of radiant energy or photon,† as it came to be called, had an energy proportional to its frequency ν, i.e., $\mathscr{E} = h\nu$, where h is known as Planck's constant. By the end of the 1920s, through the efforts of Bohr, Born, Heisenberg, Schrödinger, De Broglie, Pauli, Dirac, and others, quantum mechanics had become a well-verified theory. It gradually became evident that the concepts of particle and wave, which in the macroscopic world seem so obviously mutually exclusive, must be merged in the submicroscopic domain. The mental image of an atomic particle (e.g., electrons and neutrons) as a minute localized lump of matter would no longer suffice. Indeed, it was found that these "particles" could generate interference and diffraction patterns in precisely the same way as would light. Thus photons, protons, electrons, neutrons, and so forth—the whole lot—have both particle and wave manifestations. Still, the matter was by no means settled. "Every physicist thinks that he knows what a photon is," wrote Einstein. "I spent my life to find out what a photon is and I still don't know it."

Relativity liberated light from the aether and showed the kinship between mass and energy (via $\mathscr{E} = mc^2$).

* See, for example, *Special Relativity* by French, Chapter 5.

† The word *photon* was coined by G. N. Lewis, *Nature,* December 18, 1926.

What seemed to be two almost antithetical quantities now became interchangeable. Quantum mechanics went on to establish that a particle* of momentum p had an associated wavelength λ, such that p h/λ (whether it had rest mass or not). The neutrino, a neutral particle presumably having zero rest mass, was postulated for theoretical reasons in 1930 by Wolfgang Pauli (1900–1958) and verified experimentally in the 1950s. The easy images of submicroscopic specks of matter became untenable, and the wave–particle dichotomy dissolved into a duality.

Quantum mechanics also treats the manner in which light is absorbed and emitted by atoms. Suppose we cause a gas to glow by heating it or passing an electrical discharge through it. The light emitted is characteristic of the very structure of the atoms constituting the gas. Spectroscopy, which is the branch of optics dealing with spectrum analysis, developed from the research of Newton. William Hyde Wollaston (1766–1828) made the earliest observations of the dark lines in the solar spectrum (1802). Because of the slit-shaped aperture generally used in spectroscopes, the output consisted of narrow colored bands of light, the so-called *spectral lines.* Working independently, Joseph Fraunhofer (1787–1826) greatly extended the subject. After accidentally discovering the double line of sodium, he went on to study sunlight and made the first wavelength determinations using diffraction gratings. Gustav Robert Kirchhoff (1824–1887) and Robert Wilhelm Bunsen (1811–1899), working conjointly at Heidelberg, established that each kind of atom had its own signature in a characteristic array of spectral lines. And in 1913 Niels Henrik David Bohr (1885–1962) set forth a precursory quantum theory of the hydrogen atom, which was nonetheless able to predict the wavelengths of its emission spectrum. The light emitted by an atom is now understood to arise from its outermost electrons. An atom that somehow absorbs energy (e.g., through collisions) changes from its usual configuration, known as the ground state, to what's called an excited state. After some finite time, it relaxes back to the ground state, the electrons returning to their original configuration with respect to the nucleus, giving up the excess energy often in the form of light. The process is the domain of modern quantum theory, which describes the most minute details with incredible precision and beauty.

The flourishing of applied optics in the second half of the twentieth century represents a renaissance in itself. In the 1950s several workers began to inculcate optics with the mathematical techniques and insights of communications theory. Just as the idea of momentum provides another dimension in which to visualize aspects of mechanics, the concept of spatial frequency offers a rich new way of appreciating a broad range of optical phenomeoa. Bound together by the mathematical formalism of Fourier analysis, the outgrowths of this contemporary emphasis have been far-reaching. Of particular interest are the theory of image formation and evaluation, the transfer functions, and the idea of spatial filtering.

The advent of the high-speed digital computer brought with it a vast improvement in the design of complex optical systems. Aspherical lens elements took on renewed practical significance, and the diffraction-limited system with an appreciable field of view became a reality. The technique of ion bombardment polishing, in which one atom at a time is chipped away, was introduced to meet the need for extreme precision in the preparation of optical elements. The use of single and multilayer thin-film coatings (reflecting, antireflecting, etc.) became commonplace. Fiberoptics evolved into a practical tool, and thin-film light guides were studied. A great deal of attention was paid to the infrared end of the spectrum (surveillance systems, missile guidance, etc.), and this in turn stimulated the development of infrared materials. Plastics began to be used in optics (lens elements, replica gratings, fibers, aspherics, etc.). A new class of partially vitrified glass ceramics with exceedingly low thermal expansion was developed. A resurgence in the construction of astronomical observatories (both terrestrial and extraterrestrial) operating across the whole spectrum was well under way by the end of the 1960s and vigorously sustained in the 1980s.

The first laser was built in 1960, and within a decade laser beams spanned the range from infrared to ultraviolet. The availability of high-power coherent sources led to the discovery of a number of new optical effects

* Perhaps it might help if we just called them all *wavicles.*

Figure 1.8 These photos, which were made using electronic amplification techniques, are a compelling illustration of the granularity displayed by light in its interaction with matter. Under exceedingly faint illumination the pattern (each spot corresponding to one photon) seems almost random, but as the light level increases the quantal character of the process gradually becomes obscured. (See *Advances in Biological and Medical Physics* V, 1957, 211–242.) (Photos courtesy Radio Corporation of America.)

(harmonic generation, frequency mixing, etc.) and thence to a panorama of marvelous new devices. The technology needed to produce a practicable optical communications system was evolving fast. The sophisticated use of crystals in devices such as second-harmonic generators, electro-optic and acousto-optic modulators, and the like spurred a great deal of contemporary research in crystal optics. The wavefront reconstruction technique known as holography, which produces magnificent three-dimensional images, was found to have numerous additional applications (nondestructive testing, data storage, etc.).

The military orientation of much of the developmental work in the 1960s continued in the 1970s and the 1980s with added vigor. That technological interest in optics ranges across the spectrum from "smart bombs" and spy satellites to "death rays" and infrared gadgets that see in the dark. But economic cousiderations coupled with the need to improve the quality of life have brought products of the discipline into the consumer marketplace as never before. Today lasers are in use everywhere: reading videodiscs in living rooms, cutting steel in factories, setting type in newspapers, scanning labels in supermarkets, and performing surgery in hospitals. Millions of optical display systems on clocks and calculators and computers are blinking all around the world. The almost exclusive use, for the last one hundred years, of electrical signals to handle and transmit data is now rapidly giving way to more efficient optical techniques. A far-reaching revolution in the methods of processing and communicating information is quietly taking place, a revolution that will change our lives immensely in the years ahead.

Profound insights are slow in coming. What few we have took over three thousand years to glean, even though the pace is ever quickening. It is marvelous indeed to watch the answer subtly change while the question immutably remains—*what is light?**

* For more reading on the history of optics, see F. Cajori, *A History of Physics,* and V. Ronchi, *The Nature of Light.* Excerpts from a number of original papers can conveniently be found in W. F. Magie, *A Source Book in Physics,* and in M. H. Shamos, *Great Experiments in Physics.*

2 THE MATHEMATICS OF WAVE MOTION

There are a great many, seemingly unrelated, physical processes that can be described in terms of the mathematics of wave motion. In this respect there are fundamental similarities among a pulse traveling along a stretched string (Fig. 2.1), a surface tension ripple in a cup of tea, and the light reaching us from some remote point in the universe. This chapter will develop some of the mathematical techniques needed to treat wave phenomena in general. We will begin with some fairly simple ideas concerning the propagation of disturbances and from these arrive at the three-dimensional differential wave equation. Throughout the study of optics one utilizes plane, spherical, and cylindrical waves. Accordingly, we'll develop their mathematical representations, showing them to be solutions of the differential wave equation. This chapter will be a completely classical treatment; even so, it can be shown, although we will not do so, that our results do indeed obey the requirements of special relativity.

2.1 ONE-DIMENSIONAL WAVES

The essential aspect of a propagating wave is that it is a self-sustaining disturbance of the medium through which it travels. Envision some such disturbance ψ moving in the positive x-direction with a constant speed v. The specific nature of the disturbance is at the moment unimportant. It might be the vertical displacement of the string in Fig. 2.1 or the magnitude of an electric or magnetic field associated with an electromagnetic wave (or even the quantum-mechanical probability amplitude of a matter wave).

Since the disturbance is moving, it must be a function of both position and time and can therefore be written as

$$\psi = f(x, t). \qquad (2.1)$$

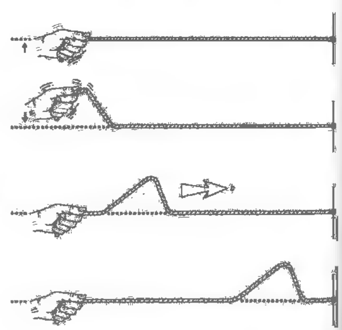


Figure 2.1 A wave on a string.

The shape of the disturbance at any instant, say $t = 0$, can be found by holding time constant at that value. In this case,

$$\psi(x, t)|_{t=0} = f(x, 0) = f(x) \qquad (2.2)$$

represents the shape or **profile** of the wave at that time. For example, if $f(x) = e^{-ax^2}$, where a is a constant, the profile has the shape of a bell, i.e., it is a Gaussian functiou. The process is analogous to taking a "photograph" of the pulse as it travels by. For the moment we will limit ourselves to a wave that *does not change its shape* as it progresses through space. Figure 2.2 is a "double exposure" of such a disturbance taken at the beginning and end of a time interval t. The pulse has moved along the x-axis a distance vt, but in all other respects it remains unaltered. We now introduce a coordinate system S', which travels along with the pulse at the speed v. In this system ψ is no longer a function of time, and as we move along with S' we see a stationary constant profile with the same functional form as Eq. (2.2). Here, the coordinate is x' rather than x, so that

$$\psi = f(x'). \qquad (2.3)$$

The disturbance looks the same at any value of t in S' as it did at $t = 0$ in S when S and S' had a common origin. It follows from Fig. 2.2 that

$$x' = x - vt, \qquad (2.4)$$

so that ψ can be written in terms of the variables associated with the stationary S system as

$$\psi(x, t) = f(x - vt). \qquad (2.5)$$

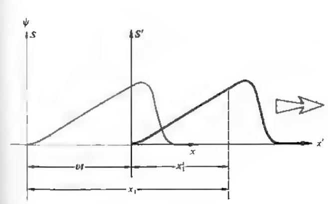


Figure 2.2 Moving reference frame.

This then represents the most general form of the one-dimensional **wave function.** To be more specific, *we have only to choose a shape* (2.2) *and then substitute* $(x - vt)$ *for* x *in* $f(x)$. *The resulting expression describes a moving wave having the desired profile.* Thus, $\psi(x, t) = e^{-a(x-vt)^2}$ is a bell-shaped wave traveling in the positive x-direction with a speed v. If we check the form of Eq. (2.5) by examining ψ after an increase in time of Δt and a corresponding increase of $v\,\Delta t$ in x, we find

$$f[(x + v\,\Delta t) - v(t + \Delta t)] = f(x - vt)$$

and the profile is unaltered.

Similarly, if the wave were traveling in the negative x-direction, i.e., to the left, Eq. (2.5) would become

$$\psi = f(x + vt), \quad \text{with} \quad v > 0. \qquad (2.6)$$

We may conclude therefore that, regardless of the shape of the disturbance, the variables x and t must appear in the function as a unit, i.e., as a single variable in the form $(x \mp vt)$. Equation (2.5) is often expressed equivalently as some function of $(t - x/v)$, since

$$f(x - vt) = F\left(-\frac{x - vt}{v}\right) = F(t - x/v). \qquad (2.7)$$

Incidentally, the pulse shown in Fig. 2.1 and the disturbance described by Eq. (2.5) are spoken of as *one-dimensional* because the waves sweep over points lying on a line—it takes only one space variable to specify them. Don't be confused by the fact that in this particular case the rope happens to rise up into a second dimension. In contrast, a two-dimensional wave propagates out across a surface, like the ripples on a pond, and can be described by two space variables.

We wish to use the information derived so far to develop the general form of the one-dimensional differential wave equation. To that end, take the partial derivative of $\psi(x, t)$ with respect to x, holding t constant. Using $x' = x - vt$, we have

$$\frac{\partial \psi}{\partial x} = \frac{\partial f}{\partial x'}\frac{\partial x'}{\partial x} = \frac{\partial f}{\partial x'}, \quad \text{since} \quad \frac{\partial x'}{\partial x} = 1. \qquad (2.8)$$

If we hold x constant, the partial derivative with respect to time is

$$\frac{\partial\psi}{\partial t} = \frac{\partial f}{\partial x'}\frac{\partial x'}{\partial t} = \mp v\frac{\partial f}{\partial x'}. \qquad (2.9)$$

Combining Eqs. (2.8) and (2.9) yields

$$\frac{\partial\psi}{\partial t} = \mp v\frac{\partial\psi}{\partial x}. \qquad (2.10)$$

This says that the rate of change of ψ with t and with x are equal, to within a multiplicative constant, as shown in Fig. 2.3. Knowing beforehand that we'll need two constants to specify a wave, we can anticipate a second-order wave equation. The second partial derivatives of Eqs. (2.8) and (2.9) yield

$$\frac{\partial^2\psi}{\partial x^2} = \frac{\partial^2 f}{\partial x'^2}$$

and

$$\frac{\partial^2\psi}{\partial t^2} = \frac{\partial}{\partial t}\left(\mp v\frac{\partial f}{\partial x'}\right) = \mp v\frac{\partial}{\partial x'}\left(\frac{\partial f}{\partial t}\right).$$

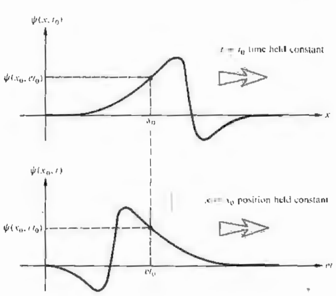


Figure 2.3 Variation of ψ with x and t.

Since

$$\frac{\partial\psi}{\partial t} = \frac{\partial f}{\partial t},$$

it follows, using Eq. (2.9), that

$$\frac{\partial^2\psi}{\partial t^2} = v^2\frac{\partial^2 f}{\partial x'^2}.$$

Combining these equations, we obtain

$$\frac{\partial^2\psi}{\partial x^2} = \frac{1}{v^2}\frac{\partial^2\psi}{\partial t^2}, \qquad (2.11)$$

which is the **one-dimensional differential wave equation**. It is apparent from the form of Eq. (2.11) that if two different wave functions ψ_1 and ψ_2 are each separate solutions, then $(\psi_1 + \psi_2)$ is also a solution.* Accordingly, the wave equation is most generally satisfied by a wave function having the form

$$\psi = C_1 f(x - vt) + C_2 g(x + vt), \qquad (2.12)$$

where C_1 and C_2 are constants and the functions are twice differentiable. This is clearly a sum of two waves traveling in opposite directions along the x-axis with the same velocity but not necessarily the same profile. The superposition principle is inherent in this equation, and we will come back to it in Chapter 7.

We began with a special case, an important one to be sure, but a special case nonetheless—most waves do not propagate with a constant profile. Still, that simple assumption has led us to the central formulation, the differential wave equation. If a function is a solution of that equation, it represents a wave. As we've seen, it will at the same time be a function of $(x \mp vt)$—specifically, one that is twice differentiable with respect to both x and t.

* Since both ψ_1 and ψ_2 are solutions

$$\frac{\partial^2\psi_1}{\partial x^2} = \frac{1}{v^2}\frac{\partial^2\psi_1}{\partial t^2} \quad \text{and} \quad \frac{\partial^2\psi_2}{\partial x^2} = \frac{1}{v^2}\frac{\partial^2\psi_2}{\partial t^2}.$$

Adding these, we get

$$\frac{\partial^2\psi_1}{\partial x^2} + \frac{\partial^2\psi_2}{\partial x^2} = \frac{\partial^2}{\partial x^2}(\psi_1 + \psi_2) = \frac{1}{v^2}\left[\frac{\partial^2\psi_1}{\partial t^2} + \frac{\partial^2\psi_2}{\partial t^2}\right] = \frac{1}{v^2}\frac{\partial^2}{\partial t^2}(\psi_1 + \psi_2),$$

so that $(\psi_1 + \psi_2)$ is also a solution of Eq. (2.11).

Figure 2.4 An ultrashort pulse of green light from a neodymium-doped glass laser. The pulse passed through a water cell whose wall is marked in millimeters. During the 10-picosecond exposure the pulse moved about 2.2 mm. (Photo courtesy Bell Laboratories.)

2.2 HARMONIC WAVES

Let's now examine the simplest wave form for which the profile is a sine or cosine curve. These are variously known as sinusoidal waves, simple harmonic waves, or more succinctly as **harmonic waves.** We shall see in Chapter 7 that any wave shape can be synthesized by a superposition of harmonic waves, and they therefore take on a special significance.

Choose as the profile the simple function

$$\psi(x, t)|_{t=0} = \psi(x) = A \sin kx = f(x), \qquad (2.13)$$

where k is a positive constant known as the **propagation number.** It's necessary to introduce the constant k simply because we cannot take the sine of a quantity that has physical units. Accordingly, kx is properly in radians. The sine varies from +1 to −1 so that the maximum value of $\psi(x)$ is A. This maximum disturbance is known as the **amplitude** of the wave (Fig. 2.5). To transform Eq. (2.13) into a *progressive wave* traveling at speed v in the positive x-direction, we need merely replace x by $(x - vt)$, in which case

$$\psi(x, t) = A \sin k(x - vt) = f(x - vt). \qquad (2.14)$$

This is clearly (see Problem 2.8) a solution of the differential wave equation (2.11). Holding either x or t fixed results in a sinusoidal disturbance, so the wave is periodic in both space and time. The **spatial period** is known as the **wavelength** and is denoted by λ, as shown in Fig. 2.5. The unit of λ is the nanometer, where $1\ \text{nm} = 10^{-9}$ m; although the micron ($1\ \mu\text{m} = 10^{-6}$ m)

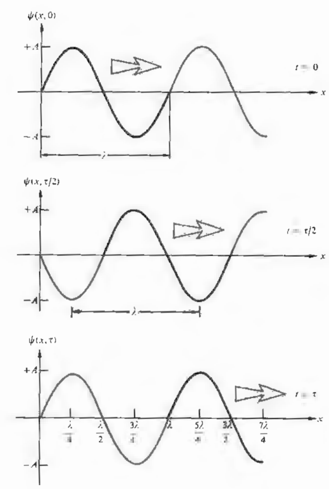


Figure 2.5 A progressive wave at three different times.

is often used, and the older **angstrom** (1 Å = 10^{-10} m) can still be found in the literature. An increase or decrease in x by the amount λ should leave ψ unaltered, that is,

$$\psi(x, t) = \psi(x \pm \lambda, t). \qquad (2.15)$$

In the case of a harmonic wave, this is equivalent to altering the argument of the sine function by $\pm 2\pi$. Therefore,

$$\sin k(x - vt) = \sin k[(x \pm \lambda) - vt] = \sin [k(x - vt) \pm 2\pi]$$

and so

$$|k\lambda| = 2\pi,$$

or, since both k and λ are positive numbers,

$$k = 2\pi/\lambda. \qquad (2.16)$$

In a completely analogous fashion, we can examine the **temporal period,** τ. This is the amount of time it takes for one complete wave to pass a stationary observer. In this case, it is the repetitive behavior of the wave in time that is of interest, so that

$$\psi(x, t) = \psi(x, t \pm \tau) \qquad (2.17)$$

and

$$\sin k(x - vt) = \sin k[x - v(t \pm \tau)]$$
$$= \sin [k(x - vt) \pm 2\pi].$$

Therefore,

$$|kv\tau| = 2\pi.$$

But these are all positive quantities; hence

$$kv\tau = 2\pi \qquad (2.18)$$

or

$$\frac{2\pi}{\lambda} v\tau = 2\pi,$$

from which it follows that

$$\tau = \frac{\lambda}{v}. \qquad (2.19)$$

The period is the number of units of time per wave (Fig. 2.6), the inverse of which is the **frequency** ν, or

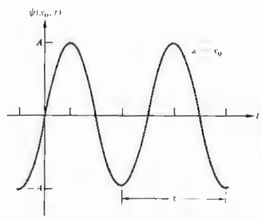


Figure 2.6 A harmonic wave.

the number of waves per unit of time. Thus,

$$\nu = \frac{1}{\tau} \quad \text{(cycles/s or Hertz)},$$

and Eq. (2.19) becomes

$$v = \nu\lambda \quad \text{(m/s)}. \qquad (2.20)$$

There are two other quantities that are often used in the literature of wave motion and these are the *angular frequency*

$$\omega \equiv \frac{2\pi}{\tau} \quad \text{(radians/s)} \qquad (2.21)$$

and the **wave number**

$$\varkappa \equiv \frac{1}{\lambda} \quad (\text{m}^{-1}). \qquad (2.22)$$

The wavelength, period, frequency, angular frequency, wave number, and propagation number all describe aspects of the repetitive nature of a wave in space and time. These concepts are equally well applied to waves that are not harmonic, as long as each wave profile is made up of a regularly repeating pattern (Fig. 2.7). We have thus far defined a number of quantities that characterize various aspects of wave motion. There exist, accordingly, a number of equivalent formulations of

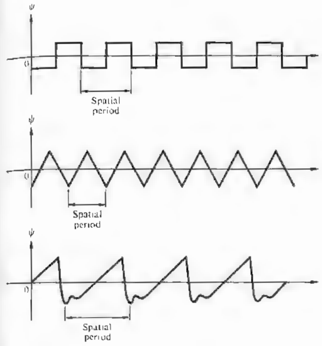


Figure 2.7 Anharmonic periodic waves.

the progressive harmonic wave. Some of the most common of these are

$$\psi = A \sin k(x \mp vt) \qquad [2.14]$$

$$\psi = A \sin 2\pi\left(\frac{x}{\lambda} \mp \frac{t}{\tau}\right) \qquad (2.23)$$

$$\psi = A \sin 2\pi(\varkappa x \mp \nu t) \qquad (2.24)$$

$$\psi = A \sin (kx \mp \omega t) \qquad (2.25)$$

$$\psi = A \sin 2\pi\nu\left(\frac{x}{v} \mp t\right) \qquad (2.26)$$

Of these, Eqs. (2.14) and (2.25) will be encountered most frequently. It should be noted that these waves are all of infinite extent, i.e., for any fixed value of t, there is no mathematical limitation on x, which varies from $-\infty$ to $+\infty$. Each wave has a single constant frequency and is therefore said to be *monochromatic.*

2.3 PHASE AND PHASE VELOCITY

Examine any one of the harmonic wave functions, such as

$$\psi(x, t) = A \sin (kx - \omega t).$$

The entire argument of the sine function is known as the **phase** φ of the wave, so that

$$\varphi = (kx - \omega t). \qquad (2.27)$$

At $t = x = 0$,

$$\psi(x, t)\big|_{\substack{x=0\\t=0}} = \psi(0, 0) = 0,$$

which is certainly a special case. More generally, we can write

$$\psi(x, t) = A \sin (kx - \omega t + \varepsilon), \qquad (2.28)$$

where ε is the **initial phase** or *epoch angle.* To get a sense of the physical meaning of ε, imagine that we wish to produce a progressive harmonic wave on a stretched string, as in Fig. 2.8. In order to generate harmonic waves, the hand holding the string would have to move such that its vertical displacement y was proportional to the negative of its acceleration, that is, in simple harmonic motion (see Problem 2.9). But at $t = 0$ and $x = 0$, the hand certainly need not be on the x-axis about to move downward, as in Fig. 2.8. It could, of course, begin its motion on an upward swing, in which case $\varepsilon = \pi$, as indicated in Fig. 2.9. In this latter case,

$$\psi(x, t) = y(x, t) = A \sin (kx - \omega t + \pi),$$

which is equivalent to

$$\psi(x, t) = A \sin (\omega t - kx)$$

or

$$\psi(x, t) = A \cos\left(\omega t - kx - \frac{\pi}{2}\right).$$

The initial phase angle is then just the constant contribution to the phase arising at the generator and is independent of how far in space, or how long in time, the wave has traveled.

The phase of a disturbance such as $\psi(x, t)$ given by Eq. (2.28) is

$$\varphi(x, t) = (kx - \omega t + \varepsilon) \tag{2.29}$$

and is obviously a function of x and t. In fact, the partial derivative of φ with respect to t, holding x constant, is the *rate of change of phase with time*, or

$$\left|\left(\frac{\partial\varphi}{\partial t}\right)_x\right| = \omega. \tag{2.30}$$

Similarly, the *rate of change of phase with distance*, holding t constant, is

$$\left|\left(\frac{\partial\varphi}{\partial x}\right)_t\right| = k. \tag{2.31}$$

These two expressions should bring to mind an equation from the theory of partial derivatives, one used quite frequently in thermodynamics, namely,

$$\left(\frac{\partial x}{\partial t}\right)_\varphi = \frac{-(\partial\varphi/\partial t)_x}{(\partial\varphi/\partial x)_t}. \tag{2.32}$$

The term on the left represents the velocity of propagation of *the condition of constant phase*. Return for a moment to Fig. 2.9 and choose any point on the profile, for example, the crest of the wave. As the wave moves through space, the displacement y of the point remains constant. Since the only variable in the harmonic wave function is the phase, it too must be constant. That is, the phase is fixed at such a value as to yield the constant y corresponding to the chosen point. The point moves along with the profile at the speed v and so too does the condition of constant phase.

Taking the appropriate partial derivatives of φ as given, for example by Eq. (2.29) and substituting them into Eq. (2.32), we get

$$\left(\frac{\partial x}{\partial t}\right)_\varphi = \pm\frac{\omega}{k} = \pm v. \tag{2.33}$$

This is the *speed* at which the profile moves and is known commonly as the *wave velocity* or, more specifically, as the phase velocity. The phase velocity carries a positive sign when the wave moves in the direction of increasing x and a negative one in the direction of decreasing x. This is consistent with our development of v as the magnitude of the wave velocity.

Consider the idea of the propagation of constant phase and how it relates to any one of the harmonic wave equations, say

$$\psi = A \sin k(x \mp vt)$$

with

$$\varphi = k(x - vt) = \text{constant};$$

as t increases, x must increase. Even if $x < 0$ so that $\varphi < 0$, x must increase (i.e., become less negative). Here, then, the condition of constant phase moves in the increasing x-direction. For

$$\varphi = k(x + vt) = \text{constant},$$

as t increases x can be positive and decreasing or negative and becoming more negative. In either case, the constant-phase condition moves in the decreasing x-direction.

Figure 2.10 depicts a source producing hypothetical two-dimensional waves on the surface of a liquid. The essentially sinusoidal nature of the disturbance, as the medium rises and falls, is evident in the diagram. But there is another useful way to envision what's happening. *The curves connecting all the points with a given phase form a set of concentric circles.* Furthermore, given that A is everywhere constant at any one distance from the source, if φ is constant over a circle, ψ too must be constant over that circle. In other words, all the corresponding peaks and troughs fall on circles and we speak of these as *circular waves*.

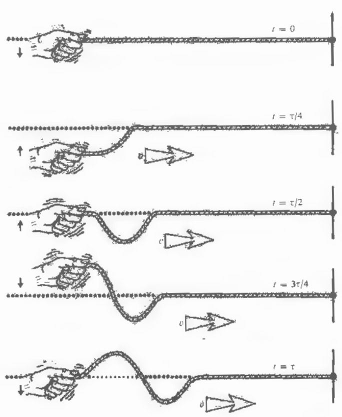


Figure 2.8 With $\varepsilon = 0$ note that at $x = 0$ and $t = \tau/4 = \pi/2\omega$, $y = A \sin(-\pi/2) = -A$.

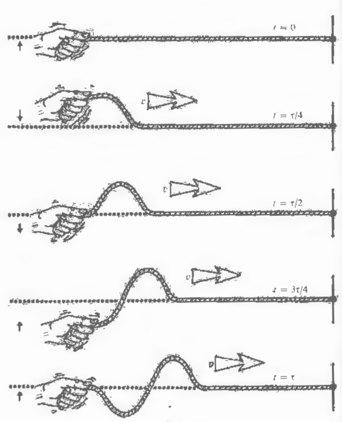


Figure 2.9 With $\varepsilon = \pi$ note that at $x = 0$ and $t = \tau/4$, $y = A \sin(\pi/2) = A$.

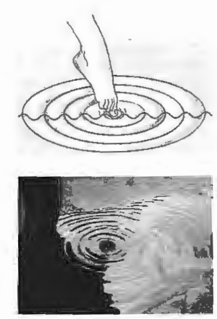


Figure 2.10 Idealized circular waves. (Photo by E.H.)

2.4 THE COMPLEX REPRESENTATION

As we develop the analysis of wave phenomena, it will become clear that the sine and cosine functions that describe harmonic waves are somewhat awkward for our purposes. As the expressions being formulated become more involved, the trigonometric manipulations required to cope with them become even more unattractive. The complex-number representation of waves offers an alternative description that is mathematically simpler to use. In fact, the complex exponential form of the wave equation is used extensively in both classical and quantum mechanics, as well as in optics.

The complex number z has the form

$$z = x + iy, \tag{2.34}$$

where $i = \sqrt{-1}$. The real and imaginary parts of z are respectively x and y, where both x and y are themselves real numbers. This is illustrated graphically in the Argand diagram in Fig. 2.11. In terms of polar coordinates (r, θ), we have

$$x = r\cos\theta, \qquad y = r\sin\theta$$

and

$$z = x + iy = r(\cos\theta + i\sin\theta).$$

The *Euler* formula*

$$e^{i\theta} = \cos\theta + i\sin\theta$$

allows us to write

$$z = re^{i\theta} = r\cos\theta + ir\sin\theta,$$

where r is the *magnitude* of z, and θ is the *phase angle* of z, in radians. The magnitude is often denoted by $|z|$ and referred to as the *modulus* or *absolute value* of the complex number. The *complex conjugate*, indicated by an asterisk, is found by replacing i wherever it appears, with $-i$, so that

$$z^* = (x + iy)^* = (x - iy)$$

$$z^* = r(\cos\theta - i\sin\theta)$$

and

$$z^* = re^{-i\theta}.$$

The operations of addition and subtraction are quite straightforward:

$$z_1 \pm z_2 = (x_1 + iy_1) \pm (x_2 + iy_2)$$

and therefore

$$z_1 \pm z_2 = (x_1 \pm x_2) + i(y_1 \pm y_2).$$

Notice that this process is very much like the component addition of vectors.

* If you have any doubts about this identity, take the differential of $z = \cos\theta + i\sin\theta$, where $r = 1$. This yields $dz = iz\,d\theta$, and integration gives $z = \exp(i\theta)$.

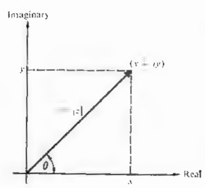


Figure 2.11 Argand diagram.

Multiplication and division are most simply expressed in polar form

$$z_1z_2 = r_1r_2e^{i(\theta_1+\theta_2)}$$

and

$$\frac{z_1}{z_2} = \frac{r_1}{r_2}e^{i(\theta_1-\theta_2)}.$$

A number of facts that will be useful in future calculations are well worth mentioning at this point. It follows readily from the ordinary trigonometric addition formulas that

$$e^{z_1+z_2} = e^{z_1}e^{z_2},$$

whence, if $z_1 = x$ and $z_2 = iy$,

$$e^z = e^{x+iy} = e^xe^{iy}.$$

The modulus of a complex quantity is given by

$$|z| = (zz^*)^{1/2},$$

so that

$$|e^z| = e^x.$$

Inasmuch as $\cos 2\pi = 1$ and $\sin 2\pi = 0$,

$$e^{i2\pi} = 1;$$

similarly,

$$e^{i\pi} = e^{-i\pi} = -1 \quad \text{and} \quad e^{\pm i\pi/2} = \pm i.$$

The function e^z is periodic, that is, it repeats itself every $i2\pi$:

$$e^{z+i2\pi} = e^ze^{i2\pi} = e^z.$$

Any complex number can be represented as the sum of a real part Re (z) and an imaginary part Im (z)

$$z = \text{Re}(z) + i\,\text{Im}(z),$$

such that

$$\text{Re}(z) = \tfrac{1}{2}(z + z^*) \quad \text{and} \quad \text{Im}(z) = \frac{1}{2i}(z - z^*).$$

From the polar form where

$$\text{Re}(z) = r\cos\theta \quad \text{and} \quad \text{Im}(z) = r\sin\theta,$$

it is clear that either part could be chosen to describe a harmonic wave. It is customary, however, to choose the real part, in which case a harmonic wave is written as

$$\psi(x, t) = \text{Re}\,[Ae^{i(\omega t - kx + \varepsilon)}], \tag{2.35}$$

which is, of course, equivalent to

$$\psi(x, t) = A\cos(\omega t - kx + \varepsilon).$$

Henceforth, wherever it's convenient, we shall write the wave function as

$$\psi(x, t) = Ae^{i(\omega t - kx + \varepsilon)} = Ae^{i\varphi} \tag{2.36}$$

and utilize this complex form in the required computations. This is done to take advantage of the ease with which complex exponentials can be manipulated. Only after arriving at a final result, and then only if we want to represent the actual wave, must we take the real part. It has, accordingly, become quite common to write $\psi(x, t)$, as in Eq. (2.36), where it is understood that the actual wave is the real part.

2.5 PLANE WAVES

The plane wave is perhaps the simplest example of a three-dimensional wave. It exists at a given time, when all the surfaces upon which a disturbance has constant phase form a set of planes, each generally perpendicular to the propagation direction. There are quite practical

reasons for studying this sort of disturbance, one of which is that by using optical devices, we can readily produce light resembling plane waves.

The mathematical expression for a plane that is perpendicular to a given vector **k** and that passes through some point (x_0, y_0, z_0) is rather easy to derive (Fig. 2.12). The position vector, in terms of its components in Cartesian coordinates, is

$$\mathbf{r} = [x, y, z].$$

It begins at some arbitrary origin O and ends at the point (x, y, z), which can, for the moment, be anywhere in space. By setting

$$(\mathbf{r} - \mathbf{r}_0) \cdot \mathbf{k} = 0, \tag{2.37}$$

we force the vector $(\mathbf{r} - \mathbf{r}_0)$ to sweep out a plane perpendicular to **k**, as its endpoint (x, y, z) takes on all allowed values. With

$$\mathbf{k} \equiv [k_x, k_y, k_z] \tag{2.38}$$

Eq. (2.37) can be expressed in the form

$$k_x(x - x_0) + k_y(y - y_0) + k_z(z - z_0) = 0 \tag{2.39}$$

or as

$$k_xx + k_yy + k_zz = a. \tag{2.40}$$

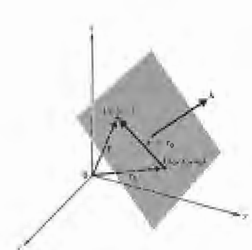


Figure 2.12 A plane wave moving in the **k**-direction.

where

$$a = k_x x_0 + k_y y_0 + k_z z_0 = \text{constant}. \qquad (2.41)$$

The most concise form of the equation of a plane perpendicular to **k** is then just

$$\mathbf{k} \cdot \mathbf{r} = \text{constant} = a. \qquad (2.42)$$

The plane is the locus of all points whose position vectors each have the same projection onto the **k**-direction.

We can now construct a set of planes over which $\psi(\mathbf{r})$ varies in space sinusoidally, namely,

$$\psi(\mathbf{r}) = A \sin (\mathbf{k} \cdot \mathbf{r}) \qquad (2.43)$$

$$\psi(\mathbf{r}) = A \cos (\mathbf{k} \cdot \mathbf{r}) \qquad (2.44)$$

or

$$\psi(\mathbf{r}) = A e^{i\mathbf{k}\cdot\mathbf{r}}. \qquad (2.45)$$

For each of these expressions $\psi(\mathbf{r})$ is constant over every plane defined by $\mathbf{k} \cdot \mathbf{r} = $ constant. Since we are dealing

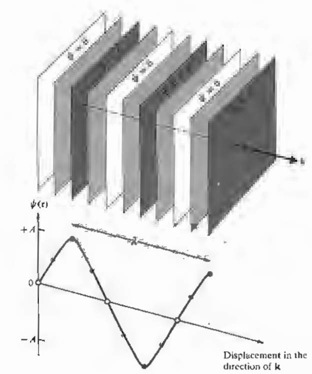


Figure 2.13 Wavefronts for a harmonic plane wave.

with harmonic functions, they should repeat themselves in space after a displacement of λ in the direction of **k**. Figure 2.13 is a rather humble representation of this kind of expression. We have drawn only a few of the infinite number of planes, each having a different $\psi(\mathbf{r})$. The planes should also have been drawn with an infinite spatial extent, since no limits were put on **r**. The disturbance clearly occupies all of space.

The spatially repetitive nature of these harmonic functions can be expressed by

$$\psi(\mathbf{r}) = \psi\left(\mathbf{r} + \frac{\lambda \mathbf{k}}{k}\right), \qquad (2.46)$$

where k is the magnitude of **k** and $\mathbf{k}/k$ is a unit vector parallel to it (Fig. 2.14). In the exponential form, this is equivalent to

$$A e^{i\mathbf{k}\cdot\mathbf{r}} = A e^{i\mathbf{k}\cdot(\mathbf{r}+\lambda\mathbf{k}/k)} = A e^{i\mathbf{k}\cdot\mathbf{r}} e^{i\lambda k}.$$

For this to be true, we must have

$$e^{i\lambda k} = 1 = e^{i2\pi};$$

therefore,

$$\lambda k = 2\pi$$

and

$$k = \frac{2\pi}{\lambda}.$$

The vector **k**, whose magnitude is the *propagation number* k (already introduced), is called the **propagation vector**.

At any fixed point in space where **r** is constant, the phase is constant and so too, is $\psi(\mathbf{r})$, in short the planes are motionless. To get things moving, $\psi(\mathbf{r})$ must be made to vary in time, something we can accomplish by introducing the time dependence in an analogous fashion to that of the one-dimensional wave. Here then

$$\psi(\mathbf{r}, t) = A e^{i(\mathbf{k}\cdot\mathbf{r} \mp \omega t)} \qquad (2.47)$$

with A, ω, and k constant. As this disturbance travels along in the **k**-direction we can assign a phase corresponding to it at each point in space and time. At any given time, *the surfaces joining all points of equal phase are known as* **wavefronts** or *wave surfaces*. Note that the wave function will have a constant value over the wavefront only if the amplitude A has a fixed value at every point on the wavefront. In general, A is a function of **r** and may not be constant over all space or even over a

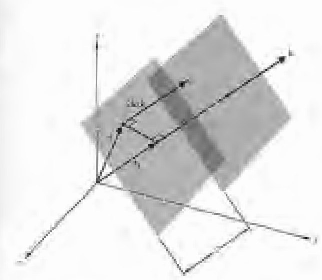


Figure 2.14 Plane waves.

wavefront. In the latter case, the wave is said to be *inhomogeneous*, but we will not be concerned with this sort of disturbance until later, when we consider laser-beams and total internal reflection.

The phase velocity of a plane wave given by Eq. (2.47) is equivalent to the propagation velocity of the wavefront. In Fig. 2.14, the scalar component of **r** in the direction of **k** is r_k. The disturbance on a wavefront is constant, so that after a time dt, if the front moves along **k** a distance dr_k, we must have

$$\psi(\mathbf{r}, t) = \psi(r_k + dr_k, t + dt) = \psi(r_k, t). \qquad (2.48)$$

In exponential form, this is

$$A e^{i(\mathbf{k}\cdot\mathbf{r} \mp \omega t)} = A e^{i(kr_k + k\,dr_k \mp \omega t \mp \omega\,dt)} = A e^{i(kr_k \mp \omega t)};$$

therefore,

$$k\,dr_k = \pm\,\omega\,dt,$$

and the magnitude of the wave velocity, dr_k/dt, is

$$\frac{dr_k}{dt} = \pm\frac{\omega}{k} = \pm v. \qquad (2.49)$$

We could have anticipated this result by rotating the coordinate system in Fig. 2.14 so that **k** was parallel to the x-axis. For that orientation

$$\psi(\mathbf{r}, t) = A e^{i(kx \mp \omega t)},$$

since $\mathbf{k} \cdot \mathbf{r} = kr_k = kx$. The wave has thereby been effectively reduced to the one-dimensional disturbance already discussed in Section 2.3.

The plane harmonic wave is often written in Cartesian coordinates as

$$\psi(x, y, z, t) = A e^{i(k_x x + k_y y + k_z z \mp \omega t)} \qquad (2.50)$$

or

$$\psi(x, y, z, t) = A e^{i[k(\alpha x + \beta y + \gamma z) \mp \omega t]}, \qquad (2.51)$$

where α, β, and γ are the direction cosines of **k** (see Problem 2.19). In terms of its components, the magnitude of the propagation vector is given by

$$|\mathbf{k}| = k = (k_x^2 + k_y^2 + k_z^2)^{1/2} \qquad (2.52)$$

and of course

$$\alpha^2 + \beta^2 + \gamma^2 = 1. \qquad (2.53)$$

We have examined plane waves with a particular emphasis on harmonic functions. The special significance of these waves is twofold: first, physically, sinusoidal waves can be generated relatively simply by using some form of harmonic oscillator; second, any three-dimensional wave can be expressed as a combination of plane waves, each having a distinct amplitude and propagation direction.

We can certainly imagine a series of plane waves like those in Fig. 2.13 where the disturbance varies in some fashion other than harmonically. It will be seen in the next section that harmonic plane waves are, indeed, a special case of a more general plane-wave solution.

2.6 THE THREE-DIMENSIONAL DIFFERENTIAL WAVE EQUATION

Of all the three-dimensional waves, only the plane wave (harmonic or not) moves through space with an unchanging profile. Clearly, then, the idea of a wave being the propagation of a disturbance whose profile is *unaltered* is somewhat lacking. This difficulty can be overcome by defining a wave as any solution of the differential wave equation. Obviously, what we need now is a three-dimensional wave equation. This should be rather easy to obtain, since we can guess at its form by generalizing from the one-dimensional expression (2.11). In Cartesian coordinates, the position variables x, y, and z must certainly appear symmetrically* in the three-dimensional equation, a fact to be kept in mind. The wave function $\psi(x, y, z, t)$ given by Eq. (2.51) is a particular solution of the differential equation we are looking for. In analogy with the derivation of Eq. (2.11), we compute the following partial derivatives from Eq. (2.51)

$$\frac{\partial^2 \psi}{\partial x^2} = -\alpha^2 k^2 \psi \tag{2.54}$$

$$\frac{\partial^2 \psi}{\partial y^2} = -\beta^2 k^2 \psi \tag{2.55}$$

$$\frac{\partial^2 \psi}{\partial z^2} = -\gamma^2 k^2 \psi \tag{2.56}$$

and

$$\frac{\partial^2 \psi}{\partial t^2} = -\omega^2 \psi. \tag{2.57}$$

Adding the three spatial derivatives and utilizing the fact that $\alpha^2 + \beta^2 + \gamma^2 = 1$, we obtain

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2} = -k^2 \psi. \tag{2.58}$$

Combining this with the time derivative Eq. (2.57) and remembering that $v = \omega/k$, we arrive at

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2} = \frac{1}{v^2}\frac{\partial^2 \psi}{\partial t^2}, \tag{2.59}$$

the *three-dimensional differential wave equation.* Note that x, y, and z do appear symmetrically, and the form is precisely what one might expect from the generalization of Eq. (2.11).

Equation (2.59) is usually written in a more concise form by introducing the *Laplacian* operator

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}, \tag{2.60}$$

whereupon it becomes simply

$$\nabla^2 \psi = \frac{1}{v^2}\frac{\partial^2 \psi}{\partial t^2}. \tag{2.61}$$

Now that we have this most important equation, let's briefly return to the plane wave and see how it fits into the scheme of things. A function of the form

$$\psi(x, y, z, t) = Ae^{ik(\alpha x + \beta y + \gamma z \mp vt)} \tag{2.62}$$

is equivalent to Eq. (2.51) and, as such, is a solution of Eq. (2.61). It can also be shown (Problem 2.22) that

$$\psi(x, y, z, t) = f(\alpha x + \beta y + \gamma z - vt) \tag{2.63}$$

and

$$\psi(x, y, z, t) = g(\alpha x + \beta y + \gamma z + vt) \tag{2.64}$$

are both plane-wave solutions of the differential wave equation. The functions f and g, which are twice differentiable, are otherwise arbitrary and certainly need not be harmonic. A linear combination of these solutions is also a solution, and we can write this in a slightly different manner as

$$\psi(\mathbf{r}, t) = C_1 f(\mathbf{r} \cdot \mathbf{k}/k - vt) + C_2 g(\mathbf{r} \cdot \mathbf{k}/k + vt), \tag{2.65}$$

where C_1 and C_2 are constants.

Cartesian coordinates are particularly suitable for describing plane waves. However, as various physical situations arise, we can often take better advantage of existing symmetries by making use of some other coordinate representations.

2.7 SPHERICAL WAVES

Toss a stone into a tank of water. The surface ripples that emanate from the point of impact spread out in two-dimensional circular waves. Extending this imagery to three dimensions, envision a small pulsating sphere surrounded by a fluid. As the source expands and contracts, it generates pressure variations that propagate outward as spherical waves.

Consider now an idealized point source of light. The radiation emanating from it streams out radially, uniformly in all directions. The source is said to be *isotropic,* and the resulting wavefronts are again concentric spheres that increase in diameter as they expand out into the surrounding space. The obvious symmetry of the wavefronts suggests that it might be more convenient to describe them mathematically, in terms of spherical polar coordinates (Fig. 2.15). In this representation the Laplacian operator is

$$\nabla^2 = \frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2 \frac{\partial}{\partial r}\right) + \frac{1}{r^2 \sin\theta}\frac{\partial}{\partial \theta}\left(\sin\theta \frac{\partial}{\partial \theta}\right) + \frac{1}{r^2 \sin^2\theta}\frac{\partial^2}{\partial \phi^2}, \tag{2.66}$$

where r, θ, ϕ are defined by

$$x = r\sin\theta\cos\phi, \qquad y = r\sin\theta\sin\phi, \qquad z = r\cos\theta.$$

Remember that we are looking for a description of spherical waves, waves that are spherically symmetrical (i.e., ones that do not depend on θ and ϕ) so that

$$\psi(\mathbf{r}) = \psi(r, \theta, \phi) = \psi(r). \tag{2.67}$$

The Laplacian of $\psi(r)$ is then simply

$$\nabla^2 \psi(r) = \frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2 \frac{\partial \psi}{\partial r}\right). \tag{2.68}$$

We can obtain this result without being familiar with Eq. (2.66). Start with the Cartesian form of the Laplacian (2.60), operate on the spherically symmetrical wave function $\psi(r)$, and convert each term to polar coordinates. Examining only the x-dependence, we have

$$\frac{\partial \psi}{\partial x} = \frac{\partial \psi}{\partial r}\frac{\partial r}{\partial x}$$

and

$$\frac{\partial^2 \psi}{\partial x^2} = \frac{\partial^2 \psi}{\partial r^2}\left(\frac{\partial r}{\partial x}\right)^2 + \frac{\partial \psi}{\partial r}\frac{\partial^2 r}{\partial x^2},$$

since

$$\psi(\mathbf{r}) = \psi(r).$$

Using

$$x^2 + y^2 + z^2 = r^2,$$

we have

$$\frac{\partial r}{\partial x} = \frac{x}{r}, \qquad \frac{\partial^2 r}{\partial x^2} = \frac{1}{r}\frac{\partial}{\partial x}(x) + x\frac{\partial}{\partial x}\left(\frac{1}{r}\right) = \frac{1}{r}\left(1 - \frac{x^2}{r^2}\right)$$

and

$$\frac{\partial^2 \psi}{\partial x^2} = \frac{x^2}{r^2}\frac{\partial^2 \psi}{\partial r^2} + \frac{1}{r}\left(1 - \frac{x^2}{r^2}\right)\frac{\partial \psi}{\partial r}.$$

Now having $\partial^2\psi/\partial x^2$, we form $\partial^2\psi/\partial y^2$ and $\partial^2\psi/\partial z^2$, and on adding get

$$\nabla^2 \psi(r) = \frac{\partial^2 \psi}{\partial r^2} + \frac{2}{r}\frac{\partial \psi}{\partial r},$$

which is equivalent to Eq. (2.68). This result can be expressed in a slightly different form:

$$\nabla^2 \psi = \frac{1}{r}\frac{\partial^2}{\partial r^2}(r\psi). \tag{2.69}$$

The differential wave equation (2.61) can then be written as

$$\frac{1}{r}\frac{\partial^2}{\partial r^2}(r\psi) = \frac{1}{v^2}\frac{\partial^2 \psi}{\partial t^2}. \tag{2.70}$$

Multiplying both sides by r, we obtain

$$\frac{\partial^2}{\partial r^2}(r\psi) = \frac{1}{v^2}\frac{\partial^2}{\partial t^2}(r\psi). \tag{2.71}$$

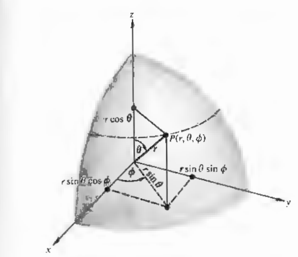


Figure 2.15 The geometry of spherical coordinates.

* There is no distinguishing characteristic for any one of the axes in Cartesian coordinates. We should therefore be able to change the names of, say, x to z, y to x, and z to y (keeping the system right-handed) without altering the differential wave equation.

Notice that this expression is now just the one-dimensional differential wave equation (2.11), where the space variable is r and the wave function is the product $(r\psi)$. The solution of Eq. (2.71) is then simply

$$r\psi(r, t) = f(r - vt)$$

or

$$\psi(r, t) = \frac{f(r - vt)}{r}. \tag{2.72}$$

This represents a spherical wave progressing radially outward from the origin, at a constant speed v, and having an arbitrary functional form f. Another solution is given by

$$\psi(r, t) = \frac{g(r + vt)}{r},$$

and in this case the wave is converging toward the origin.* The fact that this expression blows up at $r = 0$ is of little practical concern.

A special case of the general solution

$$\psi(r, t) = C_1 \frac{f(r - vt)}{r} + C_2 \frac{g(r + vt)}{r} \tag{2.73}$$

is the *harmonic spherical wave*

$$\psi(r, t) = \left(\frac{\mathscr{A}}{r}\right) \cos k(r \mp vt) \tag{2.74}$$

or

$$\psi(r, t) = \left(\frac{\mathscr{A}}{r}\right) e^{ik(r \mp vt)}, \tag{2.75}$$

wherein the constant $\mathscr{A}$ is called the *source strength*. At any fixed value of time, this represents a cluster of concentric spheres filling all space. Each wavefront, or surface of constant phase, is given by

$$kr = \text{constant}.$$

* Other more complicated solutions exist when the wave is not spherically symmetrical. See C. A. Coulson, *Waves*, Chapter 1.

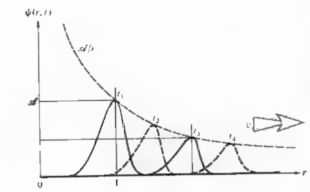


Figure 2.16 A "quadruple exposure" of a spherical pulse.

Notice that the amplitude of any spherical wave is a function of r, where the term r^{-1} serves as an attenuation factor. Unlike the plane wave, a spherical wave decreases in amplitude, thereby changing its profile, as it expands and moves out from the origin.* Figure 2.16 illustrates this graphically by showing a "multiple exposure" of a spherical pulse at four different times. The pulse has the same extent in space at any point along any radius r; that is, the width of the pulse along the r-axis is a constant. Figure 2.17 is an attempt to relate the diagrammatic representation of $\psi(r, t)$ in the previous figure to its actual form as a spherical wave. It depicts half the spherical pulse at two different times, as the wave expands outward. Remember that these results would obtain regardless of the direction of r, because of the spherical symmetry. We could also have drawn a harmonic wave, rather than a pulse, in Figs. 2.16 and 2.17. In this case, the sinusoidal disturbance would have been bounded by the curves

$$\psi = \mathscr{A}/r \quad \text{and} \quad \psi = -\mathscr{A}/r.$$

The outgoing spherical wave emanating from a point source and the incoming wave converging to a point are idealizations. In actuality, light only approximates spherical waves, as it also only approximates plane waves.

As a spherical wavefront propagates out, its radius increases. Far enough away from the source, a small area of the wavefront will closely resemble a portion of a plane wave (Fig. 2.18).

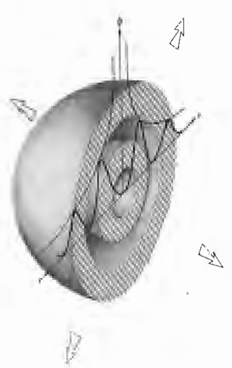


Figure 2.17 Spherical wavefronts.

Figure 2.18 The flattening of spherical waves with distance.

2.8 CYLINDRICAL WAVES

We will now briefly examine another idealized waveform, the infinite circular cylinder. Unfortunately, a precise mathematical treatment is far too involved to do here. We shall, however, outline the procedure, so that the resulting wave function will evoke no mysticism. The Laplacian of ψ in cylindrical coordinates (Fig. 2.19) is

$$\nabla^2\psi = \frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial\psi}{\partial r}\right) + \frac{1}{r^2}\frac{\partial^2\psi}{\partial\theta^2} + \frac{\partial^2\psi}{\partial z^2}, \tag{2.76}$$

where

$$x = r\cos\theta, \quad y = r\sin\theta, \quad \text{and} \quad z = z.$$

The simple case of cylindrical symmetry requires that

$$\psi(\mathbf{r}) = \psi(r, \theta, z) = \psi(r).$$

The θ-independence means that a plane perpendicular to the z-axis will intersect the wavefront in a circle, which may vary in r, at different values of z. In addition, the z-independence further restricts the wavefront to a right circular cylinder centered on the z-axis and

* The attenuation factor is a direct consequence of energy conservation. Chapter 3 contains a discussion of how these ideas apply specifically to electromagnetic radiation.

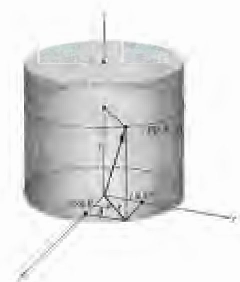


Figure 2.19 The geometry of cylindrical coordinates.

having infinite length. The differential wave equation is accordingly

$$\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial\psi}{\partial r}\right)=\frac{1}{v^2}\frac{\partial^2\psi}{\partial t^2}. \qquad (2.77)$$

We are looking for an expression for $\psi(r)$, a solution of this equation. After a bit of manipulation, in which the time dependence is separated out, Eq. (2.77) becomes something called Bessel's equation. The solutions of Bessel's equation for large values of r gradually approach simple trigonometric forms. Finally, then, when r is sufficiently large, we can write

$$\psi(r,t)\approx\frac{\mathscr{A}}{\sqrt{r}}e^{ik(r\mp vt)}$$

$$\psi(r,t)\approx\frac{\mathscr{A}}{\sqrt{r}}\cos k(r\mp vt). \qquad (2.78)$$

This represents a set of coaxial circular cylinders filling all space and traveling toward or away from an infinite line source. No solutions in terms of arbitrary functions can now be found as there were for both spherical (2.73) and plane (2.65) waves.

A plane wave impinging on the back of a flat opaque screen containing a long thin slit will result in the emission, from that slit, of a disturbance resembling a cylindrical wave (see Fig. 2.20). Extensive use has been made of this technique to generate cylindrical lightwaves. Remember that the actual wave, however generated, only resembles the idealized mathematical representation.

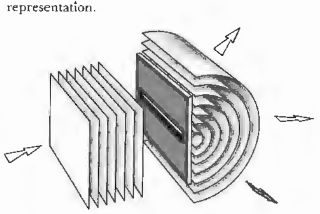


Figure 2.20 Cylindrical waves emerging from a long, narrow slit.

2.9 SCALAR AND VECTOR WAVES

There are two general classifications of waves: *longitudinal* and *transverse*. The distinction between the two arises from a difference between the direction along which the disturbance occurs and the direction, $\mathbf{k}/k$, in

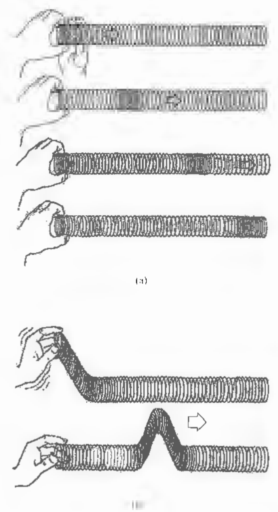


Figure 2.21 (a) A longitudinal wave in a spring. (b) A transverse wave in a spring.

which the disturbance propagates. This is rather easy to visualize when dealing with an elastically deformable material medium (Fig. 2.21). A longitudinal wave occurs when the particles of the medium are displaced from their equilibrium positions, in a direction parallel to $\mathbf{k}/k$. A transverse wave arises when the disturbance, in this case the displacement of the medium, is perpendicular to the propagation direction. Figure 2.22(a) depicts a transverse wave (as on a stretched string) traveling in the z-direction. In this instance, the wave motion is confined to a spatially fixed plane called the **plane of vibration**, and the wave is accordingly said to be *linearly* or *plane polarized*. To determine the wave completely, we must now specify the orientation of the plane of vibration, as well as the direction of propagation. This is equivalent to resolving the disturbance into components along two mutually perpendicular axes, both normal to z [see Fig. 2.22(b)]. The angle at which the plane of vibration is inclined is a constant, so that at any time ψ_x and ψ_y differ from ψ by a multiplicative constant and are both therefore solutions of the differential wave equation. A significant fact has evolved: the wave function of a transverse wave behaves somewhat like a vector quantity. With the wave moving along the z-axis, we can write

$$\boldsymbol{\psi}(z,t)=\psi_x(z,t)\hat{\mathbf{i}}+\psi_y(z,t)\hat{\mathbf{j}}, \qquad (2.79)$$

where, of course, $\hat{\mathbf{i}}$, $\hat{\mathbf{j}}$, and $\hat{\mathbf{k}}$ are the unit base vectors in Cartesian coordinates.

A scalar harmonic plane wave is given by the expression

$$\psi(\mathbf{r},t)=Ae^{i(\mathbf{k}\cdot\mathbf{r}\mp\omega t)}. \qquad [2.47]$$

A *linearly polarized* harmonic plane wave is given by the *wave vector*

$$\boldsymbol{\psi}(\mathbf{r},t)=\mathbf{A}e^{i(\mathbf{k}\cdot\mathbf{r}\mp\omega t)} \qquad (2.80)$$

or in Cartesian coordinates by

$$\boldsymbol{\psi}(x,y,z,t)=(A_x\hat{\mathbf{i}}+A_y\hat{\mathbf{j}}+A_z\hat{\mathbf{k}})e^{i(k_xx+k_yy+k_zz\mp\omega t)}. \qquad (2.81)$$

For this latter case in which the plane of vibration is fixed in space, so too is the orientation of $\mathbf{A}$. Remember that $\boldsymbol{\psi}$ and $\mathbf{A}$ differ only by a scalar and, as such, are parallel to each other and perpendicular to $\mathbf{k}/k$.

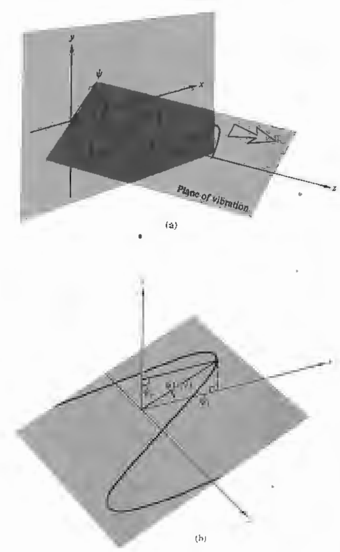


Figure 2.22 Linearly polarized waves.

Light behaves like a transverse wave, and an appreciation of its vectorial nature is of great importance. The phenomena of optical *polarization* can readily be treated in terms of this sort of vector wave picture. For *unpolarized* light, in which the wave vector changes direction randomly and rapidly, scalar approximations become useful, as in the theories of interference and diffraction.

PROBLEMS

2.1 How many "yellow" light waves ($\lambda = 580$ nm) will fit into a distance in space equal to the thickness of a piece of paper (0.003 in)? How far will the same number of microwaves ($\nu = 10^{10}$ Hz, i.e., 10 GHz, and $v = 3 \times 10^8$ m/s) extend?

2.2* The speed of light in vacuum is 3×10^8 m/s. Find the wavelength of red light having a frequency of 5×10^{14} Hz. Compare this with the wavelength of a 60-Hz electromagnetic wave.

2.3* It is possible to generate ultrasonic waves in crystals with wavelengths similar to light (5×10^{-5} cm) but with lower frequencies (6×10^8 Hz). Compute the corresponding speed of such a wave.

2.4* Make up a table with columns headed by values of θ running from $-\pi/2$ to 2π in intervals of $\pi/4$. In each column place the corresponding value of $\sin\theta$, beneath those the values of $\cos\theta$, beneath those the values of $\sin(\theta - \pi/4)$, and so on, with the functions $\sin(\theta - \pi/2)$, $\sin(\theta - 3\pi/4)$, and $\sin(\theta + \pi/2)$. Plot each of these functions, noting the effect of the phase shift. Does $\sin\theta$ lead or lag $\sin(\theta - \pi/2)$; in other words, does one of the functions reach a particular magnitude at a smaller value of θ than the other and therefore lead the other (as $\cos\theta$ leads $\sin\theta$)?

2.5* Make up a table with columns headed by values of kx running from $x = -\lambda/2$ to $x = +\lambda$ in intervals of x of $\lambda/4$—of course, $k = 2\pi/\lambda$. In each column place the corresponding values of $\cos(kx - \pi/4)$ and beneath that the values of $\cos(kx + 3\pi/4)$. Next plot the functions $15\cos(kx - \pi/4)$ and $25\cos(kx + 3\pi/4)$.

2.6* Make up a table with columns headed by values of ωt running from $t = -\tau/2$ to $t = +\tau$ in intervals of t of $\tau/4$—of course, $\omega = 2\pi/\tau$. In each column place the corresponding values of $\sin(\omega t + \pi/4)$ and $\sin(\pi/4 - \omega t)$ and then plot these two functions.

2.7 Using the wave functions

$$\psi_1 = 4\sin 2\pi(0.2x - 3t)$$

and

$$\psi_2 = \frac{\sin(7x + 3.5t)}{2.5},$$

determine in each case the values of (a) frequency, (b) wavelength, (c) period, (d) amplitude, (e) phase velocity, and (f) direction of motion. Time is in seconds and x is in meters.

2.8* Show that

$$\psi(x, t) = A\sin k(x - vt) \qquad [2.14]$$

is a solution of the differential wave equation.

2.9 Show that if the displacement of the string in Fig. 2.8 is given by

$$y(x, t) = A\sin[kx - \omega t + \varepsilon],$$

then the hand generating the wave must be moving vertically in simple harmonic motion.

2.10 Write the expression for a harmonic wave of amplitude 10^3 V/m, period 2.2×10^{-15} s, and speed 3×10^8 m/s. The wave is propagating in the negative x-direction and has a value of 10^3 V/m at $t = 0$ and $x = 0$.

2.11 Consider the pulse described in terms of its displacement at $t = 0$ by

$$y(x, t)|_{t=0} = \frac{C}{2 + x^2},$$

where C is a constant. Draw the wave profile. Write an expression for the wave, having a speed v in the negative x-direction, as a function of time t. If $v = 1$ m/s, sketch the profile at $t = 2$ s.

2.12* What is the magnitude of the wave function $\psi(z, t) = A\cos[k(z + vt) + \pi]$ at the point $z = 0$, when $t = \tau/2$ and when $t = 3\tau/4$?

2.13 Does the following function, in which A is a constant,

$$\psi(y, t) = (y - vt)A$$

represent a wave? Explain your reasoning.

2.14* Use Eq. (2.32) to calculate the speed of the wave whose representation in SI units is

$$\psi(y, t) = A\cos\pi(3 \times 10^6 y + 9 \times 10^{14} t).$$

2.15 Create an expression for the *profile* of a harmonic wave traveling in the z-direction whose magnitude at $z = -\lambda/12$ is 0.866, at $z = +\lambda/6$ is 1/2, and at $z = \lambda/4$ is 0.

2.16* Show that the imaginary part of a complex number z is given by $(z - z^*)/2i$.

2.17* Determine which of the following describe traveling waves:

$$\psi(y, t) = e^{-(a^2y^2 + b^2t^2 - 2abty)}$$

$$\psi(z, t) = A\sin(az^2 - bt^2)$$

$$\psi(x, t) = A\sin 2\pi\left(\frac{x}{a} + \frac{t}{b}\right)^2$$

$$\psi(x, t) = A\cos^2 2\pi(t - x).$$

Where appropriate draw the profile and find the speed and direction of motion.

2.18 Given the traveling wave $\psi(x, t) = 5.0\exp(-ax^2 - bt^2 - 2\sqrt{ab}\,xt)$, determine its direction of propagation. Calculate a few values of ψ and make a sketch of the wave at $t = 0$, taking $a = 25\ \text{m}^{-2}$ and $b = 9.0\ \text{s}^{-2}$. What is the speed of the wave?

2.19 Beginning with Eq. (2.50), verify that

$$\psi(x, y, z, t) = Ae^{i[k(\alpha x + \beta y + \gamma z) \mp \omega t]}$$

and that

$$\alpha^2 + \beta^2 + \gamma^2 = 1.$$

Draw a sketch showing all the pertinent quantities.

2.20 Consider a lightwave having a phase velocity of 3×10^8 m/s and a frequency of 6×10^{14} Hz. What is the shortest distance along the wave between any two points that have a phase difference of 30°? What phase shift occurs at a given point in 10^{-6} s, and how many waves have passed by in that time?

2.21 Write an expression for the wave shown in Fig. 2.23. Find its wavelength, velocity, frequency, and period.

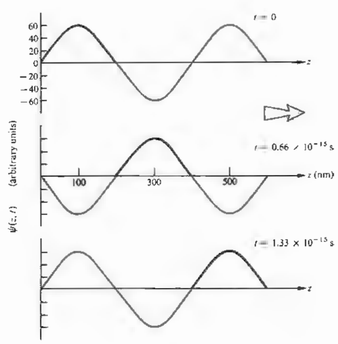


Figure 2.23 A harmonic wave.

2.22* Show that Eqs. (2.63) and (2.64), which are plane waves of arbitrary form, satisfy the three-dimensional differential wave equation.

2.23 De Broglie's hypothesis states that every particle has associated with it a wavelength given by Planck's constant ($h = 6.6 \times 10^{-34}$ J s) divided by the particle's momentum. Compare the wavelength of a 6.0-kg stone moving at a speed of 1.0 m/s with that of light.

2.24 Write an expression in Cartesian coordinates for a harmonic plane wave of amplitude A and frequency ω propagating in the direction of the vector $\mathbf{k}$, which in turn lies on a line drawn from the origin to the point (4, 2, 1). *Hint:* first determine $\mathbf{k}$ and then dot it with $\mathbf{r}$.

2.25* Write an expression in Cartesian coordinates for a harmonic plane wave of amplitude A and frequency ω propagating in the positive x-direction.

2.26 Show that $\psi(\mathbf{k} \cdot \mathbf{r}, t)$ may represent a plane wave where $\mathbf{k}$ is normal to the wavefront. *Hint:* let $\mathbf{r}_1$ and $\mathbf{r}_2$ be position vectors drawn to any two points on the plane and show that $\psi(\mathbf{r}_1, t) = \psi(\mathbf{r}_2, t)$.

2.27* Make up a table with columns headed by values of θ running from $-\pi/2$ to 2π in intervals of $\pi/4$. In each column place the corresponding value of $\sin \theta$, and beneath those the values of $2 \sin \theta$. Next add these, column by column, to yield the corresponding values of the function $\sin \theta + 2 \sin \theta$. Plot each of these three functions, noting their relative amplitudes and phases.

2.28* Make up a table with columns headed by values of θ running from $-\pi/2$ to 2π in intervals of $\pi/4$. In each column place the corresponding value of $\sin \theta$, and beneath those the values of $\sin (\theta - \pi/2)$. Next add these, column by column, to yield the corresponding values of the function $\sin \theta + \sin (\theta - \pi/2)$. Plot each of these three functions, noting their relative amplitudes and phases.

2.29* With the last two problems in mind, draw a plot of $\sin \theta$, $\sin (\theta - 3\pi/4)$, and $\sin \theta + \sin (\theta - 3\pi/4)$. Compare the amplitude of the combined function in this case with that of the previous problem.

2.30* Make up a table with columns headed by values of kx running from $x = -\lambda/2$ to $x = +\lambda$ in intervals of x of $\lambda/4$. In each column place the corresponding values of $\cos kx$ and beneath that the values of $\cos (kx + \pi)$. Next plot the functions $\cos kx$, $\cos (kx + \pi)$, and $\cos kx + \cos (kx + \pi)$.

3 ELECTROMAGNETIC THEORY, PHOTONS, AND LIGHT

The work of J. C. Maxwell and subsequent developments since the late 1800s have made it evident that light is most certainly electromagnetic in nature. Classical electrodynamics, as we shall see, unalterably leads to the picture of a continuous transfer of energy by way of electromagnetic waves. In contrast, the more modern view of quantum electrodynamics describes electromagnetic interactions and the transport of energy in terms of massless elementary "particles" known as *photons*, which are localized quanta of energy. The quantum nature of radiant energy is not always readily apparent, nor indeed is it always of practical concern in optics. There is a range of situations in which the detecting equipment is such that it is impossible, and desirably so, to distinguish individual quanta. More often than not, the stream of incident light carries a relatively large amount of energy, and the granularity is obscured in any event.

If the wavelength of light is small in comparison to the size of the apparatus, one may use, as a first approximation, the techniques of *geometrical optics*. A somewhat more precise treatment, which is applicable as well when the dimensions of the apparatus are small, is that of *physical optics*. In physical optics the dominant property of light is its wave nature. It is even possible to develop most of the treatment without ever specifying the kind of wave one is dealing with. Certainly, as far as the classical study of pbysical optics is concerned, it will suffice admirably to treat light as an electromagnetic wave.

We can think of light as another manifestation of matter. Indeed, one of the basic tenets of quantum mechanics is that both light and material objects each display similar wave–particle properties. As Erwin C. Schrödinger (1887–1961), one of the founders of quantum theory, put it:

> In the new setting of ideas the distinction [between particles and waves] has vanished, because it was discovered that all particles have also wave properties, and *vice versa*. Neither of the two concepts must be discarded, they must be amalgamated. Which aspect obtrudes itself depends not on the physical object, but on the experimental device set up to examine it.*

The quantum-mechanical treatment associates a wave equation with a particle, be it a photon, electron, proton, or whatever. In the case of material particles, the wave aspects are introduced by way of the field equation known as Schrödinger's equation. For photons we have a representation of the wave nature in the form of the classical electromagnetic field equations of Maxwell. With these as a starting point one can construct a quantum-mechanical theory of photons and their interaction with charges. The dual nature of light is evidenced by the fact that it propagates through space in a wavelike fashion and yet can display particlelike behavior during emission and absorption processes. Electromagnetic radiant energy is created and destroyed in quanta or photons and not continuously as a classical wave. Nonetheless its motion through a

* Erwin C. Schrödinger, *Science Theory and Man.*

lens, a hole, or a set of slits is governed by wave characteristics. If we're unfamiliar with this kind of behavior in the macroscopic world, it's because the wavelength of an object varies inversely with its momentum (see Chapter 13), and even a grain of sand (which is barely moving) has a wavelength so small as to be indiscernible in any conceivable experiment.

The photon has several properties that distinguish it from all other subatomic particles. These properties are of considerable interest to us, because they are responsible for the fact that quite often the quantum aspects of light are thoroughly obscured. In particular, there are no restrictions on the number of photons that can exist in a region with the same linear and angular momentum. Restrictions of this sort (the Pauli exclusion principle) do exist for most other particles (with the exception for example of the still hypothetical quantum of gravity, i.e., the graviton, He_4 and π mesons). The photon has zero rest mass, and therefore exceedingly large numbers of low-energy photons can be envisioned as present in a beam of light. Within that model dense streams of photons (many of which may have essentially the same momentum) act on the average to produce well-defined classical fields. We can draw a rough analogy with the flow of commuters through a train station during rush hour. Each one presumably behaves individually as a quantum of humanity, but all have the same intent and follow fairly similar trajectories. To a distant, myopic observer there is a seemingly smooth and continuous flow. The behavior of the stream en masse is predictable from day to day, so the precise motion of each commuter is unimportant, at least to the observer. The energy transported by a large number of photons is, *on the average,* equivalent to the energy transferred by a classical electromagnetic wave. It is for these reasons that the field representation of electromagnetic phenomena has been, and will continue to be, so useful. It should be noted, however, that when we speak of overlapping electromagnetic waves, it is essentially a euphemism for the interference of probability amplitudes, but more about that will have to wait for Chapter 13.

Quite pragmatically, then, we can consider light to be a classical electromagnetic wave, keeping in mind that there are situations (on the periphery of our present concern) for which this description is woefully inadequate.

3.1 BASIC LAWS OF ELECTROMAGNETIC THEORY

Our intent in this section is to review and develop, if only briefly, some of the ideas needed to appreciate the concept of electromagnetic waves.

We know from experiments that charges, even though separated in vacuum, experience a mutual interaction. Recall the familiar electrostatics demonstration in which a pith ball somehow senses the presence of a charged rod without actually touching it. As a possible explanation we might speculate that each charge emits (and absorbs) a stream of undetected particles (*virtual photons*). The exchange of these particles among the charges may be regarded as the mode of interaction. Alternatively, we can take the classical approach and imagine instead that every charge is surrounded by something called an electric field. We then need only suppose that each charge interacts directly with the electric field in which it is immersed. Thus if a charge q experiences a force $\mathbf{F}_E$, the *electric field* $\mathbf{E}$ at the position of the charge is defined by $\mathbf{F}_E = q\mathbf{E}$. In addition, we observe that a moving charge may experience another force $\mathbf{F}_M$, which is proportional to its velocity $\mathbf{v}$. We are thus led to define yet another field, namely, the *magnetic induction* $\mathbf{B}$, such that $\mathbf{F}_M = q\mathbf{v} \times \mathbf{B}$. If forces $\mathbf{F}_E$ and $\mathbf{F}_M$ occur concurrently, the charge is said to be moving through a region pervaded by both electric and magnetic fields, whereupon $\mathbf{F} = q\mathbf{E} + q\mathbf{v} \times \mathbf{B}$.

There are several other observations that may be interpreted in terms of these fields, and in so doing we can get a better idea of the physical properties that must be attributed to $\mathbf{E}$ and $\mathbf{B}$. As we shall see, *electric fields* are generated by both electric charges and by *time-varying magnetic fields.* Similarly, *magnetic fields* are generated by electric currents and by *time-varying electric fields.* This interdependence of $\mathbf{E}$ and $\mathbf{B}$ is a key point in the description of light, and its elaboration is the motivation for much of what follows.

3.1.1 Faraday's Induction Law

Michael Faraday made a number of major contributions to electromagnetic theory. One of the most significant was his discovery that a time-varying magnetic flux passing through a closed conducting loop results in the generation of a current around that loop. The flux of magnetic induction (or *magnetic flux density*) $\mathbf{B}$ through any open area A bounded by the conducting loop (Fig. 3.1) is given by

$$\Phi_B = \iint_A \mathbf{B} \cdot d\mathbf{S}. \tag{3.1}$$

The induced *electromotive force,* or *emf,* developed around the loop is then

$$\text{emf} = -\frac{d\Phi_B}{dt}. \tag{3.2}$$

We should not, however, get too involved with the image of wires and current and emf. Our present concern is with the electric and magnetic fields themselves. Indeed, the emf exists only as a result of the presence

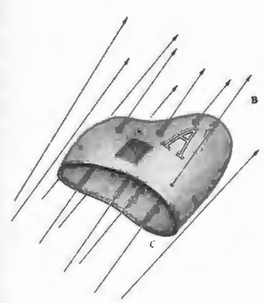


Figure 3.1 B-field through an open area A.

of an electric field given by

$$\text{emf} = \oint_C \mathbf{E} \cdot d\mathbf{l}, \tag{3.3}$$

taken around the closed curve C, corresponding to the loop. Equating Eqs. (3.2) and (3.3), and making use of Eq. (3.1), we get

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = -\frac{d}{dt} \iint_A \mathbf{B} \cdot d\mathbf{S}. \tag{3.4}$$

We began this discussion by examining a conducting loop and have arrived at Eq. (3.4); this expression, except for the path C, contains no reference to the physical loop. In fact, the path can be chosen quite arbitrarily and need not be within, or anywhere near, a conductor. The electric field in Eq. (3.4) arises not from the presence of electric charges but rather from the time-varying magnetic field. With no charges to act as sources or sinks, the field lines close on themselves, forming loops (Fig. 3.2). For the case in which the path

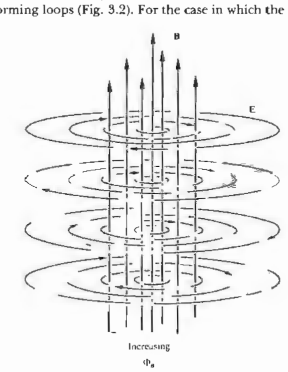


Figure 3.2 A time-varying B-field. Surrounding each point where Φ_B is changing, the E-field forms closed loops.

is fixed in space and unchanging in shape, the *induction law* (Eq. 3.4) can be rewritten as

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = -\iint_A \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S}. \qquad (3.5)$$

This, in itself, is a rather fascinating expression, since it indicates that a time-varying magnetic field will have an electric field associated with it.

3.1.2 Gauss's Law–Electric

Another fundamental law of electromagnetism is named after the German mathematician Karl Friedrich Gauss (1777–1855). It relates the flux of electric field intensity through a closed surface A

$$\Phi_E = \oiint_A \mathbf{E} \cdot d\mathbf{S} \qquad (3.6)$$

to the total enclosed charge. The circled double integral is meant to serve as a reminder that the surface is closed. The vector $d\mathbf{S}$ is in the direction of an *outward normal*, as shown in Fig. 3.3. If the volume enclosed by A is V, and if within it there is a continuous charge distribution of density ρ, then Gauss's law is

$$\oiint_A \mathbf{E} \cdot d\mathbf{S} = \frac{1}{\epsilon} \iiint_V \rho\, dV. \qquad (3.7)$$

The integral on the left is the difference between the amount of flux flowing into and out of any closed surface A. If there is a difference, it will be due to the presence of sources or sinks of the electric field within A. Clearly then, the integral must be proportional to the total enclosed charge, inasmuch as charges are the sources (+) and sinks (−) of the electric field.

The constant ϵ is known as the **electric permittivity** of the medium. For the special case of a vacuum, the *permittivity of free space* is given by $\epsilon_0 = 8.8542 \times 10^{-12}\ \mathrm{C^2\,N^{-1}\,m^{-2}}$. One function of the ϵ in Eq. (3.7) is, of course, to balance out the units, but the concept is even more basic to the description of the parallel plate capacitor (see Section 3.1.4). There it's the medium-dependent proportionality constant between the device's capacitance and its geometric characteristics. Indeed ϵ is often measured by a pro-

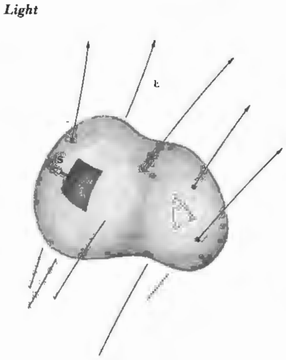


Figure 3.3 E-field through a closed area A.

cedure in which the material under study is placed within a capacitor. Conceptually, the permittivity embodies the electrical behavior of the medium: in a sense, it is a measure of the degree to which the material is permeated by the electric field in which it is immersed.

In the early days of the development of the subject, people in various areas worked in different systems of units, a state of affairs leading to some obvious difficulties. This necessitated the tabulation of numerical values for ϵ in each of the different systems, which was, at best, a waste of time. Recall that the same problem regarding densities was neatly avoided by using specific gravity (i.e., density ratios). Thus it was advantageous to tabulate values not of ϵ but of a new related quantity independent of the system of units being used. Accordingly, we define K_e as ϵ/ϵ_0. This is the *dielectric constant* (or *relative permittivity*), and it is appropriately unitless. The permittivity of a material can then be expressed in terms of ϵ_0 as

$$\epsilon = K_e \epsilon_0. \qquad (3.8)$$

Our interest in K_e anticipates the fact that the permittivity is related to the speed of light in dielectric materials, such as glass, air, quartz, and so on.

3.1.3 Gauss's Law–Magnetic

There is no known magnetic counterpart to the electric charge, that is, no isolated magnetic poles have ever been found, despite extensive searching, even in lunar soil samples. Unlike the electric field, the magnetic induction **B** does not diverge from or converge toward some kind of magnetic charge (a monopole source or sink). Magnetic induction fields can be described in terms of current distributions. Indeed we might envision an elementary magnet as a small current loop in which the lines of **B** are themselves continuous and closed. Any closed surface in a region of magnetic field would accordingly have an equal number of lines of **B** entering and emerging from it (Fig. 3.4). This situation arises from the absence of any monopoles within the enclosed volume. The flux of magnetic induction Φ_B through such a surface is zero, and we have the magnetic

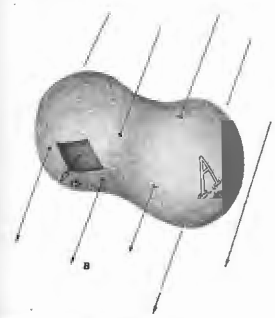


Figure 3.4 B-field through a closed area A.

equivalent of Gauss's law:

$$\Phi_B = \oiint_A \mathbf{B} \cdot d\mathbf{S} = 0. \qquad (3.9)$$

3.1.4 Ampère's Circuital Law

Another equation that will be of great interest to us is due to André Marie Ampère (1775–1836). Known as the *circuital law*, it relates a line integral of **B** tangent to a closed curve C, with the total current i passing within the confines of C:

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu \iint_A \mathbf{J} \cdot d\mathbf{S} = \mu i. \qquad (3.10)$$

The open surface A is bounded by C, and J is the current per unit area (Fig. 3.5). The quantity μ is called the **permeability** of the particular medium. For a vacuum $\mu = \mu_0$ (the *permeability of free space*), which is defined as $4\pi \times 10^{-7}\ \mathrm{N\,s^2\,C^{-2}}$.

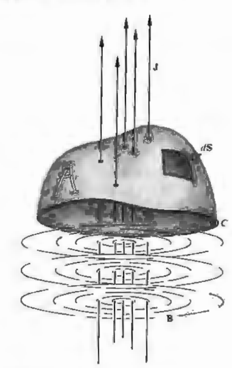


Figure 3.5 Current density through an open area A.

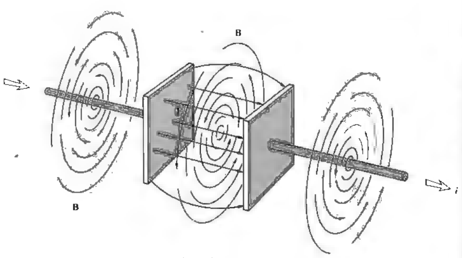


Figure 3.6 B-field concomitant with a time-varying E-field in the gap of a capacitor.

As in Eq. (3.8),

$$\mu = K_m \mu_0, \tag{3.11}$$

with K_m being the dimensionless *relative permeability*.

Equation (3.10), although often adequate, is not the whole truth. Moving charges are not the only source of a magnetic field. While charging or discharging a capacitor, one can measure a **B** field in the region between its plates (Fig. 3.6), which is indistinguishable from the field surrounding the leads, even though no current actually traverses the capacitor. Notice, however, that if A is the area of each plate, and Q the charge on it,

$$E = \frac{Q}{\epsilon A}.$$

As the charge varies, the electric field changes, and

$$\epsilon \frac{\partial E}{\partial t} = \frac{i}{A}$$

is effectively a current density. James C. Maxwell hypothesized the existence of just such a mechanism, which he called the *displacement current density,** defined by

$$\mathbf{J}_D = \epsilon \frac{\partial \mathbf{E}}{\partial t}. \tag{3.12}$$

* Maxwell's own words and ideas concerning this mechanism are examined in an article by A. M. Bork, *Am. J. Phys.* **31**, 854 (1963).

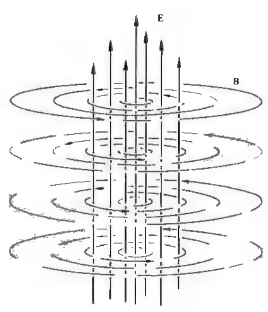


Figure 3.7 A time-varying E-field. Surrounding each point where Φ_E is changing, the B-field forms closed loops.

The restatement of Ampère's law as

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu \iint_A \left(\mathbf{J} + \epsilon \frac{\partial \mathbf{E}}{\partial t}\right) \cdot d\mathbf{S} \tag{3.13}$$

was one of Maxwell's greatest contributions. It points out that even when $\mathbf{J} = 0$, a time-varying **E**-field will be accompanied by a **B**-field (Fig. 3.7).

3.1.5 Maxwell's Equations

The set of integral expressions given by Eqs. (3.5), (3.7), (3.9), and (3.13) have come to be known as Maxwell's equations. Remember that these are generalizations of experimental results. The simplest statement of Maxwell's equations governs the behavior of the electric and magnetic fields in free space, where $\epsilon = \epsilon_0$, $\mu = \mu_0$, and both ρ and **J** are zero. In that instance,

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = -\iint_A \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S}, \tag{3.14}$$

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_0 \epsilon_0 \iint_A \frac{\partial \mathbf{E}}{\partial t} \cdot d\mathbf{S}, \tag{3.15}$$

$$\oiint_A \mathbf{B} \cdot d\mathbf{S} = 0, \tag{3.16}$$

$$\oiint_A \mathbf{E} \cdot d\mathbf{S} = 0. \tag{3.17}$$

Observe that except for a multiplicative scalar, the electric and magnetic fields appear in the equations with a remarkable symmetry. However **E** affects **B**, **B** will in turn affect **E**. The mathematical symmetry implies a good deal of physical symmetry.

Maxwell's equations can be written in a differential form, which will be somewhat more useful for our purposes. The appropriate calculation is carried out in Appendix 1, and the consequent equations for *free space*, in Cartesian coordinates, are as follows:

$$\frac{\partial \mathbf{E}_z}{\partial y} - \frac{\partial \mathbf{E}_y}{\partial z} = -\frac{\partial \mathbf{B}_x}{\partial t}, \quad \text{(i)}$$

$$\frac{\partial \mathbf{E}_x}{\partial z} - \frac{\partial \mathbf{E}_z}{\partial x} = -\frac{\partial \mathbf{B}_y}{\partial t}, \quad \text{(ii)} \tag{3.18}$$

$$\frac{\partial \mathbf{E}_y}{\partial x} - \frac{\partial \mathbf{E}_x}{\partial y} = -\frac{\partial \mathbf{B}_z}{\partial t}, \quad \text{(iii)} \tag{3.18}$$

$$\frac{\partial \mathbf{B}_z}{\partial y} - \frac{\partial \mathbf{B}_y}{\partial z} = \mu_0 \epsilon_0 \frac{\partial \mathbf{E}_x}{\partial t}, \quad \text{(i)}$$

$$\frac{\partial \mathbf{B}_x}{\partial z} - \frac{\partial \mathbf{B}_z}{\partial x} = \mu_0 \epsilon_0 \frac{\partial \mathbf{E}_y}{\partial t}, \quad \text{(ii)} \tag{3.19}$$

$$\frac{\partial \mathbf{B}_y}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial y} = \mu_0 \epsilon_0 \frac{\partial \mathbf{E}_z}{\partial t}, \quad \text{(iii)}$$

$$\frac{\partial \mathbf{B}_x}{\partial x} + \frac{\partial \mathbf{B}_y}{\partial y} + \frac{\partial \mathbf{B}_z}{\partial z} = 0, \tag{3.20}$$

$$\frac{\partial \mathbf{E}_x}{\partial x} + \frac{\partial \mathbf{E}_y}{\partial y} + \frac{\partial \mathbf{E}_z}{\partial z} = 0. \tag{3.21}$$

The transition has thus been made from the formulation of Maxwell's equations in terms of integrals over *finite regions* to a restatement in terms of derivatives at *points* in space.

We now have all that is needed to comprehend the magnificent process whereby electric and magnetic fields, inseparably coupled and mutually sustaining, propagate out into space as a single entity, free of charges and currents, sans matter, sans aether.

3.2 ELECTROMAGNETIC WAVES

We have relegated to Appendix 1 a complete and mathematically elegant derivation of the electromagnetic wave equation. We will spend some time here at the equally important task of developing a more intuitive appreciation of the physical processes involved. Three observations, from which we might build a qualitative picture, are readily available to us: the general perpendicularity of the fields, the symmetry of Maxwell's equations, and the interdependence of **E** and **B** in those equations.

In studying electricity and magnetism one soon becomes aware that there are a number of relationships described by vector cross-products or, if you like, right-hand rules. In other words, an occurrence of one sort produces a related, perpendicularly directed response. Of immediate interest is the fact that a time-varying

E-field generates a **B**-field that is everywhere perpendicular to the direction in which **E** changes (Fig. 3.7). In the same way, a time-varying **B**-field generates an **E**-field that is everywhere perpendicular to the direction in which **B** changes (Fig. 3.2). We might, accordingly, anticipate the general transverse nature of the **E**- and **B**-fields in an electromagnetic disturbance.

Consider a charge that is somehow caused to *accelerate* from rest. When the charge is motionless, it has associated with it a radial **E**-field extending in all directions to infinity. At the instant the charge begins to move, the **E**-field is altered in the vicinity of the charge, and this alteration propagates out into space at some finite speed. The time-varying electric field induces a magnetic field by means of Eq. (3.15) or (3.19). But the charge is accelerating, $\partial \mathbf{E}/\partial t$ is itself not constant, so the induced **B**-field is time-dependent. The time-varying **B**-field generates an **E**-field, (3.14) or (3.18), and the process continues, with **E** and **B** coupled in the form of a pulse. As one field changes, it generates a new field that extends a bit further, and the pulse moves out from one point to the next through space.

We can draw an overly mechanistic but rather picturesque analogy, if we imagine the electric field lines as a dense radial distribution of strings. When somehow plucked, each string is distorted, forming a kink that travels outward from the source. All these kinks combine at any instant to yield a three-dimensional expanding pulse.

The **E**- and **B**-fields can more appropriately be considered as two aspects of a single physical phenomenon, the *electromagnetic field*, whose source is a moving charge. The disturbance, once it has been generated in the electromagnetic field, is an untethered wave that moves beyond its source and independently of it. Bound together as a single entity, the time-varying electric and magnetic fields regenerate each other in an endless cycle. The electromagnetic waves reaching us from the relatively nearby center of our own galaxy have been on the wing for 30,000 years.

We have not yet considered the direction of wave propagation with respect to the constituent fields. Notice, however, that the high degree of symmetry in Maxwell's equations for free space suggests that the disturbance will propagate in a direction that is symmetrical to both **E** and **B**. That implies that an electromagnetic wave cannot be purely longitudinal (i.e., as long as **E** and **B** are not parallel). Let's now replace conjecture with a bit of calculation.

Appendix 1 shows that Maxwell's equations for free space can be manipulated into the form of two extremely concise vector expressions:

$$\nabla^2 \mathbf{E} = \epsilon_0 \mu_0 \frac{\partial^2 \mathbf{E}}{\partial t^2} \qquad [A1.26]$$

and

$$\nabla^2 \mathbf{B} = \epsilon_0 \mu_0 \frac{\partial^2 \mathbf{B}}{\partial t^2}. \qquad [A1.27]$$

The Laplacian,* ∇^2, operates on each component of **E** and **B**, so that the two vector equations actually represent a total of six scalar equations. Two of these expressions, in Cartesian coordinates, are

$$\frac{\partial^2 E_x}{\partial x^2} + \frac{\partial^2 E_x}{\partial y^2} + \frac{\partial^2 E_x}{\partial z^2} = \epsilon_0 \mu_0 \frac{\partial^2 E_x}{\partial t^2} \qquad (3.22)$$

and

$$\frac{\partial^2 E_y}{\partial x^2} + \frac{\partial^2 E_y}{\partial y^2} + \frac{\partial^2 E_y}{\partial z^2} = \epsilon_0 \mu_0 \frac{\partial^2 E_y}{\partial t^2}, \qquad (3.23)$$

with precisely the same form for E_z, B_x, B_y, and B_z. Equations of this sort, which relate the space and time variations of some physical quantity, had been studied long before Maxwell's work and were known to describe wave phenomena. Each and every component of the electromagnetic field (E_x, E_y, E_z, B_x, B_y, B_z) therefore obeys the scalar differential wave equation

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2} = \frac{1}{v^2} \frac{\partial^2 \psi}{\partial t^2}, \qquad [2.59]$$

provided that

$$v = 1/\sqrt{\epsilon_0 \mu_0}. \qquad (3.24)$$

To evaluate v Maxwell made use of the results of electrical experiments performed in 1856 in Leipzig by Wilhelm Weber (1804–1891) and Rudolph Kohlrausch (1809–1858). Equivalently, nowadays μ_0 is assigned a value of $4\pi \times 10^{-7}$ m kg/C² in SI units, and one can determine ϵ_0 directly from simple capacitor measurements. In any event,

$$\epsilon_0 \mu_0 \approx (8.85 \times 10^{-12}\ \mathrm{s^2\,C^2/m^3\,kg})(4\pi \times 10^{-7}\ \mathrm{m\,kg/C^2})$$

or

$$\epsilon_0 \mu_0 \approx 11.12 \times 10^{-18}\ \mathrm{s^2/m^2}.$$

And now the moment of truth—in free space, the predicted speed of all electromagnetic waves would then be

$$v = \frac{1}{\sqrt{\epsilon_0 \mu_0}} \approx 3 \times 10^8\ \mathrm{m/s}.$$

This theoretical value was in remarkable agreement with the previously measured speed of light (315,300 km/s) determined by Fizeau. The results of Fizeau's experiments, performed in 1849 with a rotating toothed wheel, were available to Maxwell and led him to comment:

> This velocity [i.e., his theoretical prediction] is so nearly that of light, that it seems we have strong reason to conclude that light itself (including radiant heat, and other radiations if any) is an electromagnetic disturbance in the form of waves propagated through the electromagnetic field according to electromagnetic laws.

This brilliant analysis was one of the great intellectual triumphs of all time.

It has become customary to designate the speed of light in vacuum by the symbol c, which comes from the Latin word *celer*, meaning fast. In 1983 the 17th Conférence Générale des Poids et Mesures in Paris adopted a new definition of the meter and thereby fixed the speed of light in vacuum as exactly

$$c = 2.99792458 \times 10^8\ \mathrm{m/s}.$$

The experimentally verified transverse character of light must now be explained within the context of the electromagnetic theory. To that end, consider the fairly simple case of a plane wave propagating in the positive x-direction. The electric field intensity is a solution of Eq. (A1.26), where **E** is constant over each of an infinite set of planes perpendicular to the x-axis. It is therefore a function only of x and t; that is, $\mathbf{E} = \mathbf{E}(x, t)$. We now refer back to Maxwell's equations, and in particular to Eq. (3.21), which is generally read as *the divergence of* **E** *equals zero.* Since **E** is not a function of either y or z, the equation can be reduced to

$$\frac{\partial E_x}{\partial x} = 0. \qquad (3.25)$$

If E_x is not zero—that is, if there is some component of the field in the direction of propagation—this expression tells us that it does not vary with x. At any given time E_x is constant for all values of x, but of course, this possibility cannot therefore correspond to a traveling wave advancing in the positive x-direction. Alternatively, it follows from Eq. (3.25) that for a wave, $E_x = 0$; the electromagnetic wave has no electric field component in the direction of propagation. The **E**-field associated with the plane wave is then exclusively *transverse.* Without any loss of generality, we shall deal with *plane* or *linearly* polarized waves, in which the direction of the vibrating **E**-vector is fixed. Thus we can orient our coordinate axes so that the electric field is parallel to the y-axis, whereupon

$$\mathbf{E} = \hat{\mathbf{j}} E_y(x, t). \qquad (3.26)$$

Returning to Eq. (3.18), it follows that

$$\frac{\partial E_y}{\partial x} = -\frac{\partial B_z}{\partial t} \qquad (3.27)$$

and that B_x and B_y are constant and therefore of no interest at present. The time-dependent **B**-field can only have a component in the z-direction. Clearly then, *in free space, the plane electromagnetic wave is indeed transverse* (Fig. 3.8). Except in the case of normal incidence, such waves propagating in real material media are generally not transverse—a complication arising from the fact that the medium may be dissipative and/or contain free charge.

We have not specified the form of the disturbance other than to say that it is a plane wave. Our conclusions are therefore quite general, applying equally well to pulses or continuous waves. We have already pointed out that harmonic functions are of particular interest, because any waveform can be expressed in terms of sinusoidal waves by Fourier techniques. We therefore

* In Cartesian coordinates,

$$\nabla^2 \mathbf{E} = \hat{\mathbf{i}} \nabla^2 E_x + \hat{\mathbf{j}} \nabla^2 E_y + \hat{\mathbf{k}} \nabla^2 E_z.$$

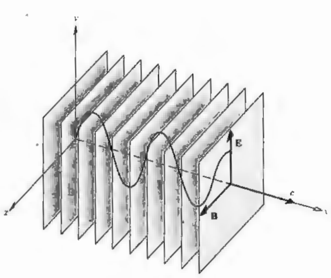


Figure 3.8 The field configuration in a plane harmonic electromagnetic wave.

limit the discussion to harmonic waves and write $E_y(x, t)$ as

$$E_y(x, t) = E_{0y} \cos [\omega(t - x/c) + \varepsilon], \qquad (3.28)$$

the speed of propagation being c. The associated magnetic flux density can be found by directly integrating Eq. (3.27), that is,

$$B_z = -\int \frac{\partial E_y}{\partial x}\, dt.$$

Using Eq. (3.28), we obtain

$$B_z = -\frac{E_{0y}\omega}{c} \int \sin [\omega(t - x/c) + \varepsilon]\, dt$$

or

$$B_z(x, t) = \frac{1}{c} E_{0y} \cos [\omega(t - x/c) + \varepsilon]. \qquad (3.29)$$

The constant of integration, which represents a time-independent field, has been disregarded. Comparison of this result with Eq. (3.28) makes it evident that

$$E_y = cB_z. \qquad (3.30)$$

Since E_y and B_z differ only by a scalar, and so have the

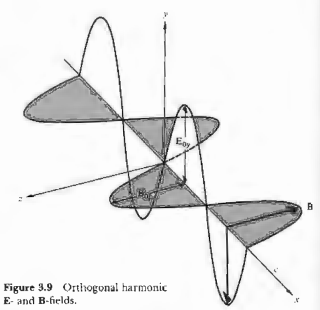


Figure 3.9 Orthogonal harmonic E- and B-fields.

same time dependence, **E** and **B** are *in phase* at all points in space. Moreover, $\mathbf{E} = \hat{\mathbf{j}}E_y(x, t)$ and $\mathbf{B} = \hat{\mathbf{k}}B_z(x, t)$ are *mutually perpendicular*, and their cross-product, $\mathbf{E} \times \mathbf{B}$, points in the propagation direction, $\hat{\mathbf{i}}$ (Fig. 3.9).

Plane waves, although of great importance, are not the only solutions to Maxwell's equations. As we saw in the previous chapter, the differential wave equation allows many solutions, among which are cylindrical and spherical waves (Fig. 3.10).

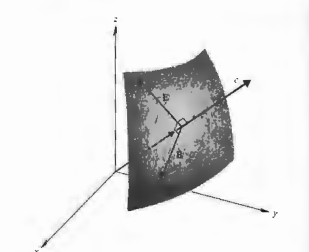


Figure 3.10 Portion of a spherical wavefront far from the source.

3.3 ENERGY AND MOMENTUM

3.3.1 Irradiance

One of the most significant properties of the electromagnetic wave is that it transports energy. The light from even the nearest star beyond the Sun travels 25 million million miles to reach the Earth, yet it still carries enough energy to do work on the electrons within your eye. Any electromagnetic field exists within some region of space, and it is therefore quite natural to consider the *radiant energy per unit volume*, or the **energy density**, u. For an electric field alone, one can compute (Problem 3.3) the energy density (e.g., between the plates of a capacitor) to be

$$u_E = \frac{\epsilon_0}{2} E^2. \qquad (3.31)$$

Similarly, the energy density of the B-field alone (as it might be computed within a toroid) is

$$u_B = \frac{1}{2\mu_0} B^2. \qquad (3.32)$$

We derived the relationship $E = cB$ specifically for a plane wave; nonetheless it is quite general in its applicability. Since $c = 1/\sqrt{\epsilon_0\mu_0}$, it follows that

$$u_E = u_B. \qquad (3.33)$$

The energy streaming through space in the form of an electromagnetic wave is shared between the constituent electric and magnetic fields. Since

$$u = u_E + u_B, \qquad (3.34)$$

clearly,

$$u = \epsilon_0 E^2 \qquad (3.35)$$

or equivalently,

$$u = \frac{1}{\mu_0} B^2. \qquad (3.36)$$

To represent the flow of electromagnetic energy, let S symbolize the transport of energy per unit time (the power) across a unit area. In the SI system it would then have units of W/m^2. Figure 3.11 depicts an electromagnetic wave traveling with a speed c through an area A. During a very small interval of time Δt, only the energy contained in the cylindrical volume, $u(c\,\Delta t\, A)$, will cross A. Thus

$$S = \frac{uc\,\Delta t\, A}{\Delta t\, A} = uc \qquad (3.37)$$

or, using Eq. (3.35),

$$S = \frac{1}{\mu_0} EB. \qquad (3.38)$$

We now make the reasonable assumption (for isotropic media) that the energy flows in the direction of propagation of the wave. The corresponding *vector* **S** is then

$$\mathbf{S} = \frac{1}{\mu_0} \mathbf{E} \times \mathbf{B} \qquad (3.39)$$

or

$$\mathbf{S} = c^2\epsilon_0 \mathbf{E} \times \mathbf{B}. \qquad (3.40)$$

The magnitude of **S** is the power per unit area crossing a surface whose normal is parallel to **S**. Named after John Henry Poynting (1852–1914), it has come to be

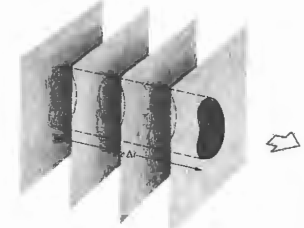


Figure 3.11 The flow of electromagnetic energy.

known as the **Poynting vector.** Let's now apply these considerations to the case of a harmonic, linearly polarized plane wave traveling through free space in the direction of **k**:

$$\mathbf{E} = \mathbf{E}_0 \cos(\mathbf{k} \cdot \mathbf{r} - \omega t) \tag{3.41}$$

$$\mathbf{B} = \mathbf{B}_0 \cos(\mathbf{k} \cdot \mathbf{r} - \omega t). \tag{3.42}$$

Using Eq. (3.40) we find

$$\mathbf{S} = c^2 \epsilon_0 \mathbf{E}_0 \times \mathbf{B}_0 \cos^2(\mathbf{k} \cdot \mathbf{r} - \omega t).$$

It should be evident that $\mathbf{E} \times \mathbf{B}$ cycles from maxima to minima. At optical frequencies, **S** is an extremely rapidly varying function of time (indeed, twice as rapid as the fields, since cosine-squared has double the frequency of cosine), so its instantaneous value would be an impractical quantity to measure. This suggests that we employ an averaging procedure. That is to say, we absorb the radiant energy during some finite interval of time using, for example, a photocell, a film plate, or the retina of a human eye. The time-averaged value of the magnitude of the Poynting vector, symbolized by $\langle S \rangle$, is a measure of the significant quantity known as the **irradiance,*** I. In this case, since $\langle \cos^2(\mathbf{k} \cdot \mathbf{r} - \omega t) \rangle = \frac{1}{2}$ (see Problem 3.4),

$$\langle S \rangle = \frac{c^2 \epsilon_0}{2} |\mathbf{E}_0 \times \mathbf{B}_0| \tag{3.43}$$

or

$$I \equiv \langle S \rangle = \frac{c\epsilon_0}{2} E_0^2. \tag{3.44}$$

The irradiance is therefore proportional to the square of the amplitude of the electric field. Two alternative ways of saying the same thing are simply

$$I = \frac{c}{\mu_0} \langle B^2 \rangle \tag{3.45}$$

and

$$I = \epsilon_0 c \langle E^2 \rangle. \tag{3.46}$$

Within a linear, homogeneous, isotropic dielectric, the expression for the irradiance becomes

$$I = \epsilon v \langle E^2 \rangle. \tag{3.47}$$

Since, as we have seen, **E** is considerably more effective at exerting forces and doing work on charges than is **B**, we shall refer to **E** as the *optical field* and use Eq. (3.46) almost exclusively.

The time rate of flow of radiant energy is the power or *radiant flux*, generally expressed in watts. If we divide the radiant flux incident on or exiting from a surface by the area of the surface, we have the *radiant flux density* (W/m^2). In the former case, we speak of the *irradiance*, in the latter the *exitance*, and in either instance the *flux density*. The irradiance is a measure of the *concentration* of power. Whether recorded by a photograph or a meter, it is the primary practical quantity corresponding to the "amount" of light flowing.

There are detectors, like the photomultiplier, that serve as *photon counters*. Each quantum of the electromagnetic field, having a frequency ν, represents an energy $h\nu$ (Planck's constant, $h = 6.625 \times 10^{-34}$ J s). If we have a uniform monochromatic beam of frequency ν, the quantity $I/h\nu$ is the average number of photons crossing a unit area (normal to the beam) per unit time, namely, the *photon flux density*. Were such a beam to impinge on a counter having an area A, then $AI/h\nu$ would be the incident *photon flux*, that is, the average number of photons arriving per unit of time.

We saw earlier that the spherical wave solution of the differential wave equation has an amplitude that varies inversely with r. Let's now examine this same feature within the context of energy conservation. Consider an isotropic point source in free space, emitting energy equally in all directions (i.e., emitting spherical waves). Surround the source with two concentric imaginary spherical surfaces of radii r_1 and r_2, as shown in Fig. 3.12. Let $E_0(r_1)$ and $E_0(r_2)$ represent the amplitudes of the waves over the first and second surfaces, respectively. If energy is to be conserved, the total amount of energy flowing through each surface per second must be equal, since there are no other sources or sinks present. Multiplying I by the surface area and taking the square root, we get

$$r_1 E_0(r_1) = r_2 E_0(r_2).$$

* In the past physicists generally used the word *intensity* to mean the flow of *energy per unit area per unit time*. By international, if not universal, agreement, that term is slowly being replaced in optics by the word *irradiance*.

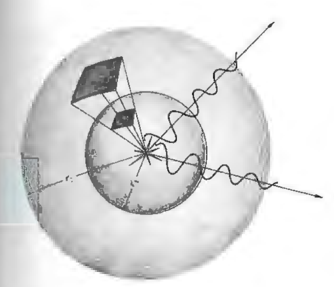


Figure 3.12 The geometry of the inverse square law.

Inasmuch as r_1 and r_2 are arbitrary, it follows that

$$rE_0(r) = \text{constant},$$

and the amplitude must drop off inversely with r. The irradiance from a point source is proportional to $1/r^2$. This is the well-known *inverse-square law*, which is easily verified with a point source and a photographic exposure meter. Notice that if we envision a beam of photons streaming radially out from the source, the same result clearly obtains.

3.3.2 Radiation Pressure and Momentum

As long ago as 1619 Johannes Kepler proposed that it was the pressure of sunlight that blew back a comet's tail so that it always pointed away from the Sun. That argument particularly appealed to the later proponents of the corpuscular theory of light. After all, they envisioned a beam of light as a stream of particles, and such a stream would obviously exert a force as it bombarded matter. For a while it seemed as though this effect might at last establish the superiority of the corpuscular over the wave theory, but all the experimental efforts to that end failed to detect the force of radiation, and interest slowly waned.

Ironically, it was Maxwell in 1873 who revived the subject by establishing theoretically that waves do indeed exert pressure. "In a medium in which waves are propagated," wrote Maxwell, "there is a pressure in the direction normal to the waves, and numerically equal to the energy in a unit of volume."

When an electromagnetic wave impinges on some material surface, it interacts with the charges that constitute bulk matter. Regardless of whether the wave is partially absorbed or reflected, it exerts a force on those charges and hence on the surface itself. For example, in the case of a good conductor, the wave's electric field generates currents, and its magnetic field generates forces on those currents.

It's possible to compute the resulting force via classical electromagnetic theory, whereupon Newton's second law (which maintains that force equals the time rate of change of momentum) suggests that the *wave itself carries momentum*. Indeed, whenever we have a flow of energy, it's reasonable to expect that there will be an associated momentum—the two are the related time and space aspects of motion.

As Maxwell showed, the **radiation pressure**, $\mathcal{P}$, equals the energy density of the electromagnetic wave. From Eqs. (3.31) and (3.32), for a vacuum, we know that

$$u_E = \frac{\epsilon_0}{2} E^2 \quad \text{and} \quad u_B = \frac{1}{2\mu_0} B^2.$$

Since $\mathcal{P} = u = u_E + u_B$,

$$\mathcal{P} = \frac{\epsilon_0}{2} E^2 + \frac{1}{2\mu_0} B^2. \tag{3.48}$$

Alternatively, using Eq. (3.37), we can express the pressure in terms of the magnitude of the Poynting vector, namely,

$$\mathcal{P} = \frac{S}{c}. \tag{3.49}$$

Notice that this equation has the units of power divided by area, divided by speed—or equivalently, force times speed divided by area and speed, or just force over area. This is the instantaneous pressure that would be exerted on a perfectly absorbing surface by a normally incident beam.

Inasmuch as the **E**- and **B**-fields are rapidly varying,

S is rapidly varying, so it's eminently practical to deal with the average radiation pressure, namely,

$$\langle \mathcal{P} \rangle = \frac{\langle S \rangle}{c} = \frac{I}{c}, \tag{3.50}$$

expressed in newtons per square meter. This same pressure is exerted on a source that itself is radiating energy.

Referring back to Fig. 3.11, if p is momentum, the force exerted by the beam on an absorbing surface is

$$A\mathcal{P} = \frac{\Delta p}{\Delta t} \tag{3.51}$$

If p_V is the *momentum per unit volume of the radiation*, then an amount of momentum $\Delta p = p_V(c\,\Delta t\,A)$ is transported to A during each time interval Δt, and

$$A\mathcal{P} = \frac{p_V(c\,\Delta t\,A)}{\Delta t} = A\frac{S}{c}.$$

Hence the volume density of electromagnetic momentum is

$$p_V = \frac{S}{c^2}. \tag{3.52}$$

When the surface under illumination is perfectly reflecting, the beam that entered with a velocity $+c$ will emerge with a velocity $-c$. This corresponds to twice the change in momentum that occurs on absorption, and hence

$$\langle \mathcal{P} \rangle = 2\frac{\langle S \rangle}{c}.$$

Notice, from Eqs. (3.49) and (3.51), that if some amount of energy $\mathcal{E}$ is transported per square meter per second, then there will be a corresponding momentum $\mathcal{E}/c$ transported per square meter per second.

In the photon picture, we envision particlelike quanta, each having an energy $\mathcal{E} = h\nu$. We can then expect a photon to carry a momentum $p = \mathcal{E}/c = h/\lambda$. Its vector momentum would be

$$\mathbf{p} = \hbar\mathbf{k}, \tag{3.53}$$

where $\mathbf{k}$ is the propagation vector and $\hbar = h/2\pi$. This all fits in rather nicely with special relativity, which relates the rest mass m_0, energy, and momentum of a particle by

$$\mathcal{E} = [(cp)^2 + (m_0c^2)^2]^{1/2}.$$

For a photon $m_0 = 0$ and $\mathcal{E} = cp$.

These quantum-mechanical ideas have been confirmed experimentally utilizing the Compton effect, which detects the energy and momentum transferred to an electron upon interaction with an individual x-ray photon.

The average flux density of electromagnetic energy from the Sun impinging normally on a surface just outside the Earth's atmosphere is about 1400 W/m^2. Assuming complete absorption, the resulting pressure would be 4.7×10^{-6} N/m^2, or 1.8×10^{-9} ounce/cm^2, as compared with, say, atmospheric pressure of about 10^5 N/m^2. The pressure of solar radiation at the Earth is tiny, but it is still responsible for a substantial planet-wide force of roughly 10 tons. Even at the very surface of the Sun, radiation pressure is relatively small (see Problem 3.19). As one might expect, it becomes appreciable within the blazing body of a large bright star, where it plays a significant part in supporting the star against gravity. Despite the modest size of the Sun's flux density, it nonetheless can produce appreciable effects over long acting times. For example, had the pressure of sunlight exerted on the Viking spacecraft during its journey been neglected, it would have missed Mars by about 15,000 km. Calculations show that it is even feasible to use the pressure of sunlight to propel a space vehicle among the inner planets.* Ships with immense reflecting sails driven by solar radiation pressure may some day ply the dark sea of local space. The pressure exerted by light was actually measured as long ago as 1901 by the Russian experimenter Pyotr Nikolaievich Lebedev (1866–1912) and independently by the Americans Ernest Fox Nichols (1869–1924) and Gordon Ferrie Hull (1870–1956). Their accomplishments were formidable, considering the light sources available at the time. Nowadays, with the advent of the laser, light can be focused down to a spot size approaching the theoretical limit of about one wavelength in radius. The resulting irradiance, and therefore the pressure is appreciable, even with a laser rated at just a few watts. It has thus become practical to consider radiation pressure for all sorts of applications, such as separating isotopes, accelerating particles, and even optically levitating small objects (Fig. 3.13).

* The charged-particle flux called the "solar wind" is 1000 to 100,000 times less effective in providing a propulsive force than is sunlight.

Figure 3.13 The tiny starlike speck is a minute (one-thousandth of an inch diameter) transparent glass sphere suspended in midair on an upward 250 mW laserbeam. (Photo courtesy Bell Laboratories.)

Light can also transport angular momentum, but this will certainly not happen with a linearly polarized wave. Accordingly, we shall defer this rather important discussion to Chapter 8, in which circular polarization is examined.

3.4 RADIATION

Although all forms of electromagnetic radiation propagate with the same speed in vacuum, they nontheless differ in frequency and wavelength. As we will see presently, that difference accounts for the diversity of behavior observed when radiant energy interacts with matter. Even so, there is only one entity, one essence of electromagnetic wave. Maxwell's equations are independent of wavelength and so suggest no fundamental differences in kind. Accordingly, it is reasonable to look for a common source-mechanism for all radiation. What we find is that the various types of radiant energy seem to have a common origin in that they are all associated somehow with *nonuniformly moving charges*. We are, of course, dealing with waves in the electromagnetic field, and charge *is* that which gives rise to field, so this is not altogether surprising.

A stationary charge has a constant **E**-field, no **B**-field, and hence produces no radiation—where would the energy come from if it did? A uniformly moving charge has both an **E**- and a **B**-field, but it does not radiate. If you traveled along with the charge, the current would thereupon vanish, hence **B** would vanish, and we would be back at the previous case, uniform motion being relative. That's reasonable, since it would make no sense at all if the charge stopped radiating just because you started walking along next to it. That leaves *nonuniformly moving charges*, which assuredly do radiate. In the photon picture this is underscored by the conviction that the fundamental interactions between matter and radiant energy are between photons and charges.

We know in general that free charges (those not bound within an atom) emit electromagnetic radiation when accelerated. That much is true for charges changing speed along a straight line within a linear accelerator, sailing around in circles inside a cyclotron, or simply oscillating back and forth in a radio antenna—**if a charge moves nonuniformly, it radiates**. A free charged particle can spontaneously absorb or emit a photon, and an increasing number of important devices, ranging from the free-electron laser (1977) to the synchrotron radiation generator, utilize this mechanism on a practical level.

3.4.1 Linearly Accelerating Charges

At constant speed the charge essentially has attached to it an unchanging radial electric field and a surrounding circular magnetic field. Although at any stationary point in space the **E**-field changes from moment to

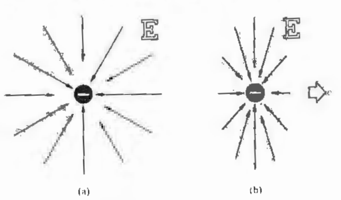


Figure 3.14 (a) Electric field of a stationary electron. (b) Electric field of a moving electron.

moment, at any instant its value can be determined by supposing that the field lines move along, fixed to the charge. Thus the field does not disengage from the charge, and there is no radiation.

The electric field of a charge at rest can be represented, as in Fig. 3.14, by a uniform, radial distribution of straight *field lines*, or *lines of force*. For a charge moving at a constant velocity **v**, the field lines are still radial and straight, but they are no longer uniformly distributed. The nonuniformity becomes evident at high speeds and is usually negligible when $v \ll c$.

In contrast, Fig. 3.15 shows the field lines associated with an electron accelerating uniformly to the right. The points O_1, O_2, O_3, and O_4 are the positions of the electron after equal time intervals. The field lines are now curved, and this, as we shall see, is a significant difference. As a further contrast, Fig. 3.16 depicts the field of an electron at some arbitrary time t_2. Before $t = 0$ the particle was always at rest at the point O. The charge was then uniformly accelerated until time t_1, reaching a speed v, which was maintained constant thereafter. We can anticipate that the surrounding field lines will somehow carry the information that the electron has accelerated. We have ample reason to assume that this "information" will propagate at the speed c. If, for example, $t_2 = 10^{-8}$ s, no point beyond 3 m from O would be aware of the fact that the charge had even moved. All the lines in that region would be uniform, straight, and centered on O, as if the charge were still

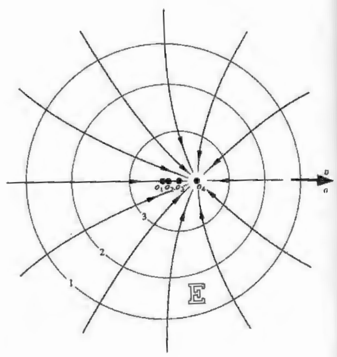


Figure 3.15 Electric field of a uniformly accelerating electron.

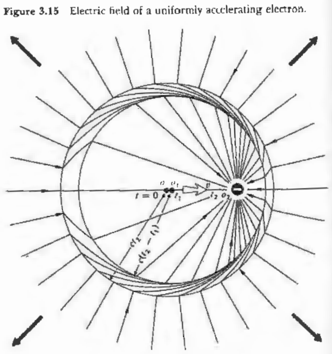


Figure 3.16 A kink in the E-field lines.

there. At time t_2 the electron is at point O_2, and it is moving with a constant speed v. In the vicinity of O_2 the field lines must then resemble those in Fig. 3.14(b). Gauss's law requires that the lines outside the sphere of radius ct_2 connect to those within the sphere of radius $c(t_2 - t_1)$, since there are no charges between them. It is now apparent that during the interval when the particle accelerated, the field lines became distorted and a kink appeared. The exact shape of the lines within the region of the kink is of little interest here. What is significant is that there now exists a *transverse component* of the electric field $\mathbf{E}_T$, which propagates outward as a pulse. At some point in space the transverse electric field will be a function of time, and it will therefore be accompanied by a magnetic field.

The radial component of the electric field drops off as $1/r^2$, while the transverse component goes as $1/r$. At large distances from the charge the only significant field will be the $\mathbf{E}_T$-component of the pulse, which is known as the *radiation field*.* For a positive charge moving slowly ($v \ll c$), the electric and magnetic radiation fields can be shown to be proportional to $\mathbf{r} \times (\mathbf{r} \times \mathbf{a})$ and $(\mathbf{a} \times \mathbf{r})$, respectively, where **a** is the acceleration. For a negative charge the reverse occurs, as shown in Fig. 3.17. Observe that the irradiance is a function of θ and that $I(0) = I(180°) = 0$ while $I(90°) = I(270°)$ is a maximum.

The energy that is radiated out into the surrounding space is supplied to the charge by some external agent. That agent is responsible for the accelerating force, which in turn does work on the charge.

3.4.2 Synchrotron Radiation

A free charged particle traveling on any sort of curved path is accelerating and so will radiate. This behavior provides a powerful mechanism for producing radiant energy, both naturally and in the laboratory. The *synchrotron radiation generator*, one of the most exciting research tools to be developed in the 1970s, does just that. Clumps of charged particles, usually electrons or positrons, interacting with an applied magnetic field are made to revolve around a large, essentially circular track at a precisely controlled speed. The frequency of the orbit determines the frequency of the emission (which also contains higher harmonics), and that is continuously variable, more or less, as desired.

*The details of this calculation using J. J. Thomson's method of analyzing the kink can be found in J. R. Tessman and J. T. Finnell, Jr. "Electric Field of an Accelerating Charge." *Am. J. Phys.* 35, 523 (1967). As a general reference for radiation, see, for example, Marion and Heald, *Classical Electromagnetic Radiation*, Chapter 7.

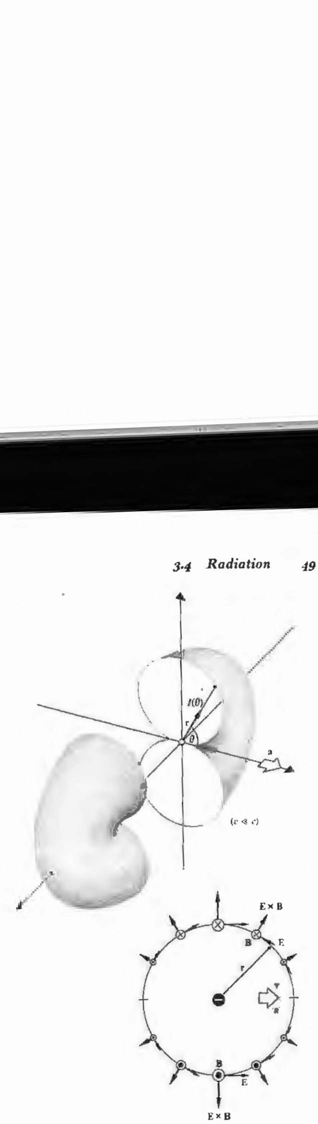


Figure 3.17 The toroidal radiation pattern of a linearly accelerating charge (split to show cross section).

A charged particle slowly revolving in a circular orbit radiates a doughnut-shaped pattern similar to the one depicted in Fig. 3.17. Again the distribution of radiation is symmetrical around **a**, which is now the centripetal acceleration acting inward along the radius drawn from the center of the circular orbit to the charge. The higher the speed, the more an observer at rest in the laboratory will "see" the backward lobe of the radiation pattern shrink while the forward lobe elongates in the direction of motion. At speeds approaching c, the particle beam (usually with a diameter comparable to that of a straight pin) radiates essentially along a narrow cone pointing tangent to the orbit in the instantaneous direction of **v** (Fig. 3.18). For $v \approx c$ the radiation will be very strongly polarized in the plane of the motion.

This "searchlight," often less than a few millimeters in diameter, sweeps around as the particle clumps circle the machine, much like the headlight on a train rounding a turn. With each revolution the beam momentarily ($<\frac{1}{2}$ ns) flashes through one of many windows in the device. The result is a tremendously intense source of rapidly pulsating radiation, tunable over a very broad range of frequencies, from infrared to light to x-rays. When magnets are used to make the circulating electrons wiggle in and out of their circular orbits, bursts of high-frequency x-rays of unparalleled intensity can be created. These beams, which are hundreds of thousands of times more powerful than a dental x-ray emission of a fraction of a watt, can easily burn a finger-sized hole through a 3-mm-thick lead plate.

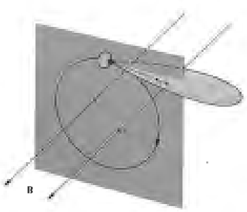


Figure 3.18 Radiation pattern for an orbiting charge.

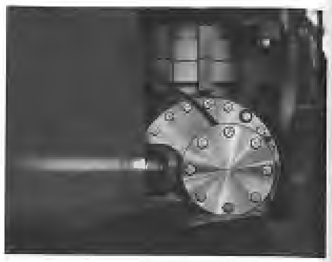


Figure 3.19 The first beam of light from the National Synchrotron Light Source (1982) emanating from its ultraviolet electron storage ring.

Though this technique was first used to produce light in an electron synchrotron as long ago as 1947, it took several decades to recognize that what was an energy-robbing nuisance to the accelerator people might be a major research tool in itself (Fig. 3.19).

In the astronomical realm, we can expect that some regions exist that are pervaded by magnetic induction fields. Charged particles trapped in these fields will move in circular or helical orbits, and if their speeds are high enough, they will emit synchrotron radiation. Figure 3.20 shows five photographs of the extragalactic Crab Nebula.* Radiation emanating from the nebula extends over the range from radio frequencies to the extreme ultraviolet. If we assume the source to be trapped circulating charges, we can anticipate strong polarization effects. These are evident in the first four photographs, which were taken through a polarizing filter. The direction of the electric field vector is indicated in each picture. Since in synchrotron radiation, the emitted **E**-field is polarized in the orbital plane, we can conclude that each photograph corresponds to a particular uniform magnetic field orientation normal to the orbits and to **E**.

It is believed that a majority of the low-frequency radiowaves reaching the Earth from outer space have their origin in synchrotron radiation. In 1960 radio

* The Crab Nebula is believed to be expanding debris left over after the cataclysmic death of a star. From its rate of expansion, astronomers calculated that the explosion took place in 1050 A.D. This was subsequently corroborated when a study of old Chinese records (the chronicles of the Peiping Observatory) revealed the appearance of an extremely bright star, in the same region of the sky, in the year 1054 A.D.

> In the first year of the period Chihha, the fifth moon, the day Chi-chou [i.e., July 4, 1054], a great star appeared .... After more than a year, it gradually became invisible.

There is little doubt that the Crab Nebula is the remnant of that supernova.

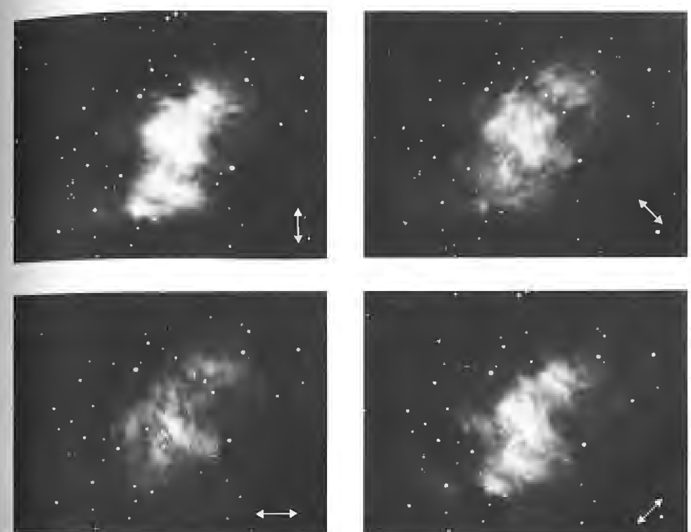


Figure 3.20(a) Synchrotron radiation arising from the Crab Nebula. In these photos only light whose **E**-field direction is as indicated was recorded. (Photos courtesy Mt. Wilson and Palomar Observatories.)

Figure 3.20(b) The Crab Nebula in unpolarized light.

astronomers used these long-wavelength emissions to identify the new class of objects known as quasars. In 1955 bursts of polarized radiowaves were discovered emanating from Jupiter. Their origin is now attributed to spiraling electrons trapped in radiation belts surrounding the planet.

3.4.3 Electric Dipole Radiation

Perhaps the simplest electromagnetic wave-producing mechanism to visualize is the oscillating dipole—two charges, one plus and one minus, vibrating to and fro along a straight line. And yet this arrangement is surely the most important of all.

Both light and ultraviolet radiation arise primarily from the rearrangement of the outermost, or weakly bound, electrons in atoms and molecules. It follows from the quantum-mechanical analysis that the electric dipole moment of the atom is the major source of this radiation. The rate of energy emission from a material system, although a quantum-mechanical process, can be envisioned in terms of the classical oscillating electric dipole. This mechanism is therefore of considerable importance in understanding the manner in which atoms, molecules, and even nuclei emit and absorb electromagnetic waves. It will be of particular interest when we study the interaction of light with matter.

We shall again simply use the results of a lengthy and rather complicated derivation. Figure 3.21 schematically depicts the electric field distribution in the region of an electric dipole. In this configuration, a negative charge oscillates linearly in simple harmonic motion about an equal stationary positive charge. If the angular frequency of the oscillation is ω, the time-dependent dipole moment $\wp(t)$ has the scalar form

$$\wp = \wp_0 \cos \omega t. \tag{3.54}$$

Note that $\wp(t)$ could represent the collective moment of the oscillating charge distribution on the atomic scale or even an oscillating current in a linear television antenna.

At $t = 0$, $\wp = \wp_0 = qd$, where d is the initial maximum separation between the centers of the two charges (Fig. 3.21a). The dipole moment is actually a vector in the direction from $-q$ to $+q$. The figure shows a sequence of field line patterns as the displacement, and therefore the dipole moment decreases, then goes to zero, and finally reverses direction. When the charges effectively overlap, $\wp = 0$ and the field lines must close on themselves.

Very near the atom, the **E**-field has the form of a static electric dipole. A bit farther out, in the region where the closed loops form, there is no specific wavelength. The detailed treatment shows that the electric field is composed of five different terms, and things are obviously complicated. Far from the dipole, in what is called the *wave* or *radiation zone*, the field configuration is particularly simple. In this zone a fixed wavelength has been established; **E** and **B** are transverse, mutually perpendicular, and in phase. Specifically,

$$E = \frac{\wp_0 k^2 \sin\theta}{4\pi\epsilon_0} \frac{\cos(kr - \omega t)}{r} \tag{3.55}$$

and $B = E/c$, where the fields are oriented as in Fig. 3.22. The Poynting vector $\mathbf{S} = \mathbf{E} \times \mathbf{B}/\mu_0$ always points radially outward in the wave zone. There, the **B**-field lines are circles concentric with, and in a plane perpendicular to, the dipole axis. This is understandable, since **B** can be considered to arise from the time-varying oscillator current.

The irradiance (radiated radially outward from the source) follows from Eq. (3.44) and is given by

$$I(\theta) = \frac{\wp_0^2 \omega^4}{32\pi^2 c^3 \epsilon_0} \frac{\sin^2\theta}{r^2}, \tag{3.56}$$

again an inverse square law dependence on distance.

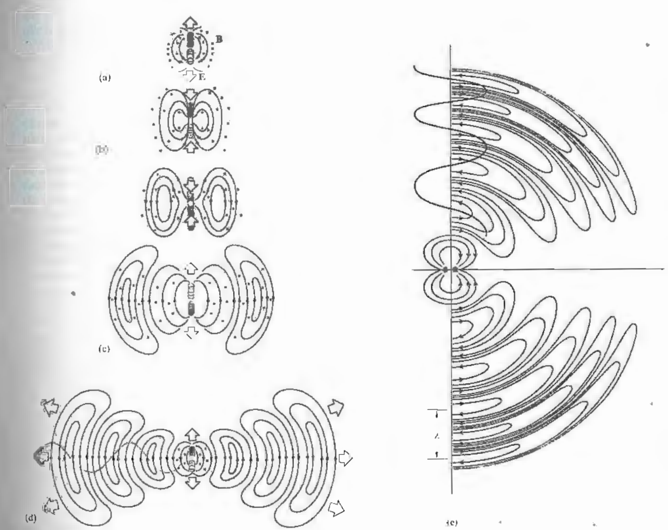


Figure 3.21 The E-field of an oscillating electric dipole.

The angular flux density distribution is toroidal, as in Fig. 3.17. The axis along which the acceleration takes place is the symmetry axis of the radiation pattern. Notice the dependence of the irradiance on ω^4—the higher the frequency, the stronger the radiation; that feature will be important when we consider scattering.

It's not difficult to attach an AC generator between two conducting rods and thereby send currents of free electrons oscillating up and down that "transmitting

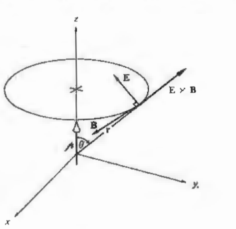


Figure 3.22 Field orientations for an oscillating electric dipole.

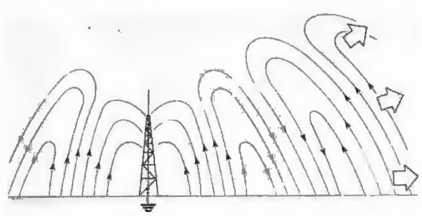


Figure 3.23 Electromagnetic waves from a transmitting tower.

antenna." Figure 3.23 shows the arrangement carried to its logical conclusion—a fairly standard AM radio tower. An antenna of this sort will function most efficiently if its length corresponds to the wavelength being transmitted or, more conveniently, to $\frac{1}{2}\lambda$. The wave being radiated is then formed at the dipole in synchronization with the oscillating current producing it. AM radiowaves are unfortunately several hundred meters long. Consequently, the antenna shown in the figure has half the $\frac{1}{2}\lambda$-dipole essentially buried in the earth. That at least saves some height, allowing us to build the device only $\frac{1}{4}\lambda$ tall. Moreover, this use of the Earth also generates a so-called *ground wave* that hugs the planet's surface, where most people with radios are likely to be located. A commercial station usually has a range somewhere between 25 and 100 miles.

3.4.4 Atoms and Light

Surely the most significant mechanism responsible for the natural emission and absorption of radiant energy—especially of light—is the *bound charge*, electrons confined within atoms. These minute negative particles, which surround the massive positive nucleus of each atom, constitute a kind of distant, tenuous charged cloud. Much of the chemical and optical behavior of ordinary matter is determined by its outer or valence electrons. The remainder of the cloud is ordinarily formed into "closed," essentially unresponsive, shells around and tightly bound to the nucleus. These closed or filled shells are made up of specific numbers of electron pairs. Even though it is not completely clear what occurs internally when an atom radiates, we do know with some certainty that light is emitted during readjustments in the outer charge distribution of the electron cloud. This mechanism is ultimately the predominant source of light in the world.

Usually, an atom exists with its clutch of electrons arranged in some stable configuration that corresponds to their lowest energy distribution or *level*. Every electron is in the lowest possible energy state available to it, and the atom as a whole is in its so called **ground state** configuration. There it will likely remain indefinitely, if left undisturbed. Any mechanism that pumps energy into the atom will alter the ground state. For instance, a collision with another atom, an electron, or a photon can affect the atom's energy state profoundly. According to quantum-mechanical theory, an atom can exist with its electron cloud in only certain specific configurations corresponding to only certain values of energy. In addition to the ground state, there are higher energy levels, the so-called *excited states*, each associated with a specific cloud configuration and a specific well-defined energy. When one or more electrons occupies a level higher than its ground-state level, the atom is said to be excited—a condition that is inherently unstable and temporary.

At low temperatures, atoms tend to be in their ground state; at progressively higher temperatures, more and more of them will become excited through atomic collisions. This sort of mechanism is indicative of a class of relatively gentle excitations—glow discharge, flame, spark, and so forth—which energize only the outermost unpaired valence electrons. We will initially concentrate on these outer electron transitions, which give rise to the emission of light, and the nearby infrared and ultraviolet.

When enough energy is imparted to an atom (typically to the valence electron), whatever the cause, the atom can react by suddenly ascending from a lower to a higher energy level. The electron will usually make a very rapid transition, a *quantum jump*, from its ground-state orbital configuration to one of the well-delineated excited states, one of the quantized rungs on its energy ladder. As a rule, the amount of energy taken up in the process equals the energy difference between the initial and final states, and since that is specific and well defined, the amount of energy that can be absorbed by an atom is quantized (i.e., limited to specific amounts). This state of atomic excitation is a short-lived resonance phenomenon. Usually, after about 10^{-8} or 10^{-9} s, the excited atom spontaneously relaxes back to a lower state, most often the ground state, losing the excitation energy along the way. This energy readjustment can occur by way of the emission of light or (especially in dense materials) by conversion to thermal energy through interatomic collisions within the medium.

If the atomic transition is accompanied by the emission of light (as it is in a rarefied gas; see Section 13.7), the energy of the photon exactly matches the quantized energy decrease of the atom. That corresponds to a specific frequency, by way of $\Delta\mathscr{E} = h\nu$, a frequency associated with both the photon and the atomic transition between the two particular states. This is said to be a *resonance frequency*, one of several (each with its own likelihood of occurring) at which the atom very efficiently absorbs and emits energy. The atom radiates a quantum of energy that presumably is created spontaneously, on the spot, by the shifting electron.

Even though what occurs during that interval of 10^{-8} s is far from clear, it can be helpful to imagine the orbital electron somehow making its downward energy transition via a gradually damped oscillatory motion at the specific resonance frequency. The radiated light can then be envisioned in a semiclassical way as emitted in a short oscillatory pulse, or wavetrain, lasting less than roughly 10^{-8} s—a picture that is in agreement with experimental observation (see Section 7.10, Fig. 7.19). It is useful to think of this electromagnetic pulse as associated in some inextricable fashion with the photon. In a way, the pulse is a semiclassical representation of the manifest wave nature of the photon. But the two are *not* equivalent in all respects: the electromagnetic wavetrain is a classical creation that can be used to describe the propagation and spatial distribution of light extremely well, yet its energy is not quantized, not localized, and that is an essential characteristic of the photon (see Chapter 13). So when we talk about photon wavetrains keep in mind that there is more to the notion than just a classical oscillatory pulse of electromagnetic wave.

The emission spectra of single atoms or low-pressure gases, whose atoms do not interact appreciably, consist of sharp "lines," that is, fairly well-defined frequencies characteristic of the atoms. There is always some frequency broadening (see Section 7.10) of that radiation due to atomic motion, collisions, and so forth, so it's never precisely monochromatic (i.e., a single color or frequency). Generally, however, the atomic transition from one level to another is characterized by the emission of a well-defined narrow range of frequencies. On the other hand, the spectra of solids and liquids, in which the atoms are now interacting with one another, is broadened into wide frequency bands. When two atoms are brought close together, the result is a slight shift in their respective energy levels, because they act upon each other. The many interacting atoms in a solid create a tremendous number of such shifted levels, in effect spreading out each of their original levels, blurring them into essentially continuous bands. Materials of this nature emit and absorb over broad ranges of frequencies.

Light emitted from a large assemblage of randomly oriented independent atoms will consist of wavetrains in all directions. Each one of these will bear no particular consistent phase relation with any of the others, nor will they share a common polarization. This is in marked contrast to the continuous, polarized, extended wavetrains generated by sustained current oscillations in a transmitting antenna (Fig. 3.23). Even in that case, however, the radiation is not truly monochromatic. The simple harmonic functions containing only one frequency are idealizations—at times reasonable ones, but idealizations nonetheless. Before switching on even a perfect generator, the radiation will obviously have been zero. Yet a harmonic function has no such limitations on its time dependence and clearly cannot, by itself, represent such a wave. If the generator has been on for a long enough time, the wave it emits will be, at best, nearly monochromatic or **quasimonochromatic**. For many applications, laser light or light passed through a narrow band filter can be adequately represented by a single harmonic function. Even so, since it is not possible to produce monochromatic radiation, the term can be used only loosely, and this point must be borne in mind.

3.5 LIGHT IN MATTER

The response of dielectric or nonconducting materials to electromagnetic fields is of special concern to us in optics. We will, of course, be dealing with transparent dielectrics in the form of lenses, prisms, plates, films, and so forth, not to mention the surrounding sea of air.

The net effect of introducing a homogeneous, isotropic dielectric into a region of free space is to change ϵ_0 to ϵ and μ_0 to μ in Maxwell's equations. The phase velocity in the medium now becomes

$$v = 1/\sqrt{\epsilon\mu}. \tag{3.57}$$

The ratio of the speed of an electromagnetic wave in vacuum to that in matter is known as the **absolute index of refraction** n and is given by

$$n = \frac{c}{v} = \sqrt{\frac{\epsilon\mu}{\epsilon_0\mu_0}} \tag{3.58}$$

In terms of the relative permittivity and relative permeability of the medium, n becomes

$$n = \sqrt{K_e K_m}. \tag{3.59}$$

The great majority of substances, with the exception of ferromagnetic materials, are only weakly magnetic; none is actually nonmagnetic. Even so, K_m generally doesn't deviate from 1 by any more than a few parts in 10^4 (e.g., for diamond $K_m = 1 - 2.2 \times 10^{-5}$). Setting $K_m = 1$ in the formula for n results in an expression known as *Maxwell's relation*, namely,

$$n = \sqrt{K_e}, \tag{3.60}$$

wherein K_e is presumed to be the *static dielectric constant*. As indicated in Table 3.1, this relationship seems to work well only for some simple gases. The difficulty arises because K_e and therefore n are actually *frequency-dependent*. The dependence of n on the wavelength (or color) of light is a well-known effect called *dispersion*. Indeed, Sir Isaac Newton used prisms to disperse white light into its constituent colors over three hundred years ago, and the phenomenon was well known if not well understood even then.

There are two interrelated questions that come to mind at this point: (1) What is the physical basis for the frequency dependence of n? and (2) What is the mechanism whereby the phase velocity in the medium is effectively made different from c? The answers to both these questions can be found by examining the interaction of an incident electromagnetic wave with the array of atoms constituting a dielectric material. An atom can react to incoming light in two different ways, depending on the incident frequency or equivalently on the incoming photon energy ($\mathscr{E} = h\nu$). Generally the atom will "scatter" the light, redirecting it without otherwise altering it. On the other hand, if the photon's energy matches that of one of the excited states, the atom will "absorb" the light, making a quantum jump to that higher energy level. In the dense atomic landscape of ordinary gases (at pressures of about 10^2 Pa and up), solids, and liquids, it's very likely that this excitation energy will rapidly be transferred, via collisions, to random atomic motion, thermal energy, before a photon can be emitted. This commonplace process (the taking up of a photon and its conversion into thermal energy) was at one time widely known as "absorption," but nowadays that word is more often used to refer just to the "taking up" aspect, regardless of what then happens to the energy. Consequently, it's now better referred to as *dissipative absorption*.

Table 3.1 Maxwell's relation.

Gases at 0°C and 1 atm		
Substance	$\sqrt{K_e}$	n
Air	1.000294	1.000293
Helium	1.000034	1.000036
Hydrogen	1.000131	1.000132
Carbon dioxide	1.00049	1.00045
Liquids at 20°C		
Substance	$\sqrt{K_e}$	n
Benzene	1.51	1.501
Water	8.96	1.333
Ethyl alcohol (ethanol)	5.08	1.361
Carbon tetrachloride	4.63	1.461
Carbon disulfide	5.04	1.628
Solids at room temp		
Substance	$\sqrt{K_e}$	n
Diamond	4.06	2.419
Amber	1.6	1.55
Fused silica	1.94	1.458
Sodium chloride	2.37	1.50

Values of K_e correspond to the lowest possible frequencies, in some cases as low as 60 Hz, whereas n is measured at about 0.5×10^{15} Hz. Sodium D light was used ($\lambda = 589.29$ nm)

In contrast to this excitation process, *ground-state* or **nonresonant scattering** occurs with incoming radiant energy of other frequencies—that is, other than resonance frequencies (see Section 13.7). Imagine an atom in its lowest state and suppose that it interacts with a photon whose energy is too small to a cause a transition to any of the higher, excited states. Despite that, the electromagnetic field of the light can be supposed to drive the electron cloud into oscillation. There is no resulting atomic transition; the atom remains in its ground state while the cloud vibrates ever so slightly at the frequency of the incident light. Once the electron cloud starts to vibrate with respect to the positive nucleus, the system constitutes an oscillating dipole and will presumably immediately begin to radiate at that same frequency. The resulting scattered light consists of a photon that sails off in some direction carrying the same amount of energy as did the incident photon—the scattering is elastic. In effect, we are supposing that the atom resembles a little dipole oscillator, a model employed by Hendrik Antoon Lorentz (1878) with remarkable success.

When an atom is in an active environment, the process of excitation and spontaneous emission is rapidly repeated. In fact, with an emission lifetime of $\approx 10^{-8}$ s an atom could spontaneously emit upward of 10^8 photons per second in a situation in which there was enough energy to keep reexciting it. Atoms have a very strong tendency to interact with resonant light (they have a large *absorption cross-section*). This means that the saturation condition, in which the atoms of a low-pressure gas are constantly emitting and being re-excited, occurs at a modest value of irradiance ($\approx 10^2$ W/m^2). So it's not very difficult to get atoms firing out photons at a rate of 100 million per second.

Generally, we can imagine that in a medium illuminated by an ordinary beam of light, each atom behaves as though it was a "source" of a tremendous number of photons (scattered either elastically or resonantly) that fly off in all directions. A stream of energy like this resembles a classical spherical wave. Thus we imagine an atom (even though it is simplistic to do so) as a point source of spherical electromagnetic wavetrains—provided we keep in mind Einstein's admonition that "outgoing radiation in the form of spherical waves does not exist."

When a material with no resonances in the visible is bathed in light, nonresonant scattering occurs and it gives each participating atom the appearance of being a tiny source of spherical wavelets. As a rule, the closer the frequency of the incident beam is to an atomic resonance, the more strongly will the interaction occur and, in dense materials, the more energy will be dissipatively absorbed. It is precisely this mechanism of selective absorption (see Section 4.4) that creates much of the visual appearance of things. It is primarily responsible for the color of your hair, skin, and clothing, the color of leaves and apples and paint.

3.5.1 Dispersion

Maxwell's theory treats matter as continuous, representing its electric and magnetic responses to applied **E**- and **B**-fields in terms of constants, ϵ and μ. Consequently, K_e and K_m are also constant, and n is therefore unrealistically independent of frequency. To deal theoretically with dispersion, the well-known frequency dependence of the refractive index, it is necessary to incorporate the atomic nature of matter and, obviously, to exploit some frequency-dependent aspect of that nature. Following H. A. Lorentz, we can then average the contributions of large numbers of atoms to represent the behavior of an isotropic dielectric medium.

When a dielectric is subjected to an applied electric field, the internal charge distribution is distorted under its influence. This corresponds to the generation of electric dipole moments, which in turn contribute to the total internal field. More simply stated, the external field separates positive and negative charges in the medium (each pair of which is a dipole), and these then contribute an additional field component. The resultant dipole moment per unit volume is called the *electric polarization* **P**. For most materials **P** and **E** are proportional and can satisfactorily be related by

$$(\epsilon - \epsilon_0)\mathbf{E} = \mathbf{P}. \qquad (3.61)$$

The redistribution of charge and the consequent polarization can occur by the following mechanisms. There are molecules that have a permanent dipole moment as a result of unequal sharing of valence electrons. These are known as *polar molecules;* the nonlinear water molecule is a fairly typical example (Fig. 3.24). Each hydrogen–oxygen bond is polar covalent, with the H-end positive with respect to the O-end. Thermal agitation keeps the molecular dipoles randomly oriented. With the introduction of an electric field, the dipoles align themselves, and the dielectric takes on an *orientational polarization*. In the case of *nonpolar molecules* and *atoms*, the applied field distorts the electron cloud, shifting it relative to the nucleus and thereby producing a dipole moment. In addition to this *electronic polarization*, there is another process that is applicable specifically to molecules, for example, the ionic crystal NaCl. In the presence of an electric field, the positive and negative ions undergo a shift with respect to each other. Dipole moments are therefore induced, resulting in what is called *ionic* or *atomic polarization*.

If the dielectric is subjected to an incident harmonic electromagnetic wave, its internal charge structure will experience time-varying forces and/or torques. These will be proportional to the electric field component of

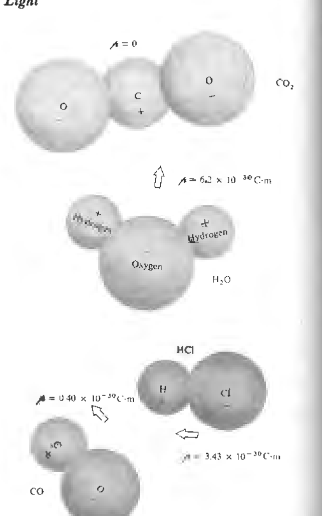


Figure 3.24 Assorted molecules and their dipole moments.

the wave.* For polar dielectrics the molecules actually undergo rapid rotations, aligning themselves with the $\mathbf{E}(t)$-field. But these molecules are relatively large and have appreciable moments of inertia. At high driving frequencies ω, polar molecules will be unable to follow

* Forces arising from the magnetic component of the field have the form $\mathbf{F}_M = q\mathbf{v} \times \mathbf{B}$ in comparison to $\mathbf{F}_E = q\mathbf{E}$ for the electric component; but $v \ll c$, so it follows from Eq. (3.30) that $\mathbf{F}_M$ is generally negligible.

the field alternations. Their contributions to **P** will decrease, and K_e will drop markedly. The relative permittivity of water is fairly constant at approximately 80, up to about 10^{10} Hz, after which it falls off quite rapidly. In contrast, electrons have little inertia and can continue to follow the field contributing to $K_e(\omega)$ even at optical frequencies (of about 5×10^{14} Hz). Thus the dependence of n on ω is governed by the interplay of the various electric polarization mechanisms contributing at the particular frequency. With this in mind, it is possible to derive an analytical expression for $n(\omega)$ in terms of what's happening within the medium on an atomic level.

The electron cloud of the atom is bound to the positive nucleus by an attractive electric force that sustains it in some sort of equilibrium configuration. Without knowing much more about the details of all the internal atomic interactions, we can anticipate that, like other stable mechanical systems which are not totally disrupted by small perturbations, a net force, F, must exist that returns the system to equilibrium. Moreover, we can reasonably expect that for very small displacements, x, from equilibrium (where $F = 0$), the force will be linear in x. In other words, a plot of $F(x)$ versus x will cross the x-axis at the equilibrium point ($x = 0$) and will be a straight line very close on either side. Thus for small displacements it can be supposed that the restoring force has the form $F = -kx$. Once somehow momentarily disturbed, an electron bound in this way will oscillate about its equilibrium position with a *natural* or **resonant** frequency given by $\omega_0 = \sqrt{k/m_e}$, where m_e is its mass. This is the oscillatory frequency of the *undriven* system.

A material medium is envisioned as an assemblage, in vacuum, of a very great many polarizable atoms, each of which is small (by comparison to the wavelength of light) and close to its neighbors. When a lightwave impinges on such a medium, each atom can be thought of as a classical *forced* oscillator being driven by the time-varying electric field $E(t)$ of the wave, which is assumed here to be applied in the x-direction. Figure 3.25(b) is a mechanical representation of just such an oscillator in an *isotropic medium* where the negatively charged shell is fastened to a stationary positive nucleus by identical springs. Even under the illumination of bright sunlight, the amplitude of the oscillations will be no greater than about 10^{-17} m. The force (F_E) exerted on an electron of charge q_e by the $E(t)$ field of a harmonic wave of frequency ω is of the form

$$F_E = q_e E(t) = q_e E_0 \cos \omega t. \qquad (3.62)$$

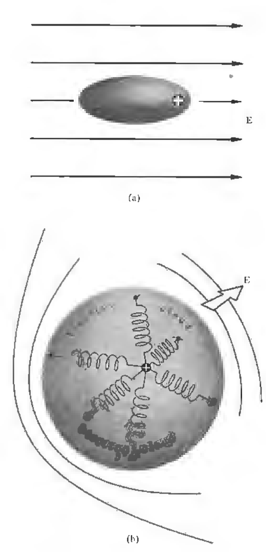


Figure 3.25 (a) Distortion of the electron cloud in response to an applied **E**-field. (b) The mechanical oscillator model for an isotropic medium—all the springs are the same, and the oscillator can vibrate equally in all directions.

Consequently, Newton's second law provides the equation of motion; that is, the sum of the forces equals the mass times the acceleration:

$$q_e E_0 \cos \omega t - m_e \omega_0^2 x = m_e \frac{d^2 x}{dt^2}. \tag{3.63}$$

The first term on the left is the driving force, the second is the opposing restoring force. To satisfy this expression, x will have to be a function whose second derivative isn't very much different from x itself. Furthermore we can anticipate that the electron will oscillate at the same frequency as $E(t)$, so we "guess" at the solution

$$x(t) = x_0 \cos \omega t$$

and substitute it in the equation to evaluate the amplitude x_0. In this way we find that

$$x(t) = \frac{q_e/m_e}{(\omega_0^2 - \omega^2)} E_0 \cos \omega t \tag{3.64}$$

or

$$x(t) = \frac{q_e/m_e}{(\omega_0^2 - \omega^2)} E(t). \tag{3.65}$$

This is the relative displacement between the negative cloud and the positive nucleus. It's traditional to leave q_e positive and speak about the displacement of the oscillator. Without a driving force (no incident wave) the oscillator will vibrate at its *resonance frequency* ω_0. In the presence of a field whose frequency is less than ω_0, $E(t)$ and $x(t)$ have the same sign, which means that the oscillator can follow the applied force (i.e., is in phase with it). However, when $\omega > \omega_0$, the displacement $x(t)$ is in a direction opposite to that of the instantaneous force $q_e E(t)$ and therefore 180° out of phase with it. Remember that we are talking about oscillating dipoles where for $\omega_0 > \omega$, the relative motion of the *positive* charge is a vibration in the direction of the field. Above resonance the positive charge is 180° out of phase with the field, and the dipole is said to lag by π rad.

The dipole moment is equal to the charge q_e times its displacement, and if there are N contributing electrons per unit volume, the electric polarization, or density of dipole moments, is

$$P = q_e x N. \tag{3.66}$$

Hence

$$P = \frac{q_e^2 N E/m_e}{(\omega_0^2 - \omega^2)} \tag{3.67}$$

and from Eq. (3.61)

$$\epsilon = \epsilon_0 + \frac{P(t)}{E(t)} = \epsilon_0 + \frac{q_e^2 N/m_e}{(\omega_0^2 - \omega^2)}. \tag{3.68}$$

Using the fact that $n^2 = K_e = \epsilon/\epsilon_0$, we can arrive at an expression for n as a function of ω, which is known as a **dispersion equation**:

$$n^2(\omega) = 1 + \frac{Nq_e^2}{\epsilon_0 m_e}\left(\frac{1}{\omega_0^2 - \omega^2}\right). \tag{3.69}$$

At frequencies increasingly above resonance, $(\omega_0^2 - \omega^2) < 0$, and the oscillator undergoes displacements that are approximately 180° out of phase with the driving force. The resulting electric polarization will therefore be similarly out of phase with the applied electric field. Hence the dielectric constant and therefore the index of refraction will both be less than 1. At frequencies increasingly below resonance, $(\omega_0^2 - \omega^2) > 0$, the electric polarization will be nearly in phase with the applied electric field. The dielectric constant and the corresponding index of refraction will then both be greater than 1. This kind of behavior, which actually represents only part of what happens, is nonetheless generally observed in all sorts of materials.

As a rule, any given substance will actually undergo several of these transitions from $n > 1$ to $n < 1$ as the illuminating frequency is made to increase. The implication is that instead of a single frequency ω_0 at which the system resonates, there apparently are several such frequencies. It would seem reasonable to generalize matters by supposing that there are N molecules per unit volume, each with f_j oscillators having natural frequencies ω_{0j}, where $j = 1, 2, 3, \ldots$. In that case,

$$n^2(\omega) = 1 + \frac{Nq_e^2}{\epsilon_0 m_e} \sum_j \left(\frac{f_j}{\omega_{0j}^2 - \omega^2}\right). \tag{3.70}$$

This is essentially the same result as that arising from the quantum-mechanical treatment, with the exception that some of the terms must be reinterpreted. Accordingly, the quantities ω_{0j} would then be the characteristic frequencies at which an atom may absorb or emit radiant energy. The f_j terms, which satisfy the requirement that $\sum_j f_j = 1$, are weighting factors known as *oscillator strengths*. They reflect the emphasis that should be placed on each one of the modes. Since they measure the likelihood that a given atomic transition will occur, the f_j terms are also known as *transition probabilities*.

A similar reinterpretation of the f_j terms is even required classically, since agreement with the experimental data demands that they be less than unity. This is obviously contrary to the definition of the f_j that led to Eq. (3.70). One then supposes that a molecule has many oscillatory modes but that each of these has a distinct natural frequency and strength.

Notice that when ω equals any of the characteristic frequencies, n is discontinuous, contrary to actual observation. This is simply the result of having neglected the damping term, which should have appeared in the denominator of the sum. Incidentally, the damping, in part, is attributable to energy lost when the forced oscillators reradiate. In solids, liquids, and gases at high pressure ($\approx 10^3$ atm), the interatomic distances are roughly 10 times less than those of a gas at standard temperature and pressure. Atoms and molecules in this relatively close proximity experience strong interactions and a resulting "frictional" force. The effect is a damping of the oscillators and a dissipation of their energy within the substance in the form of "heat" (random molecular motion).

Had we included a damping force proportional to the speed (of the form $m_e \gamma\, dx/dt$) in the equation of motion, the dispersion equation (3.70) would have been

$$n^2(\omega) = 1 + \frac{Nq_e^2}{\epsilon_0 m_e} \sum_j \frac{f_j}{\omega_{0j}^2 - \omega^2 + i\gamma_j \omega}. \tag{3.71}$$

Although this expression is fine for rarified media such as gases there is another complication that must be overcome if the equation is to be applied to dense substances. Each atom interacts with the local electric field in which it is immersed. Yet unlike the isolated atoms considered above, those in a dense material will also experience the induced field set up by their brethren. Consequently an atom "sees" in addition to the applied field $E(t)$ another field,* namely, $P(t)/3\epsilon_0$.

* This result, which applies to isotropic media, is derived in almost any text on electromagnetic theory.

Without going into the details here, it can be shown that

$$\frac{n^2 - 1}{n^2 + 2} = \frac{Nq_e^2}{3\epsilon_0 m_e} \sum_j \frac{f_j}{\omega_{0j}^2 - \omega^2 + i\gamma_j \omega}. \tag{3.72}$$

Thus far we have been considering electron-oscillators almost exclusively, but the same results would have been applicable to ions bound to fixed atomic sites as well. In that instance m_e would be replaced by the considerably larger ion mass. Thus although electronic polarization is important over the entire optical spectrum, the contributions from ionic polarization significantly affect n only in regions of resonance ($\omega_{0j} = \omega$).

The implications of a complex index of refraction will be considered later, in Section 4.3.5. At the moment we limit the discussion, for the most part, to situations in which absorption is negligible (i.e., $\omega_{0j}^2 - \omega^2 \gg \gamma_j \omega$) and n is real, so that

$$\frac{n^2 - 1}{n^2 + 2} = \frac{Nq_e^2}{3\epsilon_0 m_e} \sum_j \frac{f_j}{\omega_{0j}^2 - \omega^2}. \tag{3.73}$$

Colorless, transparent materials have their characteristic frequencies outside the visible region of the spectrum (which is why they are, in fact, colorless and transparent). In particular, glasses have effective natural frequencies above the visible in the ultraviolet, where they become opaque. In cases for which $\omega_{0j}^2 \gg \omega^2$, by comparison, ω^2 may be neglected in Eq. (3.73), yielding an essentially constant index of refraction over that frequency region. For example, the important characteristic frequencies for glasses occur at wavelengths of about 100 nm. The middle of the visible range is roughly five times that value, and there, $\omega_{0j}^2 \gg \omega^2$. Notice that as ω increases toward ω_{0j}, $(\omega_{0j}^2 - \omega^2)$ decreases and n *gradually increases with frequency*, as is clearly evident in Fig. 3.26. This is called **normal dispersion**. In the ultraviolet region, as ω approaches a natural frequency, the oscillators will begin to resonate. Their amplitudes will increase markedly, and this will be accompanied by damping and a strong absorption of energy from the incident wave. When $\omega_{0j} = \omega$ in Eq. (3.72), the damping term obviously becomes dominant. The regions immediately surrounding the various ω_{0j} in Fig. 3.27 are called *absorption bands*. There $dn/d\omega$ is negative, and the process is spoken of as **anomalous** (i.e., abnormal) **dispersion**. If white light passes through a glass prism,

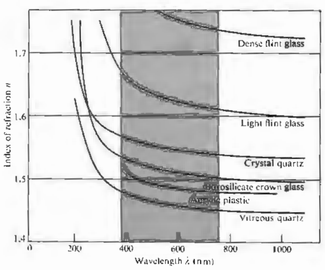


Figure 3.26 The wavelength dependence of the index of refraction for various materials.

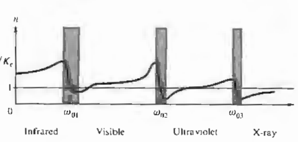


Figure 3.27 Refractive index versus frequency.

the blue constituent will have a higher index than the red and will therefore be deviated through a larger angle (see Section 5.5.1). In contrast, if we use a liquid-cell prism containing a dye solution with an absorption band in the visible, the spectrum will be altered markedly (see Problem 3.29). All substances possess absorption bands somewhere within the electromagnetic frequency spectrum, so that the term *anomalous dispersion*, being a carryover from the late 1800s, is certainly a misnomer.

As we have seen, atoms within a molecule can also vibrate about their equilibrium positions. But the nuclei are massive, and so the natural oscillatory frequencies will be low, in the infrared. Molecules such as H_2O and CO_2 will have resonances in both the infrared and ultraviolet. If water was trapped within a piece of glass during its manufacture, these molecular oscillators would be available, and an infrared absorption band would exist. The presence of oxides will also result in infrared absorption. Figure 3.28 shows the $n(\omega)$ curves for a number of important optical crystals ranging from the ultraviolet to the infrared. Note how they rise in the ultraviolet and fall in the infrared. At the even lower frequencies of radiowaves, glass will again be transparent. In comparison, a piece of stained glass evidently has a resonance in the visible where it absorbs out a particular range of frequencies, transmitting the complementary color.

As a final point, notice that if the driving frequency is greater than any of the ω_{0j} terms, then $n^2 < 1$ and $n < 1$. Such a situation can occur, for example, if we beam x-rays onto a glass plate. This is an intriguing result, since it leads to $v > c$, in seeming contradiction to special relativity. We will consider this behavior again later on, when we discuss the group velocity (Section 7.6).

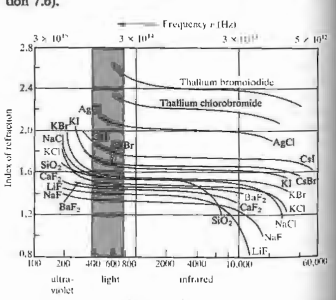


Figure 3.28 Index of refraction versus wavelength and frequency for several important optical crystals. (Adapted from data published by The Harshaw Chemical Co.)

In partial summary then, over the visible region of the spectrum, electronic polarization is the operative mechanism determining $n(\omega)$. Classically one imagines electron-oscillators vibrating at the frequency of the incident wave. When the wave's frequency is appreciably different from a characteristic or natural frequency, the oscillations are small, and there is little dissipative absorption. At resonance, however, the oscillator amplitudes are increased, and the field does an increased amount of work on the charges. Electromagnetic energy removed from the wave and converted into mechanical energy is dissipated thermally within the substance, and one speaks of an absorption peak or band. The material, although essentially transparent at other frequencies, is fairly opaque to incident radiation at its characteristic frequencies (Fig. 3.29).

3.5.2 The Propagation of Light Through a Dielectric Medium

The process whereby light propagates through a medium at a speed other than c is a fairly complicated one, and this section is devoted to making it at least physically reasonable within the context of the simple oscillator model.

Consider an incident or *primary* electromagnetic wave (in vacuum) impinging on a dielectric. As we have seen, it will polarize the medium and drive the electron-oscillators into forced vibration. They, in turn, will reradiate or *scatter* energy in the form of electromagnetic wavelets of the same frequency as that of the incident wave. In a substance whose atoms or molecules are arranged with some degree of regularity, these wavelets will tend to mutually interfere. That is, they will overlap in certain regions, whereupon they will either reinforce or diminish each other to varying degrees.

Figure 3.30 illustrates a plane wave incident from above and the resulting clutter of scattered spherical wavelets. These superimpose in the forward direction to form plane wavefronts, which we shall refer to as the *secondary* wave. The way this actually occurs can better be appreciated in Fig. 3.31, which depicts a sequence in time showing two molecules A and B interacting with

Figure 3.29 A group of semiconductor lenses made from ZnSe, CdTe, GaAs, and Ge. These materials are particularly useful in the infrared (2 μm to 30 μm), where they are highly transparent despite the fact that they are quite opaque in the visible region of the spectrum. (Photo courtesy Two-Six Incorporated.)

an incoming plane wave—a solid line represents a wave peak (a positive E-field), and a dashed line corresponds to a trough (a negative E-field). In Part (a) of the figure the incoming plane wavefront impinges on molecule A, which begins to scatter a spherical wavelet. The phase of all such wavelets (as compared with the incident wave) will be examined presently; for the moment, let it be anything, say 180°. Accordingly, molecule A begins to radiate a trough in response to being driven by a peak. Part (b) shows the scattered spherical wavelet and the primary plane wave overlapping, marching out of step but marching together. And another wavelet is emerging from A. In (c) a trough of the primary wavefront is incident on B, and it, in turn, begins to reradiate a wavelet, which must also be out of phase by 180°. In (d) we see the whole point of the diagram—all the wavelets are moving forward with the primary wave. *In the forward direction the wavelets from A and B are in phase with each other* but out of phase with the primary wave. That would be true for all such wavelets, regardless of how many molecules there were, how close together they were, or how they were distributed.

As a result of the asymmetry introduced by the beam

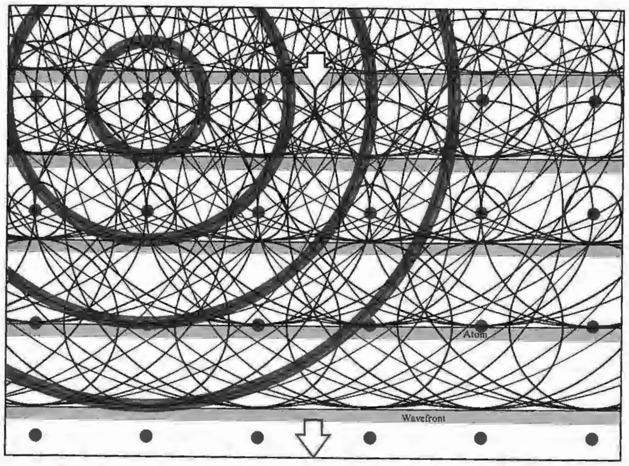
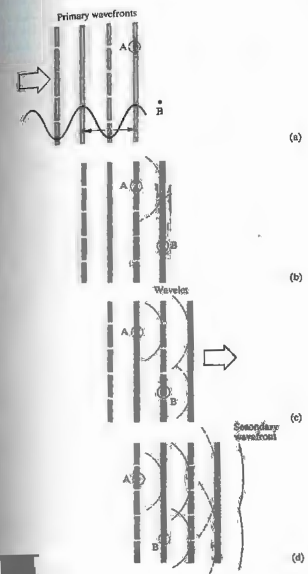


Figure 3.30 A downward plane wave incident on an ordered array of atoms. Wavelets scatter in all directions and overlap to form an ongoing secondary plane wave traveling downward.

itself, all the scattered wavelets add to each other in phase; they rise and fall together at points tangent to a plane and thus *constructively* (see Section 7.1) combine to form a forward-moving secondary plane wave. This does not happen in the backward direction or, indeed, in any other direction. If the scatterers are randomly located and far apart, the total radiation in any direction but forward will be an uncorrelated mixture of essentially independent wavelets showing no significant interference. This is approximately the situation existing about 100 miles up in the Earth's rarefied high-altitude atmosphere (see Section 8.5). By contrast, in an ordinary gas (and even the atmosphere at standard temperature and pressure has about 3 million molecules in a λ^3 cube) the wavelets ($\lambda \approx 500$ nm) scattered by sources so close together (≈ 3 nm) cannot properly be viewed as random. Nor are they random in a solid or liquid, in which the atoms are 10 times closer and arrayed in a far more orderly fashion. Here again, the scattered wavelets interfere constructively in the forward direction—that much is independent of the arrangement of the molecules—but destructive interference, in which the wavelets cancel one another (see Section 7.1), now predominates in all other directions. *In dense media there is essentially no scattering in any direction but forward;* the beam progresses through the medium in the forward direction.

For empirical reasons alone we can anticipate that the secondary wave will combine with what is left of the primary wave to yield the only observed disturbance within the medium, namely, the **refracted** wave. *Both the primary and secondary electromagnetic waves propagate through the interatomic void with the speed c.* Yet the medium can certainly possess an index of refraction other than 1. The refracted wave may appear to have a phase velocity less than, equal to, or even greater than c. The key to this apparent contradiction resides in the phase relationship between the secondary and primary waves.



3.31 In the forward direction the scattered wavelets arrive on planar wavefronts—trough with trough, peak with peak.

The classical model predicts that the electron-oscillators will be able to vibrate almost completely in phase with the driving force (i.e., the primary disturbance) only at relatively low frequencies. As the frequency of the electromagnetic field increases, the oscillators will fall behind, lagging in phase by a proportionately larger amount. A detailed analysis reveals that at resonance the phase lag will reach 90°, increasing thereafter to almost 180°, or half a wavelength, at frequencies well above the particular characteristic value. Problem 3.28 explores this phase lag for a damped driven oscillator, and Fig. 3.32 summarizes the results.

In addition to these lags there is another effect that must be considered. When the scattered wavelets recombine, the resultant secondary wave* itself lags the oscillators by 90°.

The combined effect of both these mechanisms is that at frequencies below resonance, the secondary wave lags the primary (Fig. 3.33) by some amount between approximately 90° and 180°, and at frequencies above resonance, the lag ranges from about 180° to 270°. But a phase lag of $\delta \geq 180°$ is equivalent to a phase lead of $360° - \delta$ [e.g., $\cos(\theta - 270°) = \cos(\theta + 90°)$]. This much can be seen on the right side of Fig. 3.32(b).

Within the transparent medium the primary and secondary waves overlap and, depending on their amplitudes and relative phase, generate the net refracted disturbance. Except for the fact that it is weakened by scattering, the primary wave travels into the material just as if it were traversing free space. By comparison

*This point will be made more plausible when we consider the predictions of the Huygens–Fresnel theory in the diffraction chapter. Most texts on E & M treat the problem of radiation from a sheet of oscillating charges, in which case the 90° phase lag is a natural result.

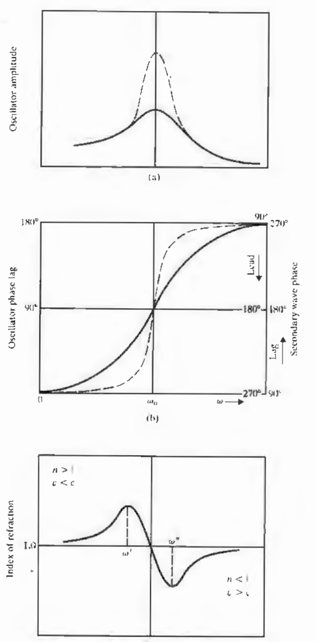


Figure 3.32 A schematic representation of (a) amplitude and (b) phase lag versus driving frequency for a damped oscillator. The dashed curves correspond to decreased damping. The corresponding index of refraction is shown in (c).

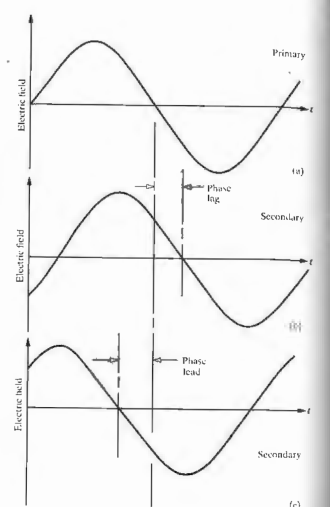


Figure 3.33 A primary wave (a) and two possible secondary waves. In (b) the secondary lags the primary—it takes longer to reach any given value. In (c) the secondary wave reaches any given value before (at an earlier time than) the primary; that is, it leads.

to this free-space wave, which initiated the process, the refracted wave is phase shifted, and this phase difference is crucial.

When the secondary wave lags (or leads) the primary, the refracted wave must also lag (or lead) it by some amount (Fig. 3.34). This qualitative relationship will serve our purposes for the moment, although it should

...ted that the phase of the resultant also depends ...he amplitudes of the interacting waves [see Eq. ...)]. Accordingly at frequencies below ω_0 the refrac-...ave lags the free-space wave, whereas at frequen-...bove ω_0 it leads the free-space wave. For the special ...n which $\omega = \omega_0$ the secondary and primary waves ...ut of phase by 180°; the former works against the ...er, so that the refracted wave is appreciably reduced ...mplitude although unaffected in phase.

...the refracted wave advances through the medium, ...tering occurs over and over again. Light traversing ...substance is progressively retarded (or advanced) ...phase. Evidently, since the speed of the wave is the ... of advance of the condition of constant phase, a change in the phase should correspond to a change in the speed.

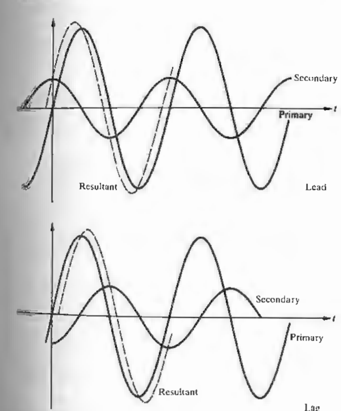


Figure 3.34 If the secondary leads the primary the resultant will also lead it.

We now wish to show that a phase shift is indeed tantamount to a difference in phase velocity. In free space, the *disturbance at some point P* may be written as

$$E_P(t) = E_0 \cos \omega t. \tag{3.74}$$

If P is now surrounded by a dielectric, there will be a cumulative phase shift ε_P, which was built up as the wave moved through the medium to P. At ordinary levels of irradiance the medium will behave linearly, and the frequency in the dielectric will be the same as that in vacuum, even though the wavelength and speed may differ. Once again, but this time in the medium, the disturbance at P is

$$E_P(t) = E_0 \cos (\omega t - \varepsilon_P), \tag{3.75}$$

where subtraction of ε_P corresponds to a phase lag. An observer at P will have to wait a longer time for a given crest to arrive when she is in the medium than she would have had to wait in vacuum. That is, if you imagine two parallel waves of the same frequency, one in vacuum and one in the material, the vacuum wave will pass P a time ε_P/ω before the other wave. Clearly then, *a phase lag of ε_P corresponds to a reduction in speed*, $v < c$ and $n > 1$. Similarly, *a phase lead yields an increase in speed*, $v > c$ and $n < 1$. Again, the scattering process is a continuous one, and the cumulative phase shift builds as the light penetrates the medium. That is to say, ε is a function of the length of dielectric traversed, as it must be if v is to be constant (see Problem 3.30).

The overall form of $n(\omega)$, as depicted in Fig. 3.32(c), can now be understood, as well. At frequencies far below ω_0 the amplitudes of the oscillators and therefore of the secondary waves are very small, and the phase angles are approximately 90°. Consequently, the refracted wave lags only slightly, and n is only slightly greater than 1. As ω increases, the secondary waves have greater amplitudes and lag by greater amounts. The result is a gradually decreasing wave speed and an increasing value of $n > 1$. Although the amplitudes of the secondary waves continue to increase, their relative phases approach 180° as ω approaches ω_0. Consequently, their ability to cause a further increase in the resultant phase lag diminishes. A turning point ($\omega = \omega'$) is reached where the refracted wave begins to experience a decreasing phase lag and an increasing speed, ($dn/d\omega <$

0). That continues until $\omega = \omega_0$, whereupon the refracted wave is appreciably reduced in amplitude but unaltered in phase and speed. At that point, $n = 1$, $v = c$, and we are more or less at the center of the absorption band.

At frequencies just beyond ω_0 the relatively large-amplitude secondary waves lead; the refracted wave is advanced in phase, and its speed exceeds c ($n < 1$). As ω increases the whole scenario is played out again in reverse (with some asymmetry due to frequency-dependent asymmetry in oscillator amplitudes and scattering). At even higher frequencies the secondary waves, which now have very small amplitudes, lead by nearly 90°. The resulting refracted wave is advanced very slightly in phase, and n gradually approaches 1.

The precise shape of a particular $n(\omega)$ curve depends on the specific oscillator damping, as well as on the amount of absorption, which in turn depends on the number of oscillators participating.

A rigorous solution to the propagation problem is known as the *Ewald–Oseen extinction theorem*. Although the mathematical formalism, involving integrodifferential equations, is far too complicated to treat here, the results are certainly of interest. It is found that the electron-oscillators generate an electromagnetic wave having essentially two terms. One of these precisely cancels the primary wave within the medium. The other, and only remaining disturbance, moves through the dielectric at a speed $v = c/n$ as the refracted wave.* Henceforth we shall simply assume that a lightwave propagating through any substantive medium travels at a speed $v \neq c$.

3.6 THE ELECTROMAGNETIC-PHOTON SPECTRUM

In 1867, when Maxwell published the first extensive account of his electromagnetic theory, the frequency band was only known to extend from the infrared, across the visible, to the ultraviolet. Although this region is of major concern in optics, it is a small segment of the vast electromagnetic spectrum (see Fig. 3.35). This section enumerates the main categories (there is actually some overlapping) into which the spectrum is usually divided.

* For a discussion of the Ewald–Oseen theorem, see *Principles of Optics* by Born and Wolf, Section 2.4.2; this is heavy reading. Also look at Reali, "Reflection from Dielectric Materials." *Am. J. Phys.* **50**, 1133 (1982).

3.6.1 Radiofrequency Waves

In 1887, eight years after Maxwell's death, Heinrich Hertz, then professor of physics at the Technische Hochschule in Karlsruhe, Germany, succeeded in generating and detecting electromagnetic waves.* His transmitter was essentially an oscillatory discharge across a spark gap (a form of oscillating electric dipole). For a receiving antenna, he used an open loop of wire with a brass knob on one end and a fine copper point on the other. A small spark visible between the two ends marked the detection of an incident electromagnetic wave. Hertz focused the radiation, determined its polarization, reflected and refracted it, caused it to interfere, setting up standing waves, and then even measured its wavelength (on the order of a meter). As he put it:

> I have succeeded in producing distinct rays of electric force, and in carrying out with them the elementary experiments which are commonly performed with light and radiant heat. . . . We may perhaps further designate them as rays of light of very great wavelength. The experiments described appear to me, at any rate, eminently adapted to remove any doubt as to the identity of light, radiant heat, and electromagnetic wave motion.

The waves used by Hertz are now classified in the *radiofrequency* range, which extends from a few hertz to about 10^9 Hz (λ, from many kilometers to 0.3 m or so). These are generally emitted by an assortment of electric circuits. For example, the 60-Hz alternating current circulating in power lines radiates with a wavelength of 5×10^6 m, or about 3×10^3 miles. There

* David Hughes may well have been the first person who actually performed this feat, but his experiments in 1879 went unpublished and unnoticed for many years.

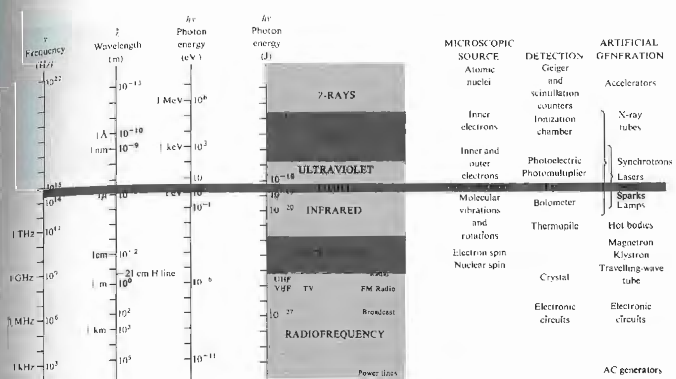


Figure 3.35 The electromagnetic-photon spectrum.

is no upper limit to the theoretical wavelength; one could leisurely swing the proverbial charged pith ball and, in so doing, produce a rather long if not very strong wave. Indeed, waves more than 18 million miles long have been detected streaming down toward Earth from outer space. The higher frequency end of the band is used for television and radio broadcasting.

At 1 MHz (10^6 Hz) a radiofrequency photon has an energy of 6.62×10^{-28} J or 4×10^{-9} eV, a very small quantity by any measure. The granular nature of the radiation is generally obscured, and only a smooth transfer of energy is apparent.

3.6.2 Microwaves

The microwave region extends from about 10^9 Hz up to about 3×10^{11} Hz. The corresponding wavelengths go from roughly 30 cm to 1.0 mm. Radiation capable of penetrating the Earth's atmosphere ranges from less than 1 cm to about 30 m. Microwaves are therefore of interest in space-vehicle communications, as well as radio astronomy. In particular, neutral hydrogen atoms, distributed over vast regions of space, emit 21-cm (1420-MHz) microwaves. A good deal of information about the structure of our own and other galaxies has been gleaned from this particular emission.

Molecules can absorb and emit energy by altering the state of motion of their constituent atoms—they can be made to vibrate and/or rotate. Again, the energy associated with either motion is quantized, and molecules possess rotational and vibrational energy levels in addition to those due to their electrons. Only polar molecules will experience forces via the **E**-field of an incident electromagnetic wave that will cause them to rotate into alignment, and only they can absorb a photon and make a rotational transition to an excited state. Since massive molecules are not able to swing around easily, we can

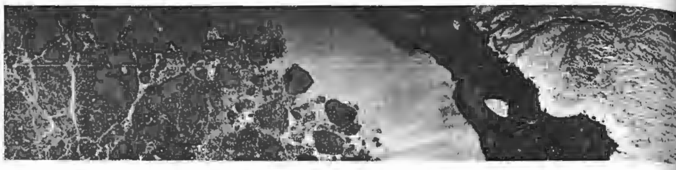


Figure 3.36 A photograph of an 18 by 75 mile area northeast of Alaska. It was taken by the *Seasat* satellite 800 kilometers (500 miles) above the Earth. The overall appearance is somewhat strange because this is actually a radar or microwave picture. The wrinkled gray region on the right is Canada. The small, bright shell shape is Banks Island, embedded in a black band of shore-fast, first-year sea ice. Adjacent to that is open water, which appears smooth and gray. The dark gray blotchy area at the far left is the main polar ice pack. There are no clouds because the radar "sees" right through them.

anticipate that they will have low-frequency rotational resonances (far IR, 0.1 mm, to microwave, 1 cm). For instance, water molecules are polar (see Fig. 3.24), and if exposed to an electromagnetic wave, they will swing around, trying to stay lined up with the alternating E-field. This will occur particularly vigorously at any one of its rotational resonances. Consequently, water molecules efficiently dissipatively absorb microwave radiation at or near such a frequency. The microwave oven (12.2 cm, 2.45 GHz) is an obvious application. On the other hand, nonpolar molecules, such as carbon dioxide, hydrogen, nitrogen, oxygen, and methane, cannot make rotational transitions by way of the absorption of photons.

Nowadays microwaves are used for everything from transmitting telephone conversations and interstation television to cooking hamburgers, from guiding planes and catching speeders (by radar) to studying the origins of the Universe, opening garage doors, and viewing the surface of the planet (Fig. 3.36). They are also quite useful for studying physical optics with experimental arrangements that are scaled up to convenient dimensions.

Photons in the low-frequency end of the microwave spectrum have little energy, and one might expect their sources to be electric circuits exclusively. Emissions of this sort can, however, arise from atomic transitions, if the energy levels involved are quite near each other. The apparent ground state of the cesium atom is a good example. It is actually a pair of closely spaced energy levels, and transitions between them involve an energy of only 4.14×10^{-5} eV. The resulting microwave emission has a frequency of 9.19263177×10^{9} Hz. This is the basis for the well-known cesium clock, the standard of frequency and time.

3.6.3 Infrared

The infrared region, which extends roughly from 3×10^{11} Hz to about 4×10^{14} Hz, was first detected by the renowned astronomer Sir William Herschel (1738–1822) in 1800. The infrared, or IR, is often subdivided into four regions: the *near IR*, i.e., near the visible (780–3000 nm), the *intermediate IR* (3000–6000 nm), the *far IR* (6000–15,000 nm), and the *extreme IR* (15,000 nm–1.0 mm). This is again a rather loose division, and there is no universality in the nomenclature. Radiant energy at the long-wavelength extreme can be generated by either microwave oscillators or incandescent sources (i.e., molecular oscillators). Indeed, any material will radiate and absorb IR via thermal agitation of its constituent molecules.

The molecules of any object at a temperature above absolute zero (−273°C) will radiate IR, even if only weakly (see Section 13.2). On the other hand, infrared is copiously emitted in a continuous spectrum from hot bodies, such as electric heaters, glowing coals, and ordinary house radiators. Roughly half the electromagnetic energy from the Sun is IR, and a common light bulb actually radiates far more IR than light. Like all warm-blooded creatures, we too are infrared emitters. The human body radiates IR quite weakly, starting at around 3000 nm, peaking in the vicinity of 10,000 nm, and trailing off from there into the extreme IR and, negligibly, beyond. This emission is exploited by see-in-the-dark sniperscopes, as well as by some rather nasty "heat"-sensitive snakes (Crotalidae, pit vipers, and Boidae, constrictors) that tend to be active at night.

Besides rotating, a molecule can vibrate in several different ways, with its atoms moving in various directions with respect to one another. The molecule need not be polar, and even a linear system such as CO_2 has three basic vibrational modes and a number of energy levels, each of which can be excited by photons. The associated vibrational emission and absorption spectra are, as a rule, in the IR (1000 nm to 0.1 mm). Many molecules have both vibrational and rotational resonances in the IR and are good absorbers, which is one reason IR is often misleadingly called "heat waves"—just put your face in the sunshine and feel the resulting build-up of thermal energy.

Infrared radiant energy is generally measured with a device that responds to the heat generated on absorption of IR by a blackened surface. There are, for example, thermocouple, pneumatic (e.g., Golay cells), pyroelectric, and bolometer detectors. These in turn depend on temperature-dependent variations in induced voltage, gas volume, permanent electric polarization, and resistance, respectively. The detector can be coupled by way of a scanning system to a cathode ray tube to produce an instantaneous television-like IR picture (Fig. 3.37) known as a thermograph (which is quite useful for diagnosing all sorts of problems, from utility transformers to faulty people). Photographic films sensitive to near IR (<1300 nm) are also available. There are IR spy satellites that look out for rocket launchings, IR resource satellites that look out for crop diseases, and IR astronomical satellites that look out into space—one of which discovered a ring of matter around the star Vega (1983); there are "heat-seeking" missiles guided by IR, and IR lasers and telescopes peering into the heavens.

Small differences in the temperatures of objects and their surroundings result in characteristic IR emission, which can be used in many ways, from detecting brain tumors and breast cancers to spotting a lurking burglar. The CO_2 laser, because it is a convenient source of continuous power at appreciable levels of 100 W and more, is widely used in industry, especially in precision cutting and heat treating. Its extreme-IR emissions (18.3 μm–23.0 μm) are readily absorbed by human tissue, making the laserbeam an effective bloodless scalpel that cauterizes as it cuts.

3.6.4 Light

Light corresponds to the electromagnetic radiation in the narrow band of frequencies from about 3.84×10^{14} Hz to roughly 7.69×10^{14} Hz (see Table 3.2). It is generally produced by a rearrangement of the outer electrons in atoms and molecules. (Don't forget syn-

Figure 3.37 Thermograph of the author. Note the cool beard.

Table 3.2 Approximate frequency and vacuum wavelength ranges for the various colors.

Color	λ_0(nm)	ν(THz)*
Red	780–622	384–482
Orange	622–597	482–503
Yellow	597–577	503–520
Green	577–492	520–610
Blue	492–455	610–659
Violet	455–390	659–769

* 1 terahertz (THz) = 10^{12} Hz, 1 nanometer (nm) = 10^{-9} m.

chrotron radiation, which is a different mechanism.)*

In an incandescent material, a hot glowing metal filament, or the solar fireball, electrons are randomly accelerated and undergo frequent collisions. The resulting broad emission spectrum is called *thermal radiation*, and it is a major source of light. In contrast, if we fill a tube with some gas and pass an electric discharge through it, the atoms therein will become excited and radiate. The emitted light is characteristic of the particular energy levels of those atoms, and it is made up of a series of well-defined frequency bands or lines. Such a device is known as a gas discharge tube. When the gas is the krypton 86 isotope, the lines are particularly narrow (zero nuclear spin, therefore no hyperfine structure). The orange-red line of Kr 86, whose vacuum wavelength is 605.7802105 nm, has a width (at half height) of only 0.00047 nm, or about 400 MHz. Accordingly, until 1983 it was the international standard of length (1,650,763.73 wavelengths equaled a meter).

Newton was the first to recognize that **white light** is actually a mixture of all the colors of the visible spectrum, that the prism does not create color by altering white light to different degrees, as had been thought for centuries, but simply fans out the light, separating it into its constituent colors. Not surprisingly, the very concept of *whiteness* seems dependent on our perception of the Earth's daylight spectrum—a broad frequency distribution that falls off more rapidly in the violet than in the red (Fig. 3.38). The human eye-brain detector perceives as white a wide mix of frequencies, usually with about the same amount of energy in each portion. That is what we shall mean when we speak about "white light"—much of the color of the spectrum, with no region predominating. Nonetheless, many different distributions will appear more or less white. We recognize a piece of paper to be white whether it's seen indoors under incandescent light or outside under skylight, even though those whites are quite different. In fact, there are many pairs of colored light beams (e.g., 656-nm red and 492-nm cyan) that will produce the sensation of whiteness, and the eye cannot always distinguish one white from another; it cannot frequency analyze light into its harmonic components the way the ear can analyze sound (see Section 7.7).

Colors are the subjective human physiological and psychological responses, primarily, to the various frequency regions extending from about 384 THz for red, through orange, yellow, green, and blue, to violet at about 769 THz (Table 3.2). Color is not a property of the light itself but a manifestation of the electrochemical sensing system—eye, nerves, brain. To be more precise, we should not say "yellow light" but rather "light that is seen as yellow." Remarkably, a variety of different frequency mixtures can evoke the same color response from the eye-brain sensor. A beam of red light (peaking at, say, 690 THz) overlapping a beam of green light (peaking at, say, 540 THz) will result, believe it or not, in the perception of *yellow* light, even though there are no frequencies present in the so-called yellow band. Apparently, the eye-brain averages the input and "sees" yellow (Section 4.4). That's why a color television screen can manage with only three phosphors: red, green, and blue.

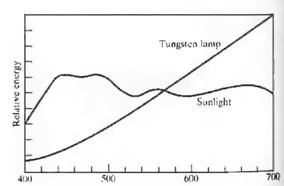


Figure 3.38 A graph of sunlight compared with the light from a tungsten lamp.

* There is no need here to define light in terms of human physiology. On the contrary, there is plenty of evidence to indicate that this would not be a very good idea. For example, see T. J. Wang, "Visual Response of the Human Eye to X Radiation." *Am. J. Phys.* **35**, 779 (1967).

In a flood of bright sunlight where the photon flux density might be 10^{21} photons/m^2 s, we can generally expect the quantum nature of the energy transport to be thoroughly obscured. However, in very weak beams, since photons in the visible range ($h\nu \approx 1.6$ eV to 3.2 eV) are energetic enough to produce effects on a distinctly individual basis, the granularity will become evident. Research on human vision indicates that as few as 10 light photons, and possibly even 1, may be detectable by the eye.

3.6.5 Ultraviolet

Adjacent to light in the spectrum is the ultraviolet region (approximately 8×10^{14} Hz to about 3.4×10^{16} Hz), discovered by Johann Wilhelm Ritter (1776–1810). Photon energies therein range from roughly 3.2 eV to 100 eV. Ultraviolet, or UV, rays from the Sun will thus have more than enough energy to ionize atoms in the upper atmosphere and in so doing create the ionosphere. These photon energies are also of the order of the magnitude of many chemical reactions, and ultraviolet rays become important in triggering those reactions. Fortunately, ozone (O_3) in the atmosphere absorbs what would otherwise be a lethal stream of solar UV. At wavelengths less than around 290 nm, UV is germicidal (i.e., it kills microorganisms). The particlelike aspects of radiant energy become increasingly evident as the frequency rises.

Humans cannot see UV very well, because the cornea absorbs it, particularly at the shorter wavelengths, while the eye lens absorbs most strongly beyond 300 nm. A person who has had a lens removed because of cataracts can see UV ($\lambda > 300$ nm). In addition to insects, such as honeybees, a fair number of other creatures can visually respond to UV. Pigeons, for example, are capable of recognizing patterns illuminated by UV and probably employ that ability to navigate by the Sun even on overcast days.

An atom emits a UV photon when an electron makes a long jump down from a highly excited state. For example, the outermost electron of a sodium atom can be raised to higher and higher energy levels until it is ultimately torn loose altogether at 5.1 eV, and the atom is ionized. If the ion subsequently recombines with a free electron, the latter will rapidly descend to the ground state, most likely in a series of jumps, each resulting in the emission of a photon. It is possible, however, for the electron to make one long plunge to the ground state, radiating a single 5.1-eV UV photon. Even more energetic UV can be generated when the inner, tightly bound electrons of an atom are excited.

The unpaired valence electrons of isolated atoms can

Figure 3.39 An ultraviolet photograph of Venus taken by *Mariner 10*.

be an important source of colored light. But when these same atoms combine to form molecules or solids, the valence electrons are ordinarily paired in the process of creating the chemical bonds that hold the thing together. Consequently, the electrons are often more tightly bound, and their molecular-excited states are higher up in the UV. Molecules in the atmosphere, such as N_2, O_2, CO_2, and H_2O, have just this sort of electronic resonance in the UV (see Section 8.5).

Nowadays there are ultraviolet photographic films and microscopes, UV orbiting celestial telescopes, synchrotron sources, and ultraviolet lasers (Fig. 3.39).

3.6.6 X-rays

X-rays were rather fortuitously discovered in 1895 by Wilhelm Conrad Röntgen (1845–1923). Extending in frequency from roughly 2.4×10^{16} Hz to 5×10^{19} Hz, they have extremely short wavelengths; most are smaller than an atom. Their photon energies (100 eV to 0.2 MeV) are large enough so that x-ray quanta can interact with matter one at a time in a clearly granular fashion, almost like bullets of energy. One of the most practical mechanisms for producing x-rays is the rapid deceleration of high-speed charged particles. The resulting broad-frequency *bremsstrahlung* (German for "braking radiation") arises when a beam of energetic electrons is fired at a material target, such as a copper plate. Collisions with the Cu nuclei produce deflections of the beam electrons, which in turn radiate x-ray photons.

In addition, the atoms of the target may become ionized during the bombardment. Should that occur through removal of an inner electron strongly bound to the nucleus, the atom will emit x-rays as the electron cloud returns to the ground state. The resulting quantized emissions are specific to the target atom, revealing its energy level structure, and accordingly are called *characteristic* radiation.

Traditional medical film-radiography generally produces little more than simple shadow castings, rather than photographic images in the usual sense; it has not been possible to fabricate useful x-ray lenses. But modern focusing methods using mirrors (see Section 5.4) have begun an era of x-ray imagery, creating

Figure 3.40 X-ray photograph of the Sun taken March, 1970. The limb of the Moon is visible in the southeast corner. (Courtesy Dr. G. Vaiana and NASA.)

detailed pictures of all sorts of things, from imploding fusion pellets to celestial sources, such as the Sun (Fig. 3.40), distant quasars, and black holes—objects at temperatures of millions of degrees that emit predominantly in the x-ray region. Orbiting x-ray telescopes have given us an exciting new eye on the Universe. There are x-ray microscopes, picosecond x-ray streak cameras, x-ray diffraction gratings, and interferometers, and work continues on x-ray holography. In 1984 a group at the Lawrence Livermore National Laboratory succeeded in producing laser radiation at a wavelength of 20.6 nm. Though this is more accurately in the extreme ultraviolet (XUV), it's close enough to the x-ray region to qualify as the first soft x-ray laser.

3.6.7 Gamma Rays

These are the highest-energy (10^4 eV to about 10^{19} eV), lowest-wavelength electromagnetic radiations. They are emitted by particles undergoing transitions within the atomic nucleus. A single gamma-ray photon carries so much energy that it can be detected with little difficulty. At the same time its wavelength has become so small that it is now extremely difficult to observe any wavelike properties.

We have gone full cycle from the radiofrequency wavelike response to gamma-ray particlelike behavior. Somewhere, not far from the (logarithmic) center of the spectrum, there is light. As with all electromagnetic radiation, its energy is quantized, but here in particular what we "see" will depend on how we "look."

PROBLEMS

3.1 Consider the plane electromagnetic wave (in SI units) given by the expressions $E_x = 0$, $E_y = 2\cos[2\pi \times 10^{14}(t - x/c) + \pi/2]$, and $E_z = 0$.

a) What are the frequency, wavelength, direction of motion, amplitude, initial phase angle, and polarization of the wave?
b) Write an expression for the magnetic flux density.

3.2 Write an expression for the **E**- and **B**-fields that constitute a plane harmonic wave traveling in the $+z$-direction. The wave is linearly polarized with its plane of vibration at 45° to the yz-plane.

3.3* Calculate the energy input necessary to charge a parallel plate capacitor by carrying charge from one plate to the other. Assume the energy is stored in the field between the plates and compute the energy per unit volume, u_E, of that region, i.e., Eq. (3.31). *Hint:* since the electric field increases throughout the process, either integrate or use its average value $E/2$.

3.4 The time average of some function $f(t)$ taken over an interval T is given by

$$\langle f(t) \rangle = \frac{1}{T} \int_{t}^{t+T} f(t')\, dt',$$

where t' is just a dummy variable. If $\tau = 2\pi/\omega$ is the period of a harmonic function, show that

$$\langle \sin^2 (\mathbf{k} \cdot \mathbf{r} - \omega t) \rangle = \tfrac{1}{2},$$

$$\langle \cos^2 (\mathbf{k} \cdot \mathbf{r} - \omega t) \rangle = \tfrac{1}{2},$$

and

$$\langle \sin (\mathbf{k} \cdot \mathbf{r} - \omega t) \cos (\mathbf{k} \cdot \mathbf{r} - \omega t) \rangle = 0,$$

when $T = \tau$ and when $T \gg \tau$.

3.5* Consider a linearly polarized plane electromagnetic wave traveling in the $+x$-direction in free space and having as its plane of vibration the xy-plane. Given that its frequency is 10 MHz and its amplitude is $E_0 = 0.08$ V/m,

a) find the period and wavelength of the wave,
b) write an expression for $E(t)$ and $B(t)$,
c) find the flux density, $\langle S \rangle$, of the wave.

3.6 A linearly polarized harmonic plane wave with a scalar amplitude of 10 V/m is propagating along a line in the xy-plane at 45° to the x-axis with the xy-plane as its plane of vibration. Please write a vector expression describing the wave assuming both k_x and k_y are positive. Calculate the flux density taking the wave to be in vacuum.

3.7 Pulses of UV lasting 2.00 ns each are emitted from a laser which has a beam of diameter 2.5 mm. Given that each burst carries an energy of 6.0 J, (a) determine the length in space of each wavetrain, and (b) find the average energy per unit volume for such a pulse.

3.8 A 1.0-mW laser has a beam diameter of 2 mm. Assuming the divergence of the beam to be negligible, compute its energy density in the vicinity of the laser.

3.9* A cloud of locusts having a density of 100 insects per cubic meter is flying north at a rate of 6 m/min. What is the flux density of locusts, i.e., how many cross an area of 1 m^2 perpendicular to their flight path per second?

3.10 Imagine that you are standing in the path of an antenna which is radiating plane waves of frequency 100 MHz and flux density 19.88×10^{-2} W/m^2. Compute the photon flux density, i.e., the number of photons per unit time per unit area. How many photons, on the average, will be found in a cubic meter of this region?

3.11* How many photons per second are emitted from a 100 W yellow light bulb if we assume negligible thermal losses and a quasimonochromatic wavelength of 550 nm? In actuality only about 2.5% of the total dissipated power emerges as visible radiation in an ordinary 100 W lamp.

3.12 A 3.0-V flashlight bulb draws 0.25 A, converting about 1.0% of the dissipated power into light ($\lambda \approx 550$ nm). If the beam has a cross-sectional area of 10 cm^2, and is approximately cylindrical,

a) how many photons are emitted per second?
b) how many photons occupy each meter of the beam?
c) what is the flux density of the beam as it leaves the flashlight?

3.13* An isotropic quasimonochromatic point source radiates at a rate of 100 W. What is the flux density at a distance of 1 m? What are the amplitudes of the **E**- and **B**-fields at that point?

3.14 Using energy arguments, show that the amplitude of a cylindrical wave must vary inversely with $\sqrt{r}$. Draw a diagram indicating what's happening.

3.15* What is the momentum of a 10^{19}-Hz x-ray photon?

3.16 Consider an electromagnetic wave impinging on an electron. It is easy to show kinematically that the average value of the time rate of change of the electron's momentum **p** is proportional to the average value of the time rate of change of the work, W, done on it by the wave. In particular,

$$\left\langle \frac{d\mathbf{p}}{dt} \right\rangle = \frac{1}{c} \left\langle \frac{dW}{dt} \right\rangle \hat{\mathbf{i}}.$$

Accordingly, if this momentum change is imparted to some completely absorbing material, show that the pressure is given by Eq. (3.50).

3.17* Derive an expression for the radiation pressure when the normally incident beam of light is totally reflected. Generalize this result to the case of oblique incidence at an angle θ with the normal.

3.18 A completely absorbing screen receives 300 W of light for 100 s. Compute the total linear momentum transferred to the screen.

3.19 The average magnitude of the Poynting vector for sunlight arriving at the top of Earth's atmosphere (1.5×10^{11} m from the Sun) is about 1.4 kW/m^2.

a) Compute the average radiation pressure exerted on a metal reflector facing the Sun.
b) Approximate the average radiation pressure at the surface of the Sun whose diameter is 1.4×10^9 m.

3.20 What force on the average will be exerted on the (40 m × 50 m) flat, highly reflecting side of a space station wall if it's facing the Sun while orbiting Earth?

3.21 A parabolic radar antenna with a 2-m diameter transmits 200-kW pulses of energy. If its repetition rate is 500 pulses per second, each lasting 2 μs, determine the average reaction force on the antenna.

3.22 Consider the plight of an astronaut floating in free space with only a 10-W lantern (inexhaustibly supplied with power). How long will it take to reach a speed of 10 m/s using the radiation as propulsion? The astronaut's total mass is 100 kg.

3.23 Consider the uniformly moving charge depicted in Fig. 3.14(b). Draw a sphere surrounding it and show via the Poynting vector that the charge does not radiate.

3.24* A plane, harmonic, linearly polarized light wave has an electric field intensity given by

$$E_z = E_0 \cos \pi 10^{15}\left(t - \frac{x}{0.65c}\right)$$

while traveling in a piece of glass. Find

a) the frequency of the light,
b) its wavelength,
c) the index of refraction of the glass.

3.25 The low-frequency relative permittivity of water varies from 88.00 at 0°C to 55.33 at 100°C. Explain this behavior. Over the same range in temperature, the index of refraction ($\lambda = 589.3$ nm) goes from roughly 1.33 to 1.32. Why is the change in n so much smaller than the corresponding change in K_e?

3.26 Show that for substances of low density, such as gases, which have a single resonant frequency ω_0, the index of refraction is given by

$$n \approx 1 + \frac{Nq_e^2}{2\epsilon_0 m_e(\omega_0^2 - \omega^2)}.$$

3.27* In the next chapter, Eq. (4.47), we'll see that a substance reflects radiant energy appreciably when its index differs most from the medium in which it is embedded.

a) The dielectric constant of ice measured at microwave frequencies is roughly 1, whereas that for water is about 80 times greater—why?
b) How is it that a radar beam easily passes through ice but is considerably reflected when encountering a dense rain?

3.28 The equation for a driven damped oscillator is

$$m_e\ddot{x} + m_e\gamma\dot{x} + m_e\omega_0^2 x = q_e E(t).$$

a) Explain the significance of each term.
b) Let $E = E_0 e^{i\omega t}$ and $x = x_0 e^{i(\omega t - \alpha)}$, where E_0 and x_0 are real quantities. Substitute into the above expression and show that

$$x_0 = \frac{q_e E_0}{m_e} \frac{1}{[(\omega_0^2 - \omega^2)^2 + \gamma^2\omega^2]^{1/2}}.$$

c) Derive an expression for the phase lag, α, and discuss how α varies as ω goes from $\omega \ll \omega_0$ to $\omega = \omega_0$ to $\omega \gg \omega_0$.

3.29* Fuchsin is a strong (aniline) dye, which in solution with alcohol has a deep red color. It appears red because it absorbs the green component of the spectrum. (As you might expect, the surfaces of crystals of fuchsin reflect green light rather strongly.) Imagine that you have a thin-walled hollow prism filled with this solution. What will the spectrum look like for incident white light? By the way, anomalous dispersion was first observed in about 1840 by Fox Talbot, and the effect was christened in 1862 by Le Roux. His work was promptly forgotten, only to be rediscovered eight years later by C. Christiansen.

3.30 Imagine that we have a nonabsorbing glass plate of index n and thickness Δy, which stands between a source S and an observer P.

a) If the unobstructed wave (without the plate present) is $E_u = E_0 \exp i\omega(t - y/c)$, show that with the plate in place the observer sees a wave

$$E_p = E_0 \exp i\omega[t - (n - 1)\,\Delta y/c - y/c].$$

b) Show that if either $n \approx 1$ or Δy is very small, then

$$E_p = E_u + \frac{\omega(n-1)\,\Delta y}{c} E_u e^{-i\pi/2}.$$

The second term on the right may be envisioned as the field arising from the oscillators in the plate.

3.31* Take Eq. (3.70) and check out the units to make sure that they agree on both sides.

3.32 The resonant frequency of lead glass is in the UV fairly near the visible, whereas that for fused silica is far into the UV. Use the dispersion equation to make a rough sketch of n versus ω for the visible region of the spectrum.

3.33 Augustin Louis Cauchy (1789–1857) determined an empirical equation for $n(\lambda)$ for substances that are transparent in the visible. His expression corresponded to the power series relation

$$n = C_1 + C_2/\lambda^2 + C_3/\lambda^4 + \cdots,$$

where the C's are all constants. In light of Fig. 3.27, what is the physical significance of C_1?

3.34 Referring to the previous problem, realize that there is a region between each pair of absorption bands for which the Cauchy equation (with a new set of constants) works fairly well. Examine Fig. 3.26: what can you say about the various values of C_1 as ω decreases across the whole spectrum? Dropping all but the first two terms, use Fig. 3.27 to determine approximate values for C_1 and C_2 for borosilicate crown glass in the visible.

3.35* Crystal quartz has refractive indices of 1.557 and 1.547 at wavelengths of 410.0 nm and 550.0 nm, respectively. Using only the first two terms in Cauchy's equation, calculate C_1 and C_2 and determine the index of refraction of quartz at 610.0 nm.

3.36* In 1871 Sellmeier derived the equation

$$n^2 = 1 + \sum_j \frac{A_j\lambda^2}{\lambda^2 - \lambda_{0j}^2},$$

where the A_j terms are constants and each λ_{0j} is the vacuum wavelength associated with a natural frequence ν_{0j}, such that $\lambda_{0j}\nu_{0j} = c$. This formulation is a considerable practical improvement over the Cauchy equation. Show that where $\lambda \gg \lambda_{0j}$, Cauchy's equation is an approximation of Sellmeier's. *Hint:* write the above expression with only the first term in the sum; expand it by the binomial theorem; take the square root of n^2 and expand again.

3.37* If an ultraviolet photon is to dissociate the oxygen and carbon atoms in the carbon monoxide molecule, it must provide 11 eV of energy. What is the minimum frequency of the appropriate radiation?

4 THE PROPAGATION OF LIGHT

4.1 INTRODUCTION

We now consider a number of phenomena related to the propagation of light and its interaction with material media. In particular, we shall study the characteristics of lightwaves as they progress through various substances, crossing interfaces, and being reflected and refracted in the process. For the most part, we shall envision light as a classical electromagnetic wave whose velocity through any medium is dependent upon that material's electric and magnetic properties. It is an intriguing fact that many of the basic principles of optics are predicated on the wave aspects of light but are completely independent of the exact nature of the wave. As we shall see, this accounts for the longevity of *Huygens's principle*, which has served in turn to describe mechanical aether waves, electromagnetic waves, and now, after three hundred years, applies to quantum optics.

Suppose, for the moment, that a wave impinges on the interface separating two different media (e.g., a piece of glass in air). As we know from our everyday experiences, a portion of the incident flux density will be diverted back in the form of a *reflected wave*, while the remainder will be transmitted across the boundary as a *refracted wave*. On a submicroscopic scale we can envision an assemblage of atoms that scatter the incident radiant energy. The manner in which these emitted wavelets superimpose and combine with each other depend on the spatial distribution of the scattering atoms. As we know from the previous chapter, the scattering process is responsible for the *index of refraction*, as well as the resultant *reflected* and *refracted* waves. This atomistic description is quite satisfying conceptually, even though it is not a simple matter to treat analytically. It should, however, be kept in mind even when applying macroscopic techniques, as indeed we shall later on.

We now seek to determine the general principles governing or at least describing the propagation, reflection, and refraction of light. In principle it should be possible to trace the progress of radiant energy through any system by applying Maxwell's equations and the associated boundary conditions. In practice, however, this is often an impractical if not an impossible task (see Section 10.1). So we shall take a somewhat different route, stopping, when appropriate, to verify that our results are in accord with electromagnetic theory.

4.2 THE LAWS OF REFLECTION AND REFRACTION

4.2.1 Huygens's Principle

Recall that a wavefront is a surface over which an optical disturbance has a constant phase. As an illustration, Fig. 4.1 shows a small portion of a spherical wavefront Σ emanating from a monochromatic point source S in a homogeneous medium. Clearly, if the radius of the wavefront as shown is r, at some later time t it will simply be $(r + vt)$, where v is the phase velocity of the wave.

But suppose instead that the light passes through a nonuniform sheet of glass, as in Fig. 4.2, so that the wavefront itself is distorted. How can we determine its new form Σ′? Or for that matter, what will Σ′ look like at some later time, if it is allowed to continue unobstructed?

A preliminary step toward the solution of this problem appeared in print in 1690 in the work entitled *Traité de la Lumière*, which had been written 12 years earlier by the Dutch physicist Christiaan Huygens. It was there that he enunciated what has since become known as **Huygens's principle**, that *every point on a primary wavefront serves as the source of spherical secondary wavelets, such that the primary wavefront at some later time is the envelope of these wavelets. Moreover, the wavelets advance with a speed and frequency equal to those of the primary wave at each point in space.* If the medium is homogeneous, the wavelets may be constructed with finite radii, whereas if it is inhomogeneous, the wavelets must have infinitesimal radii. Figure 4.3 should make this fairly clear; it shows a view of a wavefront Σ, as well as a number of spherical secondary wavelets, which, after a time t, have propagated out to a radius of vt. The envelope of all these wavelets is then asserted to correspond to the advanced primary wave Σ′. It is easy to visualize the process in terms of mechanical vibrations of an elastic medium. Indeed this is the way that Huygens envisioned it within the context of an all-pervading aether, as is evident from this comment by him:

> We have still to consider, in studying the spreading out of these waves, that each particle of matter in which a wave proceeds not only communicates its motion to the next particle to it, which is on the straight line drawn from the luminous point, but that it also necessarily gives a motion to all the others which touch it and which oppose its motion. The result is that around each particle there arises a wave of which this particle is a center.

We can make use of these ideas in two different ways. On one level, a mathematical representation of the wavelets will serve as the basis for a valuable analytical technique in treating diffraction theory. One can trace the progress of a primary wave past all sorts of apertures and obstacles by summing up the wavelet contributions mathematically. On another level, Fig. 4.3 represents a graphical application of the essential ideas and as such is known as *Huygens's construction*.

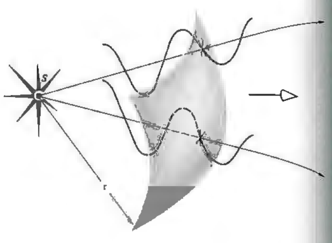


Figure 4.1 A segment of a spherical wave.

Thus far we have merely stated Huygens's principle, without any justification or proof of its validity. As we shall see (Chapter 10), Fresnel successfully modified Huygens's principle somewhat in the 1800s. A little later on, Kirchhoff showed that the *Huygens–Fresnel principle* was a direct consequence of the differential wave equation (2.59), thereby putting it on a firm mathematical base. That there was a need for a reformulation of the principle is evident from Fig. 4.3, where we deceptively only drew hemispherical wavelets.* Had we drawn them as spheres, there would have been a *back-wave* moving toward the source—something that is not observed. Since this difficulty was taken care of theoretically by Fresnel and Kirchhoff, we need not be disturbed by it. In fact, we shall overlook it completely when applying Huygens's construction, which, in the end, is best thought of as a highly useful fiction.

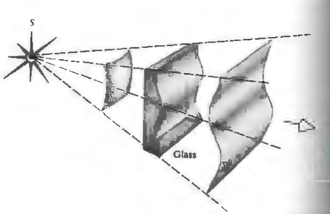


Figure 4.2 Distortion of a portion of a wavefront on passing through a material of nonuniform thickness.

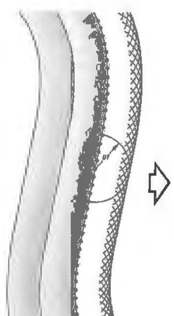


Figure 4.3 The propagation of a wavefront via Huygens's principle.

Still, Huygens's principle fits in rather nicely with our earlier discussion of the atomic scattering of radiant energy. Each atom of a material substance that interacts with an incident primary wavefront can be regarded as a point source of scattered secondary wavelets. Things are not quite as clear when we apply the principle to the propagation of light through a vacuum. It is helpful, however, to keep in mind that at any point in empty space on the primary wavefront there exists both a time-varying **E**-field and a time-varying **B**-field. These in turn create new fields that move out from the point. In this sense each point on the wavefront is analogous to a physical scattering center.

* See E. Hecht, *Phys. Teach.* **18**, 149 (1980).

4.2.2 Snell's Law and the Law of Reflection

The fundamental laws of reflection and refraction can be derived in several different ways; the first approach to be used here is based on Huygens's principle. It should be said, however, that our intention at the moment is as much to elaborate on the use of the method as to arrive at the end results. Huygens's principle will provide a highly useful and fairly simple means of analyzing and visualizing some complex propagation problems, for example, those involving anisotropic media (p. 287) or diffraction (p. 392). Consequently, it is to our advantage to gain some practice in using the technique, even if it is not the most elegant procedure for deriving the desired laws.

Figure 4.4 shows a monochromatic plane wave impinging normally down onto the smooth interface separating two homogeneous transparent media. When an incident wave comes into contact with the interface, it can be imagined as split into two: we observe one wave reflected upward and another transmitted downward. If we consider an incident wavefront Σ_i coincident with the interface splitting into Σ_r and Σ_t, both also congruent with the interface, we can utilize Huygens's construction (neglecting the back-waves). Every point on Σ_i serves as a source of secondary wavelets, which travel more or less upward into the incident medium at a speed v_i. At a time t later, the front will advance a distance $v_i t$ and appear as Σ_r'. Similarly, every point on the downward-moving front Σ_t will serve as a source for wavelets essentially heading down with a speed v_t. After a time t the transmitted front will appear a distance $v_t t$ below as Σ_t'.

The process is ongoing, repeating itself with the frequency of the incident wave.* The media are

* This assumes the use of light whose flux density is not so extraordinarily high that the fields are gigantic. With this assumption the medium will behave linearly, as is most often the case. In contrast, observable harmonics can be generated if the fields are made large enough (Section 14.4).

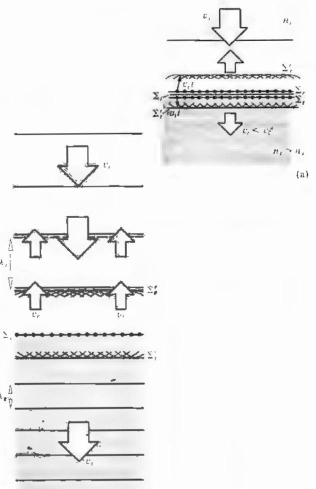


Figure 4.4 A monochromatic plane wave impinging down onto a homogeneous, isotropic medium of index n_t. Σ_i, Σ_r, and Σ_t should actually overlap.

assumed to respond linearly, so the reflected and transmitted waves have that same frequency (and period), as do all the secondary wavelets. Taking $n_t > n_i$, it follows that $c/v_t > c/v_i$, thus $v_t < v_i$, and the wavelengths (the distances between wavefronts drawn in consecutive intervals of τ) will be such that $\lambda_i > \lambda_t$ and $\lambda_i = \lambda_r$, as shown in Fig. 4.4(b). The incoming plane wave is perpendicular to the interface, and symmetry produces both reflected and transmitted plane waves that also travel out from the interface perpendicularly.

Now suppose the incident wave comes in at some other angle, as indicated in Fig. 4.5. Clearly, it sweeps across the interface again, essentially splitting into two waves: one reflected and one refracted. Let's follow the progress of a typical front in Fig. 4.6, envisioning the diagram as if it were a series of snapshots taken in successive intervals of time τ. Start when Σ_i makes contact with the interface at point *a*. At that point, both the reflected and transmitted wavefronts begin, so *a*, which lies on both fronts, can be taken as a source of both an upwardly emitted wavelet traveling at a speed v_i and a downwardly emitted wavelet traveling at a speed v_t. Now focus on another point, say, *b* on Σ_i.

After a time t_1 the plane Σ_i will have moved a distance in the incident medium of $v_i t_1$, so that *b* then corresponds to *b'*. Presumably, two wavelets will then propagate out from *b'* into the incident and transmitting media, contributing to the reflected, Σ_r', and transmitted, Σ_t', wavefronts. These wavelets are shown here after a time t_2, where $\tau = t_1 + t_2$. The rest of the diagram

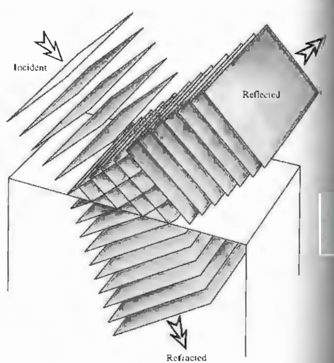


Figure 4.5 Reflection and transmission of plane waves.

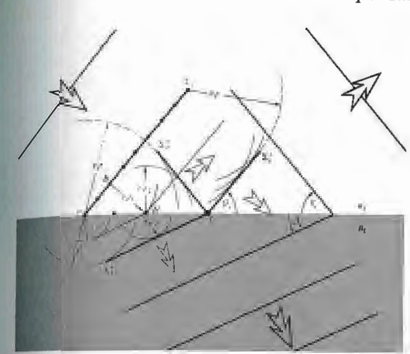


Figure 4.6 Reflection and transmission at an interface via Huygens's principle.

should be self-explanatory. Figure 4.7 is a somewhat simplified version in which θ_i, θ_r, and θ_t, as before, are the angles of *incidence*, *reflection*, and *transmission* (or *refraction*), respectively. Notice that

$$\frac{\sin\theta_i}{\overline{BD}} = \frac{\sin\theta_r}{\overline{AC}} = \frac{\sin\theta_t}{\overline{AE}} = \frac{1}{\overline{AD}}. \tag{4.1}$$

By comparison with Fig. 4.6, it should be evident that

$$\overline{BD} = v_i t, \qquad \overline{AC} = v_i t, \qquad \overline{AE} = v_t t,$$

Substituting into Eq. (4.1) and canceling t, we have

$$\frac{\sin\theta_i}{v_i} = \frac{\sin\theta_r}{v_i} = \frac{\sin\theta_t}{v_t}. \tag{4.2}$$

It follows from the first two terms that **the angle of incidence equals the angle of reflection**, that is,

$$\theta_i = \theta_r. \tag{4.3}$$

Known as the **law of reflection**, it first **appeared** in the book entitled ***Catoptrics***, which was **purported** to have **been written by Euclid.**

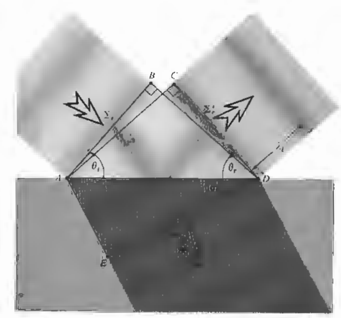


Figure 4.7 Reflected and transmitted wavefronts at a given instant.

The first and last terms of Eq. (4.2) yield

$$\frac{\sin\theta_i}{\sin\theta_t} = \frac{v_i}{v_t}, \tag{4.4}$$

or since $v_i/v_t = n_t/n_i$,

$$n_i \sin\theta_i = n_t \sin\theta_t. \tag{4.5}$$

This is the very important **law of refraction**, the physical consequences of which have been studied, at least on record, for over eighteen hundred years. On the basis of some fine observations, Claudius Ptolemy of Alexandria attempted unsuccessfully to divine the expression. Kepler nearly succeeded in deriving the law of refraction in his book *Supplements to Vitello* in 1604. Unfortunately he was misled by some erroneous data compiled earlier by Vitello (ca. 1270). The correct relationship seems to have been arrived at first by Snell* at the University of Leyden and then by the French mathematician Descartes.† In English-speaking countries Eq. (4.5) is generally referred to as **Snell's law**. Notice that it can be rewritten in the form

$$\frac{\sin\theta_i}{\sin\theta_t} = n_{ti}, \tag{4.6}$$

where $n_{ti} = n_t/n_i$ is the *ratio of the absolute indices of refraction*. In other words, it is the *relative index of refraction of the two media*. It is evident in Fig. 4.6, where $n_{ti} > 1$ (i.e., $n_t > n_i$ and $v_i > v_t$), that $\lambda_i > \lambda_t$, whereas the opposite would be true if $n_{ti} < 1$.

One feature of the above treatment merits some further discussion. It was reasonably assumed that each point on the interface, such as *c* in Fig. 4.6, coincides with a particular point on each of the incident, reflected, and transmitted waves. In other words, there is a fixed phase relationship between each of the waves at points *a*, *b*, *c*, and so forth. As the incident front sweeps across the interface, every point on it in contact with the interface is also a point on both a corresponding reflected front and a corresponding transmitted front. This situation is known as *wavefront continuity*, and it will be

*This is the common spelling, although Snel is probably more accurate.

† For a more detailed history, see Max Herzberger, "Optics from Euclid to Huygens," *Appl. Opt.* 5, 1383 (1966).

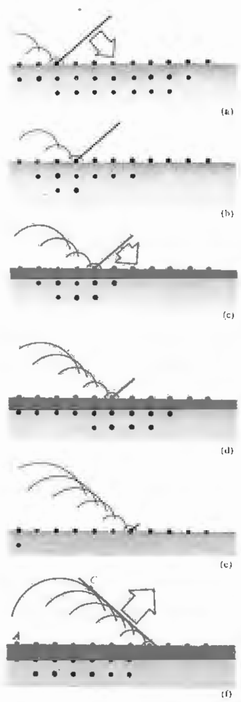


Figure 4.8 The reflection of a wave as the result of scattering.

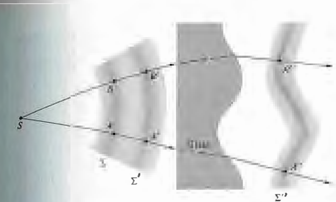


Figure 4.9 Wavefronts and rays.

justified in a more mathematically rigorous treatment in Section 4.3.1. Interestingly, Sommerfeld* has shown that the laws of reflection and refraction (independent of the kind of wave involved) can be derived directly from the requirement of wavefront continuity without any recourse to Huygens's principle, and the solution to Problem 4.9 demonstrates as much.

A far more physically appealing view of the whole process is depicted in Fig. 4.8. An electromagnetic disturbance whose wavelength (λ) is several thousand times larger than the spacing between the atoms ($d \approx 0.1$ nm) sweeps across an interface. Each atom is driven successively and scatters a wavelet. The tilt of the incident wave determines the phase delay between the scattering of each atom in turn (see Section 10.1.3 for the details). The front running from *C* to *D* is composed of wavelets that arrive in phase, superimpose, and interfere constructively. Since every point on the incident front (ranging from *A* to *B* in Fig. 4.7) has the same phase, if $\overline{AC} = \overline{BD}$, the distances traveled and therefore the phases of the wavelets arriving at *C* and *D* will be equal, as indeed they will be all across the front. From the geometry, **this can happen only for a reflected wavefront propagating in the one direction such that $\theta_i = \theta_r$. This picture of scattered interfering wavelets is essentially an atomic version of the Huygens–Fresnel principle.**

Although theoretically all the dipoles throughout the medium contribute to the reflected wave, the dominant effect is due to a surface layer only about $\frac{1}{2}\lambda$ thick, which is nonetheless typically several thousand atoms deep. Furthermore, the condition that only one beam is reflected is true provided that $\lambda \gg d$; it would not be the case with x-rays where $\lambda \approx d$, and there several scattered beams actually result; nor is it the case with a diffraction grating, where the separation between scatterers is again comparable to λ, and several reflected and transmitted beams are produced. A similar argument can be made for the scattering process giving rise to the transmitted wave and Snell's law, as Problem 4.11 establishes.

4.2.3 Light Rays

The concept of a light ray is one that will be of interest to us throughout our study of optics. *A* **ray** *is a line drawn in space corresponding to the direction of flow of radiant energy.* As such, it is a mathematical device rather than a physical entity. In practice one can produce very narrow *beams* or *pencils* of light (e.g., a laserbeam), and we might imagine a ray to be the unattainable limit on the narrowness of such a beam. Bear in mind that in an *isotropic medium* (i.e., one whose properties are the same in all directions) *rays are orthogonal trajectories of the wavefronts.* That is to say, *they are lines normal to the wavefronts at every point of intersection.* Evidently, *in such a medium a ray is parallel to the propagation vector* **k**. As you might suspect, this is not true in *anisotropic* substances, which we will consider later (see Section 8.4.1). *Within homogeneous isotropic materials, rays will be straight lines,* since by symmetry they cannot bend in any preferred direction, there being none. Moreover, because the speed of propagation is identical in all directions within a given medium, the spatial separation between two wavefronts, measured along rays, must be the same everywhere.* Points where a single ray intersects a set of wavefronts are called *corresponding points,* for example, *A*, *A'*, and *A''* in Fig. 4.9. *Evidently the separation in time between any two corresponding points on any two*

* A. Sommerfeld, *Optics,* p. 151. See also J. J. Sein, *Am. J. Phys.* **50**, 180 (1982).

* When the material is inhomogeneous or when there is more than one medium involved, it will be the *optical path length* (see Section 4.2.4) between the two wavefronts that is the same.

sequential wavefronts is identical. In other words, if wavefront Σ is transformed into Σ'' after a time t'', the distance between corresponding points on any and all rays will be traversed in that same time t''. This will be true even if the wavefronts pass from one homogeneous isotropic medium into another. This just means that each point on Σ can be imagined as following the path of a ray to arrive at Σ'' in the time t''.

If a group of rays is such that we can find a surface that is orthogonal to each and every one of them, they are said to form a *normal congruence*. For example, the rays emanating from a point source are perpendicular to a sphere centered at the source and consequently form a normal congruence.

We can now briefly consider an alternative to Huygens's principle that will also allow us to follow the progress of light through various isotropic media. The basis for this approach is the *theorem of Malus and Dupin* (introduced in 1808 by E. Malus and modified in 1816 by C. Dupin), according to which *a group of rays will preserve its normal congruence after any number of reflections and refractions* (as in Fig. 4.9). From our present vantage point of the wave theory, this is equivalent to the statement that rays remain orthogonal to wavefronts throughout all propagation processes in isotropic media. As shown in Problem 4.12, the theorem can be used to derive the law of reflection as well as Snell's law. It is often most convenient to carry out a ray trace through an optical system using the laws of reflection and refraction and then reconstruct the wavefronts. The latter can be accomplished in accord with the above considerations of equal transit times between corresponding points and the orthogonality of the rays and wavefronts.

Figure 4.10 depicts the parallel ray formation concomitant with a plane wave, where θ_i, θ_r, and θ_t, which have the exact same meanings as before, are now measured from the normal to the interface. The incident ray and the normal determine a plane known as the **plane of incidence**. Because of the symmetry of the situation, we must anticipate that both the reflected and transmitted rays will be undeflected from that plane. In other words, the respective unit propagation vectors $\hat{\mathbf{k}}_i$, $\hat{\mathbf{k}}_r$, and $\hat{\mathbf{k}}_t$ are coplanar.

In summary, then, the three basic laws of reflection and refraction are:

1. The incident, reflected, and refracted rays all lie in the plane of incidence.
2. $\theta_i = \theta_r$. [4.3]
3. $n_i \sin\theta_i = n_t \sin\theta_t$. [4.5]

These are illustrated rather nicely with a narrow light beam in the photographs of Fig. 4.11. Here, the incident medium is air ($n_i \approx 1.0$), and the transmitting medium is glass ($n_t \approx 1.5$). Consequently, $n_i < n_t$, and it follows

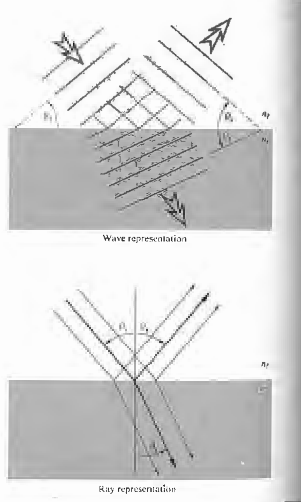


Figure 4.10 The wave and ray representations of an incident, reflected, and transmitted beam.

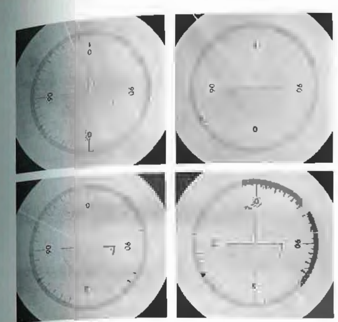


Figure 4.11 Refraction at various angles of incidence. (Photos courtesy *PSSC College Physics*, D. C. Heath & Co., 1968.)

from Snell's law that $\sin\theta_i > \sin\theta_t$. Since both angles, θ_i and θ_t, vary between 0° and 90°, a region over which the sine function is smoothly rising, it can be concluded that $\theta_i > \theta_t$. *Rays entering a higher-index medium from a lower one refract toward the normal* and vice versa. This result is evident in the figure. Notice that the bottom surface is cut circular so that the transmitted beam within the glass always lies along a radius and is therefore normal to the lower surface in every case. If a ray is normal to an interface, $\theta_i = 0 = \theta_t$, and it sails right through with no bending.

The incident beam in each portion of Fig. 4.11 is narrow and sharp, and the reflected beam is equally well defined. Accordingly, the process is known as **specular reflection** (from the word for a common mirror alloy in ancient times, speculum). **In this case, as in Fig. 4.12(a), the reflecting surface is smooth, or more precisely, any irregularities in it are small compared with a wavelength.*** **In contrast, the diffuse reflection** in Fig. 4.12(b) occurs when the surface is relatively rough. For example, "nonreflecting" glass used to cover pictures is actually glass whose surface is roughened so that it reflects diffusely. The law of reflection holds exactly over any region that is small enough to be considered smooth. These two forms of reflection are extremes; a whole range of intermediate behavior is possible. Thus, although the paper of this page was manufactured deliberately to be a fairly diffuse scatterer, the cover of the book reflects in a manner that is somewhere between diffuse and specular.

Let $\hat{\mathbf{u}}_n$ be a unit vector normal to the interface pointing in the direction from the incident to the transmitting medium (Fig. 4.13). As you will have the opportunity to prove in Problem 4.13, the first and third basic laws can be combined in the form of a *vector refraction equation:*

$$n_i(\hat{\mathbf{k}}_i \times \hat{\mathbf{u}}_n) = n_t(\hat{\mathbf{k}}_t \times \hat{\mathbf{u}}_n) \qquad [4.7]$$

or, alternatively,

$$n_t\hat{\mathbf{k}}_t - n_i\hat{\mathbf{k}}_i = (n_t \cos\theta_t - n_i \cos\theta_i)\hat{\mathbf{u}}_n. \qquad [4.8]$$

4.2.4 Fermat's Principle

The laws of reflection and refraction, and indeed the manner in which light propagates in general, can be viewed from an entirely different and intriguing perspective afforded us by **Fermat's principle**. The ideas that will unfold presently have had a tremendous influence on the development of physical thought in and beyond the study of classical optics. Apart from its implications in quantum optics (Section 13.6, p. 552), Fermat's principle provides us with an insightful and highly useful way of appreciating and anticipating the behavior of light.

Hero of Alexandria, who lived some time between 150 B.C. and 250 A.D., was the first to set forth what has since become known as a *variational principle*. In his formulation of the law of reflection, he asserted that *the path actually taken by light in going from some point S to a point P via a reflecting surface was the shortest possible one.* This can be seen rather easily in Fig. 4.14, which depicts a point source S emitting a number of rays that are

* If the surface ridges and valleys are small compared with λ, the scattered wavelets will still interfere constructively in only one direction ($\theta_i = \theta_r$).

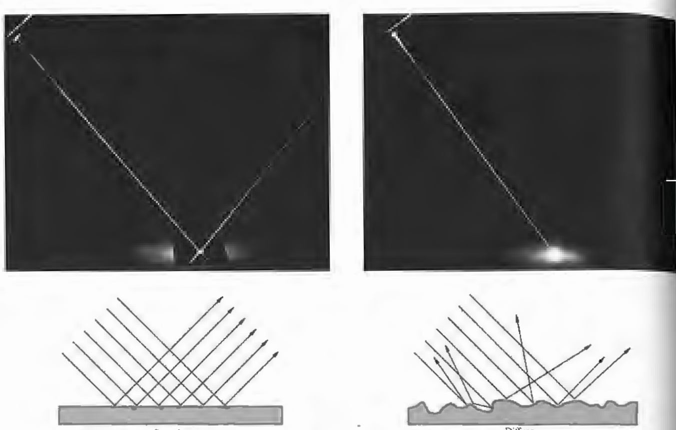


Figure 4.12 (a) Specular reflection. (b) Diffuse reflection. (Photos courtesy Donald Dunitz.)

then "reflected" toward P. Of course, only one of these paths will have any physical reality. If we simply draw the rays as if they emanated from S' (the image of S), none of the distances to P will have been altered (i.e., $SAP = S'AP$, $SBP = S'BP$, etc.). But obviously the straight-line path $S'BP$, which corresponds to $\theta_i = \theta_r$, is the shortest possible one. The same kind of reasoning (Problem 4.15) makes it evident that points S, B, and P must lie in what has previously been defined as the plane of incidence. For over fifteen hundred years Hero's curious observation stood alone, until in 1657 Fermat propounded his celebrated *principle of least time*, which encompassed both reflection and refraction. Obviously, a beam of light traversing an interface does not take a straight line or *minimum spatial path* between a point in the incident medium and one in the transmitting medium. Fermat consequently reformulated Hero's statement to read: *the actual path between [illegible] points taken by a beam of light is the one that is traversed in the least time.* As we shall see, even this form of [illegible] statement is somewhat incomplete and a bit erroneous at that. For the moment then, let us embrace it but not passionately.

As an example of the application of the principle to the case of refraction, refer to Fig. 4.15, where we minimize t, the transit time from S to P, with respect to the variable x. In other words, changing x shifts point O, thereby changing the ray from S to P. The smallest

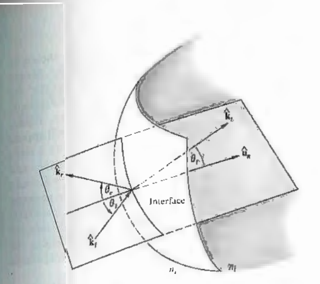


Figure 4.13 The ray geometry.

[illegible] time will then presumably coincide with the [illegible] path. Hence

$$t = \frac{\overline{SO}}{v_i} + \frac{\overline{OP}}{v_t}$$

or

$$t = \frac{(h^2 + x^2)^{1/2}}{v_i} + \frac{[b^2 + (a - x)^2]^{1/2}}{v_t}.$$

[illegible] $t(x)$ with respect to variations in x, we set [illegible], that is,

$$\frac{dt}{dx} = \frac{x}{v_i(h^2 + x^2)^{1/2}} + \frac{-(a - x)}{v_t[b^2 + (a - x)^2]^{1/2}} = 0.$$

[illegible] the diagram, we can rewrite the expression as

$$\frac{\sin \theta_i}{v_i} = \frac{\sin \theta_t}{v_t},$$

[illegible] of course no less than Snell's law (Eq. 4.4). [illegible] a beam of light is to advance from S to P in [illegible] possible time, it must comply with the empirical [illegible] refraction.

Suppose that we have a stratified material composed [illegible] layers, each having a different index of refraction, as in Fig. 4.16. The transit time from S to P will then be

$$t = \frac{s_1}{v_1} + \frac{s_2}{v_2} + \cdots + \frac{s_m}{v_m}$$

or

$$t = \sum_{i=1}^{m} s_i/v_i,$$

where s_i and v_i are the path length and speed, respectively, associated with the ith contribution. Thus

$$t = \frac{1}{c}\sum_{i=1}^{m} n_i s_i, \tag{4.9}$$

in which the summation is known as the **optical path length** (OPL) traversed by the ray, in contrast to the spatial path length $\sum_{i=1}^{m} s_i$. Clearly, for an inhomogeneous medium where n is a function of position, the summation must be changed to an integral:

$$(\text{OPL}) = \int_S^P n(s)\, ds. \tag{4.10}$$

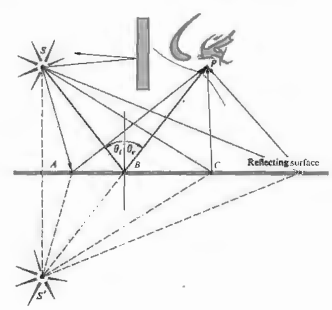


Figure 4.14 Minimum path from the source S to the observer's eye at P.

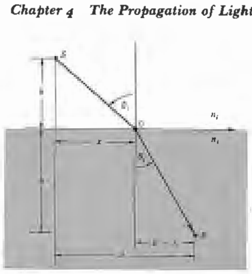


Figure 4.15 Fermat's principle applied to refraction.

Inasmuch as $t = (\text{OPL})/c$, we can restate Fermat's principle: *light, in going from points S to P, traverses the route having the smallest optical path length.* Accordingly, when light rays from the Sun pass through the inhomogeneous atmosphere of the Earth, as shown in Fig. 4.17(a), they bend so as to traverse the lower, denser regions as abruptly as possible, thus minimizing the OPL. Ergo, one can still see the Sun after it has actually passed below the horizon. In the same way, a road viewed at a glancing angle, as in Fig. 4.17(b), will appear to reflect the environs as if it were covered with a sheet of water. The air near the roadway will be warmer and less dense than that farther above it. Rays will bend upward, taking the shortest optical path, and in so doing they will appear to be reflected from a mirrored surface. The effect is particularly easy to see on long modern highways. The only requirement is that you look at the road at near glancing incidence, because the rays bend very gradually.

The original statement of Fermat's *principle of least time* has some serious failings and is, as we shall see, in need of alteration. To that end, recall that if we have a function, say $f(x)$, we can determine the specific value of the variable x that causes $f(x)$ to have a *stationary* value by setting $df/dx = 0$ and solving for x. By a stationary value we mean one for which the slope of $f(x)$ versus x is zero or equivalently where the function has a maximum, minimum, or a point of inflection with a horizontal tangent.

Fermat's principle in its modern form reads: *a light ray in going from point S to point P must traverse an optical path length that is stationary with respect to variations of that path.* In other words, the OPL for the true trajectory will equal, to a first approximation, the OPL of paths immediately adjacent to it.* Thus there will be many curves neighboring the actual one, which would take nearly the same time for the light to traverse. This latter point makes it possible to begin to understand how light manages to be so clever in its meanderings. Suppose that we have a beam of light advancing through a homogeneous isotropic medium so that a ray passes from points S to P. Atoms within the material are driven by the incident disturbance, and they reradiate in all directions. Generally, wavelets originating in the immediate vicinity of a stationary path will arrive at P by routes that differ only slightly and will therefore arrive nearly in phase and reinforce each other (see Section 7.1). Wavelets taking other paths will arrive at P out of phase and will therefore tend to cancel each other. That being the case, energy will effectively propagate along that ray from S to P that satisfies Fermat's principle.

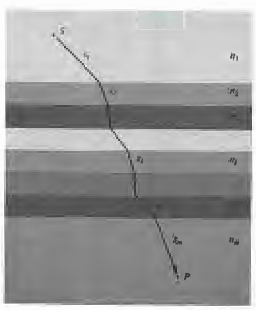


Figure 4.16 A ray propagating through a layered material.

*The first derivative of the OPL vanishes in its Taylor series expansion, since the path is stationary.

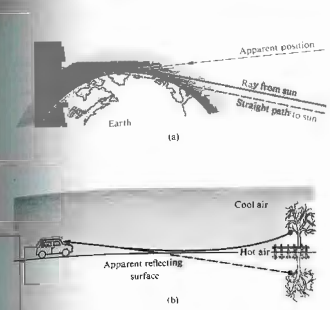


Figure 4.17 The bending of rays through inhomogeneous media.

To show that the OPL for a ray need not always be a minimum, examine Fig. 4.18, which depicts a segment of a hollow three-dimensional ellipsoidal mirror. If the source S and the observer P are at the foci of the ellipsoid, then by definition the length SQP will be constant, regardless of where on the perimeter Q happens to be. It is also a geometrical property of the ellipse that $\theta_i = \theta_r$ for any location of Q. All optical paths from S to P via a reflection are therefore precisely equal—none is a minimum, and the OPL is clearly stationary with respect to variations. Rays leaving S and striking the mirror will arrive at the focus P. From another viewpoint we can say that radiant energy emitted by S will be scattered by electrons in the mirrored surface such that the wavelets will substantially reinforce each other only at P, where they have traveled the same distances and have the same phase. In any case, if a plane mirror was tangent to the ellipse at Q, the exact same

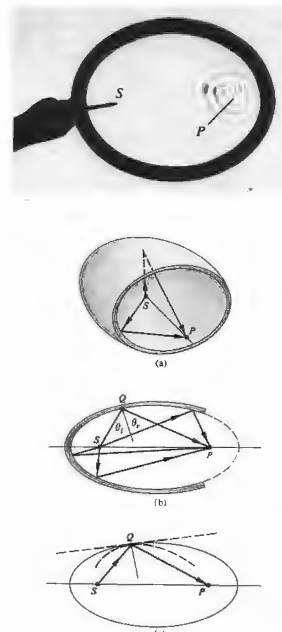


Figure 4.18 Reflection off an ellipsoidal surface. Observe the reflection of waves using a frying pan filled with water. Even though these are usually circular it is well worth playing with. (Photo courtesy *PSSC College Physics*, D. C. Heath & Co., 1968.)

path *SQP* traversed by a ray would then be a relative minimum. At the other extreme, if the mirrored surface conformed to a curve lying within the ellipse, like the dashed one shown, that same ray along *SQP* would now negotiate a relative maximum OPL. This is true even though other unused paths (where $\theta_i \neq \theta_r$) would actually be shorter (i.e., apart from inadmissible curved paths). Thus in all cases the rays travel a stationary OPL in accord with the reformulated Fermat's principle. Note that since the principle speaks only about the path and not the direction along it, a ray going from *P* to *S* will trace the same route as one from *S* to *P*. This is the very useful ***principle of reversibility.***

Fermat's achievement stimulated a great deal of effort to supersede Newton's laws of mechanics with a similar variational formulation. The work of many men, notably Pierre de Maupertuis (1698–1759) and Leonhard Euler, finally led to the mechanics of Joseph Louis Lagrange (1736–1813) and hence to the ***principle of least action,*** formulated by William Rowan Hamilton (1805–1865). The striking similarity between the principles of Fermat and Hamilton played an important part in Schrödinger's development of quantum mechanics. In 1942 Richard Phillips Feynman (b. 1918) showed that quantum mechanics can be fashioned in an alternative way using a variational approach. The continuing evolution of variational principles brings us back to optics via the modern formalism of quantum optics (see Chapter 13).

Fermat's principle is not so much a computational device as it is a concise way of thinking about the propagation of light. It is a statement about the grand scheme of things without any concern for the contributing mechanisms, and as such it will yield insights under a myriad of circumstances.

4.3 THE ELECTROMAGNETIC APPROACH

Thus far we have been able to deduce the laws of reflection and refraction using three different approaches: *Huygens' principle,* the *theorem of Malus and Dupin,* and *Fermat's principle.* Each yields a distinctive and valuable point of view. Yet another and even more powerful approach is provided by the electromagnetic theory of light. Unlike the previous techniques, which say nothing about the incident, reflected, and transmitted radiant flux densities (i.e., I_i, I_r, I_t, respectively), the electromagnetic theory treats these within the framework of a far more complete description.

The body of information that forms the subject of optics has accrued over many centuries. As our knowledge of the physical universe becomes more extensive, the concomitant theoretical descriptions must become ever more encompassing. This, quite generally, brings with it an increased complexity. And so, rather than using the formidable mathematical machinery of the quantum theory of light, we will often avail ourselves of the simpler insights of simpler times (e.g., Huygens' and Fermat's principles). Thus even though we are now going to develop another and more extensive description of reflection and refraction, we will not put aside those earlier methods. In fact, throughout this study we shall use the simplest technique that can yield sufficiently accurate results for our particular purpose.

4.3.1 Waves at an Interface

Suppose that the incident monochromatic lightwave is planar, so that it has the form

$$\mathbf{E}_i = \mathbf{E}_{0i} \exp\left[i(\mathbf{k}_i \cdot \mathbf{r} - \omega_i t)\right] \tag{4.11}$$

or, more simply,

$$\mathbf{E}_i = \mathbf{E}_{0i} \cos(\mathbf{k}_i \cdot \mathbf{r} - \omega_i t). \tag{4.12}$$

Assume that $\mathbf{E}_{0i}$ is constant in time, that is, the wave is linearly or plane polarized. We'll find in Chapter 8 that any form of light can be represented by two orthogonal linearly polarized waves, so that this doesn't actually represent a restriction. Note that just as the origin in time, $t = 0$, is arbitrary, so too is the origin *O* in space where $\mathbf{r} = 0$. Thus, making no assumptions about their directions, frequencies, wavelengths, phases, or amplitudes, we can write the reflected and transmitted waves as

$$\mathbf{E}_r = \mathbf{E}_{0r} \cos(\mathbf{k}_r \cdot \mathbf{r} - \omega_r t + \varepsilon_r) \tag{4.13}$$

and

$$\mathbf{E}_t = \mathbf{E}_{0t} \cos(\mathbf{k}_t \cdot \mathbf{r} - \omega_t t + \varepsilon_t). \tag{4.14}$$

Here ε_r and ε_t are *phase constants* relative to $\mathbf{E}_i$ and are introduced because the position of the origin is not unique. Figure 4.19 depicts the waves in the vicinity of the planar interface between two homogeneous lossless dielectric media of indices n_i and n_t.

The laws of electromagnetic theory (Section 3.1) lead to certain requirements that must be met by the fields, and these are referred to as the boundary conditions. Specifically, one of these is that the component of the electric field intensity **E** that is tangent to the interface must be continuous across it (the same is true for **H**). In other words, the total tangential component of **E** on one side of the surface must equal that on the other (Problem 4.22). Thus since $\hat{\mathbf{u}}_n$ is the unit vector normal to the interface, regardless of the direction of the electric field within the wavefront, the cross-product of it with $\hat{\mathbf{u}}_n$ will be perpendicular to $\hat{\mathbf{u}}_n$ and therefore tangent to the interface. Hence

$$\hat{\mathbf{u}}_n \times \mathbf{E}_i + \hat{\mathbf{u}}_n \times \mathbf{E}_r = \hat{\mathbf{u}}_n \times \mathbf{E}_t \tag{4.15}$$

or

$$\begin{aligned}\hat{\mathbf{u}}_n \times \mathbf{E}_{0i} \cos(\mathbf{k}_i \cdot \mathbf{r} - \omega_i t) \\ + \hat{\mathbf{u}}_n \times \mathbf{E}_{0r} \cos(\mathbf{k}_r \cdot \mathbf{r} - \omega_r t + \varepsilon_r) \\ = \hat{\mathbf{u}}_n \times \mathbf{E}_{0t} \cos(\mathbf{k}_t \cdot \mathbf{r} - \omega_t t + \varepsilon_t).\end{aligned} \tag{4.16}$$

This relationship must obtain at any instant in time and at any point on the interface ($y = b$). Consequently, $\mathbf{E}_i$, $\mathbf{E}_r$, and $\mathbf{E}_t$ must have precisely the same functional dependence on the variables t and r, which means that

$$\begin{aligned}(\mathbf{k}_i \cdot \mathbf{r} - \omega_i t)|_{y=b} &= (\mathbf{k}_r \cdot \mathbf{r} - \omega_r t + \varepsilon_r)|_{y=b} \\ &= (\mathbf{k}_t \cdot \mathbf{r} - \omega_t t + \varepsilon_t)|_{y=b}.\end{aligned} \tag{4.17}$$

With this as the case, the cosines in Eq. (4.16) cancel, leaving an expression independent of t and r, as indeed it must be. Inasmuch as this has to be true for all values of time, the coefficients of t must be equal, to wit

$$\omega_i = \omega_r = \omega_t. \tag{4.18}$$

Recall that the electrons within the media are undergoing (linear) forced vibrations at the frequency of the incident wave. Clearly, whatever light is scattered has that same frequency. Furthermore,

$$\begin{aligned}(\mathbf{k}_i \cdot \mathbf{r})|_{y=b} &= (\mathbf{k}_r \cdot \mathbf{r} + \varepsilon_r)|_{y=b} \\ &= (\mathbf{k}_t \cdot \mathbf{r} + \varepsilon_t)|_{y=b},\end{aligned} \tag{4.19}$$

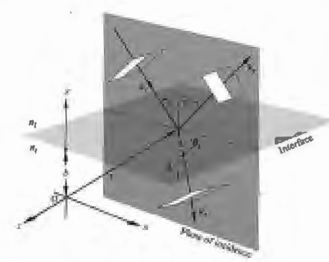


Figure 4.19 Plane waves incident on the boundary between two homogeneous, isotropic, lossless dielectric media.

wherein **r** terminates on the interface. The values of ε_r and ε_t correspond to a given position of *O*, and thus they allow the relation to be valid regardless of that location. (For example, the origin might be chosen such that **r** was perpendicular to $\mathbf{k}_i$ but not to $\mathbf{k}_r$ or $\mathbf{k}_t$.) From the first two terms we obtain

$$[(\mathbf{k}_i - \mathbf{k}_r) \cdot \mathbf{r}]_{y=b} = \varepsilon_r. \tag{4.20}$$

Recalling Eq. (2.42), this expression simply says that the endpoint of **r** sweeps out a plane (which is of course the interface) perpendicular to the vector $(\mathbf{k}_i - \mathbf{k}_r)$. To phrase it slightly differently, $(\mathbf{k}_i - \mathbf{k}_r)$ is parallel to $\hat{\mathbf{u}}_n$. Notice, however, that since the incident and reflected waves are in the same medium, $k_i = k_r$. From the fact that $(\mathbf{k}_i - \mathbf{k}_r)$ has no component in the plane of the interface, that is, $\hat{\mathbf{u}}_n \times (\mathbf{k}_i - \mathbf{k}_r) = 0$, we conclude that

$$k_i \sin\theta_i = k_r \sin\theta_r;$$

hence we have the law of reflection, that is,

$$\theta_i = \theta_r.$$

Furthermore, since $(\mathbf{k}_i - \mathbf{k}_r)$ is parallel to $\hat{\mathbf{u}}_n$ all three vectors, $\mathbf{k}_i$, $\mathbf{k}_r$, and $\hat{\mathbf{u}}_n$, are in the same plane, the plane of incidence. Again, from Eq. (4.19) we obtain

$$[(\mathbf{k}_i - \mathbf{k}_t) \cdot \mathbf{r}]_{y=b} = \varepsilon_t, \tag{4.21}$$

and therefore $(\mathbf{k}_i - \mathbf{k}_t)$ is also normal to the interface.

Thus $\mathbf{k}_i$, $\mathbf{k}_r$, $\mathbf{k}_t$, and $\hat{\mathbf{u}}_n$ are all coplanar. As before, the tangential components of $\mathbf{k}_i$ and $\mathbf{k}_t$ must be equal, and consequently

$$k_i \sin \theta_i = k_t \sin \theta_t. \qquad (4.22)$$

But because $\omega_i = \omega_t$, we can multiply both sides by c/ω, to get

$$n_i \sin \theta_i = n_t \sin \theta_t,$$

which is Snell's law. Finally, if we had chosen the origin O to be in the interface, it is evident from Eqs. (4.20) and (4.21) that ε_r and ε_t would both have been zero. That arrangement, although not as instructive, is certainly simpler, and we'll use it from here on.

4.3.2 Derivation of the Fresnel Equations

We have just found the relationship that exists among the phases of $\mathbf{E}_i(\mathbf{r}, t)$, $\mathbf{E}_r(\mathbf{r}, t)$, and $\mathbf{E}_t(\mathbf{r}, t)$ at the boundary. There is still an interdependence shared by the amplitudes $\mathbf{E}_{0i}$, $\mathbf{E}_{0r}$, and $\mathbf{E}_{0t}$, which can now be evaluated. To that end, suppose that a plane monochromatic **wave is incident on the planar surface separating two isotropic media. Whatever the polarization of the wave, we shall resolve its E- and B-fields into components parallel and perpendicular to the plane of incidence and treat these constituents separately.**

Case 1: E perpendicular to the plane of incidence. We now assume that $\mathbf{E}$ is perpendicular to the plane of incidence and that $\mathbf{B}$ is parallel to it (Fig. 4.20). Recall that $E = vB$, so that

$$\hat{\mathbf{k}} \times \mathbf{E} = v\mathbf{B} \qquad (4.23)$$

and, of course,

$$\hat{\mathbf{k}} \cdot \mathbf{E} = 0 \qquad (4.24)$$

(i.e., $\mathbf{E}$, $\mathbf{B}$, and the unit propagation vector $\hat{\mathbf{k}}$ form a right-handed system). Again making use of the continuity of the tangential components of the $\mathbf{E}$-field, we have at the boundary at any time and any point

$$\mathbf{E}_{0i} + \mathbf{E}_{0r} = \mathbf{E}_{0t}, \qquad (4.25)$$

where the cosines cancel. Realize that the field vectors as shown really ought to be envisioned at $y = 0$ (i.e., at the surface), from which they have been displaced for the sake of clarity. Note too that although $\mathbf{E}_r$ and $\mathbf{E}_t$ must be normal to the plane of incidence by symmetry, *we are guessing that they point outward* at the interface when $\mathbf{E}_i$ does. The directions of the B-fields then follow from Eq. (4.23).

We will need to invoke another of the boundary conditions in order to get one more equation. The presence of material substances that become electrically polarized by the wave has a definite effect on the field configuration. Thus, although the tangential component of $\mathbf{E}$ is continuous across the boundary, its normal component is not. Instead the normal component of the product $\epsilon\mathbf{E}$ is the same on either side of the interface. Similarly, the normal component of $\mathbf{B}$ is continuous, as is the tangential component of $\mu^{-1}\mathbf{B}$. Here the effect of the two media appears via their permeabilities μ_i and μ_t. This boundary condition will be the simplest to use, particularly as applied to reflection from the surface of a conductor.* Thus the continuity of the tangential component of $\mathbf{B}/\mu$ requires that

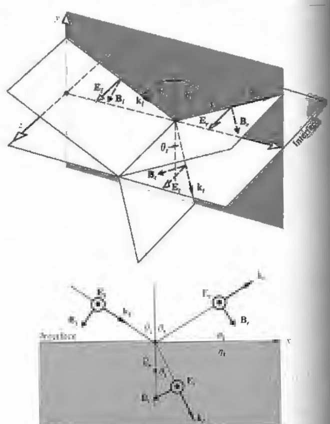


Figure 4.20 An incoming wave whose E-field is normal to the plane of incidence.

$$-\frac{B_i}{\mu_i}\cos\theta_i + \frac{B_r}{\mu_i}\cos\theta_r = -\frac{B_t}{\mu_t}\cos\theta_t, \qquad (4.26)$$

where the left and right sides are the total magnitudes of $\mathbf{B}/\mu$ parallel to the interface in the incident and transmitting media, respectively. The positive direction is that of increasing x, so that the components of $\mathbf{B}_i$ and $\mathbf{B}_t$ appear with minus signs. From Eq. (4.23) we have

$$B_i = E_i/v_i, \qquad (4.27)$$

$$B_r = E_r/v_r, \qquad (4.28)$$

and

$$B_t = E_t/v_t. \qquad (4.29)$$

Thus since $v_i = v_r$ and $\theta_i = \theta_r$, Eq. (4.26) can be written as

$$\frac{1}{\mu_i v_i}(E_i - E_r)\cos\theta_i = \frac{1}{\mu_t v_t}E_t\cos\theta_t. \qquad (4.30)$$

Making use of Eqs. (4.12), (4.13), and (4.14) and remembering that the cosines therein equal one another $y = 0$, we obtain

$$\frac{n_i}{\mu_i}(E_{0i} - E_{0r})\cos\theta_i = \frac{n_t}{\mu_t}E_{0t}\cos\theta_t. \qquad (4.31)$$

Combined with Eq. (4.25), this yields

$$\left(\frac{E_{0r}}{E_{0i}}\right)_\perp = \frac{\dfrac{n_i}{\mu_i}\cos\theta_i - \dfrac{n_t}{\mu_t}\cos\theta_t}{\dfrac{n_i}{\mu_i}\cos\theta_i + \dfrac{n_t}{\mu_t}\cos\theta_t} \qquad (4.32)$$

and

$$\left(\frac{E_{0t}}{E_{0i}}\right)_\perp = \frac{2\dfrac{n_i}{\mu_i}\cos\theta_i}{\dfrac{n_i}{\mu_i}\cos\theta_i + \dfrac{n_t}{\mu_t}\cos\theta_t}. \qquad (4.33)$$

The $\perp$ subscript serves as a reminder that we are dealing with the case in which $\mathbf{E}$ is perpendicular to the plane of incidence. These two expressions, *which are completely general statements applying to any linear, isotropic, homogeneous media,* are two of the **Fresnel equations.** Quite often one deals with dielectrics for which $\mu_i \approx \mu_t \approx \mu_0$; consequently the most common form of these equations is simply

$$r_\perp \equiv \left(\frac{E_{0r}}{E_{0i}}\right)_\perp = \frac{n_i\cos\theta_i - n_t\cos\theta_t}{n_i\cos\theta_i + n_t\cos\theta_t} \qquad (4.34)$$

and

$$t_\perp \equiv \left(\frac{E_{0t}}{E_{0i}}\right)_\perp = \frac{2n_i\cos\theta_i}{n_i\cos\theta_i + n_t\cos\theta_t}. \qquad (4.35)$$

Here $r_\perp$ denotes the **amplitude reflection coefficient**, and $t_\perp$ is the **amplitude transmission coefficient**.

Case 2: E parallel to the plane of incidence. A similar pair of equations can be derived when the incoming E-field lies in the plane of incidence, as shown in Fig. 4.21. Continuity of the tangential components of $\mathbf{E}$ on either side of the boundary leads to

$$E_{0i}\cos\theta_i - E_{0r}\cos\theta_r = E_{0t}\cos\theta_t. \qquad (4.36)$$

In much the same way as before, continuity of the tangential components of $\mathbf{B}/\mu$ yields

$$\frac{1}{\mu_i v_i}E_{0i} + \frac{1}{\mu_r v_r}E_{0r} = \frac{1}{\mu_t v_t}E_{0t}. \qquad (4.37)$$

Using the fact that $\mu_i = \mu_r$ and $\theta_i = \theta_r$, we can combine these formulas to obtain two more of the *Fresnel equations:*

$$r_\parallel \equiv \left(\frac{E_{0r}}{E_{0i}}\right)_\parallel = \frac{\dfrac{n_t}{\mu_t}\cos\theta_i - \dfrac{n_i}{\mu_i}\cos\theta_t}{\dfrac{n_i}{\mu_i}\cos\theta_t + \dfrac{n_t}{\mu_t}\cos\theta_i} \qquad (4.38)$$

* Keeping with our intent to use only the E- and B-fields, at least in the early part of this exposition, we have avoided the usual statement in terms of H, where

$$\mathbf{H} = \mu^{-1}\mathbf{B}. \qquad [A1.14]$$

and

$$t_{\parallel} \equiv \left(\frac{E_{0t}}{E_{0i}}\right)_{\parallel} = \frac{2\dfrac{n_i}{\mu_i}\cos\theta_i}{\dfrac{n_i}{\mu_t}\cos\theta_t + \dfrac{n_t}{\mu_i}\cos\theta_i}. \tag{4.39}$$

When both media forming the interface are dielectrics, the amplitude coefficients become

$$r_{\parallel} = \frac{n_t \cos\theta_i - n_i \cos\theta_t}{n_i \cos\theta_t + n_t \cos\theta_i} \tag{4.40}$$

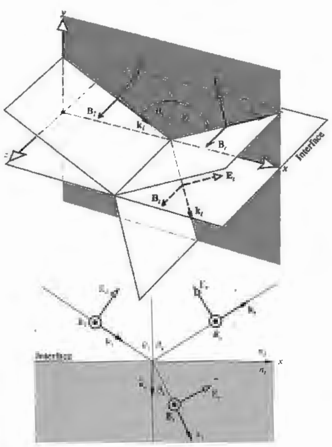


Figure 4.21 An incoming wave whose **E**-field is in the plane of incidence.

and

$$t_{\parallel} = \frac{2n_i \cos\theta_i}{n_i \cos\theta_t + n_t \cos\theta_i}. \tag{4.41}$$

One further notational simplification can be made by availing ourselves of Snell's law, whereupon the Fresnel equations for dielectric media become (Problem 4.?3)

$$r_{\perp} = -\frac{\sin(\theta_i - \theta_t)}{\sin(\theta_i + \theta_t)} \tag{4.42}$$

$$r_{\parallel} = +\frac{\tan(\theta_i - \theta_t)}{\tan(\theta_i + \theta_t)} \tag{4.43}$$

$$t_{\perp} = +\frac{2\sin\theta_t\cos\theta_i}{\sin(\theta_i + \theta_t)} \tag{4.44}$$

$$t_{\parallel} = +\frac{2\sin\theta_t\cos\theta_i}{\sin(\theta_i + \theta_t)\cos(\theta_i - \theta_t)}. \tag{4.45}$$

A note of caution must be introduced before we move on to examine the considerable significance of the preceding calculation. Bear in mind that the directions (or, more precisely, the phases) of the fields in Figs. 4.20 and 4.21 were selected rather arbitrarily. For example, in Fig. 4.20 we could have assumed that $\mathbf{E}_r$ pointed inward, whereupon $\mathbf{B}_r$ would have had to be reversed as well. Had we done that, the sign of $r_{\perp}$ would have turned out to be positive, leaving the other amplitude coefficients unchanged. The signs appearing in Eqs. (4.42) through (4.45), in this case positive, except for the first, correspond to the particular set of field directions selected. The minus sign, as we will see, just means that we didn't guess correctly concerning $\mathbf{E}_r$ in Fig. 4.20. Nonetheless, be aware that the literature is not standardized, and all possible sign variations have been labeled *Fresnel equations*—to avoid confusion *they must be related to the specific field directions from which they were derived.*

4.3.3 Interpretation of the Fresnel Equations

This section is devoted to an examination of the physical implications of the Fresnel equations. In particular, we are interested in determining the fractional amplitudes and flux densities that are reflected and refracted. In addition we shall be concerned with any possible phase shifts that might be incurred in the process.

Amplitude Coefficients

Let's briefly examine the form of the amplitude coefficients over the entire range of θ_i values. At nearly normal incidence ($\theta_i \approx 0$) the tangents in Eq. (4.43) are essentially equal to sines, in which case

$$[r_{\parallel}]_{\theta_i=0} = [-r_{\perp}]_{\theta_i=0} = \left[\frac{\sin(\theta_i - \theta_t)}{\sin(\theta_i + \theta_t)}\right]_{\theta_i=0}.$$

We will come back to the physical significance of the minus sign presently. After we have expanded the sines and used Snell's law, this expression becomes

$$[r_{\parallel}]_{\theta_i=0} = [-r_{\perp}]_{\theta_i=0} = \left[\frac{n_t\cos\theta_i - n_i\cos\theta_t}{n_t\cos\theta_i + n_i\cos\theta_t}\right]_{\theta_i=0}, \tag{4.46}$$

which follows as well from Eqs. (4.34) and (4.40). In the limit, as θ_i goes to 0, $\cos\theta_i$ and $\cos\theta_t$ both approach one, and consequently

$$[r_{\parallel}]_{\theta_i=0} = [-r_{\perp}]_{\theta_i=0} = \frac{n_t - n_i}{n_t + n_i}. \tag{4.47}$$

Thus, for example, at an air ($n_i = 1$) glass ($n_t = 1.5$) interface at nearly normal incidence, the reflection coefficients equal ±0.2.

When $n_t > n_i$ it follows from Snell's law that $\theta_i > \theta_t$, and $r_{\perp}$ is negative for all values of θ_i (Fig. 4.22). In contrast, $r_{\parallel}$ starts out positive at $\theta_i = 0$ and decreases gradually until it equals zero when $(\theta_i + \theta_t) = 90°$, since $\tan \pi/2$ is infinite. The particular value of the incident angle for which this occurs is denoted by θ_p and is referred to as the **polarization** angle (see Section 8.6.1). As θ_i increases beyond θ_p, $r_{\parallel}$ becomes progressively more negative, reaching −1.0 at 90°. If you place a single sheet of glass, a microscope slide, on this page and look straight down into it ($\theta_i = 0$), the region beneath the glass will seem decidedly grayer than the rest of the paper, because the slide will reflect at both its interfaces, and the light reaching and returning from the paper will be diminished appreciably. Now hold the slide near your eye and again view the page through it as you tilt it, increasing θ_i. The amount of light reflected will increase, and it will become more difficult to see the page through the glass. When $\theta_i \approx 90°$ the slide will look like a perfect mirror as the reflection coefficients (Fig. 4.22) go to −1.0. Even a rather poor surface, such as the cover of this book, will be mirrorlike at glancing incidence. Hold the book horizontally at the level of the middle of your eye and face a bright light; you will see the source reflected rather nicely in the cover. This suggests that even x-rays could be mirror-reflected at glancing incidence (p. 210), and modern x-ray telescopes are based on that very fact.

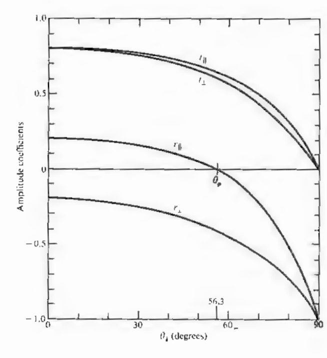


Figure 4.22 The amplitude coefficients of reflection and transmission as a function of incident angle. These correspond to external reflection $n_t > n_i$ at an air–glass interface ($n_{ti} = 1.5$).

At normal incidence Eqs. (4.35) and (4.41) lead rather straightforwardly to

$$[t_{\parallel}]_{\theta_i=0} = [t_{\perp}]_{\theta_i=0} = \frac{2n_i}{n_i + n_t}. \tag{4.48}$$

It will be shown in Problem 4.24 that the expression

$$t_{\perp} + (-r_{\perp}) = 1 \tag{4.49}$$

holds for all θ_i, whereas

$$t_{\parallel} + r_{\parallel} = 1 \qquad (4.50)$$

is true only at normal incidence.

The foregoing discussion, for the most part, was restricted to the case of **external reflection** (i.e., $n_t > n_i$). The opposite situation of **internal reflection**, in which the incident medium is the more dense ($n_i > n_t$), is of interest as well. In that instance $\theta_t > \theta_i$, and $r_\perp$, as described by Eq. (4.42), will always be positive. Figure 4.23 shows that $r_\perp$ increases from its initial value (4.47) at $\theta_i = 0$, reaching +1 at what is called the **critical angle**, θ_c. Specifically, θ_c is the special value of the incident angle for which $\theta_t = \pi/2$. Likewise, $r_\parallel$ starts off negatively (4.47) at $\theta_i = 0$ and thereafter increases, reaching +1 at $\theta_i = \theta_c$, as is evident from the Fresnel equation (4.40). Again, $r_\parallel$ passes througb zero at the *polarization angle* θ'_p. It is left for Problem 4.34 to show that the polarization angles θ'_p and θ_p for internal and external reflection at the interface between the same media are simply the complements of each other. We will return to internal reflection in Section 4.3.4, where it will be shown that $r_\perp$ and $r_\parallel$ are cnmplex quantities for $\theta_i > \theta_c$.

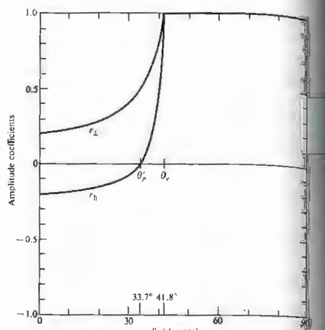


Figure 4.23 The amplitude coefficients of reflection as a function of incident angle. These correspond to internal reflection $n_t < n_i$ at an air-glass interface ($n_{ti} = 1/1.5$).

ii) Phase Shifts

It should be evident from Eq. (4.42) that $r_\perp$ is negative regardless of θ_i when $n_t > n_i$. Yet we saw earlier that had we chosen $[\mathbf{E}_r]_\perp$ in Fig. 4.20 to be in the opposite direction, the first Fresnel equation (4.42) would have changed signs, causing $r_\perp$ to become a positive quantity. Thus the sign of $r_\perp$ is associated with the relative directions of $[\mathbf{E}_{0i}]_\perp$ and $[\mathbf{E}_{0r}]_\perp$. Bear in mind that a reversal of $[\mathbf{E}_{0r}]_\perp$ is tantamount to introducing a phase shift, $\Delta\varphi_\perp$, of π radians into $[\mathbf{E}_r]_\perp$. Hence at the boundary $[\mathbf{E}_i]_\perp$ and $[\mathbf{E}_r]_\perp$ will be antiparallel and therefore π out of phase with each other, as indicated by the negative value of $r_\perp$. When we consider components normal to the plane of incidence, there is no confusion as to whether two fields are in phase or π radians out of phase: if parallel, they're in phase; if antiparallel, they're π out of phase. In summary, then, *the component of the electric field normal to the plane of incidence undergoes a phase shift of π radians upon reflection when the incident medium has a lower index than the transmitting medium.* Similarly, $t_\perp$ and $t_\parallel$ are always positive and $\Delta\varphi = 0$. *Furthermore, when $n_i > n_t$ no phase shift in the normal component results on reflection, that is, $\Delta\varphi_\perp = 0$ so long as $\theta_i < \theta_c$.*

Things are a bit less obvious when we deal with $[\mathbf{E}_i]_\parallel$, $[\mathbf{E}_r]_\parallel$, and $[\mathbf{E}_t]_\parallel$. It now becomes necessary to define more explicitly what is meant by *in phase*, since the field vectors are coplanar but generally not colinear. The field directions were chosen in Figs. 4.20 and 4.21 such that if you looked down any one of the propagation vectors toward the direction from which the light was coming, **E**, **B**, and **k** would appear to have the same relative orientation whether the ray was incident, reflected, or transmitted. We can use this as the required condition for two **E**-fields to be in phase. Equivalently, but more simply, *two fields in the incident plane are in phase if their y-components are parallel and are out of phase if the y-components are antiparallel.* Notice that when two **E**-fields are out of phase so too are their associated **B**-fields and vice versa. With this definition we need only look at the vectors normal to the plane of incidence, whether they be **E** or **B**, to determine the relative phase of the accompanying fields in the incident plane. Thus in Fig. 4.24(a) $\mathbf{E}_i$ and $\mathbf{E}_t$ are in phase, as are $\mathbf{B}_i$ and $\mathbf{B}_t$, whereas $\mathbf{E}_i$ and $\mathbf{E}_r$ are out of phase, along with $\mathbf{B}_i$ and $\mathbf{B}_r$. Similarly, in Fig. 4.24(b) $\mathbf{E}_i$, $\mathbf{E}_r$, and $\mathbf{E}_t$ are in phase, as are $\mathbf{B}_i$, $\mathbf{B}_r$, and $\mathbf{B}_t$.

Now, the amplitude reflection coefficient for the parallel component is given by

$$r_\parallel = \frac{n_t \cos\theta_i - n_i \cos\theta_t}{n_t \cos\theta_i + n_i \cos\theta_t},$$

which is positive ($\Delta\varphi_\parallel = 0$) as long as

$$n_t \cos\theta_i - n_i \cos\theta_t > 0,$$

that is, if

$$\sin\theta_i \cos\theta_i - \cos\theta_t \sin\theta_t > 0$$

or equivalently

$$\sin(\theta_i - \theta_t)\cos(\theta_i + \theta_t) > 0. \qquad (4.51)$$

This will be the case for $n_i < n_t$ if

$$(\theta_i + \theta_t) < \pi/2 \qquad (4.52)$$

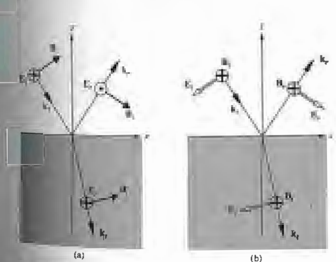


Figure 4.24 Field orientations and phase shifts.

and for $n_i > n_t$ when

$$(\theta_i + \theta_t) > \pi/2. \qquad (4.53)$$

Thus when $n_i < n_t$, $[\mathbf{E}_{0r}]_\parallel$ and $[\mathbf{E}_{0i}]_\parallel$ will be in phase ($\Delta\varphi_\parallel = 0$) until $\theta_i = \theta_p$ and out of phase by π radians thereafter. The transition is not actually discontinuous, since $[\mathbf{E}_{0r}]_\parallel$ goes to zero at θ_p. In contrast, for internal reflection $r_\parallel$ is negative until θ'_p, which means that $\Delta\varphi_\parallel = \pi$. From θ'_p to θ_c, $r_\parallel$ is positive and $\Delta\varphi_\parallel = 0$. Beyond θ_c, $r_\parallel$ becomes complex, and $\Delta\varphi_\parallel$ gradually increases to π at $\theta_i = 90°$.

Figure 4.25, which summarizes these conclusions, will be of continued use to us. The actual functional form of $\Delta\varphi_\parallel$ and $\Delta\varphi_\perp$ for internal reflection in the region where $\theta_i > \theta_c$ can be found in the literature,* but the curves depicted here will suffice for our purposes. Figure 4.25(e) is a plot of the relative phase shift between the parallel and perpendicular components, that is, $\Delta\varphi_\parallel - \Delta\varphi_\perp$. It is included here because it will be useful later on (e.g., when we consider polarization effects). Finally, many of the essential features of this discussion are illustrated in Figs. 4.26 and 4.27. The amplitudes of the reflected vectors are in accord with those of Figs. 4.22 and 4.23 (for an air–glass interface), and the phase shifts agree with those of Fig. 4.25.

Many of these conclusions can be verified with the simplest experimental equipment, namely, two linear polarizers, a piece of glass, and a small source, such as a flashlight or high-intensity lamp. By placing one polarizer in front of the source (at 45° to the plane of incidence), you can easily duplicate the conditions of Fig. 4.26. For example, when $\theta_i = \theta_p$ [Fig. 4.26(b)] no light will pass through the second polarizer if its transmission axis is parallel to the plane of incidence. In comparison, at near-glancing incidence the reflected beam will vanish when the axes of the two polarizers are almost normal to each other.

iii) Reflectance and Transmittance

Consider a circular beam of light incident on a surface, as shown in Fig. 4.28, such that there is an illuminated spot of area A. Recall that the power per unit area

* Born and Wolf, *Principles of Optics*, p. 49.

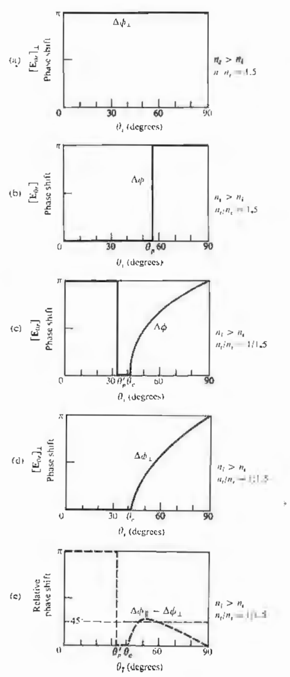


Figure 4.25 Phase shifts for the parallel and perpendicular components of the E-field corresponding to internal and external reflection.

crossing a surface in vacuum whose normal is parallel to **S**, the Poynting vector, is given by

$$\mathbf{S} = c^2\epsilon_0\mathbf{E} \times \mathbf{B}.$$

Furthermore, the radiant flux density (W/m²) or irradiance is

$$I = \langle S \rangle = \frac{c\epsilon_0}{2} E_0^2. \qquad (3.32)$$

This is the average energy per unit time crossing a unit area normal to **S** (in isotropic media **S** is parallel to **k**). In the case at hand (Fig. 4.28), let I_i, I_r, and I_t be the incident, reflected, and transmitted flux densities, respectively. The cross-sectional areas of the incident, reflected, and transmitted beams are, respectively, $A\cos\theta_i$, $A\cos\theta_r$, and $A\cos\theta_t$. Accordingly, the incident power is $I_iA\cos\theta_i$; this is the energy per unit time flowing in the incident beam and it's therefore the power arriving on the surface over A. Similarly, $I_rA\cos\theta_r$ is the power in the reflected beam, and $I_tA\cos\theta_t$ is the power being transmitted through A. We define the **reflectance** R to be the ratio of the reflected power (or flux) to the incident power:

$$R = \frac{I_r\cos\theta_r}{I_i\cos\theta_i} = \frac{I_r}{I_i}. \qquad (4.54)$$

In the same way, the **transmittance** T is defined as the ratio of the transmitted to the incident flux and is given by

$$T = \frac{I_t\cos\theta_t}{I_i\cos\theta_i}. \qquad (4.55)$$

The quotient I_r/I_i equals $(v_r\epsilon_rE_{0r}^2/2)/(v_i\epsilon_iE_{0i}^2/2)$, and since the incident and reflected waves are in the same medium, $v_r = v_i$, $\epsilon_r = \epsilon_i$, and

$$R = \left(\frac{E_{0r}}{E_{0i}}\right)^2 = r^2. \qquad (4.56)$$

In like fashion (assuming $\mu_i = \mu_t = \mu_0$),

$$T = \frac{n_t\cos\theta_t}{n_i\cos\theta_i}\left(\frac{E_{0t}}{E_{0i}}\right)^2 = \left(\frac{n_t\cos\theta_t}{n_i\cos\theta_i}\right)t^2, \qquad (4.57)$$

where use was made of the fact that $\mu_0\epsilon_t = 1/v_t^2$ and $\mu_0v_t\epsilon_t = n_t/c$. Notice that at normal incidence, which is a situation of great practical interest, $\theta_t = \theta_i = 0$, and

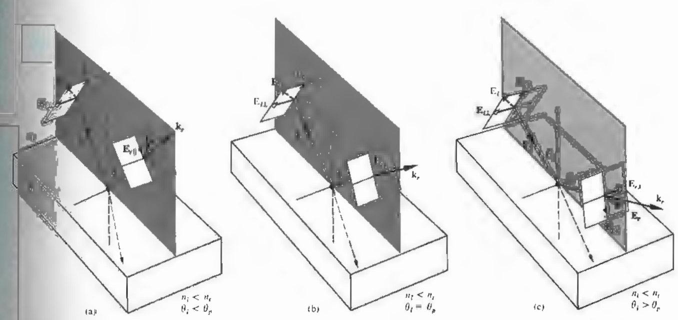


Figure 4.26 The reflected E-field at various angles concomitant with external reflection.

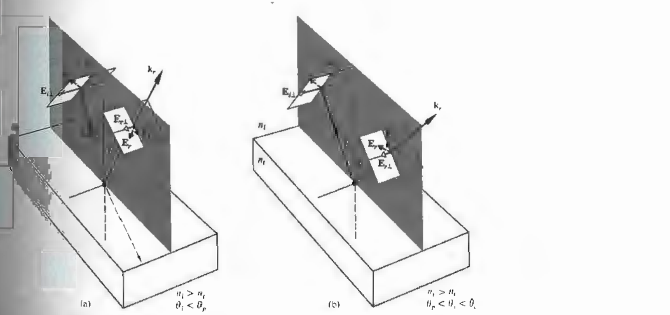


Figure 4.27 The reflected E-field at various angles concomitant with internal reflection.

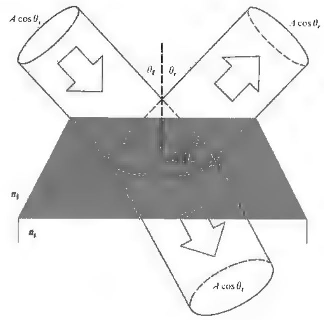


Figure 4.28 Reflection and transmission of an incident beam.

the transmittance [Eq. (4.55)], like the reflectance [Eq. (4.54)], is then simply the ratio of the appropriate irradiances. Since $R = r^2$, we need not worry about the sign of r in any particular formulation, and that makes reflectance a convenient notion. Observe that in Eq. (4.57) T is not simply equal to t^2, for two reasons. First, the ratio of the indices of refraction must be there, since the speeds at which energy is transported into and out of the interface are different, in other words, $I \propto v$, from Eq. (3.47). Second, the cross-sectional areas of the incident and reflected beams are different, and so the energy flow per unit area is affected accordingly, and that manifests itself in the presence of the ratio of the cosine terms.

Let's now write an expression representing the conservation of energy for the configuration depicted in Fig. 4.26. In other words, the total energy flowing into area A per unit time must equal the energy flowing outward from it per unit time:

$$I_i A \cos\theta_i = I_r A \cos\theta_r + I_t A \cos\theta_t. \tag{4.58}$$

When both sides are multiplied by c this expression becomes

$$n_i E_{0i}^2 \cos\theta_i = n_i E_{0r}^2 \cos\theta_i + n_t E_{0t}^2 \cos\theta_t$$

or

$$1 = \left(\frac{E_{0r}}{E_{0i}}\right)^2 + \left(\frac{n_t \cos\theta_t}{n_i \cos\theta_i}\right)\left(\frac{E_{0t}}{E_{0i}}\right)^2. \tag{4.59}$$

But this is simply

$$R + T = 1, \tag{4.60}$$

where there was no absorption. It is convenient to use the component forms, that is,

$$R_\perp = r_\perp^2 \tag{4.61}$$

$$R_\parallel = r_\parallel^2 \tag{4.62}$$

$$T_\perp = \left(\frac{n_t \cos\theta_t}{n_i \cos\theta_i}\right) t_\perp^2 \tag{4.63}$$

and

$$T_\parallel = \left(\frac{n_t \cos\theta_t}{n_i \cos\theta_i}\right) t_\parallel^2, \tag{4.64}$$

which are illustrated in Fig. 4.29. Furthermore, it can be shown (Problem 4.39) that

$$R_\parallel + T_\parallel = 1 \tag{4.65}$$

and

$$R_\perp + T_\perp = 1. \tag{4.66}$$

When $\theta_i = 0$ the incident plane becomes undefined and any distinction between the parallel and perpendicular components of R and T vanishes. In this case Eqs. (4.61) through (4.64), along with (4.47) and (4.48), lead to

$$R = R_\parallel = R_\perp = \left(\frac{n_t - n_i}{n_t + n_i}\right)^2 \tag{4.67}$$

and

$$T = T_\parallel = T_\perp = \frac{4 n_t n_i}{(n_t + n_i)^2}. \tag{4.68}$$

Thus 4% of the light incident normally on an air–glass interface will be reflected back, whether internally, $n_i > n_t$, or externally, $n_i < n_t$ (Problem 4.40). This will

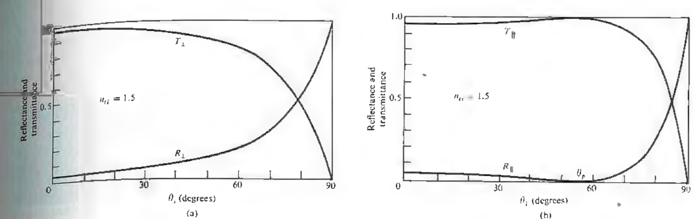


Figure 4.29 Reflectance and transmittance versus incident angle.

probably be of great concern to anyone who is working with a complicated lens system, which might have 10 or 20 such air–glass boundaries. Indeed, if you look perpendicularly into a stack of about 50 microscope slides (cover-glass slides are much thinner and easier to handle in large quantities), most of the light will be reflected. The stack will look very much like a mirror (Fig. 4.30). Figure 4.31 is a plot of the reflectance at a single interface, assuming normal incidence for various transmitting media in air. Figure 4.32 depicts the corresponding dependence of the transmittance at normal incidence on the number of interfaces and the index of the medium. Of course, this is why you can't see through a roll of "clear" smooth-surfaced plastic tape,

Figure 4.30 Near normal reflection off a stack of microscope slides. You can see the image of the camera that took the picture. (Photo by E.H.)

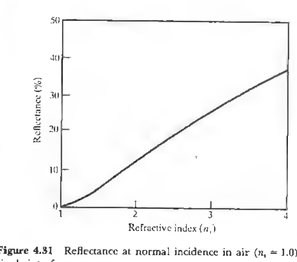


Figure 4.31 Reflectance at normal incidence in air ($n_i = 1.0$) at a single interface.

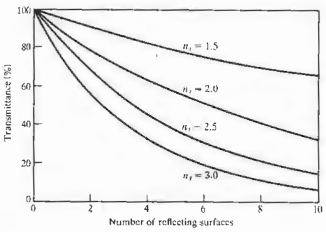


Figure 4.32 Transmittance through a number of surfaces in air ($n_i = 1.0$) at normal incidence.

and it's also why the many elements in a periscope must be coated with antireflection films (Section 9.9.2).

4.3.4 Total Internal Reflection

In the previous section it was evident that something rather interesting was happening in the case of **internal** reflection ($n_i > n_t$) when θ_i was equal to or greater than θ_c, the so-called **critical angle.** Let's now return to that situation for a somewhat closer look. Suppose that we have a source imbedded in an optically dense medium, and we allow θ_i to increase gradually, as indicated in Fig. 4.33. We know from the preceding section (Fig. 4.23) that $r_\parallel$ and $r_\perp$ increase with increasing θ_i, and therefore $t_\parallel$ and $t_\perp$ both decrease. Moreover $\theta_t > \theta_i$, since

$$\sin \theta_i = \frac{n_t}{n_i} \sin \theta_t$$

and $n_i > n_t$, in which case $n_{ti} < 1$. Thus as θ_i becomes larger, the transmitted ray gradually approaches tangency with the boundary, and as it does so more and more of the available energy appears in the reflected beam. Finally, when $\theta_t = 90°$, $\sin \theta_t = 1$ and

$$\sin \theta_c = n_{ti}. \tag{4.69}$$

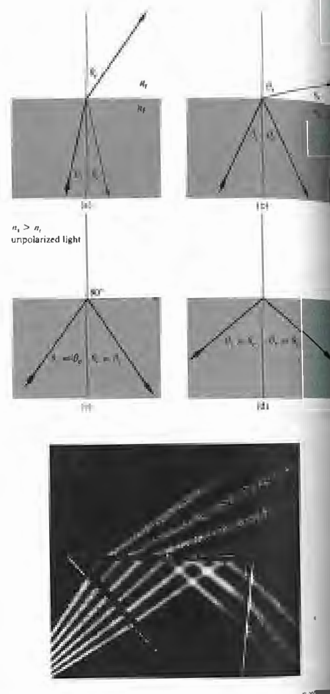


Figure 4.33 Internal reflection and the critical angle. (Photo courtesy of Educational Service, Inc.)

As noted earlier, *the critical angle is that special value of θ_i for which $\theta_t = 90°$*. For incident angles greater than or equal to θ_c, all the incoming energy is reflected back into the incident medium in the process known as **total internal reflection**. It should be stressed that the transition from the conditions depicted in Fig. 4.33(a) to those of 4.33(d) takes place without any discontinuities. That is, as θ_i becomes larger, the reflected beam grows stronger and stronger while the transmitted beam grows weaker and weaker, until the latter vanishes and the former carries all the energy at $\theta_r = \theta_c$. It's an easy matter to observe the diminution of the transmitted beam as θ_i is made larger. Just place a glass microscope slide on a printed page, this time blocking out any specularly reflected light. At $\theta_i \approx 0$, θ_t is roughly zero, and the page as seen through the glass is fairly bright and clear. But if you move your head, allowing θ_i (the angle at which you view the interface) to increase, the region of the printed page covered by the glass will appear darker and darker, indicating that T has indeed been markedly reduced.

The critical angle for our air–glass interface is roughly 42° (see Table 4.1). Consequently, a ray incident normally on the left face of either of the prisms in Fig. 4.34

Table 4.1 Critical angles.

n_{ti}	θ_c (degrees)	θ_c (radians)	n_{ti}	θ_c (degrees)	θ_c (radians)
1.30	50.2849	0.8776	1.50	41.8103	0.7297
1.31	49.7612	0.8685	1.51	41.4718	0.7238
1.32	49.2509	0.8596	1.52	41.1395	0.7180
1.33	48.7535	0.8509	1.53	40.8132	0.7123
1.34	48.2682	0.8424	1.54	40.4927	0.7067
1.35	47.7946	0.8342	1.55	40.1778	0.7012
1.36	47.3321	0.8261	1.56	39.8683	0.6958
1.37	46.8803	0.8182	1.57	39.5642	0.6905
1.38	46.4387	0.8105	1.58	39.2652	0.6853
1.39	46.0070	0.8030	1.59	38.9713	0.6802
1.40	45.5847	0.7956	1.60	38.6822	0.6751
1.41	45.1715	0.7884	1.61	38.3978	0.6702
1.42	44.7670	0.7813	1.62	38.1181	0.6653
1.43	44.3709	0.7744	1.63	37.8428	0.6605
1.44	43.9830	0.7676	1.64	37.5719	0.6558
1.45	43.6028	0.7610	1.65	37.3052	0.6511
1.46	43.2302	0.7545	1.66	37.0427	0.6465
1.47	42.8649	0.7481	1.67	36.7842	0.6420
1.48	42.5066	0.7419	1.68	36.5296	0.6376
1.49	42.1552	0.7357	1.69	36.2789	0.6332

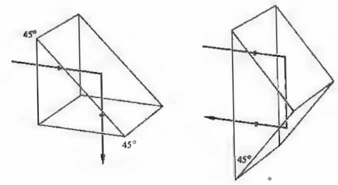


Figure 4.34 Total internal reflection.

will have a $\theta_i > 42°$ and therefore be internally reflected. This is a convenient way to reflect nearly 100% of the incident light without having to worry about the deterioration that can occur with metallic surfaces.

Another useful way to view the situation is shown in Fig. 4.35, which can be thought of as either a Huygens construction or a simplified representation of scattering off atomic oscillators. We know that the net effect of the presence of the homogeneous isotropic media is to alter the speed of the ligbt from c to v_i and v_t, respectively (p. 63). This is equivalent mathematically (via Huygens's principle) to saying that the resultant wave is the superposition of these wavelets propagating at the appropriate speeds. In Fig. 4.35(a) an incident wave results in the emission of wavelets successively from scattering centers A and B. These overlap to form the transmitted wave. The reflected wave, which comes back down into the incident medium as usual ($\theta_i = \theta_r$), is not shown. In a time t the incident front travels a distance $v_i t = \overline{CB}$, while the transmitted front moves a distance $v_t t = \overline{AD} > \overline{CB}$. Since one wave moves from A to E in the same time that the other moves from C to B, and since they have the same frequency and period, they must change phase by the same amount in the process. Thus the disturbance at point E must be in phase with that at point B; both of these points must be on the same transmitted wavefront.

It can be seen that the greater v_t is in comparison to v_i, the more tilted the transmitted front will be (i.e., the larger θ_t will be). That much is depicted in Fig. 4.35(b), where n_{ti} has been taken to be smaller by assuming n_t

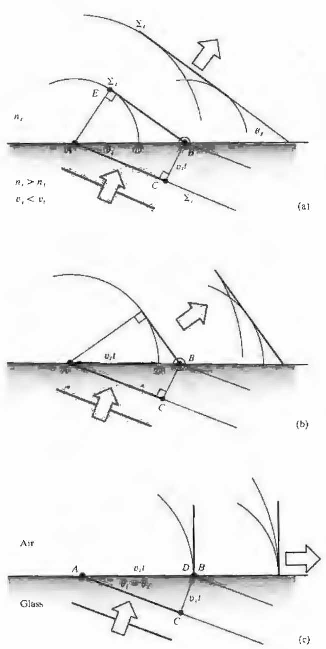


Figure 4.35 An examination of the transmitted wave in the process of total internal reflection from a scattering perspective. Here we keep θ_i and n_i constant and in successive parts of the diagram decrease n_t, thereby increasing v_t. The reflected wave ($\theta_r = \theta_i$) is not drawn.

to be smaller. The result is a higher speed v_t, increasing $\overline{AD}$ and causing a greater transmission angle. In Fig. 4.35(c) a special case is reached: $\overline{AD} = \overline{AB} = v_tt$, and the wavelets will overlap in phase *only along the line of the interface*, $\theta_t = 90°$. From triangle ABC, $\sin\theta_i = v_it/v_tt = n_t/n_i$, which is Eq. (4.69). For the two given media (i.e., for the particular value of n_{ti}), the direction in which the scattered wavelets will add constructively in the transmitting medium is along the interface. The resulting disturbance ($\theta_t = 90°$) is known as a *surface wave*.

If we assume that there is no transmitted wave, it becomes impossible to satisfy the boundary conditions using only the incident and reflected waves—things are not at all as simple as they might seem. Furthermore, we can reformulate Eqs. (4.34) and (4.40) (Problem 4.43) such that

$$r_\perp = \frac{\cos\theta_i - (n_{ti}^2 - \sin^2\theta_i)^{1/2}}{\cos\theta_i + (n_{ti}^2 - \sin^2\theta_i)^{1/2}} \qquad (4.70)$$

and

$$r_\parallel = \frac{n_{ti}^2\cos\theta_i - (n_{ti}^2 - \sin^2\theta_i)^{1/2}}{n_{ti}^2\cos\theta_i + (n_{ti}^2 - \sin^2\theta_i)^{1/2}}. \qquad (4.71)$$

Clearly then, since $\sin\theta_c = n_{ti}$ when $\theta_i > \theta_c$, $\sin\theta_i > n_{ti}$, and both $r_\perp$ and $r_\parallel$ become complex quantities. Despite this (Problem 4.44), $r_\perp r_\perp^* = r_\parallel r_\parallel^* = 1$ and $R = 1$, which means that $I_r = I_i$ and $I_t = 0$. Thus, although there must be a transmitted wave, it cannot, on the average, carry energy across the boundary. We shall not perform the complete and rather lengthy computation needed to derive expressions for all the reflected and transmitted fields, but we can get an appreciation of what's happening in the following way. The wave function for the transmitted electric field is

$$\mathbf{E}_t = \mathbf{E}_{0t}\exp i(\mathbf{k}_t\cdot\mathbf{r} - \omega t),$$

where

$$\mathbf{k}_t\cdot\mathbf{r} = k_{tx}x + k_{ty}y,$$

there being no z-component of $\mathbf{k}$. But

$$k_{tx} = k_t\sin\theta_t$$

and

$$k_{ty} = k_t\cos\theta_t,$$

as seen in Fig. 4.36. Once again using Snell's law, we find that

$$k_t\cos\theta_t = \pm k_t\left(1 - \frac{\sin^2\theta_i}{n_{ti}^2}\right)^{1/2} \qquad (4.72)$$

or, since we are concerned with the case where $\sin\theta_i > n_{ti}$,

$$k_{ty} = \pm ik_t\left(\frac{\sin^2\theta_i}{n_{ti}^2} - 1\right)^{1/2} \equiv \pm i\beta$$

and

$$k_{tx} = \frac{k_t}{n_{ti}}\sin\theta_i.$$

Hence

$$\mathbf{E}_t = \mathbf{E}_{0t}e^{\mp\beta y}e^{i(k_tx\sin\theta_i/n_{ti} - \omega t)}. \qquad (4.73)$$

Neglecting the positive exponential, which is physically untenable, we have a wave whose amplitude drops off exponentially as it penetrates the less dense medium. The disturbance advances in the x-direction as a surface or **evanescent wave.** Notice that the wavefronts or surfaces of constant phase (parallel to the yz-plane) are perpendicular to the surfaces of constant amplitude (parallel to the xz-plane), and as such the wave is *inhomogeneous* (see Section 2.5). Its amplitude decays rapidly in the y-direction, becoming negligible at a distance into the second medium of only a few wavelengths.

If you are still concerned about the conservation of energy, a more extensive treatment would have shown that energy actually circulates back and forth across the interface, resulting on the average in a zero net flow through the boundary into the second medium. Yet a puzzling point remains, inasmuch as there is still a bit of energy to be accounted for, namely, that associated with the evanescent wave that moves along the boundary in the plane of incidence. Since this energy could not have penetrated into the less dense medium under the present circumstances (so long as $\theta_i \geq \theta_c$), we must look elsewhere for its source. Under actual experimental conditions the incident beam would have a finite cross section and therefore would obviously differ from a true plane wave. This deviation gives rise (via diffraction) to a slight transmission of energy across the interface, which is manifested in the evanescent wave.

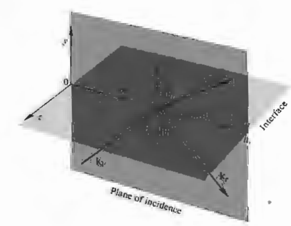


Figure 4.36 Propagation vectors for internal reflection.

Incidentally, it is clear from (c) and (d) in Fig. 4.25 that the incident and reflected waves (except at $\theta_i = 90°$) do not differ in phase by π and cannot therefore cancel each other. It follows from the continuity of the tangential component of **E** that there must be an oscillatory field in the less dense medium with a component parallel to the interface having a frequency ω (i.e., the evanescent wave).

The exponential decay of the surface wave, or *boundary wave*, as it is also sometimes called, has been confirmed experimentally at optical frequencies.*

Imagine that a beam of light traveling within a block of glass is internally reflected at a boundary. Presumably, if you pressed another piece of glass against the first, the air–glass interface could be made to vanish, and the beam would then propagate onward undisturbed. Furthermore, you might expect this transition from total to no reflection to occur gradually as the air film thinned out. In much the same way, if you hold a drinking glass or a prism, you can see the ridges of your fingerprints in a region that, because of total internal reflection, is otherwise mirrorlike. In more general terms, if the evanescent wave extends with appreciable amplitude across the rare medium into a nearby region occupied by a higher-index material, energy may flow through the gap in what is known as **frustrated total**

* Take a look at the fascinating article by K. H. Drexhage, "Monomolecular Layers and Light." *Sci. Am.* **222**, 108 (1970).

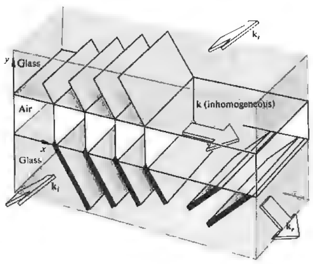


Figure 4.37 Frustrated total internal reflection.

internal reflection (FTIR). In other words, if the evanescent wave, having traversed the gap, is still strong enough to drive electrons in the "frustrating" medium, they in turn will generate a wave that significantly alters the field configuration, thereby permitting energy to flow. Figure 4.37 is a schematic representation of FTIR. The width of the lines depicting the wavefronts decreases across the gap as a reminder that the amplitude of the field behaves in the same way. The process as a whole is remarkably similar to the quantum-mechanical phenomenon of *barrier penetration* or *tunneling*, which has numerous applications in contemporary physics.

One can demonstrate FTIR with the prism arrangement of Fig. 4.38 in a manner that is fairly self-evident. Moreover, if the hypotenuse faces of both prisms are made planar and parallel, they can be positioned so as to transmit and reflect any desired fraction of the incident flux density. Devices that perform this function are known as *beam-splitters*. A *beam-splitter cube* can be made rather conveniently by using a thin, low-index transparent film as a precision spacer. Low-loss reflectors whose transmittance can be controlled by frustrating internal reflection are of considerable practical interest. FTIR can also be observed in other regions of the electromagnetic spectrum. Three-centimeter microwaves are particularly easy to work with, inasmuch as the evanescent wave will extend roughly 10^5 times farther than it would at optical frequencies. One can duplicate the above optical experiments with solid prisms made of paraffin or hollow ones of acrylic plastic filled with kerosene or motor oil. Any one of these would have an index of about 1.5 for 3-cm waves. It then becomes an easy matter to measure the dependence of the field amplitude on y.

4.3.5 Optical Properties of Metals

The characteristic feature of conducting media is the presence of a number of free electric charges (free in the sense of being unbound, i.e., able to circulate within the material). For metals these charges are of course electrons, and their motion constitutes a current. The current per unit area resulting from the application of a field $\mathbf{E}$ is related by means of Eq. (A1.15) to the conductivity of the medium σ. For a dielectric there are no free or conduction electrons and $\sigma = 0$, whereas for actual metals σ is nonzero and finite. In contrast, an idealized "perfect" conductor would have an infinite conductivity. This is equivalent to saying that the electrons, driven into oscillation by a harmonic wave, would simply follow the field's alternations. There would be no restoring force, no natural frequencies, and no absorption, only reemission. In real metals the conduction electrons undergo collisions with the thermally agitated lattice or with imperfections and in so doing irreversibly convert electromagnetic energy into joule heat. Evidently the absorption of radiant energy by a material is a function of its conductivity.

i) Waves in a Metal

If we visualize the medium as continuous, Maxwell's equations lead to

$$\frac{\partial^2 \mathbf{E}}{\partial x^2}+\frac{\partial^2 \mathbf{E}}{\partial y^2}+\frac{\partial^2 \mathbf{E}}{\partial z^2}=\mu\epsilon\frac{\partial^2 \mathbf{E}}{\partial t^2}+\mu\sigma\frac{\partial \mathbf{E}}{\partial t}, \qquad (4.7?)$$

which is Eq. (A1.21) in Cartesian coordinates. The last term, $\mu\sigma\, \partial\mathbf{E}/\partial t$, is a first-order time derivative, like the damping force in the oscillator model discussed in Sec-

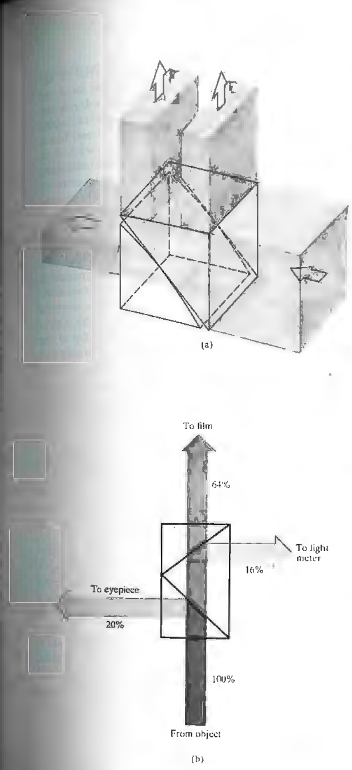


Figure 4.38 (a) A beam-splitter utilizing FTIR. (b) A typical modern application of FTIR: a conventional beam-splitter arrangement used to take photographs through a microscope. (c) Beam-splitter cubes. (Photo courtesy Melles Griot.)

tion 3.5.1. The time rate of change of **E** generates a voltage, currents circulate, and since the material is resistive, light is converted to heat—ergo absorption. This expression can be reduced to the unattenuated wave equation, if the permittivity is reformulated as a complex quantity. This in turn leads to a complex index of refraction, which, as we saw earlier (Section 3.5.1), is tantamount to absorption. We then need only substitute the complex index

$$n_c = n_R - in_I \tag{4.75}$$

(where the real and imaginary indices n_R and n_I are both real numbers) into the corresponding solution for a nonconducting medium. Alternatively, we can utilize the wave equation and appropriate boundary conditions to yield a specific solution. In either event, we can find a simple sinusoidal plane-wave solution applicable within the conductor. Such a wave propagating in the y-direction is ordinarily written as

$$\mathbf{E} = \mathbf{E}_0 \cos(\omega t - ky)$$

or as a function of n,

$$\mathbf{E} = \mathbf{E}_0 \cos \omega(t - ny/c),$$

but here the refractive index must be taken as complex. Accordingly, writing the wave as an exponential and using Eq. (4.75), we obtain

$$\mathbf{E} = \mathbf{E}_0 e^{(-\omega n_I y/c)} e^{i\omega(t - n_R y/c)} \tag{4.76}$$

or

$$\mathbf{E} = \mathbf{E}_0 e^{-\omega n_I y/c} \cos \omega(t - n_R y/c). \tag{4.77}$$

The disturbance advances in the y-direction with a speed c/n_R, precisely as if n_R were the more usual index of refraction. As the wave progresses into the conductor, its amplitude, $\mathbf{E}_0 \exp(-\omega n_I y/c)$, is exponentially attenuated. Inasmuch as irradiance is proportional to the square of the amplitude, we have

$$I(y) = I_0 e^{-\alpha y}, \tag{4.78}$$

where $I_0 = I(0)$, that is, I_0 is the irradiance at $y = 0$ (the interface), and $\alpha = 2\omega n_I/c$ is called the *absorption coefficient* or (even better) the **attenuation coefficient**. The flux density will drop by a factor of $e^{-1} = 1/2.7 \approx \frac{1}{3}$ after the wave has propagated a distance $y = 1/\alpha$, known as the *skin* or *penetration depth*. For a material to [illegible] transparent the penetration depth must be large [illegible] comparison to its thickness. The penetration depth [illegible] metals, however, is exceedingly small. For exampl[illegible] copper at ultraviolet wavelengths ($\lambda_0 \approx 100$ nm) has [illegible] miniscule penetration depth, about 0.6 nm, while it [illegible] still only about 6 nm in the infrared ($\lambda_0 \approx 10{,}000$ n[illegible]). This accounts for the generally observed opacity [illegible] metals, which nonetheless can become partly tra[illegible] parent when formed into extremely thin films (e.g. [illegible] the case of partially silvered two-way mirrors). [illegible] familiar metallic sheen of conductors corresponds [illegible] high reflectance, which arises from the fact that th[illegible] incident wave cannot effectively penetrate the mate[illegible] Relatively few electrons in the metal "see" the transm[illegible] ted wave, and therefore, although each absor[illegible] strongly, little total energy is dissipated by th[illegible] Instead, most of the incoming energy reappears as [illegible] reflected wave. The majority of metals, including [illegible] less common ones (e.g., sodium, potassium, ces[illegible] vanadium, niobium, gadolinium, holmium, yttri[illegible] scandium, and osmium) have a silvery gray appear[illegible] like that of aluminum, tin, or steel. They reflect al[illegible] all the incident light regardless of wavelengths and [illegible] therefore essentially colorless.

Equation (4.77) is certainly reminiscent of Eq. (4[illegible] and FTIR. In both cases there is an exponential d[illegible] of the amplitude. Moreover, a complete analysis wo[illegible] show that the transmitted waves are not strictly tra[illegible] verse, there being a component of the field in [illegible] direction of propagation in both instances.

The representation of metal as a continuous med[illegible] works fairly well in the low-frequency, long-wavelen[illegible] domain of the infrared. Yet we certainly might exp[illegible] that as the wavelength of the incident beam decrea[illegible] the actual granular nature of matter would have to be reckoned with. Indeed, the continuum model show[illegible] large discrepancies from experimental results at opt[illegible] frequencies. And so we again turn to the clas[illegible] atomistic picture initially formulated by Hen[illegible] Lorentz, Paul Karl Ludwig Drude (1863–1906), [illegible] others. This simple approach will provide qualita[illegible] agreement with the experimental data, but the ulti[illegible] treatment nonetheless requires quantum theory.

[illegible] Dispersion Equation

Envision the conductor as an assemblage of driven, damped oscillators. Some correspond to free electrons and will therefore have zero restoring force, whereas others are bound to the atom, much like those in the dielectric media of Section 3.5.1. The conduction electrons are, however, the predominant contributors to the optical properties of metals. Recall that the displacement of a vibrating electron was given by

$$x(t) = \frac{q_e/m_e}{(\omega_0^2 - \omega^2)} E(t). \tag{3.65}$$

[illegible] no restoring force, $\omega_0 = 0$, the displacement is [illegible] in sign to the driving force $q_e E(t)$ and therefore [illegible] of phase with it. This is unlike the situation [illegible] transparent dielectrics, where the resonance [illegible]ncies are above the visible and the electrons oscil[illegible] in phase with the driving force (Fig. 4.39). Free [illegible]ons oscillating out of phase with the incident light [illegible] radiate wavelets that tend to cancel the incoming disturbance. The effect, as we have already seen, is a rapidly decaying refracted wave.

Assuming that the average field experienced by an electron moving about within a conductor is just the applied field $\mathbf{E}(t)$, we can extend the dispersion equation of a [illegible] medium (3.71) to read

$$n^2(\omega) = 1 + \frac{Nq_e^2}{\epsilon_0 m_e}\left[\frac{f_e}{-\omega^2 + i\gamma_e\omega} + \sum_j \frac{f_j}{\omega_{0j}^2 - \omega^2 + i\gamma_j\omega}\right]. \tag{4.79}$$

The first bracketed term is the contribution from the [illegible]ectrons, wherein N is the number of atoms per unit volume. Each of these has f_e conduction electrons, which have no natural frequencies. The second term [illegible] from the bound electrons and is identical to Eq. [illegible]. It should be noted that if a metal has a particular color, it indicates that the atoms are partaking of selective absorption by way of the bound electrons, in addition to the general absorption characteristic of the free electrons. Recall that a medium that is very strongly absorbing at a given fequency doesn't actually absorb [illegible] of the incident light at that frequency but rather [illegible] *reflects* it. Gold and copper are reddish yellow

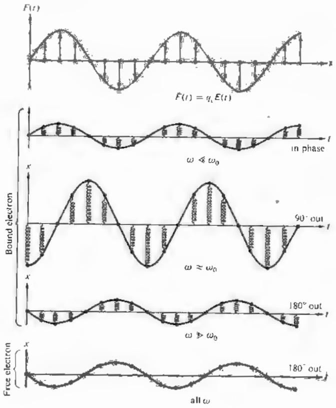


Figure 4.39 Oscillations of bound and free electrons.

because n_I increases with wavelength, and the larger values of λ are reflected more strongly. Thus, for example, gold should be fairly opaque to the longer visible wavelengths. Consequently, under white light, a gold foil less than roughly 10^{-6} m thick will indeed transmit predominantly greenish blue light.

We can get a rough idea of the response of metals to light by making a few simplifying assumptions. Accordingly, we neglect the bound electron contribution and assume that γ_e is also negligible for very large ω, whereupon

$$n^2(\omega) = 1 - \frac{Nq_e^2}{\epsilon_0 m_e \omega^2}. \tag{4.80}$$

The latter assumption is based on the fact that at high frequencies the electrons will undergo a great many oscillations between each collision. Free electrons and positive ions within a metal may be thought of as a plasma whose density oscillates at a natural frequency ω_p, the *plasma frequency*. This in turn can be shown to equal $(Nq_e^2/\epsilon_0 m_e)^{1/2}$, and so

$$n^2(\omega) = 1 - (\omega_p/\omega)^2. \quad (4.81)$$

The plasma frequency serves as a critical value below which the index is complex and the penetrating wave drops off exponentially (4.77) from the boundary; at frequencies above ω_p, n is real, absorption is small, and the conductor is transparent. In the latter circumstance n is less than 1, as it was for dielectrics at very high frequencies. Hence we can expect metals in general to be fairly transparent to x-rays. Table 4.2 lists the plasma frequencies for some of the alkali metals that are transparent even to ultraviolet.

The index of refraction for a metal will usually be complex, and the impinging wave will suffer absorption in an amount that is frequency dependent. For example, the outer visors on the Apollo space suits were overlaid with a very thin film of gold (Fig. 4.40). The coating reflected about 70% of the incident light and was used under bright conditions, such as low and forward sun angles. It was designed to decrease the thermal load on the cooling system by strongly reflecting radiant energy in the infrared while still transmitting adequately in the visible. Inexpensive metal-coated sunglasses which are quite similar in principle are also available commercially and they're well worth having just to experiment with.

The ionized upper atmosphere of the Earth contains a distribution of free electrons that behave very much like those confined within a metal. The index of refraction of such a medium will be real and less than 1 for frequencies above ω_p. In July of 1965 the *Mariner IV* spacecraft made use of this effect to examine the ionosphere of the planet Mars, 216 million kilometers from Earth.*

If we wish to communicate between two distant terrestrial points, we might bounce low-frequency waves off the Earth's ionosphere. To speak to someone on the Moon, however, we should use high-frequency sig[illegible] to which the ionosphere would be transparent.

* R. Von Eshelman, *Sci. Am.* 220, 78 (1969).

Table 4.2 Critical wavelengths and frequencies for some [illegible] metals.

Metal	λ_p (observed) nm	λ_p (calculated) nm	$\nu_p = c/$[illegible] (observed) Hz
Lithium (Li)	155	155	1.94×10[illegible]
Sodium (Na)	210	209	1.43×10[illegible]
Potassium (K)	315	287	0.95×10[illegible]
Rubidium (Rb)	340	322	0.88×10[illegible]

iii) Reflection From a Metal

Imagine that a plane wave initially in air impinge[illegible] a conducting surface. The transmitted wave advan[illegible] at some angle to the normal will be inhomogene[illegible] But if the conductivity of the medium is increased[illegible]

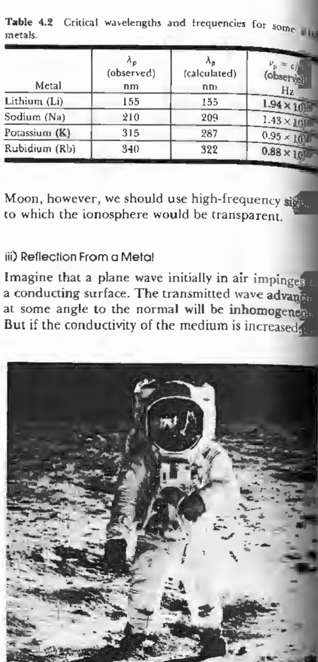


Figure 4.40 Edwin Aldrin Jr. at Tranquility Base on the M[illegible] photographer, Neil Armstrong, is reflected in the gold-coat[illegible] (Photo courtesy NASA.)

wavefr[illegible] will become aligned with the surfaces of constant amplitude, whereupon $\mathbf{k}_t$ and $\hat{\mathbf{u}}_n$ will approach parallelism. In other words, in a good conductor the transmitted wave propagates in a direction normal to the interface regardless of θ_i.

Let's now compute the reflectance, $R = I_r/I_i$, for the simplest case of normal incidence on a metal. Taking $n_i = 1$ and $n_t = n_c$ (i.e., the complex index), we have from Eq. (4.47) that

$$R = \left(\frac{n_c - 1}{n_c + 1}\right)\left(\frac{n_c - 1}{n_c + 1}\right)^*, \quad (4.82)$$

and therefore, since $n_c = n_R - in_I$,

$$R = \frac{(n_R - 1)^2 + n_I^2}{(n_R + 1)^2 + n_I^2}. \quad (4.83)$$

If the conductivity of the material goes to zero, we have the case of a dielectric, whereupon in principle [illegible]index is real ($n_I = 0$), and the attenuation coefficient, [illegible] Under those circumstances, the index of the [illegible]itting medium n_t is n_R, and the reflectance (4.83) [illegible]es identical with that of Eq. (4.67). If instead n_I is large while n_R is comparatively small, R in turn [illegible]omes large (Problem 4.49). In the unattainable limit [illegible] n_c is purely imaginary, 100% of the incident flux [illegible] would be reflected ($R = 1$). Notice that it is [illegible]sible for the reflectance of one metal to be greater [illegible] that of another even though its n_I is smaller. For exa[illegible] at $\lambda_0 = 589.3$ nm the parameters associated with solid sodium are roughly $n_R = 0.04$, $n_I = 2.4$, and $R = 0.9$; and those for bulk tin are $n_R = 1.5$, $n_I = 5.3$, and $R = 0.8$; whereas for a gallium single crystal $n_R = n_I = 5.4$, and $R = 0.7$.

[illegible] curves of $R_\parallel$ and $R_\perp$ for oblique incidence shown in Fig. 4.41 are somewhat typical of absorbing media. Thus, although R at $\theta_i = 0$ is about 0.5 for gold, as opposed to nearly 0.9 for silver in white light, the two metals have reflectances that are quite similar in shape, [illegible]ching 1.0 at $\theta_i = 90°$. Just as with dielectrics (Fig. [illegible] drops to a minimum at what is now called the *princi[illegible] angle of incidence*, but here that minimum is nonze[illegible] Figure 4.42 illustrates the spectral reflectance [illegible]al incidence for a number of evaporated metal [illegible] ideal conditions. Observe that although gold [illegible] fairly well in and below the green region of

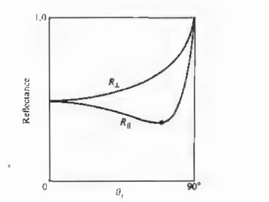


Figure 4.41 Typical reflectance for a linearly polarized beam of white light incident on an absorbing medium.

the spectrum, silver, which is highly reflective across the visible, becomes transparent in the ultraviolet at about 316 nm.

Phase shifts arising from reflection off a metal occur in both components of the field (i.e., parallel and perpendicular to the plane of incidence). These are generally neither 0 nor π, with a notable exception at $\theta_i = 90°$, where, just as with a dielectric, both components shift phase by 180° on reflection.

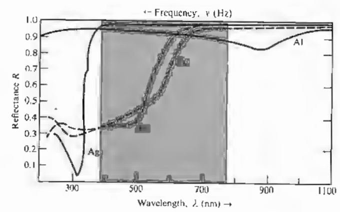


Figure 4.42 Reflectance versus wavelength for silver, gold, copper, and aluminum.

4.4 FAMILIAR ASPECTS OF THE INTERACTION OF LIGHT AND MATTER

Let's now examine some of the phenomena that paint the everyday world in a marvel of myriad colors.

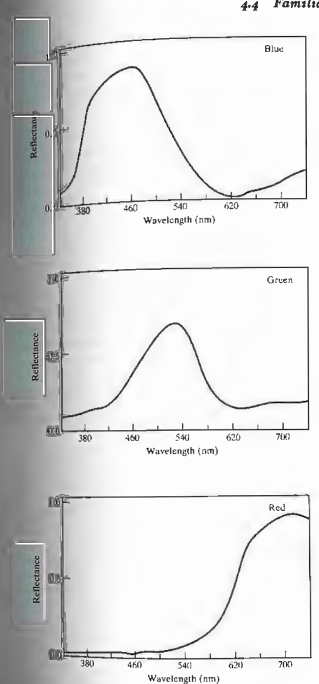
As we saw earlier (p. 72), light that contains a roughly equal amount of every frequency in the visible region of the spectrum is perceived as white. Thus a broad source of white light (whether natural or artificial) is one for which every point on its surface can be imagined as sending out, more or less in all directions, a stream of light of every visible frequency. Similarly, a reflecting surface that accomplishes essentially the same thing will also appear white: a highly reflecting, frequency-independent, *diffusely* scattering object will be perceived as white under white light.

Although water is essentially transparent, water vapor appears white, as does ground glass. The reason is simple enough—if the grain size is small but much larger than the wavelengths involved, light will enter each transparent particle, be reflected and refracted several times, and emerge. There will be no distinction among any of the frequency components, so the reflected light reaching the observer will be white. This is the mechanism accountable for the whiteness of things like sugar, salt, paper, clouds, talcum powder, snow, and paint, each grain of which is actually transparent. Similarly, a wadded-up piece of crumpled clear plastic wrap will appear whitish, as will an ordinarily transparent material filled with small air bubbles (e.g., beaten egg white). Even though we usually think of paper, talcum powder, and sugar as each consisting of some sort of opaque white substance, it's an easy matter to dispel that misconception. Cover a printed page with a few of these materials (a sheet of white paper, some grains of sugar, or talcum) and illuminate it from behind. You'll have little difficulty in seeing through them. In the case of white paint, one simply suspends colorless transparent particles, such as the oxides of zinc, titanium, or lead, in an equally transparent vehicle, for example, linseed oil or the newer acrylics. Obviously, if the particles and vehicle have the same index of refraction, there will not be any reflections at the grain boundaries. The particles will simply disappear into the conglomeration, which itself remains clear. In contrast, if the indices are markedly different, there will be a good deal of ... tion at all wavelengths (Problem 4.42), and the ... will appear white and opaque [take another look at (4.67)]. To color paint one need only dye the partic... so that they absorb all frequencies except the desi... range.

Carrying the logic in the reverse direction, if ... reduce the relative index, n_{ti}, at the grain or fibe... boundaries, the particles of material will reflect ... thereby decreasing the overall whiteness of the obj... Consequently, a wet white tissue will have a grayi... more transparent look. Wet talcum powder loses ... sparkling whiteness, becoming a dull gray, as does ... white cloth. In the same way, a piece of dyed fab... soaked in a clear liquid (e.g., water, gin, or benzen... will lose its whitish haze and become much darker, ... colors then being deep and rich like those of a still ... water-color painting.

A diffusely reflecting surface that absorbs somewh... uniformly right across the spectrum—will reflect ... less than a white surface and so appear mat gray. ... less it reflects, the darker the gray, until it absorbs al... all the light and appears black. A surface that re... perhaps 70% or 80% or more, but does so specu... will appear the familiar shiny gray of a typical m... Metals possess tremendous numbers of free elec... (p. 111) that scatter light very effectively, independ... of frequency: they are not bound to the atoms and h... no associated resonances. Moreover, the amplitu... the vibrations are an order of magnitude larger ... they were for the bound electrons. The incident ... cannot penetrate into the metal any more than a fra... of a wavelength or so before it's canceled complete... There is little or no refracted light; most of the ene... is reflected out, and only the small remainder is ... sorbed. Note that the primary difference between a ... surface and a mirrored surface is one of diffuse ... specular reflection. An artist paints a picture of a p... ished "white" metal, such as silver or aluminum, ... "reflecting" images of things in the room on top o... gray surface.

When the distribution of energy in a beam of lig... is not effectively uniform across the spectrum, the li... appears colored. Figure 4.43 depicts typical frequ...



... Reflection curves for blue, green, and red pigments. ...ical, but there is a great deal of possible variation among

distributions for what would be perceived as red, green, and blue light. These curves show the predominant frequency regions, but there can be a great deal of variation in the distributions, and they will still provoke the responses of red, green, and blue. In the early 1800s Thomas Young showed that a broad range of colors could be generated by mixing three beams of light, provided their frequencies were widely separated. When three such beams combine to produce white light they are called **primary colors.** There is no single unique set of these primaries, nor do they have to be quasimonochromatic. Since a wide range of colors can be created by mixing red (R), green (G), and blue (B), these tend to be used most frequently. They are the three components (emitted by three phosphors) that generate the whole gamut of hues seen on a color television set.

Figure 4.44 summarizes the results when beams of these three primaries are overlapped in a number of different combinations: Red plus blue is seen as *magenta* (M), a reddish purple; blue plus green is seen as *cyan* (C), a bluish green or turquoise; and perhaps most surprising, red plus green is seen as *yellow* (Y). The sum of all three primaries is white:

$$R = B + G = W,$$

$$M + G = W, \text{ since } R + B = M,$$

$$C + R = W, \text{ since } B + G = C,$$

$$Y + B = W, \text{ since } R + G = Y.$$

Any two colors that together produce white are said to be **complementary**, and the last three symbolic state-

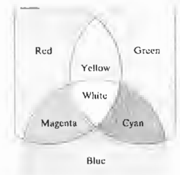


Figure 4.44 Three overlapping beams of colored light. A color television set uses these same three primary light sources—red, green, and blue.

ments exemplify that situation. Now suppose we overlap a beam of magenta and a beam of yellow:

$$M + Y = (R + B) + (R + G) = W + R;$$

the result is a combination of red and white, or pink. That raises another point: we say a color is **saturated**, that it is deep and intense, when it does not contain any white light. As Fig. 4.45 shows, pink is unsaturated red—red superimposed on a background of white.

The mechanism responsible for the yellowish red hue of gold and copper is, in some respects, similar to the process that causes the sky to appear blue. Putting it rather succinctly (see Section 8.5 for a further discussion of scattering in the atmosphere), the molecules of air have resonances in the ultraviolet and will therefore be driven into larger-amplitude oscillations as the frequency of the incident light increases toward the ultraviolet. Consequently, they will effectively take energy from and reemit (i.e., scatter) the blue component of sunlight in all directions, transmitting the complementary red end of the spectrum with little alteration. This is analogous to the selective reflection or scattering of yellow-red light that takes place at the surface of a gold film and the concomitant transmission of blue-green light. In contradistinction, the characteristic colors of most substances have their origin in the phenomenon of *selective* or *preferential absorption*. For example, water has a very light green-blue tint because of its absorption of red light. That is, the H_2O molecules have a broad resonance in the infrared, which extends somewhat into the visible. The absorption isn't very strong, so there is no accentuated reflection of red light at the surface. Instead it is transmitted and gradually absorbed out until at a depth of about 30 m of sea water, red is almost completely removed from sunlight. This same process of selective absorption is responsible for the colors of brown eyes and butterflies, of birds and bees and cabbages and kings. Indeed the great majority of objects in nature appear to have characteristic colors as the result of preferential absorption by pigment molecules. In contrast with most atoms and molecules, which have resonances in the ultraviolet and infrared, the pigment molecules must obviously have resonances in the visible. Yet visible photons have energies of roughly 1.6 eV to 3.2 eV, which, as you

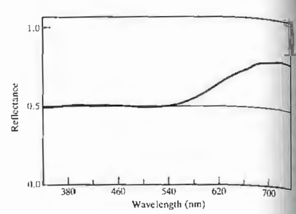


Figure 4.45 Spectral reflection of a pink pigment.

might expect, are on the low side for ordinary electron excitation and on the high side for excitation of molecular vibration. Despite this, there are atoms in which the bound electrons form incomplete shells (gold, for example) and variations in the configuration of these shells provide a mode for low-energy excitation. In addition, there is the large group of organic dye molecules, which evidently also have resonances in the visible. All such substances, whether natural or synthetic, consist of long-chain molecules made up of regularly alternating single and double bonds in what is called a conjugated system. This structure is typified by the carotene molecule $C_{40}H_{56}$ (Fig. 4.46). The carotenoids range in color from yellow to red and are found in carrots, tomatoes, daffodils, dandelions, autumn leaves, and people. The chlorophylls are another group of familiar natural pigments, but here a portion of the long chain is turned around on itself to form a ring. In any event, conjugated systems of this sort contain a number of particularly mobile electrons known as *pi electrons*. They are not bound to specific atomic sites but instead can range over the relatively large dimensions of the molecular chain or ring. In the phraseology of quantum mechanics, we would say that these are long-wavelength, low-frequency, and therefore low-energy, electron states. The energy required to raise a pi electron to an excited state is accordingly comparatively low, corresponding to that of visible photons. In effect, we can imagine the molecule as an

oscillator having a resonance frequency in the visible.

The energy levels of an individual atom are precisely defined, that is, the resonances are very sharp. With solids and liquids, however, the proximity of the atoms results in a broadening of the energy levels into wide bands. In other words, the resonances spread over a broad range of frequencies. Consequently, we can expect that a dye will not absorb just a narrow portion of the spectrum; indeed if it did, it would reflect most frequencies and appear nearly white.

Imagine a piece of stained glass with a resonance in the blue where it strongly absorbs. If you look through it at a white-light source composed of red, green, and blue, the glass will absorb blue, passing red and green, which is yellow (Fig. 4.47). The glass looks yellow: yellow cloth, paper, dye, paint, and ink all selectively absorb blue. If you peer at something that is a pure blue through a yellow filter, one that passes yellow and absorbs blue, the object will appear black. Here the filter colors the light yellow by removing blue, and we speak

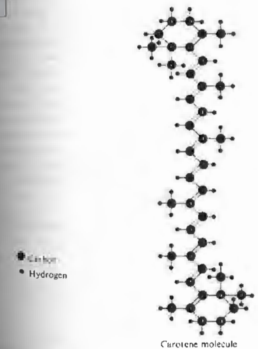


Figure 4.46 The carotene molecule.

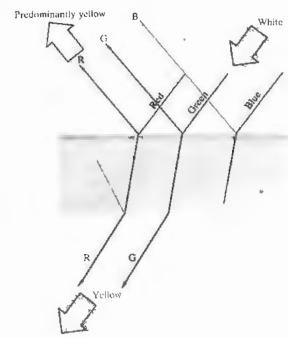


Figure 4.47 Yellow stained glass.

of the process as *subtractive* coloration, as opposed to *additive* coloration, which results from overlapping beams of light.

In the same way, fibers of a sample of white cloth or paper are essentially transparent, but when dyed each fiber behaves as if it were a chip of colored glass. The incident light penetrates the paper, emerging for the most part as a reflected beam only after undergoing numerous reflections and refractions within the dyed fibers. The exiting light will be colored to the extent that it lacks the frequency component absorbed by the dye. This is precisely why a leaf appears green, or a banana yellow.

A bottle of ordinary blue ink looks blue in either reflected or transmitted light. But if the ink is painted on a glass slide and the solvent evaporates, something rather interesting happens. The concentrated pigment absorbs so effectively that it preferentially reflects at the resonant frequency, and we are back to the idea that a strong absorber (large n_I) is a strong reflector. Thus,

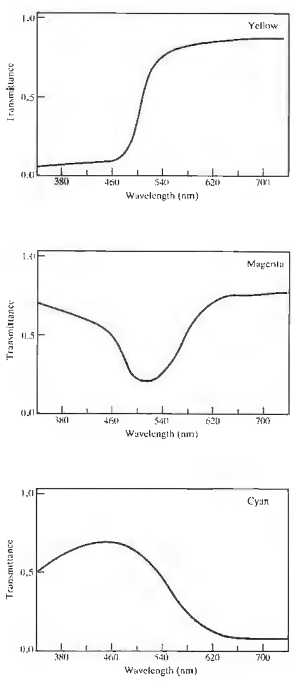


Figure 4.48 Transmission curves for colored filters.

concentrated blue-green ink reflects red, whereas red-blue ink reflects green. Try it with a felt marking pen, but you must use reflected light, being careful not to inundate the sample with unwanted light from below. (Wipe the ink to obtain a thin layer and then place the slide on a piece of black paper.)

The whole range of colors (including red, green, and blue) can be produced by passing light through various combinations of magenta, cyan, and yellow filters (Fig. 4.48). These are the primary colors of subtractive mixing, the primaries of the paint box, although they are often mistakenly spoken of as red, blue, and yellow. They are the basic colors of the dyes used to make photographs and the inks used to print them. Ideally, if you mix all the subtractive primaries together (either by combining paints or by stacking filters), you get no color, no light—black. Each removes a region of the spectrum, and together they absorb it all.

If the range of frequencies being absorbed spreads across the visible, the object will appear black. That's not to say that there is no reflection at all—you obviously can see a reflected image in a piece of black patent leather, and a rough black surface reflects also, only diffusely. If you still have those red and blue inks, mix them, add some green, and you'll get black.

In addition to the above processes specifically related to reflection, refraction, and absorption, there are many other color-generating mechanisms, which we will explore later on. For example, the scarabaeid beetles mantle themselves in the brilliant colors produced by diffraction gratings on their wing cases, and wavelength-dependent interference effects contribute to the color patterns seen on oil slicks, mother-of-pearl, soap bubbles, peacocks, and hummingbirds.

4.5 THE STOKES TREATMENT OF REFLECTION AND REFRACTION

A rather elegant and novel way of looking at reflection and transmission at a boundary was developed by the British physicist Sir George Gabriel Stokes (1819–1903). Since we will often make use of his results in future chapters, let's now examine that derivation. Suppose that we have an incident wave of amplitude E_{0i} impinging on the planar interface separating two dielectric media, as in Fig. 4.49(a). As we saw earlier in this chapter, since r and t are the fractional amplitudes reflected and transmitted, respectively (where $n_i = n_1$ and $n_t = n_2$), then $E_{0r} = rE_{0i}$ and $E_{0t} = tE_{0i}$. Again we are reminded of the fact that Fermat's principle led to the principle of reversibility, which implies that the situation depicted in Fig. 4.49(b), where all the ray directions are reversed, must also be physically possible. With the one proviso that there be no energy dissipation (no absorption), a wave's meanderings must be reversible. Equivalently, in the idiom of modern physics one speaks of *time-reversal invariance*, that is, if a process occurs, the reverse process can also occur. Thus if we film a hypothetical motion picture of the wave incident on, reflecting from, and transmitting through the interface, the behavior depicted when the film is run backward must also be physically realizable. Accordingly, examine Fig. 4.49(c), where there are now two incident waves of amplitudes $E_{0i}r$ and $E_{0i}t$. A portion of the wave whose amplitude is $E_{0i}t$ is both reflected and transmitted at the interface. Without making any assumptions, let r' and t' be the amplitude reflection and transmission coefficients, respectively, for a wave incident from below (i.e., $n_i = n_2$, $n_t = n_1$). Consequently, the reflected portion is $E_{0i}tr'$, and the transmitted portion is $E_{0i}tt'$. Similarly, the incoming wave whose amplitude is $E_{0i}r$ splits into segments of amplitude $E_{0i}rr$ and $E_{0i}rt$. If the configuration in Fig. 4.49(c) is to be identical with that in Fig. 4.49(b), then obviously

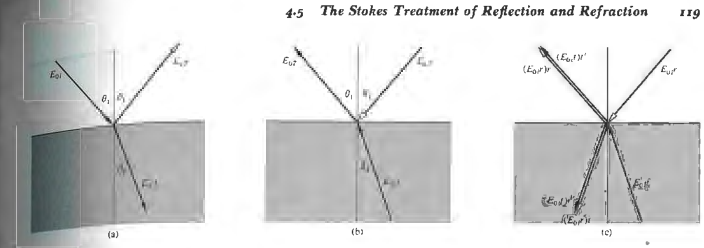


Figure 4.49 Reflection and refraction via the Stokes treatment.

$$E_{0i}tt' + E_{0i}rr = E_{0i} \tag{4.84}$$

and

$$E_{0i}rt + E_{0i}tr' = 0. \tag{4.85}$$

Hence

$$tt' = 1 - r^2 \tag{4.86}$$

and

$$r' = -r, \tag{4.87}$$

the latter two equations being known as the Stokes relations. Actually this discussion calls for a bit more caution than is usually granted it. It must be pointed out that *the amplitude coefficients are functions of the incident angles,* and therefore the Stokes relations might better be written as

$$t(\theta_1)t'(\theta_2) = 1 - r^2(\theta_1) \tag{4.88}$$

and

$$r'(\theta_2) = -r(\theta_1), \tag{4.89}$$

where $n_1 \sin \theta_1 = n_2 \sin \theta_2$. The second equation indicates, by virtue of the minus sign, that *there is a* 180° *phase difference between the waves internally and externally reflected.* It is most important to keep in mind that here θ_1 and θ_2 are pairs of angles that are related by way of Snell's law. Note as well that we never did say whether n_1 was greater or less than n_2, so Eqs. (4.88) and (4.89) apply in either case. Let's return for a moment to one of the Fresnel equations:

$$r_\perp = -\frac{\sin(\theta_i - \theta_t)}{\sin(\theta_i + \theta_t)}. \qquad [4.42]$$

If a ray enters from above, as in Fig. 4.49(a), and we assume $n_2 > n_1$, $r_\perp$ is computed by setting $\theta_i = \theta_1$ and $\theta_t = \theta_2$ (external reflection), the latter being derived from Snell's law. If, on the other hand, the wave is incident at that same angle from below (in this instance internal reflection), $\theta_i = \theta_1$ and we again substitute in Eq. (4.42), but here θ_t is not θ_2, as before. The values of $r_\perp$ for internal and external reflection *at the same incident angle* are obviously different. Now suppose, in this case of internal reflection, that $\theta_i = \theta_2$. Then $\theta_t = \theta_1$, the ray directions are the reverse of those in the first situation, and Eq. (4.42) yields

$$r'_\perp(\theta_2) = -\frac{\sin(\theta_2 - \theta_1)}{\sin(\theta_2 + \theta_1)}.$$

Although it may be unnecessary we once again point out that this is just the negative of what was determined for $\theta_i = \theta_1$ and external reflection, that is,

$$r'_\perp(\theta_2) = -r_\perp(\theta_1). \qquad (4.90)$$

The use of primed and unprimed symbols to denote the amplitude coefficients should serve as a reminder that we are once more dealing with angles related by Snell's law. In the same way, interchanging θ_i and θ_t in Eq. (4.43) leads to

$$r'_\parallel(\theta_2) = -r_\parallel(\theta_1). \qquad (4.91)$$

The 180° phase difference between each pair of components is evident in Fig. 4.25, but do keep in mind that when $\theta_i = \theta_p$, $\theta_t = \theta'_p$ and vice versa (Problem 4.46). Beyond $\theta_i = \theta_c$ there is no transmitted wave, Eq. (4.89) is not applicable, and as we have seen, the phase difference is no longer 180°.

It is common to conclude that both the parallel and perpendicular components of the externally reflected beam change phase by π radians while the internally reflected beam undergoes no phase shift at all. By now, within the particular convention we've established, this should be recognized as incorrect, or at least almost obviously [compare Figs. 4.26(a) and 4.27(a)].

4.6 PHOTONS AND THE LAWS OF REFLECTION AND REFRACTION

Suppose that light consists of a stream of photons [illegible] that one such photon strikes the interface between [illegible] dielectric media at an angle θ_i and is subseque[illegible] transmitted across it at an angle θ_t. We know that i[illegible] were just one of billions of such quanta in a narr[illegible] laserbeam, it would obediently conform to Snell's [illegible] To appreciate this behavior let's examine the dyna[illegible] associated with the odyssey of our single photon. R[illegible] that

$$\mathbf{p} = \hbar\mathbf{k},$$

and consequently the incident and transmitted [illegible]menta are $\mathbf{p}_i = \hbar\mathbf{k}_i$ and $\mathbf{p}_t = \hbar\mathbf{k}_t$, respectively [illegible] assume (without much justification) that although [illegible] material in the vicinity of the interface affects th[illegible] component of momentum, it leaves the x-compo[illegible] unchanged. Indeed we know experimentally that [illegible] momentum can be transferred to a medium fr[illegible] light beam (see Section 3.3.2). The statement of co[illegible]servation of the component of momentum parallel [illegible] the interface takes the form

$$p_{ix} = p_{tx} \qquad (4.9[illegible])$$

or

$$p_i \sin\theta_i = p_t \sin\theta_t.$$

If we use Eq. (3.53), this becomes

$$k_i \sin\theta_i = k_t \sin\theta_t$$

and hence

$$\frac{1}{\lambda_i}\sin\theta_i = \frac{1}{\lambda_t}\sin\theta_t.$$

Multiplying both sides by c/ν, we have

$$n_i \sin\theta_i = n_t \sin\theta_t,$$

which of course is Snell's law. In exactly the sa[illegible] if the photon reflects off the interface instead of being transmitted, Eq. (4.92) leads to

$$k_i \sin\theta_i = k_r \sin\theta_r,$$

and since $\lambda_i = \lambda_r$, $\theta_i = \theta_r$. It is interesting to note that

$$n_{ti} = \frac{p_t}{p_i}, \qquad (4.93)$$

and so if $n_{ti} > 1$, $p_t > p_i$. Experiments dating back as far as 1850, to those of Foucault, have shown that when $n_{ti} > 1$ the speed of propagation is actually reduced in [illegible]ansmitting media, even though the momentum [illegible]ently increases.†

[illegible] keep in mind that we have been dealing with a very simple representation that leaves much to be desired. For example, it says nothing about the atomic structure of the media or about the probability that a photon will traverse a given path. Even though this treatment is obviously simplistic, it is appealing pedagogically (see Chapter 13).

† [illegible] an increase in the photon's effective mass. See F. R. [illegible], "On Snell's Law and the Gravitational Deflection of [illegible] J. Phys. 36, 1001 (1968). Take a *cautious* look at R. A. Houst[illegible] "Nature of Light." *J. Opt. Soc. Am.* 55, 1186 (1965).

[illegible]ure 4.50 (Photos courtesy *Physics*, Boston, D. C. Heath & Co., [illegible]960.)

PROBLEMS

4.1 Calculate the transmission angle for a ray incident in air at 30° on a block of crown glass ($n_g = 1.52$).

4.2* A ray of yellow light from a sodium discharge lamp falls on the surface of a diamond in air at 45°. If at that frequency $n_d = 2.42$, compute the angular deviation suffered upon transmission.

4.3 Use Huygens's construction to create a wavefront diagram showing the form a spherical wave will have after reflection from a planar surface, as in the ripple tank photos of Fig. 4.50. Draw the ray diagram as well.

4.4* Given an interface between water ($n_w = 1.33$) and glass ($n_g = 1.50$), compute the transmission angle for a beam incident in the water at 45°. If the transmitted beam is reversed so that it impinges on the interface, show that $\theta_t = 45°$.

4.5 A beam of 12-cm planar microwaves strikes the surface of a dielectric at 45°. If $n_{ti} = \frac{4}{3}$, compute (a) the wavelength in the transmitting medium, and (b) the angle θ_t.

4.6* Light of wavelength 600 nm in vacuum enters a block of glass where $n_g = 1.5$. Compute its wavelength in the glass. What color would it appear to someone imbedded in the glass (see Table 3.2)?

4.7 Figure 4.51 shows a bundle of rays entering and emerging from a glass disk (a lens). From the configuration of the rays, determine the shape of the wavefronts at various points. Draw a diagram in profile.

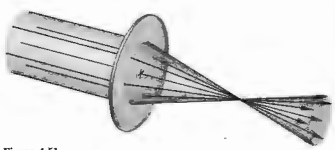


Figure 4.51

4.8 Make a plot of θ_i versus θ_t for an air–glass boundary where $n_{ga} = 1.5$.

4.9 In Fig. 4.52 the wavefronts in the incident medium match the fronts in the transmitting medium everywhere on the interface—a concept known as *wavefr*[illegible] *continuity*. Write expressions for the number of wa[illegible] per unit length along the interface in terms of θ_i and λ_i in one case and θ_t and λ_t in the other. Use [illegible] derive Snell's law. Do you think Snell's law appl[illegible] to sound waves? Explain.

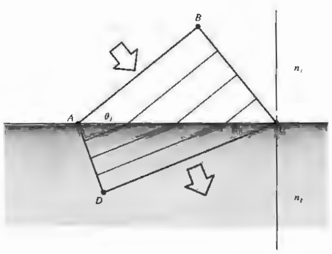


Figure 4.52

4.10* With the previous problem in mind, [illegible] Eq. (4.19) and take the origin of the coordinate sy[illegible] in the plane of incidence and on the interface [illegible] 4.20). Show that that equation is then equivalen[illegible] equating the x-components of the various propa[illegible] vectors. Show that it is also equivalent to the no[illegible] of wavefront continuity.

4.11* Figure 4.53 depicts a wavefront at $\overline{AB}$ tha[illegible] subsequently sweeps across the interface, driving ato[illegible] along it, which in turn radiate transmitted wavele[illegible] Since the refracted wave travels at a speed v_t, as[illegible] the transmitted wavelets also propagate at v_t. [illegible] wavelets then overlap and interfere (which is essen[illegible] the Huygens–Fresnel principle) to form the refr[illegible] wave. Show that the transmitted wavelets will arr[illegible] phase along $\overline{DC}$, provided Snell's law obtains.

4.12 Making use of the ideas of equal transit times between corresponding points and the orthogonali[illegible] rays and wavefronts, derive the law of reflection and Snell's law. The ray diagram of Fig. 4.54 should be helpful.

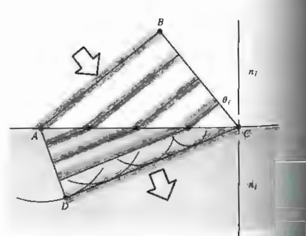


Figure 4.53

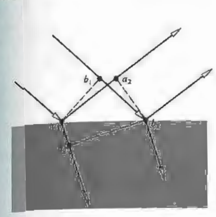


Figure 4.54

4.13 [illegible] with Snell's law, prove that the vector [illegible]tion equation has the form

$$n_t\hat{\mathbf{k}}_t - n_i\hat{\mathbf{k}}_i = (n_t \cos\theta_t - n_i \cos\theta_i)\hat{\mathbf{u}}_n. \qquad [4.8]$$

[illegible] Derive a vector expression equivalent to the law [illegible]flection. As before, let the normal go from the [illegible]dent to the transmitting medium, even though it obviously doesn't really matter.

4.1[illegible] In the case of reflection from a planar surface, [illegible] Fermat's principle to prove that the incident and [illegible]ected rays share a common plane with the normal $\hat{\mathbf{u}}_n$, namely, the plane of incidence.

4.16* Derive the law of reflection, $\theta_i = \theta_r$, by using [illegible] calculus to minimize the transit time, as required [illegible] Fermat's principle.

4.17* According to the mathematician Hermann Schwarz, there is one triangle that can be inscribed within an acute triangle such that it has a minimal perimeter. Using two planar mirrors, a laserbeam, and Fermat's principle, explain how you can show that this inscribed triangle has its vertices at the points where the altitudes of the acute triangle intersect its corresponding sides.

4.18 Show analytically that a beam entering a planar transparent plate, as in Fig. 4.55, emerges parallel to its initial direction. Derive an expression for the lateral displacement of the beam. Incidentally, the incoming and outgoing rays would be parallel even for a stack of plates of different material.

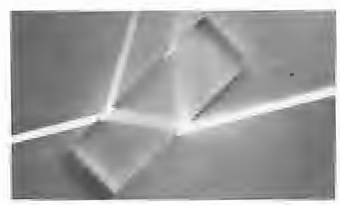


Figure 4.55 (Source unknown.)

4.19* Show that the two rays that enter the system in Fig. 4.56 parallel to each other emerge from it being parallel.

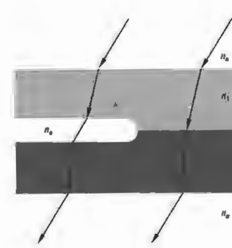


Figure 4.56

4.20 Discuss the results of Problem 4.18 in the light of Fermat's principle, that is, how does the relative index n_{21} affect things? To see the lateral displacement, look at a broad source through a thick piece of glass ($\approx\frac{1}{4}$ inch) or a stack (four will do) of microscope slides *held at an angle*. There will be an obvious shift between the region of the source seen directly and the region viewed through the glass.

4.21 Suppose a lightwave that is linearly polarized in the plane of incidence impinges at 30° on a crown-glass ($n_g = 1.52$) plate in air. Compute the appropriate amplitude reflection and transmission coefficients at the interface. Compare your results with Fig. 4.22.

4.22 Show that even in the nonstatic case the tangential component of the electric field intensity **E** is continuous across an interface. [*Hint:* using Fig. 4.57 and Eq. (3.5), shrink sides *FB* and *CD*, thereby letting the area bounded go to zero.]

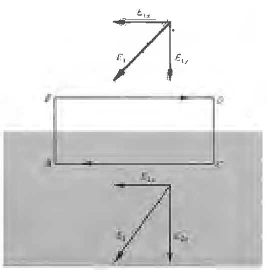


Figure 4.57

4.23 Derive Eqs. (4.42) through (4.45) for $r_\perp$, $r_\parallel$, $t_\perp$, and $t_\parallel$.

4.24 Prove that

$$t_\perp + (-r_\perp) = 1 \qquad [4.49]$$

for all θ_i, first from the boundary conditions and then from the Fresnel equations.

4.25* Verify that

$$t_\perp + (-r_\perp) = 1$$

for $\theta_i = 30°$ at a crown glass and air interface (n_g = 1.52).

4.26* Calculate the critical angle beyond which there is total internal reflection at an air–glass ($n_g = 1.5$) interface. Compare this result with that of Problem 4.8.

4.27 Derive an expression for the speed of the evanescent wave in the case of internal reflection. Write it in terms of c, n_i, and θ_i.

4.28 Light having a vacuum wavelength of 600 nm, traveling in a glass ($n_g = 1.50$) block, is incident at 45° on a glass–air interface. It is then totally internally reflected. Determine the distance into the air at which the amplitude of the evanescent wave has dropped to a value of $1/e$ of its maximum value at the interface.

4.29 Figure 4.58 shows a laserbeam incident on a piece of filter paper atop a sheet of glass whose index of refraction is to be measured—the photograph shows the resulting light pattern. Explain what is happening and derive an expression for n_t in terms of R and d.

4.30 Consider the common mirage associated with an inhomogeneous distribution of air situated above a warm roadway. Envision the bending of the rays as if it were instead a problem in total internal reflection. If an observer, at whose head $n_a = 1.00029$, sees an apparent wet spot at $\theta_i = 88.7°$ down the road, find the index of the air immediately above the road.

4.31* Use the Fresnel equations to prove that light incident at $\theta_p = \frac{1}{2}\pi - \theta_t$ results in a reflected beam that is indeed polarized.

4.32 Show that $\tan\theta_p = n_t/n_i$ and calculate the polarization angle for external incidence on a plate of crown glass ($n_g = 1.52$) in air.

4.33* Beginning with Eq. (4.38), show that for two dielectric media, in general $\tan\theta_p = [\epsilon_t(\epsilon_i\mu_t - \epsilon_t\mu_i)/\epsilon_i(\epsilon_t\mu_t - \epsilon_i\mu_i)]^{1/2}$.

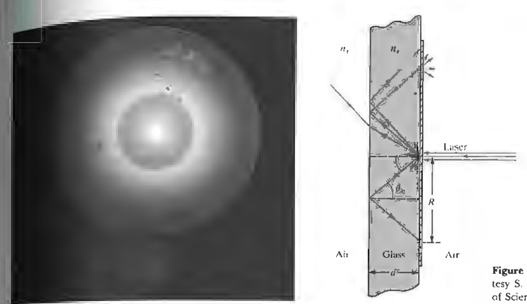


Figure 4.58 (Photo and diagram courtesy S. Reich, The Weizmann Institute of Science, Israel.)

4.34 Show that the polarization angles for internal and external reflection at a given interface are complementary, that is, $\theta_p + \theta_p' = 90°$ (see Problem 4.32).

4.35 It is often useful to work with the *azimuthal angle* γ, which is defined as the angle between the plane of vibration and the plane of incidence. Thus for linearly polarized light,

$$\tan\gamma_i = [E_{0i}]_\perp/[E_{0i}]_\parallel \qquad (4.94)$$

$$\tan\gamma_t = [E_{0t}]_\perp/[E_{0t}]_\parallel \qquad (4.95)$$

and

$$\tan\gamma_r = [E_{0r}]_\perp/[E_{0r}]_\parallel. \qquad (4.96)$$

Figure 4.59 is a plot of γ_r versus θ_i for internal and external reflection at an air–glass interface ($n_{ga} = 1.51$), where $\gamma_i = 45°$. Verify a few of the points on the curves and in addition show that

$$\tan\gamma_r = -\frac{\cos(\theta_i - \theta_t)}{\cos(\theta_i + \theta_t)}\tan\gamma_i. \qquad (4.97)$$

4.36* Making use of the definitions of the azimuthal angles in Problem 4.35, show that

$$R = R_\parallel \cos^2\gamma_i + R_\perp \sin^2\gamma_i \qquad (4.98)$$

and

$$T = T_\parallel \cos^2\gamma_t + T_\perp \sin^2\gamma_t. \qquad (4.99)$$

4.37 Make a sketch of $R_\perp$ and $R_\parallel$ for $n_i = 1.5$ and $n_t = 1$ (i.e., internal reflection).

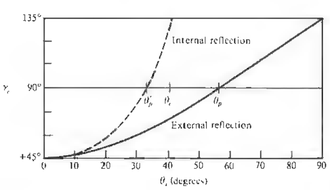


Figure 4.59

4.38 Show that

$$T_\parallel = \frac{\sin 2\theta_i \sin 2\theta_t}{\sin^2(\theta_i + \theta_t)\cos^2(\theta_i - \theta_t)} \quad (4.100)$$

and

$$T_\perp = \frac{\sin 2\theta_i \sin 2\theta_t}{\sin^2(\theta_i + \theta_t)}. \quad (4.101)$$

4.39* Using the results of Problem 4.38, that is, Eqs. (4.100) and (4.101), show that

$$R_\parallel + T_\parallel = 1 \quad [4.65]$$

and

$$R_\perp + T_\perp = 1. \quad [4.66]$$

4.40 Suppose that we look at a source perpendicularly through a stack of N microscope slides. The source seen through even a dozen slides will be noticeably darker. Assuming negligible absorption, show that the total transmittance of the stack is given by

$$T_t = (1 - R)^{2N}$$

and evaluate T_t for three slides in air.

4.41 Making use of the expression

$$I(y) = I_0 e^{-\alpha y} \quad [4.78]$$

for an absorbing medium, we define a quantity called the *unit transmittance* T_1. At normal incidence (4.55) $T = I_t/I_i$, and thus when $y = 1$, $T_1 = I(1)/I_0$. If the total thickness of the slides in the previous problem is d and if they now have a transmittance per unit length T_1, show that

$$T_t = (1 - R)^{2N}(T_1)^d.$$

4.42 Show that at normal incidence on the boundary between two dielectrics, as $n_{ti} \to 1$, $R \to 0$, and $T \to 1$. Moreover, prove that as $n_{ti} \to 1$, $R_\parallel \to 0$, $R_\perp \to 0$, $T_\parallel \to 1$, and $T_\perp \to 1$ for all θ_i. Thus as the two media take on more similar indices of refraction, less and less energy is carried off in the reflected wave. It should be obvious that when $n_{ti} = 1$ there will be no interface and no reflection.

4.43* Derive the expressions for $r_\perp$ and $r_\parallel$ given by Eqs. (4.70) and (4.71).

4.44 Show that when $\theta_i > \theta_c$ at a dielectric interface, $r_\parallel$ and $r_\perp$ are complex and $r_\perp r_\perp^* = r_\parallel r_\parallel^* = 1$.

4.45 Figure 4.60 depicts a ray being multiply reflected by a transparent dielectric plate (the amplitudes [illegible] resulting fragments are indicated). As in Section [illegible] we use the primed coefficient notation, because the angles are related by Snell's law.

a) Finish labeling the amplitudes of the last four rays.
b) Show, using the Fresnel equations, that

$$t_\parallel t'_\parallel = T_\parallel \quad (4.102)$$

$$t_\perp t'_\perp = T_\perp \quad (4.103)$$

$$r_\parallel^2 = r_\parallel'^2 = R_\parallel \quad (4.104)$$

and

$$r_\perp^2 = r_\perp'^2 = R_\perp. \quad (4.105)$$

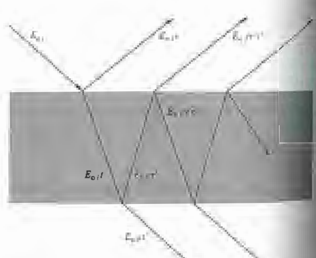


Figure 4.60

4.46* A wave, linearly polarized in the plane of incidence, impinges on the interface between two dielectric media. If $n_i > n_t$ and $\theta_i = \theta'_p$, there [illegible] reflected wave, that is, $r'_\parallel(\theta'_p) = 0$. Using Stokes's [illegible] nique, start from scratch to show that $t_\parallel(\theta_p)t'_\parallel(\theta'_p) = 1$, $r_\parallel(\theta_p) = 0$, and $\theta_t = \theta_p$ (Problem 4.34). How does this compare with Eq. (4.102)?

4.47 Making use of the Fresnel equations, show that $t_\parallel(\theta_p)t'_\parallel(\theta'_p) = 1$, as in the previous problem.

4.48 Figure 4.61 depicts a glass cube surrounded by [illegible] prisms in very close proximity to its sides. Sketch in the paths that will be taken by the two rays shown and discuss a possible application for the device.

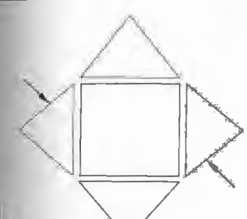


Figure 4.61

4.49 Figure 4.62 is a plot of n_I and n_R versus λ for a common metal. Identify the metal by comparing its characteristics with those considered in the chapter and discuss its optical properties.

[illegible] Figure 4.63 shows a prism-coupler arrangement developed at the Bell Telephone Laboratories. Its function is to feed a laserbeam into a thin (0.00001-inch) [illegible] film, which then serves as a sort of waveguide. One application is that of thin-film laserbeam circuitry—a kind of integrated optics. How do [illegible] it works?

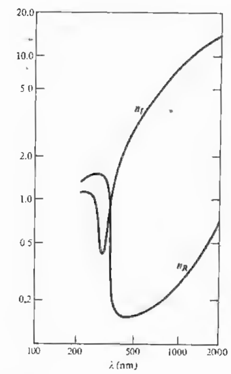


Figure 4.62

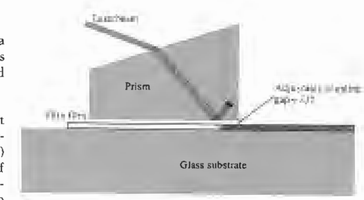


Figure 4.63

5 GEOMETRICAL OPTICS—PARAXIAL THEORY

5.1 INTRODUCTORY REMARKS

Suppose we have an object that is either self-luminous or externally illuminated, and imagine its surface as consisting of a large number of point sources. Each of these emits spherical waves, that is, rays emanate radially in the direction of energy flow or, if you like, in the direction of the Poynting vector (Fig. 4.1). In this case, the rays *diverge* from a given point source S, whereas if the spherical wave were collapsing to a point, the rays would of course be *converging*. Generally one deals only with a small portion of a wavefront. *A point from which a portion of a spherical wave diverges, or one toward which the wave segment converges, is known as a focal point of the bundle of rays.*

Now envision the situation in which we have a point source in the vicinity of some arrangement of reflecting and refracting surfaces representing an *optical system*. Of the infinity of rays emanating from S, generally speaking, only one will pass through an arbitrary point in space. Even so, it is possible to arrange for an infinite number of rays to arrive at a certain point P, as in Fig. 5.1. Thus, if for a cone of rays coming from S there is a corresponding cone of rays passing through P, the system is said to be *stigmatic* for these two points. The energy in the cone (apart from some inadvertent losses due to reflection, scattering, and absorption) reaches P, which is then referred to as a *perfect image* of S. The wave could conceivably arrive to form a finite patch of light, or *blur spot*, about P; it would still be an image of S but no longer a perfect one.

It follows from the principle of reversibility (see Section 4.2.4) that a point source placed at P would be equally well imaged at S, and accordingly the two are spoken of as *conjugate points*. In an *ideal optical system* every point of a three-dimensional region will be perfectly (or stigmatically) imaged in another region, the former being the *object space*, the latter the *image space*.

Most commonly, the function of an optical device is to collect and reshape a portion of the incident wavefront, often with the ultimate purpose of forming an image of an object. Notice that inherent in realizable systems is the limitation of being unable to collect all the emitted light; the system accepts only a segment of the wavefront. As a result, there will always be an apparent deviation from rectilinear propagation even in homogeneous media—the waves will be *diffracted*. The attainable degree of perfection in the imaging capability of a real optical system will therefore be **diffraction-limited** (there will always be a blur spot). As the wavelength of the radiant energy decreases in comparison to the physical dimensions of the optical system, the effects of diffraction become less significant. In the conceptual limit as $\lambda_0 \to 0$, rectilinear propagation obtains in homogeneous media, and we have the idealized domain of *geometrical optics*.* Behavior that is [illegible] attributable to the wave nature of light (e.g., [illegible] and diffraction) would no longer be observ[illegible] there are many situations in which the great simplicity arising from the approximation of geometrical optics more than compensates for its inac[illegible] In short, *the subject treats the controlled manipulation of wavefronts (or rays) by means of the interpositioning of reflecting and/or refracting bodies, neglecting any diffrac-*

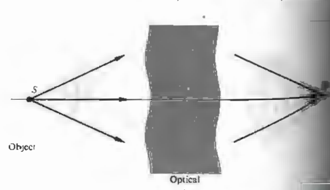


Figure 5.1 Converging and diverging waves.

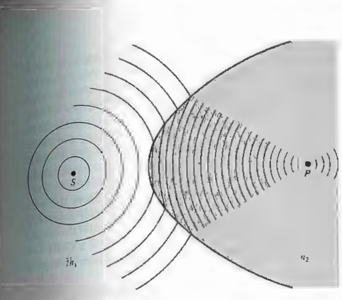


Figure 5.2 Reshaping a spherical wave at a refracting interface ($n_2 > n_1$).

[illegible] optics deals with situations in which the nonzero wavelength [illegible] must be reckoned with. Analogously, when the de Broglie wavelength of a material object is negligible, we have *classical mechanics*; when it is not, we have the domain of *quantum mechanics* (see Chapter 13).

5.2 LENSES

No doubt the most widely used optical device is the lens, and that notwithstanding the fact that we see the world through a pair of them. Lenses date back to the burning glasses of antiquity, and indeed who can say when people first peered through the liquid lens formed by a droplet of water?

As an initial step toward an understanding of what lenses do and how they manage to do it, let's examine what happens when light impinges on the curved surface of a transparent dielectric medium.

5.2.1 Refraction at Aspherical Surfaces

Imagine that we have a point source S whose spherical waves arrive at a boundary between two transparent media, as shown in Fig. 5.2. We would like to determine the shape that the interface must have for the wave traveling within the second medium to converge at a point P, there forming a perfect image of S. Practical reasons for wanting to focus a diverging wave to a point will become evident as we proceed.

The time it takes for each and every portion of a wavefront leaving S to converge at P must be identical, if a perfect image is to be formed—that much was implied by Huygens in 1678. Or as we saw in Section

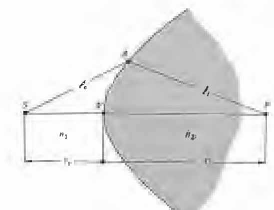


Figure 5.3 The Cartesian oval.

4.2.3, the distance between corresponding points on any and all rays will be traversed in that same time. Another way to say essentially the same thing from the perspective of Fermat's principle is that if a great many different rays are to go from S to P (i.e., if point A in Fig. 5.3 can be anywhere on the interface), each ray must traverse the same optical path length. Thus, for example, if S is in a medium of index n_1 and P is in an optically more dense medium of index n_2,

$$\ell_o n_1 + \ell_i n_2 = s_o n_1 + s_i n_2, \tag{5.1}$$

where s_o and s_i are the **object** and **image distances** measured from the *vertex* or *pole* V, respectively. Once we choose s_o and s_i, the right-hand side of this equation becomes fixed, and so

$$\ell_o n_1 + \ell_i n_2 = \text{constant}. \tag{5.2}$$

This is the equation of a *Cartesian oval* whose significance in optics was studied extensively by René Descartes in the early 1600s (Problem 5.1). Hence, when the boundary between two media has the shape of a Cartesian oval of revolution about the $\overline{SP}$, or **optical axis, S and P will be conjugate points, that is, a point source at either location will be perfectly imaged at [illegible] other. What's actually occurring physically is rather [illegible] to comprehend. Since $n_2 > n_1$, those regions of [illegible] wavefront traveling in the optically more dense medi[illegible]** move slower than those regions traversing the [illegible] material. Consequently, as the wave begins to [illegible] through the vertex of the oval, the segment immed[illegible] about the optical axis is **slowed** down from c/n_1 to [illegible] Regions of the same **wavefront** remote from the [illegible] are still in the first medium traveling with a grea[illegible] speed, c/n_1. Thus the wavefronts bend, and if the bo[illegible]dary is properly configured (in the form of a Cartesi[illegible] ovoid), the wavefronts will be inverted from diverg[illegible] to converging spherical segments.

In addition to focusing a spherical wave, we would like to be able to perform a few other reshap[illegible] operations using refracting interfaces; some of th[illegible] are illustrated in Fig. 5.4. We shall consider [illegible] briefly and more for pedagogical than practical rea[illegible] The surfaces in Fig. 5.4(a) and (b) are ellipso[illegible] whereas those in (c) and (d) are hyperholoidal. N[illegible]

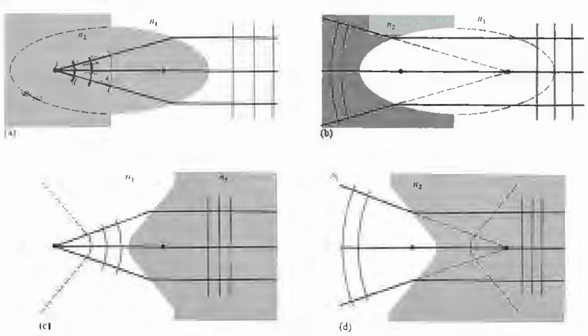


Figure 5.4 Ellipsoidal and hyperboloidal refracting surfaces ($n_2 > n_1$).

[illegible] cases the rays either diverge from or converge [illegible]ward the foci. The arrowheads have been omitted to [illegible] that the rays can go either way. In other words, an incident plane wave will converge to the farthest focus of an ellipsoid just as a spherical wave emitted from that focus will emerge as a plane wave. Furthermore, as you might expect, if we let the point S in Fig. 5.2 move out to infinity, the ovoid would gradually metamorphose into an ellipsoid.

[illegible]er than deriving expressions for these surfaces, [illegible] just justify the above remarks. To that end, examine [illegible] which relates back to Fig. 5.4(a). The optical [illegible] lengths from any point D on the planar wavefront [illegible] the focus F_1 must all be equal to the same constant C, [illegible]

$$(\overline{F_1A})n_2 + (\overline{AD})n_1 = C$$

or

$$(\overline{F_1A}) + (\overline{AD})n_{12} = C/n_2. \tag{5.3}$$

[illegible] this relationship is indeed satisfied by an ellipsoid of revolution, recall that if Σ corresponds to [illegible]trix of the ellipse, $(\overline{F_2A}) = e(\overline{AD})$, where e is [illegible]tricity. Thus if $e = n_{12}$, the left-hand side of [illegible] becomes $(\overline{F_1A}) + (\overline{F_2A})$, which is certainly constant for an ellipse. Here the eccentricity is less than 1 [illegible] n_2) and it is left for Problem 5.2 to show that [illegible]een greater than 1 (i.e., $n_1 > n_2$), the curve would [illegible] a hyperbola instead [compare (a) with (c) and (b) with (d) in Fig. 5.4]. If all this brings back memories of analytic geometry, you might keep in mind that that subject was originated by Descartes. Interestingly, it was Kepler who first (1611) suggested using conic sections [illegible]rs and lenses.

[illegible] knowledge we have at hand now may be used [illegible] construct lenses such that both the object and image [illegible]ints can be in the same medium, which is usually air. [illegible] such device to be considered [Fig. 5.6(a)] is a [illegible] lens, which utilizes the response [illegible]aracterized in Fig. 5.4(c). A diverging spherical wave [illegible]comes planar after traversing the first hyperbolic [illegible]rface and then spherically converging on leaving the [illegible]ns. Alternatively, if the second surface is made planar [illegible] that we have a *hyperbolic planar convex* lens, as in Fig. [illegible] waves within the lens will strike the [illegible] surface perpendicularly and emerge unaltered.

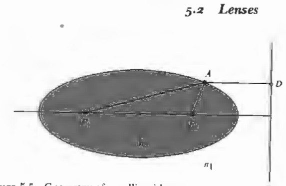
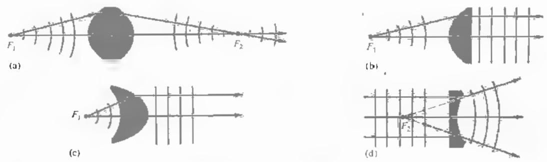


Figure 5.5 Geometry of an ellipsoid.

Another arrangement that will convert diverging spherical waves into plane waves is illustrated in Fig. 5.6(c). This is a *sphero-elliptic convex* lens, where F_1 is simultaneously at the center of the spherical surface and at the focus of the ellipsoid. Rays from F_1 strike the first surface perpendicularly and are therefore undeviated by it. As in Fig. 5.4(a), the exiting wavefronts are **planar**. All the elements thus far examined have been thicker at their midpoints than at their edges and are for that reason said to be *convex* (from the Latin *convexus*, meaning arched). In contrast, the *planar hyperbolic concave* lens (from the Latin *concavus*, meaning hollow, and easily remembered because it contains the word cave) is thinner at the middle than at the edges, as is evident in Fig. 5.6(d). A number of other arrangements are possible, and a few will be considered in the problems (5.3). Note that each of these lenses will work just as well in reverse: the waves shown emerging can instead be thought of as entering from the right.

If a point source is positioned on the optical axis at the point F_1 of the lens in Fig. 5.6(a), rays will *converge* to the conjugate point F_2. A luminous image of the source would appear on a screen placed at F_2, an image that is therefore said to be **real**. On the other hand, in Fig. 5.6(d) the point source is at infinity, and the rays emerging from the system this time are *diverging*. They appear to come from a point F_2, but no actual luminous image would appear on a screen at that location. The image here is spoken of as **virtual**, as is the familiar image generated by a plane mirror.

Optical elements (lenses and mirrors) of the sort we have talked about, with one or both surfaces neither planar nor spherical, are referred to as *aspherics*. Although their operation is easy to understand and they perform certain tasks exceedingly well, they are still



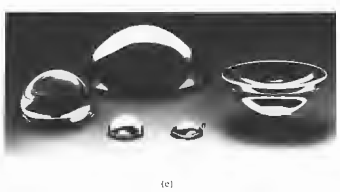


Figure 5.6 (a) A double hyperbolic lens. (b) A [illegible] convex lens. (c) A sphero-elliptic lens. (d) A planar [illegible] (e) Photo courtesy Melles Griot.

difficult to manufacture with great accuracy. Nonetheless, where the costs are justifiable or the required precision is not restrictive or the volume produced is large enough, aspherics are being used extensively and will surely have an increasingly important role. The first quality glass aspheric to be manufactured in great quantities (tens of millions) was a lens for the Kodak disk camera (1982). And the small-scale production of diffraction-limited molded-glass aspheric lenses has been reported in recent times. Today aspherical lenses are frequently used as an elegant means of correcting imaging errors in complicated optical systems.

A new generation of computer-controlled machines, aspheric generators, is producing elements with tolerances (i.e., departures from the desired surface) of better than 0.5 μm (0.000020 inch). This is still about a factor of 10 away from the generally required tolerance of $\lambda/4$ for quality optics, but that will surely come in time. Nowadays aspherics made in plastic and glass can be found in all kinds of instruments across the whole range of quality, including telescopes, projectors, cameras, and reconnaissance devices.

5.2.2 Refraction at Spherical Surfaces

Imagine that we have two pieces of material, [illegible] a concave and the other a convex spherical surface, having the same radius. It is a unique property of sphere that such pieces will fit together in [illegible] contact regardless of their mutual orientation. [illegible] we take two roughly spherical objects of suitable cur[illegible]

Figure 5.7 Polishing a spherical lens. (Photo courtesy [illegible] of America.)

[illegible] a grinding tool and the other a disk of glass, [illegible] them with some abrasive, and then randomly [illegible] them with respect to each other, we can anticipate [illegible] high spots on either object will wear away. As [illegible]ar, both pieces will gradually become more [illegible]cal (Fig. 5.7). Such surfaces are now commonly generated in batches by automatic grinding and polishing machines. In contrast, high-quality aspherical shapes require considerably more effort to produce.

It should therefore come as no surprise that the vast majority of quality lenses in use today have spherical [illegible]aces. Our intent here is to establish techniques for [illegible] such surfaces whereby a great many object points [illegible] satisfactorily imaged simultaneously in light com[illegible] of a broad frequency range. Image errors, known [illegible]ions, will occur, but it is possible with the [illegible] technology to construct high-quality spherical lens systems whose aberrations are so well controlled that image fidelity is limited only by diffraction.

[illegible] that we know why and where we are going, let's move on. Figure 5.8 depicts a wave from the point source S impinging on a spherical interface of radius R centered at C. The ray $(\overline{SA})$ will be refracted at the interface toward the local normal ($n_2 > n_1$) and there[illegible] toward the optical axis. Assume that at some point [illegible] cross the axis, as will all other rays incident at [illegible] angle θ_i (Fig. 5.9). Fermat's principle maintains that the optical path length (OPL) will be stationary, that is, its derivative with respect to the position variable will be zero. For the ray in question,

$$(\mathrm{OPL}) = n_1 \ell_o + n_2 \ell_i. \tag{5.4}$$

Using the law of cosines in triangles SAC and ACP along with the fact that $\cos\varphi = -\cos(180 - \varphi)$, we get

$$\ell_o = [R^2 + (s_o + R)^2 - 2R(s_o + R)\cos\varphi]^{1/2}$$

and

$$\ell_i = [R^2 + (s_i - R)^2 + 2R(s_i - R)\cos\varphi]^{1/2}.$$

The OPL can be rewritten as

$$(\mathrm{OPL}) = n_1[R^2 + (s_o + R)^2 - 2R(s_o + R)\cos\varphi]^{1/2} + n_2[R^2 + (s_i - R)^2 + 2R(s_i - R)\cos\varphi]^{1/2}.$$

All the quantities in the diagram (s_i, s_o, R, etc.) are positive numbers, and these form the basis of a *sign convention* which is gradually unfolding and to which

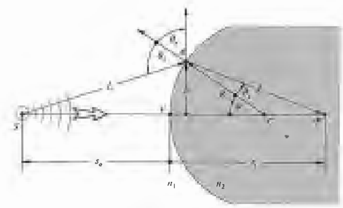


Figure 5.8 Refraction at a spherical interface.

we shall return time and again (see Table 5.1). Inasmuch as the point A moves at the end of a fixed radius (i.e., R = constant), φ is the position variable, and thus setting $d(\mathrm{OPL})/d\varphi = 0$, via Fermat's principle we have

$$\frac{n_1 R(s_o + R)\sin\varphi}{2\ell_o} - \frac{n_2 R(s_i - R)\sin\varphi}{2\ell_i} = 0,$$

from which it follows that

$$\frac{n_1}{\ell_o} + \frac{n_2}{\ell_i} = \frac{1}{R}\left(\frac{n_2 s_i}{\ell_i} - \frac{n_1 s_o}{\ell_o}\right). \tag{5.5}$$

This is the relationship that must hold among the parameters for a ray going from S to P by way of refraction at the spherical interface. Although this expression is exact, it is rather complicated. We already know that if A is moved to a new location by changing φ, the new ray will not intercept the optical axis at P—this is not a

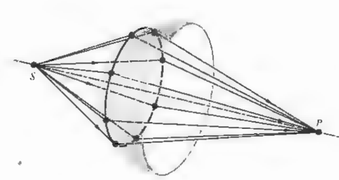


Figure 5.9 Rays incident at the same angle.

Table 5.1 Sign convention for spherical refracting surfaces and thin lenses* (light entering from the left).

s_o, f_o	+ left of V
x_o	+ left of F_o
s_i, f_i	+ right of V
x_i	+ right of F_i
R	+ if C is right of V
y_o, y_i	+ above optical axis

* This table anticipates the imminent introduction of a few quantities not yet spoken of

Cartesian oval. The approximations that are used to represent ℓ_o and ℓ_i, and thereby simplify Eq. (5.5), are crucial in all that is to follow. Recall that

$$\cos\varphi = 1 - \frac{\varphi^2}{2!} + \frac{\varphi^4}{4!} - \frac{\varphi^6}{6!} + \cdots \tag{5.6}$$

and

$$\sin\varphi = \varphi - \frac{\varphi^3}{3!} + \frac{\varphi^5}{5!} - \frac{\varphi^7}{7!} + \cdots. \tag{5.7}$$

If we assume small values of φ (i.e., A close to V), $\cos\varphi \approx 1$. Consequently, the expressions for ℓ_o and ℓ_i yield $\ell_o \approx s_o$, $\ell_i \approx s_i$, and to that approximation

$$\frac{n_1}{s_o} + \frac{n_2}{s_i} = \frac{n_2 - n_1}{R}. \tag{5.8}$$

We could have begun this derivation with Snell's law rather than Fermat's principle (Problem 5.4), in which case small values of φ would have led to $\sin\varphi \approx \varphi$ and Eq. (5.8) once again. This approximation delineates the domain of what is called *first-order theory*—we'll examine *third-order theory* ($\sin\varphi \approx \varphi - \varphi^3/3!$) in the next chapter. Rays that arrive at shallow angles with respect to the optical axis (such that φ and h are appropriately small) are known as **paraxial rays.** The *emerging wavefront segment corresponding to these paraxial rays is essentially spherical and will form a "perfect" image at its center P located at* s_i. Notice that Eq. (5.8) is independent of the location of A over a small area about the symmetry axis, namely, the *paraxial region.* Gauss, in 1841, was the first to give a systematic exposition of the formation of images under the above approximation, and the result is variously known as *first-order, paraxial,* or **Gaussian optics.** It soon became the basic theoretical tool by which lenses would be designed for several decades to come. If the optical system is well corrected, an incident spherical wave will emerge in a form very closely resembling a spherical wave. Consequently, as the perfection of the system increases, it more closely approaches first-order theory. Deviations from that of paraxial analysis will provide a convenient measure of the quality of an actual optical device.

If the point F_o in Fig. 5.10 is imaged at infinity ($s_i = \infty$), we have

$$\frac{n_1}{s_o} + \frac{n_2}{\infty} = \frac{n_2 - n_1}{R}.$$

That special object distance is defined as the *first focal length* or the *object focal length,* $s_o \equiv f_o$, so that

$$f_o = \frac{n_1}{n_2 - n_1} R. \tag{5.9}$$

The point F_o is known as the *first* or *object focus.* Similarly the *second or image focus* is the axial point F_i, where the image is formed when $s_o = \infty$, that is,

$$\frac{n_1}{\infty} + \frac{n_2}{s_i} = \frac{n_2 - n_1}{R}.$$

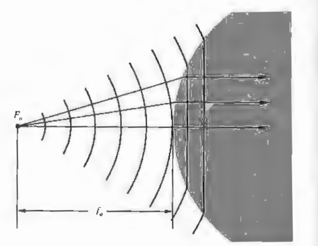


Figure 5.10 Plane waves propagating beyond a spherical interface—the object focus.

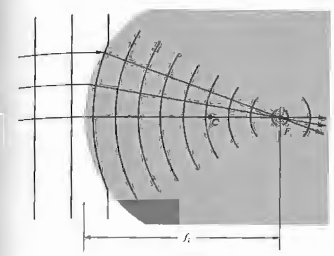


Figure 5.11 The reshaping of plane into spherical waves at a spherical interface—the image focus.

Defining the *second or image focal length* f_i as equal to s_i in this special case (Fig. 5.11), we have

$$f_i = \frac{n_2}{n_2 - n_1} R. \tag{5.10}$$

Recall that an image is virtual when the rays **diverge** from it (Fig. 5.12). Analogously, *an object is virtual when the rays converge toward it* (Fig. 5.13). Observe that the **virtual object is now on the right-hand side of the vertex, and therefore s_o will be a negative quantity. Moreover, the surface is concave, and its radius will also be negative, as required by Eq. (5.9), since f_o would be negative. In the same way the virtual image distance appearing to the left of V is negative.**

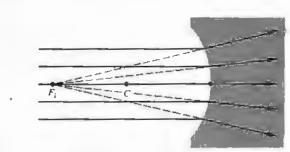


Figure 5.12 A virtual image point.

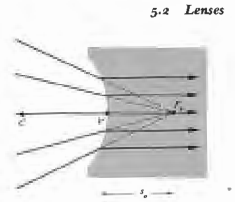


Figure 5.13 A virtual object point.

5.2.3 Thin Lenses

Lenses are made in a wide range of forms; for example, there are acoustic and microwave lenses; some of the latter are made of glass or wax in easily recognizable shapes, whereas others are far more subtle in appearance (Fig. 5.14). In the traditional sense, *a lens is an optical system consisting of two or more refracting interfaces, at least one of which is curved.* Generally the nonplanar surfaces are centered on a common axis. These surfaces are most frequently spherical segments and are often coated with thin dielectric films to control their transmission properties (see Section 9.9). A lens that consists of one element (i.e., it has only two refracting surfaces) is a *simple lens.* The presence of more than one element makes it a *compound lens.* A lens is also classified as to whether it is *thin* or *thick,* that is, whether its thickness is effectively negligible or not. We will limit ourselves, for the most part, to *centered systems* (for which all surfaces are rotationally symmetric about a common axis) of spherical surfaces. Under these restrictions, the simple lens can take the diverse forms shown in Fig. 5.15. Lenses that are variously known as *convex, converging,* or *positive* are thicker at the center and so tend to decrease the radius of curvature of the wavefronts. In other words, the wave converges more as it traverses the lens, assuming, of course, that the index of the lens is greater than that of the media in which it is immersed. *Concave, diverging,* or *negative* lenses, on the other hand,

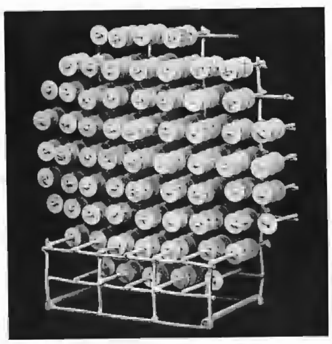


Figure 5.14 A lens for short-wavelength radiowaves. The disks serve to refract these waves much as rows of atoms refract light. (Photo courtesy Optical Society of America.)

are thinner at the center and tend to advance that portion of the wavefront, causing it to diverge more then it did upon entry.

In the broadest sense, *a lens is a refracting device that is used to reshape wavefronts in a controlled manner.* Although this is usually done by passing the wave through at least one specially shaped interface separating two different homogeneous media, it is not the only approach available. For example, it is also possible to reconfigure a wavefront by passing it through an inhomogeneous medium. A *gradient-index*, or GRIN, lens is one where the desired effect is accomplished by using a medium in which the index of refraction varies in a prescribed fashion. Different portions of the wave propagate at different speeds, and the front changes shape as it progresses. In the commercial GRIN material (available only since 1976) the index varies radially, decreasing parabolically out from the central axis.

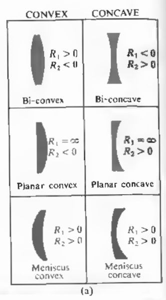


Figure 5.15 Cross sections of various centered spherical simple lenses. The surface on the left is #1 since it is encountered first. Its radius is R_1. (Photo courtesy of Melles Griot.)

Today GRIN lenses are still fabricated in quantity only in the form of small-diameter, parallel, flat-faced rods. Usually grouped together in large arrays, they have been used extensively in such equipment as facsimile machines and compact copiers. There are other unconventional lenses, including the holographic lens and even the gravitational lens (where, for example, the gravity of a galaxy bends light passing in its vicinity, thereby forming multiple images of distant celestial objects, such as quasars). We shall focus our attention in the remainder of this chapter on the more traditional types of lenses, even though you are actually reading these words through a GRIN lens (p.179).

i) Thin-Lens Equations

Return for a moment to the discussion of refraction at a single spherical interface, where the location of the conjugate points S and P is given by

$$\frac{n_1}{s_o} + \frac{n_2}{s_i} = \frac{n_2 - n_1}{R}. \tag{5.8}$$

When s_o is large for a fixed $(n_2 - n_1)/R$, s_i is relatively small. As s_o decreases, s_i moves away from the vertex, that is, both θ_i and θ_t increase until finally $s_o = f_o$ and $s_i = \infty$. At that point, $n_1/s_o = (n_2 - n_1)/R$, so that if s_o gets any smaller, s_i will have to be negative, if Eq. (5.8) is to hold. In other words, the image becomes virtual (Fig. 5.16). Let's now locate the conjugate points for the lens of index n_l surrounded by a medium of index n_m, as in Fig. 5.17, where another end has simply been ground on the piece in Fig. 5.16(c). This certainly isn't the most general set of circumstances, but it is the most common, and even more cogently, it is the simplest.* We know from Eq. (5.8) that the paraxial rays issuing from S at s_{o1} will meet at P', a distance, which we now call s_{i1}, from V_1, given by

$$\frac{n_m}{s_{o1}} + \frac{n_l}{s_{i1}} = \frac{n_l - n_m}{R_1}. \tag{5.11}$$

Thus as far as the second surface is concerned, it "sees" rays coming toward it from P', which serves as its object

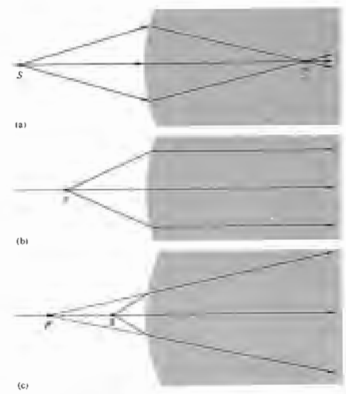


Figure 5.16 Refraction at a spherical interface.

point a distance s_{o2} away. Furthermore, the rays arriving at that second surface are in the medium of index n_l. Thus, the object space for the second interface that contains P' has an index n_l. Note that the rays from P' to that surface are indeed straight lines. Considering the fact that

$$|s_{o2}| = |s_{i1}| + d,$$

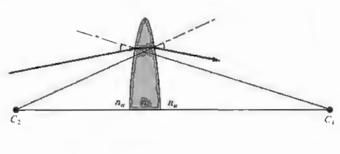
since s_{o2} is on the left and therefore positive, $s_{o2} = |s_{o2}|$, and s_{i1} is also on the left and therefore negative, $-s_{i1} = |s_{i1}|$, we have

$$s_{o2} = -s_{i1} + d. \tag{5.12}$$

Thus at the second surface Eq. (5.8) yields

$$\frac{n_l}{(-s_{i1} + d)} + \frac{n_m}{s_{i2}} = \frac{n_m - n_l}{R_2} \tag{5.13}$$

* See Jenkins and White, *Fundamentals of Optics*, p. 57, for a derivation containing three different indices.



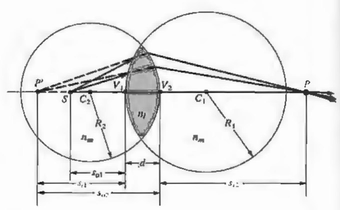


Figure 5.17 A spherical lens. (a) Refraction at the interfaces. The radius drawn from C_1 is normal to the first surface, and as the ray enters the lens it bends down *toward* that normal. The radius from C_2 is normal to the second surface; and as the ray emerges, since $n_l > n_a$, the ray bends down *away* from that normal. (b) The geometry.

Here $n_l > n_m$ and $R_2 < 0$, so that the right-hand side is positive. Adding Eqs. (5.11) and (5.13), we have

$$\frac{n_m}{s_{o1}} + \frac{n_m}{s_{i2}} = (n_l - n_m)\left(\frac{1}{R_1} - \frac{1}{R_2}\right) + \frac{n_l d}{(s_{i1} - d)s_{i1}} \qquad (5.14)$$

If the lens is thin enough ($d \to 0$), the last term on the right is effectively zero. As a further simplification, assume the surrounding medium to be air (i.e., $n_m \approx 1$). Accordingly, we have the very useful **thin-lens equation**, often referred to as the **lensmaker's formula**:

$$\frac{1}{s_o} + \frac{1}{s_i} = (n_l - 1)\left(\frac{1}{R_1} - \frac{1}{R_2}\right), \qquad (5.15)$$

where we let $s_{o1} = s_o$ and $s_{i2} = s_i$. The points V_1 and V_2 tend to coalesce as $d \to 0$, so that s_o and s_i can be measured from either the vertices or the lens center.

Just as in the case of the single spherical surface, if s_o is moved out to infinity, the image distance becomes the focal length f_i, or symbolically,

$$\lim_{s_o \to \infty} s_i = f_i.$$

Similarly

$$\lim_{s_i \to \infty} s_o = f_o.$$

It is evident from Eq. (5.15) that for a thin lens $f_i = f_o$, and consequently we drop the subscripts altogether. Thus

$$\frac{1}{f} = (n_l - 1)\left(\frac{1}{R_1} - \frac{1}{R_2}\right) \qquad (5.16)$$

and

$$\frac{1}{s_o} + \frac{1}{s_i} = \frac{1}{f}, \qquad (5.17)$$

which is the famous **Gaussian lens formula**. As an example of how these expressions might be used, let's compute the focal length in air of a thin planar-convex lens having a radius of curvature of 50 mm and an index of 1.5. With light entering on the planar surface ($R_1 = \infty$, $R_2 = -50$),

$$\frac{1}{f} = (1.5 - 1)\left(\frac{1}{\infty} - \frac{1}{-50}\right),$$

whereas if instead it arrives at the curved surface ($R_1 = +50$, $R_2 = \infty$),

$$\frac{1}{f} = (1.5 - 1)\left(\frac{1}{+50} - \frac{1}{\infty}\right),$$

and in either case $f = 100$ mm. If an object is alternately placed at distances 600 mm, 200 mm, 150 mm, 100 mm, and 50 mm from the lens on either side, we can find the image points from Eq. (5.17). Hence

$$\frac{1}{600} + \frac{1}{s_i} = \frac{1}{100}$$

and $s_i = 120$ mm. Similarly, the other image distances are 200 mm, 300 mm, ∞, and -100 mm, respectively. Interestingly enough, when $s_o = \infty$, $s_i = f$; as s_o decreases, s_i increases positively until $s_o = f$ and s_i is negative thereafter. You can qualitatively check this out with a simple convex lens and a small electric light—the high-intensity variety that uses auto lamps is probably the most convenient. Standing as far as you can from the source, project a clear image of it onto a white sheet of paper. You should be able to see the lamp quite clearly and not just as a blur. That image distance approximates f. Now move the lens in toward S, adjusting s_i to produce a clear image. It will surely increase. As $s_o \to f$, a clear image of the filament can be projected, but only on an increasingly distant screen. For $s_o < f$, there will just be a blur where the farthest wall intersects the diverging cone of rays—the image is virtual.

ii) Focal Points and Planes

Figure 5.18 summarizes pictorially some of the situations described analytically by Eq. 5.16. Observe that if a lens of index n_l is in a medium of index n_m,

$$\frac{1}{f} = (n_{lm} - 1)\left(\frac{1}{R_1} - \frac{1}{R_2}\right). \qquad (5.18)$$

The focal lengths in (a) and (b) of Fig. 5.18 are equal, because the same medium exists on either side of the lens. Since $n_l > n_m$, it follows that $n_{lm} > 1$. In both cases $R_1 > 0$ and $R_2 < 0$, so that each focal length is positive. We have a real object in (a) and a real image in (b). In (c), $n_l < n_m$, and consequently f is negative. In (d) and (e), $n_{lm} > 1$ but $R_1 < 0$, whereas $R_2 > 0$, so f is again negative, and the object in one case and the image in

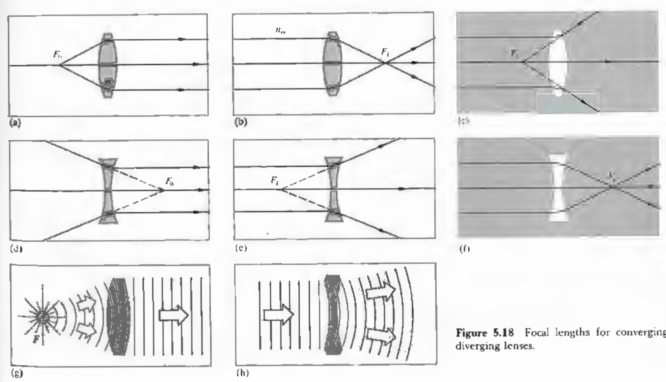


Figure 5.18 Focal lengths for converging and diverging lenses.

the other are virtual. The last situation shows $n_{tm} < 1$, yielding an $f > 0$.

Notice that in each instance it is particularly convenient to draw a ray through the center of the lens, which, because it is perpendicular to both surfaces, is undeviated. Suppose, however, that an off-axis paraxial ray emerges from the lens parallel to its incident direction, as in Fig. 5.19. We maintain that all such rays will pass through the point defined as the *optical center* of the lens O. To see this, draw two parallel planes, one on each side tangent to the lens at any pair of points A and B. This can easily be done by selecting A and B such that the radii $\overline{AC_1}$ and $\overline{BC_2}$ are themselves parallel. It is to be shown that the paraxial ray traversing $\overline{AB}$ enters and leaves the lens in the same direction. It is evident from the diagram that triangles AOC_1 and

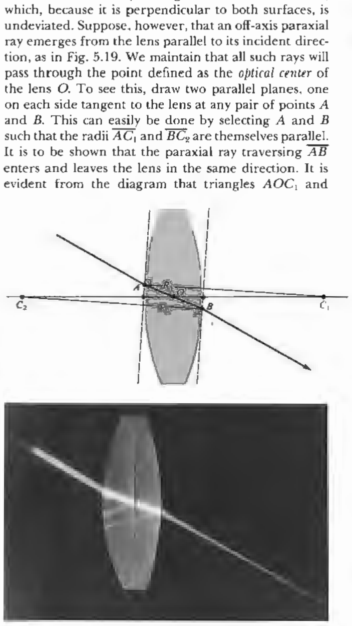


Figure 5.19 The optical center of a lens. (Photo by E.H.)

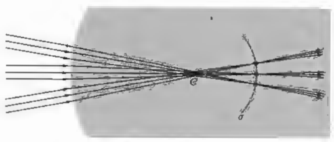


Figure 5.20 Focusing of several ray bundles.

BOC_2 are similar, in the geometric sense, and therefore their sides are proportional. Hence, $|R_1|(\overline{OC_2}) = |R_2|(\overline{OC_1})$, and since the radii are constant, the location of O is constant, independent of A and B. As we saw earlier (Problem 4.19 and Fig. 4.55), a ray traversing a medium bounded by parallel planes will be displaced laterally but will suffer no angular deviation. This displacement is proportional to the thickness, which for a thin lens is negligible. *Rays passing through O may, accordingly, be drawn as straight lines.* It is customary when dealing with thin lenses simply to place O midway between the vertices.

Recall that a bundle of parallel paraxial rays incident on a spherical refracting surface comes to a focus at a point on the optical axis (Fig. 5.11). As shown in Fig. 5.20, this implies that several such bundles entering in a narrow cone will be focused on a spherical segment σ, also centered on C. The undeviated rays normal to the surface, and therefore passing through C, locate the foci on σ. Since the ray cone must indeed be narrow, σ can satisfactorily be represented as a plane normal to the symmetry axis and passing through the image focus. It is known as a **focal plane**. In the same way, limiting ourselves to paraxial theory, a lens will focus all incident parallel bundles of rays* onto a surface called the *second or back focal plane*, as in Fig. 5.21. Here each point on σ is located by the undeviated ray through O. Similarly, the *first* or *front focal plane* contains the object focus F_o.

* Perhaps the earliest literary reference to the focal properties of a lens appears in Aristophanes' play, *The Clouds*, which dates back to 423 B.C. In it Strepsiades plots to use a burning glass to focus the Sun's rays onto a wax tablet and thereby melt out the record of a gambling debt.

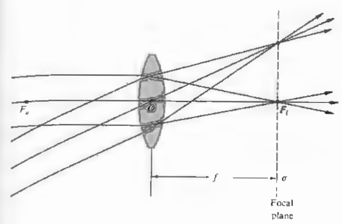


Figure 5.21 The focal plane of a lens.

iii) Finite Imagery

Thus far we've dealt with the mathematical abstraction of a single-point source, but now let's suppose that a great many such points combine to form a continuous finite object. For the moment, imagine the object to be a segment of a sphere, σ_o, centered on C, as in Fig. 5.22. If σ_o is close to the spherical interface, point S will have a virtual image P ($s_i < 0$ and therefore on the left of V). With S farther away, its image will be real ($s_i > 0$ and therefore on the right-hand side). In either case, each point on σ_o has a conjugate point on σ_i lying on a straight line through C. Within the restrictions of paraxial theory, these surfaces can be considered planar. Thus a small planar object normal to the optical axis will be imaged into a small planar region also normal to that axis. It should be noted that if σ_o is moved out to infinity, the cone of rays from each source point will become **collimated** (i.e., parallel), and the image points will lie on the focal plane (Fig. 5.21).

By cutting and polishing the right side of the piece depicted in Fig. 5.22, we can construct a thin lens, just as was done in Section (i). Once again, the image (σ_i in Fig. 5.22) formed by the first surface of the lens will serve as the object for the second surface, which in turn will generate a final image. Suppose then that σ_i in Fig. 5.22(a) is the object for the second surface, which is assumed to have a negative radius. We already know what will happen next—the situation is identical to Fig. 5.22(b) with the ray directions reversed. The *final image formed by a lens of a small planar object normal to the optical axis will itself be a small plane normal to that axis.*

The location, size, and orientation of an image produced by a lens can be determined, particularly simply, with ray diagrams. To find the image of the object in Fig. 5.23, we must locate the image point corresponding to each object point. Since all rays issuing from a source point in a paraxial cone will arrive at the image point, any two such rays will suffice to fix that point. Since we know the positions of the focal points, there are three rays that are especially easy to apply. Two of these make use of the fact that a ray passing through the focal point will emerge from the lens parallel to the optical axis and vice versa; the third is the undeviated ray through

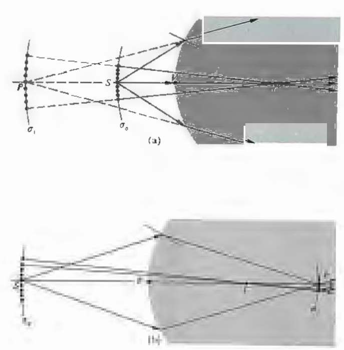


Figure 5.22 Finite imagery.

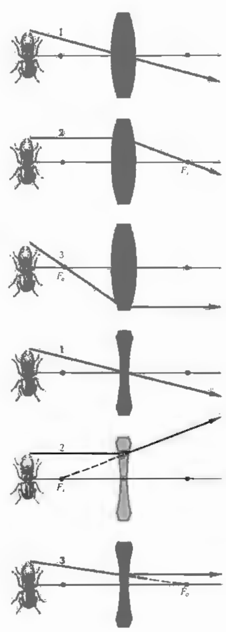


Figure 5.23 Tracing a few key rays through a positive and negative lens.

O. Figure 5.24 shows how any *two* of these three rays locate the image of a point on the object. Incidentally, this technique dates back to the work of Robert Smith as long ago as 1738.

This graphical procedure can be made even simpler by replacing the thin lens with a plane passing through its center (Fig. 5.25). Presumably, if we were to extend every incoming ray forward a little and every outgoing ray backward a bit, each pair would meet on this plane. Thus the total deviation of any ray can be envisaged as occurring all at once on that plane. This is equivalent to the actual process consisting of two separate angular shifts, one at each interface. (As we will see later, this is tantamount to saying that the two principal planes of a thin lens coincide.)

In accord with convention, transverse distances above the optical axis are taken as positive quantities, and those below the axis are given negative numerical values. Therefore in Fig. 5.25 $y_o > 0$ and $y_i < 0$. Here the image is said to be *inverted*, whereas if $y_i > 0$ when $y_o > 0$, it is *erect*. Observe that triangles AOF_i and $P_2P_1F_i$ are similar. Ergo

$$\frac{y_o}{|y_i|} = \frac{f}{(s_i - f)}. \tag{5.19}$$

Likewise, triangles S_2S_1O and P_2P_1O are similar and

$$\frac{y_o}{|y_i|} = \frac{s_o}{s_i}, \tag{5.20}$$

where all quantities other than y_i are positive. Hence

$$\frac{s_o}{s_i} = \frac{f}{(s_i - f)} \tag{5.21}$$

and

$$\frac{1}{f} = \frac{1}{s_o} + \frac{1}{s_i},$$

which is, of course, the Gaussian lens equation (5.17). Furthermore, triangles $S_2S_1F_o$ and BOF_o are similar and

$$\frac{f}{(s_o - f)} = \frac{|y_i|}{y_o}. \tag{5.22}$$

Using the distances measured from the focal points and

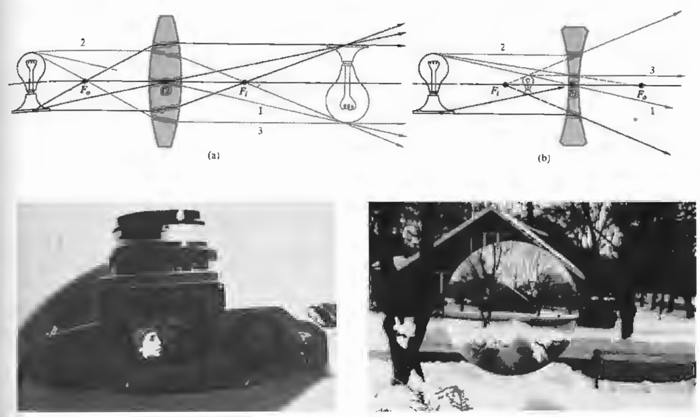


Figure 5.24 (a) A real object and a positive lens. (b) A real object and a negative lens. (c) A real image projected on the viewing screen much as the eye projects its image on the retina. (d) The minified, rightside-up, virtual image formed by a negative lens.

combining this information with Eq. (5.19), we have

$$x_o x_i = f^2. \tag{5.23}$$

This is **the Newtonian form** of the lens equation, the first statement of which appeared in Newton's *Opticks* in 1704. **The signs of x_o and x_i are reckoned with respect to their concomitant foci. By convention x_o is taken to be positive left of F_o, whereas x_i is positive on the right of F_i. To he sure, it is evident from Eq. (5.23) that x_o and x_i have like signs, which means that *the object and*** *image must be on opposite sides of their respective focal points.* This is a good thing for the neophyte to remember

Figure 5.25 Object and image location for a thin lens.

when making those hasty freehand ray diagrams for which he is already infamous.

The ratio of the transverse dimensions of the final image formed by any optical system to the corresponding dimension of the object is defined as the *lateral* or **transverse magnification**, M_T, that is,

$$M_T = \frac{y_i}{y_o}. \tag{5.24}$$

Or from Eq. (5.20)

$$M_T = -\frac{s_i}{s_o}, \tag{5.25}$$

Thus *a positive M_T connotes an erect image, while a negative value means the image is inverted* (see Table 5.2). Bear in mind that s_i and s_o are both positive for real objects and images. *Clearly, then, all such images formed by a single thin lens will be inverted.* The Newtonian expression for the magnification follows from Eqs. (5.19) and (5.22) and Fig. 5.24, whence

$$M_T = -\frac{x_i}{f} = -\frac{f}{x_o}. \tag{5.26}$$

The term magnification is a misnomer, since the magnitude of M_T can certainly be less than 1, in which case the image is smaller than the object. We have $M_T = -1$ when the object and image distances are positive and equal, and that happens (5.17) only when $s_o = s_i = 2f$. This turns out to be the configuration in which the object and image are as close together as they can possibly get (i.e., a distance $4f$ apart; see Problem 5.6). Table 5.3 summarizes a number of image configurations resulting from the juxtaposition of a thin lens and a real object. Figure 5.26 illustrates the behavior pictorially. Observe that as the object approaches the lens, the real image moves away from it.

Table 5.2 Meanings associated with the signs of various thin lens and spherical interface parameters.

Quantity	Sign +	Sign −
s_o	Real object	Virtual object
s_i	Real image	Virtual image
f	Converging lens	Diverging lens
y_o	Erect object	Inverted object
y_i	Erect image	Inverted image
M_T	Erect image	Inverted image

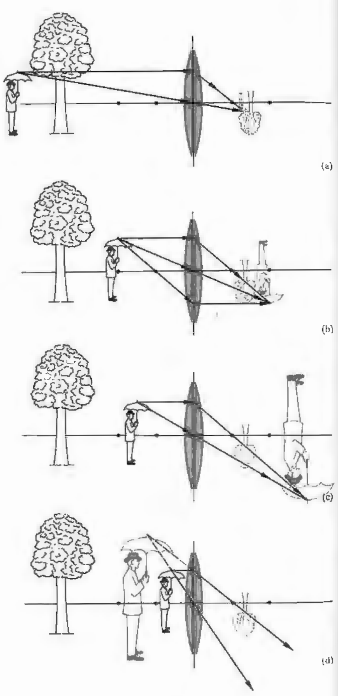


Figure 5.26 The image-forming behavior of a thin positive lens.

Table 5.3 Images of real objects formed by thin lenses.

Convex

Object: Location	Image: Type	Image: Location	Image: Orientation	Image: Relative size
$\infty > s_o > 2f$	Real	$f < s_i < 2f$	Inverted	Minified
$s_o = 2f$	Real	$s_i = 2f$	Inverted	Same size
$f < s_o < 2f$	Real	$\infty > s_i > 2f$	Inverted	Magnified
$s_o = f$		$\pm\infty$		
$s_o < f$	Virtual	$\lvert s_i \rvert > s_o$	Erect	Magnified

Concave

Object: Location	Image: Type	Image: Location	Image: Orientation	Image: Relative size
Anywhere	Virtual	$\lvert s_i \rvert < \lvert f \rvert$, $s_o > \lvert s_i \rvert$	Erect	Minified

Presumably, the image of a three-dimensional object will itself occupy a three-dimensional region of space. The optical system can apparently affect both the transverse and longitudinal dimensions of the image. The *longitudinal magnification*, M_L, which relates to the axial direction, is defined as

$$M_L = \frac{dx_i}{dx_o}. \tag{5.27}$$

This is the ratio of an infinitesimal axial length in the region of the image to the corresponding length in the region of the object. Differentiating Eq. (5.23) leads to

$$M_L = -\frac{f^2}{x_o^2} = -M_T^2 \tag{5.28}$$

for a thin lens in a single medium (Fig. 5.27). Evidently, $M_L < 0$, which implies that a positive dx_o corresponds to a negative dx_i and vice versa. In other words, a finger pointing toward the lens is imaged pointing away from it (Fig. 5.28).

Form the image of a window on a sheet of paper, using a simple convex lens. Assuming a lovely arboreal scene, image the distant trees on the screen. Now move the paper *away* from the lens, so that it intersects a different region of the image space. The trees will fade while the nearby window itself comes into view.

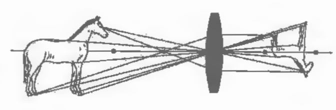


Figure 5.27 The transverse magnification is different from the longitudinal magnification.

iv) Thin-Lens Combinations

Our purpose here is not to become proficient in the subtle intricacies of modern lens design, but rather to begin to appreciate, utilize, and adapt those systems already available.

In constructing a new optical system, one generally begins by sketching out a rough arrangement using the quickest approximate calculations. Refinements are then added as the designer goes on to the prodigious and more exact ray-tracing techniques. Nowadays these computations are most often carried out by electronic digital computers. Even so, the simple thin-lens concept provides a highly useful basis for preliminary calculations in a broad range of situations.

No lens is actually a thin lens in the strict sense of having a thickness that approaches zero. Yet many simple lenses, for all practical purposes, function in a fashion equivalent to that of a thin lens. Almost all

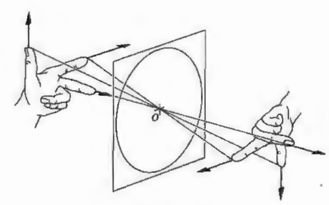


Figure 5.28 Image orientation for a thin lens.

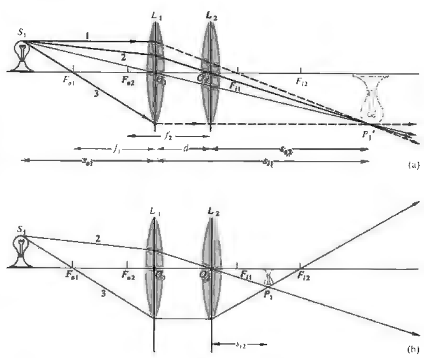


Figure 5.29 Two thin lenses separated by a distance smaller than either focal length.

spectacle lenses, which, by the way, have been used at least since the thirteenth century, are in this category. When the radii of curvature are large and the lens diameter is small, the thickness will usually be small as well. A lens of this sort would generally have a large focal length, compared with which the thickness would be quite small; many early telescope objectives fit that description perfectly.

We will now derive some expressions for parameters associated with thin-lens combinations. The approach here will be fairly simple, leaving the more elaborate traditional treatment for those tenacious enough to pursue the matter into the next chapter.

Suppose we have two thin positive lenses L_1 and L_2 separated by a distance d, which is smaller than either focal length, as in Fig. 5.29. The resulting image can be located graphically as follows. If we overlook L_2 for a moment, the image formed exclusively by L_1 is constructed with rays 1 and 3. As usual, these pass through the lens object and image foci, F_{o1} and F_{i1}, respectively. The object is in a normal plane, so that two rays determine its top, and a perpendicular to the optical axis finds its bottom. Ray 2 is then constructed running backward from P_1' through O_2. Insertion of L_2 has no effect on ray 2, whereas ray 3 is refracted through the image focus F_{i2} of L_2. The intersection of rays 2 and 3 fixes the image, which in this particular case is real, minified, and inverted.

A similar pair of lenses is illustrated in Fig. 5.30, in which the separation has been increased. Once again rays 1 and 3 through F_{i1} and F_{o1} fix the position of the intermediate image generated by L_1 alone. As before, ray 2 is drawn backward from O_2 to P_1' to S_1. The intersection of rays 2 and 3, as the latter is refracted through F_{i2}, locates the final image. This time it is real and erect. Notice that if the focal length of L_2 is increased with all else constant, the size of the image increases as well.

Analytically, we have for L_1

$$\frac{1}{s_{i1}} = \frac{1}{f_1} - \frac{1}{s_{o1}} \tag{5.29}$$

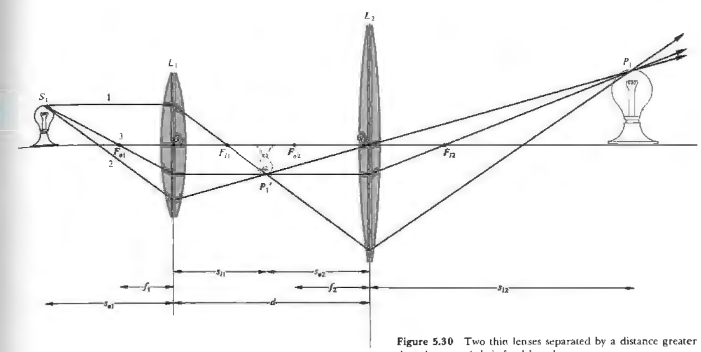


Figure 5.30 Two thin lenses separated by a distance greater than the sum of their focal lengths.

or

$$s_{i1} = \frac{s_{o1} f_1}{s_{o1} - f_1}. \tag{5.30}$$

This is positive, and the intermediate image is to the right of L_1, when $s_{o1} > f_1$ and $f_1 > 0$. For L_2

$$s_{o2} = d - s_{i1}, \tag{5.31}$$

and if $d > s_{i1}$, the object for L_2 is real (as in Fig. 5.30), whereas if $d < s_{i1}$, it is virtual ($s_{o2} < 0$, as in Fig. 5.29). In the former instance the rays approaching L_2 are diverging from P_1', whereas in the latter they are converging toward it. Furthermore,

$$\frac{1}{s_{i2}} = \frac{1}{f_2} - \frac{1}{s_{o2}}$$

or

$$s_{i2} = \frac{s_{o2} f_2}{s_{o2} - f_2}.$$

Using Eq. (5.31), we obtain

$$s_{i2} = \frac{(d - s_{i1}) f_2}{(d - s_{i1} - f_2)}. \tag{5.32}$$

In this same way we could compute the response of any number of thin lenses. It will often be convenient to have a single expression, at least when dealing with only two lenses, so substituting for s_{i1} from Eq. (5.29), we get

$$s_{i2} = \frac{f_2 d - f_2 s_{o1} f_1/(s_{o1} - f_1)}{d - f_2 - s_{o1} f_1/(s_{o1} - f_1)}. \tag{5.33}$$

Here s_{o1} and s_{i2} are the object and image distances, respectively, of the compound lens. As an example, let's compute the image distance associated with an object placed 50 cm from the first of two positive lenses. These in turn are separated by 20 cm and have focal lengths of 30 cm and 50 cm, respectively. By direct substitution (5.33)

$$s_{i2} = \frac{50(20) - 50(50)(30)/(50-30)}{20 - 50 - 50(30)/(50-30)} = 26.2\text{ cm},$$

and the image is real. Inasmuch as L_2 "magnifies" the intermediate image formed by L_1, the total transverse magnification of the compound lens is the product of the individual magnifications, that is,

$$M_T = M_{T1}M_{T2}.$$

It is left as Problem (5.25) to show that

$$M_T = \frac{f_1 s_{i2}}{d(s_{o1} - f_1) - s_{o1}f_1}. \qquad (5.34)$$

In the above example

$$M_T = \frac{30(26.2)}{20(50-30) - 50(30)} = -0.72,$$

and just as we should have guessed from Fig. 5.29, the image is minified and inverted.

The distance from the last surface of an optical system to the second focal point of that system as a whole is known as the *back focal length*, or b.f.l. Likewise, the distance from the vertex of the first surface to the first or object focus is the *front focal length*, or f.f.l. Consequently if we let $s_{i2} \to \infty$, s_{o2} approaches f_2, which combined with Eq. (5.31) tells us that $s_{i1} \to d - f_2$. Hence from Eq. (5.29)

$$\left.\frac{1}{s_{o1}}\right|_{s_{i2}=\infty} = \frac{1}{f_1} - \frac{1}{(d-f_2)} = \frac{d-(f_1+f_2)}{f_1(d-f_2)}.$$

But this special value of s_{o1} is the f.f.l.:

$$\text{f.f.l.} = \frac{f_1(d-f_2)}{d-(f_1+f_2)}. \qquad (5.35)$$

In the same way, letting $s_{o1} \to \infty$ in Eq. (5.33), $(s_{o1} - f_1) \to s_{o1}$, and since s_{i2} is then the b.f.l., we have

$$\text{b.f.l.} = \frac{f_2(d-f_1)}{d-(f_1+f_2)}. \qquad (5.36)$$

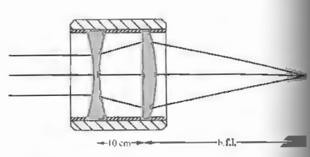
To see how this works numerically, let's find both the b.f.l. and f.f.l. for the thin-lens system in Fig. 5.31(a), where $f_1 = -30$ cm and $f_2 = +20$ cm. Then

$$\text{b.f.l.} = \frac{20[10-(-30)]}{10-(-30+20)} = 40\text{ cm},$$

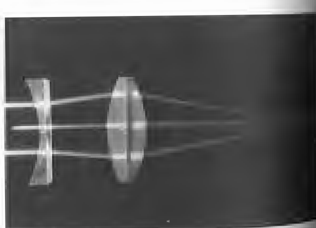
and similarly f.f.l. = 15 cm. Incidentally, notice th[illegible] $d = f_1 + f_2$, plane waves entering the compound [illegible] from either side will emerge as plane waves (Probl[illegible] 5.27), as in telescopic systems.

Observe that if $d \to 0$, that is, if the lenses are br[illegible] into contact, as in the case of some achromatic dou[illegible]

$$\text{b.f.l.} = \text{f.f.l.} = \frac{f_2 f_1}{f_2 + f_1}. \qquad (5.3[illegible])$$



(a)



(b)

Figure 5.31 A positive and negative thin-lens combination. [illegible] by E.H.)

The resultant thin lens has an *effective focal length, f*, such that

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2}. \qquad (5.38)$$

This implies that if there are N such lenses in contact,

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2} + \cdots + \frac{1}{f_N}. \qquad (5.39)$$

Many of these conclusions can be verified, at least qualitatively, with a few simple lenses. Figure 5.29 is quite easy to duplicate, and the procedure should be self-evident, whereas Fig. 5.30 requires a bit more care. First determine the focal lengths of the two lenses by [illegible]ing a distant source. Then hold one of the lenses [illegible] at a fixed distance *slightly greater than its focal length* [illegible] the plane of observation (i.e., a piece of white paper). Now comes the maneuver that requires some effort if you don't have an optical bench. Move the [illegible]ond lens (L_1) toward the source, keeping it reasonably centered. Without any attempts to block out light entering L_2 directly, you will probably see a blurred [illegible] of your hand holding L_1. Position the lenses so [illegible] the region on the screen corresponding to L_1 is as [illegible]ssible. The scene spread across L_1 (i.e., its [illegible] the image) will become clear and erect, as [illegible] n Fig. [illegible]

5.3 STOPS

5.3.1 Aperture and Field Stops

[illegible]ically finite nature of all lenses demands that [illegible] only a fraction of the energy emitted by a [illegible]. The physical limitation presented by the [illegible] of a simple lens therefore determines which [illegible] enter the system to form an image. In that [illegible] the unobstructed or *clear diameter* of the lens [illegible] as an aperture into which energy flows. Any [illegible], be it the rim of a lens or a separate diaphragm, [illegible]ines the amount of light reaching the image [illegible] known [illegible] the **aperture stop**, abbreviated as A.S. The [illegible] djustab[illegible] diaphragm that is usually located behind

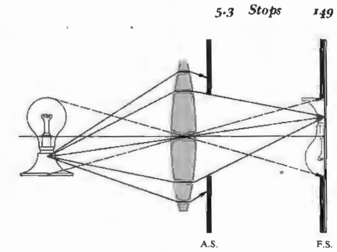


Figure 5.32 Aperture stop and field stop.

the first few elements of a compound camera lens is just such an aperture stop. Evidently it determines the light-gathering capability of the lens as a whole. As shown in Fig. 5.32, highly oblique rays can still enter a system of this sort. Usually, however, they are deliberately restricted in order to control the quality of the image. The element limiting the size or angular breadth of the object that can be imaged by the system is called the **field stop** or F.S.—it determines the field of view of the instrument. In a camera, the edge of the film itself bounds the image plane and serves as the field stop. Thus, while (Fig. 5.32) the aperture stop controls the number of rays from an object point reaching the conjugate image point, it is the field stop that will or will not obstruct those rays *in toto*. Neither the very top nor the bottom of the object in Fig. 5.32 passes the field stop. Opening the circular aperture stop would cause the system to accept a larger energy cone and in so doing increase the irradiance at each image point. In contrast, opening the field stop would allow the extremities of the object, which were previously blocked, to be imaged.

5.3.2 Entrance and Exit Pupils

Another concept, quite useful in determining whether or not a given ray will traverse the entire optical system, is the *pupil.* This is simply an *image of the aperture stop.* The **entrance pupil** of a system is the image of the aperture stop as seen from an axial point on the object through those elements preceding the stop. If there are no lenses between the object and the A.S., the latter itself serves as the entrance pupil. To illustrate the point, examine Fig. 5.33, which is a lens with a *rear aperture stop.* The image of the aperture stop in L is virtual (see Table 5.3) and magnified. It can be located by sending a few rays out from the edges of the A.S. in the usual way. In contrast, the **exit pupil** is the image of the A.S. as seen from an axial point on the image plane through the interposed lenses, if there are any. In Fig. 5.33 there are no such lenses, so the aperture stop itself serves as the exit pupil. Notice that all of this just means that the cone of light actually entering the optical system is determined by the entrance pupil, whereas the cone leaving it is controlled by the exit pupil. No rays from the source point proceeding outside of either cone will make it to the image plane.

If you wanted to use a telescope or a monocular as a camera lens, you might attach an external *front aperture stop* to control the amount of incoming light for exposure purposes. Figure 5.34 represents a similar arrangement in which the entrance and exit pupil locations should be self-evident. The last two diagrams included a ray labeled the *chief ray.* It is defined to be *any ray from an off-axis object point that passes through the center of the aperture stop. The chief ray enters the optical system along a line directed toward the midpoint of the entrance pupil,* E_{np}, *and leaves the system along a line passing through the center of the exit pupil,* E_{xp}. The chief ray, associated with a conical bundle of rays from a point on the object, effectively behaves as the central ray of the bundle and is representative of it. Chief rays are of particular importance when the aberrations of a lens design are being corrected.

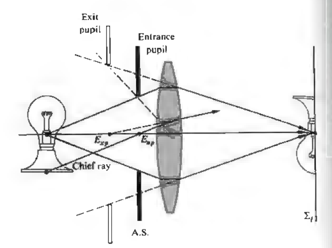


Figure 5.34 A front aperture stop.

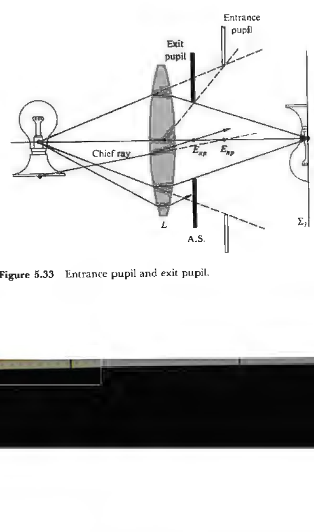


Figure 5.33 Entrance pupil and exit pupil.

Figure 5.35 depicts a somewhat more involved arrangement. The two rays shown are those that are usually traced through an optical system. One is the chief ray from a point on the periphery of the object that is to be accommodated by the system. The other is called a *marginal ray,* since it goes from the axial object point to the rim or margin of the entrance pupil (or aperture stop).

In a situation where it is not clear which element is the actual aperture stop, each component of the system must be imaged by the remaining elements to its left. *The image that subtends the smallest ongle at the axial object point is the entrance pupil.* The element whose image is the entrance pupil is then the aperture stop of the system for that object point. Problem 5.30 deals with just this kind of calculation.

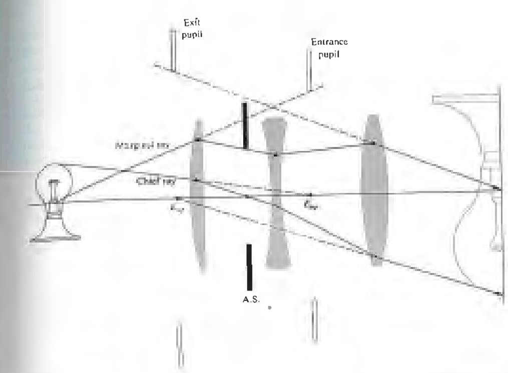


Figure 5.35 Pupils and stops for a three-lens system.

Notice how the cone of rays, in Fig. 5.36, that can reach the image plane becomes narrower as the object point moves off-axis. The effective aperture stop, which for the axial bundle of rays was the rim of L_1, has been markedly reduced for the off-axis bundle. The result is a gradual fading out of the image at points near its periphery, a process known as *vignetting.*

The locations and sizes of the pupils of an optical system are of considerable practical importance. In

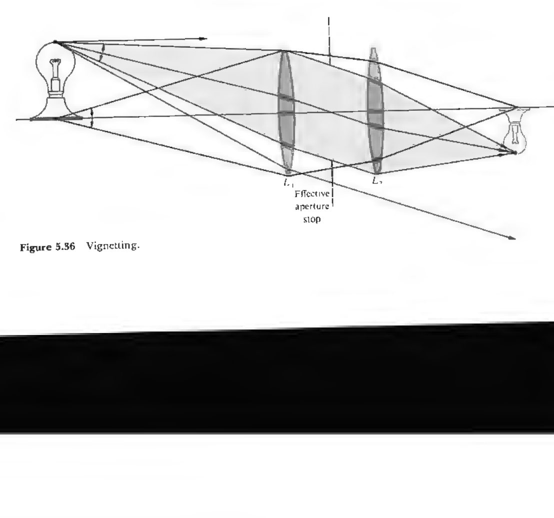


Figure 5.36 Vignetting.

visual instruments, the observer's eye is positioned at the center of the exit pupil. The pupil of the eye itself will vary from 2 mm to about 8 mm, depending on the general illumination level. Thus a telescope or binocular designed primarily for evening use might have an exit pupil of at least 8 mm (you may have heard the term *night glasses*—they were quite popular on roofs during the Second World War). In contrast, a daylight version will suffice with an exit pupil of 3 or 4 mm. The larger the exit pupil, the easier it will be to align your eye properly with the instrument. Obviously a telescopic sight for a high-powered rifle should have a large exit pupil located far enough behind the scope so as to avoid injury from recoil.

5.3.3 Relative Aperture and *f*-Number

Suppose we wish to collect the light from an extended source and form an image of it using a lens (or mirror). The amount of energy gathered by the lens (or mirror) from some small region of a distant source will be directly proportional to the area of the lens or, more generally, to the area of the entrance pupil. A large *clear aperture* will intersect a large cone of rays. Obviously, if the source were a laser with a very narrow beam, this would not necessarily be true. If we neglect losses due to reflections, absorption, and so forth, the incoming energy will be spread across a corresponding region of the image. Thus the energy per unit area per unit time (i.e., the flux density or irradiance) will be inversely proportional to the image area. The entrance pupil area, if circular, varies as the square of its radius and is therefore proportional to the square of its diameter D. Furthermore, the image area will vary as the square of its lateral dimension, which in turn [Eqs. (5.24) and (5.26)] is proportional to f^2. (Keep in mind that we are talking about an extended object rather than a point source. In the latter case, the image would be confined to a very small area independent of f.) Thus the flux density at the image plane varies as $(D/f)^2$. The ratio D/f is known as the *relative aperture*, and its inverse is said to be the **f-number**, or $f/\#$, that is,

$$f/\# \equiv \frac{f}{D}, \tag{5.40}$$

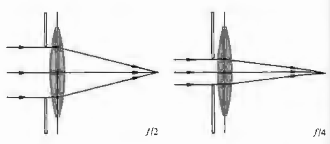


Figure 5.37 Stopping down a lens to change the *f-number*.

where $f/\#$ should be understood as a single symbol. For example, a lens with a 25-mm aperture and a 50-mm focal length has an *f-number* of 2, which is usually designated $f/2$. Figure 5.37 illustrates the point by showing a thin lens behind a variable iris diaphragm operating at either $f/2$ or $f/4$. A smaller *f-number* clearly permits more light to reach the image plane.

Camera lenses are usually specified by their focal lengths and largest possible apertures; for example, you might see "50 mm, $f/1.4$" on the barrel of a lens. Since the photographic exposure time is proportional to the square of the *f-number* the latter is sometimes spoken of as the *speed* of the lens. An $f/1.4$ lens is said to be twice as fast as an $f/2$ lens. Usually lens diaphragms have *f-number* markings of 1, 1.4, 2, 2.8, 4, 5.6, 8, 11, 16, 22, and so on. The largest relative aperture in this case corresponds to $f/1$, and that's a fast lens—$f/2$ is more typical. Each consecutive diaphragm setting increases the *f-number* by a multiplicative factor of $\sqrt{2}$ (numerically rounded off). This corresponds to a decrease in relative aperture by a multiplicative factor of $1/\sqrt{2}$ and therefore a decrease in flux density by one half. Thus, the same amount of light will reach the film whether the camera is set for $f/1.4$ at 1/500th of a second, $f/2$ at 1/250th of a second, or $f/2.8$ at 1/125th of a second.

The largest refracting telescope in the world, located at the Yerkes Observatory of the University of Chicago, has a 40-inch diameter lens with a focal length of 63 feet and therefore an *f-number* of 18.9. The entrance pupil and focal length of a mirror will, in exactly the same way, determine its *f-number*. Accordingly, the 200-inch diameter mirror of the Mount Palomar telescope, with a prime focal length of 666 inches, has an *f-number* of 3.33.

For precise work, in which reflection and absorption losses in the lens itself must be taken into consideration, the *T-number* is highly useful. In effect, it is a modified (increased) *f-number* that a given real lens would actually have to have were it to transmit an amount of light corresponding to a particular value of f/D.

5.4 MIRRORS

Mirror systems are being used in increasingly extensive applications, particularly in the x-ray, ultraviolet, and infrared regions of the spectrum. Although it is relatively simple to construct a reflecting device that will perform satisfactorily across a broad-frequency bandwidth, the same cannot be said of refracting systems. For example, a silicon or germanium lens designed for the infrared will be completely opaque in the visible (Fig. 3.29). As we will see later, when we consider their aberrations, mirrors have other attributes that contribute to their usefulness.

A mirror might simply be a piece of black glass or a finely polished metal surface. In the past mirrors were usually made by coating glass with silver, the latter beiog chosen because of its high efficiency in the UV and IR (see Fig. 4.42), and the former because of its rigidity. In recent times, vacuum-evaporated coatings of aluminum on highly polished substrates have become the accepted standard for quality mirrors. Protective coatings of silicon monoxide or magnesium fluoride are often layered over the aluminum as well. In special applications (e.g., in lasers), where even the small losses due to metal surfaces cannot be tolerated, mirrors formed of multilayered dielectric films (see Section 9.9) are indispensable.

A whole new generation of lightweight precision mirrors is being developed for use in large-scale orbiting telescopes—the technology is by no means static.

5.4.1 Planar Mirrors

As with all mirror configurations, those that are planar can be either front- or back-surfaced. The latter is the kind most commonly found in everyday use because it allows the metallic reflecting layer to be completely protected behind glass. In contrast, the majority of mirrors designed for more critical technical usage are front-surfaced (Fig. 5.38).

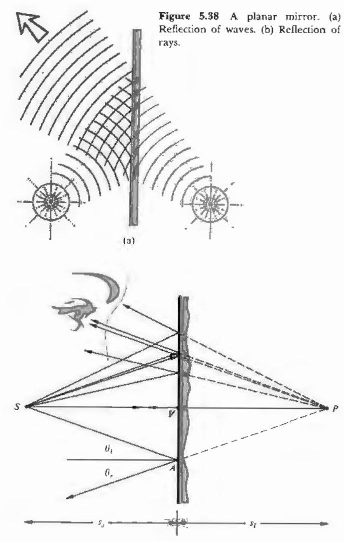


Figure 5.38 A planar mirror. (a) Reflection of waves. (b) Reflection of rays.

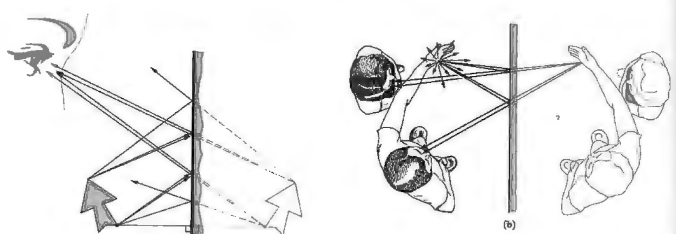


Figure 5.39 (a) The image of an extended object in a planar mirror. (b) Images in a planar mirror.

From Sections 4.2.2 and 4.2.3, it's a rather easy matter to determine the image characteristics of a planar mirror. Examining the point source and mirror arrangement of Fig. 5.38, we can quickly show that $|s_o| = |s_i|$, that is, the image *P* and object *S* are equidistant from the surface. To wit, $\theta_i = \theta_r$, from the law of reflection; $\theta_i + \theta_r$ is the exterior angle of triangle *SPA* and is therefore equal to the sum of the alternate interior angles, $\measuredangle VSA + \measuredangle VPA$. But $\measuredangle VSA = \theta_i$, and therefore $\measuredangle VSA = \measuredangle VPA$. This makes triangles *VAS* and *VPA* congruent, in which case $|s_o| = |s_i|$. (Go back and take another look at Problem 4.3 and Fig. 4.50 for the wave picture of the reflection.)

We are now faced with the problem of determining a sign convention applicable to mirrors. Whatever we choose, and you should certainly realize that there is a choice, we need only be faithful unto it for all to be well. One obvious dilemma with respect to the convention for lenses is that now the virtual image is to the right of the interface. The observer sees *P* to be positioned behind the mirror, because the eye (or camera) cannot perceive the actual reflection; it merely interpolates the rays backward along straight lines. The rays from *P* are diverging, and no light can be cast upon a screen located at *P*—the image is certainly virtual. Clearly, it is a matter of taste whether s_i should be defined as positive or negative in this instance. Since we rather like the idea of virtual object and image distances being negative, we shall define *s_o and s_i as negative when they lie to the right of the vertex V*. This will have the added benefit of yielding a mirror formula identical to the Gaussian lens equation (5.17). Evidently, the same definition of the transverse magnification

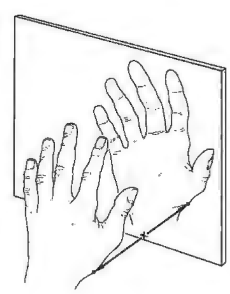
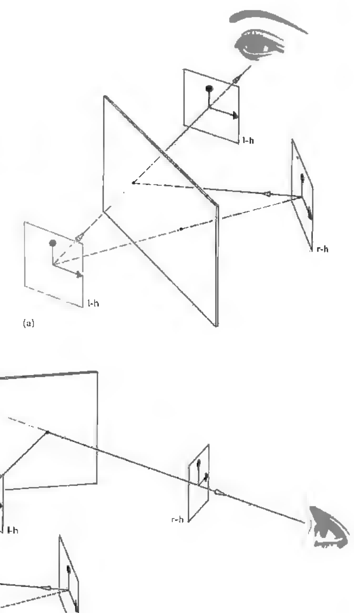


Figure 5.40 Mirror images—inversion.

(5.24) holds, where now, as before, $M_T = +1$ indicates a *life-size*, virtual, erect image.

Each point of the extended object in Fig. 5.39, a perpendicular distance s_i from the mirror, is imaged that same distance behind the mirror. In this way, the entire image is built up point by point. This is much different from the way a lens locates an image. The object in Fig. 5.28 was a left hand, and the image formed by the lens was also a left hand; to be sure, it might have been distorted ($M_L \neq M_T$), but it was still a left hand. The only evident change was a 180° rotation about the optical axis—an effect known as *reversion*. Contrarily, the mirror image of the left hand, determined by dropping perpendiculars from each point, is a right hand (Fig. 5.40). Such an image is sometimes said to be *perverted*. In deference to the more usual lay connotation of the word, its use in optics is happily waning. The process that converts a right-handed coordinate system in the object space into a left-handed one in the image space is known as *inversion*. Systems with



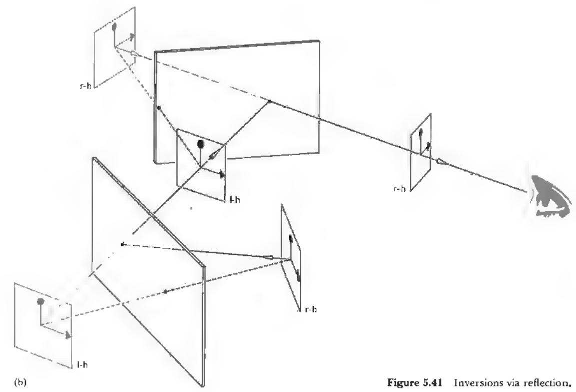


Figure 5.41 Inversions via reflection.

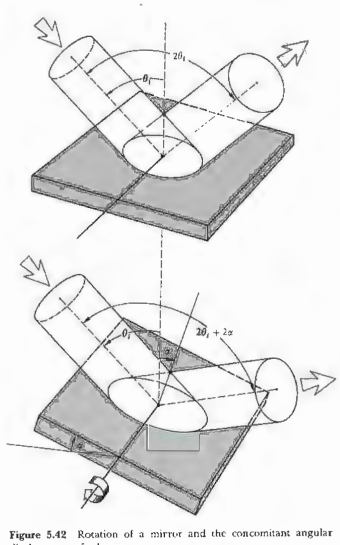


Figure 5.42 Rotation of a mirror and the concomitant angular displacement of a beam.

more than one planar mirror can be used to produce either an odd or even number of inversions. In the latter case a right-handed (r-h) object will generate a right-handed image (Fig. 5.41), whereas in the former instance, the image will be left-handed (l-h).

There are a number of practical devices that utilize rotating planar mirror systems, for example, choppers, beam deflectors, and image rotators. Mirrors are frequently used to amplify and measure the slight rotations of certain laboratory apparatus (galvanometers, torsion pendulums, current balances, etc.). As Fig. 5.42 shows, if the mirror rotates through an angle α, the reflected beam or image will move through an angle of 2α.

5.4.2 Aspherical Mirrors

Curved mirrors that form images very much like those of lenses or curved refracting surfaces have been known since the time of the ancient Greeks. Euclid, who is presumed to have authored the book entitled *Catoptrics*, discusses in it both concave and convex mirrors.* Fortunately, we developed the conceptual basis for designing such mirrors when we spoke earlier about Fermat's principle as applied to imagery in refracting systems. Suppose then, that we would like to determine the configuration a mirror must have in order that an incident plane wave be reformed upon reflection into a converging spherical wave (Fig. 5.43). If the plane wave is ultimately to converge on some point F, the optical path lengths for all rays must be equal; accordingly, for arbitrary points A_1 and A_2

$$\text{OPL} = \overline{W_1A_1} + \overline{A_1F} = \overline{W_2A_2} + \overline{A_2F}. \quad (5.41)$$

Since the plane Σ is parallel to the incident wavefront,

$$\overline{W_1A_1} + \overline{A_1D_1} = \overline{W_2A_2} + \overline{A_2D_2}. \quad (5.42)$$

Equation (5.41) will therefore be satisfied for a surface for which $\overline{A_1F} = \overline{A_1D_1}$ and $\overline{A_2F} = \overline{A_2D_2}$ or, more generally, one for which $\overline{AF} = \overline{AD}$ for any point A on the mirror. This same condition was discussed in Section 5.2.1, in which we found $\overline{AF} = e(\overline{AD})$, where e was the eccentricity of a conic section. Here the second medium is identical to the first, $n_t = n_i$, and $e = n_{ti} = 1$; in other words, the surface is a paraboloid with F as its focus and Σ as its directrix. The rays could equally well be reversed (i.e., a point source at the focus of a paraboloid would result in the emission of plane waves from the system. The paraboloidal configuration ranges in present-day applications from flashlight and auto headlight reflectors to giant radiotelescope an-

* *Dioptrics* denotes the optics of refracting elements, whereas ... denotes the optics of reflecting surfaces.

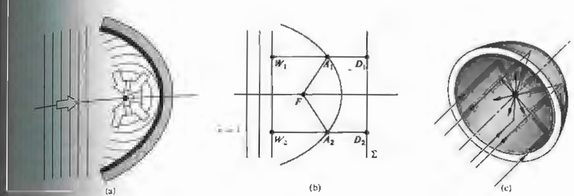


Figure 5.43 A paraboloidal mirror.

Figure 5.44 A paraboloidal radio antenna. (Photo courtesy of the ...lian News and Information Bureau.)

(Fig. 5.44), from microwave horns and acoustical dishes to optical telescope mirrors and moon-based communications antennas. The convex paraboloidal mirror is also possible but is less widely in use. Applying what we already know, it should be evident from Fig. 5.45 that an incident parallel bundle of rays will form a virtual image at F when the mirror is convex and a real image when it is concave.

There are several other aspherical mirrors of some interest, namely, the ellipsoid ($e < 1$) and hyperboloid ($e > 1$). Both produce perfect imagery between a pair of conjugate axial points corresponding to their two foci (Fig. 5.46). As we shall see imminently, the Cassegrainian and Gregorian telescope configurations utilize convex secondary mirrors that are hyperboloidal and ellipsoidal, respectively.

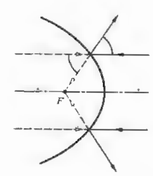


Figure 5.45 Real and virtual images for a paraboloidal mirror.

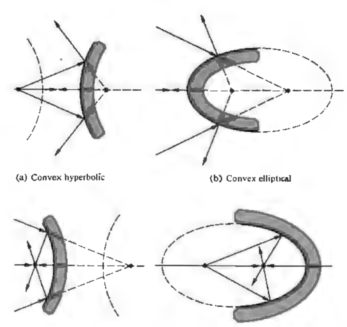


Figure 5.46 Hyperbolic and elliptical mirrors.

It should be noted that all these devices are readily available commercially. In fact, one can purchase *off-axis elements*, in addition to the more common centered systems. Thus, in Fig. 5.47 the focused beam can be further processed without obstructing the mirror.

Figure 5.47 An off-axis parabolic mirror element.

Incidentally, this geometry also obtains in large mi[illegible] wave horn antennas, which have a significant [illegible] in modern communications.

5.4.3 Spherical Mirrors

We are again reminded of the fact that precise as[illegible] surfaces are considerably more difficult to fabric[illegible] are spherical ones. The high costs are commensu[illegible] with the increased time and meticulous effort req[illegible] Motivated by these practical considerations, we [illegible] more turn to the spherical configuration to dete[illegible] the circumstances under which it might perfo[illegible] adequately.

i) The Paraxial Region

The well-known equation for the circular cross-sec[illegible] of a sphere [Fig. 5.48(a)] is

$$y^2 + (x - R)^2 = R^2,$$

where the center C is shifted from the origin O by [illegible] radius R. After writing this as

$$y^2 - 2Rx + x^2 = 0,$$

we can solve for x:

$$x = R \pm (R^2 - y^2)^{1/2}. \qquad (5.44)$$

Let's just concern ourselves with values of x less than R, that is, we will study a hemisphere, open on the [illegible] corresponding to the minus sign in Eq. (5.44). Aft[illegible] expansion in a binomial series, x takes the form

$$x = \frac{y^2}{2R} + \frac{1y^4}{2^2 2! R^3} + \frac{1 \cdot 3y^6}{2^3 3! R^5} + \cdots, \qquad (5.4[illegible])$$

This expression becomes quite meaningful as soo[illegible] we realize that the standard equation for a parab[illegible] with its vertex at the origin and its focus a distanc[illegible] the right [Fig. 5.48(b)] is simply

$$y^2 = 4fx.$$

Thus by comparing these two formulas, we se[illegible] 4f = 2R (i.e., if $f = R/2$), the first contributio[illegible] in the series can be thought of as parabolic, and the r[illegible]

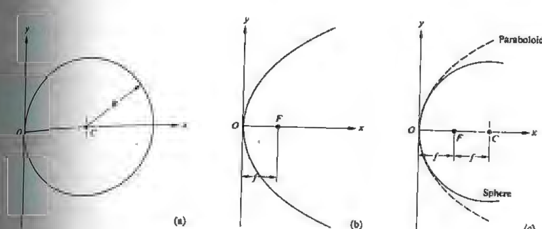


Figure 5.48 Comparison of spherical and paraboloidal mirrors.

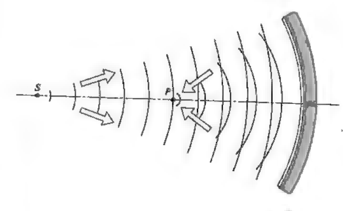
terms represent the deviation. If that deviation is Δx, then

$$\Delta x = \frac{y^4}{8R^3} + \frac{y^6}{16R^5} + \cdots. \qquad (5.47)$$

[illegible]ly this difference will be appreciable only when [illegible] relatively large [Fig. 5.48(c)] in comparison to R. *In the paraxial region, that is, in the immediate vicinity of the [illegible] axis, these two configurations will be essentially indistinguishable.* Thus if we talk about the paraxial theory of spherical mirrors as a first approximation, we can [illegible] embrace the conclusions drawn from our study of the stigmatic imagery of paraboloids. In actual use, however, y will not be so limited, and aberrations will [illegible]. Moreover, aspherical surfaces produce perfect images only for pairs of axial points—they too will suffer aberrations.

[illegible] Mirror Formula

The paraxial equation that relates conjugate object and image points to the physical parameters of a spherical [illegible] can be derived rather easily with the help of Fig. 5.49. To that end, observe that since $\theta_i = \theta_r$, the $\measuredangle SAP$ is bisected by $\overline{CA}$, which therefore divides the side $\overline{SP}$ of triangle SAP into segments proportional to the



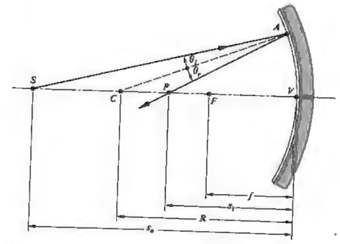


Figure 5.49 A concave spherical mirror.

remaining two sides, that is,

$$\frac{\overline{SC}}{\overline{SA}} = \frac{\overline{CP}}{\overline{PA}}. \qquad (5.48)$$

Furthermore,

$$\overline{SC} = s_o - |R| \quad \text{and} \quad \overline{CP} = |R| - s_i,$$

where s_o and s_i are on the left and therefore positive. If we use the same sign convention for R as we did when we dealt with refraction, it will be negative here, because C is to the left of V (i.e., the surface is concave). Thus $|R| = -R$ and

$$\overline{SC} = s_o + R \quad \text{and} \quad \overline{CP} = -(s_i + R).$$

In the paraxial region $\overline{SA} \approx s_o$, $\overline{PA} \approx s_i$, and so Eq. (5.48) becomes

$$\frac{s_o + R}{s_o} = -\frac{s_i + R}{s_i}$$

or

$$\frac{1}{s_o} + \frac{1}{s_i} = -\frac{2}{R}, \qquad (5.49)$$

which is often referred to as the **mirror formula**. It is equally applicable to concave ($R < 0$) and convex ($R > 0$) mirrors. The primary or object focus is again [illegible] by

$$\lim_{s_i \to \infty} s_o = f_o,$$

and the secondary or image focus corresponds to

$$\lim_{s_o \to \infty} s_i = f_i.$$

Consequently, from Eq. (5.49)

$$\frac{1}{f_o} + \frac{1}{\infty} = \frac{1}{\infty} + \frac{1}{f_i} = -\frac{2}{R},$$

to wit, $f_o = f_i = -R/2$, as we know from Fig. 5.45(c). Again, dropping the subscripts on the focal lengths, we have

$$\frac{1}{s_o} + \frac{1}{s_i} = \frac{1}{f}. \qquad (5.50)$$

Observe that f will be positive for concave mirrors ($R < 0$) and negative for convex mirrors ($R > 0$). In the latter instance the image is formed behind the mirror and is virtual (Fig. 5.50).

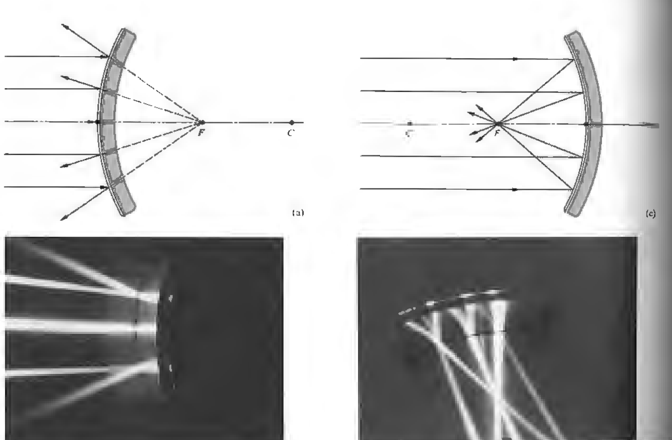


Figure 5.50 Focusing of rays via a spherical mirror. (Photos by E.H.)

iii) Finite Imagery

The remaining mirror properties are so similar to those of lenses and spherical refracting surfaces that we need only mention them briefly, without repeating the entire [illegible] development of each item. Within the restrictions of paraxial theory, any parallel off-axis bundle of rays will be focused to a point on the *focal plane* passing through F normal to the optical axis. Likewise, a finite planar object perpendicular to the optical axis will be imaged (to a first approximation) in a plane similarly [illegible]. Essentially we are saying that each object point [illegible] a corresponding image point in the plane. [illegible] certainly true for a plane mirror, but it only approximates the case for other configurations. To be sure, if a spherical mirror is appropriately restricted in its operation, the reflected waves arising from each emitted object point will closely approximate spherical waves. Under such circumstances good finite images of extended objects can be formed (Fig. 5.51). Just as each image point produced by a thin lens lies along a straight line through the optical center O, each image point for a spherical mirror will lie on a ray passing through both the center of curvature C and the object point. As with the thin lens (Fig. 5.24), the graphic location of the image is quite straightforward. Once more the top of the image is located at the intersection of two rays, one initially parallel to the axis and passing through F after reflection, and the other going straight through C (Fig. 5.52). The ray from any off-axis object point to the vertex forms equal angles with the optical axis on reflection and is therefore particularly convenient to construct as well. So too is the ray that first passes through the focus and after reflection emerges parallel to the axis.

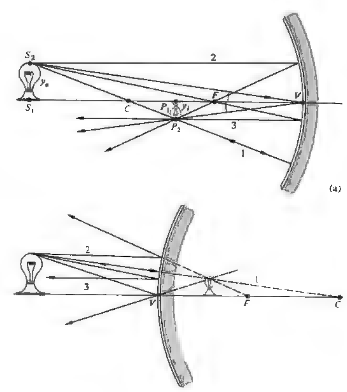


Figure 5.51 Finite imagery with spherical mirrors.

Notice that triangles S_1S_2V and P_1P_2V in Fig. 5.51(a) are similar, and hence their sides are proportional. Taking y_i to be negative, as we did before, since it is below the axis, we find that $y_i/y_o = -s_i/s_o$, which of

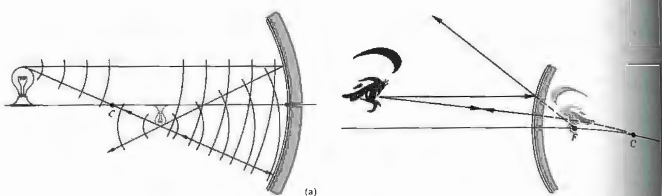


Figure 5.52 (a) Reflection from a concave mirror. (b) Reflection from a convex mirror.

course is equal to M_T, the *transverse magnification*, identical to that of the lens (5.25).

The only equation that contains information about the structure of the optical element (n, R, etc.) is that for f, and so, rather understandably, it differs for the thin lens and spherical mirror. The other functional expressions that relate s_o, s_i, and f or y_o, y_i, and M_T are, however, precisely the same. The only alteration in the previous sign convention appears in Table 5.4, where s_i on the left of V is now taken as positive. The striking similarity between the properties of a concave mirror and a convex lens on one hand and a convex mirror and a concave lens on the other are quite evident from a comparison of Tables 5.3 and 5.5, which are identical in all respects.

The properties summarized in Table 5.5 and depicted pictorially in Fig. 5.53 can easily be verified empirically. If you don't have a spherical mirror at hand, a fairly crude but functional one can be made by carefully

Table 5.4 Sign convention for spherical mirrors.

Quantity	Sign	
	+	−
s_o	Left of V, real object	Right of V, virtual object
s_i	Left of V, real image	Right of V, virtual image
f	Concave mirror	Convex mirror
R	C right of V, convex	C left of V, concave
y_o	Above axis, erect object	Below axis, inverted object
y_i	Above axis, erect image	Below axis, inverted image

Table 5.5 Images of real objects formed by spherical mirrors.

Concave				
Object	Image			
Location	Type	Location	Orientation	Relative size
$\infty > s_o > 2f$	Real	$f < s_i < 2f$	Inverted	Minified
$s_o = 2f$	Real	$s_i = 2f$	Inverted	Same size
$f < s_o < 2f$	Real	$\infty > s_i > 2f$	Inverted	Magnified
$s_o = f$		$\pm\infty$		
$s_o < f$	Virtual	$\lvert s_i \rvert > s_o$	Erect	Magnified
Convex				
Object	Image			
Location	Type	Location	Orientation	Relative size
Anywhere	Virtual	$\lvert s_i \rvert < \lvert f \rvert$, $s_o > \lvert s_i \rvert$	Erect	Minified

shaping aluminum foil over a spherical form, such as the end of a light bulb (in that particular case R [illegible] therefore f will be small). A rather nice quali[illegible] experiment involves examining the image of some [illegible] object formed by a short focal-length concave [illegible]. As you move it toward the mirror from beyond a [illegible]tance of $2f = R$, the image will gradually increase, [illegible] at $s_o = 2f$ it will appear inverted and life-size. Bring[illegible] it closer will cause the image to increase even [illegible] until it fills the entire mirror with an unrecogni[illegible] blur. As s_o becomes smaller, the now erect, magni[illegible] image will continue to decrease until the object fi[illegible] rests on the mirror, where the image is again life[illegible]

If you are not moved by all of this to jump up and make a mirror, you might try examining the image formed by a shiny spoon—either side will be interesting.

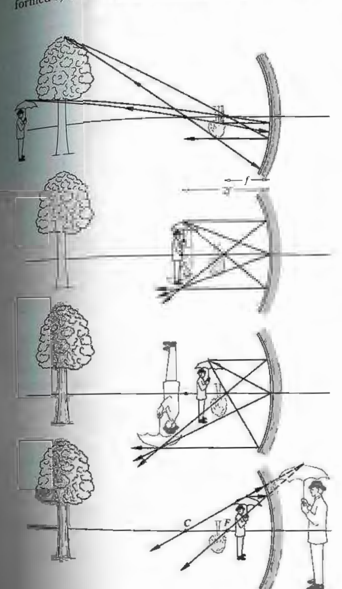


Figure 5.53 The image-forming behavior of a concave spherical mirror.

5.5 PRISMS

Prisms have many different roles in optics; there are prism combinations that serve as beam-splitters (see Section 4.3.4), polarizing devices (see Section 8.4.3), and even interferometers. Despite this diversity, the vast majority of applications make use of only one of two main prism functions. First, a prism can serve as a dispersive device, as it does in a variety of spectrum analyzers. That is to say, it is capable of separating, to some extent, the constituent frequency components in a polychromatic light beam. You might recall that the term *dispersion* was introduced earlier (Section 3.5.1) in connection with the frequency dependence of the index **of refraction, $n(\omega)$, for dielectrics. In fact, the prism provides a highly useful means of measuring $n(\omega)$ over a broad range of frequencies and for a wide variety of materials (including gases and liquids). Its second and more common function is to effect a change in the orientation of an image or in the direction of propagation of a beam. Prisms are incorporated in many optical instruments, often simply to fold the system into a** confined space. There are inversion prisms, reversion prisms, and prisms that deviate a beam without inversion or reversion—and all of this without dispersion.

5.5.1 Dispersing Prisms

Nowadays prisms come in a great variety of sizes and shapes and perform an equally great variety of functions (Fig. 5.54). Let's first consider the group known as **dispersing prisms. Typically, a ray entering a dispersing prism,** as in **Fig. 5.55, will emerge having been deflected from its original direction by an angle δ known** as the *angular deviation*. At the first refraction the ray is deviated through an angle $(\theta_{i1} - \theta_{t1})$, and at the second refraction it is further deflected through $(\theta_{t2} - \theta_{i2})$. The total deviation is then

$$\delta = (\theta_{i1} - \theta_{t1}) + (\theta_{t2} - \theta_{i2}).$$

Since the polygon $ABCD$ contains two right angles, $\measuredangle BCD$ must be the supplement of the *apex angle* α. As the exterior angle to triangle BCD, α is also the sum of the alternate interior angles, that is,

$$\alpha = \theta_{t1} + \theta_{i2}. \tag{5.51}$$

Thus

$$\delta = \theta_{i1} + \theta_{t2} - \alpha. \tag{5.52}$$

What we would like to do now is write δ as a function of both the angle of incidence for the ray (i.e., θ_{i1}) and the prism angle α; these presumably would be known. If the prism index is n and it is immersed in air ($n_a \approx 1$), it follows from Snell's law that

$$\theta_{t2} = \sin^{-1}(n \sin \theta_{i2}) = \sin^{-1}[n \sin(\alpha - \theta_{t1})].$$

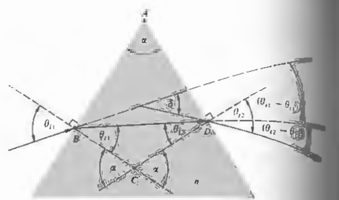


Figure 5.55 Geometry of a dispersing prism.

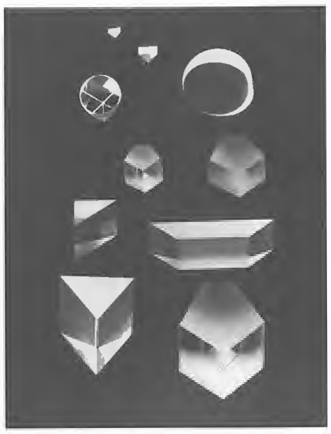


Figure 5.54 Prisms. (Photo courtesy Melles Griot.)

Upon expanding this expression, replacing [illegible] by $(1 - \sin^2 \theta_{i1})^{1/2}$, and using Snell's law we have

$$\theta_{t2} = \sin^{-1}[(\sin \alpha)(n^2 - \sin^2 \theta_{i1})^{1/2} - \sin \theta_{i1} \cos \alpha].$$

The deviation is then

$$\delta = \theta_{i1} + \sin^{-1}[(\sin \alpha)(n^2 - \sin^2 \theta_{i1})^{1/2} - \sin \theta_{i1} \cos \alpha] - \alpha. \tag{5.53}$$

Apparently δ increases with n, which is itself a [illegible] of frequency, so we might designate the devia[illegible] $\delta(\nu)$ or $\delta(\lambda)$. For most transparent dielectrics of [illegible] concern, $n(\lambda)$ decreases as the wavelength [illegible] across the visible [refer back to Fig. 3.27 for a plot of $n(\lambda)$ versus λ for various glasses]. Clearly, then, $\delta(\lambda)$ will be less for red light than it is for blue.

Missionary reports from Asia in the early 1600s in[illegible]cated that prisms were well known and highly valued in China because of their ability to generate color. A number of scientists of the era, particularly Marci, Grimaldi, and Boyle, had made some observations [illegible] prisms, but it remained for the great Sir Isaac Newton to perform the first definitive studies of dispersion [illegible] February 6, 1672, Newton presented a classic paper [illegible] the Royal Society entitled "A New Theory about Light and Colours." He had concluded that white light con-sisted of a mixture of various colors and that the [illegible] of refraction was color-dependent.

Returning to Eq. (5.53), it is evident that the de[illegible] suffered by a monochromatic beam on travers[illegible] [illegible] prism (i.e., n and α are fixed) is a function only [illegible] incident angle at the first face, θ_{i1}. A plot of the [illegible] of Eq. (5.53) as applied to a typical glass prism [illegible]n in Fig. 5.56. The smallest value of δ is known as [illegible] minimum deviation, δ_m, and it is of particular [illegible] for practical reasons. It can be determined [illegible]y by differentiating Eq. (5.53) and then setting [illegible]0, but a more indirect route will certainly be [illegible] Differentiating Eq. (5.52) and setting it equal to zero, we get

$$\frac{d\delta}{d\theta_{i1}} = 1 + \frac{d\theta_{t2}}{d\theta_{i1}} = 0$$

or [illegible]$/d\theta_{i1} = -1$. Taking the derivative of Snell's law at [illegible] interface, we get

$$\cos \theta_{i1}\, d\theta_{i1} = n \cos \theta_{t1}\, d\theta_{t1}$$

and

$$\cos \theta_{t2}\, d\theta_{t2} = n \cos \theta_{i2}\, d\theta_{i2}.$$

[illegible]e as well, on differentiating Eq. (5.51), that $d\theta_{t1} = $ [illegible], since $d\alpha = 0$. Dividing the last two equations and [illegible]tituting for the derivatives, we obtain

$$\frac{\cos \theta_{i1}}{\cos \theta_{t2}} = \frac{\cos \theta_{t1}}{\cos \theta_{i2}}.$$

Making use of Snell's law once again, we can rewrite this as

$$\frac{1 - \sin^2 \theta_{i1}}{1 - \sin^2 \theta_{t2}} = \frac{n^2 - \sin^2 \theta_{i1}}{n^2 - \sin^2 \theta_{t2}}.$$

The value of θ_{i1} for which this is true is the one for which $d\delta/d\theta_{i1} = 0$. Inasmuch as $n \neq 1$, it follows that

$$\theta_{i1} = \theta_{t2}$$

and therefore

$$\theta_{t1} = \theta_{i2}.$$

This means that the ray for which the deviation is a minimum traverses the prism symmetrically, that is, parallel to its base. Incidentally, there is a lovely argu-[illegible] why θ_{i1} must equal θ_{t2}, which is neither as [illegible]ical nor as tedious as the one we have evolved. [illegible] Suppose a ray undergoes a minimum deviation [illegible]θ_{t2}. Then if we reverse the ray, it will retrace

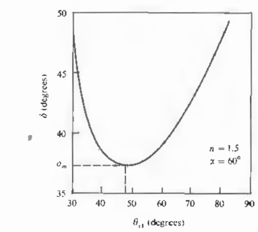


Figure 5.56 Deviation versus incident angle.

the same path, so δ must be unchanged (i.e., $\delta = \delta_m$). But this implies that there are two different incident angles for which the deviation is a minimum, and this we know is not true—ergo $\theta_{i1} = \theta_{t2}$.

In the case when $\delta = \delta_m$, it follows from Eqs. (5.51) and (5.52) that $\theta_{i1} = (\delta_m + \alpha)/2$ and $\theta_{t1} = \alpha/2$, whereupon Snell's law at the first interface leads to

$$n = \frac{\sin[(\delta_m + \alpha)/2]}{\sin \alpha/2}. \tag{5.54}$$

This equation forms the basis of one of the most accurate techniques for determining the refractive index of a transparent substance. Effectively, one fashions a prism out of the material in question, and then, measuring α and $\delta_m(\lambda)$, $n(\lambda)$ is computed employing Eq. (5.54) at each wavelength of interest. Hollow prisms whose sides are fabricated of plane-parallel glass can be filled with liquids or gases under high pressure; the glass plates will not result in any deviation of their own.

Figures 5.57 and 5.58 show two examples of *constant-deviation dispersing prisms*, which are important primarily in spectroscopy. The *Pellin–Broca* prism is probably the most common of the group. Albeit a single block of glass, it can be envisaged as consisting of two 30°–60°–90° prisms and one 45°–45°–90° prism. Suppose that in the position shown a single monochromatic ray of wavelength λ traverses the component prism *DAE* symmetrically, thereafter to be reflected at 45°

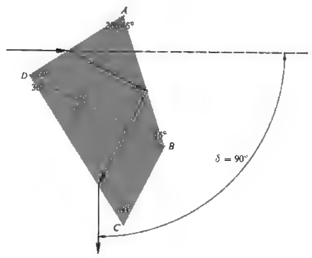


Figure 5.57 The Pellin–Broca prism.

from face AB. The ray will then traverse prism CDB symmetrically, having experienced a total deviation of 90°. The ray can be thought of as having passed through an ordinary 60° prism (DAE combined with CDB) at minimum deviation. All other wavelengths present in the beam will emerge at other angles. If the prism is now rotated slightly about an axis normal to the paper, the incoming beam will have a new incident angle. A different wavelength component, say λ_2, will now undergo a minimum deviation, which is again 90°—hence the name, *constant deviation*. With a prism of this sort, one can conveniently set up the light source and viewing system at a fixed angle (here 90°) and then simply rotate the prism to look at a particular wavelength. The device can be calibrated so that the prism-rotating dial reads directly in wavelength.

5.5.2 Reflecting Prisms

We now examine *reflecting prisms*, in which dispersion is not desirable. In this case, the beam is introduced in such a way that at least one internal reflection takes place, for the specific purpose of either changing the direction of propagation or the orientation of [illegible] or both.

Let's first establish that it is actually possible [illegible] such an internal reflection without concomitant [illegible] sion. In other words, is δ independent of λ? The [illegible] in Fig. 5.59 is assumed to have as its profile an is[illegible] triangle—this happens to be a rather common co[illegible] ration in any event. The ray refracted at the first [illegible] face is later reflected from face FG. As we saw [illegible] (Section 4.3.4), this will occur when the internal [illegible] angle is greater than the critical angle θ_c, defin[illegible]

$$\sin\theta_c = n_{ti}.$$

For a glass–air interface, this requires that θ_i be gre[illegible] than roughly 42°. To avoid any difficulties at small [illegible] angles, let's further suppose that the base of [illegible] hypothetical prism is silvered as well—certain pri[illegible] do in fact require silvered faces. The angle of devia[illegible] between the incoming and outgoing rays is

$$\delta = 180° - \measuredangle BED.$$

From the polygon $ABED$ we have

$$\alpha + \measuredangle ADE + \measuredangle BED + \measuredangle ABE = 360°.$$

Moreover, at the two refracting surfaces

$$\measuredangle ABE = 90° + \theta_{i1}$$

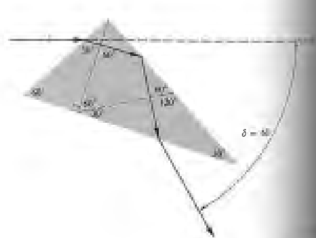


Figure 5.58 The Abbe prism.

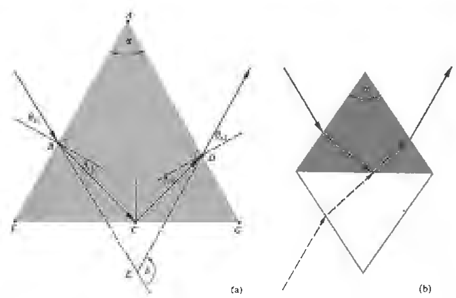


Figure 5.59 Geometry of a reflecting prism.

and

$$\measuredangle ADE = 90° + \theta_{t2}.$$

Substituting for $\measuredangle BED$ in Eq. (5.55), we get

$$\delta = \theta_{i1} + \theta_{t2} + \alpha. \qquad (5.56)$$

Since the ray at point C has equal angles of incidence and reflection, $\measuredangle BCF = \measuredangle DCG$. Thus, because the prism is isosceles, $\measuredangle BFC = \measuredangle DGC$, and triangles FBC and DGC are similar. It follows that $\measuredangle FBC = \measuredangle CDG$, and therefore $\theta_{t1} = \theta_{i2}$. From Snell's law we know that this is equivalent to $\theta_{i1} = \theta_{t2}$, whereupon the deviation becomes

$$\delta = 2\theta_{i1} + \alpha, \qquad (5.57)$$

which is certainly independent of both λ and n. The reflection will occur without any color preferences, and the prism is said to be *achromatic*. If we unfold the prism, that is, if we draw its image in the reflecting surface FG, as in Fig. 5.59(b), we see that it is equivalent in a

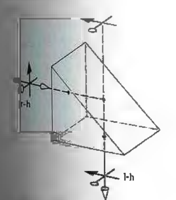


Figure 5.60 The right-angle prism.

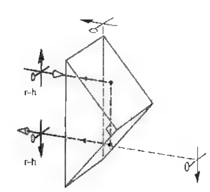


Figure 5.61 The Porro prism.

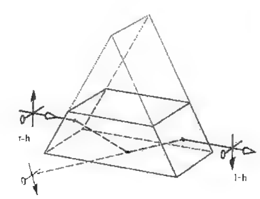


Figure 5.62 The Dove prism.

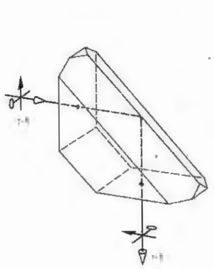


Figure 5.63 The Amici prism.

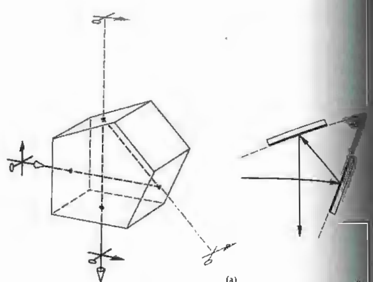


Figure 5.64 The penta prism and its mirror equivalent.

sense to a parallelepiped or thick planar plate. The image of the incident ray emerges parallel to itself, regardless of wavelength.

A few of the many widely used reflecting prisms are shown in the next several figures. These are often made from BSC-2 or C-1 glass (see Table 6.2). For the most part, the illustrations are self-explanatory, so the descriptive commentary will be brief.

The *right-angle* prism (Fig. 5.60) deviates rays normal to the incident face by 90°. Notice that the top and bottom of the image have been interchanged, that is, the arrow has been flipped over but the right and left sides have not. It is therefore an inversion system with the top face acting like a plane mirror. (To see this, imagine that the arrow and lollypop are vectors and take their cross-product. The resultant, arrow × lollypop, was initially in the propagation direction but is reversed by the prism.)

The *Porro* prism (Fig. 5.61) is physically the same as the right-angle prism but is used in a different orientation. After two reflections, the beam is deviated by 180°. Thus, if it enters right-handed, it leaves right-handed.

The *Dove* (Fig. 5.62) is a truncated version (to reduce size and weight) of the right-angle prism, used almost exclusively in collimated light. It has the interesting property (Problem 5.54) of rotating the image twice as fast as it is itself rotated about the longitudinal axis.

The *Amici* (Fig. 5.63) is essentially a truncated right-angle prism with a roof section added on to [illegible] hypotenuse face. In its most common use it has the

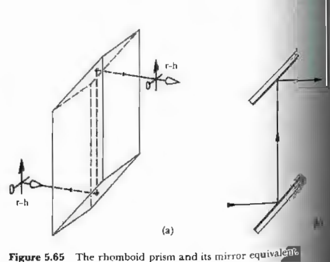


Figure 5.65 The rhomboid prism and its mirror equivalent.

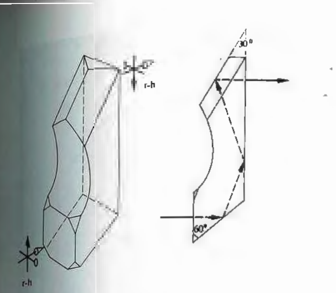


Figure 5.66 The Leman–Springer prism.

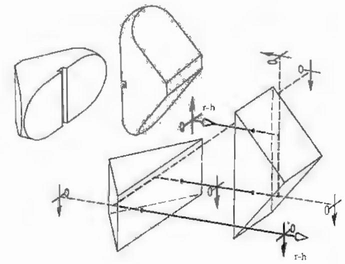


Figure 5.67 The double Porro prism.

effect of splitting the image down the middle and interchanging the right and left portions.* These prisms are expensive, because the 90° roof angle must be held to roughly [illegible] seconds of arc, or a troublesome double image will result. They are often used in simple telescope systems to correct for the reversion introduced [illegible] lenses.

The *penta* prism (Fig. 5.64) will deviate the beam by 90° without affecting the orientation of the image. Note that two of its surfaces must be silvered. These prisms are often used as end reflectors in small range finders.

The *rhomboid* prism (Fig. 5.65) displaces the line of sight without producing any angular deviation or changes in the orientation of the image.

The *Leman–Springer* prism (Fig. 5.66) also has a 90° roof. Here the line of sight is displaced without being deviated, but the emerging image is right-handed and rotated through 180°. The prism can therefore serve to erect images in telescope systems, such as gun sights and the like.

There are many more reflecting prisms that serve specific purposes. For example, if one simply cuts a cube so that the piece removed has three mutually perpendicular faces, it is called a *corner-cube* prism. It has the property of being retrodirective; that is, it will reflect all incoming rays back along their original directions. One hundred of these prisms are sitting in an 18-inch square array 240,000 miles from here, having been placed on the Moon during the Apollo 11 flight.*

The most common erecting system consists of two Porro prisms, as illustrated in Fig. 5.67. These are relatively easy to manufacture and are shown here with rounded corners to reduce weight and size. Since there are four reflections, the exiting image will be right-handed. A small slot is often cut in the hypotenuse face to obstruct rays that are internally reflected at glancing angles. Finding these slots after dismantling the family's binoculars is all too often an inexplicable surprise.

* You can see how it actually works by placing two plane mirrors at right angles and looking directly into the combination. If you wink [illegible] eye, the image will wink its *right* eye. Incidentally, if your [illegible] equally strong, you will see two seams (images of the line where the mirrors met) one running down the middle of each eye, with your nose presumably between them. If one eye is stronger, there will be only one seam, down the middle of that eye. If you close [illegible] will jump over to the other eye. This must be tried to be [illegible].

* J. E. Faller and E. J. Wampler, "The Lunar Laser Reflector," *Sci. Am.*, March 1970, p. 38.

5.6 FIBEROPTICS

In recent times, techniques have been evolved for efficiently conducting light from one point in space to another via transparent, dielectric fibers. As long as the diameter of these fibers is large compared with the wavelength of the radiant energy, the inherent wave nature of the propagation mechanism is of little importance, and the process obeys the familiar laws of geometrical optics. On the other hand, if the diameter is of the order of λ, the transmission closely resembles the manner in which microwaves advance along waveguides. Some of the propagation modes are evident in the photomicrographic end views of fibers shown in Fig. 5.68. Here the wave nature of light must be reckoned with and this behavior therefore resides in the domain of physical optics. Although optical waveguides, particularly of the thin-film variety, are of increasing interest, this discussion will be limited to the case of relatively large diameter fibers.

Consider the straight glass cylinder of Fig. 5.69 surrounded by air. Light striking its walls from within will be totally internally reflected, provided that the incident angle at each reflection is greater than $\theta_c = \sin^{-1} n_a/n_f$, where n_f is the index of the cylinder or fiber. As we will show, a *meridional ray* (i.e., one that is coplanar with the optical axis) might undergo several thousand reflections per foot as it bounces back and forth along a fiber, until it emerges at the far end (Fig. 5.70). If the fiber has a diameter D and a length L, the path length ℓ traversed by the ray will be

$$\ell = L/\cos\theta_t, \qquad (5.58)$$

or from Snell's law

$$\ell = n_f L(n_f^2 - \sin^2\theta_i)^{-1/2}. \qquad (5.59)$$

The number of reflections N is then given by

$$N = \frac{\ell}{D/\sin\theta_t} \pm 1$$

or

$$N = \frac{L\sin\theta_i}{D(n_f^2 - \sin^2\theta_i)^{1/2}} \pm 1, \qquad (5.60)$$

Figure 5.68 Optical waveguide mode patterns seen in the ... of small-diameter fibers. (Photo courtesy of Narinder S. ...

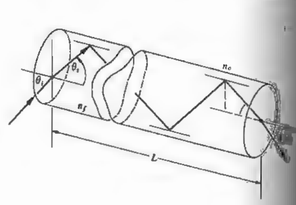
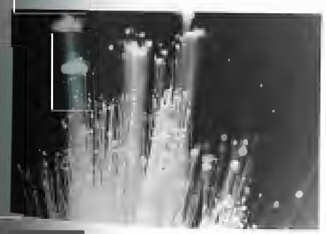


Figure 5.69 Rays reflected within a dielectric cylinder.

rounded off to the nearest whole number. The ... which depends on where the ray strikes the end ... is of no significance when N is large, as it is in prac... Thus if D is 50 μm (i.e., 50 microns where 1 μm = 10^{-6} m = 39.37×10^{-6} in), which is about 2×10^{-3} in ... hair from the head of a human is roughly 50 μm diameter), and if $n_f = 1.6$ and $\theta_i = 30°$, N turns out to be approximately 2000 reflections per foot. Fibers are available in diameters from about 2 μm to $\frac{1}{4}$ inch or so but are seldom used in sizes much smaller than about 10 μm. The large-diameter rods are generally called ... pipes. Extremely thin glass (or plastic) filaments are quite flexible and can even be woven into fabric.

The smooth surface of a single fiber must be kept clean (of moisture, dust, oil, etc.), if there is to be no ... of light (via the mechanism of frustrated total internal reflection). Similarly, if large numbers of fibers are packed in close proximity, light may leak from one ... other in what is known as *cross-talk*. For these reasons, it is now customary to enshroud each fiber in a transparent sheath of lower index called a **cladding**. This layer need only be thick enough to provide the desired isolation, but for other reasons it generally occupies about one tenth of the cross-sectional area. Although references in the literature to simple "light pipes" go back 100 years, the modern era of fiberoptics began with the introduction of clad fibers in 1953.

Typically, a fiber core might have an index (n_f) of 1.62, and the cladding an index (n_c) of 1.52, although a range of values is available. A clad fiber is shown in Fig. 5.71. Notice that there is a maximum value θ_{max} of θ_i, for which the internal ray will impinge at the critical angle, θ_c. Rays incident on the face at angles greater than θ_{max} will strike the interior wall at angles less than θ_c. They will be only partially reflected at each such encounter with the core-cladding interface and will quickly leak out of the fiber. Accordingly, θ_{max}, which is known as the acceptance angle, defines the half-angle of the acceptance cone of the fiber. To determine it we write



... Light emerging from the ends of a loose bundle of glass ... by E.H.)

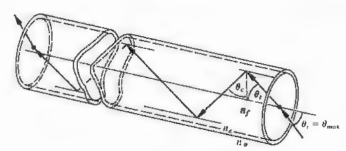


Figure 5.71 Rays in a clad optical fiber.

$$\sin\theta_c = n_c/n_f = \sin(90 - \theta_t).$$

Thus

$$n_c/n_f = \cos\theta_t \qquad (5.61)$$

or

$$n_c/n_f = (1 - \sin^2\theta_t)^{1/2}.$$

Making use of Snell's law and rearranging matters, we have

$$\sin\theta_{max} = \frac{1}{n_o}(n_f^2 - n_c^2)^{1/2}. \qquad (5.62)$$

The quantity $n_o \sin\theta_{max}$ is defined as the **numerical aperture**, or NA. Its square is a measure of the light-gathering power of the system. The term originates in microscopy, where the equivalent expression characterizes the corresponding capabilities of the objective lens. It should clearly relate to the *speed* of the system, and, in fact,

$$f/\# = \frac{1}{2(\text{NA})}. \qquad (5.63)$$

Thus for a fiber

$$\text{NA} = (n_f^2 - n_c^2)^{1/2}. \qquad (5.64)$$

The left-hand side of Eq. (5.62) cannot exceed 1, and in air ($n_o = 1.00028 \approx 1$) that means that the largest value of NA is 1. In this case, the half-angle θ_{max} equals 90°, and the fiber totally internally reflects all light entering its face (Problem 5.55). Fibers with a wide variety of numerical apertures, from about 0.2 up to and including 1.0, are commercially obtainable.

Bundles of free fibers whose ends are bound together (e.g., with epoxy), ground, and polished form flexible light guides. If no attempt is made to align the fibers in an ordered array, they form an *incoherent bundle*. This unfortunate use of the term incoherent (which should not be confused with coherence theory) just means, for example, that the first fiber in the top row at the entrance face may have its terminus anywhere in the bundle at the exit face. These *flexible light carriers* are, for that reason, relatively easy to make and inexpensive. Their primary function is simply to conduct light from one region to another. Conversely, when the fibers are carefully arranged so that their terminations occupy the same relative positions in both of the bound ends of the bundle, it is said to be *coherent*. Such an arrangement is capable of transmitting images and is consequently known as a *flexible image carrier*. Incidentally, coherent bundles are frequently fashioned by winding fibers on a drum to make ribbons, which are then carefully layered. When one end of such a device is placed face down flat on an illuminated surface, a point-by-point image of whatever is beneath it will appear at the other end (Fig. 5.72). These bundles can be tipped off with a small lens, so that they need not be in contact with the object under examination. Nowadays it is common to use fiberoptic instruments to poke into all sorts of unlikely places, from nuclear reactor cores and jet engines to stomachs and reproductive organs. When a device is used to examine internal body cavities, it's called an *endoscope*. This category includes bronchoscopes, colonoscopes, gastroscopes, and so forth, all of which are generally less than about 200 cm in length. Similar industrial instruments are usually two or three times as long and often contain 5000 to 50,000 fibers, depending on the required image resolution and the overall diameter that can be accommodated. An additional incoherent bundle incorporated into the device usually supplies the illumination.

Not all fiberoptic arrays are made flexible; for example, fused, rigid, coherent fiber faceplates, *mosaics*, are used to replace homogeneous [illegible] resolution sheet glass on cathode-ray tubes, vid[illegible] image intensifiers, and other devices. Mosaics co[illegible] of literally millions of fibers with their cladding[illegible] together have mechanical properties almost iden[illegible] homogeneous glass. Similarly, a sheet of fused [illegible] fibers can either magnify or minify an image, depe[illegible] on whether the light enters the smaller or larger [illegible] of the fiber. The compound eye of an insect such as the housefly is effectively a bundle of tapered [illegible] optical filaments. The rods and cones that make up the human retina may also channel light through total internal reflection. Another common application of mosaics involving imaging is the *field flattener*. If the image formed by a lens system resides on a curved surface, it is often desirable to reshape it into a plane, for example, to match a film plate. A mosaic can be ground and polished on one of its end surfaces to correspond to the contour of the image and on the other to match the [illegible] detector. Incidentally, a naturally occurring fibrous crystal known as ulexite, when polished, responds surprisingly like a fiberoptic mosaic. (Hobby shops often sell it for use in making jewelry.)

If you have never seen the kind of light conduction we've been talking about, try looking down the edges of a stack of microscope slides. Even better are the much [illegible] (0.18-mm) cover-glass slides. Figure 5.73 shows how daylight is conveyed to the upper surface of a stack of a few hundred of these slides held together by a rubber band.

Figure 5.72 A coherent bundle of 10 μm glass fibers transmits an image even though knotted and sharply bent. (Photo courtesy American Cystoscope Makers, Inc.)

Today fiberoptics has three very different applications: it is used for the direct transmission of images and illumination, it serves as the core of a new family [illegible] and it provides a variety of remarkable waveguides used in telecommunications. The idea of transmitting images over distances of a few meters with [illegible] bundles, however beautiful and however useful, is really a rather unsophisticated business that doesn't start to utilize the full potential inherent in [illegible] During the past few decades the application of lightguides to telecommunications has begun something of a revolution. Even more recently, fiberoptic sensors [illegible] devices that measure pressure, sound, temperature, voltage, current, liquid levels, electric and [illegible] fields, rotations, and so forth—have become [illegible] manifestation of the versatility of fibers.

[illegible] is now in the beginning stages of a new [illegible] telecommunications, with radiant energy along fibers replacing electricity moving in metal wires—not for transmitting power, but information. The much higher frequencies of light allow for an incredible increase in data-handling capacity. For example, with sophisticated transmitting techniques, a pair of copper telephone wires can be made to carry [illegible] of about two dozen simultaneous conversations. This should be compared with a single, ongoing, simple television transmission, which is equivalent to about

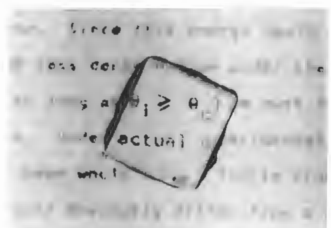


Figure 5.73 A stack of cover-glass slides held together by a rubber band serves as a coherent light guide. (Photo by E.H.)

1300 simultaneous telephone conversations, and that, in turn, is roughly the equal of sending some 2500 typewritten pages each second. Clearly, at present it's quite impractical to attempt to send television over copper telephone lines. Yet it's already possible to transmit in excess of 12,000 simultaneous conversations over a *single pair* of fibers—that's more than nine television channels. Each such fiber has a line rate of about 400 million bits of information per second (400 Mb/s), or 6000 voice circuits. This is only the beginning; rates of 2000 Mb/s will be widely available before long. The technology is in its infancy.

Capacities achieved to date don't even begin to approach the theoretical limit. Still, the accomplishments of recent times are impressive. For example, the new transatlantic cable TAT-8 is a fiberoptic system that is designed, using some clever data-handling techniques, to carry 40,000 conversations at once over just two pairs of glass fibers. TAT-1, a copper cable installed in 1956, could carry a mere 51 conversations, and the last of the bulky copper versions, TAT-7 (1983), can handle only about 8000. Significantly, the TAT-8 is designed to have regenerators or repeaters (to boost the signal strength) every 50 km (30 mi) or more. That should be compared with the copper TAT-7, which has amplifiers every 10 km or so. This feature is tremendously important in long-distance communications. Ordinary wire systems require repeaters roughly every kilometer; electrical coaxial networks extend that range to about 2 to 6 km; even radio transmissions through the atmosphere need regeneration every 30 to 50 km. It is anticipated that high-performance fiber systems will extend the repeater separation to upward of 150 km.

A major determining factor in the spacing of repeaters is the power loss due to attenuation of the signal as it propagates down the line. The decibel (dB) is the customary unit used to designate the ratio of two power levels, and as such it can provide a convenient indication of the power-out (P_o) with respect to the power-in (P_i). The number of dB $= -10 \log (P_o/P_i)$, and hence a ratio of 1 : 10 is 10 dB, 1 : 100 is 20 dB, 1 : 1000 is 30 dB, and so on. The attenuation (α) is usually specified in decibels per kilometer (dB/km) of fiber length (L). Thus $-\alpha L/10 = \log (P_o/P_i)$, and if we raise 10 to the power of both sides,

$$P_o/P_i = 10^{-\alpha L/10}. \tag{5.65}$$

As a rule, reamplification of the signal is necessary when the power has dropped by a factor of about 10^{-5}. Commercial optical glass, the kind of material available for fibers in the mid-1960s, has an attenuation of about 1000 dB/km. Light, after being transmitted 1 km through the stuff, would drop in power by a factor of 10^{-100}, and regenerators would be needed every 50 m (which is little better than communicating with a string and two tin cans). By 1970 α was down to about 20 dB/km for fused silica (quartz, SiO_2), and it was reduced to as little as 0.16 dB/km in 1982. This tremendous decrease in attenuation was achieved mostly by removing impurities (especially the ions of iron, nickel, and copper) and reducing contamination by OH groups, largely accomplished by scrupulously eliminating any traces of water in the glass (p. 62).

Figure 5.74 depicts the three major fiber configurations used in communications today. In (a) the core is relatively wide, and the indices of core and cladding are both constant throughout. This is the so-called *stepped-index* fiber, with a homogeneous core of 50 to 150 μm or more and cladding with an outer diameter

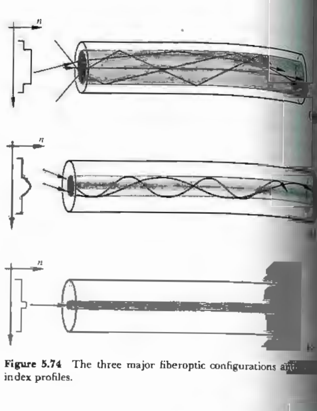


Figure 5.74 The three major fiberoptic configurations an[illegible] index profiles.

of roughly 100 to 250 μm. The oldest of the three types, the stepped-index fiber was widely used in first-[illegible] ation systems (1975–1980). The comparatively [illegible] central core makes it rugged and easily infuse[illegible] light, as well as easily terminated and coupled. [illegible] least expensive but also, as we will see prese[illegible] least effective of the lot, and for long-range appl[illegible] it has some serious drawbacks.

Depending on the launch angle into the fibe[illegible] can be hundreds, even thousands, of different ra[illegible] or modes by which energy can propagate down [illegible] (Fig. 5.75). This then is a *multimode* fiber, where[illegible] mode corresponds to a slightly different transit [illegible] Higher-angle rays travel longer paths; reflecting [illegible] side to side, they take longer to get to the end o[illegible] fiber than do rays moving along the axis. This is lo[illegible] spoken of as *intermodal dispersion* (or often just [illegible] *dispersion*), even though it has nothing to do w[illegible] frequency-dependent index of refraction. Inform[illegible]

to be transmitted is usually digitized in some coded fashion and then sent along the fibers as a flood of [illegible] pulses or bits per second. The different transit times have the undesirable effect of changing the [illegible] of the pulses of light that represent the signal. What started as a sharp rectangular pulse can smear out, after traveling a few kilometers within the fiber, into an unrecognizable blur (Fig. 5.76).

The total time delay between the arrival of the axial ray and the slowest ray, the one traveling the longest distance, is $\Delta t = t_{max} - t_{min}$. Here, referring back to Fig. 5.71, the minimum time of travel is just the axial length L divided by the speed of light in the fiber:

$$t_{min} = \frac{L}{v_f} = \frac{L}{c/n_f} = \frac{Ln_f}{c}. \tag{5.66}$$

[illegible] route (ℓ), given by Eq. (5.58), is longest [illegible] is incident at the critical angle, whereupon [illegible] holds. Combining these two, we get $\ell = Ln_f/n_c$, and so

$$t_{max} = \frac{\ell}{v_f} = \frac{Ln_f/n_c}{c/n_f} = \frac{Ln_f^2}{cn_c}. \tag{5.67}$$

Thus it follows that, subtracting Eq. (5.66) from Eq. (5.67), we get

$$\Delta t = \frac{Ln_f}{c}\left(\frac{n_f}{n_c} - 1\right). \tag{5.68}$$

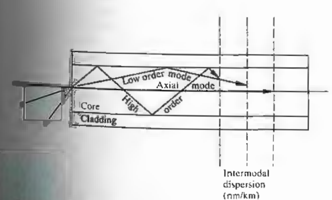


Figure 5.75 Intermodal dispersion in a stepped-index multimode fiber.

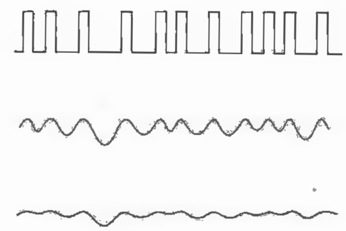


Figure 5.76 Rectangular pulses of light smeared out by increasing amounts of dispersion. Note how the closely spaced pulses degrade more quickly.

As an example, suppose $n_f = 1.500$ and $n_c = 1.489$. The delay, $\Delta t/L$, then turns out to be 37 ns/km. In other words, a sharp pulse of light entering the system will be spread out in time some 37 ns for each kilometer of fiber traversed. Moreover, traveling at a speed $v_f = c/n_f = 2.0 \times 10^8$ m/s, it will spread in space over a length of 7.4 m/km. To make sure that the transmitted signal will still be easily readable, we might require that the spatial (or temporal) separation be at least twice the spread-out width (Fig. 5.77). Now imagine the line to be 1.0 km long. In that case the output pulses are 7.4 m wide on emerging from the fiber and so must be separated by 14.8 m. This means that the input pulses must be at least 14.8 m apart; they must be separated in time by 74 ns and so cannot come any faster than one every 74 ns, which is a rate of 13.5 million pulses per second. In this way the intermodal dispersion (which is typically 15 to 30 ns/km) limits the frequency of the input signal, thereby dictating the rate at which information can be fed through the system.

This problem of delay differences can be reduced as much as a hundredfold by gradually varying the refractive index of the core, decreasing it radially outward to the cladding [Fig. 5.74(b)]. Instead of following sharp zigzag paths, the rays then smoothly spiral around the

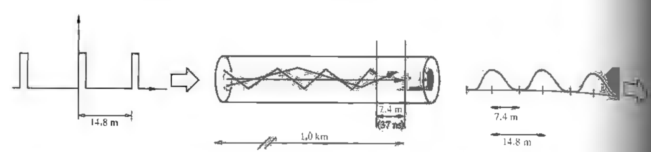


Figure 5.77 The spreading of an input signal due to intermodal dispersion.

central axis. Because the index is higher along the center, rays taking shorter paths are slowed down by proportionately greater amounts, and rays spiralling around near the cladding move more swiftly over longer paths. The result is that all the rays tend to stay more or less together in these multimode *graded-index* fibers. Typically, a graded-index fiber has a core diameter of about 20 μm to 90 μm and an intermodal dispersion of only around 2 ns/km. They are intermediate in price and widely used in medium-distance intercity applications.

Multimode fibers with core diameters of 50 μm or more are often fed by *light-emitting diodes*, or LEDs. These are comparatively inexpensive and are commonly used over relatively short spans at low transmission rates. The problem with them is that they emit a fairly broad range of frequencies. As a result, ordinary *material* or *spectral dispersion*, the fact that the fiber index is a function of frequency, becomes a limiting factor. That difficulty is essentially avoided by using spectrally pure laserbeams. Alternatively, the fibers can be operated at wavelengths near 1.3 μm, where silica glass (see Figs. 3.27 and 3.28) has little dispersion.

The last, and best, solution to the problem of intermodal dispersion is to make the core so narrow (less than 10 μm) that it will provide only one mode wherein the rays travel parallel to the central axis [Fig. 5.74(c)]. Such *single-mode* fibers of ultrapure glass (both stepped-index and the newer graded-index) provide the best performance. Typically having core diameters of only 2 μm to 9 μm, they essentially eliminate intermodal dispersion. Although they are relatively expensive and require laser sources, these single-mode fibers [redacted] at 1.55 μm (where the attenuation is about 0.2[redacted] not far from the ideal silica value of 0.1 dB/[redacted] today's premiere long-haul lightguides. A pai[redacted] fibers may someday connect your home to a [redacted] network of communications and computer facili[redacted] making the era of the copper wire seem charmi[redacted] primitive.

5.7 OPTICAL SYSTEMS

We have developed paraxial theory to a point [redacted] is now possible to appreciate the principles und[redacted] the majority of practical optical systems. To b[redacted] the subtleties involved in controlling aberration[redacted] extremely important and still beyond this discus[redacted] Even so, one could build, for example, a [redacted] (admittedly not a very good one, but a [redacted] nonetheless) using the conclusions already [redacted] first-order theory.

What better starting point for a discussion of [redacted] instruments than the most common of all—the [redacted]

5.7.1 Eyes

For our purposes, three main groupings of eyes [redacted] readily be distinguished: those that gather radi[redacted] energy and form images via a single centere[redacted] system, those that utilize a multifaceted [redacted] of tiny lenses (feeding into channels resembling optical [redacted]), and the most rudimentary, those that simply [redacted] with a small lensless hole (p.199). In addition [redacted] light eyes, the rattlesnake has infrared pinhole "eyes" called pits, which might be included in this last group. Visual lens systems of the first type have evolved independently and remarkably similarly in at least three distinct kinds of organisms. Some of the more advanced mollusks (e.g., the octopus), certain spiders (e.g., the [redacted]), and the vertebrates, ourselves included, [redacted] eyes that each form a single continuous real [redacted] on a light-sensitive screen or retina. By com[redacted] the multifaceted compound eye (Fig. 5.78) [redacted] independently among arthropods, the [redacted] with articulated bodies and limbs (e.g., insects [redacted]). It produces a mosaic sensory image com[redacted] many small-field-of-view spot contributions, one from each tiny segment of the eye (as if one were looking at the world through a tightly packed bundle [redacted] fine tubes). Like a television picture [redacted] of different-intensity dots, the compound eye divides and digitizes the scene being viewed. There is no real image formed on a retinal screen; the synthesis [redacted] electrically in the nervous system. The horse[redacted] upward of 7000 such segments, and the preda[redacted] dragonfly, an especially fast flyer, gets a better view with 30,000, as compared with some ants that manage with only about 50. The more facets, the more image dots, and the better the resolution, the sharper the composite picture. This may well be the oldest of eye types: trilobites, the little sea creatures of 500 million years ago had well-developed compound eyes. Remarkably, however different the optics, the chemistry of the image-sensing mechanisms in all Earth animals is quite similar.

i) Structure of the Human Eye

The human eye can be thought of as a positive double lens arrangement that casts a real image on a light-sensitive surface. That notion, in a rudimentary form, was apparently proposed by Kepler (1604), who wrote "Vision, I say, occurs when the image of the . . . external world . . . is projected onto the . . . concave retina." This insight gained wide acceptance only after a lovely experiment was performed in 1625 by the German Jesuit Christopher Scheiner (and independently, about five years later, by Descartes). Scheiner removed the coating on the back of an animal's eyeball and, peering through the nearly transparent retina from behind, was able to see a minified, inverted image of the scene beyond the eye. Though it resembles a simple camera,

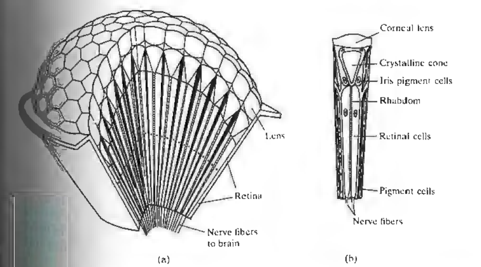


Figure 5.78 (a) The compound eye made up of many ommatidia. (b) An ommatidium, the little individual eye that each "sees" a small region in a particular direction. The corneal lens and crystalline cone channel the light into the sensing structure, the clear, rod-shaped rhabdom. Each of these is surrounded by retinal cells which lead via nerve fibers to the brain. (From Ackerman et al., *Biophysical Science*, © 1962, 1979. Englewood Cliffs, NJ: Prentice-Hall, Inc. p. 31. After R. Bushman, *Animals Without Backbones*.)

the seeing system (eye, optic nerve, and visual cortex) functions much more like a closed-circuit computerized television unit.

The eye (Fig. 5.79) is an almost spherical (24 mm long by about 22 mm across) jellylike mass contained within a tough flexible shell, the *sclera*. Except for the front portion, or *cornea*, which is transparent, the sclera is white and opaque. Bulging upward from the body of the sphere, the cornea's curved surface (which is slightly flattened, thereby cutting down on spherical aberration) serves as the first and strongest convex element of the lens system. Indeed most of the bending imparted to a bundle of rays takes place at the air–cornea interface. Incidentally, one of the reasons you can't see very well under water ($n_W \approx 1.33$) is that its index is too close to that of the cornea ($n_C \approx 1.376$) to allow for adequate refraction. Light emerging from the cornea passes through a chamber filled with a clear watery fluid called the *aqueous humor* ($n_{ah} \approx 1.336$). A ray that is strongly refracted toward the optical axis at the air–cornea interface will be only slightly redirected at the cornea–aqueous humor interface because of the similarity of their indices. Immersed in the aqueous is a diaphragm known as the *iris*, which serves as the aperture stop controlling the amount of light entering the eye through the hole, or *pupil*. It is the iris (from the Greek word for rainbow) that gives the eye its characteristic blue, brown, gray, green, or hazel color. Made up of circular and radial muscles, the iris can expand or contract the pupil over a range from about 2 mm in bright light to roughly 8 mm in darkness. In addition to this function, it is also linked to the focusing response and will contract to increase image sharpness when doing close work. Immediately behind the iris is the *crystalline lens*. The name, which is somewhat misleading, dates back to about 1000 A.D. and the work of Abû 'Alî al Hasan ibn al Hasan ibn al Haitham, alias Alhazen of Cairo, who described the eye as partitioned into three regions that were watery, crystalline, and glassy, respectively. The lens, which has both the size and shape of a small bean (9 mm in diameter and 4 mm thick), is a complex layered fibrous mass surrounded by an elastic membrane. In structure it is somewhat like a transparent onion, formed of roughly 22,000 very fine layers. It has some remarkable characteristics that distinguish it from man-

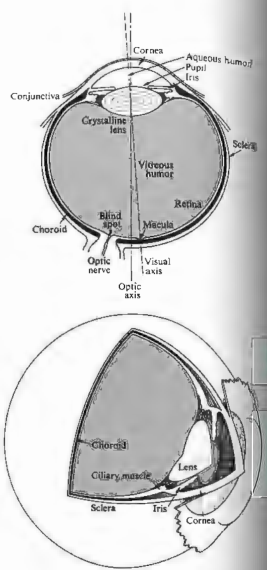


Figure 5.79 The human eye.

made lenses in use today, in addition to the [illegible] continues to grow in size. Because of its laminar [illegible] ture, rays traversing it will follow paths made [illegible] minute, discontinuous segments. The lens as a [illegible] quite pliable, albeit less so with age. Moreover, [illegible] of refraction ranges from about 1.406 at the in[illegible]

to approximately 1.386 at the less dense cortex and, as such it represents a GRIN system (p. 136). The crystal-[illegible] lens provides the needed fine-focusing mechanism through [illegible] in its shape, that is, it has a variable focal length—a feature we'll come back to presently.

The refracting components of the eye, the cornea and crystalline lens, can be treated as forming an effective double-element lens with an object focus of about 15.6 mm in front of the anterior surface of the cornea and an image focus of about 24.3 mm behind it on the retina. To simplify things a little we can take the combined lens to have an optical center 17.1 mm in front of the retina, which falls just at the rear edge of the crystalline lens.

Behind the lens is another chamber filled with a transparent gelatinous substance known as the *vitreous humor* ($n_{vh} \approx 1.337$). As an aside, it should be noted that the vitreous humor contains microscopic particles of [illegible] freely about. You can easily see [illegible] with diffraction fringes, within [illegible] squinting at a light source or looking [illegible] a pinhole—strange little amoebalike [illegible] *volitantes*) will float across the field of [illegible], a marked increase in one's percep-[illegible] floaters may be indicative of retinal detach-[illegible] you're at it, squint at the source again (a [illegible] fluorescent light works well). Closing your [illegible] completely, you'll actually be able to see the [illegible] periphery of your own pupil, beyond [illegible] glare of light will disappear into blackness. [illegible] believe it, block and then unblock some of [illegible] the glare circle will visibly expand and con-[illegible] respectively. You are seeing the shadow cast by [illegible] the inside! Seeing internal objects like this [illegible] as entoptic perception.

[illegible] the tough sclerotic wall is an inner shell, the [illegible] a dark layer, well supplied with blood [illegible] richly pigmented with melanin. The choroid [illegible] of stray light, as is the coat of black paint [illegible] inside of a camera. A thin layer (about 0.5 mm [illegible] thick) of light receptor cells covers much of [illegible] face of the choroid—this is the *retina* (from [illegible], meaning net). The focused beam of light [illegible] via electrochemical reactions in this pinkish [illegible] structure. The human eye contains two kinds of photoreceptor cells: *rods* and *cones* (Fig. 5.80). Roughly 125 million of them are intermingled nonuniformly over the retina. The ensemble of rods (each about 0.002 mm in diameter) in some respects has the characteristics of a high-speed, black and white film (such as Tri-X). It is exceedingly sensitive, performing in light too dim for the cones to respond to, yet it is unable to distinguish color, and the images it relays are not well defined. In contrast, the ensemble of 6 or 7 million cones (each about 0.006 mm in diameter) can be imagined as a separate, but overlapping, low-speed color film. It performs in bright light, giving detailed colored views, but is fairly insensitive at low light levels.

The normal wavelength range of human vision is said to be roughly 390 nm to 780 nm (Table 3.2, p. 72). However, studies have extended these limits down to about 310 nm in the ultraviolet and up to roughly 1050 nm in the infrared—indeed people have reported "seeing" x-radiation. The limitation on ultraviolet transmission in the eye is set by the crystalline lens, which absorbs in the UV. People who have had a lens removed surgically have greatly improved UV sensitivity.

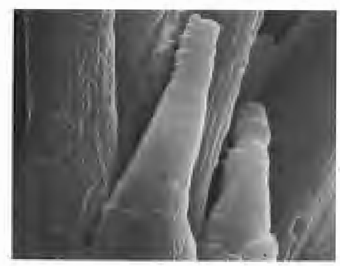


Figure 5.80 An electron micrograph of the retina of a salamander (Necturus Maculosus). Two visual cones appear in the foreground and several rods behind them. Photo from E. R. Lewis, Y. Y. Zeevi, and F. S. Werblin, *Brain Research* **15**, 559 (1969).

The area of exit of the optic nerve from the eye contains no receptors and is insensitive to light; accordingly it is known as the *blind spot* (see Fig. 5.81). The optic nerve spreads out over the back of the interior of the eye in the form of the retina.

Just about at the center of the retina is a small depression from 2.5 to 3 mm in diameter known as the yellow spot, or *macula*. There is a tiny rod-free region about 0.3 mm in diameter at its center, the *fovea centralis*. (In comparison, the image of the full Moon on the retina is about 0.2 mm in diameter—Problem 5.59.) Here the cones are thinner (with diameters of 0.0030 mm to 0.0015 mm) and more densely packed than anywhere else in the retina. Since the fovea provides the sharpest and most detailed information, the eyeball is continuously moving, so that light coming from the area on the object of primary interest falls on this region. An image is constantly shifted across different receptor cells by these normal eye movements. If such movements did not occur and the image was kept stationary on a given set of photoreceptors, it would actually tend to fade out. Another fact that indicates the complexity of the sensing system is that the rods are multiply connected to nerve fibers, and a single such fiber can be activated by any one of about a hundred rods. By contrast, cones in the fovea are individually connected to nerve fibers. The actual perception of a scene is constructed by the eye–brain system in a continuous analysis of the time-varying retinal image. Just think how little trouble the blind spot causes, even with one eye closed.

Between the nerve-fiber layer of the retina and the humor is a network of large retinal blood vessels, which

×   1   2

Figure 5.81 To verify the existence of the blind spot, close one eye and, at a distance of about 10 inches, look directly at the X—the 2 will disappear. Moving closer will cause the 2 to reappear while the 1 vanishes.

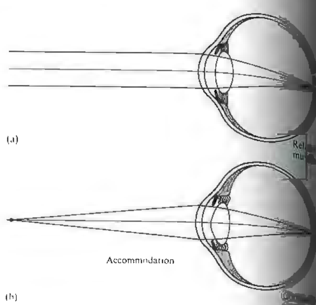


Figure 5.82 Accommodation—changes in the lens config[illegible]

can be observed entoptically. One way is to [illegible] eye and place a bright small source against the [illegible] "see" a pattern of shadows (*Purkinje figures*) cast [illegible] blood vessels on the sensitive retinal layer.

ii) Accommodation

The fine focusing, or *accommodation*, of the hum[illegible] is a function performed by the crystalline lens. [illegible] is suspended in position behind the iris by [illegible] that are connected to the *ciliary muscles*. Ordin[illegible] these muscles are relaxed, and in that state they [illegible] back on the network of fine fibers holding [illegible] the lens. This draws the pliable lens into a fairly flat configuration, increasing its radii, which in [illegible] increases its focal length (5.16). With the mus[illegible] pletely relaxed, the light from an object at in[illegible] be focused on the retina (Fig. 5.82). As the obj[illegible] closer to the eye, the ciliary muscles contract, [illegible] the external tension on the periphery of the lens, wh[illegible] then bulges slightly under its own elastic forces. In [illegible] doing the focal length decreases such that [illegible] constant. As the object comes still closer, the ciliary muscles be[illegible] more tensely contracted, and the lens surfaces take on even smaller radii. The closest point [illegible] the eye can focus is known as the **near point**. [illegible] it might be about 7 cm for a teen-ager, [illegible] for a young adult, roughly 28 to 40 cm in [illegible]dle-aged, and about 100 cm by 60 years of age. [illegible]uments are designed with this in mind, so [illegible] the eye need not strain unnecessarily. Clearly, the [illegible] cannot focus on two different objects at once. This [illegible]e obvious if, while looking through a piece [illegible] you try to focus on it and the scene beyond at [illegible] time.

[illegible] generally accommodate by varying the lens [illegible], but there are other means. Fish move only the [illegible] itself toward or away from the retina, just as [illegible] camera lens is moved to focus. Some mollusks [illegible] the same thing by contracting or expanding [illegible] eye, thus altering the relative distance [illegible] lens and retina. For birds of prey, which must [illegible]pidly moving object in constant focus over a [illegible]de range of distances as a matter of survival, the [illegible]commodation mechanism is quite different. They [illegible]date by greatly changing the curvature of the cornea.

5.7.2 Eyeglasses

[illegible] were probably invented some time in the late [illegible] century, possibly in Italy. A Florentine manu[illegible] period (1299), which no longer exists, spoke [illegible] recently invented for the convenience of [illegible] whose sight has begun to fail." These were [illegible] lenses, little more than variations on the hand-[illegible]ifying or reading glasses, and polished gem-[illegible] were no doubt employed as lorgnettes long [illegible] that Roger Bacon (ca. 1267) wrote about nega-[illegible] rather early on, but it was almost another [illegible]red years before Nicholas Cusa first discussed [illegible] eyeglasses and a hundred years more before [illegible] ceased to be a novelty, in the late 1500s. [illegible]ingly, it was considered improper to wear specta-[illegible] public even as late as the eighteenth century, [illegible] in the paintings up until that time.

In 1804 Wollaston, recognizing that traditional (fairly flat, biconvex, and concave) eyeglasses provided good vision only while one looked through their centers, patented a new, deeply curved lens. This was the forerunner of modern-day meniscus (from the Greek *meniskos*, the diminutive for moon, i.e., crescent) lenses, which allow the turning eyeball to see through them from center to margin without significant distortion.

It is customary and quite convenient in physiological optics to speak about the **dioptric power**, $\mathcal{D}$, of a lens, which is simply the reciprocal of the focal length. When f is in meters, the unit of power is the inverse meter, or *diopter*, symbolized by D: $1\ \text{m}^{-1} = 1$ D. For example, if a converging lens has a focal length of +1 m, its power is +1 D; with a focal length of −2 m (a diverging lens), $\mathcal{D} = -\frac{1}{2}$ D; for $f = +10$ cm, $\mathcal{D} = 10$ D. Since a thin lens of index n_l in air has a focal length given by

$$\frac{1}{f} = (n_l - 1)\left(\frac{1}{R_1} - \frac{1}{R_2}\right), \qquad [5.16]$$

its power is

$$\mathcal{D} = (n_l - 1)\left(\frac{1}{R_1} - \frac{1}{R_2}\right). \qquad (5.69)$$

You can get a sense of the direction in which we are moving by considering, in rather loose terms, that each surface of a lens bends the incoming rays—the more bending, the stronger the surface. A convex lens that strongly bends the rays at both surfaces has a short focal length and a large dioptric power. We already know that the focal length for two thin lenses in contact is given by

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2}. \qquad [5.38]$$

This means that the combined power is the sum of the individual powers, that is,

$$\mathcal{D} = \mathcal{D}_1 + \mathcal{D}_2.$$

Thus a convex lens with $\mathcal{D}_1 = +10$ D in contact with a negative lens of $\mathcal{D}_2 = -10$ D results in $\mathcal{D} = 0$; the combination behaves like a parallel sheet of glass. Furthermore, we can imagine a lens, for example, a double convex lens, as being composed of two planar-convex lenses in intimate contact, back to back. The power of each of these follows from Eq. (5.69); thus for the first planar-convex lens ($R_2 = \infty$),

$$\mathcal{D}_1 = \frac{(n_l - 1)}{R_1}, \qquad (5.70)$$

and for the second,

$$\mathcal{D}_2 = \frac{(n_l - 1)}{-R_2}. \qquad (5.71)$$

These expressions may be equally well defined as giving the *powers of the respective surfaces* of the initial double convex lens. In other words, *the power of any thin lens is equal to the sum of the powers of its surfaces.* Because R_2 for a convex lens is a negative number, both $\mathcal{D}_1$ and $\mathcal{D}_2$ will be positive in that case. The power of a surface, defined in this way, is not generally the reciprocal of its focal length, although it is when immersed in air. Relating this terminology to the generally used model for the human eye, we note that the power of the crystalline lens *surrounded by air* is about +19 D. The cornea provides roughly +43 of the total +58.6 D of the intact unaccommodated eye.

A normal eye, despite the connotation of the word, is not really as common as one might expect. By the term normal, or its synonym *emmetropic*, we mean an eye that is capable of focusing parallel rays on the retina while in a relaxed condition, that is, one whose second focal point lies on the retina. For the unaccommodated eye, we define the point whose image lies on the retina to be the **far point**. Thus for the normal eye the most distant point that can be brought to a focus on the retina, the far point, is located at infinity (which for all practical purposes is anywhere beyond about 5 m). In contrast, when the second focal point does not lie on the retina, the eye is *ametropic* (e.g., it suffers hyperopia, myopia, or astigmatism). This can arise either because of abnormal changes in the refracting mechanism (cornea, lens, etc.) or because of alterations in the length of the eyeball that alter the distance between the lens and the retina. The latter is by far the more common cause. Just to put things in proper perspective, note that about 25% of young adults require ±0.5 D or less of eyeglass correction, and perhaps as many as 65% need only ±1.0 D or less.

i) Nearsightedness—Negative Lenses

Myopia is the condition in which parallel [illegible] are brought to focus in front of the retina; the [illegible] the lens system as configured is too large fo[illegible] anterior–posterior axial length of the eye. Ima[illegible] distant objects fall in front of the retina, the fa[illegible] is closer in than infinity, and all points beyond [illegible] appear blurred. This is why myopia is often [illegible] *nearsightedness*—an eye with this defect sees [illegible] objects clearly (Fig. 5.83). To correct the condi[illegible] at least its symptoms, we place an additional [illegible] front of the eye such that the combined specta[illegible] lens system has its second focal point on the [illegible] Since the myopic eye can clearly see objects clos[illegible] the far point, the spectacle lens must cast relat[illegible] nearby images of distant objects. Hence we introd[illegible] a negative lens that will diverge the rays a bit. [illegible] the temptation to suppose that we are merely re[illegible] the power of the system. In point of fact, the po[illegible] the lens–eye combination is most often made t[illegible] that of the unaided eye. If you are wearing gl[illegible] correct myopia, take them off; the world gets [illegible] but it doesn't change size. Try casting a real im[illegible] a piece of paper using your glasses—it can't b[illegible]

Suppose an eye has a far point of 2 m. [illegible] well if the spectacle lens appeared to bring more [illegible] objects in closer than 2 m. If the virtual image [illegible] object at infinity is formed by a concave lens at 2 [illegible] eye will see the object clearly with an unaccom[illegible] lens. Thus using the thin-lens approximation [illegible] are generally thin to reduce weight and bulk), [illegible]

$$\frac{1}{f} = \frac{1}{s_o} + \frac{1}{s_i} = \frac{1}{\infty} + \frac{1}{-2},$$

and $f = -2$ m while $\mathcal{D} = -\frac{1}{2}$ D. Notice that the [illegible] distance, measured from the correction lens, [illegible] focal length (Fig. 5.84). The eye views the righ[illegible] virtual images of all objects formed by the correc[illegible] lens, and those images are located between its far [illegible] near points. Incidentally, the near point also [illegible] away a little, which is why myopes often pre[illegible] to remove their spectacles when threading need[illegible] or reading small print; they can then bring the ma[illegible] closer to the eye, thereby increasing the magnific[illegible]

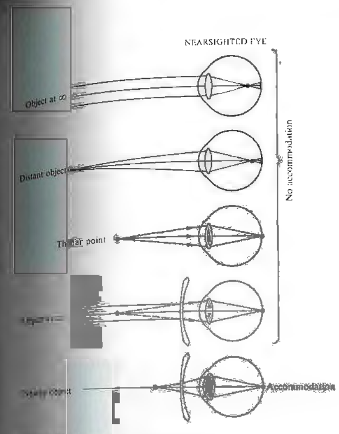


Figure 5.83 Correction of the nearsighted eye.

The calculation we have just performed overlooks [illegible] separation between the correction lens and the [illegible] effect it applies to contact lenses more than to [illegible]ectacles. The separation is usually made equal to the [illegible]stance of the first focal point of the eye (≈16 mm) [illegible] cornea, so that no magnification of the image [illegible] that of the unaided eye occurs. Many people have [illegible] eyes, yet both yield the same magnification. A [illegible] M_T for one and not the other would be a disast[illegible] Placing the correcting lens at the eye's first focal [illegible] avoids the problem completely, regardless [illegible] power of that lens [take a look at Eq. (6.8)]. To [illegible] just draw a ray from the top of some object [illegible] that focal point. The ray will enter the eye [illegible] it parallel to the optic axis, thus establishing [illegible] of the image. Yet, since this ray is unaffected [illegible]ence of the spectacle lens whose center is at

the focal point, the image's location may change on insertion of such a lens, but its height and therefore M_T will not (see Eq. 5.24).

The question now becomes: What is the equivalent power of a spectacle lens at some distance d from the eye (i.e., equivalent to that of a contact lens with a focal length f_c that equals the far-point distance). It will do for our purposes to approximate the eye by a single lens and take d from that lens to the spectacle as roughly equal to the cornea–eyeglass distance, usually around 16 mm. Given that the focal length of the correction lens is f_l and the focal length of the eye is f_e, the combination has a focal length provided by Eq. (5.36), that is,

$$\text{b.f.l.} = \frac{f_e(d - f_l)}{d - (f_l + f_e)}. \qquad (5.72)$$

This is the distance from the eye-lens to the retina. Similarly, the equivalent contact lens combined with the eye-lens has a focal length given by Eq. (5.38):

$$\frac{1}{f} = \frac{1}{f_c} + \frac{1}{f_e}, \qquad (5.73)$$

where f = b.f.l. Inverting Eq. (5.72), setting it equal to Eq. (5.73), and simplifying, we obtain the result $1/f_c = 1/(f_l - d)$, independent of the eye itself. In terms of power,

$$\mathcal{D}_c = \frac{\mathcal{D}_l}{1 - \mathcal{D}_l d}. \qquad (5.74)$$

A spectacle lens of power $\mathcal{D}_l$ a distance d from the eye-lens has an effective power the same as that of a contact lens of power $\mathcal{D}_c$. Notice that since d is measured in meters and thus is quite small, unless $\mathcal{D}_l$ is large, as

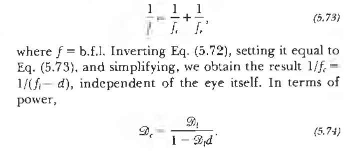


Figure 5.84 The far-point distance equals the focal length of the correction lens.

it often is, $\mathscr{D}_c \approx \mathscr{D}_l$. Usually, the point on your nose where you choose to rest your eyeglasses has little effect, but that's certainly not always the case—an improper value of d has resulted in many a headache.

ii) Farsightedness—Positive Lenses

Hyperopia (or *hypermetropia*) is the defect that causes the second focal point of the unaccommodated eye to lie behind the retina (Fig. 5.85). *Farsightedness*, as you might have guessed it would be called, is often due to a shortening of the anteroposterior axis of the eye—the lens is too close to the retina. To increase the bending of the rays, a positive spectacle lens is placed in front of the eye. The hyperopic eye can and must accommodate to see distant objects distinctly, but it will be at its limit to do so for a near point, which is much farther away than it would be normally (this we take as 25 cm). It will consequently be unable to see clearly. A converging corrective lens with positive power will effectively move a close object out beyond the near point where the eye has adequate acuity, that is, it will form a distant virtual image, which the eye can then see clearly. Suppose that a hyperopic eye has a near point of 125 cm. For an object at +25 cm to have its image at $s_i = -125$ cm so that it can be seen as if through a normal eye, the focal length must be

$$\frac{1}{f} = \frac{1}{(-1.25)} + \frac{1}{0.25} = \frac{1}{0.31},$$

or $f = 0.31$ m and $\mathscr{D} = +3.2$ D. This is in accord with Table 5.3, where $s_o < f$. These spectacles will cast real images—try it if you're hyperopic.

As shown in Fig. 5.86, the correcting lens allows the relaxed eye to view objects at infinity. In effect, it creates an image on its focal "plane," which then serves as a virtual object for the eye. The focus (whose image lies on the retina) is once again the *far point*, and it's a distance f_l *behind* the lens. The hyperope can comfortably "see" the far point, and any lens located anywhere in front of the eye that has an appropriate focal length will serve that purpose.

Very gentle finger pressure on the lids above and below the cornea will temporarily distort it, changing your vision from blurred to clear and vice versa.

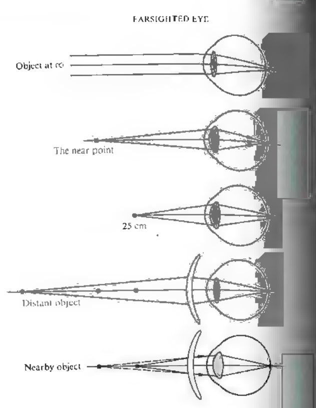


Figure 5.85 Correction of the farsighted eye.

iii) Astigmatism—Anamorphic Lenses

Perhaps the most common eye defect is ***astigmatism***. It arises from an uneven curvature of the cornea. In other words, the cornea is asymmetric. Suppose we pass two meridional planes (ones containing the optic axis)

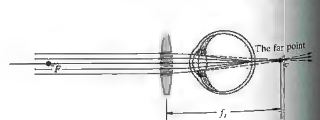


Figure 5.86 Again the far-point distance equals the focal length of the correction lens.

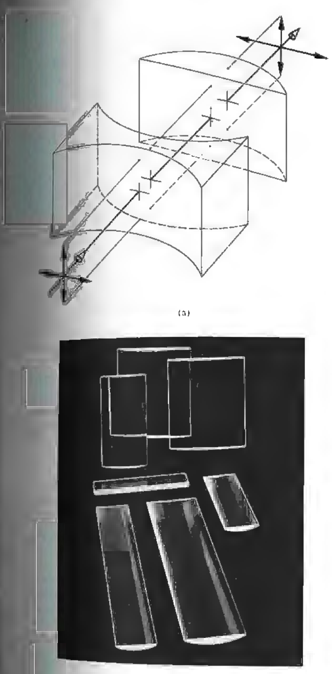


Figure 5.87 (a) Anamorphic optics. (b) Cylindrical lenses. (Photo courtesy Melles Griot.)

through the eye such that the (curvature or) power is maximal on one and minimal on the other. If these planes are perpendicular, the *astigmatism* is *regular* and correctible; if not, it is *irregular* and not easily corrected. Regular astigmatism can take different forms; the eye can be emmetropic, myopic, or hyperopic in various combinations and degrees on the two perpendicular meridional planes. Thus, as a simple example, the columns of a checker board might be well focused while the rows are blurred due to myopia or hyperopia. Obviously these meridional planes need not be horizontal and vertical.

The great astronomer Sir George B. Airy used a concave sphero-cylindrical lens to ameliorate his own myopic astigmatism in 1825. This was probably the first time astigmatism had been corrected. But it was not until the publication in 1862 of a treatise on cylindrical lenses and astigmatism by the Dutchman Franciscus Cornelius Donders (1818–1889) that ophthalmologists were moved to adopt the method on a large scale.

Any optical system that has a different value of M_T or $\mathscr{D}$ in two principal meridians is said to be *anamorphic*. Thus, for example, if we rebuilt the system depicted in Fig. 5.31, this time using cylindrical lenses (Fig. 5.87), the image would be distorted, having been magnified in only one plane. This is just the sort of distortion needed to correct for astigmatism when a defect exists in only one meridian. An appropriate planar cylindrical spectacle lens, either positive or negative, would restore essentially normal vision. When both perpendicular meridians require correction, the lens may be *sphero-cylindrical* or even *toric* as in Fig. (5.88).

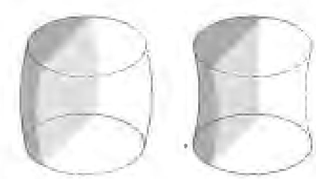


Figure 5.88 Toric surfaces.

Just as an aside, we note that anamorphic lenses are used in other areas, as for example, in the making of wide-screen motion pictures, where an extra-large horizontal field of view is compacted onto the regular film format. When shown through a special lens the distorted picture spreads out again. On occasion a television station will show short excerpts without the special lens—you may have seen the weirdly elongated result.

5.7.3 The Magnifying Glass

An observer can cause an object to appear larger, for the purpose of examining it in detail, by simply bringing it closer to her eye. As the object is brought nearer and nearer, its retinal image increases, remaining in focus until the crystalline lens can no longer provide adequate accommodation. Should the object come closer than this *near point*, the image will blur (Fig. 5.89). A single positive lens can be used, in effect to add refractive power to the eye, so that the object can be brought still closer and yet be in focus. The lens so used is referred to variously as a *magnifying glass*, a *simple magnifier*, or a *simple microscope*. In any event, its function is *to provide an image of a nearby object that is larger than the image seen by the unaided eye*. Devices of this sort have been around for a long time. In fact, a quartz convex lens ($f \approx 10$ cm), which may have served as a magnifier, was unearthed in 1885 among the ruins of the palace of King Sennacherib (705–681 B.C.) of Assyria.

Evidently, it would be desirable for the lens to form a magnified, erect image. Furthermore, the rays entering the normal eye should not be converging. Table 5.3 (p. 145) immediately suggests placing the object within the focal length (i.e., $s_o < f$). The result is shown in Fig. 5.90. Because of the relatively tiny size of the eye's pupil, it will almost certainly always be the aperture stop, and as in Fig. 5.33 (p. 150), it will also be the exit pupil.

The *magnifying power, MP,* or equivalently, the *angular magnification,* M_A, of a visual instrument is defined as *the ratio of the size of the retinal image as seen through the instrument over the size of the retinal image as seen by the unaided eye at normal viewing distance.* The latter is generally taken as the distance to the near point,

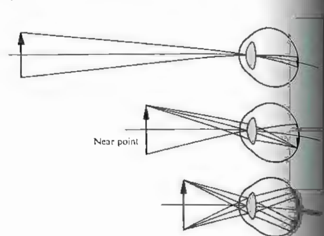


Figure 5.89 Images in relation to the near point.

d_o. The ratio of angles α_a and α_u (which are mad[redacted] chief rays from the top of the object in the instanc[redacted] the aided and unaided eye, respectively) is equiva[redacted] to MP, that is,

$$\mathrm{MP} = \frac{\alpha_a}{\alpha_u}. \qquad (5.76)$$

Keeping in mind that we are restricted to the parax[redacted] region, $\tan\alpha_a = y_i/L \approx \alpha_a$ and $\tan\alpha_u = y_o/d_o \approx \alpha_u$,

$$\mathrm{MP} = \frac{y_i d_o}{y_o L},$$

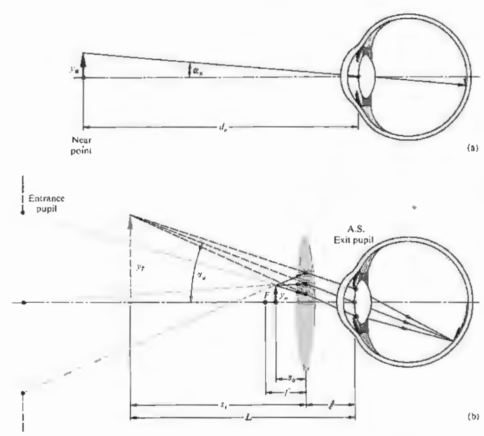
wherein y_i and y_o are above the axis and positive[redacted] make d_o and L positive quantities, MP will be pos[redacted] which is quite reasonable. When we use Eqs. (5.24) a[redacted] (5.25) for M_T along with the thin-lens equatio[redacted] the expression becomes

$$\mathrm{MP} = -\frac{s_i d_o}{s_o L} = \left(1 - \frac{s_i}{f}\right)\frac{d_o}{L}.$$

Inasmuch as the image distance is negativ[redacted] $s_i = -(L - \ell)$, and consequently,

$$\mathrm{MP} = \frac{d_o}{L}[1 + \mathscr{D}(L - \ell)],$$

$\mathscr{D}$ of course being the power of the magnifie[redacted] There are three situations of particular inter[redacted]



[redacted] the magnifying power equals $d_o\mathscr{D}$. (2) When [redacted]ly zero,

$$[\mathrm{MP}]_{\ell=0} = d_o\left(\frac{1}{L} + \mathscr{D}\right).$$

In this case the largest value of MP corresponds to the smallest value of L, which, if vision is to be clear, must equal d_o. Thus

$$[\mathrm{MP}]_{\substack{\ell=0\\ L=d_o}} = d_o\mathscr{D} + 1. \qquad (5.77)$$

Taking $d_o = 0.25$ m for the standard observer, we have

$$[\mathrm{MP}]_{\substack{\ell=0\\ L=d_o}} = 0.25\mathscr{D} + 1. \qquad (5.78)$$

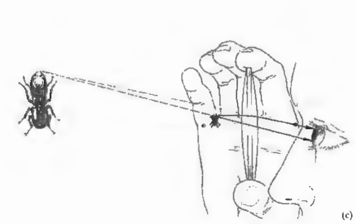


Figure 5.90 (a) An unaided view of an object. (b) The aided view through a magnifying glass. (c) A positive lens used as a magnifying glass. The object is less than one focal length from the lens.

As L increases, MP decreases, and similarly as ℓ increases, MP decreases. If the eye is very far from the lens, the retinal image will indeed be small. (3) This last is perhaps the most common situation. Here we position the object at the focal point ($s_o = f$), in which case the virtual image is at infinity ($L = \infty$). Thus from Eq. (5.76)

$$[\mathrm{MP}]_{L=\infty} = d_o \mathscr{D} \tag{5.79}$$

for all practical values of ℓ. Because the rays are parallel, the eye views the scene in a relaxed, unaccommodated configuration, a highly desirable feature. Notice that $M_T = -s_i/s_o$ approaches infinity as $s_o \to f$, whereas in marked contrast, M_A merely decreases by 1 under the same circumstances.

A magnifier with a power of 10 D has a focal length ($1/\mathscr{D}$) of 0.1 m and a MP equal to 2.5 when $L = \infty$. This is conventionally denoted as 2.5×, which means that the retinal image is 2.5 times larger with the object at the focal length of the lens than it would be were the object at the near point of the unaided eye (where the largest clear image is possible). The simplest single-lens magnifiers are limited by aberrations to roughly 2× or 3×. A large field of view generally implies a large lens, for practical reasons usually dictates a fairly small curvature of the surfaces. The radii are large, as is f, and therefore MP is small. The reading glass, the kind Sherlock Holmes made famous, is a typical example. The watchmaker's eye loupe is frequently a single-element lens, also of about 2× or 3×. Figure 5.91 shows a few more complicated magnifiers designed to operate in the range from roughly 10× to 20×. The double lens is quite common in a number of configurations. Although not particularly good, they perform satisfactorily, for example, in high-powered loupes. The Coddington is essentially a sphere with a slot cut in it to allow an aperture smaller than the pupil of the eye. A clear marble (any small sphere of glass qualifies) will also greatly magnify—but not without a good deal of distortion.

The relative refractive index of a lens and the medium in which it is immersed, n_{lm}, is wavelength dependent. But since the focal length of a simple lens varies with $n_{lm}(\lambda)$, this means that f is a function of wavelength, and the constituent colors of white light will focus at different points in space. The resultant defect is known

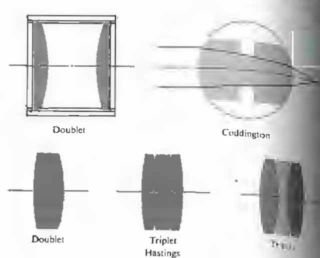


Figure 5.91 Magnifiers.

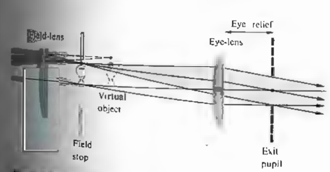
as *chromatic aberration*. In order that the image be fre[illegible] of this coloration, positive and negative lenses made [illegible] different glasses are combined to form *achromates* [illegible] Section 6.3.2). Achromatic, cemented, doublet, and triplet lenses are comparatively expensive and are usually found in small, highly corrected, high-po[illegible] magnifiers.

5.7.4 Eyepieces

The *eyepiece*, or *ocular*, is a visual optical instrum[illegible] Fundamentally a magnifier, it views not an actual [illegible] but the intermediate image of that object as for[illegible] a preceding lens system. In effect, the eye looks [illegible] the ocular, and the ocular looks into the optical sy[illegible] be it a spotting scope, compound microscope, te[illegible] or binocular. A single lens could serve the purp[illegible] poorly. If the retinal image is to be more satis[illegible] the ocular cannot have extensive aberrations. [illegible] piece of a special instrument, however, might [illegible] signed as part of the complete system, so that [illegible] can be utilized in the overall scheme to balanc[illegible] aberrations. Even so, standard eyepieces are use[illegible] changeably on most telescopes and compound [illegible] scopes. Moreover, eyepieces are quite difficult to [illegible] and the [illegible], and perhaps most fruitful, approach is to incorporate or slightly modify one of the existing designs.

The ocular must provide a virtual image (of the intermediate image), most often located at or near infinity, so that it can be comfortably viewed by a normal, relaxed eye. Furthermore, it must position the center of the exit [illegible] or *eye point* at which the observer's eye is placed at some convenient location, preferably at least 10 mm or so from the last surface. As before, ocular mag[illegible] is the product $d_o\mathscr{D}$, or as it is often written, MP = (250 mm)/f.

The **Huygens** ocular, which dates back over 250 years, is still in wide use today (Fig. 5.92), particularly [illegible]microscopy. The lens adjacent to the eye is known [illegible] *eye-lens*, and the first lens in the ocular is the [illegible]*lens*. The distance from the eye-lens to the eye point [illegible]own as the *eye relief*, and for the Huygens ocular, [illegible] uncomfortable 3 mm or so. Notice that this [illegible] requires the incoming rays to be converging so [illegible] a virtual object for the eye-lens. Clearly then, [illegible]ens eyepiece cannot be used as an ordinary [illegible] Its contemporary appeal rests in its low purchase price (see Section 6.3.2). Another old standby is [illegible]den eyepiece (Fig. 5.93). This time the prin[illegible] is in front of the field-lens, so the intermedi[illegible] will appear there in easy access. This is where you wo[illegible] place a *reticle* (or *reticule*), which might contain a set of cross hairs, precision scales, or angularly divided circular grids. (When these are formed on a [illegible] plate, they are often called *graticules*.) Since [illegible] and intermediate image are in the same



[illegible] Huygens eyepiece.

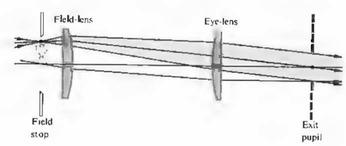


Figure 5.93 The Ramsden eyepiece.

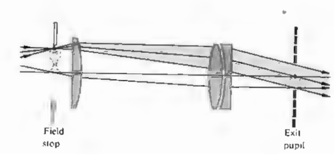


Figure 5.94 The Kellner eyepiece.

plane, both will be in focus at the same time. The roughly 12-mm eye relief is an advantage over the previous ocular. The Ramsden is relatively popular and fairly inexpensive (see Problem 6.2). The **Kellner** eyepiece represents a definite increase in image quality, although eye relief is between that of the previous two devices. The Kellner is essentially an achromatized Ramsden (Fig. 5.94). It is most commonly used in moderately wide-field telescopic instruments. The **orthoscopic** eyepiece (Fig. 5.95) has a wide field, high magnification, and long eye relief (≈20 mm). The **symmetrical (Plössl)** eyepiece (Fig. 5.96) has characteristics similar to those of the orthoscopic ocular but is generally somewhat superior to it. The **Erfle** (Fig. 5.97) is probably the most common wide-field (roughly ±30°) eyepiece. It is well corrected for all aberrations and comparatively expensive.*

* Detailed designs of these and other oculars can be found in the *Military Standardization Handbook—Optical Design*, MIL-HDBK-141.

Although there are many other eyepieces, including variable-power *zoom* devices and ones with aspherical surfaces, those discussed above are representative. They are the ones you will ordinarily find on telescopes and microscopes and on long lists in the commercial catalogs.

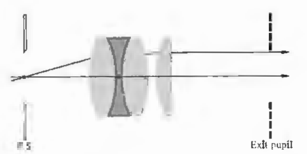


Figure 5.95 The orthoscopic eyepiece.

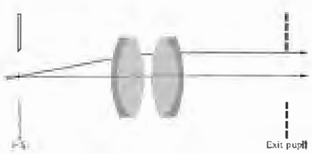


Figure 5.96 The symmetrical (Plössl) eyepiece.

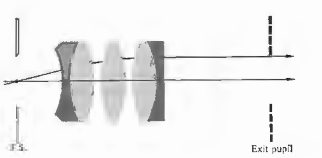


Figure 5.97 The Erfle eyepiece.

5.7.5 The Compound Microscope

The compound microscope goes a step beyond the simple magnifier by providing higher angular [illegible] nification (greater than about 30×) of *nearby* obje[illegible] invention, which may have occurred as early as [illegible] is generally attributed to a Dutch spectacle mak[illegible] Zacharias Janssen of Middleburg. Galileo runs a [illegible] second, having announced his invention of a co[illegible] microscope in 1610. A simple version, which is c[illegible] to these earliest devices than it is to a modern labora[illegible] microscope, is depicted in Fig. 5.98. The lens sy[illegible] here a singlet, closest to the object is referred to [illegible] **objective.** It forms a real, inverted, and usually [illegible] nified image of the object. This image resides in [illegible] on the plane of the field stop of the eyepiece. [illegible] diverging from each point of this image will eme[illegible] from the eye-lens (which in this simple case is the [illegible] piece itself) parallel to each other, as noted in the [illegible] vious section. The ocular magnifies this interme[illegible] image still further. Thus the magnifying power of the entire system is the product of the transverse linear magnification of the objective, M_{To}, and the angu[illegible] magnification of the eyepiece, M_{Ae}, that is,

$$MP = M_{To}M_{Ae}. \qquad (5.80)$$

Recall that $M_T = -x_i/f$, Eq. (5.26). With this in mind most, but not all, manufacturers design their micro-scopes such that the distance (corresponding to x_i) from the second focus of the objective to the first focus of the eyepiece is standardized at 160 mm. This distance, known as the *tube length*, is denoted by L in the figure. (Some authors define tube length as the image distance of the objective.) Hence, with the final image at infinity and the standard near point taken as 10 inches (254 mm),

$$MP = \left(-\frac{160}{f_o}\right)\left(\frac{254}{f_e}\right), \qquad (5.81)$$

and the image is inverted (MP < 0). According[illegible] barrel of an objective with a focal length f_o o[illegible] 32 mm will be engraved with the marking 5× [illegible] indicating a power of 5. Combined with a 10× e[illegible] (f_e = 1 inch), the microscope MP would then be [illegible]

To maintain the distance relationships [illegible] objective, field stop, and ocular, while a fo[illegible]

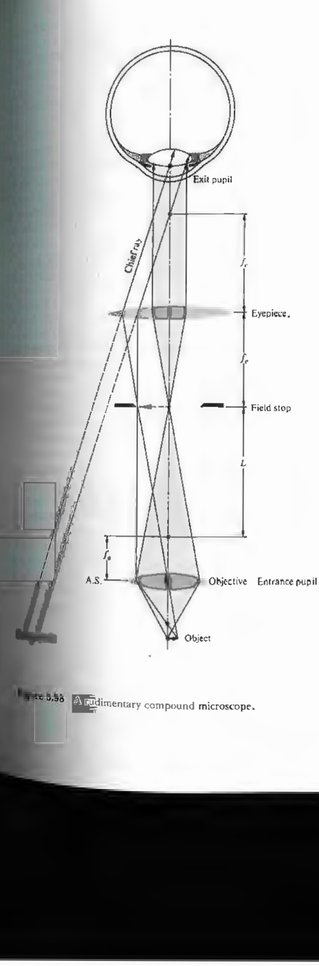


Figure 5.98 A rudimentary compound microscope.

mediate image of the object is positioned in the first focal plane of the eyepiece, all three elements are moved as a single unit.

The objective itself functions as the aperture stop and entrance pupil. Its image, formed by the eyepiece, is the exit pupil into which the eye is positioned. The field stop, which limits the extent of the largest object that can be viewed, is fabricated as part of the ocular. The image of the field stop formed by the optical elements following it is called the *exit window*, and the image formed by the optical elements preceding it is the *entrance window*. The cone angle subtended at the center of the exit pupil by the periphery of the exit window is said to be the *angular field of view in image space*.

A modern microscope objective can be roughly classified as one of three different kinds. It might be designed to work best with the object positioned below a cover glass, with no cover glass (metallurgical instruments), or with the object immersed in a liquid that is in contact with the objective. In some cases, the distinction is not critical, and the objective may be used with or without a cover glass. Four representative objectives are shown in Fig. 5.99 (see Section 6.3.1). In addition, the ordinary low-power (about 5×) cemented doublet achromate is quite common. Relatively inexpensive medium-power (10× or 20×) achromatic objectives, because of their short focal lengths, can conveniently be used when expanding and spatially filtering laser-beams.

There is one other characteristic quantity of importance, which must be mentioned here even if only briefly. The brightness of the image is, in part, dependent on the amount of light gathered in by the objective. The *f-number* is a useful parameter for describing this quantity, particularly when the object is a distant one (see Section 5.3.3). However, for an instrument working at *finite conjugates* (s_i and s_o both finite), the numerical aperture, NA, is more appropriate (see Section 5.6). In the present instance

$$NA = n_o \sin\theta_{max}, \qquad (5.82)$$

where n_o is the refractive index of the immersing medium (air, oil, water, etc.) adjacent to the objective lens, and θ_{max} is the half-angle of the maximum cone of light picked up by that lens [Fig. 5.99(b)]. In other

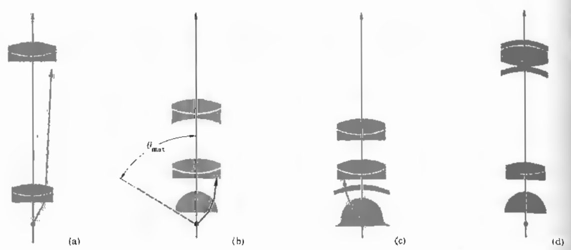


Figure 5.99 Microscope objectives: (a) Lister objective, 10 ×, NA = 0.25, f = 16 mm (two cemented achromats). (b) Amici objective, from 20 ×, NA = 0.5, f = 8 mm to 40 ×, NA = 0.8, f = 4 mm. (c) Oil-immersion objective, 100 ×, NA = 1.3, f = 1.6 mm (see Figu... (d) Apochromatic objective, 55 ×, NA ≈ 0.95, f = 3.2 (cont... fluorite lenses).

words, θ_{max} is the angle made by a marginal ray with the axis. The numerical aperture is usually the second number etched in the barrel of the objective. It ranges from about 0.07 for low-power objectives to 1.4 or so for high-power (100×) ones. Of course, if the object is in the air, the numerical aperture cannot be greater than 1.0. Incidentally, Ernst Abbe (1840–1905), while working in the Carl Zeiss microscope workshop, introduced the concept of the numerical aperture. It was he who recognized that the minimum transverse distance between two object points that can be resolved in the image, that is, the *resolving power*, varied directly as λ and inversely as the NA.

5.7.6 The Telescope

It is not at all clear who actually invented the telescope. In point of fact, it was probably invented and reinvented many times. Recall that by the seventeenth century spectacle lenses had been in use in Europe for about three hundred years. During that long span of time, the fortuitous juxtapositioning of two appropriate lenses to form a telescope seems almost inevitable. In any event, it is most likely that a Dutch optician, p... even the ubiquitous Zacharias Jenssen of mic... fame, first constructed a telescope and in additi... inklings of the value of what he was peering in... earliest indisputable evidence of the discovery, ... dates to October 2, 1608, when Hans Lippersh... tioned the States-General of Holland for a pat... device for seeing at a distance (which is what ... means in Greek). Incidentally, as you might... guessed, its military possibilities were immediately... ognized. His patent was therefore not granted; ... the government purchased the rights to the inst... and he received a commission to continue resear... Galileo heard of this work, and by 1609 he had f... ioned a telescope of his own, using two lenses an... organ pipe as a tube. It was not long before he... constructed a number of greatly improved instrum... and was astounding the world with the astronom... discoveries for which he is famous.

i) Refracting Telescopes

A simple *astronomical* telescope is shown in Fig... Unlike the compound microscope, which it ...

...sembles, its primary function is to enlarge the retinal ... distant object. In the illustration, the object ...ar distance from the objective, so that the ...diate image is formed just beyond its second ... This image will be the object for the next ...stem, that is, the ocular. It follows from Table ...145) that if the eyepiece is to form a virtual ...ified final image (within the range of normal ...modation), the object distance must be less than ... to the focal length, f_e. In practice, *the position ... intermediate image is fixed, and only the eyepiece is ... focus the instrument.* Notice that *the final image ...* but as long as the scope is used for astronomi...ons, this is of little consequence, especially ... work is photographic.

At great object distances the incident rays are ...ectively parallel—the intermediate image resides at the second focus of the objective. Usually the eyepiece ... so that its first focus overlaps the second focus ... the objective, in which case rays diverging from a ...int on the intermediate image will leave the ocular ...rallel to each other. A normal viewing eye can then focus the rays in a relaxed configuration. If the eye is nearsighted or farsighted, the ocular can be moved in or out so that the rays diverge or converge a bit to compensate. (If you are astigmatic, you'll have to keep your glasses on when using ordinary visual instruments.) We saw earlier (Section 5.2.3) that both the back and front focal lengths of a thin-lens combination go to infinity when the two lenses are separated by a distance d equal to the sum of their focal lengths (Fig. 5.101). The astronomical telescope in this configuration of *infinite conjugates* is said to be *afocal*, that is, without a focal length. As a side note, if you shine a collimated (parallel rays, i.e., plane waves) narrow laserbeam into the back end of a scope focused at infinity, it will emerge still collimated but with an increased cross-section. It is often desirable to have a broad, quasimonochromatic, plane-wave beam, and specific devices of this sort are now available commercially.

The periphery of the objective is the aperture stop, and it encompasses the entrance pupil as well, there being no lenses to the left of it. If the telescope is trained directly on some distant galaxy, the visual axis of the

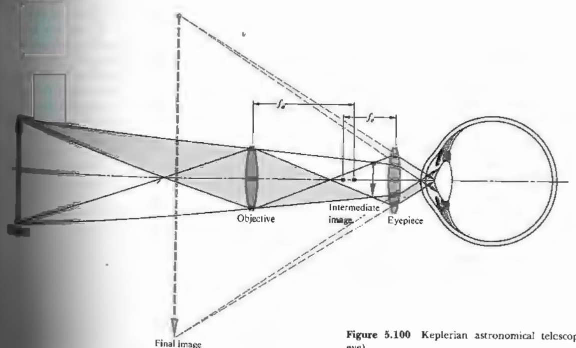


Figure 5.100 Keplerian astronomical telescope (accommodating eye).

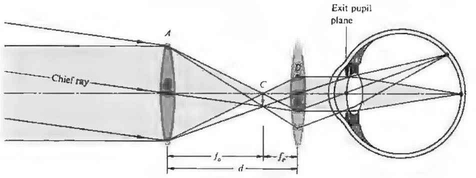


Figure 5.101 Astronomical ... infinite conjugates.

eye will presumably be collinear with the central axis of the scope. The entrance pupil of the eye should then coincide in space with the exit pupil of the scope. However, the eye is not immobile. It will move about scanning the entire field of view, which quite often contains many points of interest. In effect, the eye examines different regions of the field by rotating so that rays from a particular area fall on the fovea centralis. The direction established by the chief ray through the center of the entrance pupil to the fovea centralis is the *primary line of sight.* The axial point, fixed in reference to the head, through which the primary line of sight always passes, regardless of the orientation of the eyeball, is called the *sighting intersect.* When it is desirable to have the eye surveying the field, the sighting intersect should be positioned at the center of the telescope's exit pupil. In that case, the primary line of sight will always correspond to a chief ray through the center of the exit pupil, however the eye moves.

Suppose that the margin of the visible object ... a half-angle of α at the objective (Fig. 5.102) ... essentially the same as the angle α_u, which ... subtended at the unaided eye. As in previous ... the angular magnification is

$$\mathrm{MP} = \frac{\alpha_a}{\alpha_u}.$$

Here α_u and α_a are measures of the field of view ... object and image space, respectively. The first is ... half-angle of the actual cone of rays collected, a... second relates to the apparent cone of rays. I... arrives at the objective with a negative slope, it will ... the eye with a positive slope and vice versa. To ... the sign of MP positive for erect images, and the... consistent with previous usage (Fig. 5.90), eith... α_a must be taken to be negative—we choose the...

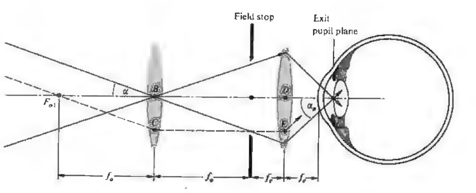


Figure 5.102 Ray angles ...

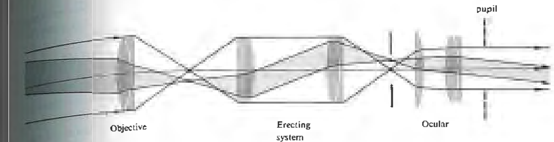


Figure 5.103 A terrestrial telescope.

...ray has a negative slope. Observe that the ... through the first focus of the objective passes ... second focus of the eyepiece, that is, F_{o1} ... conjugate points. In the paraxial approximation $\alpha \approx \alpha_u \approx \tan \alpha_u$ and $\alpha_a \approx \tan \alpha_a$. The image fills ...ion of the field stop, and half its extent equals ...tance $\overline{BC} = \overline{DE}$. Thus, from triangles $F_{o1}BC$ and ... the ratio of the tangents yields

$$\mathrm{MP} = -\frac{f_o}{f_e}. \tag{5.83}$$

Another ...venient expression for the MP comes from ... the transverse magnification of the ocular, ...uch as the exit pupil is the image of the objective ...102), we have

$$M_{Te} = -\frac{f_e}{x_o} = -\frac{f_e}{f_o}.$$

...thermore, if D_o is the *diameter of the objective* and ... *diameter of its image, the exit pupil,* then $M_{Te} =$ ...ese two expressions for M_{Te} compared with ... yield

$$\mathrm{MP} = \frac{D_o}{D_{ep}}. \tag{5.84}$$

...ctually a negative quantity, since the image ... is an easy matter to build a simple refract... by holding a lens with a long focal length in ...one with a short focal length and making sure ... $f_o + f_e$. But again, well-corrected telescopic ... generally have multielement objectives, ...ually ...lets or triplets.

To be useful when the orientation of the object is of importance, a scope must contain an additional *erecting system*—such an arrangement is known as a *terrestrial telescope.* A single erecting lens or lens system is usually located between the ocular and objective, with the result that the image is right side up. Figure 5.103 shows one with a cemented doublet objective and a Kellner eyepiece. It will obviously have to have a long draw tube, the picturesque kind that comes to mind when you think of wooden ships and cannonballs.

For that reason, *binoculars* (binocular telescopes) generally utilize erecting prisms, which accomplish the same thing in less space and also increase the separation of

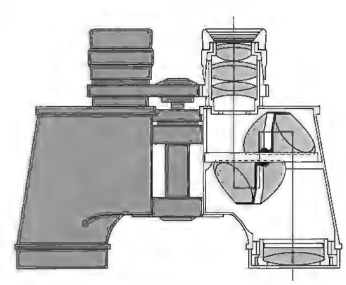


Figure 5.104 A binocular.

the objectives, thereby enhancing the stereoscopic effect. Most often these are double Porro prisms, as in Fig. 5.104 (notice the involved modified Erfle eyepiece, the wide field stop, and the achromatic doublet objective). Binoculars customarily bear several numerical markings, for example, 6 × 30, 7 × 50, or 20 × 50. The initial number is the magnification, here 6×, 7×, or 20×. The second number is the entrance-pupil diameter or, equivalently, the clear aperture of the objective, expressed in millimeters. It follows from Eq. (5.84) that the exit-pupil diameter will be the second number divided by the first, or in this case 5, 7.1, and 2.5, all in millimeters. You can hold the instrument away from your eye and see the bright circular exit pupil surrounded by blackness. To measure it, focus the device at

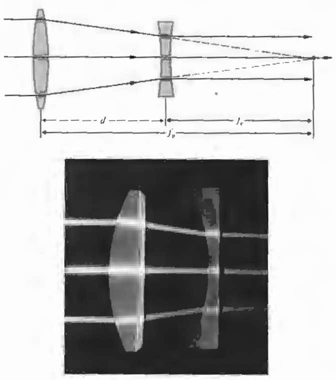


Figure 5.105 The Galilean telescope. Galileo's first scope had a planar-convex objective (5.6 cm in diameter, $f = 1.7$ m, $R = 93.5$ cm) and a planar-concave eyepiece, both of which he ground himself. It was 3× in contrast to his last scope, which was 32×. (Photo by E.H.)

infinity, point it at the sky, and observe the emergi[illegible] sharp disk of light, using a piece of paper [illegible] Determine the eye relief while you're at it.

By the way, as long as $d = f_o + f_e$, the scope [illegible] afocal, even if the eyepiece is negative (i.e., $f_e <$ [illegible] telescope built by Galileo (Fig. 5.105) had jus[illegible] negative lens as an eyepiece and therefore form[illegible] erect image [$f_e < 0$ and MP > 0 in Eq. (5.83)[illegible] telescope, the system is now mainly of histo[illegible] pedagogical interest, although one can still [illegible] two such scopes mounted side by side to form a [illegible] field glass. It is quite useful, however, as a laser [illegible] expander, because it has no internal focal points [illegible] a high power beam would otherwise ionize the [illegible] rounding air.

ii) Reflecting Telescopes

The difficulties inherent in making large lenses ar[illegible] underscored when we note that the largest [illegible] instrument is the 40-inch Yerkes telescope in Wil[illegible] Bay, Wisconsin, whereas the reflector on Mou[illegible] Palomar in southwestern California is 200 [illegible] diameter, and the Soviet Union has a 236-inch [illegible] at their Crimea Observatory. The [illegible] a lens must be transparent and free of internal [illegible] etc. A front-surfaced mirror obviously need no[illegible] indeed it need not even be transparent. A lens [illegible] supported only by its rim and may sag under [illegible] weight; a mirror can be supported by its rim [illegible] as well. Furthermore, since there is no refracti[illegible] therefore no effect on the focal length due [illegible] wavelength dependence of the index, mirrors [illegible] chromatic aberration. For these and other reaso[illegible] their frequency response), reflectors predomi[illegible] large telescopes.

Invented by the Scotsman James Gregory ([illegible] 1675), in 1661, the reflecting telescope was first suc[illegible] fully constructed by Newton in 1668, and only be[illegible] an important research tool in the hands of Wi[illegible] Herschel a century later. Figure 5.106 depicts [illegible] of reflector arrangements, each having conca[illegible] boloidal primary mirrors. The 200-inch Hale tel[illegible] is so large that a little enclosure, where an observe[illegible] sit, is positioned at the prime focus. In the [illegible]

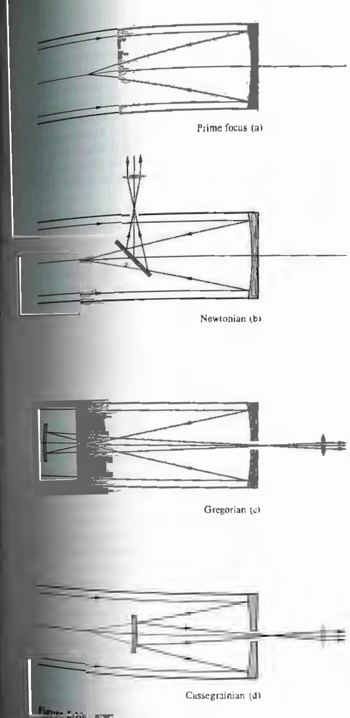


Figure 5.106 Reflecting telescopes.

version, a plane mirror or prism brings the beam out at right angles to the axis of the scope, where it can be photographed, viewed, spectrally analyzed, or photoelectrically processed. In the Gregorian arrangement, which is not particularly popular, a concave ellipsoidal secondary mirror reinverts the image, returning the beam through a hole in the primary. The Cassegrainian system utilizes a convex hyperboloidal secondary mirror to increase the effective focal length (refer back to Fig. 5.46, p. 158). It functions as if the primary mirror had the same aperture but a larger focal length or radius of curvature.

iii) Catadioptric Telescopes

A combination of reflecting (*catoptric*) and refracting (*dioptric*) elements is called a *catadioptric* system. The best known of these, although not the first, is the classic *Schmidt optical system.* We must treat it here, even if only briefly, because it represents the precursor of a new outlook in the design of large-aperture, extended-field reflecting systems. As seen in Fig. 5.107, bundles of parallel rays reflecting off a spherical mirror will form images, let's say of a field of stars, on a spherical image surface, the latter being a curved film plate in practice. The only problem with such a scheme is that although it is free of other aberrations (see Section 6.3.1), we know that rays reflected from the outer regions of the mirror will not arrive at the same focus as those from the paraxial region. In other words, the mirror is a sphere, not a paraboloid, and it suffers *spherical aberration* [Fig. 5.107(b)]. If this could be corrected, the system (in theory at least) would be capable of perfect imagery over a wide field of view. Since there is no one central axis, there are, in effect, no off-axis points. Recall that the paraboloid forms perfect images only at axial points, the image deteriorating rapidly off axis. One evening in 1929, while sailing on the Indian ocean (returning from an eclipse expedition to the Philippines), Bernhard Voldemar Schmidt (1879–1935) showed a colleague a sketch of a system he had designed to cope with the spherical aberration of a spherical mirror. He would use a thin glass corrector plate on whose surface would be ground a very shallow toroidal curve [Fig. 5.107(c)]. Light rays traversing the outer regions would

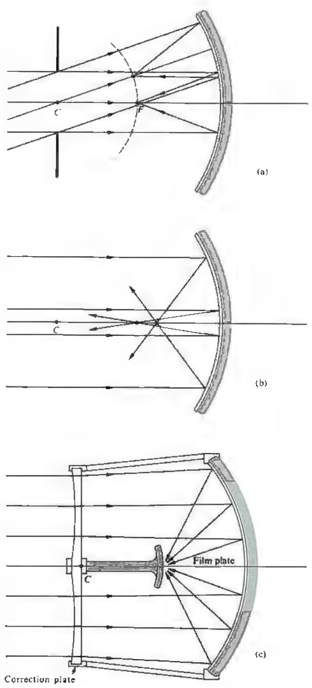


Figure 5.107 The Schmidt optical system.

be deviated by just the amount needed to be [illegible] focused on the image sphere. The corrector mu[illegible] come one defect without introducing app[illegible] amounts of other aberrations. This first system w[illegible] in 1930, and in 1949 the famous 48-inch Schmi[illegible] scope of the Palomar Observatory was complete[illegible] a fast ($f/2.5$), wide-field device, ideal for surveyi[illegible] night sky. A single photograph could encom[illegible] region the size of the bowl of the Big Dipper[illegible] compared with roughly 400 photographs by the [illegible] inch reflector to cover the same area.

Major advances in the design of catadio[illegible] instrumentation have occurred since the introdu[illegible] of the original Schmidt system.* There are no[illegible] catadioptric satellite and missile tracking instrum[illegible] meteor cameras, compact commercial telesco[illegible] telephoto objectives, and missile-homing guidance [illegible] tems. Innumerable variations on the theme exist; [illegible] replace the correcting plate with concentric men[illegible] lens arrangements (Bouwers–Maksutov), others use solid thick mirrors. One highly successful appro[illegible] utilizes a triplet aspheric lens array (Baker).

5.7.7 The Camera

The prototype of the modern photographic camer[illegible] was a device known as the *camera obscura*, the [illegible] form of which was simply a dark room with a small [illegible] in one wall. Light entering the hole cast an invert[illegible] image of the sunlit outside scene on an inside scre[illegible] The principle was known to Aristotle, and his obse[illegible] tions were preserved by Arab scholars through[illegible] Europe's long Dark Ages. Alhazen utilized it to [illegible] solar eclipses indirectly over eight hundred years [illegible] The notebooks of Leonardo da Vinci contain sever[illegible] descriptions of the obscura, but the first detailed [illegible] ment appears in *Magia naturalis* (*Natural Magi*[illegible] Giovanni della Porta. He recommended it as a dra[illegible] aid, a function to which it was soon quite popularly [illegible]

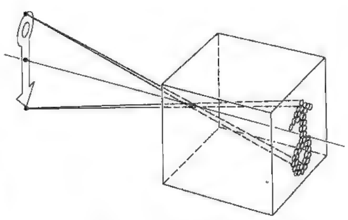
* For further reading see J. J. Villa, "Catadioptric Lenses," [illegible] *Spectra* (March/April, 1968), p. 57.
† See W. H. Price, "The Photographic Lens," *Sci. Am.* [illegible] p. 72.

Johannes Kepler, the renowned astronomer, had a portable tent version, which he used while surveying in [illegible]. By the latter part of the 1600s, the small hand-held camera obscura was commonplace. Note that the [illegible] the Nautilus, a little cuttlefish, is literally an open [illegible] obscura, which simply fills with sea water on [illegible]sion.

By replacing the viewing screen with a photosensitive [illegible], such as a film plate, the obscura becomes a [illegible] in the modern sense of the word. The first [illegible]ent photograph was made in 1826 by Joseph [illegible]hore Niépce (1765–1833), who used a box camera with a small convex lens, a sensitized pewter plate, and roughly an eight-hour exposure. It is a roof-top scene, [illegible] from the workroom window of his estate near [illegible]-sur-Saône in France. Although blurry and spotty (in its unretouched form), the large slanting roof of a barn, a pigeon house, and a distant tree are still discernible.

The lensless pinhole camera (Fig. 5.108) is by far the least [illegible]plicated device for the purpose, yet it has sever[illegible] endearing and, indeed, remarkable virtues. It can f[illegible] a well-defined, practically undistorted image of objects across an extremely wide angular field (due to great depth of focus) and over a large range of [illegible] (great depth of field). If initially the entrance [illegible] is very large, no image results. As it is decreased [illegible] diameter, the image forms and grows sharper. After [illegible] further reduction in the hole size causes the image to blur again, and one quickly finds that the aperture size for maximum sharpness is proportional [illegible] distance from the image plane. (A hole with a [illegible] diameter at 0.25 m from the film plate is con-[illegible] and works well.) There is no focusing of the [illegible] all, so no defects in that mechanism are responsible for the drop-off in clarity. The problem is actually one of diffraction, as we shall see later on (Section 10.2.5). In most practical situations, the pinhole [illegible] one overriding drawback is that it is insufferably slow (roughly $f/500$). This means that exposure [illegible] will generally be far too long, even with the most [illegible]ve films. The obvious exception is a stationary [illegible], such as a building (Fig. 5.109), for which the pinhole camera excels.

Figure 5.110 depicts the essential components of a



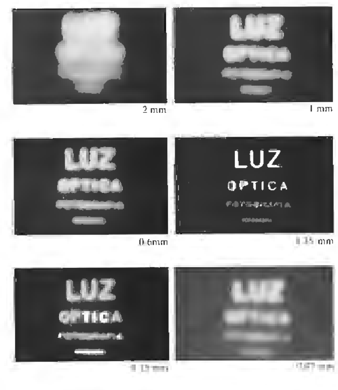


Figure 5.108 The pinhole camera. Note the variation in image clarity as the hole diameter decreases. (Photos courtesy Dr. N. Joel, UNESCO.)

Figure 5.109 Photograph taken with a pinhole camera. (Science Building, Adelphi University). Hole diameter 0.5 mm, film plane distance 24 cm, A.S.A. 3000, shutter speed 0.25 s. Note depth of field. (Photo by E.H.)

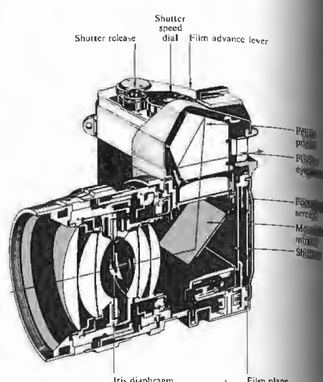


Figure 5.110 A single-lens reflex camera.

fairly popular and representative modern camera—the single-lens reflex, or SLR. Light traversing the first few elements of the lens then passes through an iris diaphragm, used in part to control the exposure time or, equivalently, the *f-number*—it is in effect a variable-aperture stop. On emerging from the lens, light strikes a movable mirror tilted at 45°, then goes up through the focusing screen to the penta prism and out the finder eyepiece. When the shutter release is pressed, the diaphragm closes down to a preset value, the mirror swings up out of the way, and the focal-plane shutter opens, exposing the film. The shutter then closes, the diaphragm opens fully, and the mirror drops back in place. Nowadays most SLR systems have any one of a number of built-in light-meter arrangements, which are automatically coupled to the diaphragm and shutter,

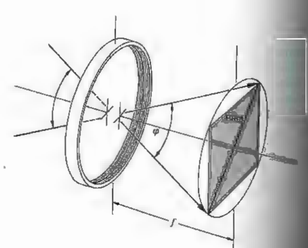


Figure 5.111 Angular field of view when focused at infinity.

[illegible] those components are excluded from the diagram for the sake of simplicity.

[illegible] the camera, the entire lens is moved toward or away from the film plane. Since its focal length is [illegible] s_o varies, so too must s_i. The *angular field of* [illegible] loosely be thought of as relating to the fraction of the scene included in the photograph. It is furthermore required that the entire photograph surface correspond to a region of satisfactory image quality. More precisely, the angle subtended at the lens, by a circle encompassing the film area, is the angular field of view φ (Fig. 5.111). As a rough but reasonable approximation of a common arrangement, take the diagonal distance across the film to equal the focal length. Thus $\varphi/2 \approx$

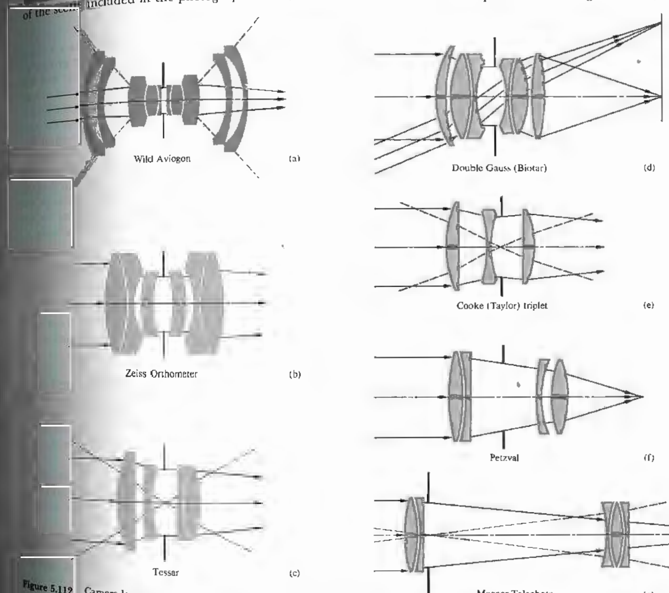


Figure 5.112 Camera lenses.

$\tan^{-1}\frac{1}{2}$, that is, $\varphi \approx 53°$. If the object comes in from infinity, s_i must increase. The lens is then backed away from the film plate to keep the image in focus, and the field of view, as recorded on the film whose periphery is the field stop, decreases. A *standard* SLR lens has a focal length in the range of about 50 to 58 mm and a field of view of 40° to 50°. With the film size kept constant, a reduction of f results in a wider field angle. Accordingly, *wide-angle* SLR lenses range from $f \approx$ 40 mm down to about 6 mm, and φ goes from about 50° to a remarkable 220° (the latter being a special-purpose lens wherein distortion is unavoidable). The *telephoto* has a long focal length, roughly 80 mm or more. Consequently, its field of view drops off rapidly, until it is only a few degrees at $f \approx 1000$ mm.

The standard photographic objective must have a large relative aperture, $1/(f/\#)$, to keep exposure times short. Moreover, the image is required to be flat and undistorted, and the lens should have a wide angular field of view as well. All of this is no mean task, and it is not surprising that a high-quality innovative photographic objective remains particularly difficult to design, even with our marvelous, mathematical, electronic *idiot savants*. The evolution of a modern lens still begins with a creative insight that leads to a promising new form. In the past, these were laboriously perfected relying on intuition, experience, and, of course trial and error with a succession of developmental lenses. Today, for the most part, the computer serves this function without the need of numerous prototypes. Many contemporary photographic objectives are variations of well-known successful forms. Figure 5.112 illustrates the general configuration of several important lenses, roughly progressing from wide angle to telephoto. Particular specifications are not given, because variations are numerous. The *Aviogon* and Zeiss *Orthometer* are wide-angle lenses, whereas the *Tessar* and *Biotar* are often standard lenses. The *Cooke triplet*, described in 1893 by H. Dennis Taylor of Cooke and Sons, is still being made (note the similarity with the Tessar). It contains the smallest number of elements by which all seven third-order aberrations can essentially be made to vanish. Even earlier (ca. 1840), Josef Max Petzval designed what was then a rapid (portrait) lens for Voightländer and Son. Its modern offshoots are

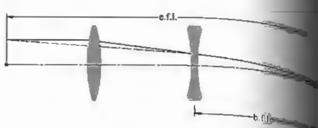


Figure 5.113 A telephoto lens.

myriad. In general, a telephoto objective has a positive front grouping and a distant negative rear group. It often resembles the Galilean scope except that the lenses are shifted a bit so that the system is not afocal. These are usually rather large and heavy at the long focal lengths, although calcium fluoride elements have begun to help in both respects. As can be seen in Fig. 5.113, the telephoto has a large effective focal length, e.f.l., that is, it behaves as if it were a positive lens with a long focal length located a large distance in front of the focal plane. Thus while the image size is large, the back focal length is conveniently short, allowing the lens to be handily slipped into a standard camera body.

PROBLEMS

5.1 We wish to construct a Cartesian oval such that the conjugate points will be separated by 11 cm when the object is 5 cm from the vertex. If $n_1 = 1$ and $n_2 =$ [illegible], draw several points on the required surface.

5.2* Figure 5.114 depicts a point source at [illegible] curved interface between two homogeneous media ($n_t > n_i$). Show that for rays to propagate in the [illegible] mitting medium as a parallel bundle, the interface [illegible] be hyperbolic with an eccentricity of (n_t/n_i) [illegible]

5.3 Diagrammatically construct an ellipto-spheric negative lens, showing the form of both rays and [illegible] fronts as they pass through the lens. Do the same [illegible] an oval-spheric positive lens.

5.4* Making use of Fig. 5.115, Snell's law, and the [illegible] that in the paraxial region $\alpha = h/s_o$, $\varphi \approx h/R$, and [illegible] h/s_i, derive Eq. (5.8).

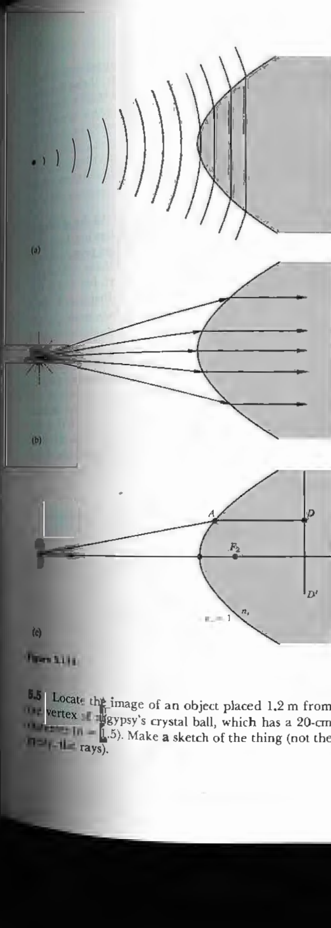


Figure 5.114

5.5 Locate the image of an object placed 1.2 m from the vertex of a gypsy's crystal ball, which has a 20-cm [illegible] ($n = 1.5$). Make a sketch of the thing (not the [illegible] rays).

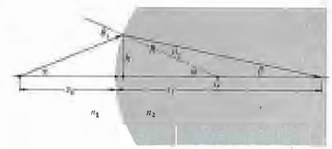


Figure 5.115

5.6 Prove that the minimum separation between conjugate *real* object and image points for a thin positive lens is $4f$.

5.7 A biconcave lens ($n_l = 1.5$) has radii of 20 cm and 10 cm and an axial thickness of 5 cm. Describe the image of an object 1-inch tall placed 8 cm from the first vertex.

5.8* Use the thin-lens equation on the previous problem to see how far off it is in determining the final-image location.

5.9 An object 2 cm high is positioned 5 cm to the right of a positive thin lens with a focal length of 10 cm. Describe the resulting image completely, using *both* the Gaussian and Newtonian equations.

5.10 Make a rough graph of the Gaussian lens equation, that is, plot s_i versus s_o, using unit intervals of f along each axis. (Get both segments of the curve.)

5.11 What must the focal length of a thin negative lens be for it to form a virtual image 50 cm away of an ant that is 100 cm away? Given that the ant is to the right of the lens, locate and describe its image.

5.12* Compute the focal length in air of a thin biconvex lens ($n_l = 1.5$) having radii of 20 and 40 cm. Locate and describe the image of an object 40 cm from the lens.

5.13 Determine the focal length of a planar-concave lens ($n_l = 1.5$) having a radius of curvature of 10 cm. What is its power in diopters?

5.14* Determine the focal length in air of a thin spherical planar-convex lens having a radius of curvature of 50.0 mm and an index of 1.50. What, if anything, would happen to the focal length if the lens were placed in a tank of water?

5.15* We wish to place an object 45 cm in front of a lens and have its image appear on a screen 90 cm behind the lens. What must be the focal length of the appropriate positive lens?

5.16 The horse in Fig. 5.27 is 2.25 m tall, and it stands with its face 15.0 m from the plane of the thin lens whose focal length is 3.00 m.

a) Determine the location of the image of the equine nose.
b) Describe the image in detail—type, orientation, and magnification.
c) How tall is the image?
d) If the horse's tail is 17.5 m from the lens, how long, nose-to-tail, is the image of the beast?

5.17* A candle that is 6.00 cm tall is standing 10 cm from a thin concave lens whose focal length is −30 cm. Determine the location of the image and describe it in detail. Draw an appropriate ray diagram.

5.18* Two positive lenses with focal lengths of 0.30 m and 0.50 m are separated by a distance of 0.20 m. A small frog rests on the central axis 0.50 m in front of the first lens. Locate the resulting image with respect to the second lens.

5.19 The image projected by an equiconvex lens (n = 1.50) of a frog 5.0 cm tall and 0.60 m from a screen is to be 25 cm high. Please compute the necessary radii of the lens.

5.20 A thin double convex glass lens (with an index of 1.56) while surrounded by air has a 10-cm focal length. If it is placed under water (having an index of 1.33) 100 cm beyond a small fish, where will the guppy's image be formed?

5.21 A homemade television projection system uses a large positive lens to cast the image of the screen onto a wall. The final picture is enlarged three [illegible] although rather dim, it's nice and clear. If the lens [illegible] a focal length of 60 cm, what should be the [illegible] between the screen and the wall? Why use a [illegible] How should we mount the set with respect [illegible]

5.22 Write an expression for the focal length [illegible] a thin lens immersed in water ($n_w = \frac{4}{3}$) in terms [illegible] focal length when it's in air (f_a).

5.23* A convenient way to measure the focal le[illegible] of a positive lens makes use of the following fact[illegible] pair of conjugate object and (real) image points [illegible] P) are separated by a distance $L > 4f$, there will b[illegible] locations of the lens, a distance d apart, for [illegible] same pair of conjugates obtain. Show that

$$f = \frac{L^2 - d^2}{4L}.$$

Note that this avoids measurements made specifi[illegible] from the vertex, which are generally not [illegible]

5.24 An equiconvex thin lens L_1 is cemented i[illegible] mate contact with a thin negative lens, L_2, such tha[illegible] combination has a focal length of 50 cm in air. [illegible] indices are 1.50 and 1.55, respectively, and [illegible] length of L_2 is −50 cm, determine all the radii [illegible] vature.

5.25 Verify Eq. (5.34), which gives M_T [illegible] tion of two thin lenses.

5.26 Compute the image location and magnifi[illegible] of an object 30 cm from the front doublet of the[illegible] lens combination in Fig. 5.116. Do the calculat[illegible] by finding the effect of each lens separately. Make [illegible] of appropriate rays.

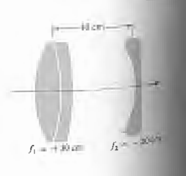


Figure 5.116

5.27* [illegible] a ray diagram for the combination of two [illegible] wherein their separation equals the sum [illegible] respective focal lengths. Do the same thing for the [illegible] one of the lenses is negative.

5.28 Redraw the ray diagram for a compound micro- [illegible] (Fig. 5.98), but this time treat the intermediate [illegible] as if it were a real object—this approach should [illegible] simpler.

5.29* Redraw the telescope in Fig. 5.101, taking advantage of the fact that the intermediate image can be [illegible] of as a real object (as in the previous [illegible]

5.30 Consider the case of two positive thin lenses, L_1 and L_2, separated by 5 cm. Their diameters are 6 and [illegible] respectively, and their focal lengths are $f_1 = 9$ cm [illegible] 3 cm. If a diaphragm with a hole 1 cm in diameter is located between them, 2 cm from L_2, find (a) [illegible] aperture stop and (b) the locations and sizes of the [illegible] for an axial point, S, 12 cm in front of (to the [illegible]) L_1.

5.31 Make a sketch roughly locating the aperture stop [illegible] and exit pupils for the lens in Fig. 5.117.

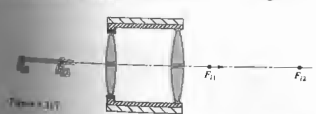


Figure 5.117

5.32 [illegible] sketch roughly locating the aperture stop and e[illegible] and exit pupils for the lens in Fig. 5.118, assum[illegible] object point to be beyond (to the left of) [illegible]

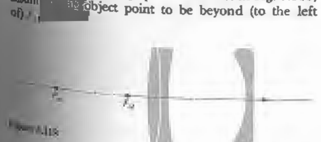


Figure 5.118

5.33 Draw a ray diagram locating the images of a point source as formed by a pair of mirrors at 90° (Fig. 5.119).

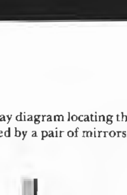


Figure 5.119

5.34* Make a sketch of a ray diagram, locating the images of the arrow shown in Fig. 5.120.

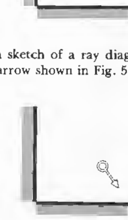


Figure 5.120

5.35 Show that Eq. (5.49) for a spherical surface is equally applicable to a plane mirror.

5.36 Locate the image of a paperclip 100 cm away from a convex spherical mirror having a radius of curvature of 80 cm.

5.37* Describe the image you would see standing 5 feet from, and looking directly toward, a brass ball 1 foot in diameter hanging in front of a pawn shop.

5.38 The image of a red rose is formed by a concave spherical mirror on a screen 100 cm away. If the rose is 25 cm from the mirror, determine its radius of curvature.

5.39 From the image configuration determine the shape of the mirror hanging on the back wall in van Eyck's painting of *John Arnolfini and His Wife* (Fig. 5.121).

Figure 5.121 Detail of *John Arnolfini and His Wife* by Jan van Eyck—National Gallery, London.

Figure 5.122 *Venus and Cupid* by Diego Rodriguez de Silva y Velásquez—National Gallery, London.

Figure 5.123 *The Bar at the Folies Bergères* by Édouard [illegible] Courtauld Institute Galleries, London.

5.40 Is Ve[illegible] in Velasquez's painting of *Venus and* [illegible] 5.122) looking at herself in the mirror? [illegible]

[illegible] in Manet's painting *The Bar at the Folies* [illegible] 5.123) is standing in front of a large planar [illegible] in it is her back and a man in evening [illegible]hom she appears to be talking. It would [illegible] feeling [illegible] that [illegible] the vie[illegible] standing where that gentleman must [illegible] From th[illegible] laws of geometrical optics, what is amiss?

5.42* We [illegible] to design an eye for a robot, using a [illegible]cave sp[illegible] mirror such that the image of an [illegible]ct 1.0 m tall and 10 m away fills its 1.0-cm–square [illegible]tosensit[illegible]ector (which is movable for focusing [illegible]poses). [illegible] should this detector be located with [illegible] What should be the focal length [illegible] Draw a ray diagram.

5.43 You are herewith requested to design a little [illegible] be fixed at the end of a shaft for use in the mouth of some happy soul. The requirements [illegible] that the image be erect as seen by the dentist [illegible] that when held 1.5 cm from a tooth the mirror [illegible] an image twice life-size.

5.44 Prove that with a spherical mirror of radius R, [illegible]bject at a distance s_o will result in an image that is [illegible]ified by an amount

$$M_T = \frac{R}{2s_o + R}.$$

5.45* [illegible]eratometer is a device used to measure the [illegible] of the cornea of the eye, which is [illegible] fitting contact lenses. In effect, an [illegible]ated object is placed a known distance from the [illegible] and the image reflected off the cornea is [illegible] instrument allows the operator to [illegible] of that virtual image. Suppose that the [illegible] is found to be 0.037× when the object [illegible]ce is [illegible] at 100 mm. What is the radius of cur[illegible]e?

[illegible] Cons[illegible] a spherical mirror, show that the [illegible]ons of [illegible] and image are given by

$$s_o = [illegible] 1)/M_T \quad \text{and} \quad s_i = -f(M_T - 1).$$

5.47 Looking into the bowl of a soupspoon, a man standing 25 cm away sees his image reflected with a magnification of −0.064. Determine the radius of curvature of the spoon.

5.48* A large upright convex spherical mirror in an amusement park is facing a plane mirror 10.0 m away. A girl 1.0 m tall standing midway between the two sees herself twice as tall in the plane mirror as in the spherical one. In other words, the angle subtended at the observer by the image in the plane mirror is twice the angle subtended by the image in the spherical mirror. What is the focal length of the latter?

5.49* The telescope depicted in Fig. 5.124 consists of two spherical mirrors. The radius of curvature is 2.0 m for the larger mirror (which has a hole through its center) and 60 cm for the smaller. How far from the smaller mirror should the film plane be located if the object is a star? What is the effective focal length of the system?

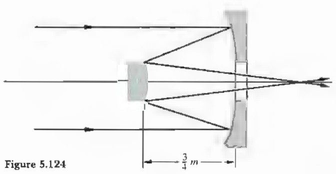


Figure 5.124

5.50* Suppose you have a concave spherical mirror with a focal length of 10 cm. At what distance must an object be placed if its image is to be erect and one and a half times as large? What is the radius of curvature of the mirror? Check with Table 5.5.

5.51 Describe the image that would result for an object 3 inches tall placed 20 cm from a spherical concave shaving mirror having a radius of curvature of −60 cm.

5.52* Figures 5.125 and 5.126 are taken from an introductory physics book. What's wrong with them?

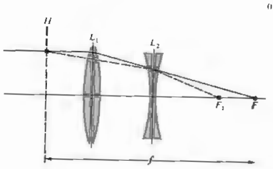


Figure 5.125

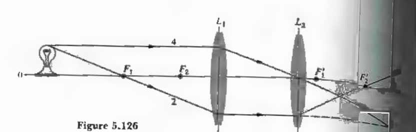


Figure 5.126

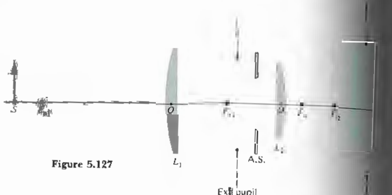


Figure 5.127

5.53 Figure 5.127 shows a lens system, an object, and the appropriate pupils. Diagrammatically locate the image.

5.54 Referring to the dove prism in Fig. 5.60, rotate it through 90° about an axis along the ray direction. Sketch the new configuration and determine the angle through which the image is rotated.

5.55 Determine the numerical aperture of a single clad optical fiber, given that the core has an index of 1.62, and the clad 1.52. When immersed in air, what is its maximum acceptance angle? What would happen to a ray incident at, say, 45°?

5.56 Given a modern fused silica fiber with an attenuation of 0.2 dB/km, how far can a signal travel along it before the power level drops by half?

5.57 The number of modes in a stepped-in[illegible] fiber is provided by the expression

$$N_m = \tfrac{1}{2}(\pi D \, \mathrm{NA}/\lambda_0)^2.$$

Given a fiber with a core diameter of 50 μm, and [illegible] 1.482 and $n_f = 1.500$, determine N_m when the [illegible] illuminated by an LED emitting at a central wav[illegible] of 0.85 μm.

5.58* Determine the intermodal delay (in ns[illegible] a stepped-index fiber with a cladding of index [illegible] and a core of index 1.500.

5.59 Using the information on the eye in Section [illegible] compute the approximate size (in millimeters) [illegible] image of the Moon as cast on the retina. The M[illegible] a diameter of 2160 miles and is roughly 2[illegible]0,0[illegible] from here, although this, of course, varies.

5.60* Figure 5.128 shows an arrangement in which the beam is deviated through a constant angle σ, equal [illegible] angle β between the plane mirrors, regard[illegible] angle of incidence. Prove that this is indeed the case.

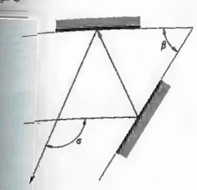


Figure 5.128

5.61 An object 20 m from the objective ($f_o = 4$ m) of an [illegible] telescope is imaged 30 cm from the [illegible] ($f_e = 60$ cm). Find the total linear magnification of the scope.

5.62* Figure 5.129, which purports to show an erecting lens system, is taken from an old, out-of-print optics text. What's wrong with it?

[illegible] a photograph of a moving merry-go-round [illegible]y exposed, but blurred, at $\frac{1}{30}$ s and $f/11$, what [illegible] diaphragm setting be if the shutter speed is [illegible] s in order to "stop" the motion?

5.64 The field of view of a simple two-element astronomical telescope is restricted by the size of the eye-lens. Make a ray sketch showing the vignetting that arises.

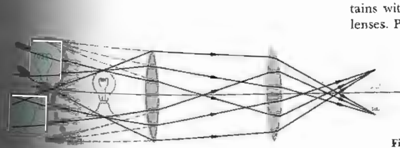


Figure 5.129

5.65 A *field-lens*, as a rule, is a positive lens placed at (or near) the intermediate image plane in order to collect the rays that would otherwise miss the next lens in the system. In effect, it increases the field of view without changing the power of the system. Redraw the ray diagram of the previous problem to include a field-lens. Show that as a consequence the eye relief is reduced somewhat.

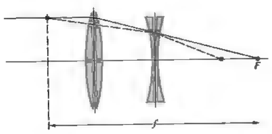
5.66* Describe completely the image that results when a bug sits at the vertex of a thin positive lens. How does this relate directly to the manner in which a field-lens works (see previous problem)?

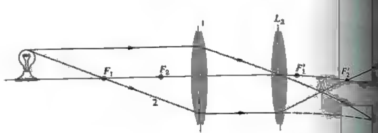
5.67* It is determined that a patient has a near point at 50 cm. If the eye is approximately 2.0 cm long,

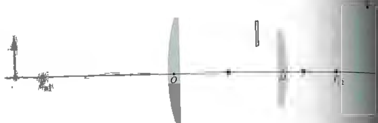
a) How much power does the refracting system have when focused on an object at infinity? When focused at 50 cm?
b) How much accommodation is required to see an object at a distance of 50 cm?
c) What power must the eye have to see clearly an object at the standard near-point distance of 25 cm?
d) How much power should be added to the patient's vision system by a correcting lens?

5.68* An optometrist finds that a farsighted person has a near point at 125 cm. What power will be required for contact lenses if they are effectively to move that point inward to a more workable distance of 25 cm so that a book can be read comfortably? Use the fact that if the object is imaged at the near point, it can be seen clearly.

5.69 A farsighted person can see very distant mountains with relaxed eyes while wearing +3.2-D contact lenses. Prescribe spectacle lenses that will serve just as







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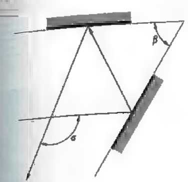

Figure 5.128

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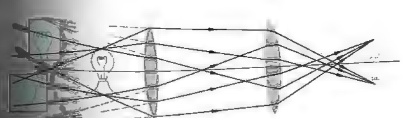


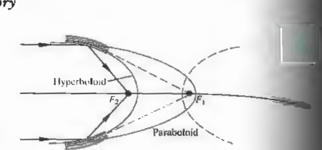
well when worn 17 mm in front of the cornea. Locate and compare the far point in both cases.

5.70* A jeweler is examining a diamond 5.0 mm in diameter with a loupe having a focal length of 25.4 mm.

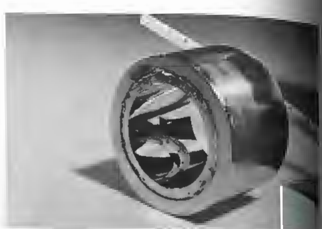
a) Determine the maximum angular magnification of the loupe.
b) How big does the stone appear through the magnifier?
c) What is the angle subtended by the diamond at the unaided eye when held at the near point?
d) What angle does it subtend at the aided eye?

5.71 Suppose we wish to make a microscope (that can be used with a relaxed eye) out of two positive lenses, both with a focal length of 25 mm. Assuming the object is positioned 27 mm from the objective, (a) how far apart should the lenses be, and (b) what magnification can we expect?

5.72* Figure 5.130 shows a glancing-incidence x-ray focusing system designed in 1952 by Hans Wolter. How does it work? Microscopes with this type of system have been used to photograph, in x-rays, the implosion of fuel pellet targets in laser fusion research. Similar x-ray optical arrangements have been used in astronomical telescopes (Fig. 3.40).



(a)



(b)

Figure 5.130 (a) X-ray focusing system. (b) X-ray mirrors. (Photo courtesy Lawrence Livermore National Laboratory.)

6 MORE ON GEOMETRICAL OPTICS

The pre[illegible] chapter, for the most part, dealt with paraxial [illegible] spherical lens systems. The two [illegible] approximations were, rather [illegible] we had *thin* lenses and that first-order [illegible] for their analysis. Neither of these [illegible]ons can be maintained throughout the design [illegible]sion optical system, but, taken together, they [illegible] the basis for a first rough solution. This chapter [illegible] things a bit further by examining thick lenses [illegible]rations; even at that, it is only a beginning. [illegible]vent of computerized lens design requires a [illegible]ertain shift in emphasis—there is little need to do what [illegible] computer can do better. Moreover, the sheer wealth [illegible] material developed over centuries demands [illegible] bit of judicious pruning to avoid a plethora of pedantry.

6.1 [illegible]CK LENSES AND LENS SYSTEMS

[illegible] 6.1 depicts a thick lens (i.e., one whose thickness [illegible] no means negligible). As we shall see, it could [illegible]ly well be envisioned more generally as an optical [illegible], allowing for the possibility that it consists of a [illegible] of simple lenses, not merely one. The first and [illegible] focal points, or if you like, the object and image [illegible] and F_i, can conveniently be measured from the [illegible] (outermost) vertices. In that case we have the [illegible] front and back focal lengths denoted by f.f.l. [illegible]f.l. When extended, the incident and emerged

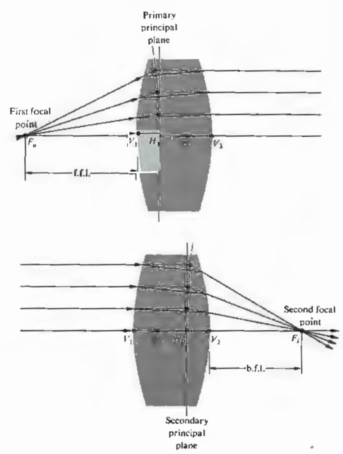


Figure 6.1 A thick lens.

rays will meet at points, the locus of which forms a curved surface that may or may not reside within the lens. The surface, approximating a plane in the paraxial region, is termed the **principal plane** (see Section 6.3.1). Points where the primary and secondary principal planes (as shown in Fig. 6.1) intersect the optical axis are known as the **first** and **second principal points**, H_1 and H_2, respectively. They provide a set of very useful references from which to measure several of the system parameters. We saw earlier (Fig. 5.19, p.140) that a ray traversing the lens through its optical center emerges parallel to the incident direction. Extending both the incoming and outgoing rays until they cross the optical axis locates what are called the **nodal points**, N_1 and N_2 in Fig. 6.2. *When the lens is surrounded on both sides by the same medium, generally air, the nodal and principal points will be coincident.* The six points, two focal, two principal, and two nodal, constitute the **cardinal points** of the system. As shown in Fig. 6.3, the principal planes can lie completely outside the lens system. Here, although differently configured, each lens in either group has the same power. Observe that in the symmetrical lens the principal planes are, quite reasonably, symmetrically located. In the case of either the planar-concave or planar-convex lens, one principal plane is tangent to the curved surface—as should be expected from the definition (applied to the paraxial region). In contrast, the principal points can be external for meniscus lenses. One often speaks of this succession of shapes with the same power as exemplifying *lens bending*. A rule of thumb for ordinary glass lenses in air is that the separation $\overline{H_1H_2}$ roughly equals one third the len[illegible] thickness $\overline{V_1V_2}$.

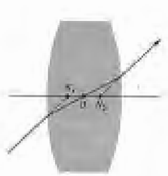


Figure 6.2 Nodal points.

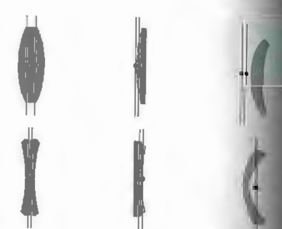


Figure 6.3 Lens bending.

The thick lens can be treated as consisting of tw[illegible] spherical refracting surfaces separated by a dis[illegible] between their vertices, as in Section 5.2.3, whe[illegible] thin-lens equation was derived. After a great d[illegible] algebraic manipulation,* wherein d is not neg[illegible] one arrives at a very interesting result for the thi[illegible] immersed in air. The expression for the con[illegible] points once again can be put in the Gaussian fo[illegible]

$$\frac{1}{s_o}+\frac{1}{s_i}=\frac{1}{f},$$

provided that both these object and image dista[illegible] measured from the first and second principal [illegible] respectively. Moreover, the *effective focal le*[illegible] simply the *focal length*, f, is also reckoned with respect to the principal planes and is given by

$$\frac{1}{f}=(n_l-1)\left[\frac{1}{R_1}-\frac{1}{R_2}+\frac{(n_l-1)d}{n_lR_1R_2}\right]$$

The principal planes are located at distances of [illegible] h_1 and $\overline{V_2H_2}=h_2$, *which are positive when the* [illegible] *to the right of their respective vertices.* Figure 6.4 il[illegible]

* For the complete derivation, see Morgan, *Introduction to Geometric and Physical Optics*, p. 57.

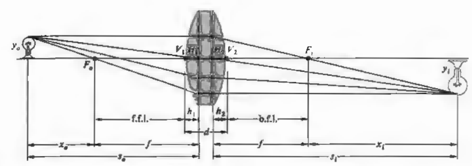


Figure 6.4 Thick lens geometry.

the arrangement of the various quantities. The values of h_1 and h_2 are given by

$$h_1=-\frac{f(n_l-1)d}{R_2n_l} \tag{6.3}$$

and

$$h_2=-\frac{f(n_l-1)d}{R_1n_l}. \tag{6.4}$$

In the same way the Newtonian form of the lens [illegible]on holds, as is evident from the similar triangles [illegible] 6.4. Thus

$$x_ix_o=f^2, \tag{6.5}$$

as long as f is given the present interpretation. And from the same triangles

$$M_T=\frac{y_i}{y_o}=-\frac{x_i}{f}=-\frac{f}{x_o}, \tag{6.6}$$

[illegible] if $d\to 0$, Eqs. (6.1), (6.2), and (6.5) are trans[illegible] the thin-lens expressions (5.17), (5.16), and [illegible] a numerical example, let's find the image [illegible] for an object positioned 30 cm from the vertex [illegible] convex lens having radii of 20 cm and 40 cm, [illegible] of 1 cm, and an index of 1.5. From Eq. (6.2) the focal length (in centimeters) is

$$\frac{1}{f}=(1.5-1)\left[\frac{1}{20}-\frac{1}{-40}+\frac{(1.5-1)1}{1.5(20)(-40)}\right],$$

[illegible] $f=26.8$ cm. Furthermore,

$$h_1=-\frac{26.8(0.5)1}{-40(1.5)}=+0.22\text{ cm}$$

and

$$h_2=-\frac{26.8(0.5)1}{20(1.5)}=-0.44\text{ cm},$$

which means that H_1 is to the right of V_1, and H_2 is to the left of V_2. Finally, $s_o=30+0.22$, whence

$$\frac{1}{30.2}+\frac{1}{s_i}=\frac{1}{26.8},$$

and $s_i=238$ cm, measured from H_2.

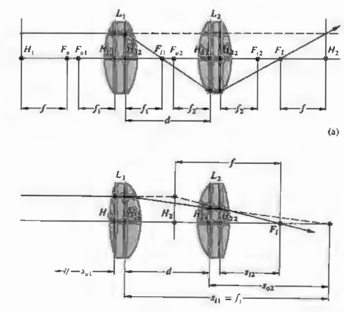


Figure 6.5 A compound thick lens.

The principal points are conjugate to each other. In other words, since $f = s_o s_i/(s_o + s_i)$, when $s_o = 0$, s_i must be zero, because f is finite and thus a point at H_1 is imaged at H_2. Furthermore, an object in the first principal plane ($x_o = -f$) is imaged in the second principal plane ($x_i = -f$) with unit magnification ($M_T = 1$). It is for this reason that they are sometimes spoken of as *unit planes.* Hence any ray directed toward a point on the first principal plane will emerge from the lens as if it originated at the corresponding point (the same distance above or below the axis) on the second principal plane.

Suppose we now have a compound lens consisting of two thick lenses, L_1 and L_2 (Fig. 6.5). Let s_{o1}, s_{i1}, and f_1 and s_{o2}, s_{i2}, and f_2 be the object and image distances and focal lengths for the two lenses, all measured with respect to their own principal planes. We know that the transverse magnification is the product of the magnifications of the individual lenses, that is,

$$M_T = \left(-\frac{s_{i1}}{s_{o1}}\right)\left(-\frac{s_{i2}}{s_{o2}}\right) = -\frac{s_i}{s_o}, \tag{6.7}$$

where s_o and s_i are the object and image distances for the combination as a whole. When s_o is equal to infinity $s_o = s_{o1}$, $s_{i1} = f_1$, $s_{o2} = -(s_{i1} - d)$, and $s_i = f$. Since

$$\frac{1}{s_{o2}} + \frac{1}{s_{i2}} = \frac{1}{f_2},$$

it follows (Problem 6.1), upon substituting into Eq. (6.7), that

$$-\frac{f_1 s_{i2}}{s_{o2}} = f$$

or

$$f = -\frac{f_1}{s_{o2}}\left(\frac{s_{o2} f_2}{s_{o2} - f_2}\right) = \frac{f_1 f_2}{s_{i1} - d + f_2}.$$

Hence

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2} - \frac{d}{f_1 f_2}. \tag{6.8}$$

This is the effective focal length of the combination of two thick lenses where all distances are measured from principal planes. The principal planes for the system as

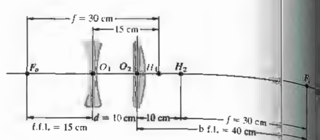


Figure 6.6 A compound lens.

a whole are located using the expressions

$$\overline{H_{11}H_1} = \frac{fd}{f_2} \tag{6.9}$$

and

$$\overline{H_{22}H_2} = -\frac{fd}{f_1}, \tag{6.10}$$

which will not be derived here (see Section [illegible]) have in effect found an equivalent thick-lens [illegible] tion of the compound lens. Note that if the [illegible] lenses are thin, the pairs of points H_{11}, H_{12} [illegible] H_{22} coalesce, whereupon d becomes the [illegible] center lens separation, as in Section 5.2.3. [illegible] returning to the thin lenses of Fig. 5.31 [illegible] $f_2 = 20$, and $d = 10$, as in Fig. 6.6,

$$\frac{1}{f} = \frac{1}{-30} + \frac{1}{20} - \frac{10}{(-30)(20)},$$

so $f = 30$ cm. We found earlier (p.148) that [illegible] 40 cm and f.f.l. = 15 cm. Moreover, since [illegible] lenses, Eqs. (6.9) and (6.10) can be written as

$$\overline{O_1H_1} = \frac{30(10)}{20} = +15 \text{ cm}$$

and

$$\overline{O_2H_2} = -\frac{30(10)}{-30} = +10 \text{ cm}.$$

Both are positive, and therefore the planes [illegible] right of O_1 and O_2, respectively. Both computed [illegible] agree with the results depicted in the diagram. [illegible]

enters from the right, the system resembles a telephoto lens that must be placed 15 cm from the film plane, yet has an effective focal length of 30 cm.

The same procedures can be extended to three, four, or more lenses. Thus

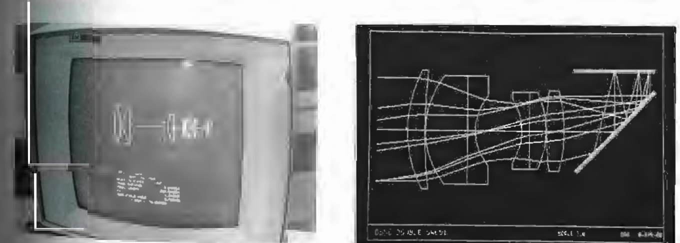
$$f = f_1\left(-\frac{s_{i2}}{s_{o2}}\right)\left(-\frac{s_{i3}}{s_{o3}}\right)\cdots \tag{6.11}$$

Equivalently, the first two lenses can be envisioned as combined to form a single thick lens whose principal points and focal length are calculated. It, in turn, is combined with the third lens, and so on with each successive element.

6.2 ANALYTICAL RAY TRACING

[illegible] is unquestionably one of the designer's chief [illegible]ols. Having formulated an optical system on paper, [illegible] can mathematically shine rays through it to evaluate [illegible]mance. Any ray, paraxial or otherwise, can be [illegible] through the system exactly. Conceptually it's a [illegible] matter of applying the refraction equation

$$n_i(\hat{\mathbf{k}}_i \times \hat{\mathbf{u}}_n) = n_t(\hat{\mathbf{k}}_t \times \hat{\mathbf{u}}_n) \tag{4.7}$$



(a) (b)

[illegible] Computer lens display. (Photo by E.H.) (b) Computer [illegible] courtesy of Optical Research Associates.)

at the first surface, locating where the transmitted ray then strikes the second surface, applying the equation once again, and so on all the way through. At one time *meridional rays* (those in the plane of the optical axis) were traced almost exclusively, because nonmeridional or *skew rays* (which do not intersect the axis) are considerably more complicated to deal with mathematically. The distinction is of less importance to a high-speed electronic computer (Fig. 6.7) which simply takes a trifle longer to make the trace. Thus, whereas it would probably take 10 or 15 minutes for a skilled person with a desk calculator to evaluate the trajectory of a single skew ray through a single surface, a computer might require less than a thousandth of a second for the same job, and equally important, it would be ready for the next calculation with undiminished enthusiasm.

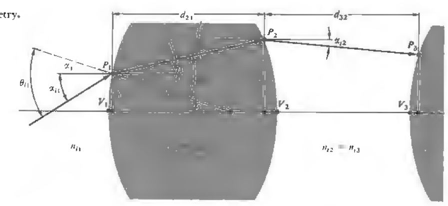
The simplest case that will serve to illustrate the ray-tracing process is that of a paraxial, meridional ray traversing a thick spherical lens. Applying Snell's law in Fig. 6.8 at point P_1 yields

$$n_{i1}\theta_{i1} = n_{t1}\theta_{t1}$$

or

$$n_{i1}(\alpha_{i1} + \alpha_1) = n_{t1}(\alpha_{t1} + \alpha_1).$$

Figure 6.8 Ray geometry.



Inasmuch as $\alpha_1 = y_1/R_1$, this becomes

$$n_{t1}(\alpha_{t1} + y_1/R_1) = n_{i1}(\alpha_{i1} + y_1/R_1).$$

Rearranging terms, we get

$$n_{t1}\alpha_{t1} = n_{i1}\alpha_{i1} - \left(\frac{n_{t1} - n_{i1}}{R_1}\right) y_1,$$

but as we saw in Section 5.7.2, the power of a single refracting surface is

$$\mathscr{D}_1 = \frac{(n_{t1} - n_{i1})}{R_1}.$$

Hence

$$n_{t1}\alpha_{t1} = n_{i1}\alpha_{i1} - \mathscr{D}_1 y_1. \tag{6.12}$$

This is often called the *refraction equation* pertaining to the first interface. Having undergone refraction at point P_1, the ray advances through the homogeneous medium of the lens to point P_2 on the second interface. The height of P_2 can be expressed as

$$y_2 = y_1 + d_{21}\alpha_{t1}, \tag{6.13}$$

on the basis that $\tan \alpha_{t1} \approx \alpha_{t1}$. This is known as the *transfer equation*, because it allows us to follow the ray from P_1 to P_2. Recall that the angles are positive if the ray has a positive slope. Since we are dealing with the paraxial region $d_{21} \approx \overline{V_2V_1}$ and y_2 is easily computed. Equations (6.11) and (6.12) are then used successively to trace a ray through the entire system. Of course, these are meridional rays and because of the lenses' symmetry about the optical axis, such a ray remains in the same meridional plane throughout its sojourn. The process is two-dimensional; there are two equations in two unknowns, α_{t1} and y_2. In contrast, a skew ray would have to be treated in three dimensions.

6.2.1 Matrix Methods

In the beginning of the 1930s, T. Smith formulated a rather interesting way of handling the ray-tracing equations. The simple linear form of the expressions and the repetitive manner in which they are applied suggested the use of matrices. The processes of refraction and transfer might then be performed mathematically by matrix operators. These initial insights were not widely appreciated for almost thirty years. However, the early 1960s saw a rebirth of interest in this approach, which is now flourishing.* We shall only outline some of the salient features of the method, leaving a more detailed study to the references.

Let's begin by writing the formulas

$$n_{t1}\alpha_{t1} = n_{i1}\alpha_{i1} - \mathscr{D}_1 y_{i1} \tag{6.14}$$

and

$$y_{t1} = 0 + y_{i1}, \tag{6.15}$$

[illegible] not very insightful, since we merely replaced [illegible] (6.12) by the symbol y_{t1} and then let $y_{t1} = y_{i1}$. [illegible] of business is for purely cosmetic purposes, [illegible] see in a moment. In effect, it simply says that [illegible] of reference point P_1 above the axis in the [illegible] medium (y_{i1}) equals its height in the transmitting medium (y_{t1})—which is obvious. But now the pair [illegible] equations can be recast in matrix form as

$$\begin{bmatrix} n_{t1}\alpha_{t1} \\ y_{t1} \end{bmatrix} = \begin{bmatrix} 1 & -\mathscr{D}_1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} n_{i1}\alpha_{i1} \\ y_{i1} \end{bmatrix}. \tag{6.16}$$

This could equally well be written as

$$\begin{bmatrix} \alpha_{t1} \\ y_{t1} \end{bmatrix} = \begin{bmatrix} n_{i1}/n_{t1} & -\mathscr{D}_1/n_{t1} \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \alpha_{i1} \\ y_{i1} \end{bmatrix}, \tag{6.17}$$

so that the precise form of the 2×1 column matrices is actually a matter of preference. In any case, these can be envisioned as rays on either side of P_1, one before and the other after refraction. Accordingly, using $\mathbf{r}_{t1}$ and $\mathbf{r}_{i1}$ for the two rays, we can write

$$\mathbf{r}_{t1} = \begin{bmatrix} n_{t1}\alpha_{t1} \\ y_{t1} \end{bmatrix} \quad \text{and} \quad \mathbf{r}_{i1} = \begin{bmatrix} n_{i1}\alpha_{i1} \\ y_{i1} \end{bmatrix}. \tag{6.18}$$

The 2×2 matrix is the **refraction matrix**, denoted as

$$\mathscr{R}_1 = \begin{bmatrix} 1 & -\mathscr{D}_1 \\ 0 & 1 \end{bmatrix}, \tag{6.19}$$

so Eq. (6.16) can be concisely stated as

$$\mathbf{r}_{t1} = \mathscr{R}_1 \mathbf{r}_{i1}, \tag{6.20}$$

which [illegible] says that $\mathscr{R}_1$ transforms the ray $\mathbf{r}_{i1}$ into the [illegible] during refraction at the first interface. From Fig. [illegible] we have $n_{i2}\alpha_{i2} = n_{t1}\alpha_{t1}$, that is,

$$n_{i2}\alpha_{i2} = n_{t1}\alpha_{t1} + 0 \tag{6.21}$$

and

$$y_{i2} = d_{21}\alpha_{t1} + y_{t1}, \tag{6.22}$$

where $n_{i2} = n_{t1}$, $\alpha_{i2} = \alpha_{t1}$, and use was made of Eq. (6.13), with y_2 rewritten as y_{i2} to make things pretty. Thus

$$\begin{bmatrix} n_{i2}\alpha_{i2} \\ y_{i2} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ d_{21}/n_{t1} & 1 \end{bmatrix} \begin{bmatrix} n_{t1}\alpha_{t1} \\ y_{t1} \end{bmatrix}. \tag{6.23}$$

The **transfer matrix**

$$\mathscr{T}_{21} = \begin{bmatrix} 1 & 0 \\ d_{21}/n_{t1} & 1 \end{bmatrix} \tag{6.24}$$

takes the transmitted ray at P_1 (i.e., $\mathbf{r}_{t1}$) and transforms it into the incident ray at P_2:

$$\mathbf{r}_{i2} = \begin{bmatrix} n_{i2}\alpha_{i2} \\ y_{i2} \end{bmatrix}.$$

Hence Eqs. (6.21) and (6.22) become simply

$$\mathbf{r}_{i2} = \mathscr{T}_{21}\mathbf{r}_{t1}. \tag{6.25}$$

If we make use of Eq. (6.20), this becomes

$$\mathbf{r}_{i2} = \mathscr{T}_{21}\mathscr{R}_1\mathbf{r}_{i1}. \tag{6.26}$$

The 2×2 matrix formed by the product of the transfer and refraction matrices $\mathscr{T}_{21}\mathscr{R}_1$ will carry the ray incident at P_1 into the ray incident at P_2. Notice that the determinant of $\mathscr{T}_{21}$, denoted by $|\mathscr{T}_{21}|$, equals 1, that is, $(1)(1) - (0)(d_{21}/n_{t1}) = 1$. Similarly $|\mathscr{R}_1| = 1$, and since the determinant of a matrix product equals the product of the individual determinants, $|\mathscr{T}_{21}\mathscr{R}_1| = 1$. This provides a quick check on the computations. Carrying the procedure through the second interface (Fig. 6.8) of the lens, which has a refraction matrix $\mathscr{R}_2$, it follows that

$$\mathbf{r}_{t2} = \mathscr{R}_2\mathbf{r}_{i2}, \tag{6.27}$$

or from Eq. (6.26)

$$\mathbf{r}_{t2} = \mathscr{R}_2\mathscr{T}_{21}\mathscr{R}_1\mathbf{r}_{i1}. \tag{6.28}$$

The **system matrix** $\mathscr{A}$ is defined as

$$\mathscr{A} = \mathscr{R}_2\mathscr{T}_{21}\mathscr{R}_1 \tag{6.29}$$

and has the form

$$\mathscr{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}. \tag{6.30}$$

Since

$$\mathscr{A} = \begin{bmatrix} 1 & -\mathscr{D}_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ d_{21}/n_{t1} & 1 \end{bmatrix} \begin{bmatrix} 1 & -\mathscr{D}_1 \\ 0 & 1 \end{bmatrix}$$

or

$$\mathscr{A} = \begin{bmatrix} 1 & -\mathscr{D}_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & -\mathscr{D}_1 \\ d_{21}/n_{t1} & -\mathscr{D}_1 d_{21}/n_{t1} + 1 \end{bmatrix},$$

* For further reading see K. Hallbach, "Matrix Representation of Gaussian Optics." *Am. J. Phys.* **32**, 90 (1964); W. Brouwer, *Matrix Methods in Optical Instrument Design*; E. L. O'Neill, *Introduction to Statistical Optics*; or A. Nussbaum, *Geometric Optics*.

we can write

$$\begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} = \begin{bmatrix} 1 - \mathscr{D}_2 d_{21}/n_{t1} & -\mathscr{D}_1 + (\mathscr{D}_2\mathscr{D}_1 d_{21}/n_{t1}) - \mathscr{D}_2 \\ d_{21}/n_{t1} & -\mathscr{D}_1 d_{21}/n_{t1} + 1 \end{bmatrix}, \tag{6.31}$$

and again $|\mathscr{A}| = 1$ (Problem 6.15). The value of each element in $\mathscr{A}$ is expressed in terms of the physical lens parameters, such as thickness, index, and radii (via $\mathscr{D}$). Thus the cardinal points that are properties of the lens, determined solely by its make-up, should be deducible from $\mathscr{A}$. The system matrix in this case (6.31) transforms an incident ray at the first surface to an emerging ray at the second surface; as a reminder we will write it as $\mathscr{A}_{21}$.

The concept of image formation enters rather directly (Fig. 6.9) after introduction of appropriate object and image planes. Consequently, the first operator $\mathscr{T}_{1O}$ transfers the reference point from the object (i.e., P_O to P_1). The next operator $\mathscr{A}_{21}$ then carries the ray through the lens, and a final transfer $\mathscr{T}_{I2}$ brings it to the image plane (i.e., P_I). Thus the ray at the image point ($\mathbf{r}_I$) is given by

$$\mathbf{r}_I = \mathscr{T}_{I2}\mathscr{A}_{21}\mathscr{T}_{1O}\mathbf{r}_O, \tag{6.32}$$

where $\mathbf{r}_O$ is the ray at P_O. In component form this is

$$\begin{bmatrix} n_I\alpha_I \\ y_I \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ d_{I2}/n_I & 1 \end{bmatrix} \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ d_{1O}/n_O & 1 \end{bmatrix} \begin{bmatrix} n_O\alpha_O \\ y_O \end{bmatrix}. \tag{6.33}$$

Notice that $\mathscr{T}_{1O}\mathbf{r}_O = \mathbf{r}_{i1}$ and that $\mathscr{A}_{21}\mathbf{r}_{i1} = \mathbf{r}_{t2}$, hence $\mathscr{T}_{I2}\mathbf{r}_{t2} = \mathbf{r}_I$. The subscripts $O, 1, 2, \ldots, I$ correspond to reference points P_O, P_1, P_2, and so on, and subscripts i and t denote the side of the reference point (i.e., whether incident or transmitted). Operation by a refraction matrix will change i to t but not the reference point designation. On the other hand, operation by a transfer matrix obviously does change the latter.

Ordinarily the physical significances of the components of $\mathscr{A}$ are found by expanding out Eq. (6.33), but this is too involved to do here. Instead, let's return

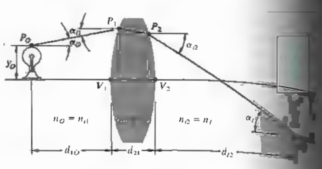


Figure 6.9 Image geometry.

to Eq. (6.31) and examine several of the terms. For example,

$$-a_{12} = \mathscr{D}_1 + \mathscr{D}_2 - \mathscr{D}_2\mathscr{D}_1 d_{21}/n_{t1}.$$

If we suppose, for the sake of simplicity, that the lens is in air, then

$$\mathscr{D}_1 = \frac{n_{t1} - 1}{R_1} \quad \text{and} \quad \mathscr{D}_2 = \frac{n_{t1} - 1}{-R_2},$$

as in Eqs. (5.70) and (5.71). Hence

$$-a_{12} = (n_{t1} - 1)\left[\frac{1}{R_1} - \frac{1}{R_2} + \frac{(n_{t1} - 1)d_{21}}{R_1 R_2 n_{t1}}\right].$$

But this is the expression for the focal length of a thick lens (6.2); in other words,

$$a_{12} = -1/f. \tag{6.34}$$

If the imbedding media were different on each side of the lens (Fig. 6.10), this would become

$$a_{12} = -\frac{n_{i1}}{f_o} = -\frac{n_{t2}}{f_i}. \tag{6.35}$$

Similarly it is left as a problem to verify that

$$\overline{V_1H_1} = \frac{n_{i1}(1 - a_{11})}{-a_{12}} \tag{6.36}$$

and

$$\overline{V_2H_2} = \frac{n_{t2}(a_{22} - 1)}{-a_{12}},$$

which locate the principal points.

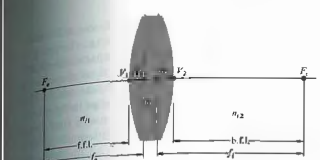


Figure 6.10 Principal planes and focal lengths.

As an example of how the technique can be used, let's apply it, at least in principle, to the Tessar lens* shown in Fig. 6.11. The system matrix has the form

$$\mathscr{A}_{71} = [illegible]\mathscr{T}_{65}\mathscr{R}_5\mathscr{T}_{54}\mathscr{R}_4\mathscr{T}_{43}\mathscr{R}_3\mathscr{T}_{32}\mathscr{R}_2\mathscr{T}_{21}\mathscr{R}_1,$$

where

$$[illegible] \begin{bmatrix} [illegible] & 0 \\ \frac{0.357}{1.6116} & 1 \end{bmatrix}, \quad \mathscr{T}_{32} = \begin{bmatrix} 1 & 0 \\ \frac{0.189}{1} & 1 \end{bmatrix},$$

$$\mathscr{T}_{43} = \begin{bmatrix} 1 & 0 \\ \frac{0.081}{1.6053} & 1 \end{bmatrix},$$

[illegible] Furthermore,

$$\mathscr{R}_1 = \begin{bmatrix} 1 & -\frac{1.6116 - 1}{1.628} \\ 0 & 1 \end{bmatrix}, \quad \mathscr{R}_2 = \begin{bmatrix} 1 & -\frac{1 - 1.6116}{-27.57} \\ 0 & 1 \end{bmatrix},$$

$$\mathscr{R}_3 = \begin{bmatrix} 1 & -\frac{1.6053 - 1}{-3.457} \\ 0 & 1 \end{bmatrix},$$

and so on. Multiplying out the matrices, in what is

obviously a horrendous although conceptually simple calculation, one presumably will get

$$\mathscr{A}_{71} = \begin{bmatrix} 0.848 & -0.198 \\ 1.338 & 0.867 \end{bmatrix},$$

and from that, $f = 5.06$, $\overline{V_1H_1} = 0.77$, and $\overline{V_7H_2} = -0.67$.

As a last point, it is often convenient to consider a system of thin lenses using the matrix representation. To that end, return to Eq. (6.31). It describes the system matrix for a single lens, and if we let $d_{21} \to 0$, it corresponds to a thin lens. This is equivalent to making $\mathscr{T}_{21}$ a unit matrix, thus

$$\mathscr{A} = \mathscr{R}_2\mathscr{R}_1 = \begin{bmatrix} 1 & -(\mathscr{D}_1 + \mathscr{D}_2) \\ 0 & 1 \end{bmatrix}. \tag{6.38}$$

But as we saw in Section 5.7.2, the power of a thin lens $\mathscr{D}$ is the sum of the powers of its surfaces. Hence

$$\mathscr{A} = \begin{bmatrix} 1 & -\mathscr{D} \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & -1/f \\ 0 & 1 \end{bmatrix}. \tag{6.39}$$

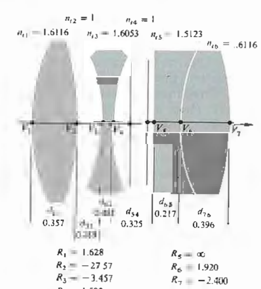


Figure 6.11 A Tessar.

* This particular example was chosen primarily because Nussbaum's book Geometric Optics contains a simple Fortran computer program [illegible] for this lens. It would be almost silly to evaluate the system matrix by hand. Since Fortran is an easily mastered computer language, the program is well worth further study.

In addition, for two thin lenses separated by a distance d, in air, the system matrix is

$$\mathcal{A} = \begin{bmatrix} 1 & -1/f_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ d & 1 \end{bmatrix} \begin{bmatrix} 1 & -1/f_1 \\ 0 & 1 \end{bmatrix}$$

or

$$\mathcal{A} = \begin{bmatrix} 1 - d/f_2 & -1/f_1 + d/f_1 f_2 - 1/f_2 \\ d & -d/f_1 + 1 \end{bmatrix}.$$

Clearly then,

$$-a_{12} = \frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2} - \frac{d}{f_1 f_2},$$

and from Eqs. (6.36) and (6.37)

$$\overline{O_1H_1} = fd/f_2, \qquad \overline{O_2H_2} = -fd/f_1,$$

all of which by now should be quite familiar. Note how easy it would be with this approach to find the focal length and principal points for a compound lens composed of three, four, or more thin lenses.

6.3 ABERRATIONS

To be sure, we already know that first-order theory is no more than a good approximation—an exact ray trace or even measurements performed on a prototype system would certainly reveal inconsistencies with the corresponding paraxial description. Such departures from the idealized conditions of Gaussian optics are known as **aberrations**. There are two main types: **chromatic aberrations** (which arise from the fact that n is actually a function of frequency or color) and **monochromatic aberrations**. The latter occur even with light that is highly monochromatic, and they in turn fall into two subgroupings. There are monochromatic aberrations that deteriorate the image, making it unclear, such as *spherical aberration, coma,* and *astigmatism.* In addition, there are aberrations that deform the image, for example, *Petzval field curvature* and *distortion.*

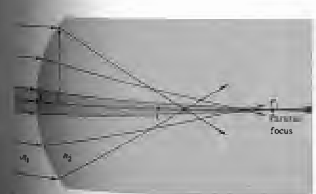
We have known all along that spherical surfaces in general would yield perfect imagery only in the paraxial region. Now we must determine the kind and extent of deviations that result simply from using those surfaces with finite apertures. By the judicious ma[illegible] tion of a system's physical parameters (e.g., the [illegible] shapes, thicknesses, glass types, and separatio[illegible] lenses, as well as the locations of stops), these ab[illegible] can indeed be minimized. In effect, one cancels [illegible] most undesirable faults by a slight change in [illegible] of a lens here or a shift in the position of a [illegible] (very much like trimming up a circuit with small [illegible] capacitors, coils, and pots). When it's all fin[illegible] unwanted deformations of the wavefront inc[illegible] passes through one surface will, it is hoped, be [illegible] as it traverses some other surfaces further down [illegible]

As early as 1950 ray-tracing programs were bein[illegible] developed for the new digital computers, and [illegible] efforts were already under way to create lens-de[illegible] software. In the early 1960s computerized lens [illegible] was a tool of the trade used by manufacturers [illegible] wide. Today there are elaborate computer p[illegible] for "automatically" designing and analyzing the [illegible] mance of all sorts of complicated optical [illegible] Broadly speaking, you give the computer a qua[illegible] (or merit function) of some sort to aim for [illegible] essentially tell it how much of each aberration yo[illegible] willing to tolerate). Then you give it a roughly de[illegible] system (e.g., some Tessar configuration), which [illegible] first approximation meets the particular requirem[illegible] Along with that, you feed in whatever parameters [illegible] be held constant, such as a given *f-number,* focal len[illegible] or lens diameter, the field of view, or magnific[illegible] The computer will then trace several rays through [illegible] system and evaluate the image errors. Having [illegible] given leave to vary, say, the curvatures and axial [illegible] rations of the elements, it will calculate the optim[illegible] effect of such changes on the quality factor, mak[illegible] and then reevaluate. After a number of itera[illegible] it will have changed the initial configuration so [illegible] meets the specified limits on aberrations. The [illegible] design will still be a Tessar, but not the orig[illegible] The result is, if you will, an *optimum configurati[illegible]* probably not *the* optimum. We can be fairly cert[illegible] all aberrations cannot be made exactly zero in any real system comprising spherical surfaces. [illegible] there is no currently known way to determine [illegible] to zero we can actually come. A quality factor [illegible] what like a crater-pocked surface in a multidime[illegible] space. The computer will carry the design from one hole to the next until it finds one deep enough to meet [illegible]ifications. There it stops and presumably pre[illegible] with a perfectly satisfactory configuration. But [illegible] no way to tell if that solution corresponds to ther[illegible]est hole, without sending the computer out the [illegible] again to meander along totally different [illegible] We mention all of this so that the reader may [illegible] the current state of the art. In a word, it is [illegible] but still incomplete; it is "automatic" but a bit [illegible]

6.3.1 [illegible]nochromatic Aberrations

[illegible]xial treatment was based on the assumption [illegible]at sin φ, as in Fig. 5.8, could be represented satisfac[illegible]rily by φ alone; that is, the system was restricted to [illegible]erating in an extremely narrow region about the [illegible]is. Obviously, if rays from the periphery of a [illegible] to be included in the formation of an image, the [illegible]atement $\sin\varphi \approx \varphi$ is somewhat unsatisfactory. [illegible] also occasionally wrote Snell's law simply [illegible] $= n_t\theta_t$, which again would be inappropriate. In [illegible]ent, if the first two terms in the expansion

$$\sin\varphi = \varphi - \frac{\varphi^3}{3!} + \frac{\varphi^5}{5!} - \frac{\varphi^7}{7!} + \cdots \qquad [5.7]$$



[illegible] Spherical aberration resulting from refraction at a single [illegible]

are retained as an improved approximation, we have the so-called *third-order theory.* Departures from first-order theory that then result are embodied in the five *primary aberrations* (spherical aberration, coma, astigmatism, field curvature, and distortion). These were first studied in detail by Ludwig von Seidel (1821–1896) in the 1850s. Accordingly, they are frequently spoken of as the *Seidel aberrations.* In addition to the first two contributions, the series obviously contains many other terms, smaller to be sure, but still to be reckoned with. Thus, there are most certainly *higher-order aberrations.* The difference between the results of exact ray tracing and the computed primary aberrations can therefore be thought of as the sum of all contributing higher-order aberrations. We shall restrict this discussion to the primary aberrations exclusively.

i) Spherical Aberration

Let's return for a moment to Section 5.2.2 (p.134), where we computed the conjugate points for a single refracting spherical interface. We found that for the paraxial region,

$$\frac{n_1}{s_o} + \frac{n_2}{s_i} = \frac{n_2 - n_1}{R} \qquad [5.8]$$

If the approximations for ℓ_o and ℓ_i are improved a bit (Problem 6.23), we get the third-order expression:

$$\frac{n_1}{s_o} + \frac{n_2}{s_i} = \frac{n_2 - n_1}{R} + h^2\left[\frac{n_1}{2s_o}\left(\frac{1}{s_o} + \frac{1}{R}\right)^2 + \frac{n_2}{2s_i}\left(\frac{1}{R} - \frac{1}{s_i}\right)^2\right]. \qquad (6.40)$$

The additional term, which varies approximately as h^2, is clearly a measure of the deviation from first-order theory. As shown in Fig. 6.12, rays striking the surface at greater distances above the axis (h) are focused nearer the vertex. In brief, spherical aberration, or SA, corresponds to a dependence of focal length on aperture for nonparaxial rays. Similarly, for a converging lens, as in Fig. 6.13, the marginal rays will, in effect, be bent too much, being focused in front of the paraxial rays. Keep in mind that spherical aberration pertains only to object points that are on the optical axis. The distance between the axial intersection of a ray and the paraxial focus, F_i, is known as the **longitudinal spherical aberration**,

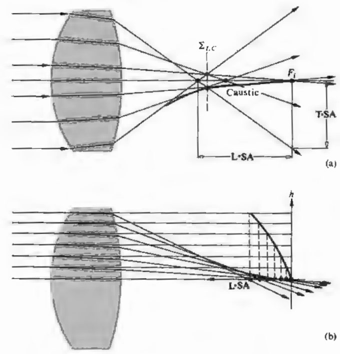


Figure 6.13 Spherical aberration for a lens. The envelope of the refracted rays is called a caustic. The intersection of the marginal rays and the caustic locates Σ_{LC}.

or L · SA, of that ray. In this case, the SA is *positive.* In contrast the marginal rays for a diverging lens will generally intersect the axis behind the paraxial focus, and we say that its spherical aberration is therefore *negative.*

If a screen is placed at F_i in Fig. 6.13, the image of a star will appear as a bright central spot on the axis surrounded by a symmetrical halo delineated by the cone of marginal rays. For an extended image, SA [illegible] reduce the contrast and degrade the details. The [illegible] above the axis where a given ray strikes this sc[illegible] is called the **transverse** (or **lateral**) **spherical aber**[illegible], or T · SA for short. Evidently, SA can be redu[illegible] stopping down the aperture—but that redu[illegible] amount of light entering the system as well. No[illegible] if the screen is moved to the position labeled Σ[illegible] image blur will have its smallest diameter. This is [illegible] as the *circle of least confusion,* and Σ_{LC} is general[illegible] best place to observe the image. If a lens ex[illegible] appreciable SA, it will have to be refocused af[illegible] stopped down, because the position of Σ[illegible] approach F_i as the aperture decreases.

The amount of spherical aberration, when the [illegible]ture and focal length are fixed, varies with bo[illegible] object distance and the lens shape. For a conv[illegible] lens, the nonparaxial rays are too strongly bent. [illegible] we imagine the lens as roughly resembling two [illegible] joined at their bases, it is evident that *the incid*[illegible] *will undergo a minimum deviation when it makes,* [illegible] *less, the same angle as does the emerging ray* (Section [illegible]). A striking example is illustrated in Fig. 6.14, [illegible] simply turning the lens around markedly reduc[illegible] SA. When the object is at infinity a simple conc[illegible] convex lens that has an almost, but not quite, [illegible] side will suffer a minimum amount of spheric[illegible]tion. In the same way, if the object and image [illegible] are to be equal ($s_o = s_i = 2f$), the lens should be [illegible]vex to minimize SA. A combination of a conver[illegible] and a diverging lens (as in an achromatic doublet) [illegible] also be utilized to diminish spherical aberratio[illegible].

Recall that the aspherical lenses of Section [illegible] completely free of spherical aberration for a spec[illegible] pair of conjugate points. Moreover, Huygens seems [illegible] have been the first to discover that two such axial points exist for spherical surfaces as well. These are shown in Fig. 6.15(a), which depicts rays issuing from P and leaving the surface as if they came from P'. It is left as a problem to show that the appropriate locations of P and P' are those indicated in the figure. Just as with the aspherical lenses, spherical lenses can be formed that have this same zero SA for the pair of points P and P'. One simply grinds another surface of radius $\overline{PA}$ centered on P to form either a positive- or negative-meniscus lens. The oil-immersion microscope objective uses this principle to great advantage. The object under study is positioned at P and surrounded by oil of index n_2, as in Fig. 6.16. P and P' are the proper conjugate points for zero SA for the first element, and P' and P'' are those for the meniscus lens.

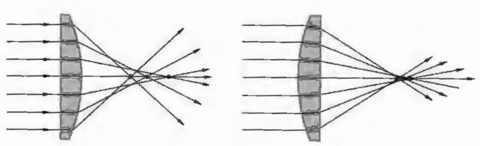


Figure 6.14 SA for a [illegible]

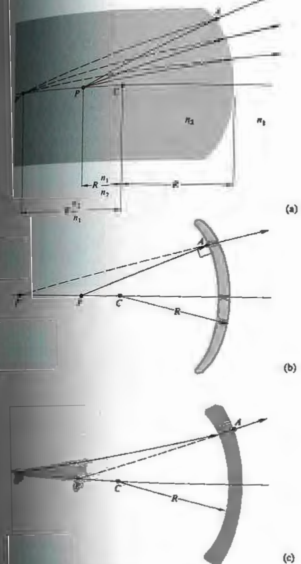


Figure 6.15 Corresponding axial points for which SA is zero.

ii) Coma

Coma, or *comatic aberration,* is an image-degrading, monochromatic, primary aberration associated with an object point even a short distance from the axis. Its origins lie in the fact that the principal "planes" can actually be treated as planes only in the paraxial region. They are, in fact, principal curved surfaces (Fig. 6.1). In the absence of SA a parallel bundle of rays will focus at the axial point F_i, a distance b.f.l. from the rear vertex. Yet the effective focal lengths and therefore the transverse magnifications will differ for rays traversing off-axis regions of the lens. When the image point is on the optical axis, this situation is of little consequence,

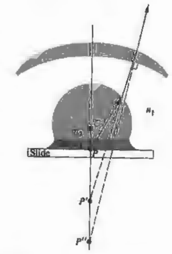


Figure 6.16 An oil-immersion microscope objective.

but when the ray bundle is oblique and the image point is off-axis, coma will be evident. The dependence of M_T on h, the ray height at the lens, is shown in Fig. 6.17. Here meridional rays traversing the extremities of the lens arrive at the image plane closer to the axis than do the rays in the vicinity of the *principal ray* (i.e., the ray that passes through the principal points). In this instance, the least magnification is associated with the marginal rays that would form the smallest image—the coma is said to be negative. By comparison, the coma in Fig. 6.18 is positive, because the marginal rays focus farther from the axis. Several skew rays are drawn from an extra-axial object point S in Fig. 6.19 to illustrate the formation of the geometrical comatic image of a point. Observe that each circular cone of rays whose endpoints (1-2-3-4-1-2-3-4) form a ring on the lens is imaged in what H. Dennis Taylor called a *comatic circle* on Σ_i. This case corresponds to positive coma, so the larger the ring on the lens, the more distant its comatic circle from the axis. When the outer ring is the intersection of marginal rays, the distance from 0 to 1 in the image is the *tangential coma*, and the length from 0 to 3 on Σ_i is termed the *sagittal coma*. A little more than half of the energy in the image appears in the roughly triangular region between 0 and 3. The coma flare, which owes its name to its cometlike tail, is often thought to be the worst of all aberrations, primarily because of its asymmetric configuration.

Like SA, coma is dependent on the shape of the lens. Thus, a strongly concave positive-meniscus lens) with the object at infinity will have a large negative coma. Bending the lens so that it becomes planar-convex), then equiconvex (), convex-planar (, and [illegible] meniscus (will change the coma from negative, [illegible] to positive. The fact that it can be made exact[illegible] for a single lens with a given object distance [illegible] significant. The particular shape it then has (s_o [illegible] almost convex-planar and nearly the configurati[illegible] minimum SA.

It is important to realize that *a lens that is well* [illegible] *for the case in which one conjugate point is at infinity* [illegible] *may not perform satisfactorily when the object is near*[illegible] would therefore do well, when using off-the-shel[illegible] in a system operating at finite conjugates, to [illegible] two infinite conjugate corrected lenses, as in [illegible] In other words, since it is unlikely that a lens [illegible] the desired focal length, which is also corrected [illegible] the particular set of finite conjugates, can be [illegible]

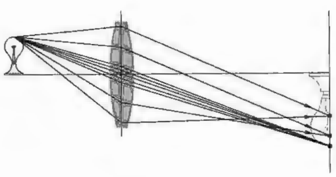


Figure 6.17 Negative coma.

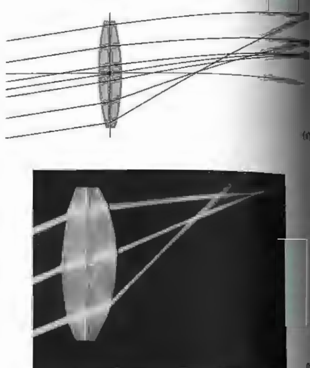
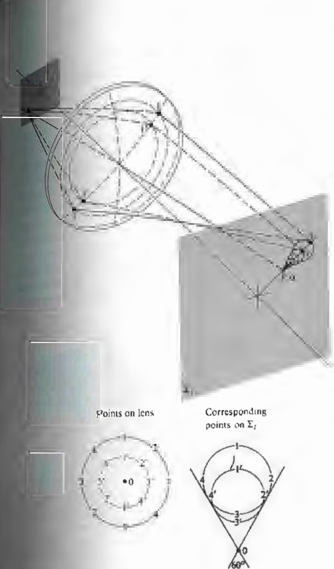


Figure 6.18 Positive coma. (Photo by E.H.)



[illegible] The geometrical coma image of a point. The central [illegible] point image at the vertex of the cone.

[illegible]de, this back-to-back lens approach is an [illegible]ealing alternative.

[illegible]oma can also be negated by using a stop at the [illegible]cation, as William Hyde Wollaston (1766– [illegible]overed in 1812. The order of the list of [illegible] aberrations (SA, coma, astigmatism, Petzval [illegible] and distortion) is significant, because any one of them, except SA and Petzval curvature, will be affected by the position of a stop, but only if one of the preceding aberrations is also present in the system. Thus while SA is independent of the location along the axis of a stop, coma will not be, as long as SA is present. This can be appreciated by examining the representation in Fig. 6.21. With the stop at Σ_1, ray 3 is the chief ray, there is SA but no coma; that is, the ray pairs meet on 3. If the stop is moved to Σ_2, the symmetry is upset, ray 4 becomes the chief ray, and the rays on either side of it, such as 3 and 5, meet above not on it—there is positive coma. With the stop at Σ_3, rays 1 and 3 intersect below the chief ray, 2, and there is negative coma. In this way, controlled amounts of the aberration can be introduced into a compound lens in order to cancel coma in the system as a whole.

The optical sine theorem is an important relationship that must be introduced here even if space precludes

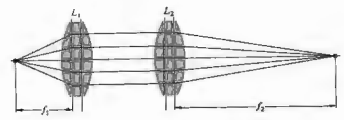


Figure 6.20 A combination of two infinite conjugate lenses yielding a system operating at finite conjugates.

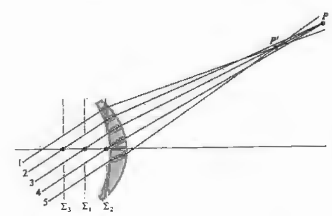


Figure 6.21 The effect of stop location on coma.

its formal proof. It was discovered independently in 1873 by Abbe and Helmholtz, although a different form of it was given 10 years earlier by R. Clausius (of thermodynamics fame). In any event, it states that

$$n_o y_o \sin \alpha_o = n_i y_i \sin \alpha_i, \qquad (6.41)$$

where n_o, y_o, α_o and n_i, y_i, α_i are the index, height, and slope angle of a ray in object and image space, respectively, at any aperture size* (Fig. 6.9). If coma is to be zero,

$$M_T = \frac{y_i}{y_o} \qquad [5.24]$$

must be constant for all rays. Suppose then that we send a marginal and a paraxial ray through the system. The former will comply with Eq. (6.41), the latter with its paraxial version (in which $\sin \alpha_o = \alpha_{op}$, $\sin \alpha_i = \alpha_{ip}$). Since M_T is to be constant over the entire lens, we equate the magnification for both marginal and paraxial rays to get

$$\frac{\sin \alpha_o}{\sin \alpha_i} = \frac{\alpha_{op}}{\alpha_{ip}} = \text{constant}, \qquad (6.42)$$

which is known as the *sine condition.* A necessary criterion for the absence of coma is that the system meet the sine condition. If there is no SA, compliancy with the sine condition will be both necessary and sufficient for zero coma.

It's an easy matter to observe coma. In fact, anyone who has focused sunlight with a simple positive lens has no doubt seen the effects of this aberration. A slight tilt of the lens, so that the nearly collimated rays from the Sun make an angle with the optical axis, will cause the focused spot to flare out into the characteristic comet shape.

iii) Astigmatism

When an object point lies an appreciable distance from the optical axis the incident cone of rays will strike the lens asymmetrically, giving rise to a third primary aberration known as **astigmatism.** The word derives from the Greek *a-*, meaning not, and *stigma*, meaning spot or point. To facilitate its description, envision the meridional plane (also called the *tangential plane*) containing both the chief ray (i.e., the one passing through the center of the aperture) and the optical axis. The *sagittal plane* is then defined as the plane containing the chief ray, which, in addition, is perpendicular to the meridional plane (Fig. 6.22). Unlike the latter, which is unbroken from one end of a complicated lens system to the other, the sagittal plane generally changes slope as the chief ray is deviated at the various elements. Hence to be accurate we should say that there are actually several sagittal planes, one attendant with each region within the system. Nevertheless, all skew rays from the object point lying in a sagittal plane are termed *sagittal rays.*

* To be precise, the sine theorem is valid for all values of α_o only in the sagittal plane (from the Latin *sagitta*, meaning arrow), which is discussed in the next section.

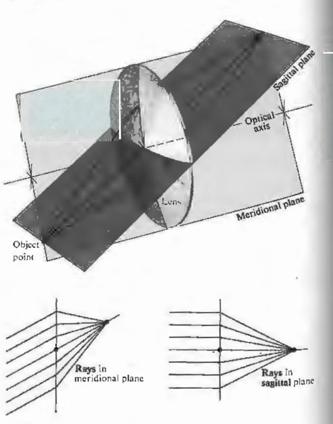


Figure 6.22 The sagittal and meridional planes.

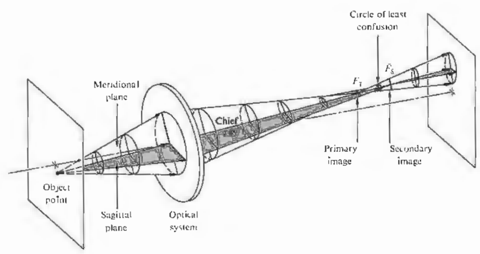


Figure 6.23 Astigmatism.

In the case of an axial object point, the cone of rays is symmetrical with respect to the spherical surfaces of a lens. There is no need to make a distinction between meridional and sagittal planes. The ray configurations in all planes containing the optical axis are identical. In the absence of spherical aberration, all the focal lengths are the same, and consequently all rays arrive at a single focus. In contrast, the configuration of an oblique, parallel ray bundle will be different in the meridional and sagittal planes. As a result, the focal lengths in these planes will be different as well. In effect, here the meridional rays are tilted more with respect to the lens than are the sagittal rays, and they have a shorter focal length. It can be shown,* using Fermat's principle, that the *focal length difference* depends effectively on the power of the lens (as opposed to the shape or index) and the angle at which the rays are inclined. This *astigmatic difference*, as it is often called, increases rapidly as the rays become more oblique, that is, as the object point moves further off the axis, and is, of course, zero on axis.

Having two distinct focal lengths, the incident conical bundle of rays takes on a considerably altered form after refraction (Fig. 6.23). The cross-section of the beam as it leaves the lens is initially circular, but it gradually becomes elliptical with the major axis in the sagittal plane, until at the *tangential* or *meridional focus* F_T, the ellipse degenerates into a *line* (at least in third-order theory). All rays from the object point traverse this line, which is known as the *primary image.* Beyond this point the beam's cross-section rapidly opens out until it is again circular. At that location the image is a circular blur known as the *circle of least confusion.* Moving further from the lens the beam's cross-section again deforms into a line, called the *secondary image.* This time it's in the meridional plane at the *sagittal focus*, F_S. Remember that in all of this we are assuming the absence of SA and coma.

Since the circle of least confusion increases in diameter as the astigmatic difference increases (i.e., as the object moves further off-axis), the image will deteriorate, losing definition around its edges. Observe that the secondary line image will change in orientation with changes in the object position, but it will always point toward the optical axis, that is, it will be radial. Similarly, the primary line image will vary in orientation, but it will remain normal to the secondary image. This arrangement causes the interesting effect shown in Fig. 6.24 when the object is made up of radial and tangential elements. The primary and secondary images are, in effect, formed of transverse and radial dashes, which increase in size with distance from the axis. In the latter case, the dashes point like arrows toward the center of the image—ergo, the name sagitta.

* See A. W. Barton, *A Text Book on Light*, p. 124.

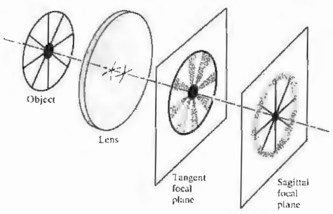


Figure 6.24 Images in the tangent and sagittal focal planes.

The existence of the sagittal and tangential foci can be verified directly with a fairly simple arrangement. Place a positive lens with a short focal length (about 10 or 20 mm) in the beam of a He–Ne laser. Position another positive test lens with a somewhat longer focal length far enough away so that the now diverging beam fills that lens. A convenient object, to be located between the two lenses, is a piece of ordinary wire screening (or a transparency). Align it so the wires are horizontal (x) and vertical (y). If the test lens is rotated roughly 45° about the vertical (with the x-, y-, and z-axes fixed in the lens), astigmatism should be observable. The meridional is the xz-plane (z being the lens axis, now at about 45° to the laser axis), and the sagittal plane corresponds to the plane of y and the laser axis. As the wire mesh is moved toward the test lens, a point will be reached where the horizontal wires are in focus on a screen beyond the lens, whereas the vertical wires are not. This is the location of the sagittal focus. Each point on the object is imaged as a short line in the meridional (horizontal) plane, which accounts for the fact that only the horizontal wires are in focus. Moving the mesh slightly closer to the lens will bring the vertical lines into clarity while the horizontal ones are blurred. This is the tangential focus. Try rotating the mesh about the central laser axis while at either focus.

Note that unlike visual astigmatism, which arose from an actual asymmetry in the surfaces of the optical system, the third-order aberration by that same name applies to spherically symmetrical lenses.

Mirrors, with the singular exception of the plane mirror, suffer much the same monochromatic aberrations as do lenses. Thus although a paraboloidal mirror is free of SA for an infinitely distant axial object point, its off-axis imagery is quite poor due to astigmatism and coma. This strongly restricts its use to narrow field devices, such as searchlights and astronomical telescopes. A concave spherical mirror shows SA, coma, and astigmatism. Indeed one could draw a diagram just like Fig. 6.23 with the lens replaced by an obliquely illuminated spherical mirror. Incidentally, such a mirror displays appreciably less SA than would a simple convex lens of the same focal length.

iv) Field Curvature

Suppose we had an optical system that was free of all the aberrations thus far considered. There would then be a one-to-one correspondence between points on the object and image surfaces (i.e., stigmatic imagery). We mentioned earlier (Section 5.2.3) that a planar object normal to the axis will be imaged approximately as a plane only in the paraxial region. At finite apertures the resulting curved stigmatic image surface is a manifestation of the primary aberration known as **Petzval field curvature**, after the Hungarian

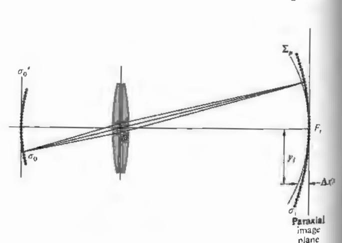


Figure 6.25 Field curvature.

mathematician Josef Max Petzval (1807–1891). The effect can readily be appreciated by examining Figs. 5.22 (p. 141) and 6.25. A spherical object segment σ_o is imaged by the lens as a spherical segment σ_i, both centered at O. Flattening out σ_o into the plane σ_o' will cause each object point to move toward the lens along the concomitant chief ray, thus forming a paraboloidal *Petzval surface* Σ_P. Whereas the Petzval surface for a positive lens curves *inward* toward the object plane, for a negative lens it curves *outward*, that is, away from that plane. Evidently, a suitable combination of positive and negative lenses will negate field curvature. Indeed, the displacement Δx of an image point at height y_i on the Petzval surface from the paraxial image plane is given by

$$\Delta x = \frac{y_i^2}{2} \sum_{j=1}^{m} \frac{1}{n_j f_j}, \tag{6.43}$$

where n_j and f_j are the indices and focal lengths of the m thin lenses forming the system. This implies that the Petzval surface will be unaltered by changes in the positions or shapes of the lenses or in the location of the stop, so long as the values of n_j and f_j are fixed. Notice that for the simple case of two thin lenses ($m = 2$) having any spacing, Δx *can be made zero* provided that

$$\frac{1}{n_1 f_1} + \frac{1}{n_2 f_2} = 0$$

or, equivalently,

$$n_1 f_1 + n_2 f_2 = 0. \tag{6.44}$$

This is the so-called *Petzval condition*. As an example of its use, suppose we combine two thin lenses, one positive, the other negative, such that $f_1 = -f_2$ and $n_1 = n_2$. Since

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2} - \frac{d}{f_1 f_2}, \tag{6.8}$$

$$f = \frac{f_1^2}{d},$$

the system can satisfy the Petzval condition, have a flat field, and still have a finite positive focal length.

In visual instruments a certain amount of curvature can be tolerated, because the eye can accommodate for it. Clearly, in photographic lenses field curvature is most undesirable, since it has the effect of rapidly blurring the off-axis image when the film plane is at F_i. An effective means of nullifying the inward curvature of a positive lens is to place a negative *field flattener* lens near the focal plane. This is often done in projection and photographic objectives when it is not otherwise practicable to meet the Petzval condition (Fig. 6.26). In this position the flattener will have little effect on other aberrations (take another look at Fig. 6.7).

Astigmatism is intimately related to field curvature. In the presence of the former aberration, there will be *two* paraboloidal image surfaces, the tangential, Σ_T, and the sagittal, Σ_S (as in Fig. 6.27). These are the loci of all the primary and secondary images, respectively, as the object point roams over the object plane. At a given height (y_i), a point on Σ_T always lies three times as far from Σ_P as does the corresponding point on Σ_S, and both are on the same side of the Petzval surface (Fig. 6.27). When there is no astigmatism Σ_S and Σ_T coalesce on Σ_P. It is possible to alter the shapes of Σ_S and Σ_T by bending or relocating the lenses or by moving the stop. The configuration of Fig. 6.27(b) is known as an *artificially flattened* field. A stop in front of an inexpensive meniscus box camera lens is usually arranged to produce just this effect. The surface of least confusion, Σ_{LC}, is

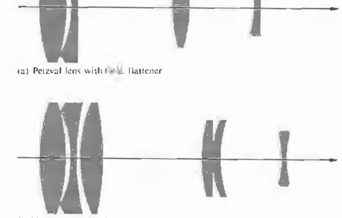


Figure 6.26 The field flattener.

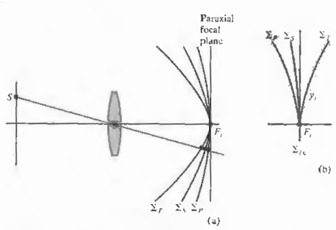


Figure 6.27 The tangential, sagittal and Petzval image surfaces.

planar, and the image there is tolerable, losing definition at the margins because of the astigmatism. That is to say, although their loci form Σ_{LC}, the circles of least confusion increase in diameter with distance off the axis. Modern good-quality photographic objectives are generally *anastigmats*; that is, they are designed so that Σ_S and Σ_T cross each other, yielding an additional off-axis angle of zero astigmatism. The Cooke Triplet, Tessar, Orthometer, and Biotar (Fig. 5.112) are all

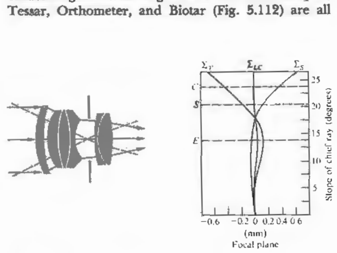


Figure 6.28 A typical Sonnar. The markings *C*, *S*, and *E* denote the limits of the 35-mm film formate (field stop), i.e., corners, sides, and edges. The Sonnar family lies between the double Gauss and the triplet.

anastigmats, as is the relatively fast Zeiss Sonn[illegible] residual astigmatism is illustrated graphically [illegible] 6.28. Note the relatively flat field and small a[illegible] astigmatism over most of the film plane.

Let's return briefly to the Schmidt camera shown in Fig. 5.107 (p. 198), since we are now in a better [illegible] to appreciate how it functions. With a stop at [illegible] of curvature of the spherical mirror, all chief ray[illegible] by definition pass through *C*, are incident nor[illegible] the mirror. Moreover, each pencil of rays from [illegible] object point is symmetrical about its chief ray [illegible] each chief ray serves as an optical axis, so th[illegible] off-axis points and, in principle, no coma or a[illegible] Instead of attempting to flatten the image [illegible] designer has coped with curvature by simply [illegible] the film plate to conform with it.

v) Distortion

The last of the five primary, monochromatic [illegible] is **distortion**. Its origin lies in the fact that the [illegible] magnification, M_T, may be a function of the [illegible] image distance, y_i. Thus, that distance may diffe[illegible] the one predicted by paraxial theory in which [illegible] constant. In other words, distortion arises [illegible] different areas of the lens have different focal [illegible] and different magnifications. In the [illegible] the other aberrations, distortion is manifest in a mis[illegible] shaping of the image as a whole, even though ea[illegible] is sharply focused. Consequently, when pro[illegible] an optical system suffering *positive* or *pincush[illegible] tion*, a square array deforms, as in Fig. 6.29(b)[illegible] instance, each image point is displaced radially [illegible] from the center, with the most distant points m[illegible] the greatest amount (i.e., M_T increases [illegible] Similarly, *negative* or *barrel distortion* correspo[illegible] situation in which M_T decreases with the axial [illegible] and in effect, each point on the image moves ra[illegible] inward toward the center [Fig. 6.29(c)]. Distortio[illegible] easily be seen by just looking through an aberra[illegible] at a piece of lined or graph paper. Fairly thin lens[illegible] will show essentially no distortion, whereas [illegible] positive or negative, thick, simple lenses will ge[illegible] suffer positive or negative distortion, respective[illegible] introduction of a stop into a system of thin le[illegible]

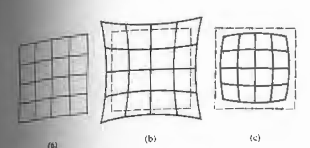


Figure 6.29 Distortion.

[illegible] accompanied by distortion, as indicated in [illegible] One exception is the case in which the aper-[illegible] lens, so that the chief ray is, in effect, [illegible] ray (i.e., it passes through the principal [illegible] coalesced at *O*). If the stop is in front of a [illegible], as in Fig. 6.30(b), the object distance [illegible] along the chief ray will be greater than it was [illegible] at the lens ($S_2A > S_2O$). Thus x_o will be [illegible] (5.26) M_T will be smaller—ergo, barrel [illegible] In other words, M_T for an off-axis point will be less with a front stop in position than it would be [illegible] The difference is a measure of the aberration, [illegible] the way, exists regardless of the size of the aperture. In the same way, a rear stop [Fig. 6.30(c)] [illegible] x_o along the chief ray (i.e., $S_2O > S_2B$), thereby increasing M_T and introducing pincushion distortion. *Interchanging the object and image thus has the effect of changing the sign of the distortion* for a given lens and stop. The aforementioned stop positions will produce the opposite effect when the lens is negative.

All of this suggests the use of a stop midway between identical lens elements. The distortion from the first lens will precisely cancel the contribution from the second. This approach has been used to advantage in the design of a number of photographic lenses (Fig. 5.112). To be sure, if the lens is perfectly symmetrical and operating as in Fig. 6.30(d), the object and image distances will be equal, hence $M_T = 1$. (Incidentally, coma and lateral color will then be identically zero as well.) This applies to (finite conjugate) copy lenses used, for example, to record data. Nonetheless, even when M_T is not 1, making the system approximately symmetrical about a stop is a very common practice, since it markedly reduces these several aberrations.

Distortion can arise in compound lens systems, as for example in the telephoto arrangement shown in Fig. 6.31. For a distant object point, the margin of the positive achromat serves as the aperture stop. In effect, the arrangement is like a negative lens with a front stop, so it displays positive or pincushion distortion.

Suppose a chief ray enters and emerges from an

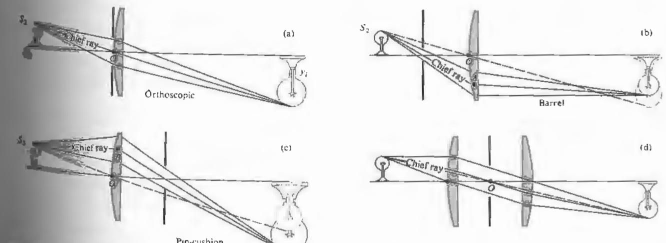


Figure 6.30 The effect of stop location on distortion.

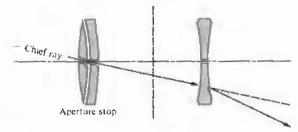


Figure 6.31 Distortion in a compound lens.

optical system in the same direction as, for example, in Fig. 6.30(d). The point at which the ray crosses the axis is the optical center of the system, but since this is a chief ray, it is also the center of the aperture stop. This is the situation approached in Fig. 6.30(a), with the stop up against the thin lens. In both instances the incoming and outgoing segments of the chief ray are parallel, and there is zero distortion, that is, the system is *orthoscopic*. This also implies that the entrance and exit pupils will correspond to the principal planes (if the system is immersed in a single medium—see Fig. 6.2). Bear in mind that the chief ray is now a principal ray. *A thin-lens system will have zero distortion if its optical center is coincident with the center of the aperture stop.* By the way, in a pinhole camera, the rays connecting conjugate object and image points are straight and pass through the center of the aperture stop. The entering and emerging rays are obviously parallel (being one and the same), and there is no distortion.

6.3.2 Chromatic Aberrations

The five primary or Seidel aberrations have been considered in terms of monochromatic light. To be sure, if the source has a broad spectral bandwidth, these aberrations are influenced accordingly; but the effects are inconsequential, unless the system is quite well corrected. There are, however, chromatic aberrations that arise specifically in polychromatic light, which are far more significant. The ray-tracing equation (6.12) is a function of the indices of refraction, which in turn vary with wavelength. Different "colored" rays will traverse a system along different paths, and this is the [illegible] tial feature of chromatic aberration.

Since the thin-lens equation

$$\frac{1}{f} = (n_l - 1)\left(\frac{1}{R_1} - \frac{1}{R_2}\right)$$

is wavelength-dependent via $n_l(\lambda)$, the focal [illegible] also vary with λ. In general (Fig. 3.26, [illegible] decreases with wavelength over the visible [illegible] thus $f(\lambda)$ increases with λ. The result is [illegible] Fig. 6.32, where the constituent colors in a collim[illegible] beam of white light are focused at different [illegible] the axis. The axial distance between two su[illegible] points spanning a given frequency range (e.g., [illegible] red) is termed the *axial* (or *longitudinal*) *chromati*[illegible] *tion*, A · CA for short.

It's an easy matter to observe chromatic abe[illegible] or CA, with a thick, simple converging len[illegible] illuminated by a polychromatic point source [illegible] cand[illegible] flame will do), the lens will cast a real image su[illegible] by a halo. If the plane of observation is then [illegible] nearer the lens, the periphery of the blurred [illegible] become tinged in orange-red. Moving it back [illegible] the lens, beyond the best image, will cause [illegible] to become tinted in blue-violet. The location of [illegible] of least confusion (i.e., the plane Σ_{LC}) correspo[illegible] the position where the best image will app[illegible] looking directly through the lens at a source—[illegible] ation will be far more striking.

The image of an off-axis point will be formed [illegible] constituent frequency components, each arrivin[illegible] different height above the axis (Fig. 6.33). In essen[illegible] the frequency dependence of f causes a [illegible]

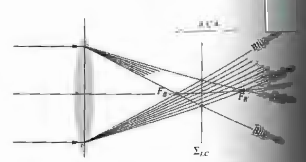


Figure 6.32 Axial chromatic aberration.

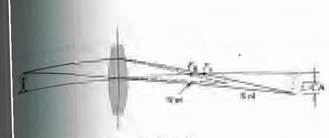


Figure 6.33 [illegible]

[illegible] of the transverse magnification as well. The [illegible] nce between two such image points (most often taken to be blue and red) is a measure of the [illegible] *matic aberration*, L · CA, or *lateral color*. Con[illegible] a chromatically aberrant lens illuminated by [illegible] will fill a volume of space with a continuum [illegible] less overlapping images, varying in size and [illegible] cause the eye is most sensitive to the yellow-[illegible] ortion of the spectrum, the tendency is to focus [illegible] for that region. With such a configuration one [illegible] all the other colored images superimposed [illegible] ly out of focus, producing a whitish blur or [illegible] erlay.

When the blue focus, F_B, is to the left of the red [illegible] cus, F_R, the A · CA is said to be positive, as it is in [illegible] Conversely, a negative lens would generate [illegible] ative A · CA, with the more strongly deviated blue [illegible] ring to originate at the right of the red focus. [illegible] what is happening is that the lens, whether convex or concave, is prismatic in shape; that is, it [illegible] her thinner or thicker as the radial distance [illegible] axis increases. As you well know, rays are [illegible] deviated either toward or away from the axis, [illegible] In both cases the rays are bent toward the [illegible] base" of the prismatic cross-section. But the [illegible] lar deviation is an increasing function of n, and [illegible] fore it decreases with λ. Hence blue light is deviated the most and is focused nearest the lens. In other words, for a convex lens the red focus is farthest and [illegible] right; for a concave lens it is farthest and to the [illegible]

[illegible] omatic Doublets

[illegible] that a combination of two thin lenses, [illegible] one negative, could conceivably result

in the precise overlapping of F_R and F_B (Fig. 6.34). Such an arrangement is said to be *achromatized* for those two specific wavelengths. Notice that what we would like to do is effectively eliminate the total dispersion (i.e., the fact that each color is deviated by a different amount) and not the total deviation itself. With the two lenses separated by a distance d,

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2} - \frac{d}{f_1 f_2}. \qquad [6.8]$$

Rather than retain the second term in the thin-lens equation (5.16), let's abbreviate the notation and write $1/f_1 = (n_1 - 1)\rho_1$ and $1/f_2 = (n_2 - 1)\rho_2$ for the two elements. Then

$$\frac{1}{f} = (n_1 - 1)\rho_1 + (n_2 - 1)\rho_2 - d(n_1 - 1)\rho_1(n_2 - 1)\rho_2. \qquad (6.45)$$

This expression will yield the focal length of the doublet for red (f_R) and blue (f_B) light when the appropriate indices are introduced, namely, n_{1R}, n_{2R}, n_{1B}, and n_{2B}. But if f_R is to equal f_B, then

$$1/f_R = 1/f_B$$

and

$$(n_{1R} - 1)\rho_1 + (n_{2R} - 1)\rho_2 - d(n_{1R} - 1)\rho_1(n_{2R} - 1)\rho_2 = (n_{1B} - 1)\rho_1 + (n_{2B} - 1)\rho_2 - d(n_{1B} - 1)\rho_1(n_{2B} - 1)\rho_2. \qquad (6.46)$$

One case of particular importance corresponds to $d = 0$, that is, the two lenses are in contact. Expanding out Eq.

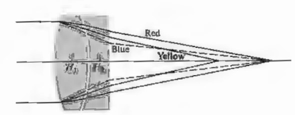


Figure 6.34 An achromatic doublet. The paths of the rays are much exaggerated.

(6.46) with $d = 0$ then leads to

$$\frac{\rho_1}{\rho_2} = -\frac{n_{2B} - n_{2R}}{n_{1B} - n_{1R}}. \tag{6.47}$$

The focal length of the compound lens (f_Y) can conveniently be specified as that associated with yellow light, roughly midway between the blue and red extremes. For the component lenses in yellow light, $1/f_{1Y} = (n_{1Y} - 1)\rho_1$ and $1/f_{2Y} = (n_{2Y} - 1)\rho_2$. Hence

$$\frac{\rho_1}{\rho_2} = \frac{(n_{2Y} - 1)}{(n_{1Y} - 1)} \frac{f_{2Y}}{f_{1Y}}. \tag{6.48}$$

Equating Eqs. (6.47) and (6.48) leads to

$$\frac{f_{2Y}}{f_{1Y}} = -\frac{(n_{2B} - n_{2R})/(n_{2Y} - 1)}{(n_{1B} - n_{1R})/(n_{1Y} - 1)}. \tag{6.49}$$

The quantities

$$\frac{n_{2B} - n_{2R}}{n_{2Y} - 1} \quad \text{and} \quad \frac{n_{1B} - n_{1R}}{n_{1Y} - 1}$$

are known as the **dispersive powers** of the two materials forming the lenses. Their reciprocals, V_2 and V_1, are variously known as the *dispersive indices, V-numbers*, or **Abbe numbers**. The lower the Abbe numbers, the greater the dispersive power. Thus

$$\frac{f_{2Y}}{f_{1Y}} = -\frac{V_1}{V_2}$$

or

$$f_{1Y}V_1 + f_{2Y}V_2 = 0. \tag{6.50}$$

Since the dispersive powers are positive, so too are the V-numbers. This implies, as we anticipated, that one of the two component lenses must be negative, and the other positive, if Eq. (6.50) is to obtain, that is, if f_R is to equal f_B.

At this point we could presumably design an *achromatic doublet*, and indeed we presently shall, but a few additional points must be made first. The designation of wavelengths as red, yellow, and blue is far too imprecise for practical application. Instead it is customary to refer to specific spectral lines whose wavelengths are known with great precision. The *Fraunhofer lines*, as they are called, serve as the needed reference markers across the spectrum. Several of these

Table 6.1 Several strong Fraunhofer lines.

Designation	Wavelength (Å)*	Source
C	6562.816 Red	H
D_1	5895.923 Yellow	Na
D	Center of doublet 5892.9	Na
D_2	5889.953 Yellow	Na
D_3 or d	5875.618 Yellow	He
b_1	5183.618 Green	Mg
b_2	5172.699 Green	Mg
c	4957.609 Green	Fe
F	4861.327 Blue	H
f	4340.465 Violet	H
g	4226.728 Violet	Ca
K	3933.666 Violet	Ca

* 1 Å = 0.1 nm.

Table 6.2 Optical glass.

Type number	Name	n_D	[illegible]
511:635	Borosilicate crown—BSC-1	1.5110	[illegible]
517:645	Borosilicate crown—BSC-2	1.5170	[illegible]
513:605	Crown—C	1.5125	[illegible]
518:596	Crown	1.5180	59.6
523:586	Crown—C-1	1.5230	[illegible]
529:516	Crown flint—CF-1	1.5286	[illegible]
541:599	Light barium crown—LBC-1	1.5411	[illegible]
573:574	Barium crown—LBC-2	1.5725	[illegible]
574:577	Barium crown	1.5744	[illegible]
611:588	Dense barium crown—DBC-1	1.6110	[illegible]
617:550	Dense barium crown—DBC-2	1.6170	55.0
611:572	Dense barium crown—DBC-3	1.6109	[illegible]
562:510	Light barium flint—LBF-2	1.5616	[illegible]
588:534	Light barium flint—LBF-1	1.5880	[illegible]
584:460	Barium flint—BF-1	1.5838	[illegible]
605:436	Barium flint—BF-2	1.6053	[illegible]
559:452	Extra light flint—ELF-1	1.5585	[illegible]
573:425	Light flint—LF-1	1.5725	42.5
580:410	Light flint—LF-2	1.5795	[illegible]
605:380	Dense flint—DF-1	1.6050	[illegible]
617:366	Dense flint—DF-2	1.6170	[illegible]
621:362	Dense flint—DF-3	1.6210	[illegible]
649:338	Extra dense flint—EDF-1	1.6490	[illegible]
666:324	Extra dense flint—EDF-5	1.6660	[illegible]
673:322	Extra dense flint—EDF-2	1.6725	[illegible]
689:309	Extra dense flint—EDF	1.6890	[illegible]
720:293	Extra dense flint—EDF-3	1.7200	[illegible]

From T. Calvert, "Optical Components," *Electromechanical Design* [illegible] Type number is given by $(n_D - 1):(10V_D)$, where n_D is rounded [illegible] decimal places. For more data see Smith, *Modern Optical Engineering* [illegible]

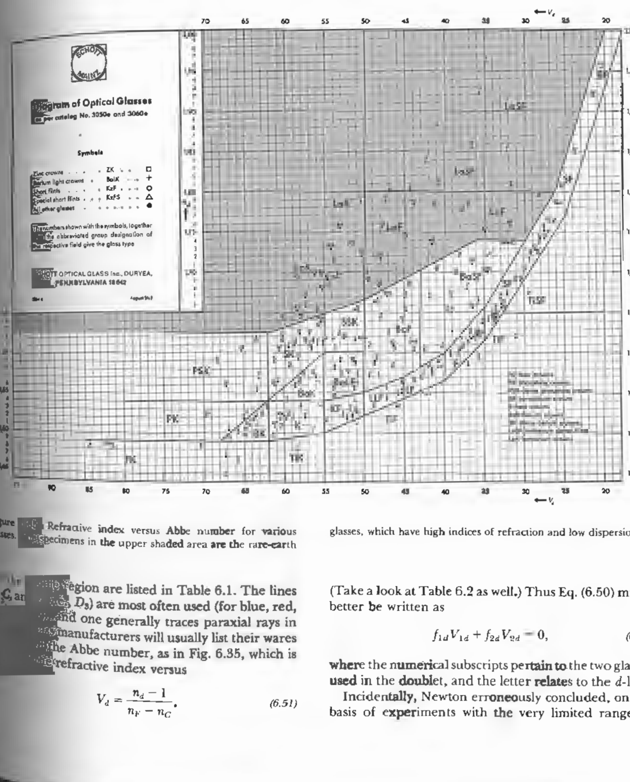


Figure [illegible] Refractive index versus Abbe number for various glasses. [illegible] specimens in the upper shaded area are the rare-earth glasses, which have high indices of refraction and low dispersions.

[illegible] region are listed in Table 6.1. The lines F, C, an[illegible] D_3) are most often used (for blue, red, [illegible] and one generally traces paraxial rays in [illegible] manufacturers will usually list their wares [illegible] the Abbe number, as in Fig. 6.35, which is [illegible] refractive index versus

$$V_d = \frac{n_d - 1}{n_F - n_C}. \tag{6.51}$$

(Take a look at Table 6.2 as well.) Thus Eq. (6.50) might better be written as

$$f_{1d}V_{1d} + f_{2d}V_{2d} = 0, \tag{6.52}$$

where the numerical subscripts pertain to the two glasses used in the doublet, and the letter relates to the d-line.

Incidentally, Newton erroneously concluded, on the basis of experiments with the very limited range of materials available at the time, that the dispersive power was constant for all glasses. This is tantamount to saying (Eq. 6.52) that $f_{1d} = -f_{2d}$, in which case the doublet would have zero power. Newton, accordingly, shifted his efforts from the refracting to the reflecting telescope, and this fortunately turned out to be a good move in the long run. The achromat was invented around 1733 by Chester Moor Hall, Esq., but it lay in limbo until it was seemingly reinvented and patented in 1758 by the London optician John Dollond.

Several forms of the achromatic doublet are shown in Fig. 6.36. Their configurations depend on the glass types selected, as well as on the choice of the other aberrations to be controlled. By the way, when purchasing off-the-shelf doublets of unknown origin, be careful not to buy a lens that has been deliberately designed to include certain aberrations in order to compensate for errors in the original system from which it came. Perhaps the most commonly encountered doublet is the cemented Fraunhofer achromat. It's formed of a crown* double-convex lens in contact with a concave-planar (or nearly planar) flint lens. The use of a crown front element is quite popular because of its resistance to wear. Since the overall shape is roughly convex-planar, by selecting the proper glasses, both spherical aberration and coma can be corrected as well. Suppose that we wish to design a Fraunhofer achromat of focal length 50 cm. We can get some idea of how to select glasses by solving Eq. (6.52) simultaneously with the compound-lens equation

$$\frac{1}{f_{1d}} + \frac{1}{f_{2d}} = \frac{1}{f_d}$$

to get

$$\frac{1}{f_{1d}} = \frac{V_{1d}}{f_d(V_{1d} - V_{2d})} \tag{6.53}$$

and

$$\frac{1}{f_{2d}} = \frac{V_{2d}}{f_d(V_{2d} - V_{1d})}, \tag{6.54}$$

* Traditionally the glasses in the range $n_d > 1.60$, $V_d > 50$, and $n_d < 1.60$, $V_d > 55$ are known as *crowns*, and the others are *flints*. Note the letter designations in Fig. 6.35.

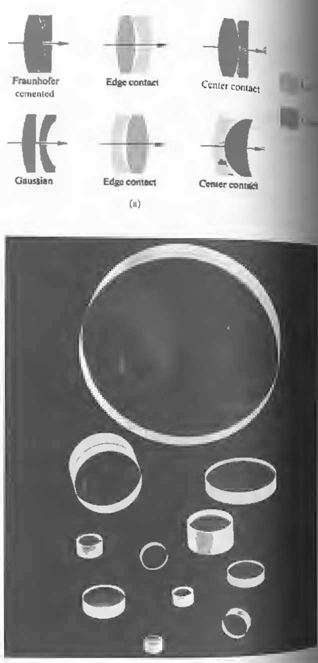


Figure 6.36 (a) Achromatic doublets. (b) Doublets and [illegible] (Photo courtesy Melles Griot.)

[illegible]r to avoid small values of f_{1d} and f_{2d}, which [illegible]itate strongly curved surfaces on the com[illegible], the difference $V_{1d} - V_{2d}$ should be made [illegible]ly 20 or more is convenient). From Fig. [illegible]quivalent) we select, say, BK1 and F2. These [illegible]ed indices of $n_C = 1.50763$, $n_d = 1.51009$, [illegible] and $n_C = 1.61503$, $n_d = 1.62004$, $n_F =$ [illegible]08, respectively. Likewise, their V-numbers are [illegible]lly given rather accurately, and we needn't com[illegible]. In this instance they are $V_{1d} = 63.46$ and [illegible]7, respectively. The focal lengths, or if you [illegible] powers of the two lenses, are given by Eqs. [illegible] (6.54):

$$\mathcal{D}_{1d} = \frac{1}{f_{1d}} = \frac{63.46}{0.50(27.09)}$$

and

$$\mathcal{D}_{2d} = \frac{1}{f_{2d}} = \frac{36.37}{0.50(-27.09)}.$$

Hence [illegible] $= 4.685$ D and $\mathcal{D}_{2d} = -2.685$ D, the sum [illegible]ng 2 D, which is 1/0.5, as it should be. For ease of [illegible]ication let the first or positive lens be equiconvex. [illegible]equently its radii R_{11} and R_{12} are equal in magni[illegible] Hence

$$\rho_1 = \frac{1}{R_{11}} - \frac{1}{R_{12}} = \frac{2}{R_{11}}$$

or, [illegible]

$$[illegible] = \frac{\mathcal{D}_{1d}}{n_{1d} - 1} = \frac{4.685}{0.51009} = 9.185.$$

[illegible] $= -R_{12} = 0.2177$ m. Furthermore, having [illegible]that the lenses be in intimate contact, we have [illegible] that is, the second surface of the first lens [illegible]e first surface of the second lens. For the [illegible]

$$\rho_2 = \frac{1}{R_{21}} - \frac{1}{R_{22}} = \frac{\mathcal{D}_{2d}}{n_{2d} - 1}$$

or

$$\frac{1}{-0.2177} - \frac{1}{R_{22}} = \frac{-2.685}{0.62004}$$

[illegible] $R_{22} =$ [illegible]9 m. In summary, the radii of the crown

element are $R_{11} = 21.8$ cm and $R_{12} = -21.8$ cm while the flint has radii of $R_{21} = -21.8$ cm and $R_{22} = -381.9$ cm.

Note that for a thin-lens combination the principal planes coalesce, so that achromatizing the focal length corrects both A · CA and L · CA. In a thick doublet, however, even though the focal lengths for red and blue are made identical, the different wavelengths may have different principal planes. Consequently, although the magnification is the same for all wavelengths, the focal points may not coincide; in other words, correction is made for L · CA but not for A · CA.

In the above analysis only the C- and F-rays were brought to a common focus, and the d-line was introduced to establish a focal length for the doublet as a whole. It is not possible for *all* wavelengths traversing a doublet achromat to meet at a common focus. The resulting residual chromatism is known as *secondary spectrum*. The elimination of secondary spectrum is particularly troublesome when the design is limited to the glasses currently available. Nevertheless, a fluorite (CaF_2) element combined with an appropriate glass element can form a doublet achromatized at three wavelengths and having very little secondary spectrum. More often triplets are used for color correction at three or even four wavelengths. The secondary spectrum of a binocular can easily be observed by looking at a distant white object. Its borders will be slightly haloed in magenta and green—try shifting the focus forward and backward.

ii) Separated Achromatic Doublets

It is also possible to achromatize the focal length of a doublet composed of two widely separated elements of the same glass. Return to Eq. (6.46) and set $n_{1R} = n_{2R} = n_R$ and $n_{1B} = n_{2B} = n_B$. After a bit of straightforward algebraic manipulation, it becomes

$$(n_R - n_B)[(\rho_1 + \rho_2) - \rho_1 \rho_2 d(n_B + n_R - 2)] = 0$$

or

$$d = \frac{1}{(n_B + n_R - 2)}\left(\frac{1}{\rho_1} + \frac{1}{\rho_2}\right).$$

Again introducing the yellow reference frequency, as we did before, namely, $1/f_{1Y} = (n_{1Y} - 1)\rho_1$ and $1/f_{2Y} =$

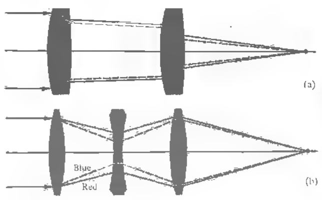


Figure 6.37 Achromatized lenses.

$(n_{2Y} \quad 1)\rho_2$, we can replace ρ_1 and ρ_2. Hence

$$d = \frac{(f_{1Y} + f_{2Y})(n_Y - 1)}{n_B + n_R - 2},$$

where $n_{1Y} = n_{2Y} = n_Y$. Assuming $n_Y \quad (n_B + n_R)/2$, we have

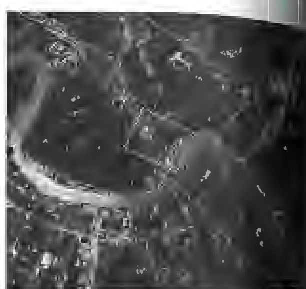
$$d = \frac{f_{1Y} + f_{2Y}}{2}$$

or in d-light

$$d = \frac{f_{1d} + f_{2d}}{2}. \tag{6.55}$$

This is precisely the form taken by the Huygens ocular (Section 5.7.4). Since the red and blue focal lengths are the same, but the corresponding principal planes for the doublet need not be, the two rays will generally not meet at the same focal point. Thus the ocular's lateral chromatic aberration is well corrected, but axial chromatic aberration is not.

In order for a system to be free of both chromatic aberrations, the red and blue rays must emerge parallel to each other (no L · CA) and must intersect the axis at the same point (no A · CA), which means they must overlap. Since this is effectively the case with a thin achromat, it implies that multielement systems, as a rule, should consist of achromatic components in order to keep the red and blue rays from separating (Fig. 6.37). As with all such invocations there are exceptions. The Taylor triplet (Section 5.7.7) is one. The two colored rays for which it is achromatized separate within the lens but are recombined and emerge together.



(a)

(b)

Figure 6.38 a, b

(c)

(a) New Orleans and the Mississippi River photo- 12,500 m (41,000 ft) with Itek's Metritek-21 camera ound resolution, 1 m; scale, 1:59,492. (b) Photo scale, 0. (c) Photo scale, 1:2500.

6.3.3 Concluding Remarks

For the practical reason of manufacturing ease, the vast majority of optical systems are limited to lenses having spherical surfaces. There are, to be sure, toric and cylindrical lenses as well as many other asphericS. Indeed, very fine, and as a rule very expensive devices, such as high-altitude reconnaisance cameras and tracking systems, may have several aspherical elements. Even so, spherical lenses are here to stay and with them are their inherent aberrations which must satisfactorily be dealt with. As we have seen, the designer (and his faithful electronic companion) must manipulate the system variables (indices, shapes, spacings, stops, etc.) in order to balance out offensive aberrations. This is done to whatever degree and in whatever order is appropriate for the specific optical system. Thus one might tolerate far more distortion and curvature in an ordinary telescope than in a good photographic objective. Likewise, there is little need to worry about chromatic aberration if you want to work exclusively with laser light of almost a single frequency. In any event, this chapter has only touched on the problems (more to appreciate than solve them). That they are most certainly amenable to solution is evidenced, for example, by the remarkable aerial photographs in Fig. 6.38, which speak rather eloquently for themselves.

PROBLEMS

6.1* Work out the details leading to Eq. (6.8).

6.2 According to the military handbook MIL-HDBK-141 (23.3.5.3), the Ramsden eyepiece (Fig. 5.93) is made up of two planar-convex lenses of equal focal length f' separated by a distance $2f'/3$. Determine the overall focal length f of the thin-lens combination and locate the principal planes and the position of the field stop.

6.3 Write an expression for the thickness d of a double-convex lens such that its focal length is infinite.

6.4 Suppose we have a positive meniscus lens of radii 6 and 10 and a thickness of 3 (any units, as long as you're consistent), with an index of 1.5. Deter[illegible] its focal length and the locations of its principal [illegible] (compare with Fig. 6.3).

6.5 Using Eq. (6.2), derive an expression [illegible] length of a homogeneous transparent [illegible] R. Locate its principal points.

6.6* A spherical glass bottle 20 cm in diame[illegible] walls that are negligibly thin is filled with wate[illegible] bottle is sitting on the back seat of a [illegible] day. What's its focal length?

6.7* With the previous two problems in [illegible] pute the magnification that results when the im[illegible] a flower 4.0 m from the center of a solid, clear [illegible] sphere with a 0.20-m diameter (and a refractive [illegible] of 1.4) is cast on a nearby wall. Describe the ima[illegible] in detail.

6.8* A thick glass lens of index 1.50 has radii of +23 cm and +20 cm, so that both [illegible] of the corresponding centers of curvature. Given that the thickness is 9.0 cm, find the focal [illegible]. Show that in general $R_1 - R_2 = d/3$ for such afo[illegible] power lenses. Draw a diagram showing what [illegible] to an axial incident parallel bundle of rays as [illegible] through the system.

6.9 It is found that sunlight is focused to a sp[illegible] from the back face of a thick lens, which has its [illegible] points at $H_1 = +0.2$ cm and $H_2 = -0.4$ cm. [illegible] the location of the image of a candle that is place[illegible] 49.8 cm in front of the lens.

6.10* Please establish that the separation between principal planes for a thick glass lens is roughly one third its thickness. The simplest geometry occ[illegible] a planar-convex lens tracing a ray from the obje[illegible] What can you say about the relationship betw[illegible] focal length and the thickness for this lens type?

6.11 A crown glass double-convex lens, [illegible] and operating at a wavelength of 900 nm, has [illegible] of refraction of 3/2. Given that its radii are 4.0 [illegible] 15 cm, locate its principal points and compute its [illegible]

[illegible] television screen is placed 1.0 m from the [illegible], where will the real image of the picture [illegible]

6.12* [illegible]agine two identical double-convex thick lenses [illegible]parated by a distance of 20 cm between their [illegible] vertices. Given that all the radii of curvature [illegible] the refractive indices are 1.5, and the thickness [illegible] lens is 5.0 cm, calculate the combined focal length.

[illegible] compound lens is composed of two thin lenses [illegible] by 10 cm. The first of these has a focal length [illegible], and the second a focal length of −20 cm. [illegible] the focal length of the combination and locate the corresponding principal points. Draw a diagram of the system.

6.14* A [illegible]nvex-planar lens of index 3/2 has a thickness of [illegible].2 cm and a radius of curvature of 2.5 cm. [illegible] system matrix when light is incident on [illegible]

6.[illegible] Show that the determinant of the system matrix in [illegible](6.31) is equal to 1.

6.16 Show that Eqs. (6.36) and (6.37) are equivalent to Eqs. (6.3) and (6.4), respectively.

6.17 [illegible]w that the planar surface of a concave-planar [illegible] doesn't contribute to the system matrix.

6.18 [illegible]mpute the system matrix for a thick biconvex lens of index 1.5 having radii of 0.5 and 0.25 and a [illegible] of 0.3 (in any units you like). Check that [illegible] = 1.

6.19* [illegible] matrix for a thick biconvex lens in air is given by

$$\begin{bmatrix} 0.6 & -2.6 \\ 0.2 & 0.8 \end{bmatrix}.$$

Knowing that the first radius is 0.5 cm, that the thickness is 0.3 cm, and that the index of the lens is 1.5, find the other radius.

6.20* A concave-planar glass ($n = 1.50$) lens in air has a radius of 10.0 cm and a thickness of 1.00 cm. Determine the system matrix and check that its determinant is 1. At what positive angle (in radians measured above the axis), should a ray strike the lens at a height of 2.0 cm, if it is to emerge from the lens at the same height but parallel to the optical axis?

6.21* Considering the lens in Problem 6.18, determine its focal length and the location of the focal points with respect to its vertices V_1 and V_2.

6.22 Referring back to Fig. 6.15, show that when $\overline{P'P} = Rn_2/n_1$ and $\overline{PC} = Rn_1/n_2$ all rays originating at P appear to come from P'.

6.23 Starting with the exact expression given by Eq. (5.5), show that Eq. (6.40) results, rather than Eq. (5.8), when the approximations for ℓ_o and ℓ_i are improved a bit.

6.24 Supposing that Fig. 6.39 is to be imaged by a lens system suffering spherical aberration only, make a sketch of the image.

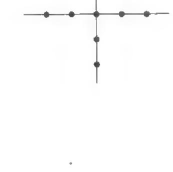


Figure 6.39

7 THE SUPERPOSITION OF WAVES

In succeeding chapters we shall study the phenomena of polarization, interference, and diffraction. These all share a common conceptual basis in that they deal, for the most part, with various aspects of the same process. Stating this in the simplest terms, we are really concerned with what happens when two or more light waves overlap in some region of space. The precise circumstances governing this superposition, of course, determine the final optical disturbance. Among other things we are interested in learning how the specific properties of each constituent wave (amplitude, phase, frequency, etc.) influence the ultimate form of the composite disturbance.

Recall that each field component of an electromagnetic wave (E_x, E_y, E_z, B_x, B_y, and B_z) satisfies the scalar three-dimensional differential wave equation,

$$\frac{\partial^2\psi}{\partial x^2}+\frac{\partial^2\psi}{\partial y^2}+\frac{\partial^2\psi}{\partial z^2}=\frac{1}{v^2}\frac{\partial^2\psi}{\partial t^2}. \qquad [2.59]$$

A significant feature of this expression is that it is *linear;* in other words, $\psi(\mathbf{r}, t)$ and its derivatives appear only to the first power. Consequently, if $\psi_1(\mathbf{r}, t)$, $\psi_2(\mathbf{r}, t), \ldots, \psi_n(\mathbf{r}, t)$ are individual solutions of Eq. (2.59), *any linear combination* of them will, in turn, be a solution. Thus

$$\psi(\mathbf{r}, t) = \sum_{i=1}^{n} C_i\psi_i(\mathbf{r}, t) \qquad (7.1)$$

satisfies the wave equation, where the coefficients C_i are simply arbitrary constants. Known as the *principle of superposition,* this property suggests that the resultant disturbance at any point in a medium is the alge... sum of the separate constituent waves (Fig. 7.1). A...

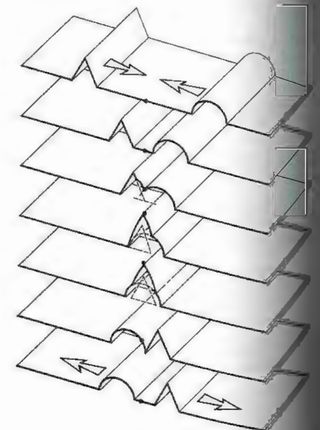


Figure 7.1 The superposition of two disturbances.

...interested only in linear systems where the ...on principle is actually applicable. Do keep ...wever, that large-amplitude waves, whether ...or waves on a string, can generate a non... response. The focused beam of a high-intensity ...where the electric field might be as high as ...V/cm) is easily capable of eliciting nonlinear effects (see Chapter 14). By comparison, the electric field ...ed with sunlight here on Earth has an amplitude ...about 10 V/cm.

There are many instances in which we need not be ...with the vector nature of light, and for the ...t we will restrict ourselves to such cases. For ...ple, if the lightwaves all propagate along the same ...and share a common constant plane of vibration, ...could each be described in terms of one electric-field component. These would all be either parallel or ...parallel at any instant and could thus be treated as scalars. A good deal more will be said about this point as we progress; for now, let's represent the optical disturbance as a scalar function $E(\mathbf{r}, t)$, which is a solution of Eq. (2.59). This approach leads to a simple scalar theory that is highly useful as long as we are careful about applying it.

...ADDITION OF WAVES OF THE SAME ...QUENCY

7.1 ...LGEBRAIC METHOD

...call that we can write a solution of the differential ...ve equation in the form

$$E(x, t) = E_0 \sin [\omega t - (kx + \epsilon)], \qquad (7.2)$$

in which E_0 is the amplitude of the harmonic disturbance propagating along the positive x-axis. Alternatively, let

$$\alpha(x, \epsilon) = -(kx + \epsilon) \qquad (7.3)$$

so that

$$E(x, t) = E_0 \sin [\omega t + \alpha(x, \epsilon)]. \qquad (7.4)$$

Suppose then that we have two such waves

$$E_1 = E_{01} \sin (\omega t + \alpha_1) \qquad (7.5a)$$

and

$$E_2 = E_{02} \sin (\omega t + \alpha_2), \qquad (7.5b)$$

each with the same frequency and speed, overlapping in space. The resultant disturbance is the linear superposition of these waves. Thus

$$E = E_1 + E_2$$

or, on expanding Eqs. (7.5a) and (7.5b),

$$E = E_{01}(\sin \omega t \cos \alpha_1 + \cos \omega t \sin \alpha_1) + E_{02}(\sin \omega t \cos \alpha_2 + \cos \omega t \sin \alpha_2).$$

When we separate out the time-dependent terms this becomes

$$E = (E_{01} \cos \alpha_1 + E_{02} \cos \alpha_2) \sin \omega t + (E_{01} \sin \alpha_1 + E_{02} \sin \alpha_2) \cos \omega t. \qquad (7.6)$$

Since the bracketed quantities are constant in time, let

$$E_0 \cos \alpha = E_{01} \cos \alpha_1 + E_{02} \cos \alpha_2 \qquad (7.7)$$

and

$$E_0 \sin \alpha = E_{01} \sin \alpha_1 + E_{02} \sin \alpha_2. \qquad (7.8)$$

This is not an obvious substitution, but it will be legitimate as long as we can solve for E_0 and α. To that end, square and add Eqs. (7.7) and (7.8) to get

$$E_0^2 = E_{01}^2 + E_{02}^2 + 2E_{01}E_{02} \cos (\alpha_2 - \alpha_1) \qquad (7.9)$$

and divide Eq. (7.8) by (7.7) to get

$$\tan \alpha = \frac{E_{01} \sin \alpha_1 + E_{02} \sin \alpha_2}{E_{01} \cos \alpha_1 + E_{02} \cos \alpha_2}. \qquad (7.10)$$

Provided these last two expressions are satisfied for E_0 and α, the situation of Eqs. (7.7) and (7.8) is valid. The total disturbance then becomes

$$E = E_0 \cos \alpha \sin \omega t + E_0 \sin \alpha \cos \omega t$$

or

$$E = E_0 \sin (\omega t + \alpha). \qquad (7.11)$$

Thus a single disturbance results from the superposition

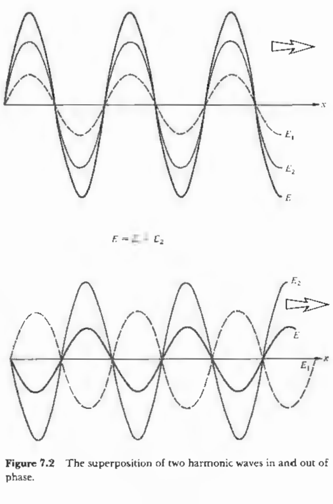


Figure 7.2 The superposition of two harmonic waves in and out of phase.

of the sinusoidal waves E_1 and E_2. *The composite wave (7.11) is harmonic and of the same frequency as the constituents, although its amplitude and phase are different.* The flux density of a light wave is proportional to its amplitude squared, by way of Eq. (3.44). Hence it follows from Eq. (7.9) that the resultant flux density is not simply the sum of the component flux densities—there is an additional contribution $2E_{01}E_{02}\cos(\alpha_2 - \alpha_1)$, known as the **interference term**. The crucial factor is the difference in phase between the two *interfering* waves E_1 and E_2, $\delta \equiv (\alpha_2 - \alpha_1)$. When $\delta = 0, \pm 2\pi, \pm 4\pi, \ldots$ the resultant amplitude is a maximum, whereas $\delta = \pm\pi, \pm 3\pi, \ldots$ yields a minimum (Problem 7.3). In the former case, the waves are said to be in pha… overlaps crest. In the latter instance the waves a… out of phase and trough overlaps crest, as shown… 7.2. Realize that the *phase difference* may arise from a difference in path length traversed by the two … as well as a difference in the initial phase angle …

$$\delta = (kx_1 + \varepsilon_1) - (kx_2 + \varepsilon_2)$$

or

$$\delta = \frac{2\pi}{\lambda}(x_1 - x_2) + (\varepsilon_1 - \varepsilon_2).$$

Here x_1 and x_2 are the distances from the sources … the two waves to the point of observation, and … wavelength in the pervading medium. If the wav… initially in phase at their respective emitters, t… ε_2, and

$$\delta = \frac{2\pi}{\lambda}(x_1 - x_2).$$

This would also apply to the case in which two di… bances from the same source traveled different routes before arriving at the point of observation. Since $n = c/v = \lambda_0/\lambda$,

$$\delta = \frac{2\pi}{\lambda_0} n(x_1 - x_2).$$

The quantity $n(x_1 - x_2)$ is known as the **optical… difference** and will be represented by the abbrev… OPD or by the symbol Λ. It's the difference in the two optical path lengths [Eq. (4.9)]. Bear in mind that it … possible, in more complicated situations, for each wave to travel through a number of different thicknesses of different media (Problem 7.6). Notice … $(x_1 - x_2)/\lambda$ is the number of waves in the med… sponding to the path difference; one route is … wavelengths longer than the other. Si… wavelength is associated with a 2π radian phase … $\delta = 2\pi(x_1 - x_2)/\lambda$, or, more succinctly,

$$\delta = k_0\Lambda,$$

k_0 being the propagation number in vacuum … $2\pi/\lambda_0$. One route is essentially δ radians longer than the other.

Waves for which $\varepsilon_1 - \varepsilon_2$ is *constant*, regardless of …

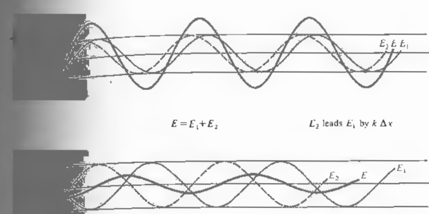


Figure 7.3 Waves out of phase by $k\Delta x$.

…aid to be **coherent**, a situation we shall assume …roughout most of this discussion.

…ecial case of some interest is the superposition of the waves

$$E_1 = E_{01}\sin[\omega t - k(x + \Delta x)]$$

and

$$E_2 = E_{02}\sin(\omega t - kx),$$

…in particular $E_{01} = E_{02}$ and $\alpha_2 - \alpha_1 = k\,\Delta x$. It is …Problem 7.7 to show that in this case Eqs. (7.9), … and (7.11) lead to a resultant wave of

$$E = 2E_{01}\cos\left(\frac{k\,\Delta x}{2}\right)\sin\left[\omega t - k\left(x + \frac{\Delta x}{2}\right)\right]. \qquad (7.17)$$

…gs out rather clearly the dominant role played …h-length difference, Δx, especially when the … emitted in phase ($\varepsilon_1 = \varepsilon_2$). There are many …instances in which one arranges just these conditions, as will be seen later. If $\Delta x \ll \lambda$, the resultant has an amplitude that is nearly $2E_{02}$, whereas if $\Delta x = \lambda/2$, it is zero. The former situation is referred to as **constructive interference**, and the latter as **destructive interference** (see Fig. 7.3).

By repeated applications of the procedure used to arrive at Eq. (7.11), we can show that the *superposition of any number of coherent harmonic waves having a given frequency and traveling in the same direction leads to a harmonic wave of that same frequency* (Fig. 7.4). We happen to have chosen to represent the two waves above in terms of sine functions, but the same results would prevail if we used cosine functions. In general, then, the sum of N such waves,

$$E = \sum_{i=1}^{N} E_{0i}\cos(\alpha_i \pm \omega t),$$

is given by

$$E = E_0\cos(\alpha \pm \omega t), \qquad (7.18)$$

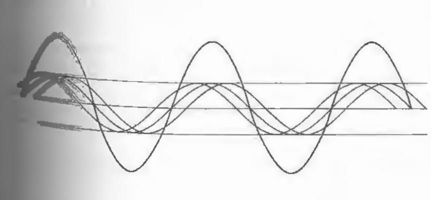


Figure 7.4 The superposition of three harmonic waves yields a harmonic wave.

where

$$E_0^2 = \sum_{i=1}^{N} E_{0i}^2 + 2\sum_{j>i}^{N}\sum_{i=1}^{N} E_{0i}E_{0j}\cos(\alpha_i - \alpha_j) \quad (7.19)$$

and

$$\tan\alpha = \frac{\sum_{i=1}^{N} E_{0i}\sin\alpha_i}{\sum_{i=1}^{N} E_{0i}\cos\alpha_i}. \quad (7.20)$$

Pause for a moment and satisfy yourself that these relations are indeed true.

Consider a number (N) of atomic emitters comprising an ordinary light source (an incandescent bulb, candle flame, or discharge lamp). Each atom is effectively an independent source of photon wavetrains (Section 3.4.4), and these, in turn, each extend in time for roughly 1 to 10 ns. In other words, the atoms generally emit wavetrains that have a sustained phase for only up to about 10 ns, after which a new wavetrain may be emitted with a totally random phase, and it too will be sustained for less than approximately 10 ns, and so forth. On the whole each atom may be thought of as emitting a disturbance composed of a stream of photons that varies in its phase rapidly and randomly. In any event, the phase of the light from one atom, $\alpha_i(t)$, will remain constant with respect to the phase from another atom $\alpha_j(t)$, for only a time of at most 10 ns before it changes randomly: the atoms are coherent for up to about 10^{-8} s. Since flux density is proportional to the time average of E_0^2, generally taken over a comparatively long interval of time, it follows that the second summation in Eq. (7.19) will contribute terms proportional to $\langle\cos[\alpha_i(t) - \alpha_j(t)]\rangle$, each of which will average out to zero because of the random rapid nature of the phase changes. Only the first summation remains in the time average, and its terms are constants. If the atoms are each emitting wavetrains of the same amplitude E_{01}, then

$$E_0^2 = NE_{01}^2. \quad (7.21)$$

The resultant flux density arising from N sources having random, rapidly varying phases is given by N times the flux density of any one source. In other words, *it is determined by the sum of the individual flux densities.* A flashlight whose atoms are all emitting a random tumult p[illegible] light, which, as the superposition of these ess[illegible] "incoherent" wavetrains, is itself rapidly and ran[illegible] varying in phase. Thus two or more such bulbs wil[illegible] light that is essentially incoherent (i.e., for du[illegible] longer than about 10 ns), light whose total com[illegible] irradiance will simply equal the sum of the [illegible] contributed by each individual bulb. This is [illegible] for candle flames, flashbulbs, and all thermal [illegible] from laser) sources. We cannot expect to *see* [illegible] ence when the lightwaves from two reading [illegible] overlap.

At the other extreme, if the sources are coherent [illegible] in phase at the point of observation (i.e., $\alpha_i = \alpha_j$), [illegible] (7.19) will become

$$E_0^2 = \sum_{i=1}^{N} E_{0i}^2 + 2\sum_{j>i}^{N}\sum_{i=1}^{N} E_{0i}E_{0j}$$

or, equivalently,

$$E_0^2 = \left(\sum_{i=1}^{N} E_{0i}\right)^2.$$

Again supposing that each amplitude is E_{01}, we get

$$E_0^2 = (NE_{01})^2 = N^2E_{01}^2. \quad (7.22)$$

In this case of in-phase coherent sources, we have a situation in which the amplitudes are added first and then squared to determine the resulting flux density. The superposition of coherent waves generally has the effect of altering the spatial distribution of the energy but not the total amount present. If there are regions where the flux density is greater than the sum of the individual flux densities, there will be regions where it is less than the sum.

7.2 THE COMPLEX METHOD

It is often mathematically convenient to make use of the complex representation of trigonometric functions when dealing with the superposition of harmonic disturbances. The wave

$$E_1 = E_{01}\cos(kx \pm \omega t + \varepsilon_1)$$

or

$$E_1 = E_{01}\cos(\alpha_1 \mp \omega t)$$

can then be written as

$$E_1 = E_{01}e^{i(\alpha_1 \mp \omega t)}, \quad (7.24)$$

if we remember that we are interested only in the real part (see Section 2.4). Suppose that there are N such overlapping waves having the same frequency and traveling in the *positive x-direction.* The resultant wave is given by

$$E = E_0e^{i(\alpha + \omega t)},$$

which is equivalent to Eq. (7.18) or, upon summation of the component waves,

$$E = \left[\sum_{j=1}^{N} E_{0j}e^{i\alpha_j}\right]e^{+i\omega t}. \quad (7.25)$$

The quantity

$$E_0e^{i\alpha} = \sum_{j=1}^{N} E_{0j}e^{i\alpha_j} \quad (7.26)$$

is known as the *complex amplitude* of the composite wave and is simply the sum of the complex amplitudes of the constituents. Since

$$E_0^2 = (E_0e^{i\alpha})(E_0e^{i\alpha})^*, \quad (7.27)$$

we can always compute the resultant irradiance from Eqs. (7.26) and (7.27). For example, if $N = 2$,

$$E_0^2 = (E_{01}e^{i\alpha_1} + E_{02}e^{i\alpha_2})(E_{01}e^{-i\alpha_1} + E_{02}e^{-i\alpha_2}),$$

whence

$$E_0^2 = E_{01}^2 + E_{02}^2 + E_{01}E_{02}[e^{i(\alpha_1-\alpha_2)} + e^{-i(\alpha_1-\alpha_2)}]$$

or

$$E_0^2 = E_{01}^2 + E_{02}^2 + 2E_{01}E_{02}\cos(\alpha_1 - \alpha_2),$$

which is identical to Eq. (7.9).

7.3 PHASOR ADDITION

The summation described in Eq. (7.26) can be represented graphically as an addition of vectors in the complex plane (recall the Argand diagram in Fig. 2.11). In the parlance of electrical engineering, the complex amplitude is known as a **phasor**, and it is specified by its magnitude and phase, often written simply in the form $E_0\angle\alpha$. The method of phasor addition to be developed now can be employed without any appreciation of its relationship to the complex-number formalism. For simplicity's sake, we will for the most part circumvent the use of that interpretation in what is to follow. Imagine, then, that we have a disturbance described by

$$E_1 = E_{01}\sin(\omega t + \alpha_1).$$

In Fig. 7.5(a) we represent the wave by a vector of length E_{01} rotating counterclockwise at a rate ω such that its projection on the vertical axis is $E_{01}\sin(\omega t + \alpha_1)$. If we were concerned with cosine waves, we would take the projection on the horizontal axis. Incidentally, the rotating vector is, of course, a phasor $E_{01}\angle\alpha_1$, and the R and

Figure 7.5 Phasor addition.

I designations signify the real and imaginary axes. Similarly, a second wave

$$E_2 = E_{02} \sin (\omega t + \alpha_2)$$

is depicted along with E_1 in Fig. 7.5(b). Their algebraic sum, $E = E_1 + E_2$, is the projection on the I-axis of the resultant phasor determined by the vector addition of the component phasors, as in Fig. 7.5(c). The law of cosines applied to the triangle of sides E_{01}, E_{02}, and E_0 yields

$$E_0^2 = E_{01}^2 + E_{02}^2 + 2E_{01}E_{02} \cos (\alpha_2 - \alpha_1),$$

where use was made of the fact that $\cos [\pi - (\alpha_2 - \alpha_1)] = -\cos (\alpha_2 - \alpha_1)$. This is identical to Eq. (7.9), as it must be. Using the same diagram, observe that $\tan \alpha$ is given by Eq. (7.10) as well. We are usually concerned with finding E_0 rather than $E(t)$, and since E_0 is unaffected by the constant revolving of all the phasors, it will often be convenient to set $t = 0$ and thus eliminate that rotation.

Some rather elegant schemes, such as the *vibration curve* and the *Cornu spiral* (Chapter 10), will be predicated on the technique of phasor addition. Moreover,

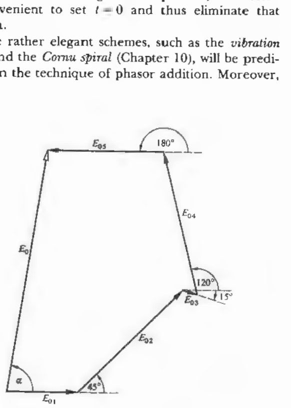


Figure 7.6 The sum of E_1, E_2, E_3, E_4 and E_5.

it is a pictorial approach, and that often helps [illegible] insights. As a final example, let's briefly exa[illegible] wave resulting from the addition of

$$E_1 = 5 \sin \omega t$$
$$E_2 = 10 \sin (\omega t + 45°)$$
$$E_3 = \sin (\omega t - 15°)$$
$$E_4 = 10 \sin (\omega t + 120°)$$

and

$$E_5 = 8 \sin (\omega t + 180°),$$

where ω is in degrees per second. The approp[illegible] phasors $5\angle 0°$, $10\angle 45°$, $1\angle -15°$, $10\angle 120°$, and $8\angle$[illegible] are plotted in Fig. 7.6. Notice that each phase [illegible], whether positive or negative, is referenced to the horizontal. One need only read off $E_0\angle\alpha$ with a scal[illegible] and protractor to get $E = E_0 \sin (\omega t + \alpha)$. It [illegible] that this technique offers a tremendous advant[illegible] in speed and simplicity, if not in accuracy.

7.4 STANDING WAVES

We saw in Chapter 2 that the general solution [illegible] the differential wave equation consisted of the sum [illegible] traveling waves,

$$\psi(x, t) = C_1 f(x - vt) + C_2 g(x + vt). \quad [illegible]$$

In particular let us choose to examine [illegible] *of the same frequency propagating in opposite* [illegible] A situation of practical concern arises when the incid[illegible] wave is reflected backward off some sort of mirro[illegible] rigid wall will do for sound waves or a conducting [illegible] for electromagnetic waves. Imagine that an inco[illegible] wave traveling to the left,

$$E_I = E_{0I} \sin (kx + \omega t + \varepsilon_I) \quad [illegible]$$

strikes a mirror at $x = 0$ and is reflected [illegible] the form

$$E_R = E_{0R} \sin (kx - \omega t + \varepsilon_R). \quad [illegible]$$

The composite wave in the region to the righ[illegible] mirror is $E = E_I + E_R$. We could perform the [illegible]

[illegible] and arrive at a general solution* much like [illegible] Section 7.1. There are, however, some valnable [illegible] insights to be gained by taking a slightly more [illegible] approach.

[illegible] initial phase ε_I may be set to zero by merely [illegible] clock at a time when $E_I = E_{0I} \sin kx$. Certain [illegible] determined by the physical setup must be [illegible] mathematical solution, and these are known [illegible] *boundary conditions.* For example, if we were [illegible] a rope with one end tied to a wall at $x = 0$, [illegible] must always have a zero displacement. The [illegible] waves, one incident and the other [illegible] would have to add in such a way as to yield [illegible] wave at $x = 0$. Similarly at the boundary [illegible] conducting sheet the resultant electromag- [illegible] must have a zero electric-field component [illegible] the surface. Assuming $E_{0I} = E_{0R}$, the boun- [illegible] conditions require that at $x = 0$, $E = 0$, and since [illegible] follows from Eqs. (7.28) and (7.29) that $\varepsilon_R = 0$. The composite disturbance is then

$$E = E_{0I}[\sin (kx + \omega t) + \sin (kx - \omega t)].$$

Applying the identity

$$\sin \alpha + \sin \beta = 2 \sin \tfrac{1}{2}(\alpha + \beta) \cos \tfrac{1}{2}(\alpha - \beta),$$

we obtain

$$E(x, t) = 2E_{0I} \sin kx \cos \omega t. \tag{7.30}$$

This is the equation for a **standing** or **stationary wave**, [illegible] to a traveling wave. Its profile does not move [illegible] space; it is clearly not of the form $f(x \pm vt)$. At any point $x = x'$, the amplitude is a constant equal to $2E_{0I}$ [illegible], and $E(x', t)$ varies harmonically as $\cos \omega t$. At certain points, namely, $x = 0, \lambda/2, \lambda, 3\lambda/2, \ldots,$ the [illegible] will be zero at all times. These are known as **nodes** or *nodal points* (Fig. 7.7). Halfway between each adjacent node, that is, at $x = \lambda/4$, $3\lambda/4$, [illegible] the amplitude has a maximum value of $\pm 2E_{0I}$. [illegible] points are known as the **antinodes.** The disturb[illegible] $E(x, t)$ will be zero at all values of x whenever $\cos$ [illegible] $= 0$, [illegible] is, when $t = (2m + 1)\tau/4$, where $m = 0$, [illegible] and τ is the period of the component waves.

If the re[illegible] off the mirror is not perfect, as is

* [illegible] J. M. Pearson, *A Theory of Waves.*

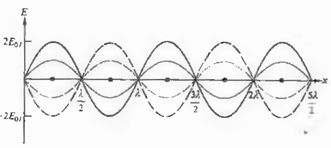


Figure 7.7 A standing wave at various times.

often the case, the composite wave will contain a traveling component along with the stationary wave. Under such conditions there will be a net transfer of energy, whereas for the pure standing wave there is none.

It was by measuring the distances between the nodes of standing waves that Hertz was able to determine the wavelength of the radiation in his historic experiments (see Section 3.6). A few years later, in 1890, Otto Wiener first demonstrated the existence of standing lightwaves. The arrangement he used is depicted in Fig. 7.8. It shows a normally incident parallel beam of quasi-monochromatic light reflecting off a front-silvered mirror. A transparent photographic film, less than $\lambda/20$ thick, deposited on a glass plate, was inclined to the mirror at an angle of about 10^{-3} radians. In that way the film plate cut across the pattern of standing plane waves. After developing the emulsion it was found to

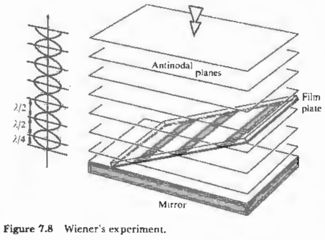


Figure 7.8 Wiener's experiment.

be blackened along a series of equidistant parallel bands. These corresponded to the regions where the photographic layer had intersected the antinodal planes. Significantly, there was no blackening of the emulsion at the mirror's surface. It can be shown that the nodes and antinodes of the magnetic field component of an electromagnetic standing wave alternate with those of the electric field (Problem 7.10). We might suspect as much from the fact that at $t = (2m + 1)\tau/4$, $E = 0$ for all values of x, so to conserve energy it follows that $B \neq 0$. In agreement with theory, Hertz had previously (1888) determined the existence of a nodal point of the electric field at the surface of his reflector. Accordingly, Wiener could conclude that the blackened regions were associated with antinodes of the **E**-field. *Thus it is the electric field that triggers the photochemical process.* In a similar way Drude and Nernst showed that the **E**-field is responsible for fluorescence. These observations are all quite understandable, since the force exerted on an electron by the **B**-field component of an electromagnetic wave is generally negligible in comparison to that of the **E**-field. It is for these reasons that the electric field is referred to as the *optic disturbance* or *light field.*

THE ADDITION OF WAVES OF DIFFERENT FREQUENCY

Thus far the analysis has been restricted to the superposition of waves, all having the same frequency. Yet one never actually has disturbances, of any kind, that are strictly monochromatic. It will be far more realistic, as we shall see, to speak of quasimonochromatic light, which is composed of a narrow range of frequencies. The study of such light will lead us to the important concepts of bandwidth and coherence time.

The ability to modulate light effectively (Section 8.11.3) makes it possible to couple electronic and optical systems in a way that has had and will certainly continue to have far-reaching effects on the entire technology. Moreover, with the advent of electro-optical techniques, light already has a new and significant role as a carrier of information. This section is devoted to developing some of the mathematical ideas needed to appreciate this new emphasis.

7.5 BEATS

Consider the composite disturbance arising [illegible] bination of the waves

$$E_1 = E_{01} \cos (k_1 x - \omega_1 t)$$

and

$$E_2 = E_{01} \cos (k_2 x - \omega_2 t),$$

which have equal amplitudes and zero initial [illegible] angles. The net wave

$$E = E_{01}[\cos (k_1 x - \omega_1 t) + \cos (k_2 x - \omega_2 t)]$$

can be reformulated as

$$E = 2E_{01} \cos \tfrac{1}{2}[(k_1 + k_2)x - (\omega_1 + \omega_2)t] \times \cos \tfrac{1}{2}[(k_1 - k_2)x - (\omega_1 - \omega_2)t],$$

using the identity

$$\cos \alpha + \cos \beta = 2 \cos \tfrac{1}{2}(\alpha + \beta) \cos \tfrac{1}{2}(\alpha - \beta).$$

We now define the quantities $\bar{\omega}$ and $\bar{k}$, which [illegible] the *average angular frequency* and *average propagation* [illegible] respectively. Similarly the quantities ω_m and [illegible] designated the *modulation frequency* and [illegible] *propagation number*, respectively. Let

$$\bar{\omega} = \tfrac{1}{2}(\omega_1 + \omega_2) \qquad \omega_m = \tfrac{1}{2}(\omega_1 - \omega_2)$$

and

$$\bar{k} = \tfrac{1}{2}(k_1 + k_2) \qquad k_m = \tfrac{1}{2}(k_1 - k_2);$$

thus

$$E = 2E_{01} \cos (k_m x - \omega_m t) \cos (\bar{k}x - \bar{\omega}t).$$

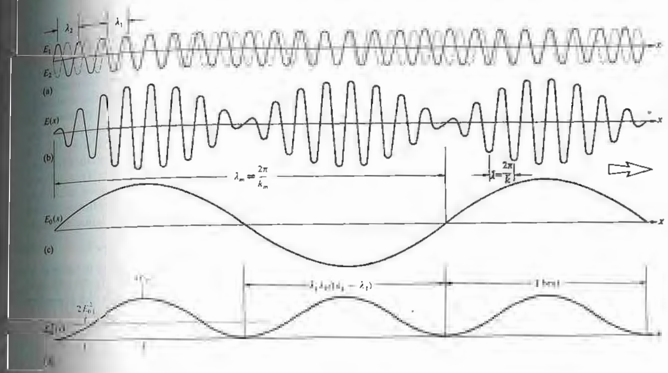
The total disturbance may be regarded as a travel[illegible] wave of frequency $\bar{\omega}$ having a time-varying or modulated amplitude $E_0(x, t)$ such that

$$E(x, t) = E_0(x, t) \cos (\bar{k}x - \bar{\omega}t),$$

where

$$E_0(x, t) = 2E_{01} \cos (k_m x - \omega_m t).$$

In applications of interest here, ω_1 and ω_2 will always be rather large. In addition, if they are comparable to each other, $\omega_1 \approx \omega_2$, then $\bar{\omega} \gg \omega_m$ and $E_0(x, t)$ will



[illegible] The superposition of two harmonic waves of different frequency.

change slowly, whereas $E(x, t)$ will vary quite rapidly (Fig. 7.9). The irradiance is proportional to

$$E_0^2(x, t) = 4E_{01}^2 \cos^2 (k_m x - \omega_m t)$$

or

$$E_0^2(x, t) = 2E_{01}^2[1 + \cos (2k_m x - 2\omega_m t)].$$

Notice that $E_0^2(x, t)$ oscillates about a value of $2E_{01}^2$ with [illegible] frequency of $2\omega_m$ or simply $(\omega_1 - \omega_2)$, which [illegible] as the **beat frequency**. In other words, E_0 [illegible] at the modulation frequency, whereas E_0^2 varies twice that, namely, the beat frequency.

Beats were first observed with the use of light in 1955 [illegible] Gudmundsen, and Johnson.* To obtain [illegible] slightly different frequency they used the Zeeman effect. When the atoms of a discharge lamp, in this case mercury, are subjected to a magnetic field, their energy levels split. As a result the emitted light contains two frequency components, ν_1 and ν_2, which differ in proportion to the magnitude of the applied field. When these components are recombined at the surface of a photoelectric mixing tube, the beat frequency, $\nu_1 - \nu_2$, is generated. Specifically, the field was adjusted so that $\nu_1 - \nu_2 = 10^{10}$ Hz, which conveniently corresponds to a 3-cm microwave signal. The recorded photoelectric current had the same form as the $E_0^2(x)$ curve in Fig. 7.9(d).

The advent of the laser has since made the observation of beats using light considerably easier. Even a beat frequency of a few Hz out of 10^{14} Hz can be seen as a variation in phototube current. The observation of beats now represents a particularly sensitive and fairly simple means of detecting small frequency differences. For

* [illegible]ster, R. A. Gudmundsen, and P. O. Johnson, "Photo[illegible] of Incoherent Light," *Phys. Rev.* **99**, 1691 (1955).

example, a modern version of the famous Michelson–Morley experiment that beats two infrared laserbeams will be considered in Section 9.8.3. The ring laser (Section 9.8.5), functioning as a gyroscope, utilizes beats to measure frequency differences induced as a result of the rotation of the system. The Doppler effect, which accounts for the frequency shift when light is reflected off a moving surface, provides another series of applications of beats. By scattering light off a target, whether solid, liquid, or even gaseous, and then beating the original and reflected waves, we get a precise measure of the target speed. In much the same way on an atomic scale, laser light will shift in phase upon interacting with sound waves moving in a material (this phenomenon is called Brillouin scattering). Thus $2\omega_m$ becomes a measure of the speed of sound in the medium.

7.6 GROUP VELOCITY

The disturbance examined in the previous section,

$$E(x, t) = E_0(x, t) \cos (\bar{k}x - \bar{\omega}t), \qquad (7.34)$$

consists of a high-frequency ($\bar{\omega}$) *carrier wave, amplitude-modulated* by a cosine function. Suppose, for a moment, that the wave in Fig. 7.9(b) were not modulated, that is, E_0 = constant. Each small peak in the carrier would travel to the right with the usual phase velocity. In other words,

$$v = -\frac{(\partial\varphi/\partial t)_x}{(\partial\varphi/\partial x)_t}. \qquad [2.32]$$

From Eq. (7.34) the phase is given by $\varphi = (\bar{k}x - \bar{\omega}t)$, hence

$$v = \bar{\omega}/\bar{k}. \qquad (7.36)$$

Clearly, this is the phase velocity whether the carrier is modulated or not. In the former case the peaks simply change amplitude periodically as they stream along.

Evidently, there is another motion to be concerned with, and that is the propagation of the modulation envelope. Return to Fig. 7.9(a) and suppose that the constituent waves, $E_1(x, t)$ and $E_2(x, t)$, advance with the same speed, $v_1 = v_2$. Imagine, if you will, the two harmonic functions having different wavelengths and frequencies drawn on separate sheets of clear [illegible] When these are overlayed in some way [as in Fig. [illegible] the resultant is a stationary beat pattern. If the[illegible] are both moved to the right at the same speed [illegible] resemble traveling waves, the beats will obvious[illegible] with that same speed. The rate at which the mo[illegible] envelope advances is known as the **group velo[illegible]** v_g. In this instance the group velocity equals the [illegible] velocity of the carrier (the average speed, $\bar{\omega}/\bar{k}$). In [illegible] words, $v_g = v = v_1 = v_2$. This applies specifically [illegible] *dispersive media* in which the phase velocity is inde[illegible] dent of wavelength so that the two waves could [illegible] the same speed. For a more generally applicable sol[illegible] examine the expression for the modulation enve[illegible]

$$E_0(x, t) = 2E_{01} \cos (k_m x - \omega_m t). \qquad [illegible]$$

The speed with which that wave moves is again given by Eq. (2.32), but now we can forget the car[illegible] The modulation therefore advances at a rate de[illegible] on the phase of the envelope $(k_m x - \omega_m t)$, and

$$v_g = \frac{\omega_m}{k_m}$$

or

$$v_g = \frac{\omega_1 - \omega_2}{k_1 - k_2} = \frac{\Delta\omega}{\Delta k}.$$

Realize, however, that ω may be dependent on λ or equivalently on k. The particular function $\omega = \omega(k)$ [illegible] called a *dispersion relation.* When the frequen[illegible] $\Delta\omega$, centered about $\bar{\omega}$, is small, $\Delta\omega/\Delta k$ is appro[illegible] equal to the derivative of the dispersion relatio[illegible]

$$v_g = \frac{d\omega}{dk}. \qquad (7.37)$$

The modulation or signal propagates at a speed v_g th[illegible] be greater than, equal to, or less than v, the phase vel[illegible] the carrier. Equation (7.37) is quite general and [illegible] true, as well, for any group of overlapping waves as long as their frequency range is narrow.

Since $\omega = kv$, Eq. (7.37) yields

$$v_g = v + k\frac{dv}{dk}. \qquad (7.38)$$

As a consequence, in nondispersive media in which [illegible]

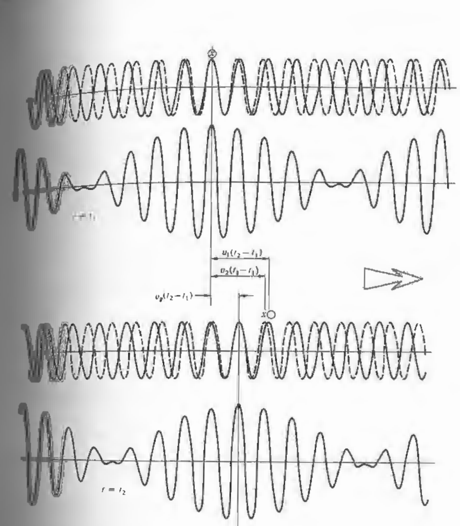


Figure 7.10 Group and phase velocities.

[illegible] independent of λ, $dv/dk = 0$ and $v_g = v$. Specifically, in vacuum $\omega = kc$, $v = c$, and $v_g = c$. In dispersive media ($v_1 \neq v_2$, as in Fig. 7.10) in which $n(k)$ is known, $\omega = kc/n$, and it is useful to reformulate v_g as

$$v_g = \frac{c}{n} - \frac{kc}{n^2}\frac{dn}{dk},$$

or

$$v_g = v\left(1 - \frac{k}{n}\frac{dn}{dk}\right). \qquad (7.39)$$

For optical media, in regions of normal dispersion, the refractive index increases with frequency ($dn/dk > 0$), and as a result $v_g < v$. Clearly, one should also define a *group index of refraction*

$$n_g = c/v_g, \qquad (7.40)$$

which must be carefully distinguished from n. In 1885 A. A. Michelson measured n_g in carbon disulfide using pulses of white light and obtained 1.758 in comparison to $n = 1.635$.

The special theory of relativity makes it quite clear that there are no circumstances under which a signal can propagate at a speed greater than c. Yet we have already seen that under certain circumstances (Section 3.5.1) the phase velocity can exceed c. The contradiction is only an apparent one, arising from the fact that although a monochromatic wave can indeed have a speed in excess of c, it cannot convey information. In contrast, a signal in the form of any modulated wave will propagate at the group velocity, which is always less than c in normally dispersive media.*

7.7 ANHARMONIC PERIODIC WAVES — FOURIER ANALYSIS

Figure 7.11 depicts a disturbance that arises from the superposition of two harmonic functions having different amplitudes and wavelengths. Notice that something rather curious has taken place—the composite disturbance is **anharmonic**; in other words, it is not sinusoidal. As we have already said, and will certainly say again, *purely sinusoidal* waves have no actual physical existence. This fact emphasizes the practical significance of anharmonic disturbances and is the motivation for our present concern with them. Figure 7.11 suggests that by using a number of sinusoidal functions whose amplitudes, wavelengths, and relative phases have been judiciously selected, it would be possible to synthesize some rather interesting wave profiles. An exceptionally beautiful mathematical technique for doing precisely this was devised by the French physicist Jean Baptiste Joseph, Baron de Fourier (1768–1830). This theory is predicated on what has come to be known as *Fourier's theorem*, which states that *a function f(x), having a spatial period λ, can be synthesized by a sum of harmonic functions whose wavelengths are integral submultiples of λ (that is, λ, λ/2, λ/3, etc.)*. This Fourier-series representation has the mathematical form

$$f(x) = C_0 + C_1 \cos\left(\frac{2\pi}{\lambda}x + \varepsilon_1\right) + C_2 \cos\left(\frac{2\pi}{\lambda/2}x + \varepsilon_2\right) + \cdots, \qquad (7.41)$$

* In regions of anomalous dispersion (Section 3.5.1) where $dn/dk < 0$, v_g may be greater than c. Here, however, the signal propagates at yet a different speed, known as the *signal velocity*, v_s. Thus $v_s = v_g$ except in a resonance absorption band. In all cases v_s corresponds to the velocity of energy transfer and never exceeds c.

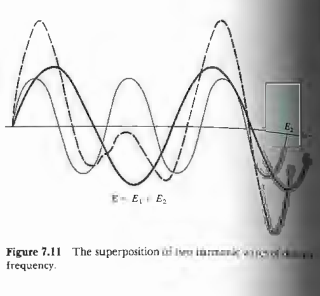


Figure 7.11 The superposition [illegible] frequency.

where the C-values are constants, and of course the profile $f(x)$ may correspond to a traveling wave [illegible] To get some sense of how this scheme works, [illegible] that although C_0 by itself is obviously a poor [illegible] for the original function, it will be [illegible] few points where it crosses the $f(x)$ curve. [illegible] way, adding on the next term improves things a bit, since the function

$$[C_0 + C_1 \cos(2\pi x/\lambda + \varepsilon_1)]$$

will be chosen so as to cross the $f(x)$ curve [illegible] frequently. If the synthesized function [the ri[illegible] side of Eq. (7.41)] comprises an infinite n[illegible] terms, selected to intersect the anharmonic fu[illegible] an infinite number of points, the series will pres[illegible] be identical to $f(x)$.

It is usually more convenient to reformulate [illegible] by making use of the trigonometric identity

$$C_m \cos(mkx + \varepsilon_m) = A_m \cos mkx + B_m \sin mkx$$

where $k = 2\pi/\lambda$, λ being the wavelength of $f(x)$, $A_m =$ $C_m \cos \varepsilon_m$, and $B_m = -C_m \sin \varepsilon_m$. Thus

$$f(x) = \frac{A_0}{2} + \sum_{m=1}^{\infty} A_m \cos mkx + \sum_{m=1}^{\infty} B_m \sin mkx \qquad (7.42)$$

The first term is written as $A_0/2$ because of the mathe-

matical simplification it will lead to later on. The process of determining the coefficients A_0, A_m, and B_m for a specific periodic function $f(x)$ is referred to as **Fourier analysis**. We'll spend a moment now deriving a set of equations for these coefficients that can be used henceforth. To that end, integrate both sides of Eq. (7.42) over any spatial interval equal to λ, for example, from 0 to λ or from $-\lambda/2$ to $+\lambda/2$ or, more generally, from x' to $x' + \lambda$. Since over any such interval

$$\int_0^\lambda \sin mkx\, dx = \int_0^\lambda \cos mkx\, dx = 0,$$

there is only one nonzero term to be evaluated, namely,

$$\int_0^\lambda f(x)\, dx = \int_0^\lambda \frac{A_0}{2}\, dx = A_0 \frac{\lambda}{2},$$

and thus

$$A_0 = \frac{2}{\lambda} \int_0^\lambda f(x)\, dx. \qquad (7.43)$$

To find A_m and B_m we will make use of the orthogonality of sinusoidal functions (Problem 7.24), that is, the fact that

$$\int_0^\lambda \sin akx \cos bkx\, dx = 0 \qquad (7.44)$$

$$\int_0^\lambda \cos akx \cos bkx\, dx = \frac{\lambda}{2} \delta_{ab} \qquad (7.45)$$

$$\int_0^\lambda \sin akx \sin bkx\, dx = \frac{\lambda}{2} \delta_{ab}, \qquad (7.46)$$

where a and b are nonzero positive integers and δ_{ab}, known as the *Kronecker delta*, is a shorthand notation equal to zero when $a \neq b$ and equal to 1 when $a = b$. To find A_m we now multiply both sides of Eq. (7.42) by $\cos \ell kx$, ℓ being a positive integer, and then integrate over a spatial period. Only one term is nonvanishing, and that is the single contribution in the second sum, which corresponds to $\ell = m$, in which case

$$\int_0^\lambda f(x) \cos mkx\, dx = \int_0^\lambda A_m \cos^2 mkx\, dx = \frac{\lambda}{2} A_m.$$

Thus

$$A_m = \frac{2}{\lambda} \int_0^\lambda f(x) \cos mkx\, dx. \qquad (7.47)$$

This expression can be used to evaluate A_m *for all values of m, including m = 0*, as is evident from a comparison of Eqs. (7.43) and (7.47). Similarly, multiplying Eq. (7.42) by $\sin \ell kx$ and integrating, leads to

$$B_m = \frac{2}{\lambda} \int_0^\lambda f(x) \sin mkx\, dx. \qquad (7.48)$$

In summary, a periodic function $f(x)$ can be represented as a Fourier series

$$f(x) = \frac{A_0}{2} + \sum_{m=1}^{\infty} A_m \cos mkx + \sum_{m=1}^{\infty} B_m \sin mkx, \qquad [7.42]$$

where, knowing $f(x)$, the coefficients are computed using

$$A_m = \frac{2}{\lambda} \int_0^\lambda f(x) \cos mkx\, dx \qquad [7.47]$$

and

$$B_m = \frac{2}{\lambda} \int_0^\lambda f(x) \sin mkx\, dx. \qquad [7.48]$$

Be aware that there are some mathematical subtleties related to the convergence of the series and the number of singularities in $f(x)$, but we need not be concerned with these matters here.

There are certain symmetry conditions that are well worth recognizing, because they lead to some computational short cuts. Thus if a function $f(x)$ is *even*, that is, if $f(-x) = f(x)$, or equivalently, if it is symmetric about $x = 0$, its Fourier series will contain only cosine terms ($B_m = 0$ for all m) that are themselves even functions. Likewise *odd* functions that are antisymmetric about $x = 0$, that is, $f(-x) = -f(x)$, will have series expansions containing only sine functions ($A_m = 0$ for all m). In either case, one need not bother to calculate both sets of coefficients. This is particularly helpful when the location of the origin ($x = 0$) is arbitrary, and we can choose it so as to make life as simple as possible. Nonetheless, keep in mind that many common functions are neither odd nor even (e.g., e^x).

As an example of the technique, let's compute the Fourier series that corresponds to a square wave. We select the location of the origin as shown in Fig. 7.12,

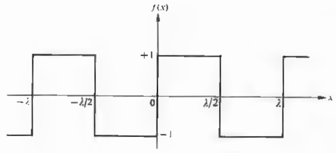


Figure 7.12 A periodic square wave.

and so

$$f(x) = \begin{cases} +1 & \text{when } 0 < x < \lambda/2 \\ -1 & \text{when } \lambda/2 < x < \lambda. \end{cases}$$

Since $f(x)$ is odd, $A_m = 0$, and

$$B_m = \frac{2}{\lambda}\int_0^{\lambda/2} (+1)\sin mkx\,dx + \frac{2}{\lambda}\int_{\lambda/2}^{\lambda} (-1)\sin mkx\,dx,$$

thus

$$B_m = \frac{1}{m\pi}[-\cos mkx]_0^{\lambda/2} + \frac{1}{m\pi}[\cos mkx]_{\lambda/2}^{\lambda}.$$

Remembering that $k = 2\pi/\lambda$, we obtain

$$B_m = \frac{2}{m\pi}(1 - \cos m\pi).$$

The Fourier coefficients are therefore

$$B_1 = \frac{4}{\pi}, \qquad B_2 = 0, \qquad B_3 = \frac{4}{3\pi},$$

$$B_4 = 0, \qquad B_5 = \frac{4}{5\pi}, \ldots,$$

and the required series is simply

$$f(x) = \frac{4}{\pi}\left(\sin kx + \tfrac{1}{3}\sin 3kx + \tfrac{1}{5}\sin 5kx + \cdots\right). \tag{7.49}$$

Figure 7.13 is a plot of a few partial sums of the series as the number of terms increases. We could pass over to the time domain to find $f(t)$ by just changing kx to ωt. Suppose that we have three ordinary electronic oscil-

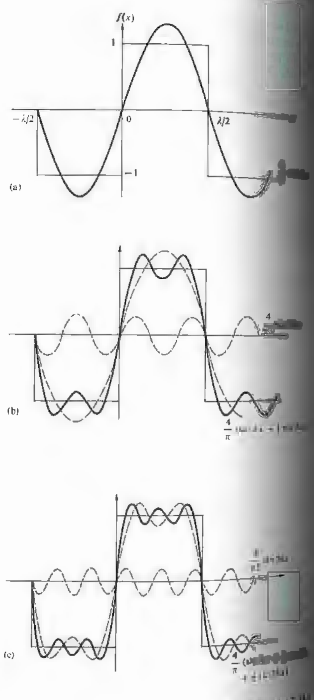


Figure 7.13 Synthesis of a periodic square wave. [illegible]

[illegible]re 7.13(d)

[illegible] output voltages vary sinusoidally and are [illegible] in both frequency and amplitude. If these [illegible] in series with their frequencies set at [illegible] 3ω, an[illegible] 5ω and the total signal is examined on an [illegible]illoscop[illegible] we can synthesize any of these curves, as [illegible]3(d). Similarly, we might simultaneously strike [illegible] on an appropriately tuned piano with just [illegible]orce on each to create a chord, or composite [illegible] having the curve in Fig. 7.13(c) as its profile. [illegible]enough, the human ear–brain audio system [illegible] of Fourier analysis of a simple composite wave [illegible]onic constituents—presumably there are [illegible] who could even name each note in the chord. [illegible] we postponed any detailed consideration of [illegible]armonic periodic functions, such as those in Fig. [illegible], and restricted our analysis to purely sinusoidal [illegible] now have a cogent rationale for having done [illegible] on we can envision this kind of distur[illegible] superposition of harmonic constituents of [illegible]rent frequencies whose individual behavior can be [illegible]ied separately. Accordingly, we can write

$$f(x \pm vt) = \frac{A_0}{2} + \sum_{m=1}^{\infty} A_m \cos mk(x \pm vt) + \sum_{m=1}^{\infty} B_m \sin mk(x \pm vt) \tag{7.50}$$

or equivalently

$$f(x \pm vt) = \sum_{m=0}^{\infty} C_m \cos[mk(x \pm vt) + \varepsilon_m] \tag{7.51}$$

for any such *anharmonic periodic wave.*

As a last example let's now analyze the square wave of Fig. 7.14 into its Fourier components. We notice that with the origin chosen as shown, the function is even, and all the B_m terms are zero. The appropriate Fourier coefficients (Problem 7.25) are then

$$A_0 = \frac{4}{a} \quad \text{and} \quad A_m = \frac{4}{a}\left(\frac{\sin m2\pi/a}{m2\pi/a}\right). \tag{7.52}$$

Unlike the previous function, this one has a nonzero value of A_0. You might have already noticed that $A_0/2$ is actually the *mean value* of $f(x)$, and since the curve lies completely above the axis, it will clearly not be zero.

The expression $(\sin u)/u$ arises so frequently in optics that it is given the special name **sinc** $\boldsymbol{u}$, and its values are listed in Table 1 (p. 624). Since the limit of sinc u as u goes to zero is 1, A_m can represent all the coefficients, if we let $m = 0, 1, 2, \ldots$.

The form we are using is rather general, inasmuch as the width of the square peak, $2(\lambda/a)$, can be any fraction of the total wavelength, depending on a. The Fourier series is then

$$f(x) = \frac{2}{a} + \sum_{m=1}^{\infty} \frac{4}{a}\,\text{sinc}\, m2\pi/a \cos mkx. \tag{7.53}$$

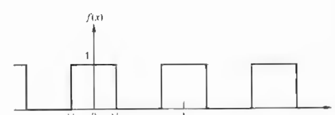


Figure 7.14 A periodic anharmonic function.

If we were synthesizing the corresponding function of time, $f(t)$, having a square peak of width $2(\tau/a)$, the same expression (7.53) would apply where kx was simply replaced by ωt. Here ω is the *angular temporal frequency* of the periodic function $f(t)$ and is known as the **fundamental**. It is the lowest frequency of the cosine term and arises when $m = 1$. Frequencies of $2\omega, 3\omega, 4\omega, \ldots$, are known as *harmonics* of the fundamental and are associated, of course, with $m = 2, 3, 4, \ldots$. In much the same way, since λ is the *spatial period*, $\kappa = 1/\lambda$ is the **spatial frequency**, and $k = 2\pi\kappa$ might be called the **angular spatial frequency**. Once again one speaks of the harmonics, of frequency $2k, 3k, 4k, \ldots$, where these are spatial alternations. Evidently, the dimensions of κ are cycles per unit length (e.g., cycles per mm or possibly just cm^{-1}), and those of k are radians per unit length.

Before we press on it's important to clarify a few points so as to avoid a common confusion concerning the use of the terms spatial frequency and spatial period (or wavelength). Figure 7.14 shows a one-dimensional periodic square-wave function spread out in space along the x-axis. This might be a pattern seen on the face of an oscilloscope or the profile of a rather extraordinary disturbance moving along a taut rope. In either case, it repeats itself in space over a distance known as the wavelength and one over that is the spatial frequency. Now suppose instead that the pattern corresponds to an irradiance distribution, a series of bright and dark stripes, for instance, the kind of thing you might see looking through a narrow horizontal slit against a picket fence or, even better, while scanning on a line across a group of alternately clear and opaque bands (Fig. 14.2) illuminated by monochromatic light. Again the pattern will have some spatial period and frequency determined by the rate at which it repeats in space, but this time the light itself will also have a spatial frequency (k) and period (λ), as well as a temporal frequency and period, quite apart from the other. The pattern might have a wavelength (λ) of 20 cm, and the light generating it a wavelength (λ) of 500 nm. Herein lies the area of potential confusion. Henceforth, we will reserve the symbols k and λ for the lightwave itself and use k and λ to describe spatial optical patterns.

Now return to the square function of Fig. 7.14 and suppose that we set $a = 4$, or in other words, we cause the square peak to have a width of $\lambda/2$. In that instance

$$f(x) = \frac{1}{2} + \frac{2}{\pi}\left(\cos kx - \tfrac{1}{3}\cos 3kx + \tfrac{1}{5}\cos 5kx - \cdots\right).$$

As a matter of fact, if the graph of the function [illegible] such that a horizontal line could divide it into [illegible] shaped segments, above and below that line, the [illegible] series will consist of only odd harmonics. Were [illegible] plot the curve representing the partial sum of [illegible] through $m = 9$, it would closely resemble the [illegible] wave. In contrast, if the width of the peak is [illegible] the number of terms in the series needed to produce the same general resemblance to $f(x)$ will be increased. This can be appreciated by examining the ratio

$$\frac{A_m}{A_1} = \frac{\sin m2\pi/a}{m \sin 2\pi/a}. \qquad (7.55)$$

Observe that for $a = 4$, the ninth term [illegible] is fairly small, $A_9 \approx 10\% \, A_1$. In comparison, [illegible] 100 times narrower (that is, $a = 400$), A_9 [illegible] Similarly, whereas it takes terms through $m =$ [illegible] cate the curve of Fig. 7.13(b) when $a = 4$, it will take up to $m = 8$ to produce roughly the equivalent profile when $a = 8$. Making the peak narrower has the [illegible] of introducing higher-order harmonics, which in turn have smaller wavelengths. We might guess, then, [illegible] it is not the total number of terms in the series [illegible] of prime importance but rather the relative [illegible] of the smallest features being reproduced and [illegible] sponding wavelengths available.* If there [illegible] details in the profile, the series must contain [illegible] tively short-wavelength (or in the time domain, [illegible] period) contributions.

The negative values of A_m in Eq. (7.53) and [illegible] (7.15) should simply be thought of as the amp[illegible] those harmonic contributions that are to be ad[illegible] the synthesis with their phases shifted by 180° [illegible] pared with the positive terms. The equivalence [illegible] a negative amplitude and a π-rad phase shift [illegible] from the fact that $A_m \cos(kx + \pi) = -A_m \cos kx$ [illegible]

* Evidently one is not going to be able to build a castle [illegible] the blocks are a good deal smaller than the castle.

7.8 NONPERIODIC WAVES — FOURIER INTEGRALS

[illegible] Fig. 7.14 and imagine that we keep the width [illegible] are peak constant while λ is made to increase [illegible] limit. As λ approaches infinity, the resulting [illegible] will no longer appear periodic. We then have one single square pulse, the adjacent peaks having moved off to infinity. This suggests a possible way of [illegible] eralizing the method of Fourier series to include [illegible] periodic functions. As we shall see, these are of [illegible] interest in physics, particularly in optics and [illegible] mechanics.

[illegible] this can be accomplished, let's initially set $a = 4$ and choose some value of λ; anything will do, [illegible] cm. The peak then has a width of $\frac{1}{2}$ cm, that [illegible] centered at $x = 0$, as illustrated in Fig. 7.15(a). [illegible] portance of each particular frequency, mk, can [illegible] preciated by examining the value of the corre[illegible] ing Fourier coefficient, in this case A_m. The [illegible] may be thought of as weighting factors that [illegible] ly emphasize the various harmonics. Figure [illegible] tains a plot of a number of values of A_m (where [illegible] $= 0, 1, 2, \ldots$) versus mk for the foregoing [illegible] ve—such a curve is known as the *spatial* [illegible] *spectrum*. We can regard A_m as a function, [illegible] of mk, which may be nonzero only at values of [illegible] 1, 2, ... If the quantity a is now made equal to [illegible] λ is increased to 2 cm, the peak width will be [illegible] ly unaffected. The only alteration is a doubling [illegible] space between peaks. Yet a very interesting [illegible] ge in the spatial frequency spectrum is evident in [illegible] 7.15(b). Note that the density of components along [illegible] mk-axis has increased markedly. Nonetheless, [illegible] still zero when $mk = 4\pi, 8\pi, 12\pi, \ldots$, but since [illegible] is now π rather than 2π, there will be more terms [illegible] these zero points. Finally, let $a = 16$ and [illegible] 4 cm. Again the individual peaks are unal[illegible] pe, but the terms in the frequency spectrum [illegible] more densely packed. In effect, the pulse, [illegible] with λ, is getting smaller and smaller, [illegible] quiring higher frequencies to synthesize it. [illegible] the envelope of the curve, which was barely [illegible] in Fig. 7.15(a), is quite evident in Fig. 7.15(c). [illegible] envelope is identical in each case, except for a scale factor. It is determined only by the shape of the original signal and will be quite different for other configurations. We can conclude that as λ increases and

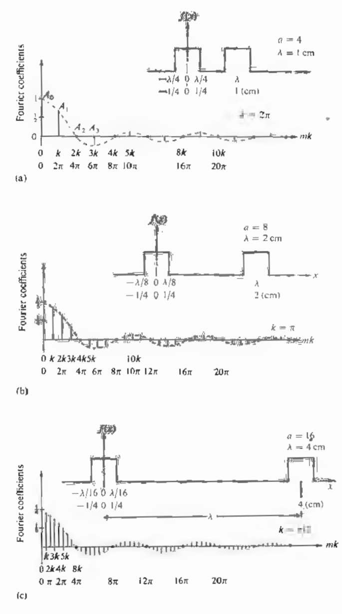


Figure 7.15 The square pulse as a limiting case. The negative coefficients correspond to a phase shift of π radians.

the function takes on the appearance of a single square pulse, the space between each of the $A(mk)$ contributions in the spectrum will decrease. The discrete spectral lines, while decreasing in amplitude, will gradually merge, becoming individually unresolvable. In other words, in the limit as λ approaches ∞, the spectral lines will become infinitely close to each other. As k becomes extremely small, m must consequently become exceedingly large, if mk is to be at all appreciable. Changing notation, we replace mk, the angular frequency of the harmonics, by k_m. Although it comprises discrete terms, in the limit k_m will be transformed into k (i.e., a continuous frequency distribution). The function $A(k_m)$ in the limit will become the envelope shown in Fig. 7.15. It is obviously no longer meaningful to talk about the fundamental frequency and its harmonics. The pulse being synthesized, $f(x)$, has no apparent fundamental frequency.

Recall that an integral is actually the limit of a sum as the number of elements goes to infinity and their size approaches zero. Thus it should not be surprising that the *Fourier series* must be replaced by the so-called **Fourier integral** as λ goes to infinity. That integral, which we state here without proof, is

$$f(x) = \frac{1}{\pi}\left[\int_0^\infty A(k)\cos kx\, dk + \int_0^\infty B(k)\sin kx\, dk\right] \tag{7.56}$$

provided that

$$A(k) = \int_{-\infty}^{\infty} f(x)\cos kx\, dx$$

and

$$B(k) = \int_{-\infty}^{\infty} f(x)\sin kx\, dx. \tag{7.57}$$

The similarity with the series representation should be obvious. The quantities $A(k)$ and $B(k)$ are interpreted as the amplitudes of the sine and cosine contributions in the range of angular spatial frequency between k and $k + dk$. They are generally spoken of as the **Fourier cosine** and **sine transforms**, respectively. In the foregoing example of a square pulse, it is the cosine transform, $A(k)$, that will be found to correspond to the envelope in Fig. 7.15.

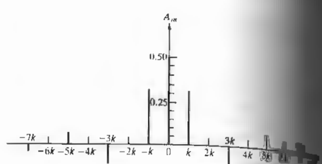


Figure 7.16 A symmetrical frequency spectrum for th[illegible] in Figure 7.15(a). Note that the zeroth term is actually [illegible] is indeed the amplitude of the $m = 0$ contribution to th[illegible]

A careful examination of Fig. 7.15 and Eq. [illegible] reveals that except for the zero-frequency [illegible] amplitudes of the contributions to the synthe[illegible] $(4/a)\,\text{sinc}\, m2\pi/a$: the envelope of the curve [illegible] function. Remember that the first term in [illegible] $\frac{1}{2}A_0$, not A_0, which suggests another way to repre[illegible] the frequency spectrum. Inasmuch as $\cos(mk$[illegible] $\cos(-mkx)$, we can divide the amplitude of e[illegible] bution beyond $m = 0$ in half and plot it twice [illegible] a positive value of k and again with a negative o[illegible] 7.16). This mathematical contrivance provides [illegible] symmetrical curve, but it's introduced here [illegible] is common practice to represent frequency s[illegible] in that fashion. As we will see in Chapter 11, [illegible] powerful Fourier transform methods involve a [illegible] representation that automatically gives rise to [illegible] metrical distribution of positive and negativ[illegible] frequency terms. Certain optical phenomena [illegible] diffraction) also occur symmetrically in space [illegible] marvelous relationship can be constructed w[illegible] the spatial frequency spectrum, provided that it [illegible] passes positive and negative frequencies. The [illegible] frequency is a useful mathematical device, and [illegible] redeeming grace. Still, all physical processes [illegible] expressed exclusively in terms of positive freq[illegible] and we shall continue to do just that throug[illegible] remainder of this chapter.

7.9 PULSES AND WAVE PACKETS

Let's now determine the Fourier-integral representation of the square pulse in Fig. 7.17, which is described by the function

$$f(x) = \begin{cases} E_0 & \text{when } |x| < L/2 \\ 0 & \text{when } |x| > L/2. \end{cases}$$

Since $f(x)$ is an even function, the sine transform, $B(k)$, will be found to be zero (7.57), and

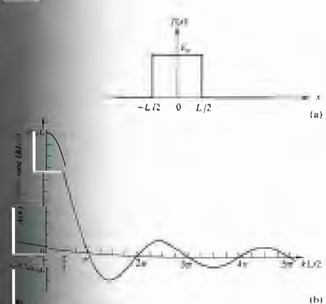
$$A(k) = \int_{-\infty}^{\infty} f(x)\cos kx\, dx = \int_{-L/2}^{+L/2} E_0 \cos kx\, dx.$$

Hence

$$A(k) = \frac{E_0}{k}\sin kx\Big|_{-L/2}^{+L/2} = \frac{2E_0}{k}\sin kL/2.$$

[illegible]ing numerator and denominator by L and re[illegible]ing terms, we have

$$A(k) = E_0 L\frac{\sin kL/2}{kL/2}$$



[illegible] 7.17 The square pulse and its transform.

or equivalently

$$A(k) = E_0 L\, \text{sinc}\,(kL/2). \tag{7.58}$$

The Fourier transform of the square pulse is plotted in Fig. 7.17(b) and should be compared with the envelope in Fig. 7.15. Realize that as L increases, the spacing between successive zeroes of $A(k)$ decreases and vice versa. Moreover, when $k = 0$, it follows from Eq. (7.58) that $A(0) = E_0 L$.

It is a simple matter to write out the integral representation of $f(x)$ using Eq. (7.56):

$$f(x) = \frac{1}{\pi}\int_0^\infty E_0 L\, \text{sinc}\,(kL/2)\cos kx\, dk. \tag{7.59}$$

An evaluation of this integral is left for Problem 7.26.

Earlier, when we talked about monochromatic waves, we pointed out that they were in fact fictitious, at least physically. There will always have been some point in time when the generator, however perfect, was turned on. Figure 7.18 depicts a somewhat idealized harmonic pulse corresponding to the function

$$E(x) = \begin{cases} E_0 \cos k_p x & \text{when } -L \le x \le L \\ 0 & \text{when } |x| > L. \end{cases}$$

We chose to work in the space domain but could certainly have envisioned the disturbance as a function of time. We are effectively examining the spatial profile of the wave $E(x - vt)$ at $t = 0$ rather than the temporal profile at $x = 0$. The spatial frequency k_p is that of the harmonic region of the pulse itself. Proceeding with the analysis, we note that $E(x)$ is an even function, consequently $B(k) = 0$ and

$$A(k) = \int_{-L}^{+L} E_0 \cos k_p x \cos kx\, dx.$$

This is identical to

$$A(k) = \int_{-L}^{+L} E_0 \tfrac{1}{2}[\cos(k_p + k)x + \cos(k_p - k)x]\, dx,$$

which integrates to

$$A(k) = E_0 L\left[\frac{\sin(k_p + k)L}{(k_p + k)L} + \frac{\sin(k_p - k)L}{(k_p - k)L}\right]$$

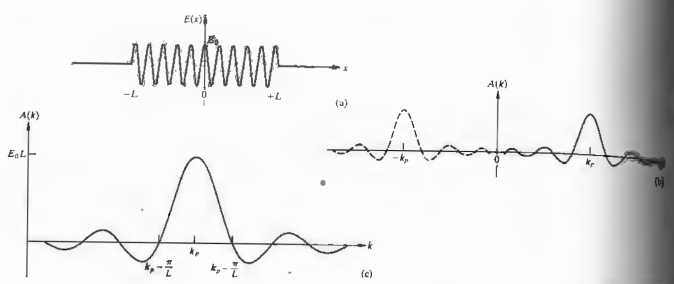


Figure 7.18 A finite cosine wavetrain and its transform.

or, if you like,

$$A(k) = E_0L[\text{sinc}\,(k_p + k)L + \text{sinc}\,(k_p - k)L]. \quad (7.60)$$

When there are many waves in the train ($\lambda_p \ll L$), $k_pL \gg 2\pi$. Thus $(k_p + k)L \gg 2\pi$, and therefore sinc $(k_p + k)L$ is down to fairly small values. In contrast, when $k_p = k$, the second sinc function in the brackets has a maximum value of 1. In other words, the function given by Eq. (7.60) can be thought of as having a peak at $k = -k_p$, as shown in part (b) of the drawing. Since only positive values of k are to be allowed, only the tail of that left-side peak that crosses into the positive k region will contribute. As we have just seen, such contributions will be negligible far from $k = -k_p$, especially when $L \gg \lambda_p$ and the peaks are both narrow and widely spaced. The positive tail of the left-side peak then falls off rapidly beyond $k = -k_p$. Consequently, we can neglect the first sinc in this particular case and write the transform as

$$A(k) = E_0L\,\text{sinc}\,(k_p - k)L \quad (7.61)$$

[Fig. 7.18(c)]. Even though the wavetrain is very long, since it is not infinitely long it must be synthesized from a continuous range of spatial frequencies. Thus it can be thought of as the composite of an infinite ensemble of harmonic waves. In that context one speaks of such pulses as *wave packets* or *wave groups*. As we might have expected, the dominant contribution is associated with $k = k_p$. Had the analysis been carried out in the time domain, the same results would have obtained [illegible] the transform was centered about the temporal frequency ω_p. Quite clearly, as the wavetrain [illegible] infinitely long (i.e., $L \to \infty$), its frequency spectrum shrinks, and the curve of Fig. 7.18(c) closes down to a single tall spike at k_p (or ω_p). This is obviously the limiting case of the idealized monochromatic [illegible]

Since we can think of $A(k)$ as the amplitude of the contributions to $E(x)$ in the range k to $k + dk$, [illegible] $A(k)$ must be related to the energy of the wave in [illegible] (Problem 7.27). We'll come back to this point in Chapter 11 when we consider the *power spectrum*. [illegible] moment, merely observe [Fig. 7.18(c)] that [illegible] energy is carried in the spatial frequency range $k_p - \pi/L$ to $k_p + \pi/L$, extending between the [illegible] on either side of the central peak. An increase in the length of the wavetrain causes the energy of the [illegible] to become concentrated in an ever narrowing [illegible] k about k_p.

The wave packet in the time domain, that is,

$$E(t) = \begin{cases} E_0 \cos \omega_p t & \text{when } -T \le t \le T \\ 0 & \text{when } |t| > T \end{cases}$$

has the transform

$$A(\omega) = E_0T\,\text{sinc}\,(\omega_p - \omega)T, \quad (7.62)$$

where ω and k are related by the phase velocity. The [illegible] except for the notational change from k to ω and L to T, is identical to that of Fig. 7.18(c). For the particular wave packet being studied [illegible] range of angular frequencies (ω or k) that the transform comprises is certainly not finite. Yet if we [illegible] to speak of the *width* of the transform ($\Delta\omega$ or Δk), Fig. 7.18(c) suggests that we use $\Delta k = 2\pi/L$ or $\Delta\omega = 2\pi/T$. In contrast, the spatial or temporal extent of the [illegible] unambiguous at $\Delta x = 2L$ or $\Delta t = 2T$, respectively. The product of the width of the packet in what [illegible] called *k-space* and its width in *x-space* is $\Delta k\, \Delta x = 4\pi$ or analogously $\Delta\omega\, \Delta t = 4\pi$. One speaks of the quantities Δk and $\Delta\omega$ as the **frequency bandwidths**. Had we [illegible] a differently shaped pulse, the product of the [illegible] width and the pulse length might certainly have [illegible] somewhat different. The ambiguity arises because [illegible] not yet chosen one of the alternative possibilities for specifying $\Delta\omega$ and Δk. For example, rather than using the first minima of $A(k)$ (there are transforms that have no such minima, such as the Gaussian function

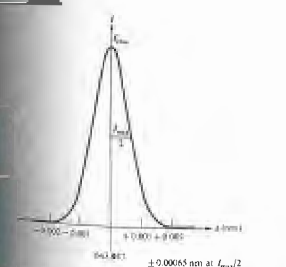


Figure 7.19 The cadmium red [illegible] spectral line from a low-pressure lamp.

of Section 11.2), we could have let Δk be the width of $A^2(k)$ at a point where the curve had dropped to $\frac{1}{2}$ or possibly $1/e$ of its maximum value. In any event, it will suffice for the time being to observe that

$$\Delta\nu \sim 1/\Delta t, \quad (7.63)$$

that is, the frequency bandwidth is the same order of magnitude as the reciprocal of the temporal extent of the pulse (Problem 7.28). If the wave packet has a narrow bandwidth, it will extend over a large region of space and time. Accordingly, a radio tuned to receive a bandwidth of $\Delta\nu$ will be capable of detecting pulses of duration no shorter than $\Delta t \sim 1/\Delta\nu$.

These considerations are of profound importance in quantum mechanics where wave packets describe particles, and Eq. (7.63) is akin to the Heisenberg uncertainty principle.

7.10 OPTICAL BANDWIDTHS

Suppose that we examine the light emitted by what is loosely termed a monochromatic source, for example, a sodium discharge lamp. When the beam is passed through some sort of spectrum analyzer we will be able to observe all its various frequency components. Typically we will find that there are a number of fairly narrow frequency ranges that contain most of the energy and that these are separated by much larger regions of darkness. Each such brightly colored band is known as a *spectral line*. There are devices in which the light enters by way of a slit, and each line is actually a colored image of that slit. Other analyzers represent the frequency distribution on the screen of an oscilloscope. In any event, the individual spectral lines are never infinitely sharp. They always consist of a band of frequencies, however small (Fig. 7.19).

The electron transitions responsible for the generation of light have a duration on the order of 10^{-8} s to 10^{-9} s. Because the emitted wavetrains are finite, there will be a spread in the frequencies present, known as the *natural linewidth* (see Section 11.3.4). Moreover, since the atoms are in random thermal motion, the frequency spectrum will be altered by the Doppler effect. In addition, the atoms suffer collisions that interrupt the wavetrains and again tend to broaden the frequency distribution. The total effect of all these mechanisms is that each spectral line has a bandwidth $\Delta\nu$ rather than one single frequency. The time that satisfies Eq. (7.63) is referred to as the **coherence time** (henceforth to be written Δt_c), and the length Δx_c given by

$$\Delta x_c = c\,\Delta t_c \qquad (7.64)$$

is the **coherence length**. As will become evident presently, the coherence length is the extent in space over which the wave is nicely sinusoidal so that its phase can be predicted reliably. The corresponding temporal duration is the coherence time. These concepts are extremely important in considering the interaction of waves, and we will come back to them later in the discussion of interference.

Though the concept of the photon wavetrain is already familiar, we are now in a position, armed with a little Fourier analysis, to deduce something about its configuration. This can be done by essentially working backward from the experimental observation that the frequency distribution of a spectral line from a quasimonochromatic (nonlaser) source can be represented by a bell-shaped Gaussian function (Section 2.1). That is, the irradiance versus frequency is found to be Gaussian. But irradiance is proportional to the electric field amplitude squared, and since the square of a Gaussian function is a Gaussian function, it follows that the net amplitude of the light field is also bell-shaped.

Now suppose a single photon wavetrain, one of N identical such packets making up the beam, resembles Fig. 7.20(a) in that it is a harmonic function modulated by a Gaussian envelope. Its Fourier transform, $A(\omega)$, is also Gaussian. Imagine that we look at only one and the same harmonic frequency component that goes into making up each photon wavetrain, for example, the one corresponding to ω'. Remember that this component is an infinitely long, constant-amplitude sinusoid. If every packet is indeed identical, the amplitude of the Fourier component associated with ω' will be the same in each. At any point in a stream of photons these ω'-component monochromatic waves, one from each wavetrain, will have a random relative phase distribution that rapidly changes in time with the arrival of

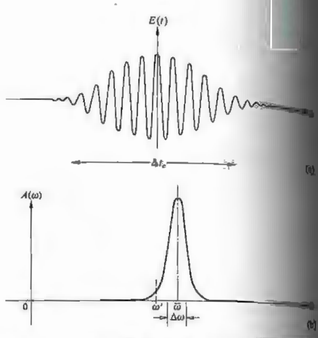


Figure 7.20 A cosinusoidal wavetrain modulated [illegible] Gaussi[illegible] envelope along with its transform, which is also Gau[illegible]

each photon. Thus all such contributi[illegible] together (7.21) will correspond on average [illegible] monic wave of frequency ω' having an ampli[illegible] portional to $N^{1/2}$, and this is the ω' part o[illegible] ne[illegible] observed field. The same will be true for ev[illegible] frequency constituting the packets. This me[illegible] that there is the same amount of energy presen[illegible] at [illegible] frequency in the net light field of the beam a[illegible] in the totality of the separate consituent wa[illegible] Moreover, we know all about this energy-freq[illegible] tribution; it's Gaussian, so the transform of th[illegible] wavetrain must be Gaussian too. In other wo[illegible] observed spectral line corresponds to the pow[illegible] trum of the beam, but it also corresponds to [illegible] spectrum of an individual photon packet. I[illegible] diance is Gaussian, the photon wavetrain [illegible] Gaus[illegible]

As a result of the randomness of the wavetrai[illegible] individual harmonic components of the resulta[illegible] will not have the same relative phases as they [illegible] each packet. Thus the profile of the resultant wi[illegible] from that of the separate wave packets, even [illegible]

the amplitude of each frequency component present in the resultant is simply $N^{1/2}$ times its amplitude in any one packet. The observed spectral line corresponds to the power spectrum of the resultant beam, to be sure, but it also corresponds to the power spectrum of an individual packet. Ordinarily there will be a tremendous number of arbitrarily overlapping wave groups, so that the envelope of the resultant will rarely, if ever, be zero. If the source is quasimonochromatic (i.e., if the bandwidth is small compared with the mean frequency $\bar{\nu}$), we can envision the resultant as being "almost" sinusoidal.

In summary, the composite lightwave can be pictured as in Fig. 7.21. We might imagine the frequency and amplitude to be randomly varying, the former over a range $\Delta\nu$ centered at $\bar{\nu}$. Accordingly, the **frequency** [illegible] defined as $\Delta\nu/\bar{\nu}$, is a useful measure of spectral [illegible] Even a coherence time as short as 10^{-9} s corre[illegible]o roughly a few million wavelengths of the oscillating carrier ($\bar{\nu}$), so that any amplitude or [illegible] variations will occur quite slowly in com[illegible] Equivalently we can introduce a time-varying [illegible]tor such that the disturbance can be written as

$$E(t) = E_0(t)\cos\left[\epsilon(t) - 2\pi\bar{\nu}t\right], \qquad (7.65)$$

where the separation between wave crests changes in time.

[illegible]ge duration of a wave packet is Δt_c, so two [illegible] the wave in Fig. 7.21 separated by more than [illegible] on different contributing wavetrains. These [illegible] thus be completely uncorrelated in phase. [illegible]ords, if we determined the electric field of [illegible]site wave as it passed by an idealized detector, [illegible] predict its phase fairly accurately for times less than Δt_c later, but not at all for times greater [illegible]. In Chapter 12 we will consider the *degree of coherence* that applies over the region between these extremes as well.

White light has a frequency range from 0.4×10^{15} Hz to about 0.7×10^{15} Hz, that is, a bandwidth of about 0.3×10^{15} Hz. The coherence time is then roughly 3×10^{-15} s, which corresponds (7.64) to wavetrains having a spatial extent only a few wavelengths long. Accordingly, *white light may be envisaged as a random succession of very short pulses.* Were we to synthesize white light, we would have to superimpose a broad, continuous range of harmonic constituents in order to produce the very short wave packets. Inversely, we can pass white light through a Fourier analyzer, such as a diffraction grating or a prism, and in so doing actually generate those components.

The available bandwidth in the visible spectrum ($\approx$300 THz) is so broad that it represents something of a wonderland for the communications engineer. For example, a typical television channel occupies a range of about 4 MHz in the electromagnetic spectrum ($\Delta\nu$ is determined by the duration of the pulses needed to control the scanning electron beam). Thus the visible region could carry roughly 75 million television channels. Needless to say, this is an area of active research (see Section 8.11).

Ordinary discharge lamps have relatively large bandwidths leading to coherence lengths only on the order of several millimeters. In contrast, the spectral lines emitted by low-pressure isotope lamps such as Hg^{198} ($\lambda_{air} = 546.078$ nm) or the international standard Kr^{86} ($\lambda_{air} = 605.616$ nm) have bandwidths of roughly 1000 MHz. The corresponding coherence lengths are of the order of 1 m, and coherence times are about 1 ns. The frequency stability is about one part per million—these sources are certainly quasimonochromatic.

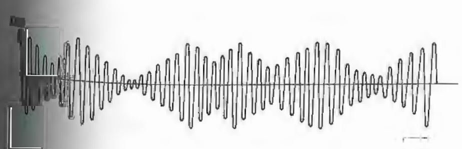


Figure 7.21 A quasimonochromatic lightwave.

The most spectacular of all present-day sources is the laser. Under optimum conditions, with temperature variations and vibrations meticulously suppressed, a laser was actually operated at quite close to its theoretical limit of frequency constancy. A short-term frequency stability of about 8 parts per 10^{14} was attained† with a He–Ne continuous gas laser at $\lambda_0 = 1153$ nm. That corresponds to a remarkably narrow bandwidth of about 20 Hz. More common and not very difficult to obtain are frequency stabilities of several parts per 10^9. There are commercially available CO_2 lasers that provide a short-term ($\sim 10^{-1}$ s) $\Delta\nu/\bar{\nu}$ ratio of 10^{-9} and a long-term ($\sim 10^3$ s) value of 10^{-8}.

PROBLEMS

7.1 Determine the resultant of the superposition of the parallel waves $E_1 = E_{01} \sin(\omega t + \epsilon_1)$ and $E_2 = E_{02} \sin(\omega t + \epsilon_2)$ when $\omega = 120\pi$, $E_{01} = 6$, $E_{02} = 8$, $\epsilon_1 = 0$, and $\epsilon_2 = \pi/2$. Plot each function and the resultant.

7.2* Considering Section 7.1, suppose we began the analysis to find $E = E_1 + E_2$ with two cosine functions $E_1 = E_{01}\cos(\omega t + \alpha_1)$ and $E_2 = E_{02}\cos(\omega t + \alpha_2)$. To make things a little less complicated, let $E_{01} = E_{02}$ and $\alpha_1 = 0$. Add the two waves algebraically and make use of the familiar trigonometric identity $\cos\theta + \cos\Phi = 2\cos\frac{1}{2}(\theta + \Phi)\cos\frac{1}{2}(\theta - \Phi)$ in order to show that $E = E_0\cos(\omega t + \alpha)$, where $E_0 = 2E_{01}\cos\alpha_2/2$ and $\alpha = \alpha_2/2$. Now show that these same results follow from Eqs. (7.9) and (7.10).

7.3* Show that when the two waves of Eq. (7.5) are in phase, the resulting amplitude squared is a maximum equal to $(E_{01} + E_{02})^2$, and when they are out of phase it is a minimum equal to $(E_{01} - E_{02})^2$.

7.4* Show that the *optical path*, defined as the sum of the products of the various indices times the thicknesses of media traversed by a beam, that is, $\Sigma_i n_i x_i$, is equivalent to the length of the path in vacuum that would take the same time for that beam to negotiate.

7.5 Answer the following:

a) How many wavelengths of $\lambda_0 = 500$ nm light will span a 1-m gap in vacuum?
b) How many waves span the gap when a glass [illegible] 5 cm thick ($n = 1.5$) is inserted in the path?
c) Determine the OPD between the two situations.
d) Verify that Λ/λ_0 corresponds to the difference between the solutions to (a) and (b) above.

7.6* Determine the optical path difference for the [illegible] waves A and B, both having vacuum wavelengths [illegible] 500 nm, depicted in Fig. 7.22; the glass ($n = 1.5$) [illegible] is filled with water ($n = 1.33$). If the waves start out in phase and all the above numbers are exact, find their relative phase difference at the finishing line.

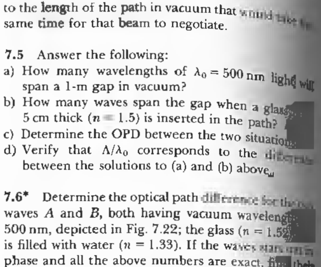


Figure 7.22

7.7* Using Eqs. (7.9), (7.10), and (7.11), show that the resultant of the two waves

$$E_1 = E_{01}\sin[\omega t - k(x + \Delta x)]$$

and

$$E_2 = E_{01}\sin(\omega t - kx)$$

is

$$E = 2E_{01}\cos\left(\frac{k\,\Delta x}{2}\right)\sin\left[\omega t - k\left(x + \frac{\Delta x}{2}\right)\right]. \qquad [7.17]$$

7.8 Add the two waves of Problem 7.7 directly to find Eq. (7.17).

† T. S. Jaseja, A. Javan, and C. H. Townes, "Frequency Stability of Helium–Neon Lasers and Measurements of Length." *Phys. Rev. Letters* **10**, 165 (1963).

7.9 Use the complex representation to find the resultant $E = E_1 + E_2$, where

$$E_1 = E_0\cos(kx + \omega t) \quad \text{and} \quad E_2 = -E_0\cos(kx - \omega t).$$

Describe the composite wave.

7.10 The electric field of a standing electromagnetic plane wave is given by

$$E(x, t) = 2E_0 \sin kx \cos \omega t. \qquad [7.30]$$

[illegible] expression for $B(x, t)$. (You might want to [illegible] another look at Section 3.2.) Make a sketch of the standing wave.

[illegible] Considering Wiener's experiment (Fig. 7.8) in [illegible] monochromatic light of wavelength 550 nm, if the film [illegible] angled at 1.0° to the reflecting surface, determine the number of bright bands per centimeter that will appear on it.

7.12* Microwaves of frequency 10^{10} Hz are beamed directly at a metal reflector. Neglecting the refractive index of air, determine the spacing between successive nodes in the resulting standing wave pattern.

7.13* A standing wave is given by

$$E = 100 \sin \tfrac{2}{3}\pi x \cos 5\pi t.$$

[illegible] the two waves that can be superimposed to generate it.

7.14* Imagine that we strike two tuning forks, one with a frequency of 340 Hz, the other 342 Hz. What will we hear?

[illegible] 7.23 shows a carrier of frequency ω_c being [illegible] modulated by a sine wave of frequency ω_m, that is,

$$E = E_0(1 + \alpha\cos\omega_m t)\cos\omega_c t.$$

[illegible] is equivalent to the superposition of three [illegible] frequencies ω_c, $\omega_c + \omega_m$, and $\omega_c - \omega_m$. When [illegible] modulating frequencies are present, we write E as a Fourier series and sum over all values of [illegible]. The terms $\omega_c + \omega_m$ constitute what is called the *upper sideband*, and all the $\omega_c - \omega_m$ terms form the *lower sideband*. What bandwidth would you need in order to transmit the complete audible range?

7.16 Given the dispersion relation $\omega = ak^2$, compute both the phase and group velocities.

7.17 The speed of propagation of a surface wave in a liquid of depth much greater than λ is given by

$$v = \sqrt{\frac{g\lambda}{2\pi} + \frac{2\pi Y}{\rho\lambda}},$$

where

g = acceleration of gravity

λ = wavelength

ρ = density

Y = surface tension.

Compute the group velocity of a pulse in the long wavelength limit (these are called *gravity waves*).

7.18* Show that the group velocity can be written as

$$v_g = v - \lambda\frac{dv}{d\lambda}.$$

7.19 Show that the group velocity can be written as

$$v_g = \frac{c}{n + \omega(dn/d\omega)}.$$

7.20* Determine the group velocity of waves when the phase velocity varies inversely with wavelength.

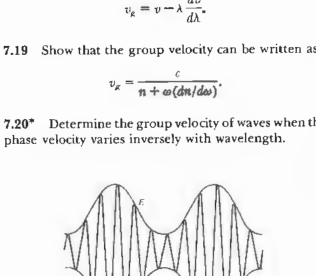


Figure 7.23

7.21* Show that the group velocity can be written as

$$v_g = \frac{c}{n} + \frac{\lambda c}{n^2}\frac{dn}{d\lambda}.$$

7.22 Using the dispersion equation,

$$n^2(\omega) = 1 + \frac{Nq_e^2}{\epsilon_0 m_e}\sum_j\left(\frac{f_j}{\omega_{0j}^2 - \omega^2}\right), \qquad [3.70]$$

show that the group velocity is given by

$$v_g = \frac{c}{1 + Nq_e^2/\epsilon_0 m_e \omega^2 2}$$

for high-frequency electromagnetic waves (e.g., x-rays). Keep in mind that since f_j are the weighting factors, $\Sigma_j f_j = 1$. What is the phase velocity? Show that $vv_g \approx c^2$.

7.23* Analytically determine the resultant when the two functions $E_1 = 2E_0 \cos \omega t$ and $E_2 = \frac{1}{2}E_0 \sin 2\omega t$ are superimposed. Draw E_1, E_2, and $E = E_1 + E_2$. Is the resultant periodic; if so, what is its period in terms of ω?

7.24 Show that

$$\int_0^\lambda \sin akx \cos bkx\, dx = 0 \qquad [7.44]$$

$$\int_0^\lambda \cos akx \cos bkx\, dx = \frac{\lambda}{2}\delta_{ab} \qquad [7.45]$$

$$\int_0^\lambda \sin akx \sin bkx\, dx = \frac{\lambda}{2}\delta_{ab}, \qquad [7.46]$$

where $a \neq 0$, $b \neq 0$, and a and b are positive integers.

7.25 Compute the Fourier series components for the periodic function shown in Fig. 7.14.

7.26 Change the upper limit of Eq. (7.59) from ∞ to a and evaluate the integral. Leave the answer in terms of the so-called *sine integral:*

$$\mathrm{Si}(z) = \int_0^z \mathrm{sinc}\, w\, dw,$$

which is a function whose values are commonly tabulated.

7.27 Write an expression for the transform $A(\omega$[illegible] the harmonic pulse of Fig. 7.24. Check that [illegible] 50% or greater for values of u *roughly* less than [illegible] With that in mind, show that $\Delta\nu\,\Delta t \sim 1$, where Δ[illegible] the bandwidth of the transform at half its maxim[illegible] amplitude. Verify that $\Delta\nu\,\Delta t \sim 1$ at half the maximu[illegible] irradiance as well. The purpose here is to get so[illegible] sense of the kind of approximations used in the [illegible]cussion.

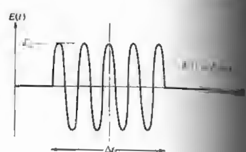


Figure 7.24

7.28 Derive an expression for the coherence [illegible] (in vacuum) of a wavetrain that has a frequency [illegible] width $\Delta\nu$; express your answer in terms of the lin[illegible] $\Delta\lambda_0$ and the mean wavelength $\bar{\lambda}_0$ of the train.

7.29 Consider a photon in the visible region [illegible] spectrum emitted during an atomic transition [illegible] 10^{-8} s. How long is the wave packet? Keeping [illegible] the results of the previous problem (if you've do[illegible] estimate the linewidth of the packet ($\bar{\lambda}_0 = 500$[illegible] What can you say about its monochromaticity [illegible]cated by the frequency stability?

7.30 The first† experiment directly measuring the bandwidth of a laser (in this case a continuou[illegible] $Pb_{0.88}Sn_{0.12}Te$ diode laser) has been successfull[illegible] out. The laser, operating at $\lambda_0 = 10{,}600$[illegible] heterodyned with a CO_2 laser, and bandwidt[illegible] row as 54 kHz were observed. Compute the cor[illegible]ing frequency stability and coherence length [illegible] lead-tin-telluride laser.

† D. Hinkley and C. Freed, *Phys. Rev. Letters* **23**, 277 (1969).

7.31* A magnetic-field technique for stabilizing a He–Ne laser to 2 parts in 10^{10} has been patented. At 632.8 nm, what would be the coherence length of a laser with such a frequency stability?

7.32 Imagine that we chop a continuous laser beam (assumed to be monochromatic at $\lambda_0 = 632.8$ nm) into 0.1-ns pulses, using some sort of shutter. Compute the resultant linewidth $\Delta\lambda$, bandwidth, and coherence length. Find the bandwidth and linewidth that would result if we could chop at 10^{15} Hz.

7.33* Suppose that we have a filter with a pass band [illegible] centered at 600 nm, and we illuminate it with [illegible] Compute the coherence length of the emerging wave.

7.34* A filter passes light with a mean wavelength of $\bar{\lambda}_0 = 500$ nm. If the emerging wavetrains are roughly $20\bar{\lambda}_0$ long, what is the frequency bandwidth of the exiting light?

7.35* Suppose we spread white light out into a fan of wavelengths by means of a diffraction grating and then pass a small select region of that spectrum out through a slit. Because of the width of the slit, a band of wavelengths 1.2 nm wide centered on 500 nm emerges. Determine the frequency bandwidth and the coherence length of this light.

8 POLARIZATION

8.1 THE NATURE OF POLARIZED LIGHT

It has already been established that light may be treated as a transverse electromagnetic wave. Thus far we have considered only **linearly polarized** or **plane-polarized** light, that is, light for which the orientation of the electric field is constant, although its magnitude and sign vary in time (Fig. 3.9). The electric field or optical disturbance therefore resides in what is known as the **plane of vibration**. That fixed plane contains both **E** and **k**, the electric field vector and the propagation vector in the direction of motion. Imagine now that we have two harmonic, linearly polarized light waves of the same frequency, moving through the same region of space, in the same direction. If their electric field vectors are collinear, the superimposing disturbances will simply combine to form a resultant linearly polarized wave. Its amplitude and phase will be examined in detail, under a diversity of conditions, in the next chapter, when we consider the phenomenon of interference. In contradistinction, if the two lightwaves are such that their respective electric field directions are mutually perpendicular, the resultant wave may or may not be linearly polarized. The exact form that light will take (i.e., its *state of polarization*) and how we can observe it, produce it, change it, and make use of it will be the concern of this chapter.

8.1.1 Linear Polarization

We can represent the two orthogonal optical distur[illegible] bances that were considered above in the form

$$\mathbf{E}_x(z, t) = \hat{\mathbf{i}} E_{0x} \cos (kz - \omega t) \tag{8.1}$$

and

$$\mathbf{E}_y(z, t) = \hat{\mathbf{j}} E_{0y} \cos (kz - \omega t + \varepsilon), \tag{8.2}$$

where ε is the relative phase difference betwe[illegible] the waves, both of which are traveling in the [illegible] Keep in mind from the start that because [illegible] in the form $(kz - \omega t)$, the addition of a *positive* [illegible] that the cosine function in Eq. (8.2) will not at[illegible] same value as the cosine in Eq. (8.1) until [illegible] (ε/ω). Accordingly, E_y lags E_x by $\varepsilon > 0$. Of cours[illegible] is a negative quantity, E_y leads E_x by $\varepsilon < 0$. The[illegible] tant optical disturbance is the vector sum of the[illegible] two perpendicular waves:

$$\mathbf{E}(z, t) = \mathbf{E}_x(z, t) + \mathbf{E}_y(z, t). \tag{8.3}$$

If ε is zero or an integral multiple of $\pm 2\pi$, the w[illegible] are said to be **in phase**. In that particular case[illegible] becomes

$$\mathbf{E} = (\hat{\mathbf{i}} E_{0x} + \hat{\mathbf{j}} E_{0y}) \cos (kz - \omega t).$$

The resultant wave therefore has a fixed ampli[illegible] equal to $(\hat{\mathbf{i}} E_{0x} + \hat{\mathbf{j}} E_{0y})$; in other words, it too is lin[illegible]

[illegible] as shown in Fig. 8.1. The waves advance [illegible] of observation where the fields are to [illegible] There one sees a single resultant **E** oscillat- [illegible] tilted line, cosinusoidally in time [Fig. [illegible] E-field progresses through one complete [illegible] cle as the wave advances along the z-axis [illegible] wavelength. This process of addition can [illegible] through [illegible] equally well in reverse; that is, we can [illegible] carri[illegible] resolve [illegible] plane-polarized wave into two orthogonal [illegible]

[illegible] now that ε is an odd integer multiple of $\pm\pi$. [illegible] are said to be 180° out of phase, and

$$\mathbf{E} = (\hat{\mathbf{i}} E_{0x} - \hat{\mathbf{j}} E_{0y}) \cos (kz - \omega t). \tag{8.5}$$

[illegible] linearly polarized, but the plane of vibration has been rotated (and not necessarily by 90°) from that of the previous condition, as indicated in Fig. 8.2.

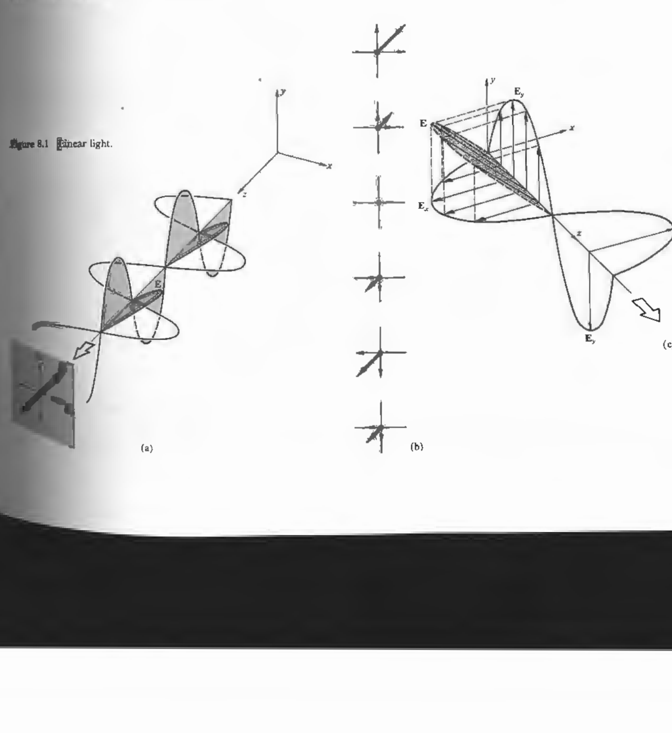


Figure 8.1 Linear light.

8.1.2 Circular Polarization

Another case of particular interest arises when both constituent waves have equal amplitudes (i.e., $E_{0x} = E_{0y} = E_0$), and in addition, their relative phase difference $\varepsilon = -\pi/2 + 2m\pi$, where $m = 0, \pm 1, \pm 2, \ldots$. In other words, $\varepsilon = -\pi/2$ or any value increased or decreased from $-\pi/2$ by whole number multiples of 2π. Accordingly

$$\mathbf{E}_x(z, t) = \hat{\mathbf{i}} E_0 \cos (kz - \omega t) \tag{8.6}$$

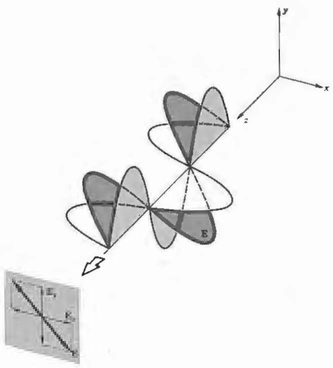


Figure 8.2 Linear light.

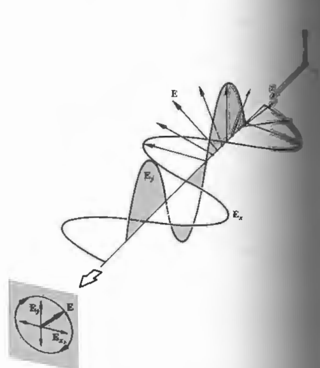


Figure 8.3 Right-circular light.

and

$$\mathbf{E}_y(z, t) = \hat{\mathbf{j}} E_0 \sin (kz - \omega t). \tag{8.7}$$

The consequent wave is given by

$$\mathbf{E} = E_0[\hat{\mathbf{i}} \cos (kz - \omega t) + \hat{\mathbf{j}} \sin (kz - \omega t)] \tag{8.8}$$

(Fig. 8.3). Notice that now the scalar amplitude of **E**, that is, $(\mathbf{E} \cdot \mathbf{E})^{1/2} = E_0$, is a constant. But the direction of **E** is time-varying, and it is not restricted, as before, to a single plane. Figure 8.4 depicts what is happening at some arbitrary point z_0 on the axis. At $t = 0$, **E** lies along the reference axis in Fig. 8.4(a), and so

$$\mathbf{E}_x = \hat{\mathbf{i}} E_0 \cos kz_0 \quad \text{and} \quad \mathbf{E}_y = \hat{\mathbf{j}} E_0 \sin kz_0 .$$

At a later time, $t = kz_0/\omega$, $\mathbf{E}_x = \hat{\mathbf{i}} E_0$, $\mathbf{E}_y = 0$, and **E** is along the x-axis. The resultant electric field vector **E** is rotating *clockwise* at an angular frequency of ω, as seen by an observer toward whom the wave is moving (i.e., looking back at the source). Such a wave is said to be **right-circularly polarized** (Fig. 8.5), and one ge[illegible] simply refers to it as *right-circular light.* The [illegible] makes one complete rotation as the wave [illegible] through one wavelength. In comparison, if $\varepsilon =$ [illegible] $5\pi/2$, $9\pi/2$, and so on (i.e., $\varepsilon = \pi/2 + 2m\pi$; [illegible] $0, \pm 1, \pm 2, \pm 3, \ldots$), then

$$\mathbf{E} = E_0[\hat{\mathbf{i}} \cos (kz - \omega t) - \hat{\mathbf{j}} \sin (kz - \text{[illegible]})]$$

The amplitude is unaffected, but **E** now rotates co[illegible] *clockwise*, and the wave is referred to as **left-circ[illegible] polarized.**

A linearly polarized wave can be synthesi[illegible] two oppositely polarized circular waves of eq[illegible] tude. In particular, if we add the right-circula[illegible] Eq. (8.8) to the left-circular wave of Eq. (8.9)[illegible]

$$\mathbf{E} = 2E_0 \hat{\mathbf{i}} \cos (kz - \omega t),$$

which [illegible] constant amplitude vector of $2E_0\hat{\mathbf{i}}$ and is [illegible] linearly polarized.

8.1.3 [illegible]ical Polarization

As far as the mathematical description is concerned, [illegible]ear and circular light may be considered to be [illegible] cases of **elliptically polarized** light, or more [illegible] *elliptical light.* This means that, in general, the [illegible]t electric field vector **E** will rotate and change [illegible]itude as well. In such cases the endpoint of **E** [illegible], in a fixed space perpendicular to **k**, as the wave sweeps by. We can see this better by actuall[illegible]iting an expression for the curve traversed by the [illegible] of **E**. To that end, recall that

$$E_x = E_{0x} \cos (kz - \omega t) \tag{8.11}$$

and

$$E_y = E_{0y} \cos (kz - \omega t + \varepsilon). \tag{8.12}$$

The [illegible]uation of the curve we are looking for should not be a [illegible]unction of either position or time; in other words we should be able to get rid of the $(kz - \omega t)$ dependence. Expand the expression for E_y into

$$E_y/E_{0y} = \cos (kz - \omega t) \cos \varepsilon - \sin (kz - \omega t) \sin \varepsilon$$

and combine it with E_x/E_{0x} to yield

$$\frac{E_y}{E_{0y}} - \frac{E_x}{E_{0x}} \cos \varepsilon = -\sin (kz - \omega t) \sin \varepsilon. \tag{8.13}$$

It follows from Eq. (8.11) that

$$\sin (kz - \omega t) = [1 - (E_x/E_{0x})^2]^{1/2},$$

so Eq. (8.13) leads to

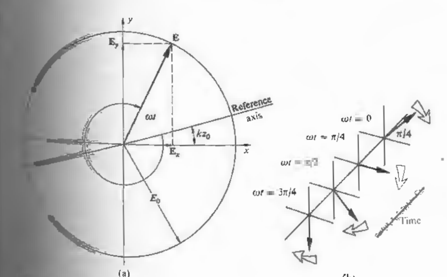
$$\left(\frac{E_y}{E_{0y}} - \frac{E_x}{E_{0x}} \cos \varepsilon\right)^2 = \left[1 - \left(\frac{E_x}{E_{0x}}\right)^2\right] \sin^2 \varepsilon.$$

Finally, on rearranging terms, we have

$$\left(\frac{E_y}{E_{0y}}\right)^2 + \left(\frac{E_x}{E_{0x}}\right)^2 - 2\left(\frac{E_x}{E_{0x}}\right)\left(\frac{E_y}{E_{0y}}\right) \cos \varepsilon = \sin^2 \varepsilon. \tag{8.14}$$

This is the equation of an ellipse making an angle α with the (E_x, E_y)-coordinate system (Fig. 8.6) such that

$$\tan 2\alpha = \frac{2E_{0x}E_{0y} \cos \varepsilon}{E_{0x}^2 - E_{0y}^2}. \tag{8.15}$$



[illegible]tion of the electric vector in a right-circular wave. [illegible]rotation rate is ω and $kz = \pi/4$.

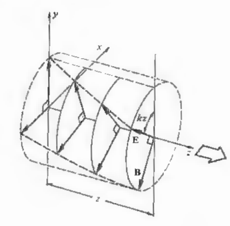


Figure 8.5 Right-circular light.

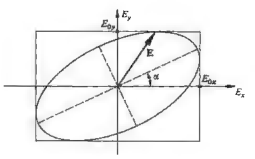


Figure 8.6 Elliptical light.

Equation (8.14) might be a bit more recognizable if the principal axes of the ellipse were aligned with the coordinate axes, that is, $\alpha = 0$ or equivalently $\varepsilon = \pm\pi/2$, $\pm 3\pi/2$, $\pm 5\pi/2, \ldots$, in which case we have the familiar form

$$\frac{E_y^2}{E_{0y}^2} + \frac{E_x^2}{E_{0x}^2} = 1. \tag{8.16}$$

Furthermore, if $E_{0y} = E_{0x} = E_0$, this can be reduced to

$$E_y^2 + E_x^2 = E_0^2, \tag{8.17}$$

which, in agreement with our previous results, is a circle. If ε is an even multiple of π, Eq. (8.14) results in

$$E_y = \frac{E_{0y}}{E_{0x}} E_x \tag{8.18}$$

and similarly for odd multiples of π,

$$E_y = -\frac{E_{0y}}{E_{0x}} E_x. \tag{8.19}$$

These are both straight lines having slopes of $\pm E_{0y}/E_{0x}$; in other words, we have linear light.

Figure 8.7 diagrammatically summarizes most of these conclusions. This very important diagram is labeled across the bottom "E_x leads E_y by: 0, $\pi/4$, $\pi/2$, $3\pi/4, \ldots$," where these are the positive values of ε to be used in Eq. (8.2). The same set of curves will occur if "E_y leads E_x by: 2π, $7\pi/4$, $3\pi/2$, $5\pi/4, \ldots$," and that happens when ε equals -2π, $-7\pi/4$, $-3\pi/2$, $-5\pi/4$, and so forth. Figure 8.7(b) illustrates how E_x leading E_y by $\pi/2$ is equivalent to E_y leading E_x by $3\pi/2$ (where the sum of these two angles equals 2π). This will be of continuing concern as we go on to shift the re[illegible] phases of the two orthogonal components [illegible] making the lightwave.

We are now in a position to refer to a par[illegible] lightwave in terms of its specific **state of** [illegible] We shall say that linearly polarized or pla[illegible] light is in a $\mathscr{P}$-state, and right- or left-cir[illegible] in an $\mathscr{R}$- or $\mathscr{L}$-*state*, respectively. Similarly, [illegible] of **elliptic polarization corresponds to an** [illegible] already seen that a $\mathscr{P}$-state can be repr[illegible] superposition of $\mathscr{R}$- and $\mathscr{L}$-states, and the [illegible] for an $\mathscr{E}$-state. In this case, as shown in [illegible] amplitudes of the two circular waves are different [illegible] analytical treatment is left for Problem 8.8.)

8.1.4 Natural Light

An ordinary light source consists of a very la[illegible] of randomly oriented atomic emitters. [illegible] atom radiates a polarized wavetrain for rou[illegible] All emissions having the same frequency w[illegible] to form a single resultant polarized wave, w[illegible] for no longer than 10^{-8} s. New wavetrains a[illegible] emitted, and the overall polarization change[illegible] pletely unpredictable fashion (see Section 8.[illegible] changes take place at so rapid a rate as to [illegible] single resultant polarization state indiscernib[illegible] is referred to as **natural light**. It is also known a[illegible] *ized light*, but this is a bit of a misnomer, since [illegible] the light is composed of a rapidly varying su[illegible] the different polarization states.

We can mathematically represent natural light in terms of two arbitrary, *incoherent*, orthog[illegible] polarized waves of equal amplitude (i.e., wa[illegible] the relative phase difference varies rapid[illegible] domly).

Keep in mind that an idealized monochro[illegible] wave must be depicted as an infinite wave[illegible] disturbance is resolved into two orthogonal [illegible] perpendicular to the direction of propag[illegible] turn, must have the same frequency, [illegible] extent, and therefore be mutually coheren[illegible] constant). In other words, *a perfectly monoch[illegible] wave is always polarized.* In fact, Eqs. (8.1) a[illegible] [illegible]the Cartesian components of a transverse ($E_z = 0$) [illegible]onic plane wave.

Whether natural in origin or artificial, light is gen[illegible] neither completely polarized nor completely [illegible]ized; both cases are extremes. More often, the [illegible] field vector varies in a way that is neither totally [illegible] nor totally irregular, and one refers to such an [illegible] disturbance as being *partially polarized.* One use[illegible] way of describing this behavior is to envision it as the [illegible] of the superposition of specific amounts of natural and polarized light.

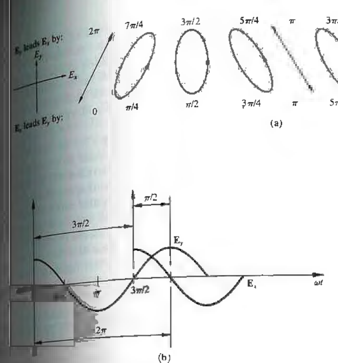


Figure 8.7 (a) Various polarization configurations. The light would be circular with $\varepsilon = \pi/2$ or $3\pi/2$ if $E_{0x} = E_{0y}$, but here for the sake of generality E_{0y} was taken to be larger than E_{0x}. (b) E_x leads E_y (or [illegible]) or alternatively, E_y leads E_x (or E_x lags E_y) by $3\pi/2$.

8.1.5 [illegible]lar Momentum and [illegible]oton Picture

We have already seen that an electromagnetic wave [illegible] an object can impart both energy and linear momentum to that body (Section 3.3). Moreover, if the incident plane wave is circularly polarized, we can expect electrons within the material to be set into circular motion in response to the force generated by the rotating **E**-field. Alternatively, we might picture the field as being composed of two orthogonal $\mathscr{P}$-states that are 90° out of phase. These simultaneously drive the electron in two perpendicular directions with a $\pi/2$ phase difference. The resulting motion is again circular. In effect the torque exerted by the **B**-field averages to zero over an orbit, and the **E**-field drives the electron with an angular velocity ω equal to the frequency of the electromagnetic wave. Angular momentum will thus be imparted by the wave to the substance in which the electrons are imbedded and to which they are bound. We can treat the problem rather simply without actually going into the details of the dynamics. The power delivered to the system is the energy transferred per

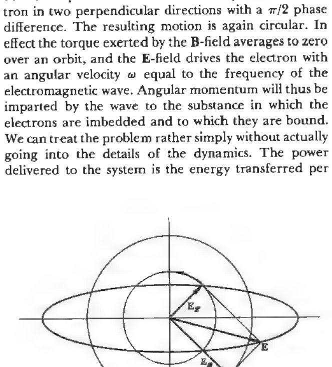


Figure 8.8 Elliptical light as the superposition of an $\mathscr{R}$- and $\mathscr{L}$-state.

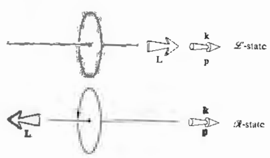


Figure 8.9 Angular momentum of a photon.

unit time, $d\mathscr{E}/dt$. Furthermore, the power generated by a torque Γ acting on a rotating body is just $\omega\Gamma$ (which is analogous to vF for linear motion), so

$$\frac{d\mathscr{E}}{dt} = \omega\Gamma. \tag{8.20}$$

Since the torque is equal to the time rate of change of the angular momentum L, it follows that on the average

$$\frac{d\mathscr{E}}{dt} = \omega\frac{dL}{dt}. \tag{8.21}$$

A charge that absorbs a quantity of energy $\mathscr{E}$ from the incident circular wave will simultaneously absorb an amount of angular momentum L such that

$$L = \frac{\mathscr{E}}{\omega}. \tag{8.22}$$

If the incident wave is in an $\mathscr{R}$-state, its **E**-vector rotates clockwise, looking toward the source. This is the direction in which a positive charge in the absorbing medium would rotate, and the angular momentum vector is therefore taken to point in the direction opposite to the propagation direction,* as shown in Fig. 8.9.

According to the quantum-mechanical description, an electromagnetic wave transfers energy in quantized packets or photons such that $\mathscr{E} = h\nu$. Thus $\mathscr{E} = \hbar\omega$ ($\hbar \equiv h/2\pi$), and the *intrinsic* or *spin* angular momentum of a photon is either $-\hbar$ or $+\hbar$, where the signs [illegible] right- or left-handedness, respectively. Notice [illegible] *angular momentum of a photon is completely indep*[illegible] *its energy*. Whenever a charged particle emits or [illegible] electromagnetic radiation, along with change[illegible] energy and linear momentum, it will undergo a change of $\pm\hbar$ in its angular momentum.*

The energy transferred to a target by an [illegible] monochromatic electromagnetic wave can be [illegible] as being transported in the form of a stream of [illegible] photons. Quite obviously, we can anticipate a [illegible] sponding quantized transport of angular mo[illegible] A purely left-circularly polarized plane wave [illegible] angular momentum to the target as if all the [illegible] photons in the beam had their spins aligne[illegible] direction of propagation. Changing the light [illegible] right circular reverses the spin orientation of the pho[illegible] well as the torque exerted by them on the tar[illegible] 1935, using an extremely sensitive torsion pend[illegible] Richard A. Beth (b. 1906) was actually able to p[illegible] such measurements.†

Thus far we've had no difficulty in describ[illegible] right- and left-circular light in the photon p[illegible] what is linearly or elliptically polarized light? [illegible] light in a $\mathscr{P}$-state can be synthesized by the [illegible] superposition of equal amounts of light in [illegible] states (with an appropriate phase difference) [illegible] photon whose angular momentum is [illegible] measured will be found to have its spin either [illegible] parallel or antiparallel to **k**. A beam of linear lig[illegible] interact with matter as if it were composed, [illegible] instant, of equal numbers of right- and left-[illegible] photons. There is a subtle point that has to be [illegible] here. We cannot say that the beam is actually made [illegible] of precisely equal amounts of well-defined right- and [illegible] photons; the photons are all identical. [illegible] individual photon exists in either spin state [illegible] likelihood. If we measured the angular [illegible] the constituent photons, $-\hbar$ would result [illegible]. This is all we can observe. We are not [illegible] often as [illegible] the photon is doing before the measure-[illegible] to w[illegible] (if in[illegible]d it exists before the measurement). As [illegible] beam will therefore impart no total angular [illegible] to a target.

[illegible]st, if each photon does not occupy both spin [illegible] the same probability, one angular momentum, say $+\hbar$, will be found to occur somewhat more [illegible] than the other, $-\hbar$. In this instance, a net positive angular momentum will therefore be imparted to the target. The result *en masse* is elliptically polarized light, that is, a superposition of unequal amounts of $\mathscr{R}$- and [illegible] bearing a particular phase relationship.

* This choice of terminology is admittedly a bit awkward. Yet its use in optics is fairly well established, even though it is completely antithetic to the more reasonable convention adopted in elementary particle physics.

* As a rather important yet simple example, consider the [illegible] atom. It is composed of a proton and an electron, each hav[illegible] of $\hbar/2$. The atom has slightly more energy when the spi[illegible] particles are in the same direction. It is possible, howeve[illegible] in a very long time, roughly 10^7 years, one of the spins wil[illegible] and be antiparallel to the other. The change in angular m[illegible] of the atom is then $\hbar$, and this is imparted to an emitted ph[illegible] carries off the slight excess in energy as well. This is [illegible] 21-cm microwave emission, which is so significant in ra[illegible]

† Richard A. Beth, "Mechanical Detection and Measure[illegible] Angular Momentum of Light," *Phys. Rev.* **50**, 115 (1936)[illegible]

8.2 POLARIZERS

[illegible] some idea of what polarized light is, [illegible] logical step is to develop an understanding of [illegible] niques used to generate it, change it, and in [illegible] manipulate it to fit our needs. An optical device [illegible] input is natural light and whose output is some [illegible] of polarized light is quite reasonably known as a *polarizer*. For example, recall that one possible representation of unpolarized light is the superposition of two equal-amplitude, incoherent, orthogonal $\mathscr{P}$-states. An instrument that separates these two components, discarding one and passing on the other, is known as a *linear polarizer*. Depending on the form of the output, we could also have *circular* or *elliptical polarizers*. All these devices vary in effectiveness down to what might be called leaky or *partial* polarizers.

Polarizers come in many different configurations, as we shall see, but they are all based on one of four fundamental physical mechanisms: *dichroism*, or selective absorption; *reflection*; *scattering*; and *birefringence*, or double refraction. There is, however, one underlying property that they all share, which is simply that *there must be some form of asymmetry associated with the process*. This is certainly understandable, since the polarizer must somehow select a particular polarization state and discard all others. In truth, the asymmetry may be a subtle one related to the incident or viewing angle, but usually it is an obvious anisotropy in the material of the polarizer itself.

8.2.1 Malus's Law

One matter needs to be settled before we go on: how do we determine experimentally whether or not a device is actually a linear polarizer?

By definition, if natural light is incident on an ideal linear polarizer, as in Fig. 8.10, only light in a $\mathscr{P}$-state

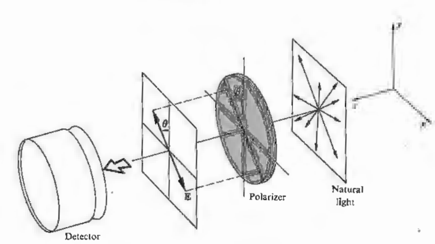


Figure 8.10 A linear polarizer.

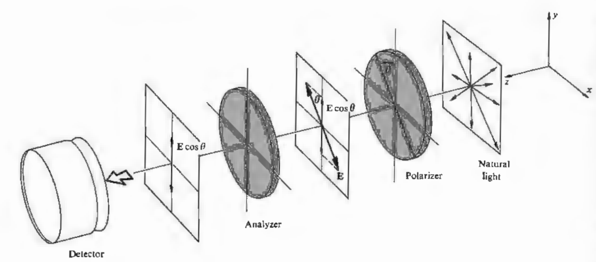


Figure 8.11 A linear polarizer and analyzer—Malus's law.

will be transmitted. That $\mathscr{P}$-state will have an orientation **parallel** to a specific direction, which we will call the **transmission axis** of the **polarizer**. In other words, only the component of the optical field parallel to the transmission axis will pass through the device essentially unaffected. If the polarizer in Fig. 8.10 is rotated about the z-axis, the reading of the detector (e.g., a photocell) will be unchanged because of the complete symmetry **of unpolarized light. Keep in mind that we are most certainly dealing with waves, but because of the very high frequency of light, our detector will**, for **practical reasons, measure only the incident irradiance. Since the** irradiance is proportional to the square of the amplitude of the electric field [Eq. (3.44)], we need only concern ourselves with that amplitude.

Now suppose that we **introduce** a second **identical ideal polarizer,** or **analyzer, whose** transmission **axis is vertical (Fig. 8.11).** If the **amplitude** of the electric **field** transmitted by the polarizer is E_0, only its component, $E_0 \cos\theta$, parallel to the transmission axis of the analyzer will be passed on to the detector (assuming no absorption). According to Eq. (3.44), the irradiance reaching the detector is then given by

$$I(\theta) = \frac{c\epsilon_0}{2} E_0^2 \cos^2\theta. \qquad (8.[illegible])$$

The maximum irradiance, $I(0) = c\epsilon_0 E_0^2/2$, occurs when the angle θ between the transmission axes of the analyzer and polarizer is zero. Equation (8.23) can accordingly be rewritten as

$$I(\theta) = I(0)\cos^2\theta. \qquad (8.[illegible])$$

This is known as **Malus's law**, having first been published in 1809 by Étienne Malus, military engineer and captain in the army of Napoleon.

Observe that $I(90°) = 0$. This arises from [illegible] the electric field that has passed through th[illegible] is perpendicular to the transmission axis of t[illegible] (the two devices so arranged are said to be [illegible] field is therefore parallel to what is called t[illegible] *axis* of the analyzer and hence obviously has no c[illegible] ponent along the transmission axis. We can use the setup of Fig. 8.11 along with Malus's law to determine whether a particular device is a linear polarizer.

8.3 DICHROISM

In its broadest sense the term ***dichroism*** **refers to the** selective absorption **of one of the two orthogonal $\mathscr{P}$-state** components of an **incident beam. The dichroic polarizer** itself is physically **anisotropic, producing a strong asym**metric or preferential **absorption of one field com**ponent while being **essentially transparent to the other.**

8.3.1 The Wire-Grid Polarizer

The simplest device **of this sort is a** grid of parallel conducting wires, as shown in **Fig. 8.12.** Imagine that an unpolarized **electromagnetic wave impinges on the** grid from **the right. The electric field can** be resolved into the usual two orthogonal **components**, in this case, one chosen to be parallel to the wires and the other perpendicular to them. The y-component of the field drives the conduction electrons along the length of each [illegible] generating a current. The electrons in turn [illegible] with lattice atoms, imparting energy to them and [illegible] heating the wires (joule heat). In this manner [illegible] transferred from the field to the grid. In [illegible] electrons accelerating along the y-axis radiate [illegible] forward and backward directions. As should [illegible] expected, the incident wave tends to be canceled by [illegible] wave radiated in the forward direction, resulting [illegible] little or no transmission of the y-component of the field. The radiation propagating in the backward direction simply appears as a reflected wave. **In contrast,** the electrons are not free to move very far in **the x-direction**, and **the corresponding field component of the wave is** essentially unaltered **as** it **propagates through the grid.** ***The transmission axis of the grid is perpendicular to the wires.*** It is a common error to assume naively that the y-component of the field somehow slips through the **spaces between the wires.**

One can easily confirm our conclusions using microwaves and a grid made of ordinary electrical wire. It is not so easy a matter, however, to fabricate a grid that will polarize light, but it has been done! In 1960 George R. Bird and Maxfield Parrish, Jr., constructed a grid having an incredible 2160 wires per mm.* **Their feat was accomplished by evaporating a stream of gold (or at other times aluminum) atoms at nearly grazing** incidence onto a plastic diffraction grating replica (see Section 10.2.7). The metal accumulated along the edges of each step in the grating to form thin microscopic "wires" whose width and spacing were less than one **wavelength across.**

Although the wire grid is useful, particularly in the **infrared, it is mentioned** here more for pedagogical than practical reasons. The underlying principle on which it is based is shared by other, more common, dichroic polarizers.

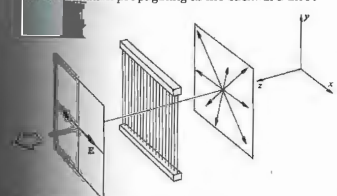


Figure 8.12 A wire-grid polarizer.

8.3.2 Dichroic Crystals

There are certain materials that are inherently dichroic because of an anisotropy in their respective crystalline structures. Probably the best known of these is the **naturally occurring mineral** ***tourmaline,*** **a semiprecious stone often used in jewelry. Actually there are several tourmalines, which are boron silicates of differing** chemical composition [e.g., $NaFe_3B_3Al_6Si_6O_{27}(OH)_4$]. For this substance there is a specific **direction** within the **crystal known** as the principal or *optic* axis, which is **determined by its** atomic configuration. The electric field component **of an incident** lightwave that is perpendicular to the **principal axis** is strongly absorbed by the

* G. R. Bird and M. Parrish, Jr., "The Wire Grid as a Near-Infrared Polarizer," *J. Opt. Soc. Am.* **50**, 886 (1960).

sample. The thicker the crystal, the more complete the absorption (Fig. 8.13). A plate cut from a tourmaline crystal parallel to its principal axis and several millimeters thick will accordingly serve as a linear polarizer. In this instance the crystal's principal axis becomes the polarizer's transmission axis. But the usefulness of tourmaline is rather limited by the fact that its crystals are comparatively small. Moreover, even the transmitted light suffers a certain amount of absorption. To complicate matters, this undesirable absorption is strongly wavelength dependent and the specimen will therefore be colored. A tourmaline crystal held up to natural white light might appear green (they come in other colors as well) when viewed normal to the principal axis and nearly black when viewed along that axis, where all the **E**-fields are perpendicular to it (ergo the term dichroic, meaning two colors).

There are several other substances that display similar characteristics. A crystal of the mineral hypersthene, a ferromagnesian silicate, might look green under white light polarized in one direction and pink for a different polarization direction.

We can get a qualitative picture of the mechanism that gives rise to crystal dichroism by considering the microscopic structure of the sample. (You might want to take another look at Section 3.5.) Recall that the atoms within a crystal are strongly bound together by short-range forces to form a periodic lattice. The electrons, which are responsible for the optical properties, can be envisioned as elastically tied to their respective equilibrium positions. Electrons associated with a given atom are also under the influence of the surrounding nearby atoms, which themselves may not be symmetrically distributed. As a result, the elastic binding forces on the electrons will be different in different directions. Accordingly, their response to the harmonic electric field of an incident electromagnetic wave will vary with the direction of **E**. If in addition to being anisotropic the material is absorbing, a detailed analysis would have to include an orientation-dependent conductivity. Currents will exist, and energy from the wave will be converted into joule heat. The attenuation, in addition to varying in direction, may be dependent on frequency as well. This means that if the incoming white light is in a $\mathcal{P}$-state, the crystal will appear colored, and the color will depend on the orientation of **E**. Substances that display two or even three different [illegible] to be dichroic or trichroic, respectively.*

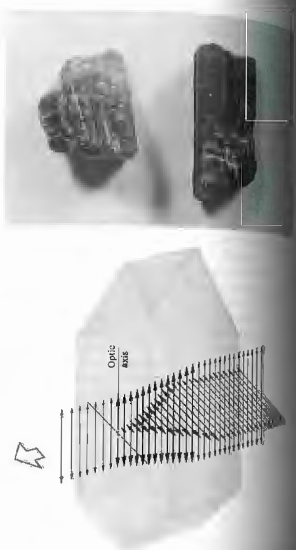


Figure 8.13 A diochroic crystal. The naturally [illegible] evident in the photograph of the tourmaline crystals [illegible] the optic axis. (Photo by E.H.)

* More will be said about these processes later on [illegible] birefringence. Suffice it to say now that for crystals [illegible] there are two distinct directions, and therefore two [illegible] displayed by *absorbing* specimens. In *biaxial* [illegible] distinct directions and the possibility of three [illegible]

8.3.3 Polaroid

In 1928 Edwin Herbert Land, then a 19-year-old undergraduate at Harvard College, invented the first dichroic sheet polarizer, known commercially as *polaroid J-sheet*. It [illegible] a synthetic dichroic substance called [illegible] or *quinine sulfate periodide*.* Land's own [illegible] account of his early work is rather infor[illegible] makes fascinating reading. It is particularly interesting to follow the sometimes whimsical origins of what is now, no doubt, the most widely used group of polarizers. The following is an excerpt from Land's remarks:

> In the literature there are a few pertinent high spots in the development of polarizers, particularly the work of William Bird Herapath, a physician in Bristol, England, whose pupil, a Mr. Phelps, had found that when he [illegible] iodine into the urine of a dog that had been [illegible] little scintillating green crystals formed in [illegible] liquid. Phelps went to his teacher, and [illegible] then did something which I [Land] think was [illegible] under the circumstances; he looked at the crys[illegible] a microscope and noticed that in some places they were light where they overlapped and in some [illegible] were dark. He was shrewd enough to recog[illegible] here was a remarkable phenomenon, a new [illegible] material [now known as herapathite]. . . .
> [illegible] Herapath's work caught the attention of Sir David [illegible] who was working in those happy days on the [illegible] . . . . Brewster, who invented the kaleido[illegible] wrote a book about it, and in that book he men[illegible] that he would like to use herapathite crystals for [illegible]. When I was reading this book, back in [illegible] 1927, I came across his reference to these [illegible] crystals, and that started my interest in [illegible].

[illegible] initial approach to creating a new form of [illegible] was to grind herapathite into millions [illegible] crystals, which were naturally needle[illegible] Their small size lessened the problem of the [illegible] of light. In his earliest experiments the crys[illegible] aligned nearly parallel to each other by means of magnetic or electric fields. Later Land found that they would be mechanically aligned when a viscous colloidal suspension of the herapathite needles was extruded through a long narrow slit. The resulting *J*-sheet was effectively a large flat dichroic crystal. The individual submicroscopic crystals still scattered light a bit, and as a result, *J*-sheet was somewhat hazy. In 1938 Land invented *H-sheet*, which is now probably the most widely used linear polarizer. It does not contain dichroic crystals but is instead a molecular analogue of the wire grid. A sheet of clear polyvinyl alcohol is heated and stretched in a given direction, its long hydrocarbon molecules becoming aligned in the process. The sheet is then dipped into an ink solution rich in iodine. The iodine impregnates the plastic and attaches to the straight long-chain polymeric molecules, effectively forming a chain of its own. The conduction electrons associated with the iodine can move along the chains as if they were long thin wires. The component of **E** in an incident wave that is parallel to the molecules drives the electrons, does work on them, and is strongly absorbed. The transmission axis of the polarizer is therefore perpendicular to the direction in which the film was stretched.

Each separate miniscule dichroic entity is known as a *dichromophore*. In *H*-sheet the dichromophores are of molecular dimensions, so scattering represents no problem. *H*-sheet is a very effective polarizer across the

* [illegible] "Some Aspects of the Development of Sheet Polarizers." [illegible] 41, 957 (1951).

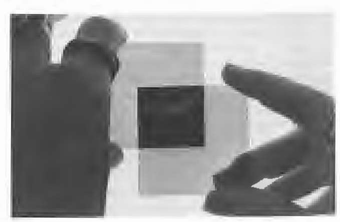


Figure 8.14 A pair of crossed polaroids. Each polaroid appears gray because it absorbs roughly half the incident light. (Photo by E.H.)

entire visible spectrum but is somewhat less so at the blue end. When a bright white light is viewed through a pair of crossed H-sheet polaroids, as in Fig. 8.14, the *extinction* color will be a deep blue as a result of this leakage. HN-50 would be the designation of a hypothetical, ideal H-sheet having a *neutral color* (N) and transmitting 50% of the incident natural light while absorbing the other 50%, which is the undesired polarization component. In practice, however, about 4% of the incoming light will be reflected back at each surface (antireflection coatings are not generally used), leaving 92%. Half of this is presumably absorbed, and thus we might contemplate an HN-46 polaroid. Actually, large quantities of HN-38, HN-32, and HN-22, each differing by the amount of iodine present, are produced commercially and are readily available (Problem 8.7).

Many other forms of polaroid have been developed.* *K-sheet*, which is humidity- and heat-resistant, has as its dichromophore the straight-chain hydrocarbon polyvinylene. A combination of the ingredients of H- and K-sheets leads to *HR-sheet*, a near-infrared polarizer.

Polaroid vectograph is a commercial material designed to be incorporated in a process for making three-dimensional photographs. The stuff never was successful at its intended purpose, but it can be used to produce some rather thought-provoking, if not mystifying, demonstrations. Vectograph film is a water-clear plastic laminate of two sheets of polyvinyl alcohol arranged so that their stretch directions are at right angles to each other. In this form there are no conduction electrons available, and the film is not a polarizer. Using an iodine solution, imagine that we draw an X on one side of the film and a Y overlapping it on the other. Under natural illumination the light passing through the X will be in a $\mathcal{P}$-state perpendicular to the $\mathcal{P}$-state light coming from the Y. In other words, the painted regions form two crossed polarizers. They will be seen superimposed on each other. Now, if the vectograph is viewed through a linear polarizer that can be rotated, either the X, the Y, or both will be seen. Obviously, more imaginative drawings can be made (one need only remember to make the one on the far side backward).

*See *Polarized Light: Production and Use*, by Shurcliff, or its more readable little brother, *Polarized Light*, by Shurcliff and Ballard.

8.4 BIREFRINGENCE

Many crystalline substances (i.e., solids whose [illegible] arranged in some sort of regular repetitive [illegible] *optically anisotropic*. In other words, their opti[illegible] ties are not the same in all directions within any [illegible] sample. The dichroic crystals of the previous [illegible] are but one special subgroup. We saw there [illegible] crystal's lattice atoms were not completely sym[illegible] arrayed, the binding forces on the electrons [illegible] anisotropic. Earlier, in Fig. 3.25(b) we represen[illegible] isotropic oscillator using the simple mechanical [illegible] of a spherical charged shell bound by identical [illegible] to a fixed point. This was a fitting represen[illegible] *optically isotropic* substances (amorphous soli[illegible] glass and plastic, are usually, but not always, [illegible] Figure 8.15 shows another charged shell, this [illegible] by springs of differing stiffness (i.e., having [illegible] spring constants). An electron that is displa[illegible] equilibrium along a direction parallel to [illegible] "springs" will evidently oscillate with a differen[illegible] teristic frequency than it would were it dis[illegible] some other direction. As we have pointed out [illegible] (Section 3.5.2), light propagates through a tr[illegible] substance by exciting the electrons within the [illegible] The electrons are driven by the E-field and they [illegible]

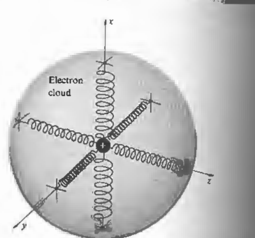


Figure 8.15 Mechanical model depicting a negatively [illegible] bound to a positive nucleus by pairs of springs ha[illegible] stiffness.

[illegible]econdary wavelets recombine, and the resul[illegible] wave moves on. The speed of the wave, [illegible] the index of refraction, is determined by [illegible] between the frequency of the **E**-field and [illegible]or characteristic frequency of the electrons. [illegible] *in the binding force will therefore be manifest* [illegible] *anisotropy in the refractive index.* For example, if [illegible] light were to move through some hypothetical [illegible] so that it encountered electrons that could be [illegible]nted by Fig. 8.15, its speed would be governed [illegible]ientation of **E**. If **E** were parallel to the stiff [illegible] is, in a direction of strong binding, here [illegible]axis, the electron's natural frequency would [illegible]portional to the square root of the spring [illegible] contrast, with **E** along the y-axis, where [illegible] force is weaker, the natural frequency [illegible] somewhat lower. Keeping in mind our earlier [illegible] dispersion and the $n(\omega)$ curve of Fig. 3.26, [illegible]riate indices of refraction might look like [illegible] 8.16. A material of this sort, which displays [illegible] indices of refraction, is said to be **birefrin-**[illegible] the crystal is such that the frequency of the [illegible]ight appears in the vicinity of ω_d, in Fig. 8.16, [illegible] in the absorption band of $n_y(\omega)$. A crystal so [illegible]ed will be strongly absorbing for one polarization [illegible]ection (y) and transparent for the other (x). [illegible] material that absorbs one of the [illegible] $\mathcal{P}$-states, passing on the other, is in fact [illegible] Furthermore, suppose that the crystal symmetry is such that the binding forces in the y- and [illegible]ctions are identical; in other words, each of these [illegible] the same natural frequency and they are [illegible]. The x-axis now defines the direction of [illegible]xis. Inasmuch as a crystal can be represented [illegible] of these oriented anisotropic charged oscil[illegible], *the optic axis is actually a direction and not merely a* [illegible] *line.* The model works rather nicely for dichroic [illegible] if light were to propagate along the optic [illegible] the yz-plane), it would be strongly absorbed, [illegible]oved normal to that axis, it would emerge [illegible]early [illegible]larized.

[illegible] *refringence* used to be used instead of our present-day [illegible]. It comes from the Latin *refractus* by way of an etymo[illegible] beginning with *frangere*, meaning to break.

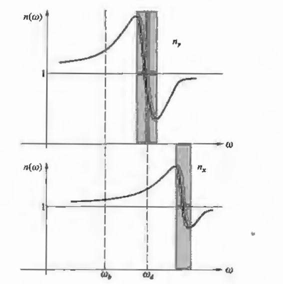


Figure 8.16 Refractive index versus frequency along two axes in a crystal. Regions where $dn/d\omega < 0$ correspond to absorption bands.

Often the characteristic frequencies of birefringent crystals are above the optical range, and they appear colorless. This is represented by Fig. 8.16 where the incident light is now considered to have frequencies in the region of ω_0. Two different indices are apparent, but absorption for either polarization is negligible. Equation (3.70) shows that $n(\omega)$ varies inversely with the natural frequency. This means that a large effective spring constant (i.e., strong binding) corresponds to a low polarizability, a low dielectric constant, and a low refractive index.

We will construct, if only pictorially, a linear polarizer utilizing birefringence by causing the two orthogonal $\mathcal{P}$-states to follow different paths and thus actually separate. Even more fascinating things can be done with birefringent crystals, as we shall see later.

8.4.1 Calcite

Let's now spend a moment relating the above ideas to an actual and somewhat typical birefringent crystal, calcite. Calcite or calcium carbonate ($CaCO_3$) is a rather

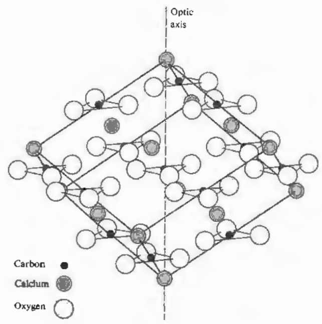


Figure 8.17 Arrangement of atoms in calcite.

common naturally occurring substance. Both marble and limestone are made up of many small calcite crystals bonded together. Of particular interest are the beautiful large single crystals, which, although they are becoming rare, can still be found, particularly in India, Mexico, and South Africa. Calcite is the most common material for making linear polarizers for use with high-power lasers.

Figure 8.17 shows the distribution of carbon, calcium, and oxygen within the calcite structure; Fig. 8.18 is a view from above, looking down along what has, in anticipation, been labeled the optic axis in Fig. 8.17. Each CO_3 group forms a triangular cluster whose plane is perpendicular to the optic axis. Notice that if we rotated Fig. 8.18 about a line normal to and passing through the center of any one of the carbonate groups, the same exact configuration of atoms would appear three times during each revolution. The direction we have designated as the optic axis corresponds to a rather special crystallographic orientation, in that it is an axis of *3-fold symmetry.* The large birefringence displayed by calcite arises from the fact that the carbonate groups are all in planes normal to the optic axis. The be[illegible] of their electrons, or rather the mutual int[illegible] the induced oxygen dipoles, is markedly diffe[illegible] E is either in or normal to those planes (Pro[illegible] In any event the asymmetry is clear enoug[illegible]

Calcite samples can readily be split, formi[illegible] surfaces known as *cleavage planes.* The crys[illegible] tially made to come apart between specifi[illegible] atoms where the interatomic bonding is rela[illegible]

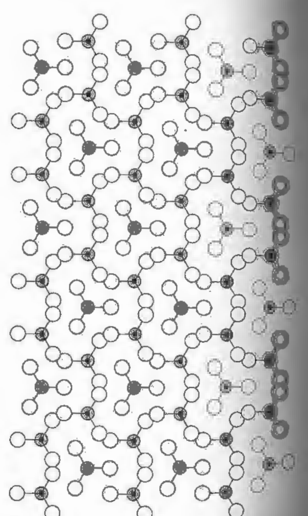


Figure 8.18 Atomic arrangement for calcite looking down the optical axis.

[illegible]ge planes in calcite (Fig. 8.18) are normal to [illegible]erent directions. As a crystal grows, atoms are added [illegible]er upon layer, following the same pattern. But [illegible] material may be available to the growth [illegible] on one side than on another, resulting in a [illegible] externally complicated shape. Even so, [illegible]vage planes are dependent on the atomic [illegible]ation, and if one cuts a sample so that each [illegible] a cleavage plane, its form will be related to [illegible]arrangement of its atoms. Such a specimen is [illegible] to as a *cleavage form.* In the case of calcite it is [illegible]bohedron, with each face a parallelogram whose [illegible] 78° 5′ and 101° 55′ (Fig. 8.19). Note that [illegible]ly two *blunt corners* where the surface planes [illegible] three obtuse angles. A line passing through [illegible]f either of the blunt corners, oriented so [illegible]es equal angles with each face (45.5°) and [illegible]3.8°), is clearly an axis of 3-fold symmetry. [illegible] be a bit more obvious if we cut the rhomb [illegible]ges of equal length.) Evidently such a line [illegible]spond to the optic axis. Whatever the natural shape [illegible] particular calcite specimen, you need only find [illegible] *corner* and you have the optic axis.

In [illegible]rasmus Bartholinus (1625–1692), doctor of [illegible] and professor of mathematics at the University of [illegible]openhagen (and incidentally, Römer's father-[illegible] came upon a new and remarkable optical [illegible]on in calcite, which he called *double refraction.* [illegible] been discovered not long before, near

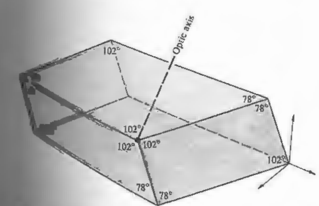


Figure 8.19 [illegible]cite cleavage form.

Figure 8.20 Double image formed by a calcite crystal (not cleavage form). (Photo by E.H.)

Eskifjordur in Iceland, and was then known as *Iceland spar.* In the words of Bartholinus:*

> Greatly prized by all men is the diamond, and many are the joys which similar treasures bring, such as precious stones and pearls . . . but he, who, on the other hand, prefers the knowledge of unusual phenomena to these delights, he will, I hope, have no less joy in a new sort of body, namely, a transparent crystal, recently brought to us from Iceland, which perhaps is one of the greatest wonders that nature has produced. . . .
>
> As my investigation of this crystal proceeded there showed itself a wonderful and extraordinary phenomenon: objects which are looked at through the crystal do not show, as in the case of other transparent bodies, a single refracted image, but they appear double.

The double image referred to by Bartholinus is quite evident in the photograph in Fig. 8.20. If we send a narrow beam of natural light into a calcite crystal normal to a cleavage plane, it will split and emerge as two parallel beams. To see the same effect quite simply, we need only place a black dot on a piece of paper and then cover it with a calcite rhomb. The image will now consist of two gray dots (black where they overlap). Rotating the crystal will cause one of the dots to remain stationary while the other appears to move in a circle

* W. F. Magie, *A Source Book in Physics.*

about it, following the motion of the crystal. The rays forming the fixed dot, which is the one invariably closer to the upper blunt corner, behave as if they had merely passed through a plate of glass. In accord with a suggestion made by Bartholinus, they are known as the **ordinary rays**, or *o-rays*. The rays coming from the other dot, which behave in such an unusual fashion, are known as the **extraordinary rays**, or *e-rays*. If the crystal is examined through an analyzer, it will be found that the ordinary and extraordinary images are linearly polarized (Fig. 8.21). Moreover, the two emerging $\mathscr{P}$-states are orthogonal.

Any number of planes can be drawn through the rhomb so as to contain the optic axis, and these are all called *principal planes*. More specifically, if the principal plane is also normal to a pair of opposite surfaces of the cleavage form, it slices the crystal across a *principal section*. There are evidently three of these passing through any one point; each is a parallelogram having angles of 109° and 71°. Figure 8.22 is a diagrammatic representation of an initially unpolarized beam traversing a principal section of a calcite rhomb. The filled-in circles and arrows drawn along the rays indicate that

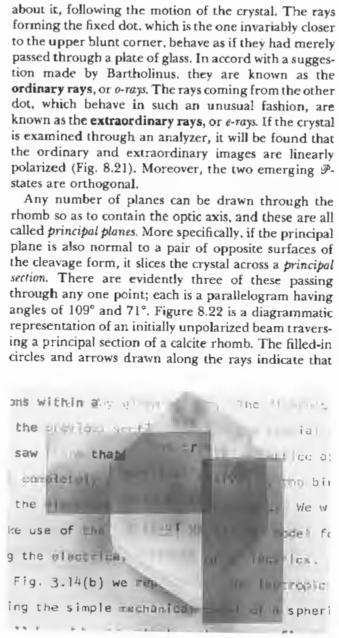


Figure 8.21 A calcite crystal (blunt corner on the bottom). The transmission axes of the two polarizers are parallel to their short edges. Where the image is doubled the lower, undeflected one is the ordinary image. Take a long look, there's a lot in this one. (Photo by E.H.)

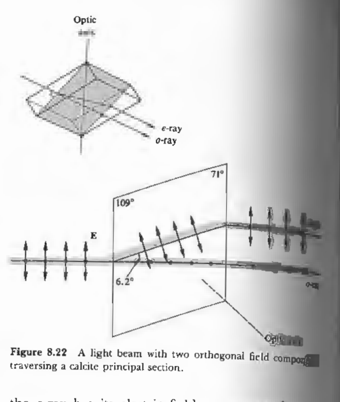
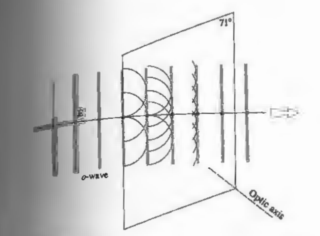


Figure 8.22 A light beam with two orthogonal field compo[illegible] traversing a calcite principal section.

the *o*-ray has its electric field vector normal to the principal section, and the field of the *e*-ray is [illegible] to the principal section.

To simplify matters a bit, let **E** in the incident [illegible] wave be linearly polarized perpendicular to [illegible] axis, as shown in Fig. 8.23. The wave strikes [illegible] of the crystal, thereupon driving electrons [illegible] tion, and they in turn reradiate secondary [illegible]. The wavelets superimpose and recombine [illegible] the refracted wave, and the process is [illegible] and over again until the wave emerges from the [illegible]. This represents a cogent physical argument for ap[illegible] ideas of **Huygens's principle**. Huygens[illegible] although without benefit of electromagnet[illegible] used his construction to explain successfully [illegible] aspects of double refraction in calcite as lo[illegible] 1690. It should be made clear from the outset [illegible] that his treatment is incomplete,* in which [illegible] appealingly, although deceptively, simple.

* A. Sommerfeld, *Optics*, p. 148.



[illegible] An incident plane wave polarized perpendicular to the [illegible]

[illegible] the **E**-field is perpendicular to the optic [illegible], one assumes that every point on the wavefront [illegible] initially corresponds to the surface) acts as a [illegible] spherical wavelets, all of which are in phase. [illegible] as long as the *field of the wavelets is everywhere* [illegible] *optic axis*, they will expand into the crystal in [illegible] directions with a speed $v_\perp$, as they would in an [illegible] medium. (Keep in mind that the speed is a [illegible] of frequency.) Since the *o*-wave displays no [illegible] behavior, this assumption seems a reasonable [illegible]. The envelope of the wavelets is essentially a [illegible] of a plane wave, which in turn serves as a [illegible] of secondary point sources. The process [illegible] and the wave moves straight across the [illegible].

[illegible] consider the incident wave in Fig. 8.24 [illegible] field is parallel to the principal section. Notice that [illegible] now has a component normal to the optic axis, [illegible] a component parallel to it. Since the medium [illegible] light of a given frequency polarized [illegible] to the optic axis propagates with a speed $v_\parallel$, [illegible] $\neq v_\perp$. In particular for calcite and sodium [illegible] ($\lambda = 589$ nm), $1.486 v_\parallel = 1.658 v_\perp = c$. What [illegible] Huygens's wavelets can we expect now? At the [illegible] oversimplifying matters, we represent each *e*-

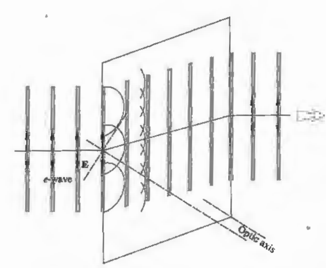


Figure 8.24 An incident plane wave polarized parallel to the principal section.

wavelet, for the moment at least, as a small sphere (Fig. 8.25). But $v_\parallel > v_\perp$, so that the wavelet will elongate in all directions normal to the optic axis. We therefore speculate, as Huygens did, that the secondary wavelets associated with the *e*-wave are ellipsoids of revolution about the optic axis. The envelope of all the ellipsoidal wavelets is essentially a portion of a plane wave parallel to the incident wave. This plane wave, however, will evidently undergo a sidewise displacement in traversing

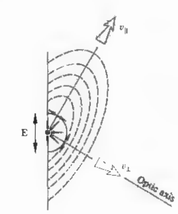


Figure 8.25 Wavelets within calcite.

the crystal. The beam moves in a direction parallel to the lines connecting the origin of each wavelet and the point of tangency with the planar envelope. It is known as the *ray direction and corresponds to the direction in which energy propagates.* This is an instance in which the direction of the ray is not normal to the wavefront.

If the incident beam is natural light, the two situations depicted in Figs. 8.23 and 8.24 will exist simultaneously, with the result that the beam will split into two orthogonal linearly polarized beams (Fig. 8.22). You can actually see the two diverging beams within a crystal by using a properly oriented narrow laserbeam (**E** neither normal nor parallel to the principal plane, which is usually the case). Light will scatter off internal flaws, making its path fairly visible.

The electromagnetic description of what is happening is rather complicated but well worth examining at this point, even if only superficially. Recall from Chapter 3 that the incident **E**-field will polarize the dielectric; that is, it will shift the distribution of charges, thereby creating electric dipoles. The field within the dielectric is thus altered by the inclusion of an induced field, and

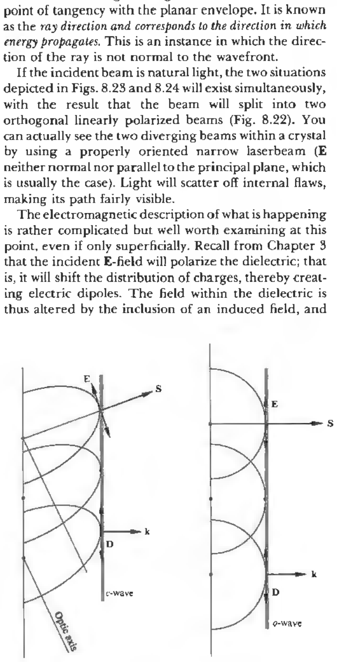


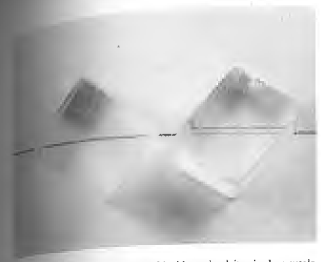
Figure 8.26 Orientations of the E-, D-, S-, and k-vectors.

one is led to introduce a new quantity, the [illegible] **D** (see Appendix 1). In isotropic media **D** is [illegible] **E** by a scalar quantity, and the two are therefore [illegible] parallel. In anisotropic crystals **D** and **E** are related [illegible] a tensor and are not always parallel. If we [illegible] Maxwell's equations to the problem of a wa[illegible] through such a medium, we find that the field[illegible] within the wavefront are **D** and **B** and not [illegible] **E** and **B**. In other words, the propagation [illegible] which is normal to the surfaces of constant ph[illegible] now perpendicular to **D** rather than **E**. In fact [illegible] and **k** are all coplanar. Clearly then, the *ray d*[illegible] corresponds to the direction of the Poynting [illegible] $\mathbf{S} = v^2\epsilon\mathbf{E} \times \mathbf{B}$, which is generally different from [illegible] **k**. Because of the manner in which the [illegible] are distributed, **E** and **D** will, however, be collinear when they are both either parallel or perpendicula[illegible] optic axis.* This means that the *o*-wavelet will e[illegible] an effectively isotropic medium and thus be sp[illegible] having **S** and **k** collinear. In contrast the *e*-wave[illegible] have **S** and **k**, or equivalently **E** and **D**, parallel [illegible] directions along or normal to the optic axis. At a[illegible] points on the wavelet it is **D** that is tangent to the ellipsoid, and therefore it is always **D** that ends up in the envelope or composite planar wavefront [illegible] crystal (Fig. 8.26).

8.4.2 Birefringent Crystals

Cubic crystals, such as sodium chloride (i.e., com[illegible] salt), have their atoms arranged in a relatively [illegible] and highly symmetric form. (There are *four* [illegible] symmetry axes, each running from one corner to a[illegible] opposite corner, unlike calcite, which has one su[illegible] Light emanating from a point source within such a crystal will propagate uniformly in all directio[illegible] spherical wave. As with amorphous solids, ther[illegible]

* In the oscillator model the general case corresponds to [illegible] in which **E** is not parallel to any of the spring directions [illegible] will drive the charge, but its resultant motion will not [illegible] in the direction of **E** because of the anisotropy of the binding fo[illegible] The charge will be displaced most, for a given force componen[illegible] direction of weakest restraint. The induced field will thus [illegible] the same orientation as **E**.



[illegible] Images in sodium chloride and calcite single crystals. [illegible]

[illegible]rred directions in the material. It will have a [illegible]dex of refraction and be *optically isotropic* (Fig. [illegible] that case all the springs in the oscillator model will [illegible]dently be identical.

[illegible] belonging to the *hexagonal*, *tetragonal*, and [illegible] systems have their atoms arranged so that light [illegible]gating in some general direction will encounter [illegible]. Such substances are optically [illegible]otropic and birefringent. The optic axis corre[illegible]nds to a direction about which the atoms are [illegible]symmetrically. Crystals like these, for which [illegible]nly one such direction, are known as *uniaxial*. A [illegible]source of natural light imbedded within one of [illegible]mens gives rise to spherical *o*-wavelets and [illegible] *e*-wavelets. It is the orientation of the field [illegible] to the optic axis that determines the speeds [illegible] these wavelets expand. The **E**-*field of the o-wa*[illegible]*everywhere normal to the optic axis,* so it moves at a [illegible] $v_\perp$ in all directions. Similarly the *e*-wave has [illegible]speed $v_\perp$ only in the direction of the optic axis (Fig. [illegible]25), along which it is always tangent to the *o*-wave. [illegible] this direction, **E** *is parallel to the optic axis,* [illegible]portion of the wavelet expands at a speed $v_\parallel$ [illegible] Uniaxial materials have two principal indices [illegible], $n_o \equiv c/v_\perp$ and $n_e \equiv c/v_\parallel$ (Problem 8.22) as [illegible]cated in Table 8.1.

Table 8.1 Refractive indices of some uniaxial birefringent crystals ($\lambda_0 = 589.3$ nm).

Crystal	n_o	n_e
Tourmaline	1.669	1.638
Calcite	1.6584	1.4864
Quartz	1.5443	1.5534
Sodium nitrate	1.5854	1.3369
Ice	1.309	1.313
Rutile (TiO_2)	2.616	2.903

The difference $\Delta n = (n_e - n_o)$ is a measure of the birefringence. In calcite $v_\parallel > v_\perp$, $(n_e - n_o)$ is -0.172, and it is said to be *negative uniaxial.* In comparison, there are other crystals, such as quartz (crystallized silicon dioxide) and ice, for which $v_\perp > v_\parallel$. Consequently, the ellipsoidal *e*-wavelets are enclosed within the spherical *o*-wavelets, as shown in Fig. 8.29. (Quartz is optically active and therefore actually a bit more complicated.) In that case, $(n_e - n_o)$ is positive, and the crystal is said to be *positive uniaxial.*

The remaining crystallographic systems, namely *orthorhombic*, *monoclinic*, and *triclinic*, have two optic axes and are therefore said to be *biaxial*. Such substances,

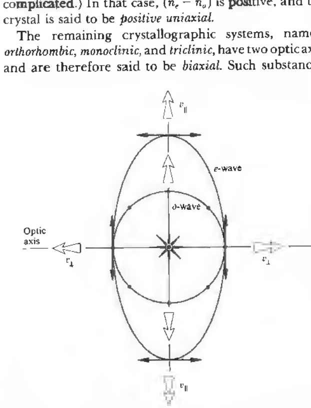


Figure 8.28 Wavelets in a negative uniaxial crystal.

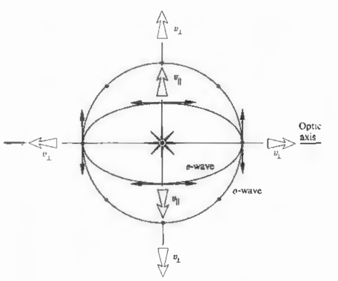


Figure 8.29 Wavelets in a positive uniaxial crystal.

for example, mica $[KH_2Al_3(SO_4)_3]$, have three different principal indices of refraction. Each set of springs in the oscillator model would then be different. The birefringence of biaxial crystals is measured as the numerical difference between the largest and smallest of these indices.

8.4.3 Birefringent Polarizers

It will now be a rather easy matter, at least conceptually, to make some sort of linear birefringent polarizer. Any number of schemes for separating the *o*- and *e*-waves have been employed, all of them, of course, relying on fact that $n_e \neq n_o$.

The most renowned birefringent polarizer was introduced in 1828 by the Scottish physicist William Nicol (1768–1851). The *Nicol prism*, as it is called, is now mainly of historical interest, having long been superseded by other, more effective polarizers. Putting it rather succinctly, the device is made by first grinding and polishing the ends (from 71° to 68°; see Fig. 8.23) of a suitably long, narrow calcite rhombohedron; then, after cutting the rhomb diagonally, the two pieces are polished and cemented back together with Canada balsam [illegible] 8.30). The balsam cement is transparent and [illegible] index of 1.55 almost midway between n_e and n_o. [illegible] incident beam enters the "prism," the *o*- and *e*-rays [illegible] fracted, they separate and strike the balsam layer. [illegible] critical angle at the calcite–balsam interface for the [illegible] about 69° (Problem 8.24). The *o*-ray (entering [illegible] narrow cone of roughly 28°) will be totally [illegible] reflected and thereafter absorbed by a layer [illegible] paint on the sides of the rhomb. The *e*-ray [illegible] laterally displaced but otherwise essentially [illegible] at least in the optical region of the spectrum [illegible] balsam absorbs in the ultraviolet).

[illegible] Foucault polarizer (Fig. 8.31) is constructed [illegible] other than calcite, which is transparent from [illegible] 5000 nm in the infrared to about 230 nm in the [illegible] aviolet. It therefore can be used over a broad [illegible] al range. The incoming ray strikes the surface [illegible] ally, and **E** can be resolved into components that are [illegible] completely parallel or perpendicular to the optic axis. The two rays traverse the first calcite section without any deviation. (We'll come back to this point later on when we talk about retarders.) Notice that if the angle of incidence on the calcite–air interface is θ, one need only arrange things so that $n_e < 1/\sin\theta < n_o$ in order for the *o*-ray, and not the *e*-ray, to be totally internally reflected. If the two prisms are now cemented together (glycerine or mineral oil are used in the ultraviolet) and the interface angle is changed appropriately, the device is known as a *Glan–Thompson* polarizer. Its field of view is roughly 30°, in comparison to about 10° for the Glan–Foucault, or *Glan–Air*, as it is often called. The latter, however, has the advantage of being able to handle the considerably higher power levels often encountered with lasers. For example, whereas the maximum irradiance for a Glan–Thompson could be about 1 W/cm² (continuous wave as opposed to pulsed), a typical Glan–Air might have an upper limit of 100 W/cm² (continuous wave). The difference is, of

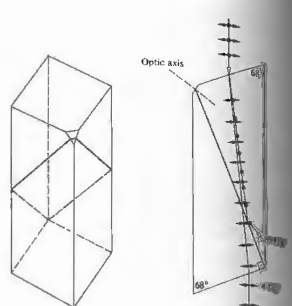
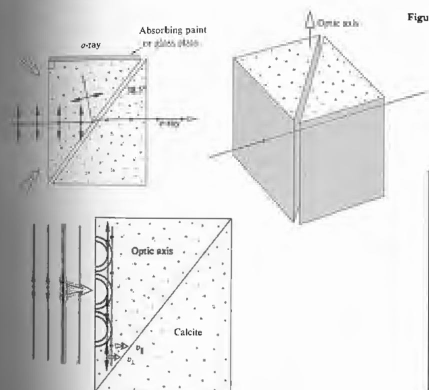


Figure 8.30 The Nicol prism. The little flat on the blunt [illegible] locates the optic axis. (Photo by E.H.)

Figure 8.31 The Glan–Foucault prism. (Photo by E.H.)



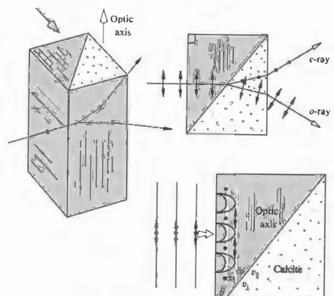


Figure 8.32 The Wollaston prism.

course, due to deterioration of the interface cement (and the absorbing paint, if it's used).

The *Wollaston prism* is actually a polarizing beam-splitter, because it passes both orthogonally polarized components. It can be made of calcite or quartz in the form indicated in Fig. 8.32. Observe that the two component rays separate at the diagonal interface. There, the *e*-ray becomes an *o*-ray, changing its index accordingly. In calcite $n_e < n_o$, and the emerging *o*-ray is bent toward the normal. Similarly, the *o*-ray, whose field is initially perpendicular to the optic axis, becomes an *e*-ray in the right-hand section. This time, in calcite the *e*-ray is bent away from the normal to the interface (see Problem 8.25). The deviation angle between the two emerging beams is determined by the prism's wedge angle, θ. Prisms providing deviations ranging from about 15° to roughly 45° are available commercially. They can be purchased cemented (e.g., with castor oil or glycerine) or not cemented at all (i.e., optically contacted), depending on the frequency and power requirements.

8.5 SCATTERING AND POLARIZATION [redacted]

8.5.1 An Introduction to Scattering

We can begin to understand many apparent [redacted] phenomena in terms of differing aspects [redacted] recurring atomic processes, and so we aga [redacted] the electron. When an electromagnetic wave [redacted] on an atom or molecule it interacts with [redacted] electron cloud, imparting energy to the atom [redacted] can be pictured as if the lowest energy or [redacted] of the atom were set into vibration. The osci [redacted] frequency of the electron cloud is equal to the [redacted] frequency ν, that is, the frequency of the harm [redacted] E-field of the lightwave. The amplitude of the [redacted] tion will be relatively large only when ν is [redacted] of the resonant frequency of the atom. In fact [redacted] nance we can employ the simple description [redacted] as first being in its ground state; upon [redacted] photon (having the resonating frequency), it [redacted] transition to an excited state. In dense media [redacted] will most likely return to its ground state, ha [redacted] pated its excess energy thermally. In rarefied gase [redacted] atom will generally make the downward tra [redacted] emitting a photon, an effect known as *resonance* [redacted]

At frequencies below or above resonance, the electrons vibrating with respect to the nucleus ma [redacted] ded as oscillating electric dipoles, and as su [redacted]

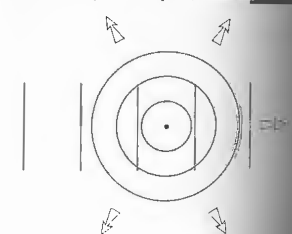


Figure 8.33 Scattering of a spherical wavelet.

[redacted] reradiate electromagnetic energy at a [redacted] coinciding with that of the incident light. [redacted] sonant emission propagates out in the dipole [redacted] pattern of Fig. 3.21. *The removal of energy from* [redacted] *dent wave and the subsequent reemission of some* [redacted] *that energy is known as scattering* (Fig. 8.33). It [redacted] rlying physical mechanism operative in [redacted] efraction, and diffraction; the scattering [redacted] ndamental indeed.

In [redacted] to electron-oscillators, which generally have [redacted] nances in the ultraviolet, there are atomic- [redacted], which correspond to the vibration of the [redacted] atoms within a molecule. Because of their [redacted] atomic-oscillators usually have resonances [redacted] ed. Moreover, they have relatively small [redacted] and are therefore of little con- [redacted] here.

[redacted] plitude of an oscillator, and thus the amount [redacted] removed from the incident wave, increases [redacted] frequency of the wave approaches a natural [redacted] cy of the atom. For low-density gases, in which atomic [redacted] eractions are negligible, absorption will be [redacted] ficant, and the reradiated or scattered wave will [redacted] off increasingly more energy as the driving [redacted] approaches a resonance. This results in some [redacted] eresting effects when the atom's natural [redacted] are in the ultraviolet and the incident wave [redacted] sible region. In that case, as the frequency [redacted] coming light increases, more and more of it [redacted] tically scattered. As an example, imagine that you are [redacted] tside on a bright clear morning. The sky is brilliant [redacted] lue, and you are surrounded, even inundated, with blue light. Sunlight streaming into the [redacted] re from one direction is scattered in all direc- [redacted] he air molecules. Without an atmosphere, the sky would be as black as the void of space, a [redacted] made in the Apollo lunar photographs (Fig. 8.34). [redacted] would then see only light that shone directly [redacted] atmosphere, the red end of the spectrum [redacted] part, undeviated, whereas the blue or [redacted] cy end is substantially scattered. This high- [redacted] scattered light reaches the observer from many directions, making the entire sky appear bright and blue [redacted] ig. 8.35). When the Sun is very low in the [redacted] its rays [redacted] through a great thickness of air. The

Figure 8.34 A half-Earth hanging in the black Moon sky. (Photo courtesy NASA)

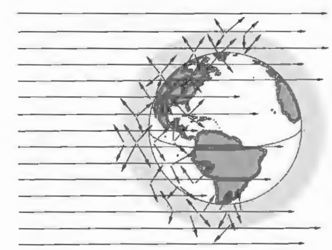


Figure 8.35 Scattering of sky light.

blues and violets are scattered sideways out of the beam much more strongly than are the yellows and reds, which continue to propagate along a line of sight from the Sun to from the Earth's familiar fiery sunsets.

Lord Rayleigh was the first to work out the dependence of the scattered flux density on frequency. In accord with Eq. (3.56), which describes the radiation pattern for an oscillating dipole, *the scattered flux density is directly proportional to the fourth power of the driving frequency.* The scattering of light by objects that are small in comparison to the wavelength is known as **Rayleigh scattering.** The molecules of dense transparent media, be they gaseous, liquid, or solid, will similarly scatter predominantly bluish light, if only feebly. The effect is quite weak, particularly in liquids and solids, because the oscillators are arrayed in a more orderly fashion, and the reemitted wavelets tend to reinforce each other only in the forward direction, canceling sideways scattering.*

The smoke rising from the end of a lighted cigarette is made up of particles that are smaller than the wavelength of light, making it appear blue when seen against a dark background. In contrast, exhaled smoke contains relatively large water droplets and appears white. Each droplet is larger than the constituent wavelengths of light and thus contains so many oscillators it is able to sustain the ordinary processes of reflection and refraction. These effects are not preferential to any one frequency component in the incident white light. The light reflected and refracted several times by a droplet and then finally returned to the observer is therefore also white. This accounts for the whiteness of small grains of salt and sugar, fog, clouds, paper, powders, ground glass, and, more ominously, the typical pallid, polluted city sky.

Particles that are approximately the size of a wavelength (remember that atoms are roughly a fraction of a nanometer across) scatter light in a very distinctive way. A large distribution of such equally sized particles can give rise to a whole range of transmitted colors. In 1883 the volcanic island Krakatoa, located in the Sunda Strait west of Java, blew apart in a fantastic conflagration. Great quantities of fine volcanic dust were spewed high into the atmosphere and drifted over vast regions of the Earth. For a few years afterward the Sun and Moon repeatedly appeared green or blue, [illegible] and sunsets were abnormally colored.

* Recall that you can see the two beams passing through a birefringent calcite crystal only if the sample contains enough flaws to act as scattering centers.

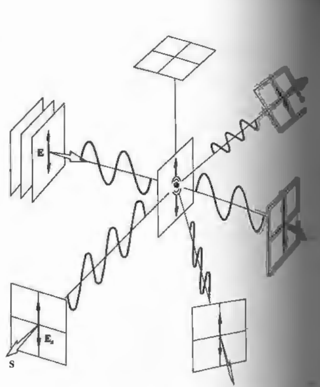


Figure 8.36 Scattering of polarized light by a molecule.

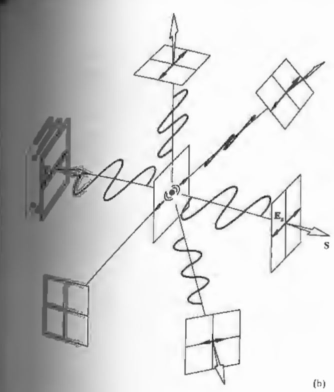


Figure 8.36b

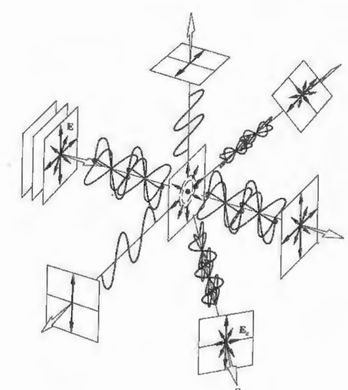


Figure 8.37 Scattering of unpolarized light by a molecule.

In 1908 Gustav Mie (1868–1957) published [illegible] solution of the scattering problem for hom[illegible] spherical particles of any size. Although compl[illegible] his solution has great practical value, parti[illegible] applied to colloidal and metallic suspensions, [illegible] particles, fog, clouds, and the solar corona, to name only a few.

8.5.2 Polarization by Scattering

Imagine that we have a linearly polarized plane wave incident on an air molecule, as pictured in Fig. 8.36. The orientation of the electric field of the scattered radiation (i.e., $\mathbf{E}_s$) follows the dipole pattern [illegible] $\mathbf{E}_s$, the Poynting vector **S**, and the oscillating [illegible] all coplanar (Fig. 3.22). The vibrations induc[illegible] [illegible] parallel to the **E**-field of the incoming light [illegible] are perpendicular to the propagation direc[illegible] [illegible] once again that the dipole does not radiate [illegible] of its axis. Now if the incident wave is [illegible], it can be represented by two orthogonal, [illegible] $\mathscr{P}$-states, in which case the scattered light [illegible] is equivalent to a superposition of the condi[illegible] in Fig. 8.36, (a) and (b). Evidently, the [illegible] in the forward direction is completely [illegible] off that axis it is partially polarized, becom[illegible] [illegible] more polarized as the angle increases. [illegible] direction of observation is normal to the [illegible], the light is completely linearly polarized. [illegible] easily verify these conclusions if you happen [illegible] of polaroid. Locate the Sun and then [illegible] region of the sky at roughly 90° to the solar [illegible] you'll find that portion of the sky to be partially [illegible] normal to the rays (see Fig. 8.38). It's not [illegible] polarized mainly because of molecular [illegible], the presence of large particles in the air, [illegible] polarizing effects of multiple scattering. The

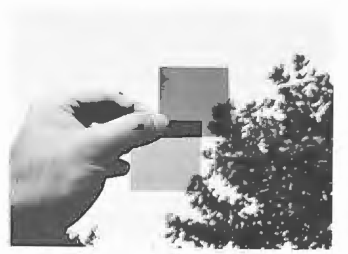


Figure 8.38 A pair of crossed polarizers. The upper polaroid is noticeably darker than the lower one, indicating the partial polarization of sky light. (Photo by E.H.)

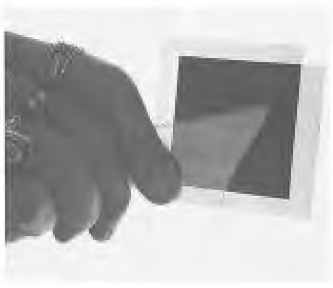


Figure 8.39 A piece of waxed paper between crossed polarizers.

latter condition can be illustrated by placing a piece of waxed paper between crossed polaroids (Fig. 8.39). Because the light undergoes a good deal of scattering and multiple reflections within the waxed paper, a given oscillator may "see" the superposition of many essentially unrelated E-fields. The resulting emission is almost completely depolarized.

As a final experiment, put a few drops of milk in a glass of water and illuminate it (perpendicular to its axis) using a bright flashlight. The solution will appear bluish white in scattered light and yellowish in direct light, indicating that the operative mechanism is Rayleigh scattering. Accordingly, the scattered light will also be partially polarized.

Using very much the same ideas Charles Glover Barkla (1877–1944) in 1906 established the transverse wave nature of x-ray radiation by showing that it could be polarized in certain directions as a result of scattering off matter.

8.6 POLARIZATION BY REFLECTION

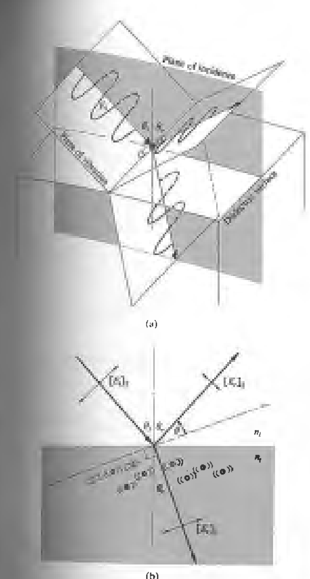
One of the most common sources of polarized light is the ubiquitous process of reflection from dielectric media. The glare spread across a window pa[illegible] of paper, or a balding head, the sheen on [illegible] of a telephone, a billiard ball, or a book ja[illegible] generally partially polarized.

The effect was first studied by Étienne Malu[illegible] The Paris Academy had offered a prize for a ma[illegible] cal theory of double refraction, and Malus acc[illegible] undertook a study of the problem. He was sta[illegible] the window of his house in the Rue d'Enfer one [illegible] examining a calcite crystal. The Sun was setti[illegible] its image reflected toward him from the window[illegible] Luxembourg Palace not far away. He held up th[illegible] and looked through it at the Sun's reflection. [illegible] astonishment, he saw one of the double images [illegible] pear as he rotated the calcite. After the Sun had [illegible] continued to verify his observations into the [illegible] candlelight reflected from the surfaces of [illegible] glass.* The significance of birefringence and [illegible] nature of polarized light were becoming clear [illegible] first time. At that time no satisfactory explana[illegible] of polarization existed within the context of th[illegible] theory. During the next 13 years the work of [illegible] men, principally Thomas Young and Augustin [illegible] finally led to the representation of light as [illegible] transverse vibration. (Keep in mind that all this [illegible] the electromagnetic theory of light by roughly [illegible]

The electron-oscillator model provides a [illegible] simple picture of what happens when light is [illegible] on reflection. Unfortunately, it's not a complete [illegible] tion, since it does not account for the behavior [illegible] netic nonconducting materials.† Nonetheless [illegible] an incoming plane wave linearly polarized so that its E-field is perpendicular to the plane of inciden[illegible] (Fig. 8.40). The wave is refracted at the interface, [illegible] the medium at some transmission angle θ_t. Its [illegible] field drives the bound electrons, in this [illegible] the plane of incidence, and they in turn reradi[illegible] portion of that reemitted energy appears in [illegible] of a reflected wave. It should be clear then from the [illegible] and the dipole radiation pattern that both the [illegible] and refracted waves must also be in $\mathcal{P}$-states normal to the incident plane.* In contradistinction, if the incoming E-field is in the incident plane, the electron-oscillators near the surface will vibrate under the influence of the refracted wave, as shown diagrammatically in Fig. 8.40(b). Observe that a rather interesting thing is happening to the reflected wave. Its flux density is now relatively low, because the reflected ray direction makes a small angle θ with the dipole axis. If we could arrange things so that $\theta = 0$, or equivalently $\theta_r + \theta_t =$

* Try it with a candle flame and a piece of glass. Ho[illegible] $\theta_p \approx 56°$ for the most pronounced effect. At near glan[illegible] both of the images will be bright and neither will vanish [illegible] the crystal—Malus apparently lucked out at a good ang[illegible] window.

† W. T. Doyle, "Scattering Approach to Fresnel's [illegible] Brewster's Law," *Am. J. Phys.* 53, 463 (1985).



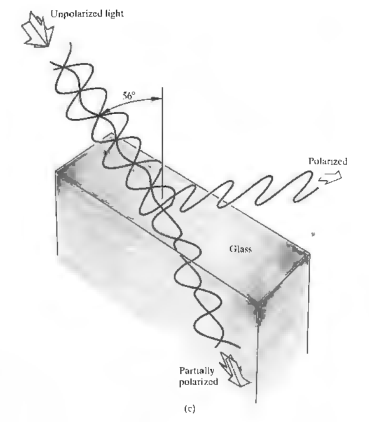


Figure 8.40 (a) A wave reflecting and refracting at an interface. (b) Electron-oscillators and Brewster's law. (c) The polarization of light that occurs on reflection from a dielectric, such as glass, water, or plastic.

* [illegible] reflection is determined by the scattering array, as [illegible] 10.2.7. The scattered wavelets in general combine [illegible] only one direction, yielding a reflected ray at an [illegible] of the incident ray.

90°, the reflected wave would vanish entirely. *Under those circumstances, for an incoming unpolarized wave made up of two incoherent orthogonal 𝒫-states, only the component polarized normal to the incident plane and therefore parallel to the surface will be reflected.* The particular angle of incidence for which this situation occurs is designated by θ_p and referred to as the **polarization angle** or **Brewster's angle**, whereupon $\theta_p + \theta_t = 90°$. Hence, from Snell's law

$$n_i \sin \theta_p = n_t \sin \theta_t$$

and the fact that $\theta_t = 90° - \theta_p$, it follows that

$$n_i \sin \theta_p = n_t \cos \theta_p$$

and

$$\tan \theta_p = n_t/n_i. \tag{8.25}$$

This is known as *Brewster's law* after the man who discovered it empirically, Sir David Brewster (1781–1868), professor of physics at St. Andrews [illegible] and, of course, inventor of the kaleidoscope.

When the incident beam is in air $n_i = 1$ and if the transmitting medium is glass, in which case [illegible] the polarization angle is ≈56°. Similarly if an [illegible] ized beam strikes the surface of a pond (n_t ≈ [illegible] H_2O) at an angle of 53°, the reflected beam [illegible] completely polarized with its E-field perpendi[illegible] the plane of incidence or, if you like, paral[illegible] water's surface (Fig. 8.41). This suggests a rat[illegible] way to locate the transmission axis of an [illegible] polarizer; one just needs a piece of glass or a pond.

The problem immediately encountered in [illegible] this phenomenon to construct an effective po[illegible] in the fact that the reflected beam, although co[illegible] polarized, is weak, and the transmitted beam [illegible] strong, is only partially polarized. One sch[illegible] trated in Fig. 8.42, is often referred [illegible] *polarizer*. It was invented by Dominique F. J. [illegible]

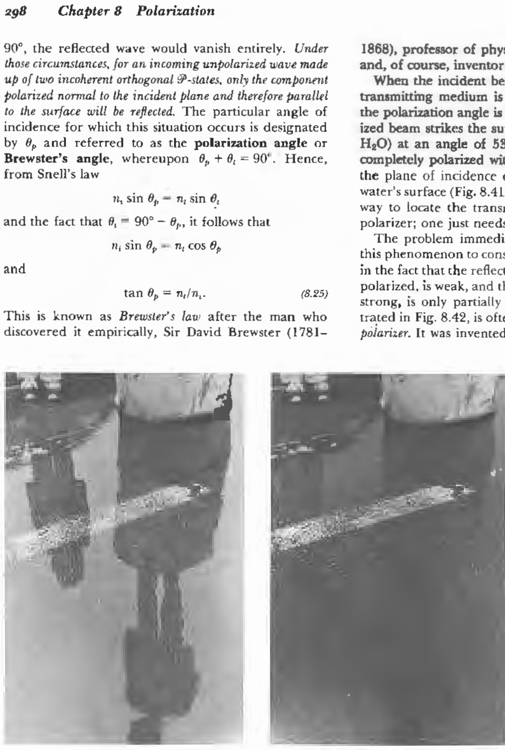
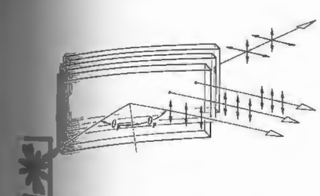


Figure 8.41 Light [illegible] off a puddle is partially [illegible] ized. (a) When viewed th[illegible] a Polaroid filter whose [illegible] mission axis is parallel [illegible] ground, the glare is passe[illegible] visible. When the Pola[illegible] transmission axis is [illegible] dicular to the [illegible] most of the glare [illegible] (Photo courtesy Martin Seymour.)



[illegible] The pile-of-plates polarizer.

[illegible] the year 1812. Devices of this kind can be fabricated [illegible] glass plates in the visible, silver chloride plates in [illegible] red, and quartz or vycor in the ultraviolet. It's [illegible] to construct a crude arrangement of this [illegible] a dozen or so microscope slides. (The beautiful [illegible] may appear when the slides are in contact [illegible] d in the next chapter.)

8.6.1 [illegible] Application of the Fresnel Equations

In [illegible] 4 we obtained a set of formulas known as the [illegible], which describe the effects of an [illegible] electromagnetic plane wave falling on the [illegible] between two different dielectric media. These [illegible] relate the reflected and transmitted field [illegible] to the incident amplitude by way of the [illegible] incidence θ_i and transmission θ_t. For linear [illegible] its E-field parallel to the plane of incidence, [illegible] the *amplitude reflection coefficient* as $r_\parallel \equiv$ [illegible] that is, the ratio of the reflected to incident [illegible] *amplitudes*. Similarly when the electric field [illegible] to the incident plane, we have $r_\perp \equiv [E_{0r}/E_{0i}]_\perp$. [illegible] ponding irradiance ratio (the incident and [illegible] beams have the same cross-sectional area) is [illegible] *reflectance*, and since irradiance is proportional [illegible] the square of the amplitude of the field,

$$R_\parallel = r_\parallel^2 = [E_{0r}/E_{0i}]_\parallel^2 \quad \text{and} \quad R_\perp = r_\perp^2 = [E_{0r}/E_{0i}]_\perp^2.$$

[illegible] appropriate Fresnel equations yields

$$R_\parallel = \frac{\tan^2(\theta_i - \theta_t)}{\tan^2(\theta_i + \theta_t)} \tag{8.26}$$

and

$$R_\perp = \frac{\sin^2(\theta_i - \theta_t)}{\sin^2(\theta_i + \theta_t)}. \tag{8.27}$$

Observe that whereas $R_\perp$ can never be zero, $R_\parallel$ is indeed zero when the denominator is infinite, that is, when $\theta_i + \theta_t = 90°$. The reflectance, for linear light with **E** parallel to the plane of incidence, thereupon vanishes; $E_{r\parallel} = 0$ and the beam is completely transmitted. This is of course the essence of Brewster's law.

If the incoming light is unpolarized, we can represent it by two now familiar orthogonal, incoherent, equal-amplitude 𝒫-states. Incidentally, the fact that they are equal in amplitude means that the amount of energy in one of these two polarization states is the same as that in the other (i.e., $I_{i\parallel} = I_{i\perp} = I_i/2$), which is quite reasonable. Thus

$$I_{r\parallel} = I_{r\parallel} I_i / 2I_{i\parallel} = R_\parallel I_i/2,$$

and in the same way $I_{r\perp} = R_\perp I_i/2$. The reflectance in natural light, $R = I_r/I_i$, is therefore given by

$$R = \frac{I_{r\parallel} + I_{r\perp}}{I_i} = \tfrac{1}{2}(R_\parallel + R_\perp). \tag{8.28}$$

Figure 8.43 is a plot of Eqs. (8.26), (8.27), and (8.28) for the particular case when $n_i = 1$ and $n_t = 1.5$. The middle curve, which corresponds to incident natural light, shows that only about 7.5% of the incoming light is reflected when $\theta_i = \theta_p$. The transmitted light is then evidently partially polarized. When $\theta_i \neq \theta_p$ both the transmitted and reflected waves are partially polarized.

It is often desirable to make use of the concept of the **degree of polarization** V, defined generally as

$$V = \frac{I_p}{I_p + I_u}, \tag{8.29}$$

in which I_p and I_u are the constituent flux densities of polarized and unpolarized light. For example, if $I_p = 4\ \text{W/m}^2$ and $I_u = 6\ \text{W/m}^2$, then $V = 40\%$ and the beam is partially polarized. With unpolarized light $I_p = 0$ and obviously $V = 0$, whereas at the opposite extreme, if $I_u = 0$, $V = 1$ and the light is completely polarized; thus $0 \le V \le 1$. One frequently deals with partially polarized, linear, quasimonochromatic light. In that case if we rotate an analyzer in the beam, there will be an

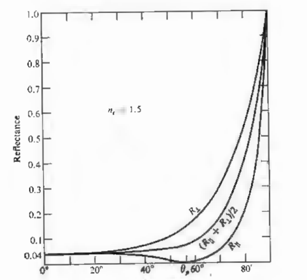


Figure 8.43 Reflectance versus incident angle.

orientation at which the transmitted irradiance is maximum (I_{max}), and perpendicular to this, a direction where it is minimum (I_{min}). Clearly $I_p = I_{max} - I_{min}$, and so

$$V = \frac{I_{max} - I_{min}}{I_{max} + I_{min}}. \tag{8.30}$$

Note that V is actually a property of the beam, which may obviously be partially or even completely polarized before encountering any sort of polarizer.

8.7 RETARDERS

We shall now consider a class of optical elements known as **retarders**, which serve to change the polarization of an incident wave. In principle the operation of a retarder is quite simple. One of the two constituent coherent $\mathscr{P}$-states is somehow caused to lag in phase behind the other by a predetermined amount. Upon emerging from the retarder, the relative phase of the two components is different than it was initially, and thus the polarization state is different as well. Indeed, once we have developed the concept of the retarder, [illegible] able to convert any given polarization state [illegible] other and in so doing create circular and [illegible] polarizers as well.

8.7.1 Wave Plates and Rhombs

Recall that a plane monochromatic wave incid[illegible] uniaxial crystal, such as calcite, is generally di[illegible] two, emerging as an ordinary and an extr[illegible] beam. In contrast, we can cut and polish a cal[illegible] so that its optic axis will be normal to both [illegible] and back surfaces (Fig. 8.44). A normally incid[illegible] wave can only have its **E**-field perpendicular [illegible] axis. The secondary spherical and ellipsoidal [illegible] will be tangent to each other in the direc[illegible] optic axis. The *o*- and *e*-waves, which are [illegible] these wavelets, will be coincident, and a single [illegible] ted plane wave will pass through the crystal [illegible] no relative phase shifts and no double imag[illegible]

Now suppose that the direction of the optic [illegible] arranged to be parallel to the front and back su[illegible] as shown in Fig. 8.45. If the **E**-field of an inci[illegible] monochromatic plane wave has components pa[illegible] and perpendicular to the optic axis, two separate [illegible] waves will propagate through the crystal. Si[illegible] $n_o > n_e$, and the *e*-wave will move across the [illegible] more rapidly than the *o*-wave. After travers[illegible] of thickness d the resultant electromagnetic [illegible] superposition of the *e*- and *o*-waves, which [illegible] relative phase difference of $\Delta\varphi$. Keep in mind [illegible] are harmonic waves of the same frequency [illegible] fields are orthogonal. The relative optical pa[illegible] difference is given by

$$\Lambda = d(|n_o - n_e|), \tag{8.31}$$

and since $\Delta\varphi = k_0\Lambda$,

$$\Delta\varphi = \frac{2\pi}{\lambda_0} d(|n_o - n_e|). \tag{8.32}$$

* If you have a calcite rhomb, find the blunt corner and [illegible] crystal until you are looking along the direction of the [illegible] through one of the faces. The two images will converge [illegible] completely overlap.

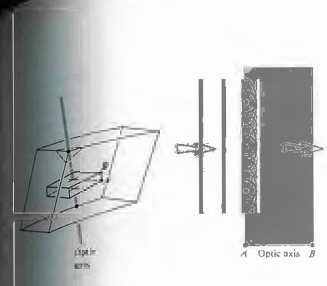


Figure 8.44 A calcite plate cut perpendicular to the optic axis.

where [illegible] is the wavelength in vacuum (the form containing the absolute value of the index [illegible] is the most general statement). The state of [illegible] of the emergent light evidently depends [illegible] amplitudes of the incoming orthogonal field [illegible] and of course on $\Delta\varphi$.

[illegible] Full-Wave Plate

If $\Delta\varphi$ is equal to 2π, the *relative retardation* is one [illegible]elength; the *e*- and *o*-waves are back in phase, and [illegible]e is no observable effect on the polarization of the [illegible]dent monochromatic beam. When the *relative* [illegible]*rdation* $\Delta\varphi$, which is also known as the *retardance*, is [illegible] the device is called a *full-wave plate*. (This does not [illegible]n that $d = \lambda$.) In general the quantity $|n_o - n_e|$ in [illegible] changes little over the optical range, so that [illegible] effectively as $1/\lambda_0$. Evidently a full-wave plate can [illegible]ion only in the manner discussed for a par[illegible] wavelength, and retarders of this sort are thus [illegible] to be *chromatic*. If such a device is placed at some [illegible]rary orientation between crossed linear polarizers, [illegible] light entering it (in this case let it be white light) [illegible]ear. Only the one wavelength that satisfies Eq. (8.32) will pass through the retarder unaffected, [illegible] to be absorbed in the analyzer. All other [illegible]ngths will undergo some retardance and will [illegible]ingly [illegible] from the wave plate as various forms of elliptical light. Some portion of this light will proceed through the analyzer, finally emerging as the complementary color to that which was extinguished. It is a common error to assume that a full-wave plate behaves as if it were isotropic at all frequencies; it obviously doesn't.

Recall that in calcite, the wave whose **E**-field vibrations are parallel to the optic axis travels fastest, that is, $v_\parallel > v_\perp$. The direction of the optic axis in a *negative* uniaxial retarder is therefore often referred to as the **fast axis**, and the direction perpendicular to it is the **slow axis.** For *positive* uniaxial crystals, such as quartz, these principal axes are reversed, with the slow axis corresponding to the optic axis.

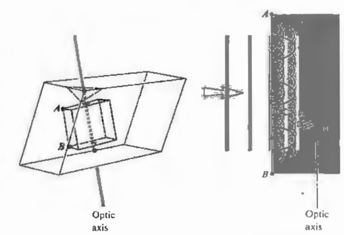


Figure 8.45 A calcite plate cut parallel to the optic axis.

The Half-Wave Plate

A retardation plate that introduces a relative phase difference of π radians or 180° between the *o*- and *e*-waves is known as a *half-wave plate*. Suppose that the plane of vibration of an incoming beam of linear light makes some arbitrary angle θ with the fast axis, as shown in Fig. 8.46. In a negative material the *e*-wave will have a higher speed (same ν) and a longer wavelength than the *o*-wave. When the waves emerge from the plate there will be a relative phase shift of $\lambda_0/2$ (that is, $2\pi/2$ radians), with the effect that **E** will have rotated through 2θ. Going back to Fig. 8.7, it should be evident that a

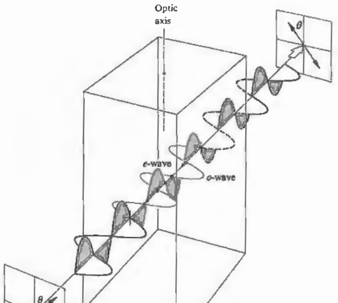


Figure 8.46 A half-wave plate.

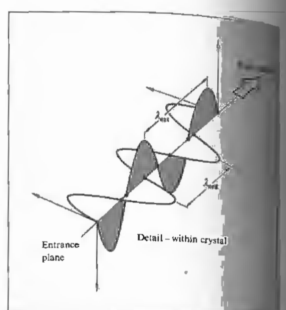
half-wave **plate** will **similarly flip** elliptical light. In addi**tion**, it will **invert** the **handedness** of circular or elliptical light, chan**ging right** to left and vice versa.

As the **e- and o-waves** progress through any retardation plate, their re**lative phase** difference $\Delta\varphi$ **increases**, and the state of **polarization** of the wave **therefore gradually changes** from **one point in the plate to the next. Figure 8.7 can** be **envisioned as a sampling of a few of these states** at **one instant in time taken at** different locations. Evidently if the thickness of the material is such that

$$d(|n_o - n_e|) = (2m + 1)\lambda_0/2,$$

where $m = 0, 1, 2, \ldots$, it will function as a half-wave **plate** ($\Delta\varphi = \pi, 3\pi, 5\pi$, etc.).

Although its behavior is simple to visualize, calcite is actually not often used to make retardation plates. It is quite brittle and difficult to handle in thin slices, but more than that, its birefringence, the difference



between n_e and n_o, is a bit too large for [illegible]. On the other hand, quartz with its [illegible] fringence is frequently used, but it has no natu[illegible] cleavage planes and must be cut, ground, and [illegible] making it rather expensive. The biaxial crystal [illegible] used most often. There are several forms of [illegible] serve the purpose admirably, for example, [illegible] phlogopite, biotite, or muscovite. The most com[illegible] occurring variety is the pale brown muscovite [illegible] easily cleaved into strong, flexible, and exce[illegible] large-area sections. Moreover, its two principa[illegible] almost exactly parallel to the cleavage pla[illegible] those axes the indices are about 1.599 and 1.59[illegible] for sodium light, and although these numbers var[illegible] from one sample to the next, their difference [illegible] constant. The minimum thickness of a [illegible] plate is about 60 microns. Crystalline quar[illegible] crystal magnesium fluoride (for the IR range from 3000 nm to about 6000 nm), and cadmium sul[illegible] the IR range from 6000 nm to about 12,000 [illegible] also widely used for wave plates.

Retarders are also made from sheets of poly[illegible] alcohol that have been stretched so as to align [illegible] long-chain organic molecules. Because of the [illegible]

[illegible] electrons in the material do not experience [illegible]nding forces along and perpendicular to the [illegible] these molecules. Substances of this sort are [illegible] permanently birefringent, even though they are [illegible]stalline.

[illegible] can make a rather nice half-wave plate by just [illegible] a strip of ordinary (glossy) cellophane tape over [illegible] surface of a microscope slide. The fast axis, [illegible] the vibration direction of the faster of the two [illegible] corresponds to the transverse direction across [illegible]'s width, and the slow axis is along its length. [illegible] its manufacture, cellophane (which is made [illegible] regenerated cellulose extracted from cotton or [illegible]ulp) is formed into sheets, and in the process its [illegible]les become aligned, leaving it birefringent. If [illegible] your half-wave plate between crossed linear [illegible], it will show no effect when its principal axes [illegible] with those of the polarizers. If, however, it is [illegible] with respect to the polarizer, the E-field [illegible]om the tape will be flipped 90° and will thus [illegible] the transmission axis of the analyzer. Light [illegible]rough the region covered by the tape as if [illegible] in the black background of the crossed [illegible] (Fig. 8.47). A piece of cellophane wrapping (e.g., from certain cigarette packs) will generally also [illegible] a half-wave plate. See if you can determine [illegible]rientation of each of its principal axes using the [illegible] and crossed polaroids. (Notice the fine [illegible] ridges on the sheet cellophane.)

[illegible]arter-Wave Plate

[illegible]e plate is an optical element that introduces a relative phase shift of $\Delta\varphi = \pi/2$ between the [illegible]nt orthogonal o- and e-components of a wave. [illegible] once again from Fig. 8.7 that a phase shift of 90[illegible] convert linear to elliptical light and vice versa. [illegible] be apparent that linear light incident parallel [illegible] principal axis will be unaffected by any sort of [illegible]on plate. You can't have a *relative* phase [illegible] without having two components. With incident natural light, the two constituent $\mathscr{P}$-states are [illegible], that is, their relative phase difference [illegible] randomly and rapidly. The introduction of an [illegible] constant phase shift by any form of retarder

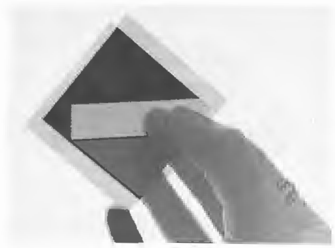


Figure 8.47 A hand holding a piece of Scotch tape stuck to a microscope slide between two crossed polaroids. (Photo by E.H.)

will still result in a random phase difference and thus have no noticeable effect. When linear light at 45° to either **principal axis** is incident on a **quarter-wave plate,** its o- **and** e-**compone**nts have equal **amplitudes. Under** these spe**cial circumstances** a **90°** phase shift **converts** the wave **into circular light.** Sim**ilar**ly, an inco**ming** circular beam will emerge linearly polarized.

Quarter-**wave plates** are also usually made of quartz, mica, or or**ganic poly**meric plastic. In any case, the thickness of the birefringent material must satisfy the **expression** $d(|n_o - n_e|) = (4m + 1)\lambda_0/4$. **You can make a crude quarter-wave plate using household plastic food wrap, the thin stretchy stuff that comes on rolls. Like cellophane, it has ridges running in the long direction, which coincides with a principal axis. Overlap about a** half dozen layers, being careful to keep the ridges **parallel. Position the plastic at 45° to the axes of a polarizer and examine it through a rotating analyzer. Keep adding one layer at a time until the irradiance stays roughly constant as the analyzer turns; at that** point you will have circular light and a quarter-wave **plate.** This is easier said than done in white light, but it's well worth trying.

Commercial wave plates are generally designated by their *linear retardation*, which might be, for example, 140 nm for a quarter-wave plate. This simply means that the device has a 90° retardance only for green light of wavelength 560 nm (i.e., 4 × 140). The linear retardation is usually not given quite that precisely; 140 ± 20 nm is more realistic. The retardation of a wave plate can be increased or decreased from its specified value by tilting it somewhat. If the plate is rotated about its fast axis, the retardation will increase, whereas a rotation about the slow axis has the opposite effect. In this way a wave plate can be tuned to a specific frequency in a region about its nominal value.

The Fresnel Rhomb

We saw in Chapter 4 that the process of total internal reflection introduced a relative phase difference between the two orthogonal field components. In other words, the components parallel and perpendicular to the plane of incidence were shifted in phase with respect to each other. In glass ($n = 1.51$) a shift of 45° accompanies internal reflection at the particular incident angle of 54.6° [Fig. 4.25(e)]. The Fresnel rhomb shown in Fig. 8.48 utilizes this effect by causing the beam to be internally reflected twice, thereby imparting a 90° relative phase shift to its components. If the incoming plane wave is linearly polarized at 45° to the plane of incidence, the field components $[E_i]_\parallel$ and $[E_i]_\perp$ will

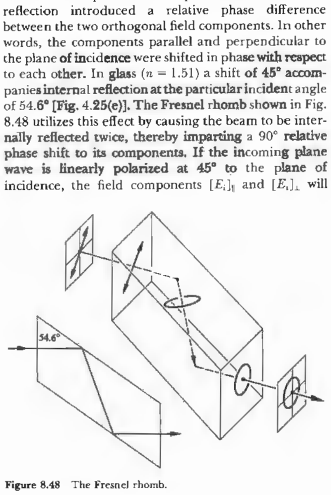


Figure 8.48 The Fresnel rhomb.

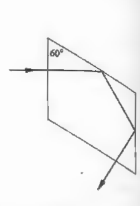


Figure 8.49 The Mooney rhomb.

initially be equal. After the first reflection [illegible] within the glass will be elliptically polarized [illegible] second reflection it will be circular. Since the [illegible] is almost independent of frequency over a large [illegible] the rhomb is essentially an *achromatic* 90° retard[illegible] Mooney rhomb ($n = 1.65$) shown in Fig. 8.49 is [illegible] in principle, although its operating characteri[illegible] different in some respects.

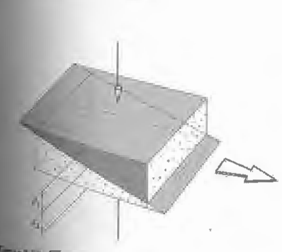
8.7.2 Compensators

A compensator is an optical device that is capable of [illegible] ing a controllable retardance on a wave. Unlike [illegible] plate where $\Delta\varphi$ is fixed, the relative phase di[illegible] arising from a compensator can be varied conti[illegible] Of the many different kinds of compensators, [illegible] consider only two of those that are used most widely. The Babinet compensator, depicted in Fig. 8[illegible] of two independent calcite, or more comm[illegible] wedges whose optic axes are indicated by the lines [illegible] dots in the figure. A ray passing vertically [illegible] through the device at some arbitrary point will [illegible] a thickness of d_1 in the upper wedge and d_2 i[illegible] one. The relative phase difference imparted [illegible] by the first crystal is $2\pi d_1(|n_o - n_e|)/\lambda_0$, and [illegible] second crystal is $-2\pi d_2(|n_o - n_e|)/\lambda_0$. As in the [illegible] prism, which this system closely resembles [illegible] has larger angles and is much thicker, the o-[illegible] in the upper wedge become the e- and o-ray[illegible] tively, in the bottom wedge. The compensa[illegible] (the wedge angle is typically about 2.5°), a[illegible]

[illegible] of the rays is negligible. The total phase [illegible] is then

$$\Delta\varphi = \frac{2\pi}{\lambda_0}(d_1 - d_2)(|n_o - n_e|). \tag{8.33}$$

[illegible]nsator is made of calcite, the e-wave leads [illegible] the upper wedge, and therefore if $d_1 > d_2$, [illegible]onds to the total angle by which the e-[illegible] leads the o-component. The converse is true [illegible] compensator; in other words, if $d_1 > d_2$, [illegible] angle by which the o-wave leads the e-wave. [illegible]nter, where $d_1 = d_2$, the effect of one wedge [illegible] canceled by the other, and $\Delta\varphi = 0$ for all [illegible]hs. The retardation will vary from point to [illegible] the surface, being constant in narrow regions [illegible] the width of the compensator along which the [illegible] thicknesses are themselves constant. If light [illegible] way of a slit parallel to one of these regions [illegible] then move either wedge horizontally with a [illegible] screw, we can get any desired $\Delta\varphi$ to emerge. [illegible] Babinet is positioned at 45° between [illegible] polarizers a series of parallel, equally spaced, [illegible]tinction fringes will appear across the width of [illegible]. These mark the positions where the [illegible] were a full-wave plate. In white light the [illegible] be colored, with the exception of the black [illegible] band ($\Delta\varphi = 0$). The retardance of an



[illegible] The Babinet compensator.

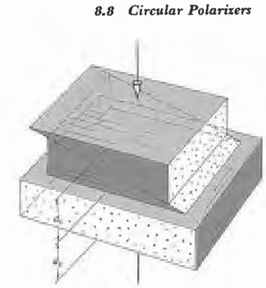


Figure 8.51 The Soleil compensator.

unknown plate can be found by placing it on the compensator and examining the fringe shift it produces.

The Babinet can be modified to produce a uniform retardation over its surface by merely rotating the top wedge 180° about the vertical, so that its thin edge rests on the thin edge of the lower wedge. This configuration will, however, slightly deviate the beam. Another variation of the Babinet, which has the advantage of producing a uniform retardance over its surface and no beam deviation, is the *Soleil compensator* shown in Fig. 8.51. Generally made of quartz (although MgF_2 and CdS are used in the infrared), it consists of two wedges and one plane-parallel slab whose optic axes are oriented as indicated. The quantity d_1 corresponds to the total thickness of both wedges, which is constant for any setting of the positioning micrometer screw.

8.8 CIRCULAR POLARIZERS

Earlier we concluded that linear light whose **E**-field is at 45° to the principal axes of a quarter-wave plate will emerge from that plate circularly polarized. Any series combination of an appropriately oriented linear polarizer and a 90° retarder will therefore perform as a **circular polarizer**. The two elements function completely independently, and whereas one might be birefringent, the other could be of the reflection type. The handedness of the emergent circular light depends on whether the transmission axis of the linear polarizer is at +45° or −45° to the fast axis of the retarder. Either circular state, $\mathscr{L}$ or $\mathscr{R}$, can be generated quite easily. In fact, if the linear polarizer is situated between two retarders, one oriented at +45° and the other at −45°, the combination will be "ambidextrous." In short, it will yield an $\mathscr{R}$-state for light entering from one side and an $\mathscr{L}$-state when the input is on the other side.

CP-HN is the commercial designation for a popular one-piece circular polarizer. It is a laminate of an HN polaroid and a stretched polyvinyl alcohol 90° retarder. The *input side* of such an arrangement is evidently the face of the linear polarizer. If the beam is incident on the *output side* (i.e., on the retarder), it will thereafter pass through the H-sheet and can only emerge linearly polarized.

A circular polarizer can be used as an analyzer to determine the handedness of a wave that is already known to be circular. To see how this might be done, imagine that we have the four elements labeled A, B, C, and D in Fig. 8.52. The first two, A and B, taken together form a circular polarizer, as do C and D. The precise handedness of these polarizers is unimportant now, as long as they are both the same, which is tantamount to saying that the fast axes of the retarders are parallel. Linear light coming from A receives a 90° retardance from B, at which point it is circul[illegible] As [illegible] passes through C another 90° retardance i[illegible] on, resulting once more in a linearly polariz[illegible] wave. In effect, B and C together form a half-wave [illegible] which merely flips the linear light from A through a [illegible] angle of 2θ, in this case 90°. Since the linear w[illegible] C is parallel to the transmission axis of D, [illegible] through it and out of the system. In this simple [illegible] we've actually proved something that is rathe[illegible] If the circular polarizers $A + B$ and $C + D$ [illegible] left-handed, we've shown that *left-circular lig[illegible] a left-circular polarizer from the output side will b[illegible] ted.* Furthermore, it should be apparent, a[illegible] some thought, that right-circular light will [illegible] $\mathscr{P}$-state perpendicular to the transmission axis [illegible] so will be absorbed. The converse is true a[illegible] is, *of the two circular forms, only light in an* [illegible] *pass through a right-circular polarizer having* [illegible] *the output side.*

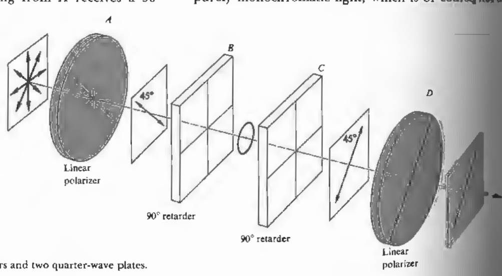


Figure 8.52 Two linear polarizers and two quarter-wave plates.

8.9 POLARIZATION OF POLYCHROMATIC LI[illegible]

8.9.1 Bandwidth and Coherence Time [illegible] Polychromatic Wave

We are again reminded of the fact that by its ve[illegible] purely monochromatic light, which is of course not a [illegible]ality, must be polarized. The two orthogonal [illegible]nts of such a wave have the same frequency, [illegible] a constant amplitude. If the amplitude of [illegible]soidal component varied, it would be [illegible] the presence of other additional frequen[illegible] Fourier-analyzed spectrum. Moreover, the [illegible]ponents have a constant relative phase [illegible] that is, they are coherent. A monochromatic [illegible] is an infinite wavetrain whose properties [illegible] for all time; whether it is in an $\mathscr{R}$-, $\mathscr{L}$-, [illegible]state, the wave is completely polarized.

[illegible] light sources are polychromatic; that is to say, [illegible] radiant energy having a range of frequencies. [illegible] examine what happens on a submicroscopic [illegible] particular attention to the polarization [illegible] emitted wave. Envision an electron-oscillator [illegible] excited into vibration (possibly by a col[illegible] thereupon radiates. Depending on its precise [illegible] oscillator will emit some form of polarized [illegible] in Section 7.2.6, we picture the radiant energy [illegible]gle atom as a wavetrain having a finite spatial extent Δx_c. Assume for the moment that its polarization [illegible] is essentially constant for a duration of the order of the coherence time Δt_c (which, as you recall, corre[illegible] to the temporal extent of the wavetrain, i.e., [illegible]). A typical source generally consists of a large [illegible] of such radiating atoms, which we can envision as oscillating with different phases at some [illegible] frequency $\bar{\nu}$. Suppose then that we examine [illegible] coming from a very small region of the source, [illegible] the emitted rays arriving at a point of observa[illegible] essentially parallel. During a time that is short [illegible]son with the average coherence time, the [illegible] and phases of the wavetrains from the [illegible] atoms will be essentially constant. This means [illegible] were to look toward the source in some direction, we would, at least for an instant, "see" a [illegible] superposition of the waves emitted in that direction. In other words we would "see" a resultant [illegible] a given polarization state. That state would [illegible] an interval less than the coherence time before it changed, but even so it would correspond to a great many oscillations at the frequency $\bar{\nu}$. Clearly, if the bandwidth $\Delta\nu$ is broad, the coherence time ($\Delta t_c \sim 1/\Delta\nu$) will be small, and any polarization state will be short-lived. Evidently *the concepts of polarization and coherence are related in a fundamental way.*

Now consider a wave whose bandwidth is very small in comparison with its mean frequency, in other words, a quasimonochromatic wave. It can be represented by two orthogonal harmonic $\mathscr{P}$-states, as in Eqs. (8.1) and (8.2), but here the amplitudes and epoch angles are functions of time. Furthermore, the frequency and propagation number correspond to the mean values of the spectrum present in the wave, namely, $\bar{\omega}$ and $\bar{k}$. Thus

$$\mathbf{E}_x(t) = \hat{\mathbf{i}} E_{0x}(t) \cos [\bar{k}z - \bar{\omega}t + \varepsilon_x(t)] \qquad (8.34a)$$

and

$$\mathbf{E}_y(t) = \hat{\mathbf{j}} E_{0y}(t) \cos [\bar{k}z - \bar{\omega}t + \varepsilon_y(t)]. \qquad (8.34b)$$

The polarization state, and accordingly $E_{0x}(t)$, $E_{0y}(t)$, $\varepsilon_x(t)$, and $\varepsilon_y(t)$, will vary slowly, remaining essentially constant over a large number of oscillations. Keep in mind that the narrow bandwidth implies a relatively large coherence time. If we watch the wave during a much longer interval, the amplitudes and epoch angles will vary somehow, either independently or in some correlated fashion. If the variations are completely uncorrelated, the polarization state will remain constant only for an interval, small compared to the coherence time. In other words, the ellipse describing the polarization state may change shape, orientation, and handedness. Since, speaking practically, no existing detector could discern any one particular state lasting for so short a time, we would conclude that the wave was unpolarized. Antithetically, if the ratio $E_{0x}(t)/E_{0y}(t)$ were constant even though both terms varied, and if $\varepsilon = \varepsilon_y(t) - \varepsilon_x(t)$ were constant as well, the wave would be polarized. Here the necessity for correlation among these different functions is quite obvious. Yet we can actually impress these conditions on the wave by merely passing it through a polarizer, thereby removing any undesired constituents. The time interval over which the wave thereafter maintains its polarization state is no longer dependent on the bandwidth, because the wave's components have been appropriately correlated. The light could be polychromatic (even white) yet completely polarized. It will behave very much like the idealized monochromatic waves treated in Section 8.1. Between these two extremes of completely polarized and unpolarized light is the condition of partial polarization. In fact, it can be shown that any quasimonochromatic wave can be represented as the sum of a polarized and an unpolarized wave, where the two are independent and either may be zero.

8.9.2 Interference Colors

Insert a crumpled sheet of cellophane between two polaroids illuminated by white light. Alternatively, take an ordinary plastic bag (polyethylene), which shows nothing special between crossed polaroids, and stretch it. That will align its molecules, making it birefringent. Now crumple it up and examine it again. The resulting pattern will be a profusion of multicolored regions, which vary in hue as either polaroid rotates. These **interference colors,** as they are generally called, arise from the wavelength dependence of the retardation. The usual variegated nature of the patterns is due to local variations in thickness, birefringence, or both.

The appearance of interference colors is quite common and can easily be observed in any number of substances. For example, the effect can be seen with a piece of multilayered mica, a chip of ice, a stretched plastic bag, or finely crushed particles of an ordinary white (quartz) pebble. To appreciate [redacted] phenomenon occurs, examine Fig. 8.53. [redacted] of monochromatic linear light is schemati[redacted] passing through some small region of a b[redacted] plate Σ. Over that area the birefringence an[redacted] are both assumed to be constant. The trans[redacted] is generally elliptical. Equivalently, we envis[redacted] emerging from Σ as composed of two ortho[redacted] waves (i.e., the x- and y-components of the [redacted] which have a relative phase difference $\Delta\varphi$, [redacted] by Eq. (8.32). Only the components of these [redacted] bances, which are in the direction of the [redacted] axis of the analyzer, will pass through it and on to the observer. Now these components, which also [redacted] phase difference of $\Delta\varphi$, are coplanar and ca[redacted] fere. When $\Delta\varphi = \pi, 3\pi, 5\pi, \ldots$, they are compl[redacted] out of phase and cancel each other. When [redacted] $0, 2\pi, 4\pi, \ldots$, the waves are in phase and re[redacted] other. Suppose then that the retardance aris[redacted] point P_1 on Σ for blue light ($\lambda_0 = 435$ nm) is [redacted] case blue will be strongly transmitted. It follows from Eq. (8.32) that $\lambda_0\Delta\varphi = 2\pi d(|n_o - n_e|)$ is essentiall[redacted] stant determined by the thickness and the [redacted] gence. At the point in question, therefo[redacted] 1740π for all wavelengths. If we now change [redacted] yellow light ($\lambda_0 = 580$ nm), $\Delta\varphi \approx 3\pi$ and the [redacted] P_1 [redacted]pletely canceled. Under white-light illumination that [redacted]articular point on Σ will seem as if it had [redacted] yellow completely, passing on all the other colors, but none as strongly as blue. Another way of [redacted]is is that the blue light emerging from the [redacted]out P_1 is linear ($\Delta\varphi = 4\pi$) and parallel to the [redacted] transmission axis. In contrast, the yellow light [redacted] ($\Delta\varphi = 3\pi$) and along the extinction axis; the [redacted]rs are elliptical. The region about P_1 behaves [redacted]wave plate for yellow and full-wave plate for [redacted] analyzer were rotated 90°, the yellow would [redacted]ted, and the blue extinguished. By definition [redacted] are said to be complementary when their [redacted] yields white light. Thus when the analyzer [redacted] through 90° it will alternately transmit or [redacted]omplementary colors. In much the same way [redacted]ght be a point P_2 somewhere else on Σ where [redacted]for red ($\lambda_0 = 650$ nm). Then, $\lambda_0\Delta\varphi = 2600\pi$, [redacted] light ($\lambda_0 = 520$ nm) will have a retar[redacted] 5π and be extinguished. Clearly then, if the [redacted] from one region to the next over the [redacted]en, so too will the color of the light transmitted [redacted]analyzer.

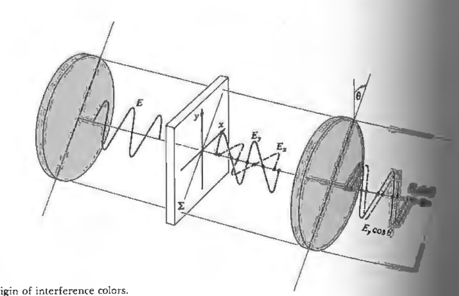


Figure 8.53 The origin of interference colors.

8.10 [redacted]ICAL ACTIVITY

[redacted] which light interacts with material sub[redacted] can yield a great deal of valuable information [redacted]their molecular structures. The process to be [redacted], although of specific interest in the study [redacted]had and is continuing to have far-reaching [redacted] the sciences of chemistry and biology.

In 1811 the French physicist Dominique F. J. Arago [redacted] rather fascinating phenomenon now [redacted]*optical activity.* It was then that he discovered [redacted]plane of vibration of a beam of linear light [redacted] continuous rotation as it propagated along [redacted]axis of a quartz plate (Fig. 8.54). At about the [redacted] Jean Baptiste Biot (1774–1862) saw this same [redacted]le using both the vaporous and liquid forms [redacted]atural substances like turpentine. Any such [redacted] that causes the **E**-field of an incident linear [redacted] to appear to rotate is said to be *optically* [redacted], as Biot found, one must distinguish between right- and left-handed rotation. If while looking in the direction of the source, the plane of vibration appears to have revolved clockwise, the substance is referred to as *dextrorotatory,* or *d-rotatory* (from the Latin *dextro,* meaning right). Alternatively, if **E** appears to have been displaced counterclockwise, the material is *levorotatory,* or *l-rotatory* (from the Latin *levo,* meaning left).

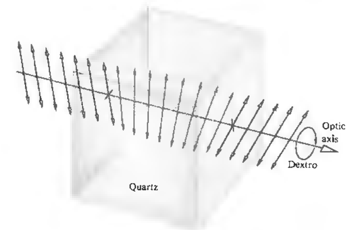


Figure 8.54 Optical activity displayed by quartz.

In 1822 the English astronomer Sir John F. W. Herschel (1792–1871) recognized that *d*-rotatory and *l*-rotatory behavior in quartz actually corresponded to two different crystallographic structures. Although the molecules are identical (SiO_2), crystal quartz can be either right- or left-handed, depending on the arrangement of those molecules. As shown in Fig. 8.55, the

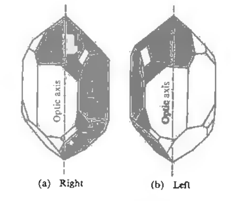


Figure 8.55 Right- and left-handed quartz crystals.

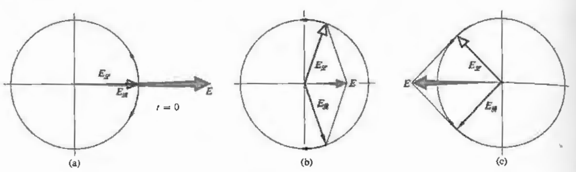


Figure 8.56 The superposition of an $\mathscr{R}$- and an $\mathscr{L}$-state at $z = 0$.

external appearances of these two forms are the same in all respects, except that one is the mirror image of the other; they are said to be *enantiomorphs* of each other. All transparent enantiomorphic substances are optically active. Furthermore, molten quartz and *fused* quartz, neither of which is crystalline, are not optically active. Evidently, in quartz optical activity is associated with the structural distribution of the molecules as a whole. There are many substances, both organic and inorganic (e.g., benzil and $NaBrO_3$, respectively), which, like quartz, exhibit optical activity only in crystal form. In contrast, many naturally occurring organic compounds, such as sugar, tartaric acid, and turpentine, are optically active in solution or in the liquid state. Here the *rotatory power*, as it is often referred to, is evidently an attribute of the individual molecules. There are also more complicated substances for w[illegible] activity is associated with both the molecules [illegible] and their arrangement within the various [illegible] example is rubidium tartrate. A *d*-rotator[illegible] solu[illegible] that compound will change to *l-rotatory* whe[illegible] crys-tallized.

In 1825 Fresnel, without addressin[illegible] the act[illegible] mechanism involved, proposed a simple [illegible] logical description of optical activity. Since [illegible] linear wave can be represented as a superp[illegible] and $\mathscr{L}$-states, he suggested that these tw[illegible] circular light propagate at different spee[illegible] material shows *circular birefringence;* that is[illegible] two indices of refraction, one for $\mathscr{R}$-states [illegible] for $\mathscr{L}$-states ($n_{\mathscr{L}}$). In traversing an optically [illegible] men, the two circular waves would get o[illegible]

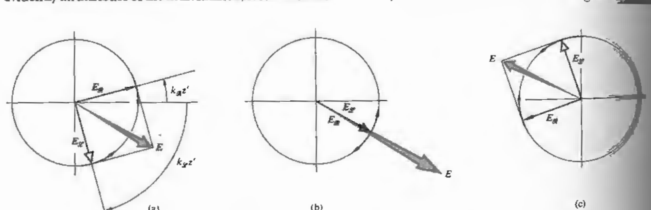


Figure 8.57 The superposition of an $\mathscr{R}$- and an $\mathscr{L}$-state at $z = z'$ ($k_{\mathscr{L}} > k_{\mathscr{R}}$).

[illegible] ultant linear wave would appear to have [illegible] We can see how this is possible analytically by [illegible] to Eqs. (8.8) and (8.9), which described [illegible] matic right- and left-circular light propagat-[illegible] z-direction. It was seen in Eq. (8.10) that the [illegible] two waves is indeed linearly polarized. We [illegible] these expressions slightly in order to remove [illegible] two in the amplitude of Eq. (8.10), in which [illegible]

$$[illegible] \frac{E_0}{2}[\hat{\mathbf{i}} \cos (k_{\mathscr{R}}z - \omega t) + \hat{\mathbf{j}} \sin (k_{\mathscr{R}}z - \omega t)] \quad (8.35a)$$

and

$$[illegible] \frac{E_0}{2}[\hat{\mathbf{i}} \cos (k_{\mathscr{L}}z - \omega t) - \hat{\mathbf{j}} \sin (k_{\mathscr{L}}z - \omega t)] \quad (8.35b)$$

[illegible] the right- and left-handed constituent waves. [illegible] constant, $k_{\mathscr{R}} = k_0 n_{\mathscr{R}}$ and $k_{\mathscr{L}} = k_0 n_{\mathscr{L}}$. The resul-[illegible] ance is given by $\mathbf{E} = \mathbf{E}_{\mathscr{R}} + \mathbf{E}_{\mathscr{L}}$, and after a bit [illegible] ometric manipulation, it becomes

$$[illegible] \cos [(k_{\mathscr{R}} + k_{\mathscr{L}})z/2 - \omega t] [\hat{\mathbf{i}} \cos (k_{\mathscr{R}} - k_{\mathscr{L}})z/2 + [illegible] \sin (k_{\mathscr{R}} - k_{\mathscr{L}})z/2]. \quad (8.36)$$

[illegible] osition where the wave enters the medium [illegible] is linearly polarized along the x-axis, as shown [illegible] 56, that is,

$$\mathbf{E} = E_0 \hat{\mathbf{i}} \cos \omega t. \quad (8.37)$$

Notice [illegible] any point along the path, the two com-[illegible] the same time dependence and are there-[illegible]. This just means that anywhere along the z-axis [illegible] resultant is linearly polarized (Fig. 8.57), although its orientation is certainly a function of z. [illegible] if $n_{\mathscr{R}} > n_{\mathscr{L}}$ or equivalently $k_{\mathscr{R}} > k_{\mathscr{L}}$, **E** will [illegible] nterclockwise, whereas if $k_{\mathscr{L}} > k_{\mathscr{R}}$, the rota-[illegible] ckwise (looking toward the source). Tradi-[illegible] angle β through which **E** rotates is defined [illegible] when it is clockwise. Keeping this sign con-[illegible] mind, it should be clear from Eq. (8.36) that [illegible] oint z makes an angle of $\beta = -(k_{\mathscr{R}} - k_{\mathscr{L}})z/2$ [illegible] to its original orientation. If the medium [illegible] s d, the angle through which the plane of [illegible] tes is then

$$\beta = \frac{\pi d}{\lambda_0}(n_{\mathscr{L}} - n_{\mathscr{R}}), \quad (8.38)$$

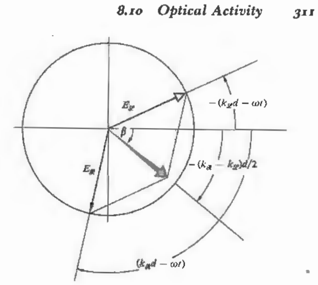


Figure 8.58 The superposition of an $\mathscr{R}$- and an $\mathscr{L}$-state at $z = d$ ($k_{\mathscr{L}} > k_{\mathscr{R}}$, $k_{\mathscr{L}} > k_{\mathscr{R}}$, $\lambda_{\mathscr{L}} < \lambda_{\mathscr{R}}$, and $v_{\mathscr{L}} < v_{\mathscr{R}}$).

where $n_{\mathscr{L}} > n_{\mathscr{R}}$ is *d*-rotatory and $n_{\mathscr{R}} > n_{\mathscr{L}}$ is *l-rotatory* (Fig. 8.58).

Fresnel was actually able to separate the constituent $\mathscr{R}$- and $\mathscr{L}$-states of a linear beam using the composite prism of Fig. 8.59. It consists of a number of right- and left-handed quartz segments cut with their optic axes as shown. The $\mathscr{R}$-state propagates more rapidly in the first prism than in the second and is thus refracted toward the normal to the oblique boundary. The opposite is true for the $\mathscr{L}$-state, and the two circular

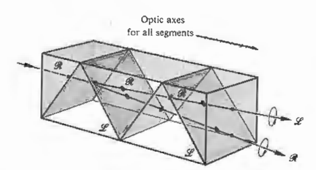


Figure 8.59 The Fresnel composite prism.

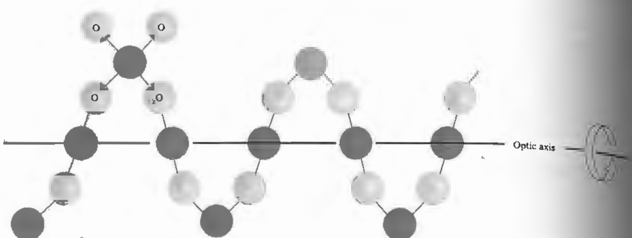


Figure 8.60 Right-handed quartz.

waves increase in angular separation at each interface.

In sodium light the *specific rotatory power*, which is defined as β/d, is found to be 21.7°/mm for quartz. Thus it follows that $|n_{\mathscr{L}} - n_{\mathscr{R}}| = 7.1 \times 10^{-5}$ for light propagating along the optic axis. In that particular direction ordinary double refraction, of course, vanishes. However, with the incident light propagating normal to the optic axis (as is frequently the case in polarizing prisms, wave plates, and compensators), quartz behaves like any optically inactive, positive, uniaxial crystal. There are other birefringent, optically active crystals, both uniaxial and biaxial, such as cinnabar, HgS ($n_o = 2.854$, $n_e = 3.201$), which has a rotatory power of 32.5°/mm. In contrast, the substance $NaClO_3$ is optically active (3.1°/mm) but not birefringent. The rotatory power of liquids, in comparison, is so relatively small that it is usually specified in terms of 10-cm path lengths; for example, in the case of turpentine ($C_{10}H_6$) it is only −37°/10 cm (10°C with $\lambda_0 = 589.3$ nm). The rotatory power of solutions varies with the concentration. This fact is particularly helpful in determining, for example, the amount of sugar present in a urine sample or a commercial sugar syrup.

You can observe optical activity rather easily using colorless corn syrup, the kind available in any grocery store. You won't need much of it, since β/d is roughly +30°/inch. Put about an inch of syrup in a glass container between crossed polaroids and [redacted] a flashlight. The beautiful colors that [redacted] analyzer is rotated arise from the fact that [redacted] of λ_0, an effect known as *rotatory dispersion*. [redacted] to get roughly monochromatic light, you can [redacted] determine the rotatory power of the syrup.*

The first great scientific contribution [redacted] by Lou[redacted] Pasteur (1822–1895) came in 1848 and [redacted] with his doctoral research. He showed that [redacted] which is an optically inactive form of tartaric acid, [redacted] actually composed of a mixture containing [redacted] tities of right- and left-handed constituents [redacted] of this sort, which have the same molecul[redacted] but differ somehow in structure, are called *isom*[redacted] was able to crystallize racemic acid and then, separ[redacted] the two different types of mirror-image cry[redacted] tiomorphs) that resulted. When dissolved [redacted] water, they formed *d*-rotatory and *l*-rotatory [redacted] This implied the existence of molecules tha[redacted] chemically the same, were themselves mirror [redacted] each other; such molecules are now know[redacted] *stereoisomers*. These ideas were the basis for [redacted]

* A gelatin filter works well, but a piece of colored [redacted] also do nicely. Just remember that the cellophane will [redacted] plate (see Section 8.7.1), so don't put it between the [redacted] you align its principal axes appropriately.

[redacted]reochemistry of organic and inorganic [redacted] one is concerned with the three- [redacted]tial distribution of atoms within a given [redacted]

8.10.1 [redacted]seful Model

[redacted]nomenon of optical activity is extremely com- [redacted] and although it can be treated in terms of [redacted]romagnetic theory, it actually requires a [redacted]chanical solution.* Despite this, we will [redacted]mplified model, which will yield a qualita- [redacted]ble, description of the process. Recall that [redacted]ed an optically isotropic medium by a [redacted]eous distribution of isotropic electron-oscil- [redacted] vibrated parallel to the E-field of an incident [redacted]ve. An [redacted]ptically anisotropic medium was similarly [redacted] distribution of anisotropic oscillators that [redacted] at some angle to the driving E-field. We now [redacted] the electrons in optically active substances [redacted] to move along twisting paths that, for [redacted] assumed to be helical. In other words, [redacted] is pictured much as if it were a conduct- [redacted] silicon and oxygen atoms in a quartz [redacted] known to be arranged in either right- or [redacted] spirals about the optic axis, as indicated in [redacted] In the present representation this crystal [redacted]respond to a parallel array of helices. In [redacted], an active sugar solution would be [redacted] to a distribution of randomly oriented [redacted]aving the same handedness.† [redacted] might anticipate that the incoming wave [redacted]differently with the specimen, depending on whether it "saw" right- or left-handed helices. Thus we could expect different indices for the $\mathscr{R}$- and $\mathscr{L}$-components of the wave. The detailed treatment of the process that leads to circular birefringence in crystals is by no means simple, but at least the necessary asymmetry is evident. How, then, can a random array of helices, corresponding to a solution, produce optical activity? Let us examine one such molecule in this simplified representation, for example, one whose axis happens to be parallel to the harmonic **E**-field of the electromagnetic wave. That field will drive charges up and down along the length of the molecule, effectively producing a time-varying electric dipole moment $\mathfrak{p}(t)$, parallel to the axis. In addition, we now have a current associated with the spiraling motion of the electrons.

[redacted] "Optical Activity and Molecular Dissymmetry," [redacted] *Phys.* 9, 239 (1968), contains a fairly extensive [redacted] further reading.

[redacted] to these solid and liquid states, there is a third [redacted] of substances, which is rather useful because of its [redacted] properties. It is known as the *mesomorphic* or *liquid* [redacted] crystals are organic compounds that can flow and [redacted] characteristic molecular orientations. In particular [redacted] crystals have a helical structure and therefore exhibit [redacted] rotatory powers, of the order of 40,000°/mm. The [redacted]-like molecular arrangement is considerably smaller [redacted]

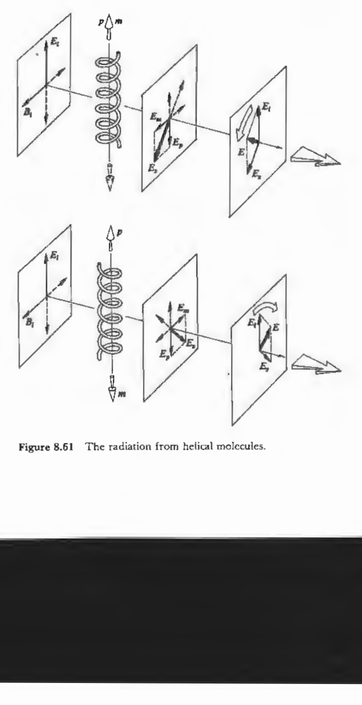


Figure 8.61 The radiation from helical molecules.

This in turn generates an oscillating magnetic dipole moment $m(t)$, which is also along the helix axis (Fig. 8.61). In contrast, if the molecule were parallel to the **B**-field of the wave, there would be a time-varying flux and thus an induced electron current circulating around the molecule. This would again yield oscillating axial electric and magnetic dipole moments. In either case *$p(t)$ and $m(t)$ will be parallel or antiparallel to each other depending on the sense of the particular molecular helix.* Clearly, energy has been removed from the field, and both oscillating dipoles will scatter (i.e., reradiate) electromagnetic waves. The electric field $\mathbf{E}_p$ emitted in a given direction by an electric dipole is perpendicular to the electric field $\mathbf{E}_m$ emitted by a magnetic dipole. Accordingly, the sum of these, which is the resultant field $\mathbf{E}_s$ scattered by a helix, will not be parallel to the incident field $\mathbf{E}_i$ along the direction of propagation (the same is of course true for the magnetic fields). The plane of vibration of the resultant transmitted light $(\mathbf{E}_s + \mathbf{E}_i)$ will thus be rotated in a direction determined by the sense of the helix. The amount of the rotation will vary with the orientation of each molecule, but it will always be in the same direction for helices of the same sense.

Although this discussion of optically active molecules as helical conductors is admittedly superficial, the analogy is well worth keeping in mind. In fact, if we direct a linear 3-cm microwave beam onto a box filled with a large number of identical copper helices (e.g., 1 cm long by 0.5 cm in diameter and insulated from each other), the transmitted wave will undergo a rotation of its plane of vibration.*

8.10.2 Optically Active Biological Substances

Before moving on to other things, we should mention a few of what are probably the most fascinating observations associated with optical activity, namely, those in the field of biology. Whenever organic molecules are synthesized in the laboratory, an equal number of *d*- and *l*-isomers are produced, with the effect that the compound is optically inactive. One migh[illegible] that if they exist at all, equal amounts of *d*[illegible] stereoisomers will be found in natural[illegible] stances. This is by no means the case. Natu[illegible] sugar (sucrose, $C_{12}H_{22}O_{11}$), no matter where it is [illegible] whether extracted from sugar cane or su[illegible] always *d*-rotatory. Moreover, the simple su[illegible] or *d*-glucose ($C_6H_{12}O_6$), which as its na[illegible] *d*-rotatory, is the most important carbohy[illegible] human metabolism. Evidently, living thi[illegible] can somehow distinguish between optical isomer[illegible]

All proteins are fabricated of compounds [illegible] *amino acids.* These in turn are combinations o[illegible] hydrogen, oxygen, and nitrogen. There are [illegible] amino acids, and all of them (with the exceptio[illegible] the simplest one, glycine, which is not enantiomo[illegible] generally *l*-rotatory. This means that if we break up [illegible] protein molecule, whether it comes from an [illegible] eggplant, a beetle or a Beatle, the constitu[illegible] amino acids will be *l*-rotatory. One important ex[illegible] group of antibiotics, such as penicillin, which [illegible] some dextro amino acids. In fact, this may well a[illegible] for the toxic effect penicillin has on bacteria[illegible]

It is intriguing to speculate about the possi[illegible] of life on this and other planets. For exampl[illegible] on Earth originally consist of both mirror-[illegible] Five amino acids were found in a meteorite [illegible] Victoria, Australia, on September 28, [illegible] has revealed the existence of roughly equal [illegible] the optically right- and left-handed forms. [illegible] marked contrast to the overwhelming pred[illegible] the left-handed form found in terrestrial rocks. [illegible] implications are many and marvelous.*

8.11 INDUCED OPTICAL EFFECTS—OPTI[illegible] MODULATORS

There are a number of different physical effe[illegible] ing polarized light that all share the single [illegible] feature of somehow being externally indu[illegible] In [illegible] instances one exerts an external influe[illegible]

* I. Tinoco and M. P. Freeman, "The Optical Activity of Oriented Copper Helices," *J. Phys. Chem.* **61**, 1196 (1957).

* See *Physics Today*, Feb. 1971, p. 17, for additional di[illegible] references for further reading.

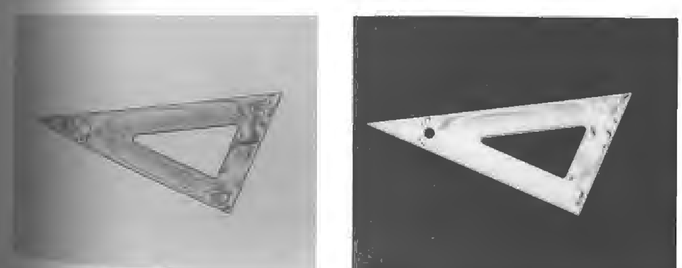
[illegible]rce, a magnetic or electric field) on the [illegible], thereby changing the manner in which [illegible] light.

8.11.1 [illegible]oelasticity

[illegible] David Brewster discovered that normally [illegible]otropic substances could be made optically [illegible] the application of mechanical stress. The [illegible] is variously known as ***mechanical birefrin-*** [illegible]**lasticity**, or *stress birefringence.* Under com[illegible] tension the material takes on the properties [illegible] a negative or positive uniaxial crystal, respectively. [illegible] the effective optic axis is in the direction [illegible] stress, and the induced birefringence is proportional to the stress. Clearly then, if the stress is not uniform over the sample, neither is the birefringence [illegible] imposed on a transmitted wave [Eq. (8.32)].

[illegible]elasticity serves as the basis of a technique for [illegible] the stresses in both transparent and opaque [illegible] structures (Fig. 8.62). Improperly annealed [illegible]y mounted glass, whether serving as an automobile windshield or a telescope lens, will develop internal stresses that can easily be detected. Information concerning the surface strain on opaque objects can be obtained by bonding photoelastic coatings to the parts under study. More commonly, a transparent scale model of the part is made out of a material *optically sensitive to stress*, such as epoxy, glyptol, or modified polyester resins. The model is then subjected to the forces that the actual component would experience in use. Since the birefringence varies from point to point over the surface of the model, when it is placed between crossed polarizers, a complicated variegated fringe pattern will reveal the internal stresses. Examine almost any piece of clear plastic or even a block of unflavored gelatin between two polaroids; try stressing it further and watch the pattern change accordingly (Fig. 8.63).

The retardance at any point on the sample is proportional to the *principal stress difference;* that is, $(\sigma_1 - \sigma_2)$, where the sigmas are the orthogonal principal stresses. For example, if the sample were a plate under vertical tension, σ_1 would be the maximum principal stress in the vertical direction and σ_2 would be the minimum principal stress, in this case zero, horizontally. In more complicated situations, the principal stresses, as well as



[illegible] 8.62 A clear plastic triangle between polaroids. (Photo by E.H.)

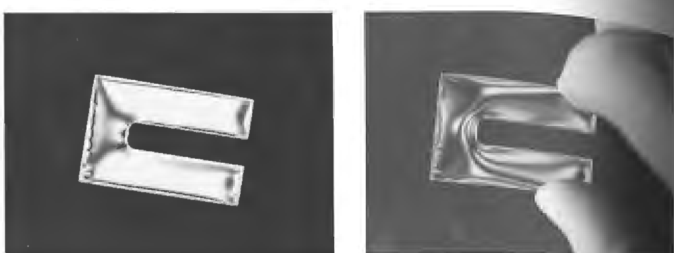


Figure 8.63 A stressed piece of clear plastic between polaroids. (Photo by E.H.)

their differences, will vary from one region to the next. Under white-light illumination, the loci of all points on the specimen for which $(\sigma_1 - \sigma_2)$ is constant are known as *isochromatic regions*, and each such region corresponds to a particular color. Superimposed on these colored fringes will be a separate system of black bands. At any point where the E-field of the incident linear light is parallel to either local principal stress axis, the wave will pass through the sample unaffected, regardless of wavelength. With crossed polarizers, that light will be absorbed by the analyzer, yielding a black region known as an *isoclinic* band (Problem 8.35). In addition to being beautiful to look at, the fringes also provide both a qualitative map of the stress pattern and a basis for quantitative calculations.

8.11.2 The Faraday Effect

Michael Faraday in 1845 discovered that the manner in which light propagated through a material medium could be influenced by the application of an external magnetic field. In particular, he found that the plane of vibration of linear light incident on a piece of glass rotated when a strong magnetic field was applied in the propagation direction. The **Faraday** or **magneto-optic effect** was one of the earliest indications of the interrelationship between electromagnetism [redacted] Although it is reminiscent of *optical activity* [redacted] we shall see, an important distinction [redacted] effects.

The angle β (measured in minutes of arc) [redacted] which the plane of vibration rotates is given by the empirically determined expression

$$\beta = \mathcal{V}Bd, \qquad (8.3?)$$

where B is the static magnetic flux [redacted] gauss), d is the length of medium [redacted] $\mathcal{V}$ is a factor of proportionality known [redacted] *constant*. The Verdet constant for a [redacted] varies with both frequency (dropping [redacted] decreases) and temperature. It is [redacted] of 10^{-5} min of arc $gauss^{-1}$ cm^{-1} for gases [redacted] of arc $gauss^{-1}$ cm^{-1} for solids and [redacted] 8.2). You can get a better feeling for the [redacted] these numbers by imagining, for [redacted] sample of H_2O in the moderately large [redacted] (the Earth's field is about one half [redacted] ticular case, a rotation of 2° 11′ would result [redacted] 0.0131.

By convention, *a positive Verdet* [redacted] *a (diamagnetic) material for which the* [redacted] *l-rotatory when the light moves parallel to the* [redacted] *and d-rotatory when it propagates* [redacted]

[redacted] reversal of handedness occurs in the case [redacted] optical activity. For a convenient mnemonic, [redacted] B-field to be generated by a solenoidal coil [redacted] sample. The plane of vibration, when [redacted] in the same direction as the current [redacted] of the beam's propagation direction [redacted] its axis. The effect can, accordingly, be [redacted] by reflecting the light back and forth a few [redacted] the sample.

[redacted] treatment of the Faraday effect in[redacted] theory of dispersion, [redacted] of B on the atomic or molecular [redacted] levels. It will suffice here merely to outline the [redacted] argument for nonmagnetic materials. [redacted] light to be circular and monochro[redacted] bound electron will take on a [redacted] orbit being driven by the rotating [redacted] wave (the effect of the wave's **B**-field is [redacted] introduction of a large constant applied [redacted] field perpendicular to the plane of the orbit [redacted] in a radial force F_M on the electron. That [redacted] toward or away from the circle's [redacted] on the handedness of the light and [redacted] of the constant **B**-field. The total radial [redacted] the elastic restoring force) can therefore [redacted] values and so too can the radius of [redacted], for a given magnetic field there [redacted] values of the electric dipole moment, [redacted], and the permittivity, as well as two values of the index of refraction, $n_{\mathcal{R}}$ and $n_{\mathcal{L}}$. The [redacted] then proceed in precisely the same fash[redacted] Fresnel's treatment of optical activity. As

Table 8.2 [redacted] constants for some selected substances.

[redacted]	Temperature (°C)	$\mathcal{V}$ (min of arc $gauss^{-1}$ cm^{-1})
[redacted]	18	0.0317
[redacted]	20	0.0131
[redacted]	16	0.0359
[redacted]	20	0.0166
[redacted]	26	−0.00058
[redacted]	0	6.27×10^{-6}
[redacted]	0	9.39×10^{-6}

[redacted] 760 mm Hg.
[redacted] are given in the usual handbooks.

before, one speaks of two normal modes of propagation of electromagnetic waves through the medium, the $\mathcal{R}$- and $\mathcal{L}$-states.

For ferromagnetic substances things are somewhat more complicated. In the case of a magnetized material β is proportional to the component of the magnetization in the direction of propagation rather than the component of the applied dc field.

There are a number of practical applications of the Faraday effect. It can be used to analyze mixtures of hydrocarbons, since each constituent has a characteristic magnetic rotation. Moreover, when utilized in spectroscopic studies it yields information about the properties of energy states above the ground level. In recent times the Faraday effect has been put to even more exciting and promising uses. Since the advent of the laser in the early 1960s, a tremendous effort has been made to utilize the enormous potential of laser light as a communications medium (see Section 7.2.6). An essential component of any such system is the *modulator*, whose function it is to impress information on the beam. Such a device must have the capability of somehow varying the lightwave at high speeds and in a controlled fashion. It might, for example, alter the wave's amplitude, polarization, propagation direction, phase, or frequency in a manner related to the signal that is to be transmitted. The Faraday effect provides one possible basis for such a modulator. Clearly, if a device of this sort is to function efficiently, each unit length of the medium must absorb as little light as possible while imparting as large a rotation to the beam as possible. To this end, a number of rather exotic ferromagnetic materials have been studied. An infrared modulator of this sort was constructed by R. C. LeCraw. It utilizes the synthetic magnetic crystal yttrium-iron garnet (YIG), to which has been added a quantity of gallium. YIG has a structure similar to that of natural gem garnets. The device is depicted schematically in Fig. 8.64. A linear infrared laser beam enters the crystal from the left. A transverse dc magnetic field saturates the magnetization of the YIG crystal in that direction. The total magnetization vector (arising from the constant field and the field of the coil) can vary in direction, being tilted toward the axis of the crystal by an amount proportional to the modulating current in the coil. Since the Faraday rotation depends on the axial component of the magnetization, the coil current controls β. The analyzer then converts this polarization modulation to amplitude modulation by way of Malus's law [Eq. (8.24)]. In short, the signal to be transmitted is introduced across the coil as a modulating voltage, and the emerging laser beam carries that information in the form of amplitude variations.

There are actually several other magneto-optic effects. We shall consider only two of these, and rather succinctly at that. The *Voigt* and *Cotton–Mouton effects* both arise when a constant magnetic field is applied to a transparent medium perpendicular to the direction of propagation of the incident light beam. The former occurs in vapors, whereas the latter, which is considerably stronger, occurs in liquids. In either case the medium displays birefringence similar to that of a uniaxial crystal whose optic axis is in the direction of the dc magnetic field, that is, normal to the light beam [Eq. (8.32)]. The two indices of refraction now correspond to the situations in which the plane of vibration of the wave is either normal or parallel to the constant magnetic field. Their difference Δn (i.e., the birefringence) is proportional to the square of the applied magnetic field. It arises in liquids from an aligning of the optically and magnetically anisotropic molecules of the medium with that field. If the incoming light propagates at some angle to the static field [redacted] $\pi/2$, the Faraday and Cotton–Mouton [redacted] currently, with the former generally [redacted] larger of the two. The Cotton–Mouton is [redacted] analogue of the Kerr electro-optic effec[redacted] sidered next.

8.11.3 The Kerr and Pockels Effects

The first electro-optic effect was discove[redacted] tish physicist John Kerr (1824–1907) in [redacted] that an isotropic transparent substance [redacted] fringent when placed in an electric field E[redacted] takes on the characteristics of a uniaxial [redacted] optic axis corresponds to the direction of the [redacted] field. The two indices, $n_\parallel$ and $n_\perp$, are associat[redacted] the two orientations of the plane of vibratio[redacted] wave, namely, parallel and perpendicular [redacted] electric field, respectively. Their differe[redacted] birefringence, and it is found to be

$$\Delta n = \lambda_0 K E^2,$$

where K is the *Kerr constant.* When K is [illegible] most often is, Δn, which can be thought of as [illegible] is positive, and the substance behaves like [redacted] uniaxial crystal. Values of the Kerr constant [redacted]

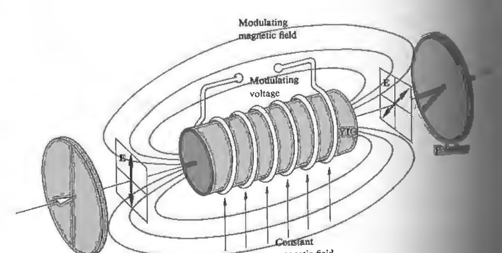


Figure 8.64 A Faraday effect modulator.

[illegible] Kerr constants for some selected liquids (20°C, λ_0 = [illegible]

Substance		K (in units of 10^{-7} cm statvolt^{-2})
[illegible]	C_6H_6	0.6
[illegible]	CS_2	3.2
[illegible]	$CHCl_3$	−3.5
[illegible]	H_2O	4.7
[illegible]	$C_5H_7NO_2$	123
[illegible]	$C_6H_5NO_2$	220

[illegible] in electrostatic units, so that one must [redacted] enter E in Eq. (8.40) in statvolts per cm [redacted] 300 V). Observe that, as with the Cotton– [redacted] *the Kerr effect is proportional to the square* [redacted] *often referred to as the quadratic electro-optic* [redacted] nomenon in liquids is attributed to a [redacted] ent of anisotropic molecules by the E- [redacted] the situation is considerably more complicated.

[redacted] depicts an arrangement known as a Kerr [redacted] tical modulator. It consists of a glass cell [redacted] electrodes, which is filled with a polar [redacted] *cell,* as it is called, is positioned between [redacted] polarizers whose transmission axes are at 45° t[redacted] applied E-field. With zero voltage across pla[redacted] no light will be transmitted; the shutter is losed. [redacted] application of a modulating voltage generates a field, causing the cell to function as a variable wave plate and thus opening the shutter proportionately. The great value of such a device lies in the fact [redacted] ond effectively to frequencies roughly as [redacted] Kerr cells, usually containing nitroben- [redacted] bon disulfide, have been used for a number years [redacted] a variety of applications. They serve as [illegible] [redacted] gh-speed photography and as light-beam ppers [redacted] replace rotating toothed wheels. As such, y have been utilized in measurements of the speed of light. Kerr cells are also extensively used as Q-itches [redacted] Chapter 14) in pulsed laser systems.

If the [redacted] functioning as the electrodes have an [illegible] ive [redacted] of ℓ cm and are separated by a distance [illegible] is given by

$$\Delta\varphi = 2\pi K \ell V^2/d^2, \qquad (8.41)$$

where V is the applied voltage. Thus a nitrobenzene cell in which d is one cm and ℓ is several cm will require a rather large voltage, roughly 3×10^4 V, in order to respond as a half-wave plate. This is a characteristic quantity known as the ***half-wave voltage,*** $V_{\lambda/2}$. Another drawback is that nitrobenzene is both poisonous and explosive. Transparent solid substances, such as the mixed crystal potassium tantalate niobate ($KTa_{0.65}Nb_{0.35}O_3$), KTN for short, or barium titanate ($BaTiO_3$), which show a Kerr effect, are therefore of interest as electro-optical modulators.

There is another very important electro-optical effect known as the ***Pockels effect,*** after the German physicist Friedrich Carl Alwin Pockels (1865–1913), who studied it extensively in 1893. It is a linear electro-optical effect, inasmuch as the induced birefringence is proportional to the first power of the applied **E**-field and therefore the applied voltage. The Pockels effect exists only in certain crystals that lack a center of symmetry; in other words, crystals having no central point through which every atom can be reflected into an identical atom. There are 32 crystal symmetry classes, 20 of which may show the Pockels effect. Incidentally, these same 20 classes are also piezoelectric. Thus, many crystals and all liquids are excluded from displaying a linear electro-optic effect.

The first practical Pockels cell, which could perform as a shutter or modulator, was not made until the 1940s, when suitable crystals were finally developed. The

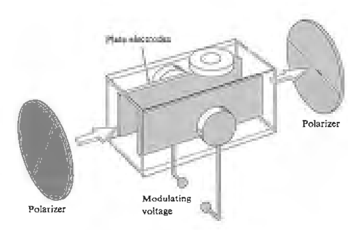


Figure 8.65 A Kerr cell.

operating principle for such a device is one we've already discussed. In brief, the birefringence is varied electronically by means of a controlled applied electric field. The retardance can be altered as desired, thereby changing the state of polarization of the incident linear wave. In this way, the system functions as a polarization modulator. Early devices were made of ammonium dihydrogen phosphate ($NH_4H_2PO_4$), or ADP, and potassium dihydrogen phosphate (KH_2PO_4), known as KDP; both are still widely in use. A great improvement was provided by the introduction of single crystals of potassium dideuterium phosphate (KD_2PO_4), or KD*P, which yields the same retardation with voltages less than half of those needed for KDP. This process of infusing crystals with deuterium is accomplished by growing them in a solution of heavy water. Today cells made with KD*P or CD*A (cesium dideuterium arsenate) are available commercially. Tremendous effort has gone into research on electro-optical crystals. The development of these materials is continually adding exotic names to the jargon of the new technology, such as lithium tantalate, rubidium dihydrogen arsenate, lithium niobate, barium titanate, and barium sodium niobate, to mention only a few.

A *Pockels cell* is simply an appropriate noncentrosymmetric, oriented, single crystal immersed in a controllable electric field. Such devices can usually be operated

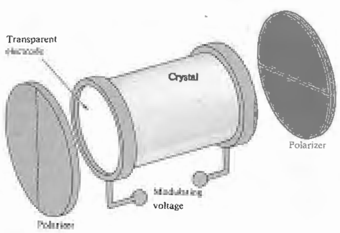


Figure 8.66 A Pockels cell.

at fairly low voltages (roughly 5 to 10 times less than that of an equivalent Kerr cell); they are linear, and of course there is no problem with toxic liquids. The response time of KDP is quite short, typically less than 10 ns, and it can modulate a light beam at up to about 25 GHz (i.e., 25×10^9 Hz). There are two common configurations, referred to as *transverse* and *longitudinal*, depending on whether the applied **E**-field is perpendicular or parallel to the direction of propagation, respectively. The longitudinal type is illustrated, in its most basic form, in Fig. 8.66. Since the beam traverses the electrodes, these are usually made of transparent metal-oxide coatings (e.g., SnO, InO, or CdO), thin metal films, grids, or rings. The crystal itself is generally uniaxial in the absence of an applied field, and it is aligned such that its optic axis is along the beam's propagation direction. For such an arrangement the retardance is given by

$$\Delta\varphi = 2\pi n_o^3 r_{63} V/\lambda_0, \tag{8.42}$$

where r_{63} is the *electro-optic constant* in m/V, n_o is the *ordinary* index of refraction, V is the potential difference in volts, and λ_0 is the vacuum wavelength in meters.* Since the crystals are anisotropic, their properties vary in different directions, and they must be described by a group of terms referred to collectively as the second-rank electro-optic tensor r_{ij}. Fortunately, we need only concern ourselves here with one of its components, namely, r_{63}, values of which are given in Table 8.4. The half-wave voltage corresponds to a value of $\Delta\varphi = \pi$, in which case

$$\Delta\varphi = \pi \frac{V}{V_{\lambda/2}} \tag{8.43}$$

and from Eq. (8.42)

$$V_{\lambda/2} = \frac{\lambda_0}{2n_o^3 r_{63}}. \tag{8.44}$$

As an example, for KDP, $r_{63} = 10.6 \times 10^{-12}$ m/V, $n_o \approx 1.51$, and we obtain $V_{\lambda/2} \approx 7.6 \times 10^3$ V at $\lambda_0 = 546.1$ nm.

* This expression, along with the appropriate one for the transverse mode, is derived rather nicely in A. Yariv, *Quantum Electronics*. Even so, the treatment is sophisticated and not recommended for casual reading.

Table 8.4 Electro-optic constants (room temperature, $\lambda_0 = 546.1$ nm).

Material	r_{63} (units of 10^{-12} m/V)	n_o (approx.)	$V_{\lambda/2}$ (in kV)
ADP ($NH_4H_2PO_4$)	8.5	1.52	9.2
KDP (KH_2PO_4)	10.6	1.51	7.6
KDA (KH_2AsO_4)	~13.0	1.57	~6.2
KD*P (KD_2PO_4)	~23.3	1.52	~3.4

Pockels cells have been used as ultra-fast shutters, as switches for lasers, and dc to 30-GHz light modulators. They are also being applied in a wide range of electro-optical systems, for example, data processing and display techniques.†

8.12 A MATHEMATICAL DESCRIPTION OF POLARIZATION

Thus far we have considered polarized light in terms of the electric field component of the wave. The most general representation was, of course, that of elliptical light. There we envisioned the endpoint of the vector **E** continuously sweeping along the path of an ellipse having a particular shape—the circle and line being special cases. The period over which the ellipse was traversed equaled that of the lightwave (i.e., roughly 10^{-15} s) and was thus far too short to be detected. In contrast, measurements made in practice are generally averages over comparatively long time intervals. Clearly, it would be advantageous to formulate an alternative description of polarization in terms of convenient observables, namely irradiances. Our motives are far more than the ever-present combination of aesthetics and pedagogy. The formalism to be considered has far-reaching significance in other areas of study, for example, particle physics (the photon is, after all an elementary particle) and quantum mechanics. It serves in some respects to link the classical and quantum-mechanical pictures. But even more demanding of our present attention are the considerable practical advantages to be gleaned from this alternative description. We shall evolve an elegant procedure for predicting the effects of complex systems of polarizing elements on the ultimate state of an emergent wave. The mathematics, written in the compressed form of matrices, will require only the simplest manipulation of those matrices. The complicated logic associated with phase retardations, relative orientations, and so forth, for a tandem series of wave plates and polarizers is almost all built in. One need only select appropriate matrices from a chart and drop them into the mathematical mill.

8.12.1 The Stokes Parameters

The modern representation of polarized light actually had its origins in 1852 in the work of G. G. Stokes. He introduced four quantities that are functions only of observables of the electromagnetic wave and are now known as the **Stokes parameters.*** The polarization state of a beam of light (either natural or totally or partially polarized) can be described in terms of these quantities. We will first define the parameters operationally and then relate them to electromagnetic theory. Imagine that we have a set of four filters, each of which, under *natural* illumination, will transmit half the incident light, the other half being discarded. The choice is not a unique one, and a number of equivalent possibilities exist. Suppose then that the first filter is simply isotropic, passing all states equally, whereas the second and third are linear polarizers whose transmission axes are horizontal and at +45° (diagonal along the first and third quadrants), respectively. The last filter is a circular polarizer opaque to $\mathscr{L}$-states. Each of these four filters is positioned alone in the path of the beam under

† The reader interested in light modulation in general should consult D. F. Nelson, "The Modulation of Laser Light," *Scientific American* (June 1968). For some of the practical details see R. S. Ploss, "A Review of Electro-Optics Materials, Methods and Uses," *Optical Spectra* (Jan./Feb. 1969), or R. Goldstein, "Pockels Cell Primer," *Laser Focus Magazine* (Feb. 1968), both of which contain useful bibliographies.

* Much of the material in this section is treated more extensively in Shurcliff's *Polarized Light: Production and Use*, which is something of a classic on the subject. You might also look at M. J. Walker, "Matrix Calculus and the Stokes Parameters of Polarized Radiation," *Am. J. Phys.* **22**, 170 (1954), and W. Bickel and W. Bailey, "Stokes Vectors, Mueller Matrices, and Polarized Scattered Light," *Am. J. Phys.* **53**, 468 (1985).

investigation, and the transmitted irradiances I_0, I_1, I_2, I_3 are measured with a type of meter that is insensitive to polarization (not all of them are). The operational definition of the Stokes parameters is then given by the relations

$$\mathcal{S}_0 = 2I_0 \qquad (8.45a)$$

$$\mathcal{S}_1 = 2I_1 - 2I_0 \qquad (8.45b)$$

$$\mathcal{S}_2 = 2I_2 - 2I_0 \qquad (8.45c)$$

$$\mathcal{S}_3 = 2I_3 - 2I_0. \qquad (8.45d)$$

Notice that $\mathcal{S}_0$ is simply the incident irradiance, and $\mathcal{S}_1$, $\mathcal{S}_2$, and $\mathcal{S}_3$ specify the state of polarization. Thus $\mathcal{S}_1$ reflects a tendency for the polarization to resemble either a horizontal $\mathcal{P}$-state (whereupon $\mathcal{S}_1 > 0$) or a vertical one (in which case $\mathcal{S}_1 < 0$). When the beam displays no preferential orientation with respect to these axes ($\mathcal{S}_1 = 0$) it may be elliptical at ±45°, circular, or unpolarized. Similarly $\mathcal{S}_2$ implies a tendency for the light to resemble a $\mathcal{P}$-state oriented in the direction of +45° (when $\mathcal{S}_2 > 0$) or in the direction of −45° (when $\mathcal{S}_2 < 0$) or neither ($\mathcal{S}_2 = 0$). In quite the same way $\mathcal{S}_3$ reveals a tendency of the beam toward right-handedness ($\mathcal{S}_3 > 0$), left-handedness ($\mathcal{S}_3 < 0$), or neither ($\mathcal{S}_3 = 0$).

Now recall the expressions for quasimonochromatic light,

$$\mathbf{E}_x(t) = \hat{\mathbf{i}} E_{0x}(t) \cos [(\bar{k}z - \bar{\omega}t) + \varepsilon_x(t)] \qquad [8.34(a)]$$

and

$$\mathbf{E}_y(t) = \hat{\mathbf{j}} E_{0y}(t) \cos [(\bar{k}z - \bar{\omega}t) + \varepsilon_y(t)], \qquad [8.34(b)]$$

where $\mathbf{E}(t) = \mathbf{E}_x(t) + \mathbf{E}_y(t)$. Using these in a fairly straightforward way, we can recast the Stokes parameters* as

$$\mathcal{S}_0 = \langle E_{0x}^2 \rangle + \langle E_{0y}^2 \rangle \qquad (8.46a)$$

$$\mathcal{S}_1 = \langle E_{0x}^2 \rangle - \langle E_{0y}^2 \rangle \qquad (8.46b)$$

$$\mathcal{S}_2 = \langle 2E_{0x}E_{0y} \cos \varepsilon \rangle \qquad (8.46c)$$

$$\mathcal{S}_3 = \langle 2E_{0x}E_{0y} \sin \varepsilon \rangle. \qquad (8.46d)$$

Here $\varepsilon = \varepsilon_y - \varepsilon_x$ and we've dropped the constant $\epsilon_0 c/2$, so that the parameters are now *proportional* to irradiances. For the hypothetical case of perfe[illegible] matic light, $E_{0x}(t)$, $E_{0y}(t)$, and $\varepsilon(t)$ are [illegible] dent, and one need only drop the ⟨ [illegible] (8.46) to get the applicable Stokes para[illegible] ingly enough, these same results can [illegible] time averaging Eq. (8.14), which is the ge[illegible] for elliptical light.*

If the beam is unpolarized, $\langle E_{0x}^2 \rangle$ = [illegible] averages to zero, because the amplitude [illegible] always positive. In that case $\mathcal{S}_0 = \langle E_{0x}^2 \rangle + \langle E$[illegible] $\mathcal{S}_2 = \mathcal{S}_3 = 0$. The latter two parameters go to [illegible] both cos ε and sin ε average to zero indep[illegible] the amplitudes. It is often convenient to [illegible] Stokes parameters by dividing each one b[illegible] $\mathcal{S}_0$. This has the effect of using an inciden[illegible] irradiance. The set of parameters ($\mathcal{S}_0, \mathcal{S}$[illegible] *natural light* in the normalized representa[illegible] (1, 0, 0, 0). If the light is horizontally pola[illegible] no vertical component, and the normalized [illegible] are (1, 1, 0, 0). Similarly, for vertically p[illegible] we have (1, −1, 0, 0). Representations of a [illegible] polarization states are listed in Table 8.5 (the [illegible] are displayed vertically for reasons to be di[illegible] Notice that for completely polarized light it [illegible] Eq. (8.46) that

$$\mathcal{S}_0^2 = \mathcal{S}_1^2 + \mathcal{S}_2^2 + \mathcal{S}_3^2. \qquad (8.[illegible])$$

Moreover, for partially polarized light it can be shown that the degree of polarization (8.29) is given by

$$V = (\mathcal{S}_1^2 + \mathcal{S}_2^2 + \mathcal{S}_3^2)^{1/2}/\mathcal{S}_0.$$

Imagine now that we have two quasimonoch[illegible] waves described by $(\mathcal{S}_0', \mathcal{S}_1', \mathcal{S}_2', \mathcal{S}_3')$ and $(\mathcal{S}_0'', \mathcal{S}$[illegible] which are superimposed in some region of [illegible] long as the waves are *incoherent*, any one of the Stokes parameters of the resultant will be the s[illegible] of th[illegible] corresponding parameters of the constitu[illegible] (all [illegible] which are proportional to irradiance). In [illegible] the set of parameters describing the resulta[illegible] $\mathcal{S}_0'', \mathcal{S}_1' + \mathcal{S}_1'', \mathcal{S}_2' + \mathcal{S}_2'', \mathcal{S}_3' + \mathcal{S}_3''$). For example, i[illegible] density vertical $\mathcal{P}$-state (1, −1, 0, 0) is ad[illegible] *incoherent* $\mathcal{L}$-state (see Table 8.5) of flux density [illegible]

* For the details see E. Hecht, "Note on an Operational Definition of the Stokes Parameters," *Am. J. Phys.* 38, 1156 (1970).

* E. Collett, "The Description of Polarization in Classical [illegible] *Am. J. Phys.* 36, 713 (1968).

Table 8.5 [illegible]kes and Jones vectors for some polarization states.

[illegible]larization	Stokes vectors	Jones vectors
[illegible]	$\begin{bmatrix}1\\1\\0\\0\end{bmatrix}$	$\begin{bmatrix}1\\0\end{bmatrix}$
[illegible]	$\begin{bmatrix}1\\-1\\0\\0\end{bmatrix}$	$\begin{bmatrix}0\\1\end{bmatrix}$
[illegible]	$\begin{bmatrix}1\\0\\1\\0\end{bmatrix}$	$\frac{1}{\sqrt{2}}\begin{bmatrix}1\\1\end{bmatrix}$
[illegible] −45°	$\begin{bmatrix}1\\0\\-1\\0\end{bmatrix}$	$\frac{1}{\sqrt{2}}\begin{bmatrix}1\\-1\end{bmatrix}$
[illegible]-state	$\begin{bmatrix}1\\0\\0\\1\end{bmatrix}$	$\frac{1}{\sqrt{2}}\begin{bmatrix}1\\-i\end{bmatrix}$
[illegible]-state	$\begin{bmatrix}1\\0\\0\\-1\end{bmatrix}$	$\frac{1}{\sqrt{2}}\begin{bmatrix}1\\i\end{bmatrix}$

[illegible], −2), the composite wave has parameters [illegible]0, −2). It is an ellipse of flux density 3, more vertical than horizontal ($\mathcal{S}_1 < 0$), left-handed [illegible]), and having a degree of polarization of $\sqrt{5}/3$. [illegible] of Stokes parameters for a given wave can [illegible] as a *vector;* we have already seen how two [illegible]rent) vectors add.* Indeed, it will not be [illegible] of three-dimensional vector, but this sort [illegible]tion is rather widely used in physics to [illegible]ge. More specifically, the parameters [illegible] are arranged in the form of what is called a *column vector*,

$$\mathcal{S} = \begin{bmatrix}\mathcal{S}_0\\ \mathcal{S}_1\\ \mathcal{S}_2\\ \mathcal{S}_3\end{bmatrix}. \qquad (8.49)$$

8.12.2 The Jones Vectors

Another representation of polarized light, which complements that of the Stokes parameters, was invented in 1941 by the American physicist R. Clark Jones. The technique he evolved has the advantages nf being applicable to coherent beams and at the same time being extremely concise. Yet unlike the previous formalism, it is *only applicable to polarized waves.* In that case it would seem that the most natural way to represent the beam would be in terms of the electric vector itself. Written in column form, this *Jones vector* is

$$\mathbf{E} = \begin{bmatrix} E_x(t) \\ E_y(t) \end{bmatrix}, \qquad (8.50)$$

where $E_x(t)$ and $E_y(t)$ are the instantaneous scalar components of $\mathbf{E}$. Obviously, knowing $\mathbf{E}$, we know everything about the polarization state. And if we preserve the phase information, we will be able to handle coherent waves. With this in mind, rewrite Eq. (8.50) as

$$\mathbf{E} = \begin{bmatrix} E_{0x} e^{i\varphi_x} \\ E_{0y} e^{i\varphi_y} \end{bmatrix}, \qquad (8.51)$$

where φ_x and φ_y are the appropriate phases. Horizontal and vertical $\mathcal{P}$-states are thus given by

$$\mathbf{E}_h = \begin{bmatrix} E_{0x} e^{i\varphi_x} \\ 0 \end{bmatrix} \quad \text{and} \quad \mathbf{E}_v = \begin{bmatrix} 0 \\ E_{0y} e^{i\varphi_y} \end{bmatrix}, \qquad (8.52)$$

respectively. The sum of two coherent beams, as with the Stokes vectors, is formed by a sum of the corresponding components. Since $\mathbf{E} = \mathbf{E}_h + \mathbf{E}_v$, when, for example $E_{0x} - E_{0y}$ and $\varphi_x = \varphi_y$, $\mathbf{E}$ is given by

$$\mathbf{E} = \begin{bmatrix} E_{0x} e^{i\varphi_x} \\ E_{0x} e^{i\varphi_x} \end{bmatrix} \qquad (8.53)$$

* [illegible] requirements for a collection of objects to form a [illegible] themselves be vectors in such a space are discussed [illegible], *Introduction to Vector Analysis.*

or, after factoring, by

$$\mathbf{E} = E_{0x}e^{i\varphi_x}\begin{bmatrix}1\\1\end{bmatrix}, \tag{8.54}$$

which is a $\mathscr{P}$-state at +45°. This is the case since the amplitudes are equal and the phase difference is zero. There are many applications in which it is not necessary to know the exact amplitudes and phases. In such instances we can *normalize* the irradiance to unity, thereby forfeiting some information but gaining much simpler expressions. This is done by dividing both elements in the vector by the same scalar (real or complex) quantity, such that the sum of the squares of the components is one. For example, dividing both terms of Eq. (8.53) by $\sqrt{2}\,E_{0x}e^{i\varphi_x}$ leads to

$$\mathbf{E}_{45} = \frac{1}{\sqrt{2}}\begin{bmatrix}1\\1\end{bmatrix}. \tag{8.55}$$

Similarly, in normalized form

$$\mathbf{E}_h = \begin{bmatrix}1\\0\end{bmatrix} \quad \text{and} \quad \mathbf{E}_v = \begin{bmatrix}0\\1\end{bmatrix}. \tag{8.56}$$

Right-circular light has $E_{0x} = E_{0y}$, and the y-component leads the x-component by 90°. Since we are using the form $(kz - \omega t)$, we will have to add $-\pi/2$ to φ_y, thus

$$\mathbf{E}_{\mathscr{R}} = \begin{bmatrix}E_{0x}e^{i\varphi_x}\\E_{0x}e^{i(\varphi_x-\pi/2)}\end{bmatrix}.$$

Dividing both components by $E_{0x}e^{i\varphi_x}$, we have

$$\begin{bmatrix}1\\e^{-i\pi/2}\end{bmatrix} = \begin{bmatrix}1\\-i\end{bmatrix};$$

hence the normalized Jones vector is†

$$\mathbf{E}_{\mathscr{R}} = \frac{1}{\sqrt{2}}\begin{bmatrix}1\\-i\end{bmatrix} \quad \text{and similarly} \quad \mathbf{E}_{\mathscr{L}} = \frac{1}{\sqrt{2}}\begin{bmatrix}1\\i\end{bmatrix}. \tag{8.57}$$

The sum $\mathbf{E}_{\mathscr{R}} + \mathbf{E}_{\mathscr{L}}$ is

$$\frac{1}{\sqrt{2}}\begin{bmatrix}1+1\\-i+i\end{bmatrix} = \frac{2}{\sqrt{2}}\begin{bmatrix}1\\0\end{bmatrix}.$$

† Had we used $(\omega t - kz)$ for the phase, the terms in $\mathbf{E}_{\mathscr{R}}$ would have been interchanged. The present notation, although possibly a bit more difficult to keep straight (e.g., $-\pi/2$ for a phase lead), is more often used in modern works. Be wary when consulting references (e.g., Shurcliff).

This is a horizontal $\mathscr{P}$-state having an [redacted] that of either component, a result in [redacted] our earlier calculation of Eq. (8.10). The [redacted] for elliptical light can be obtained by the [redacted] used to arrive at $\mathbf{E}_{\mathscr{R}}$ and $\mathbf{E}_{\mathscr{L}}$, where now [redacted] be equal to E_{0y}, and the phase difference need not 90°. In essence, for vertical and horizontal [redacted] we need to do is stretch out the circular form into ellipse by multiplying either component by a scalar. Thus

$$\frac{1}{\sqrt{5}}\begin{bmatrix}2\\-i\end{bmatrix}$$

describes one possible form of horizontal [redacted] elliptical light.

Two vectors **A** and **B** are said to be orthogonal when $\mathbf{A}\cdot\mathbf{B} = 0$; similarly two complex vectors are [redacted] when $\mathbf{A}\cdot\mathbf{B}^* = 0$. One refers to two pola[redacted] as being *orthogonal* when their Jones vectors [redacted] orthogonal. For example,

$$\mathbf{E}_{\mathscr{R}}\cdot\mathbf{E}_{\mathscr{L}}^* = \tfrac{1}{2}[(1)(1)^* + (-i)(i)^*] = 0$$

or

$$\mathbf{E}_h\cdot\mathbf{E}_v^* = [(1)(0)^* + (0)(1)^*] = 0,$$

where taking the complex conjugates of [redacted] obviously leaves them unaltered. Any pola[redacted] will have a corresponding orthogonal state [redacted]

$$\mathbf{E}_{\mathscr{R}}\cdot\mathbf{E}_{\mathscr{R}}^* = \mathbf{E}_{\mathscr{L}}\cdot\mathbf{E}_{\mathscr{L}}^* = 1$$

and

$$\mathbf{E}_{\mathscr{R}}\cdot\mathbf{E}_{\mathscr{L}}^* = \mathbf{E}_{\mathscr{L}}\cdot\mathbf{E}_{\mathscr{R}}^* = 0.$$

Such vectors form an *orthonormal set*, as [redacted] As we have seen, any polarization state [redacted] by a linear combination of the vectors [redacted] the orthonormal sets. These same ideas [redacted] able importance in quantum mechanics [redacted] deals with orthonormal wave functions.

8.12.3 The Jones and Mueller Ma[redacted]

Suppose that we have a polarized incident beam represented by its Jones vector $\mathbf{E}_i$, which passe[redacted]

[redacted]ement, emerging as a new vector $\mathbf{E}_t$ corre- the transmitted wave. The optical element [redacted]med $\mathbf{E}_i$ into $\mathbf{E}_t$, a process that can be [redacted]athematically using a 2 × 2 matrix. Recall [redacted] matrix is just an array of numbers that has [redacted]ed addition and multiplication operations. Let [redacted] the transformation matrix of the optical [redacted] question. Then

$$\mathbf{E}_t = \mathscr{A}\mathbf{E}_i, \tag{8.59}$$

where

$$\mathscr{A} = \begin{bmatrix}a_{11} & a_{12}\\a_{21} & a_{22}\end{bmatrix}, \tag{8.60}$$

and the column vectors are to be treated like any other matrices. As a reminder, we write Eq. (8.59) as

$$\begin{bmatrix}E_{tx}\\E_{ty}\end{bmatrix} = \begin{bmatrix}a_{11} & a_{12}\\a_{21} & a_{22}\end{bmatrix}\begin{bmatrix}E_{ix}\\E_{iy}\end{bmatrix}, \tag{8.61}$$

and, upon expanding, we obtain

$$E_{tx} = a_{11}E_{ix} + a_{12}E_{iy},$$

$$E_{ty} = a_{21}E_{ix} + a_{22}E_{iy}.$$

Table 8.6 contains a brief listing of Jones matrices for various optical elements. To appreciate how these are used let's examine a few applications. Suppose that $\mathbf{E}_i$ represents a $\mathscr{P}$-state at +45°, which passes through a [redacted]ave plate whose fast axis is vertical (i.e., in the [redacted]). The polarization state of the emergent wave [redacted]ound as follows, where we drop the constant-amplitude factors for convenience:

$$\begin{bmatrix}1 & 0\\0 & -i\end{bmatrix}\begin{bmatrix}1\\1\end{bmatrix} = \begin{bmatrix}E_{tx}\\E_{ty}\end{bmatrix},$$

and thus

$$\mathbf{E}_t = \begin{bmatrix}1\\-i\end{bmatrix}.$$

The beam, as you well know, is right-circular. If the wave passes through a series of optical elements represented [redacted] matrices $\mathscr{A}_1, \mathscr{A}_2, \ldots, \mathscr{A}_n$, then

$$\mathbf{E}_t = \mathscr{A}_n\cdots\mathscr{A}_2\mathscr{A}_1\mathbf{E}_i.$$

The matrices do not commute; they must be applied in the proper order. The wave leaving the first optical element in the series is $\mathscr{A}_1\mathbf{E}_i$; after passing through the second element, it becomes $\mathscr{A}_2\mathscr{A}_1\mathbf{E}_i$, and so on. To illustrate the process, return to the wave considered above (i.e., a $\mathscr{P}$-state at +45°), but now have it pass through two quarter-wave plates, both with their fast

Table 8.6 Jones and Mueller matrices.

Linear optical element	Jones matrix	Mueller matrix
Horizontal linear polarizer ↔	$\begin{bmatrix}1 & 0\\0 & 0\end{bmatrix}$	$\frac{1}{2}\begin{bmatrix}1 & 1 & 0 & 0\\1 & 1 & 0 & 0\\0 & 0 & 0 & 0\\0 & 0 & 0 & 0\end{bmatrix}$
Vertical linear polarizer ↕	$\begin{bmatrix}0 & 0\\0 & 1\end{bmatrix}$	$\frac{1}{2}\begin{bmatrix}1 & -1 & 0 & 0\\-1 & 1 & 0 & 0\\0 & 0 & 0 & 0\\0 & 0 & 0 & 0\end{bmatrix}$
Linear polarizer at +45° ⤢	$\frac{1}{2}\begin{bmatrix}1 & 1\\1 & 1\end{bmatrix}$	$\frac{1}{2}\begin{bmatrix}1 & 0 & 1 & 0\\0 & 0 & 0 & 0\\1 & 0 & 1 & 0\\0 & 0 & 0 & 0\end{bmatrix}$
Linear polarizer at −45° ⤡	$\frac{1}{2}\begin{bmatrix}1 & -1\\-1 & 1\end{bmatrix}$	$\frac{1}{2}\begin{bmatrix}1 & 0 & -1 & 0\\0 & 0 & 0 & 0\\-1 & 0 & 1 & 0\\0 & 0 & 0 & 0\end{bmatrix}$
Quarter-wave plate, fast axis vertical	$e^{i\pi/4}\begin{bmatrix}1 & 0\\0 & -i\end{bmatrix}$	$\begin{bmatrix}1 & 0 & 0 & 0\\0 & 1 & 0 & 0\\0 & 0 & 0 & -1\\0 & 0 & 1 & 0\end{bmatrix}$
Quarter-wave plate, fast axis horizontal	$e^{i\pi/4}\begin{bmatrix}1 & 0\\0 & i\end{bmatrix}$	$\begin{bmatrix}1 & 0 & 0 & 0\\0 & 1 & 0 & 0\\0 & 0 & 0 & 1\\0 & 0 & -1 & 0\end{bmatrix}$
Homogeneous circular polarizer right ↻	$\frac{1}{2}\begin{bmatrix}1 & i\\-i & 1\end{bmatrix}$	$\frac{1}{2}\begin{bmatrix}1 & 0 & 0 & 1\\0 & 0 & 0 & 0\\0 & 0 & 0 & 0\\1 & 0 & 0 & 1\end{bmatrix}$
Homogeneous circular polarizer left ↺	$\frac{1}{2}\begin{bmatrix}1 & -i\\i & 1\end{bmatrix}$	$\frac{1}{2}\begin{bmatrix}1 & 0 & 0 & -1\\0 & 0 & 0 & 0\\0 & 0 & 0 & 0\\-1 & 0 & 0 & 1\end{bmatrix}$

axes vertical. Thus, again discarding the amplitude factors, we have

$$E_t = \begin{bmatrix} 1 & 0 \\ 0 & -i \end{bmatrix}\begin{bmatrix} 1 & 0 \\ 0 & -i \end{bmatrix}\begin{bmatrix} 1 \\ 1 \end{bmatrix},$$

whereupon

$$E_t = \begin{bmatrix} 1 & 0 \\ 0 & -i \end{bmatrix}\begin{bmatrix} 1 \\ -i \end{bmatrix},$$

and finally

$$E_t = \begin{bmatrix} 1 \\ -1 \end{bmatrix}.$$

The transmitted beam is a $\mathscr{P}$-state at $-45°$, having essentially been flipped through 90° by a half-wave plate. When the same series of optical elements is being used to examine various states it becomes desirable to replace the product $\mathscr{A}_n \cdots \mathscr{A}_2\mathscr{A}_1$ by the single 2×2 *system matrix* obtained by carrying out the multiplication (the order in which it is calculated should be $\mathscr{A}_2\mathscr{A}_1$, then $\mathscr{A}_3\mathscr{A}_2\mathscr{A}_1$, etc.).

In 1943 Hans Mueller, then a professor of physics at the Massachusetts Institute of Technology, devised a matrix method for dealing with the Stokes vectors. Recall that the Stokes vectors have the attribute of being applicable to both polarized and partially polarized light. The Mueller method shares this quality and thus serves to complement the Jones method. The latter, however, can easily deal with coherent waves, whereas the former cannot. The Mueller, 4×4, matrices are applied in much the same way as are the Jones matrices. There is therefore little need to discuss the method at length; a few simple examples, augmented by Table 8.6, should suffice. Imagine that we pass a unit-irradiance unpolarized wave through a linear horizontal polarizer. The Stokes vector of the emerging wave $\mathcal{S}_t$ is

$$\mathcal{S}_t = \frac{1}{2}\begin{bmatrix} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}\begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} \frac{1}{2} \\ \frac{1}{2} \\ 0 \\ 0 \end{bmatrix}.$$

The transmitted wave has an irradiance of $\frac{1}{2}(\mathcal{S}_0 = \frac{1}{2})$ and is linearly polarized horizontally ($\mathcal{S}_1 > 0$). As another example, suppose we have a partially polarized elliptical wave whose Stokes parameters have bee[illegible] to be, say, (4, 2, 0, 3). Its irradiance is 4; it i[illegible] horizontal than vertical ($\mathcal{S}_1 > 0$), it is right-[illegible] 0), and it has a degree of polarization o[illegible] none of the parameters can be larger tha[illegible] value of $\mathcal{S}_3 = 3$ is fairly large, indicating that the ellip[illegible] resembles a circle. If the wave is now mad[illegible] a quarter-wave plate with a vertical fast axis, the[illegible]

$$\mathcal{S}_t = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \end{bmatrix}\begin{bmatrix} 4 \\ 2 \\ 0 \\ 3 \end{bmatrix}$$

and thus

$$\mathcal{S}_t = \begin{bmatrix} 4 \\ 2 \\ -3 \\ 0 \end{bmatrix}.$$

The emergent wave has the same irradiance[illegible] of polarization but is now partially linearly[illegible]

We have only touched on a few of the more[illegible] aspects of the matrix methods. The full [illegible] the subject goes far beyond these introductory remar[illegible]

PROBLEMS

8.1 Describe completely the state of polariza[illegible] of each of the following waves:

a) $\mathbf{E} = \hat{\mathbf{i}}E_0 \cos(kz - \omega t) - \hat{\mathbf{j}}E_0 \cos(kz - \omega t)$
b) $\mathbf{E} = \hat{\mathbf{i}}E_0 \sin 2\pi(z/\lambda - \nu t) - \hat{\mathbf{j}}E_0 \sin 2\pi($[illegible]$ - \nu t)$
c) $\mathbf{E} = \hat{\mathbf{i}}E_0 \sin(\omega t - kz) + \hat{\mathbf{j}}E_0 \sin(\omega t - kz$ [illegible] $\pi/4)$
d) $\mathbf{E} = \hat{\mathbf{i}}E_0 \cos(\omega t - kz) + \hat{\mathbf{j}}E_0 \cos(\omega t - kz$ [illegible] $\pi/2)$

8.2 Consider the disturbance given by the [illegible] $\mathbf{E}(z, t) = [\hat{\mathbf{i}} \cos \omega t + \hat{\mathbf{j}} \cos(\omega t - \pi/2)]E_0 \sin kz$. [illegible] of wave is it? Draw a rough sketch showing[illegible] features.

* One can weave a more elaborate and mathema[illegible] development in terms of something called the cohere[illegible] further, but more advanced, reading, see O'Neill, [illegible] *Statistical Optics*.

8.3 [illegible]tically, show that the superposition of an $\mathscr{R}$- and [illegible]state having different amplitudes will yield [illegible] as shown in Fig. 8.8. What must ε be to [illegible] figure?

8.4 Write an expression for a $\mathscr{P}$-state lightwave of [illegible]ular [illegible]equency ω and amplitude E_0 propagating [illegible] the x-axis with its plane of vibration at an angle [illegible]° to the xy-plane. The disturbance is zero at $t = 0$ [illegible]

8.5* Write an expression for a $\mathscr{P}$-state lightwave of [illegible] [illegible]equency ω and amplitude E_0 propagating along a [illegible]e in the xy-plane at 45° to the x-axis and having its plane of vibration corresponding to the xy-plane. At $t = 0$, $y = 0$, and $x = 0$ the field is zero.

8.6 Write an expression for an $\mathscr{R}$-state lightwave of [illegible]quency ω propagating in the positive x-direction [illegible] that at $t = 0$ and $x = 0$ the **E**-field points in the [illegible]

8.7 [illegible]ght that is initially natural and of flux density [illegible] through two sheets of HN-32 whose trans- [illegible]axes are parallel, what will be the flux density [illegible]merging beam?

8.8* [illegible] will be the irradiance of the emerging beam [illegible]zer of the previous problem is rotated 30°?

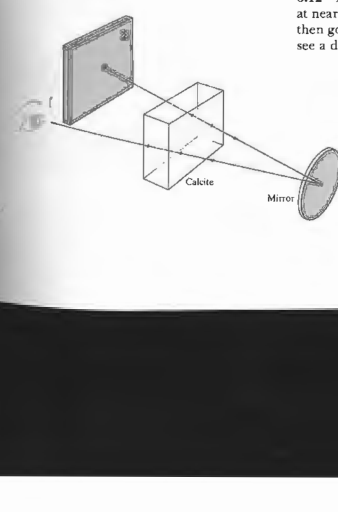


Figure 8.67

8.9* Suppose that we have a pair of crossed polarizers with transmission axes vertical and horizontal. The beam emerging from the first polarizer has flux density I_1, and of course no light passes through the analyzer (i.e., $I_2 = 0$). Now insert a perfect linear polarizer (HN-50) with its transmission axis at 45° to the vertical between the two elements—compute I_2. Think about the motion of the electrons that are radiating in each polarizer.

8.10* Imagine that you have two identical perfect linear polarizers and a source of natural light. Place them one behind the other and position their transmission axes at 0° and 50°, respectively. Now insert between them a third linear polarizer with its transmission axis at 25°. If 1000 W/m² of light is incident, how much will emerge with and without the middle polarizer in place?

8.11 Suppose that an ideal polarizer is rotated at a rate ω between a similar pair of stationary crossed polarizers. Show that the emergent flux density will be modulated at four times the rotational frequency. In other words, show that

$$I = \frac{I_1}{8}(1 - \cos 4\omega t),$$

where I_1 is the flux density emerging from the first polarizer and I is the final flux density.

8.12 Figure 8.67 shows a ray traversing a calcite crystal at nearly normal incidence, bouncing off a mirror, and then going through the crystal again. Will the observer see a double image of the spot on Σ?

8.13* A pencil mark on a sheet of paper is covered by a calcite crystal. With illumination from above, isn't the light impinging on the paper already polarized, having passed through the crystal? Why then do we see two images? Test your solution by polarizing the light from a flashlight and then reflecting it off a sheet of paper. Try specular reflection off glass; is the reflected light polarized?

8.14 Discuss in detail what you see in Fig. 8.68. The crystal in the photograph is calcite, and it has a blunt corner at the upper left. The two polaroids have their transmission axes parallel to their *short* edges.

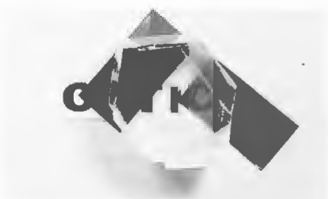
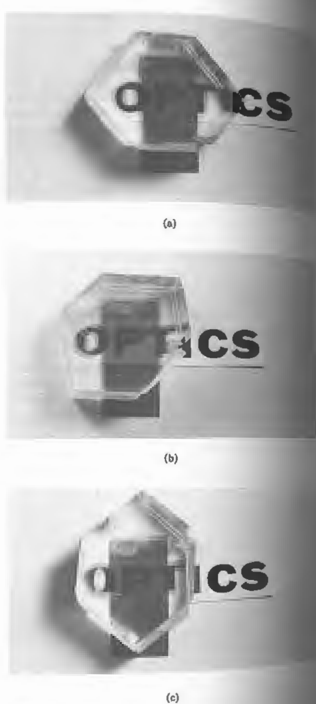


Figure 8.68

8.15 The calcite crystal in Fig. 8.69 is shown in three different orientations. Its blunt corner is on the left in (a), the lower left in (b), and the bottom in (c). The polaroid's transmission axis is horizontal. Explain each photograph, particularly (b).

8.16 In discussing calcite we pointed out that its large birefringence arises from the fact that the carbonate groups lie in parallel planes (normal to the optic axis). Show in a sketch and explain why the polarization of the group will be less when **E** is perpendicular to the CO_3 plane than when **E** is parallel to it. What does this mean with respect to $v_\perp$ and $v_\parallel$, that is, the wave's speeds when **E** is linearly polarized perpendicular or parallel to the optic axis?



(a)

(b)

(c)

Figure 8.69

8.17* [illegible]agine that we have a transmitter of microwaves that radiates a linearly polarized wave whose [illegible]own to be parallel to the dipole direction. [illegible]eflect as much energy as possible off the [illegible]ond (having an index of refraction of 9.0). [illegible]ssary incident angle and comment on the [illegible]f the beam.

8.18* A beam of natural light is incident on an air–[illegible]erface ($n_{ti} = 1.5$) at 40°. Compute the degree [illegible]ation of the reflected light.

8.19* [illegible] of natural light incident in air on a glass [illegible]face at 70° is partially reflected. Compute [illegible] overall reflectance. How would this compare with the case of incidence at, say, 56.3°? Explain.

8.20 A ray of yellow light is incident on a calcite plate [illegible] The plate is cut so that the optic axis is parallel [illegible] face and perpendicular to the plane of [illegible]nd the angular separation between the two emerging rays.

[illegible]am of light is incident normally on a quartz [illegible]optic axis is perpendicular to the beam. If [illegible] nm, compute the wavelengths of both the ordinary and extraordinary waves. What are their frequencies?

8.22 A beam of light enters a calcite prism from the left, as shown in Fig. 8.70. There are three possible [illegible]s of the optic axis of particular interest, and [illegible]spond to the x-, y-, and z-directions. Imagine [illegible] such prisms. In each case sketch the [illegible]ing and emerging beams, showing the state of [illegible]ization. How can any one of these be used to [illegible] n_o and n_e?

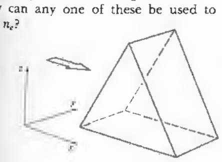


Figure 8.70

8.23 The electric field vector of an incident $\mathscr{P}$-state makes an angle of +30° with the horizontal fast axis of a quarter-wave plate. Describe, in detail, the state of polarization of the emergent wave.

8.24 Compute the critical angle for the ordinary ray, that is, the angle for total internal reflection at the calcite–balsam layer of a Nicol prism.

8.25* Draw a quartz Wollaston prism, showing all pertinent rays and their polarization states.

8.26 The prism shown in Fig. 8.71 is known as a *Rochon polarizer.* Sketch all the pertinent rays, assuming

a) that it is made of calcite.
b) that it is made of quartz.
c) Why might such a device be more useful than a dichroic polarizer when functioning with high-flux-density laser light?
d) What valuable feature of the Rochon is lacking in the Wollaston polarizer?

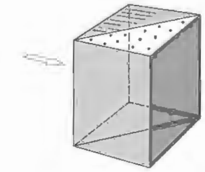


Figure 8.71

8.27* Take two ideal polaroids (the first with its axis vertical and the second, horizontal) and insert between them a stack of 10 half-wave plates, the first with its fast axis rotated $\pi/40$ rad from the vertical, and each subsequent one rotated $\pi/40$ rad from the previous one. Determine the ratio of the emerging to incident irradiance, showing your logic clearly.

8.28* Suppose you were originally given only a linear polarizer and a quarter-wave plate. How could you determine which was which?

8.29* An $\mathscr{L}$-state traverses an eighth-wave plate having a horizontal fast axis. What is its polarization state on emerging?

8.30* Figure 8.72 shows two polaroid linear polarizers and between them a microscope slide to which is attached a piece of cellophane tape. Explain what you see.

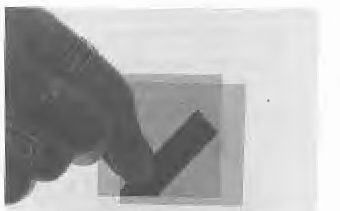


Figure 8.72

8.31 A Babinet compensator is positioned at 45° between crossed linear polarizers and is being illuminated with sodium light. When a thin sheet of mica (indices 1.599 and 1.594) is placed on the compensator, the black bands all shift by $\frac{1}{4}$ of the space separating them. Compute the retardance of the sheet and its thickness.

8.32 Imagine that we have unpolarized room light incident almost normally on the glass surface of a radar screen. A portion of it would be specularly reflected back toward the viewer and would thus tend to obscure the display. Suppose now that we cover the screen with a right-circular polarizer, as shown in Fig. 8.73. Trace the incident and reflected beams, indicating their polarization states. What happens to the reflected beam?

8.33 Is it possible for a beam to consist of two orthogonal incoherent $\mathscr{P}$-states and not be natural light? Explain. How might you arrange to have such a beam?

8.34* The specific rotatory power for sucrose [illegible] solved in water at 20°C ($\lambda_0 = 589.3$ nm) [illegible] +66.45° [illegible] 10 cm of path traversed through a solution containing 1 g of active substance (sugar) per cm³ of solution. A vertical $\mathscr{P}$-state (sodium light) enters at one end of a 1-m tube containing 1000 cm³ of solution, of which 10 [illegible] is sucrose. At what orientation will the $\mathscr{P}$-state [illegible]

8.35 On examining a piece of stressed [illegible] material between crossed linear polarizers, we would see a set of colored bands (isochromatics) and, [illegible] posed on these, a set of dark bands (isoclinics). How might we remove the isoclinics, leaving only the [illegible] matics? Explain your solution. Incidentally, the [illegible] arrangement is independent of the orientation of the photoelastic sample.

8.36* Consider a Kerr cell whose plates are [illegible] by a distance d. Let ℓ be the effective length [illegible] plates (slightly different from the actual length because of fringing of the field). Show that

$$\Delta\varphi = 2\pi K\ell V^2/d^2. \tag{8.41}$$

8.37 Compute the half-wave voltage for a [illegible] Pockels cell made of ADA (ammonium [illegible] arsenate) at $\lambda_0 = 550$ nm, where $r_{63} = 5.5$ [illegible] $n_0 = 1.58$.

8.38 Find a Jones vector $\mathbf{E}_2$ representing a [illegible] state orthogonal to

$$\mathbf{E}_1 = \begin{bmatrix} 1 \\ -2i \end{bmatrix}.$$

Sketch both of these.

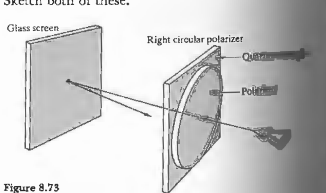


Figure 8.73

8.39* Two incoherent light beams represented by [illegible] and (3, 0, 0, 5) are superimposed.

(a) Describe in detail the polarization states of each of these.

(b) [illegible]ermine the resulting Stokes parameters of the [illegible]ned beam and describe its polarization state.

(c) [illegible] its degree of polarization?

(d) [illegible] the resulting light produced by overlapping the [illegible]coherent beams (1, 1, 0, 0) and (1, −1, 0, 0)? Explain.

8.40* Show by direct calculation, using Mueller [illegible] that a unit-irradiance beam of natural light [illegible] through a vertical linear polarizer is converted [illegible]tical $\mathscr{P}$-state. Determine its relative irradiance and degree of polarization.

8.41* Show by direct calculation, using Mueller [illegible] that a unit-irradiance beam of natural light [illegible]ough a linear polarizer with its transmission [illegible] is converted into a $\mathscr{P}$-state at +45°. Determine its relative irradiance and degree of polarization.

[illegible]w by direct calculation, using Mueller [illegible] that a beam of horizontal $\mathscr{P}$-state light passing [illegible]λ-plate with its fast axis horizontal emerges [illegible]

8.43* Confirm that the matrix

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}$$

[illegible] as a Mueller matrix for a quarter-wave plate [illegible]ast axis at +45°. Shine linear light polarized at [illegible] through it. What happens? What emerges when a [illegible]zontal $\mathscr{P}$-state enters the device?

8.44 Derive the Mueller matrix for a quarter-wave plate with its fast axis at −45°. Check that this matrix [illegible]ly cancels the previous one, so that a beam [illegible] through the two wave plates successively [illegible] unaltered.

8.45* Pass a beam of horizontally polarized linear light through each one of the $\frac{1}{4}\lambda$-plates in the two previous questions and describe the states of the emerging light. Explain which field component is leading which and how Fig. 8.7 compares with these results.

8.46 Use Table 8.6 to derive a Mueller matrix for a half-wave plate having a vertical fast axis. Utilize your result to convert an $\mathscr{R}$-state into an $\mathscr{L}$-state. Verify that the same wave plate will convert an $\mathscr{L}$- to an $\mathscr{R}$-state. Advancing or retarding the relative phase by $\pi/2$ should have the same effect. Check this by deriving the matrix for a half-wave plate with a horizontal fast axis.

8.47 Construct one possible Mueller matrix for a right-circular polarizer made out of a linear polarizer and a quarter-wave plate. Such a device is obviously an inhomogeneous two-element train and will differ from the *homogeneous* circular polarizer of Table 8.6. Test your matrix to determine that it will convert natural light to an $\mathscr{R}$-state. Show that it will pass $\mathscr{R}$-states, as will the homogeneous matrix. Your matrix should convert $\mathscr{L}$-states incident on the input side to $\mathscr{R}$-states, whereas the homogeneous polarizer will totally absorb them. Verify this.

8.48* If the Pockels cell modulator shown in Fig. 8.66 is illuminated by light of irradiance I_i, it will transmit a beam of irradiance I_t such that

$$I_t = I_i \sin^2(\Delta\varphi/2).$$

Make a plot of I_t/I_i versus applied voltage. What is the significance of the voltage that corresponds to maximum transmission? What is the lowest voltage above zero that will cause I_t to be zero for ADP ($\lambda_0 = 546.1$ nm)? How can things be rearranged to yield a maximum value of I_t/I_i for zero voltage? In this new configuration what irradiance results when $V = V_{\lambda/2}$?

8.49 Construct a Jones matrix for an isotropic plate of absorbing material having an amplitude transmission coefficient of t. It might sometimes be desirable to keep track of the phase, since even if $t = 1$, such a plate is still an isotropic phase retarder. What is the Jones matrix for a region of vacuum? What is it for a perfect absorber?

8.50 Construct a Mueller matrix for an isotropic plate of absorbing material having an amplitude transmission coefficient of t. What Mueller matrix will completely depolarize any wave without affecting its irradiance? (It has no physical counterpart.)

8.51 Keeping Eq. (8.29) in mind, write [illegible] for the unpolarized flux-density compo[illegible] partially polarized beam in terms of the [illegible] meters. To check your result, add an unpo[illegible] vector of flux density 4 to an $\mathscr{R}$-state of [illegible] Then see if you get $I_u = 4$ for the resultant [illegible]

9 INTERFERENCE

T[illegible]ate color patterns shimmering across an oil [illegible] asphalt pavement result from one of the more [illegible] manifestations of the phenomenon of [illegible].* On a macroscopic scale we might con[illegible]ated problem of the interaction of surface [illegible] pool of water. Our everyday experience [illegible] of situation allows us to envision a complex [illegible]of disturbances (as shown, e.g., in Fig. 9.1). [illegible] be regions where two (or more) waves [illegible]pped, partially or even completely canceling [illegible] Still other regions might exist in the pattern, [illegible]sultant troughs and crests are even more [illegible] than those of any of the constituent waves. [illegible] superimposed, the individual waves sepa[illegible]ntinue on, completely unaffected by their previous encounter.

[illegible]ena arising from optical interference would, [illegible] be quite difficult to interpret in terms of a [illegible]scular model. The wave theory of the elec[illegible]nature of light, however, provides a natural [illegible]hich to proceed. Recall that the expression [illegible]he optical disturbance is a second-order, [illegible], linear, partial, differential equation [illegible] have seen, it therefore obeys the important [illegible]*perposition*. Accordingly, the resultant elec[illegible]nsity **E**, at a point in space where two or [illegible]twaves overlap, is equal to the *vector sum* of the individual constituent disturbances. Briefly then, *optical interference may be termed an interaction of two or more lightwaves yielding a resultant irradiance that deviates*

Figure 9.1 Water waves from two point sources in a ripple tank.

* [illegible]water on the asphalt allows the oil film to assume the [illegible]th planar surface. The black asphalt absorbs the [illegible], preventing back reflection, which would tend to [illegible]ges.

from the sum of the component irradiances.

Out of the multitude of optical systems that produce interference, we will choose a few of the more important to examine. Interferometric devices will be divided, for the sake of discussion, into two groups: *wavefront splitting* and *amplitude splitting.* In the first instance, portions of the primary wavefront are used either directly as sources to emit secondary waves or in conjunction with optical devices to produce virtual sources of secondary waves. These secondary waves are then brought together, thereupon to interfere. In the case of amplitude splitting, the primary wave itself is divided into two segments, which travel different paths before recombining and interfering.

9.1 GENERAL CONSIDERATIONS

We have already examined the problem of the superposition of two scalar waves (Section 7.1), and in many respects those results will again be applicable. But light is, of course, a vector phenomenon; the electric and magnetic fields are vector fields. And an appreciation of this fact is fundamental to any kind of intuitive understanding of optics. Still, there are many situations in which the particular optical system can be so configured that the vector nature of light is of little practical significance. We will therefore derive the basic interference equations within the context of the vector model, thereafter delineating the conditions under which the scalar treatment is applicable.

In accordance with the principle of superposition, the electric field intensity $\mathbf{E}$, at a point in space, arising from the separate fields $\mathbf{E}_1, \mathbf{E}_2, \ldots$ of various contributing sources is given by

$$\mathbf{E} = \mathbf{E}_1 + \mathbf{E}_2 + \cdots. \qquad (9.1)$$

Once again, note that the optical disturbance, or light field $\mathbf{E}$, varies in time at an exceedingly rapid rate, roughly

$$4.3 \times 10^{14}\ \text{Hz} \quad \text{to} \quad 7.5 \times 10^{14}\ \text{Hz},$$

making the actual field an impractical quantity to detect. On the other hand, the irradiance I can be measured directly with a wide variety of sensors (e.g., photocells, bolometers, photographic emulsions, or eyes). Inde[redacted] then, if we are to study interferenc[redacted] we [redacted] be[redacted] approach the problem by way of the irradian[redacted]

Much of the analysis to follow can be perfo[redacted] without specifying the particular shape of the [redacted] fronts, and the results are therefore quite gene[redacted] in their applicability (Problem 9.1). For the sake o[redacted] plicity, however, consider two point sourc[redacted] emitting monochromatic waves of the same frequency in a homogeneous medium. Furthermo[redacted] let [redacted] separation a be much greater than λ. Locate [redacted] point of observation P far enough away from the so[redacted] that at P the wavefronts will be planes (Fig. 9.2). [redacted] the moment, we will consider only linearly polari[redacted] waves of the form

$$\mathbf{E}_1(\mathbf{r}, t) = \mathbf{E}_{01} \cos (\mathbf{k}_1 \cdot \mathbf{r} - \omega t + \varepsilon_1) \qquad (9.2a)$$

and

$$\mathbf{E}_2(\mathbf{r}, t) = \mathbf{E}_{02} \cos (\mathbf{k}_2 \cdot \mathbf{r} - \omega t + \varepsilon_2). \qquad (9.2b)$$

We saw in Chapter 3 that the irradiance at P [redacted]

$$I = \epsilon v \langle \mathbf{E}^2 \rangle.$$

Inasmuch as we will be concerned only with relative irradiances within the same medium, we will, for the time being at least, simply neglect the constants[redacted]

$$I = \langle \mathbf{E}^2 \rangle.$$

What is meant by $\langle \mathbf{E}^2 \rangle$ is of course the time [redacted] the magnitude of the electric field intensity s[redacted] $\langle \mathbf{E} \cdot \mathbf{E} \rangle$. Accordingly

$$\mathbf{E}^2 = \mathbf{E} \cdot \mathbf{E},$$

where now

$$\mathbf{E}^2 = (\mathbf{E}_1 + \mathbf{E}_2) \cdot (\mathbf{E}_1 + \mathbf{E}_2),$$

and thus

$$\mathbf{E}^2 = \mathbf{E}_1^2 + \mathbf{E}_2^2 + 2\mathbf{E}_1 \cdot \mathbf{E}_2. \qquad (9.3)$$

Taking the time average of both sides, we find that the irradiance becomes

$$I = I_1 + I_2 + I_{12},$$

provided that

$$I_1 = \langle \mathbf{E}_1^2 \rangle,$$

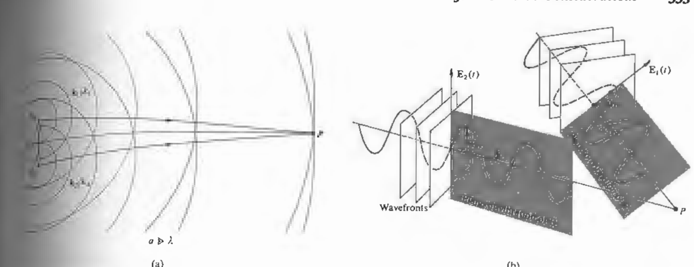


Figure 9.2 [redacted]aves from two point sources overlapping in space.

$$I_2 = \langle \mathbf{E}_2^2 \rangle, \qquad (9.6)$$

and

$$I_{12} = 2\langle \mathbf{E}_1 \cdot \mathbf{E}_2 \rangle. \qquad (9.7)$$

[redacted]er expression is known as the *interference term.* [redacted]uate it in this specific instance, we form

$$\mathbf{E}_1 \cdot \mathbf{E}_2 = \mathbf{E}_{01} \cdot \mathbf{E}_{02} \cos (\mathbf{k}_1 \cdot \mathbf{r} - \omega t + \varepsilon_1) \times \cos (\mathbf{k}_2 \cdot \mathbf{r} - \omega t + \varepsilon_2) \qquad (9.8)$$

or equivalently

$$\mathbf{E}_1 \cdot \mathbf{E}_2 = \mathbf{E}_{01} \cdot \mathbf{E}_{02} [\cos (\mathbf{k}_1 \cdot \mathbf{r} + \varepsilon_1) \times \cos \omega t + \sin (\mathbf{k}_1 \cdot \mathbf{r} + \varepsilon_1) \sin \omega t] \times [\cos (\mathbf{k}_2 \cdot \mathbf{r} + \varepsilon_2) \cos \omega t + \sin (\mathbf{k}_2 \cdot \mathbf{r} + \varepsilon_2) \sin \omega t]. \qquad (9.9)$$

[redacted]the time average of some function $f(t)$, taken [redacted]nterval T, is

$$\langle f(t) \rangle = \frac{1}{T} \int_t^{t+T} f(t')\, dt'. \qquad (9.10)$$

The period τ of the harmonic functions is $2\pi/\omega$, and [redacted]ent concern $T \gg \tau$. In that case the $1/T$ [redacted]front of the integral has a dominant effect.

After multiplying out and averaging Eq. (9.9) we have

$$\langle \mathbf{E}_1 \cdot \mathbf{E}_2 \rangle = \tfrac{1}{2} \mathbf{E}_{01} \cdot \mathbf{E}_{02} \cos (\mathbf{k}_1 \cdot \mathbf{r} + \varepsilon_1 - \mathbf{k}_2 \cdot \mathbf{r} - \varepsilon_2),$$

where use was made of the fact that $\langle \cos^2 \omega t \rangle = \frac{1}{2}$, $\langle \sin^2 \omega t \rangle = \frac{1}{2}$, and $\langle \cos \omega t \sin \omega t \rangle = 0$. The interference term is then

$$I_{12} = \mathbf{E}_{01} \cdot \mathbf{E}_{02} \cos \delta, \qquad (9.11)$$

and δ, equal to $(\mathbf{k}_1 \cdot \mathbf{r} - \mathbf{k}_2 \cdot \mathbf{r} + \varepsilon_1 - \varepsilon_2)$, is the *phase difference* arising from a combined path-length and initial phase-angle difference. Notice that if $\mathbf{E}_{01}$ and $\mathbf{E}_{02}$ (and therefore $\mathbf{E}_1$ and $\mathbf{E}_2$) are perpendicular, $I_{12} = 0$ and $I = I_1 + I_2$. Two such orthogonal $\mathscr{P}$-states will combine to yield an $\mathscr{R}$-, $\mathscr{L}$-, $\mathscr{P}$-, or $\mathscr{E}$-state, but the flux-density distribution will be unaltered.

The most common situation in the work to follow corresponds to $\mathbf{E}_{01}$ parallel to $\mathbf{E}_{02}$. In that case, the irradiance reduces to the value found in the scalar treatment of Section 7.1. Under those conditions

$$I_{12} = E_{01} E_{02} \cos \delta.$$

This can be written in a more convenient way by noticing that

$$I_1 = \langle \mathbf{E}_1^2 \rangle = \frac{E_{01}^2}{2} \qquad (9.12)$$

and

$$I_2 = \langle \mathbf{E}_2^2 \rangle = \frac{E_{02}^2}{2}. \tag{9.13}$$

The interference term becomes

$$I_{12} = 2\sqrt{I_1 I_2}\cos\delta,$$

whereupon the total irradiance is

$$I = I_1 + I_2 + 2\sqrt{I_1 I_2}\cos\delta. \tag{9.14}$$

At various points in space, the resultant irradiance can be greater, less than, or equal to $I_1 + I_2$, depending on the value of I_{12}, that is, depending on δ. A maximum in the irradiance is obtained when $\cos\delta = 1$, so that

$$I_{max} = I_1 + I_2 + 2\sqrt{I_1 I_2} \tag{9.15}$$

when

$$\delta = 0, \pm 2\pi, \pm 4\pi, \ldots.$$

In this case the phase difference between the two waves is an integer multiple of 2π, and the disturbances are said to be *in phase.* One speaks of this as *total constructive interference.* When $0 < \cos\delta < 1$ the waves are *out of phase,* $I_1 + I_2 < I < I_{max}$, and the result is known as *constructive interference.* At $\delta = \pi/2$, $\cos\delta = 0$, the optical disturbances are said to be 90° out of phase, and $I = I_1 + I_2$. For $0 > \cos\delta > -1$ we have the condition of *destructive* interference, $I_1 + I_2 > I > I_{min}$. The minimum in the irradiance results when the waves are 180° out of phase, troughs overlap crests, $\cos\delta = -1$, and

$$I_{min} = I_1 + I_2 - 2\sqrt{I_1 I_2}. \tag{9.16}$$

This occurs when $\delta = \pm\pi, \pm 3\pi, \pm 5\pi, \ldots$, and it is referred to as *total destructive interference.*

Another somewhat special yet very important case arises when the amplitudes of both waves reaching P in Fig. 9.2 are equal (i.e., $\mathbf{E}_{01} = \mathbf{E}_{02}$). Since the irradiance contributions from both sources are then equal, let $I_1 = I_2 = I_0$. Equation (9.14) can now be written as

$$I = 2I_0(1 + \cos\delta) = 4I_0\cos^2\frac{\delta}{2}, \tag{9.17}$$

from which it follows that $I_{min} = 0$ and $I_{max} = 4I_0$.

Equation (9.14) holds equally well fo[illegible] waves emitted by S_1 and S_2. Such waves can [illegible] as

$$\mathbf{E}_1(r_1, t) = \mathbf{E}_{01}(r_1)\exp[i(kr_1 - \omega t + \varepsilon_1)] \quad (9.1[illegible])$$

and

$$\mathbf{E}_2(r_2, t) = \mathbf{E}_{02}(r_2)\exp[i(kr_2 - \omega t [illegible] \quad (9.1[illegible])$$

The terms r_1 and r_2 are the radii of the [illegible] wavefronts overlapping at P; in other [illegible], they specify the distances from the sources to [illegible] In this [illegible]

$$\delta = k(r_1 - r_2) + (\varepsilon_1 - \varepsilon_2). \quad (9.1[illegible])$$

The flux density in the region surround[illegible] S_1 and S_2 will certainly vary from point to point [illegible] varies. Nonetheless, from the principle of co[illegible] of energy, we expect the spatial average of [illegible] constant and equal to the average of $I_1 + I_2$. [illegible] average of I_{12} must therefore be zero, [illegible] verified by Eq. (9.11), since the average o[illegible] term is, in fact, zero (for further discussion [illegible] see Problem 9.2).

Equation (9.17) will be applicable when th[illegible] between S_1 and S_2 is small in comparison [illegible] r_2 and when the interference region is also sm[illegible] in the same sense. Under these circumstances $\mathbf{E}_{01}$ [illegible] be considered independent of position, that [illegible] over the small region examined. If the emitti[illegible] are of equal strength, $E_{01} = E_{02}$, $I_1 = I_2 =$ [illegible] have

$$I = 4I_0\cos^2\tfrac{1}{2}[k(r_1 - r_2) + (\varepsilon_1 - \varepsilon_2)].$$

Irradiance maxima occur when

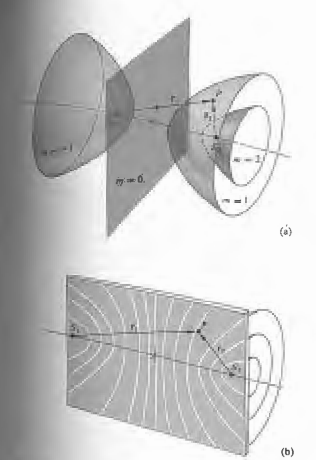
$$\delta = 2\pi m,$$

provided that $m = 0, \pm 1, \pm 2, \ldots$. Similarly minima [illegible] which $I = 0$, arise when

$$\delta = \pi m',$$

where $m' = \pm 1, \pm 3, \pm 5, \ldots$, or if you like, [illegible] can be Using Eq. (9.19) these two expressions fo[illegible] rewritten such that maximum irradiance o[illegible] when

$$(r_1 - r_2) = [2\pi m + (\varepsilon_2 - \varepsilon_1)]/k \quad (9.20[illegible])$$



[illegible] Hyperboloidal surfaces of maximum irradiance for two [illegible] Note that m is positive where $r_1 > r_2$.

and minimum when

$$(r_1 - r_2) = [\pi m' + (\varepsilon_2 - \varepsilon_1)]/k. \tag{9.20b}$$

[illegible] of these equations defines a family of surfaces [illegible] of which is a hyperboloid of revolution. The [illegible] the hyperboloids are separated by distances [illegible] right-hand sides of Eqs. (9.20a) and (9.20b). [illegible] located at S_1 and S_2. If the waves are in phase at the emitter, $\varepsilon_1 - \varepsilon_2 = 0$, and Eqs. (9.20a) and [illegible] can be simplified to

$$(r_1 - r_2) = 2\pi m/k = m\lambda \tag{9.21a}$$

$$(r_1 - r_2) = \pi m'/k = \tfrac{1}{2}m'\lambda \tag{9.21b}$$

for maximum and minimum irradiance, respectively.

Figure 9.3(a) shows a few of the surfaces over which there are irradiance maxima. The dark and light zones that would be seen on a screen placed in the region of interference are known as **interference fringes** [Fig. 9.3(b)]. Notice that the central bright band, equidistant from the two sources, is the so-called zeroth-order fringe ($m = 0$), which is straddled by the $m' = \pm 1$ minima, and these, in turn, are bounded by the first-order ($m = \pm 1$) maxima, which are straddled by the $m' = \pm 3$ minima, and so forth.

9.2 CONDITIONS FOR INTERFERENCE

It should be kept in mind that for a fringe pattern to be observed, the two sources need not be in phase with each other. A somewhat shifted but otherwise identical interference pattern will occur if there is some initial phase difference between the sources, so long as it remains constant. Such sources (which may or may not be in step but are always marching together) are said to be **coherent.*** Remember that because of the granular nature of the emission process, conventional quasi-monochromatic sources produce light that is a mix of photon wavetrains. At each illuminated point in space there is a net field that oscillates nicely (through roughly a million cycles) for less than 10 ns or so before it randomly changes phase. This interval over which the lightwave resembles a sinusoid is a measure of what is called its **temporal coherence.** The average time interval during which the lightwave oscillates in a predictable way we have already designated as the coherence time of the radiation. The longer the coherence time, the greater the temporal coherence of the source.

As observed from a fixed point in space, the passing lightwave appears fairly sinusoidal for some number of oscillations between abrupt changes of phase. The corresponding spatial extent over which the lightwave oscillates in a regular, predictable way we have called the coherence length [Eq. (7.64)]. Once again, it will be convenient to picture the light beam as a progression of well-defined, more or less sinusoidal, wavegroups of

* Chapter 10 is devoted to the study of coherence, so here we'll merely touch on those aspects that are immediately pertinent.

average length Δx_c, whose phases are quite uncorrelated to one another. Bear in mind that temporal coherence is a manifestation of spectral purity. If the light were ideally monochromatic, the wave would be a perfect sinusoid with an infinite coherence length. All real sources fall short of this, and all actually emit a range of frequencies, albeit sometimes quite narrow. For instance, an ordinary laboratory discharge lamp has a coherence length of several millimeters, whereas certain kinds of lasers routinely provide coherence lengths of tens of kilometers.

Two ordinary sources, two light bulbs or candle flames, can be expected to maintain a constant relative phase for a time no greater than Δt_c, so the interference pattern they produce will randomly shift around in space at an exceedingly rapid rate, averaging out and making it quite impractical to observe. Until the advent of the laser, it was a working principle that no two individual sources could ever produce an observable interference pattern. The coherence time of lasers, however, can be appreciable (of the order of milliseconds), and interference via independent lasers has been detected electronically (though not yet by the rather slow human eye). The most common means of overcoming this problem, as we shall see, is to make one source serve to produce two coherent secondary sources.

If two beams are to interfere to produce a stable pattern, they must have very nearly the same frequency. A significant frequency difference would result in a rapidly varying, time-dependent phase difference, which in turn would cause I_{12} to average to zero during the detection interval (see Section 7.1). Still, if the sources both emit white light, the component reds will interfere with reds, and the blues with blues. A great many fairly similar, slightly displaced, overlapping monochromatic patterns will produce one total white-light pattern. It will not be as sharp or as extensive as a quasimonochromatic pattern, but *white light will produce observable interference.*

The clearest patterns will exist when the interfering waves have equal or nearly equal amplitudes. The central regions of the dark and light fringes will then correspond to complete destructive and constructive interference, respectively, yielding maximum contrast.

In the previous section, we assumed that the two overlapping optical disturbance vectors were [illegible] polarized and parallel. Nonetheless, the [illegible] Section 9.1 apply as well to more complicat[illegible] indeed the treatment is applicable rega[illegible] polarization state of the waves. To apprec[illegible] that any polarization state can be synthesi[illegible] orthogonal $\mathscr{P}$-states. For natural (unpo[illegible] light) these $\mathscr{P}$-states are mutually incoherent, but that represents no particular difficulty.

Suppose that every wave has its propaga[illegible] vector in the same plane, so that we can label the constitu[illegible] orthogonal $\mathscr{P}$-states with respect to that plan[illegible] for example, $\mathbf{E}_\parallel$ and $\mathbf{E}_\perp$, which are parallel [illegible] dicular to the plane, respectively [Fig. 9.4[illegible] plane wave, whether polarized or not, ca[illegible] in the form $(\mathbf{E}_\parallel + \mathbf{E}_\perp)$. Imagine that the wav[illegible] and $(\mathbf{E}_{\parallel 2} + \mathbf{E}_{\perp 2})$ emitted from two identi[illegible] sources superimpose in some region of spa[illegible] The resulting flux-density distribution will consist [illegible] two independent, precisely, overlapping interfer[illegible] terns $\langle(\mathbf{E}_{\parallel 1} + \mathbf{E}_{\parallel 2})^2\rangle$ and $\langle(\mathbf{E}_{\perp 1} + \mathbf{E}_{\perp 2})^2\rangle$. [illegible] although we derived the equations of the [illegible] tion specifically for linear light, they are app[illegible] to any polarization state, including natural light[illegible]

Notice that even though $\mathbf{E}_{\perp 1}$ and $\mathbf{E}_{\perp 2}$ are always parallel to each other, $\mathbf{E}_{\parallel 1}$ and $\mathbf{E}_{\parallel 2}$, which are in the reference plane, need not be. They will be par[illegible] when the two beams are themselves paralle[illegible] $\mathbf{k}_2$). The inherent vector nature of the in[illegible] process as manifest in the dot-product repres[illegible] (9.11) of I_{12} cannot therefore be ignored. As [illegible] see, there are many practical situations in [illegible] beams approach being parallel, and in these [illegible] scalar theory will do rather nicely. Even so, (b) [illegible] (c) in Fig. 9.4 are included as an urge to caution[illegible] depict the imminent overlapping of tw[illegible] linearly polarized waves. In Fig. 9.4(b) th[illegible] tors are parallel, even though the beam[illegible] interference would nonetheless result. In [illegible] optical vectors are perpendicular, and [illegible] would be the case here even if the beams [illegible]

Fresnel and Arago made an extensiv[illegible] conditions under which the interferenc[illegible] of polar[illegible] light occurs, and their conclusions summar[illegible] some [illegible] above considerations. The **Fresnel–Arago laws** are as follows:

1. [illegible]thogonal, coherent $\mathscr{P}$-states cannot interfere [illegible] the sense that $I_{12} = 0$ and no fringes result.
2. [illegible]arallel, coherent $\mathscr{P}$-states will interfere in the [illegible]me way as will natural light.
3. The two constituent orthogonal $\mathscr{P}$-states of natural [illegible]not interfere to form a readily observable [illegible] pattern even if rotated into alignment. This [illegible] is understandable, since these $\mathscr{P}$-states are [illegible]nt.

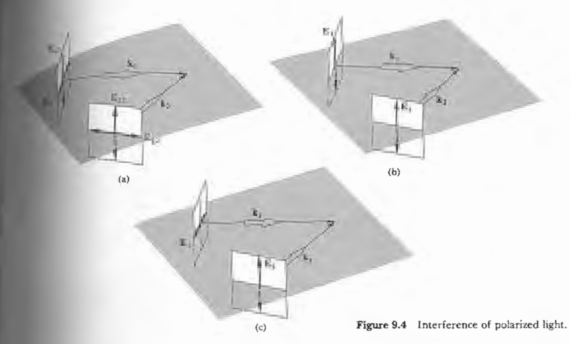


Figure 9.4 Interference of polarized light.

9.3 [illegible]EFRONT-SPLITTING INTERFEROMETERS

[illegible] for a moment to Fig. (9.3), where the equation

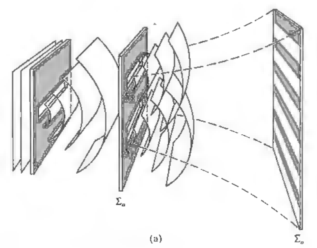
$$(r_1 - r_2) = m\lambda \qquad [9.21a]$$

[illegible] the surfaces of maximum irradiance. Since [illegible]ngth λ for light is very small, a large number [illegible] corresponding to the lower values of m will [illegible], and on either side of, the plane $m = 0$. A number of fairly straight parallel fringes will therefore appear on a screen placed perpendicular to that $(m = 0)$ plane and in the vicinity of it, and for this case the approximation $r_1 \approx r_2$ will hold. If S_1 and S_2 are then displaced normal to the $\overline{S_1S_2}$ line, the fringes will merely be displaced parallel to themselves. Two narrow slits will therefore increase the irradiance, leaving the central region of the two-point source pattern otherwise essentially unchanged.

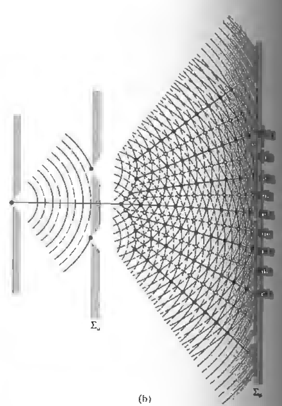
Consider a hypothetical monochromatic plane wave illuminating a long narrow slit. From that primary slit a cylindrical wave will emerge. Suppose that this wave, in turn, falls on two parallel, narrow, closely spaced slits, S_1 and S_2. This is shown in a three-dimensional view in Fig. 9.5(a). When symmetry exists, the segments of the primary wavefront arriving at the two slits will be exactly in phase, and the slits will constitute two coherent secondary sources. We expect that wherever the two waves coming from S_1 and S_2 overlap, interference will occur (provided that the optical path difference is less than the coherence length, $c\,\Delta t_c$).

Consider the construction shown in Fig. 9.5(c). In a

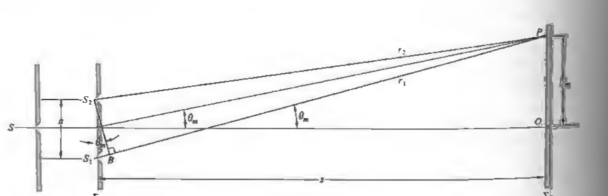
Figure 9.5 Young's experiment. (a) Cylindrical waves superimposed in the region beyond the aperture screen. (b) Overlapping waves showing peaks and troughs. (c) The geometry of Young's experiment. (d) A path-length difference of one wavelength corresponds to $m = \pm 1$ and the first-order maximum. (e) (Photo courtesy M. Cagnet, M. Francon, and J. C. Thrierr: *Atlas optischer Erscheinungen*, Berlin–Heidelberg–New York: Springer, 1962.) (f) A modern version of Young's experiment using a photodetector (e.g., a photovoltaic cell or photodiode like the RS 305-462) and an $X - Y$ recorder. The detector rides on a motor driven slide and scans the interference pattern.



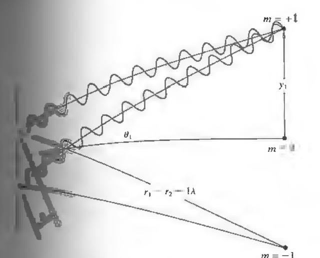
(a)



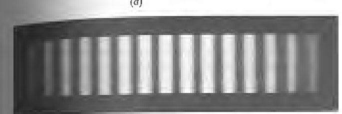
(b)



(c)



(d)



(e)

[illegible] physical situation the distance between each of [illegible] screens would be very large in comparison with the [illegible] between the two slits, several thousand times [illegible], and all the fringes would be fairly close to the [illegible] O of the screen. The path difference between [illegible] along $\overline{S_1P}$ and $\overline{S_2P}$ can be determined, to a [illegible] approximation, by dropping a perpendicular [illegible] onto $\overline{S_1P}$. This path difference is given by

$$(\overline{S_1B}) = (\overline{S_1P}) - (\overline{S_2P}) \tag{9.22}$$

or

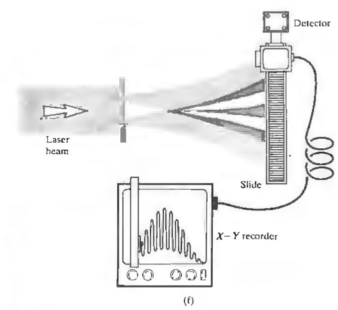
$$(\overline{S_1B}) = r_1 - r_2.$$

[illegible] with this approximation (Problem 9.13), [illegible] express the path difference as

$$r_1 - r_2 = a\theta, \tag{9.23}$$

since [illegible] $\sin\theta$. Notice that

$$\theta = \frac{y}{s}, \tag{9.24}$$



(f)

so

$$r_1 - r_2 = \frac{a}{s}y. \tag{9.25}$$

In accordance with Section 9.1, *constructive* interference will occur when

$$r_1 - r_2 = m\lambda. \tag{9.26}$$

Thus, from the last two relations we obtain

$$y_m = \frac{s}{a}m\lambda. \tag{9.27}$$

This gives the position of the mth bright fringe on the screen, if we count the maximum at 0 as the zeroth fringe. The angular position of the fringe is obtained by substituting the last expression into Eq. (9.24); thus

$$\theta_m = \frac{m\lambda}{a}. \tag{9.28}$$

This relationship can be obtained directly by inspecting

Fig. 9.5(c). For the mth-order interference maximum, m whole wavelengths should fit within the distance $r_1 - r_2$. Therefore, from the triangle S_1S_2B,

$$a \sin \theta_m = m\lambda \qquad (9.29)$$

or

$$\theta_m = m\lambda/a.$$

The spacing of the fringes on the screen can be gotten readily from Eq. (9.27). The difference in the positions of two consecutive maxima is

$$y_{m+1} - y_m = \frac{s}{a}(m+1)\lambda - \frac{s}{a}m\lambda$$

or

$$\Delta y = \frac{s}{a}\lambda. \qquad (9.30)$$

Since this pattern is equivalent to that obtained for two overlapping spherical waves (at least in the $r_1 \approx r_2$ region), we can apply Eq. (9.17). Using the phase difference

$$\delta = k(r_1 - r_2).$$

Equation (9.17) can be rewritten as

$$I = 4I_0 \cos^2 \frac{k(r_1 - r_2)}{2},$$

provided, of course, that the two beams are coherent and have equal irradiances I_0. With

$$r_1 - r_2 = ya/s,$$

the resultant irradiance becomes

$$I = 4I_0 \cos^2 \frac{ya\pi}{s\lambda}.$$

As shown in Fig. 9.6, consecutive maxima [redacted] by the Δy given in Eq. (9.30). It should be [redacted] that we effectively assumed that the slits were [redacted] infinitesimally wide, and so the cosine-square [redacted] of Fig. 9.6 are really an unattainable idealiza[redacted] actual pattern, Fig. 9.5(e), drops off with distance [redacted] either side of O because of diffraction.

In addition, as P in Fig. 9.5(c) is taken farther from the axis, $\overline{S_1B}$ (which is less than or equal to $\overline{S_1S_2}$) increases. If the primary source has [redacted] length, as the optical path difference increas[redacted] cally paired wavegroups will no longer be abl[redacted] at P exactly together—there will be an [redacted] amount of overlap in portions of uncorrel[redacted] wavegroups, and the contrast of the fringes will degrade. It is possible for Δx_c to be less than $\overline{S_1B}$. In that case, instead of two correlated portions [redacted] wavegroup arriving at P, only segments of [redacted] wavegroups will overlap, and the fringes will va[redacted] depicted in Fig. 9.7(a), when the path-length di[redacted] exceeds the coherence length, wavegrou[redacted] source S_1 arrives at P with wavegroup-D_2 fro[redacted] is interference, but it lasts only for a short [redacted] the pattern shifts as wavegroup-D_1 begi[redacted]o overlap wavegroup-C_2, since the relative phases [redacted] If the coherence length was larger [redacted] the path difference smaller, wavegroup-D_1 would more or less interact with its clone wavegroup-D_2, and [redacted] pair. The phases would then be correl[redacted] interference pattern stable [Fig. 9.7(b)]. Since [redacted] light source will have a coherence length of o[redacted] three wavelengths or so, it follows from Eq. (9[redacted] only [redacted] fringes will be seen on either side of [redacted] maximum.

[redacted] light (or with broad bandwidth illumination) all the constituent colors will arrive at $y = 0$ in [redacted]g traveled equal distances from each aper[redacted]eroth-order fringe will be essentially white, [redacted] higher order maxima will show a spread [redacted]engths, since y_m is a function of λ, according [redacted]27). Thus in white light we can visualize the [redacted]imum as the mth-order band of wavelengths; [redacted]at will lead directly to the diffraction grating [redacted] chapter.

* Modifications of this pattern arising as a result of [redacted] width of either the primary S or secondary-source sli[redacted] sidered in later chapters (10 and 12). In the fo[redacted] contrast will be used as a measure of the degree of [redacted] 12.1). In the latter, diffraction effects become sig[redacted]

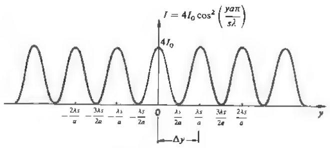
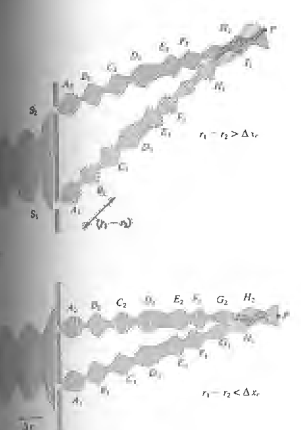


Figure 9.6 Idealized irradiance versus distance curve.



[redacted] schematic representation of how light, composed of a [redacted] wavegroups with a coherence length Δx_c, produces [redacted] (a) the path-length difference exceeds Δx_c and (b) [redacted] difference is less than Δx_c.

The fringe pattern can be directly observed by punching two small pinholes in a thin card. The holes should be approximately the size of the type symbol for a period on this page, and the separation between their centers about three radii. A street lamp, car headlight, or traffic signal at night, located a few hundred feet away, will serve as a plane wave source. The card should be positioned directly in front of and *very close to the eye*. The fringes will appear perpendicular to the line of centers. The pattern is much more readily seen with slits, as discussed in Section 10.2.2, but you should give the pinholes a try.

Microwaves, because of their long wavelength, also offer an easy way to observe double-slit interference. Two slits (e.g., $\lambda/2$ wide by λ long, separated by 2λ) cut in a piece of sheet metal or foil will serve quite well as secondary sources (Fig. 9.8).

The interferometric configuration discussed above, with either point or slit sources, is known as **Young's experiment**. The same physical and mathematical considerations apply directly to a number of other wavefront-splitting interferometers. Most common among these are Fresnel's double mirror, Fresnel's double prism, and Lloyd's mirror.

Fresnel's double mirror consists of two plane front-silvered mirrors inclined to each other at a very small angle, as shown in Fig. 9.9. One portion of the cylindrical wavefront coming from slit S is reflected from the first mirror, and another portion of the wavefront is reflected from the second mirror. An interference

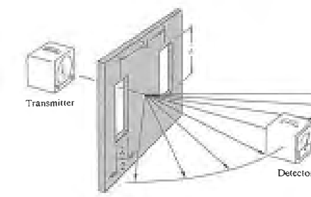


Figure 9.8 A microwave interferometer.

field exists in space in the region where the two reflected waves are superimposed on each other. The images (S_1 and S_2) of the slit S in the two mirrors can be considered as separate coherent sources, placed at a distance a apart. It follows from the laws of reflection, as illustrated in Fig. 9.9(a), that $\overline{SA} = \overline{S_1A}$ and $\overline{SB} = \overline{S_2B}$, so that $\overline{SA} + \overline{AP} = r_1$ and $\overline{SB} + \overline{BP} = r_2$. The optical path-length difference between the two rays is then simply $r_1 - r_2$. The various maxima occur at $r_1 - r_2 = m\lambda$, as they do with Young's interferometer. Again, the separation of the fringes is given by

$$\Delta y = \frac{s}{a}\lambda,$$

where s is the distance between the plane of the two virtual sources (S_1, S_2) and the screen. The arrangement in Fig. 9.9 has again been deliberately exaggerated to make the geometry somewhat clearer. Notice that the angle θ between the mirrors must be quite small if the electric field vectors for each of the two [illegible] be parallel, or nearly so. Let $\mathbf{E}_1$ and $\mathbf{E}_2$ re[illegible] lightwaves emitted from the coherent virtual [illegible] and S_2. At any instant in time at the point P [illegible] each of these vectors can be resolved into compo[illegible] parallel and perpendicular to the plane of the [illegible] With $\mathbf{k}_1$ and $\mathbf{k}_2$ parallel to $\overline{AP}$ and $\overline{BP}$, resp[illegible] should be apparent that the components of [illegible] in the plane of the figure will approach being parallel only for small θ.

The Fresnel double prism or biprism [illegible] thin prisms joined at their bases, as shown in Fig. [illegible] A single cylindrical wavefront impinges on [illegible] The top portion of the wavefront is refrac[illegible] ward, and the lower segment is refracted upward. In the region of superposition, interference o[illegible] Here, again, two virtual sources S_1 and S_2 exist, separated by a distance a, which can be expressed in terms of the prism angle α (Problem 9.15), where [illegible] The

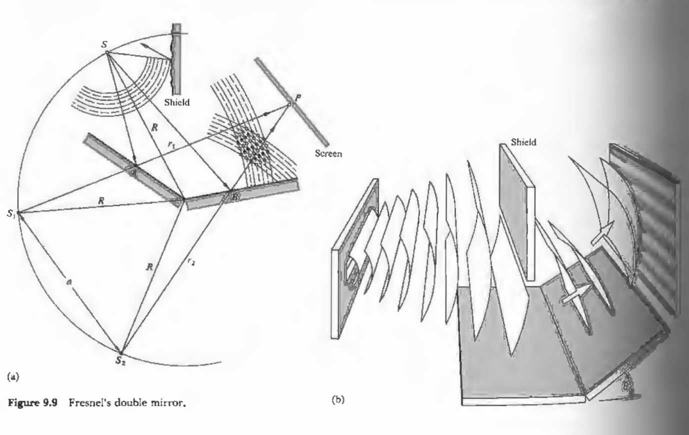
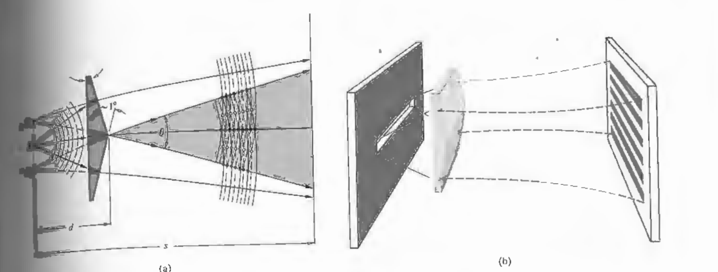


Figure 9.9 Fresnel's double mirror.



[illegible] Fresnel's biprism.

[illegible] separation of the fringes is the same [illegible]

The last [illegible]avefront-splitting interferometer that we will [illegible]nsider is Lloyd's mirror, shown in Fig. 9.11. It [illegible] flat piece of either dielectric or metal that [illegible] from which is reflected a portion of [illegible]drical wavefront coming from slit S. Another [illegible] the wavefront proceeds directly from the slit to the [illegible]creen. For the separation a, between the two [illegible] [illegible]urces, we take the distance between the actual slit [illegible]d its image S_1 in the mirror. The spacing of the [illegible]ges is once again given by $(s/a)\lambda$. The distinguishi[illegible] feature of this device is that at glancing [illegible] ($\theta_i \approx \pi/2$) the reflected beam undergoes a [illegible] phase shift. (Recall that the amplitude reflection [illegible]ients are then both equal to -1.) With an additional phase shift of $\pm\pi$,

$$\delta = k(r_1 - r_2) \pm \pi,$$

[illegible] becomes

$$I = 4I_0 \sin^2\left(\frac{\pi a y}{s\lambda}\right).$$

[illegible]nge pattern for Lloyd's mirror is complemen[illegible]at of Young's interferometer; the maxima of [illegible]ttern exist at values of y that correspond to minima in the other pattern. The top edge of the mirror is equivalent to $y = 0$ and will be the center of a dark fringe rather than a bright one, as in Young's device. The lower half of the pattern will be obstructed by the presence of the mirror itself. Consider what would happen if a thin sheet of transparent material were placed in the path of the rays traveling directly to the screen. The transparent sheet would have the effect of increasing the number of wavelengths in each direct ray. The entire pattern would accordingly move

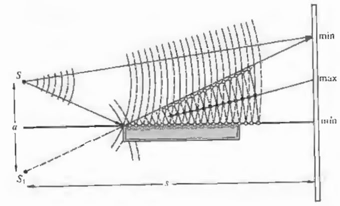


Figure 9.11 Lloyd's mirror.

upward, where the reflected rays would travel a bit farther before interfering. Because of the obvious inherent simplicity of this device, it has been used over a very wide region of the electromagnetic spectrum. The actual reflecting surfaces have ranged from crystals for x-rays, ordinary glass for light, and wire screening for microwaves to a lake or even the Earth's ionosphere for radio waves.*

All the above interferometers can be demonstrated quite readily. The necessary parts, mounted on a single optical bench, are shown diagrammatically in Fig. 9.12. The source of light should be a strong one; if a laser is not available, a discharge lamp or a carbon arc followed by a water cell, to cool things down a bit, will do nicely. The light will not be monochromatic, but the fringes, which will be colored, can still be observed. A satisfactory approximation of monochromatic light can be obtained with a filter placed in front of the arc. A low-power He–Ne laser is perhaps the easiest source to work with, and you won't need a water cell or filter.

9.4 AMPLITUDE-SPLITTING INTERFEROMETERS

Suppose that a lightwave was incident on a half-silvered mirror† or simply on a sheet of glass. Part of the wave would be transmitted and part would be reflected. Both the transmitted and reflected waves would, of course, have lower amplitudes than the original one. One might say figuratively that the amplitude had been "split." If the two separate waves could somehow be brought together again at a detector, interference would result, as long as the original coherence between the two had not been destroyed. If the path lengths differed by a distance greater than that of the wavegroup (i.e., the coherence length), the portions reunited at the detector

* For a discussion of the effects of a finite slit width and a finite frequency bandwidth, see R. N. Wolfe and F. C. Eisen, "Irradiance Distribution in a Lloyd Mirror Interference Pattern," *J. Opt. Soc. Am.* **38**, 706 (1948).

† A *half-silvered mirror* is one that is semitransparent, because the metallic coating is too thin to be opaque. You can look through it, and at the same time you can see your reflection in it. *Beam-splitters*, as devices of this kind are called, can also be made of thin stretched plastic films, known as *pellicles*, or even uncoated glass plate.

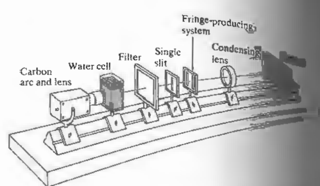


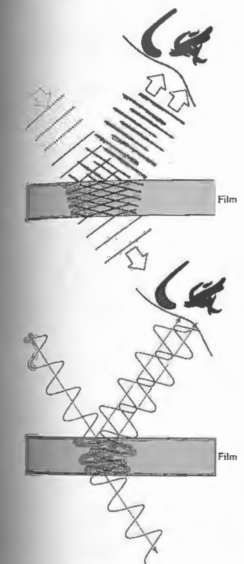
Figure 9.12 Bench setup to study wavefront-splitting [illegible] with a carbon arc source.

would correspond to different wavegroups. No [illegible] phase relationship would exist between them [illegible] case, and the fringe pattern would be unstable [illegible] point of being unobservable. We will get [illegible] ideas when we consider coherence theory in [illegible] For the moment we restrict ourselves, for the [illegible] to those cases in which the path difference [illegible] the coherence length.

9.4.1 Dielectric Films—Double-Beam Interference

Interference effects are observable in sheet transparent materials, the thicknesses of which vary over a very broad range, from films less than the length [illegible] wave (e.g., for green light λ_0 equals about [illegible] ness of this printed page) to plates several [illegible] thick. A layer of material is referred to as a [illegible] a given wavelength of electromagnetic radiation when its thickness is of the order of that wavelength. Before the early 1940s the interference phenomena a[illegible] with thin dielectric films, although well known, had fairly limited practical applicability. The rather spectacular color displays arising from oil slicks and [illegible] films, however pleasing aesthetically and theoretic[illegible] were mainly curiosities.

With the advent of suitable vacuum deposition techniques in the 1930s, precisely controlled coatings could be produced on a commercial scale, and this, in turn [illegible] a rebirth of interest in dielectric films. During [illegible] World War, both sides were finding the [illegible] variety of coated optical devices, and by [illegible] multilayered coatings were in widespread use.



[illegible] wave and ray representations of thin-film interfer[illegible] reflected from the top and bottom of the film interferes [illegible] fringe pattern.

Fringes of Equal Inclination

Initially, consider the simple case of a transparent parallel plate of dielectic material having a thickness d (Fig. 9.13). Suppose that the film is nonabsorbing and that the amplitude-reflection coefficients at the interfaces are so low that only the first two reflected beams E_{1r} and E_{2r} (both having undergone only one reflection) need be considered (Fig. 9.14). In practice, the amplitudes of the higher-order reflected beams (E_{3r}, etc.) generally decrease very rapidly, as can be shown for the air–water and air–glass interfaces (Problem 9.21). For the moment, consider S to be a monochromatic point source. The film serves as an amplitude-splitting device, so that E_{1r} and E_{2r} may be considered as arising from two coherent virtual sources lying behind the film; that is, the two images of S formed by reflection at the first and second interfaces. The reflected rays are parallel on leaving the film and can be brought together at a point P on the focal plane of a telescope objective or on the retina of the eye when focused at infinity. From Fig. 9.14, the optical path-length difference for the first two reflected beams is given by

$$\Lambda = n_f[(\overline{AB}) + (\overline{BC})] - n_1(\overline{AD}),$$

and since $(\overline{AB}) = (\overline{BC}) = d/\cos\theta_t$,

$$\Lambda = \frac{2n_f d}{\cos\theta_t} - n_1(\overline{AD}).$$

Now, to find an expression for $(\overline{AD})$, write

$$(\overline{AD}) = (\overline{AC})\sin\theta_i;$$

if we make use of Snell's law, this becomes

$$(\overline{AD}) = (\overline{AC})\frac{n_f}{n_1}\sin\theta_t,$$

where

$$(\overline{AC}) = 2d\tan\theta_t. \tag{9.32}$$

The expression for Λ now becomes

$$\Lambda = \frac{2n_f d}{\cos\theta_t}(1 - \sin^2\theta_t)$$

or finally

$$\Lambda = 2n_f d\cos\theta_t. \tag{9.33}$$

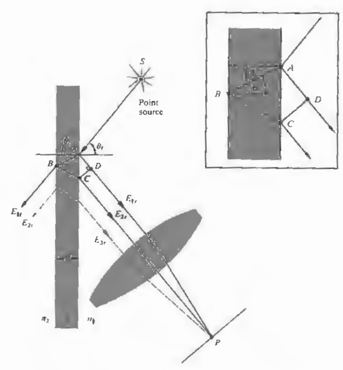


Figure 9.14 Fringes of equal inclination.

The corresponding phase difference associated with the optical path-length difference is then just the product of the free-space propagation number and Λ, that is, $k_0\Lambda$. If the film is immersed in a single medium, the index of refraction can simply be written as $n_1 = n_2 = n$. Realize, of course, that n may be less than n_f, as in the case of a soap film in air, or greater than n_f, as with an air film between two sheets of glass. In either case there will be an additional phase shift arising from the reflections themselves. Recall that for incident angles up to about 30°, regardless of the polarization of the incoming light, the two beams, one internally and one externally reflected, will experience a *relative phase shift* of π radians (Fig. 4.25 and Section 4.5). Accordingly,

$$\delta = k_0\Lambda \pm \pi$$

and more explicitly

$$\delta = \frac{4\pi n_f}{\lambda_0} d \cos \theta_t \pm \pi \qquad (9.34)$$

or

$$\delta = \frac{4\pi d}{\lambda_0}(n_f^2 - n^2 \sin^2 \theta_i)^{1/2} \pm \pi. \qquad (9.[illegible])$$

The sign of the phase shift is immaterial, so we will choose the negative sign to make the equation[illegible] simpler in form. In reflected light an interfe[illegible] maximum, a bright spot, appears at P when δ [illegible] in other words, an even multiple of π. [illegible] (9.34) can be rearranged to yield

$$\text{(maxima)} \qquad d \cos \theta_t = (2m + 1)\frac{\lambda_f}{4}, \qquad [illegible] \qquad (9.[illegible])$$

where use has been made of the fact that [illegible]

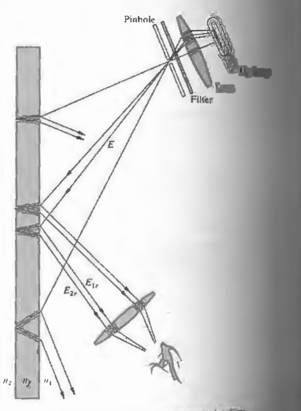


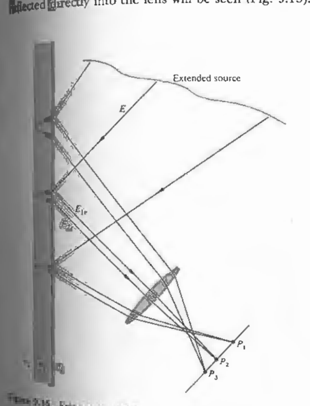
Figure 9.15 Fringes seen on a small [illegible]

[illegible] corresponds to minima in the transmitted [illegible] minima in reflected light (maxima [illegible] light) result when δ = $(2m \pm 1)\pi$, that is, [illegible] of π. For such cases Eq. (9.34) yields

$$d \cos \theta_t = 2m\frac{\lambda_f}{4}. \qquad (9.37)$$

[illegible] of odd and even multiples of $\lambda_f/4$ in [illegible] (9.37) is rather significant, as we will see [illegible] could, of course, have a situation in which [illegible] n_2 or $n_1 < n_f < n_2$, as with a fluoride film [illegible] on an optical element of glass immersed in [illegible] phase shift would then not be present, and [illegible] would simply be modified appropri-[illegible]

[illegible] used to focus the rays has a small aperture, [illegible] fringes will appear on a small portion of [illegible] rays leaving the point source that are [illegible] directly into the lens will be seen (Fig. 9.15).



[illegible] Fringes [illegible] large region of the film.

For an extended source, light will reach the lens from various directions, and the fringe pattern will spread out over a large area of the film (Fig. 9.16).

The angle θ_i or equivalently θ_t, determined by the position of P, will in turn control δ. The fringes appearing at points P_1 and P_2 in Fig. 9.17 are, accordingly, known as **fringes of equal inclination**. (Problem 9.26 discusses some easy ways to see these fringes.) Keep in mind that each source point on the extended source is incoherent with respect to the others.

Notice that as the film becomes thicker, the separation $(\overline{AC})$ between E_{1r} and E_{2r} also increases, since

$$(\overline{AC}) = 2d \tan \theta_t. \qquad [9.32]$$

When only one of the two rays is able to enter the pupil of the eye, the interference pattern will disappear. The larger lens of a telescope can then be used to gather in both rays, once again making the pattern visible. The separation can also be reduced by reducing θ_i and

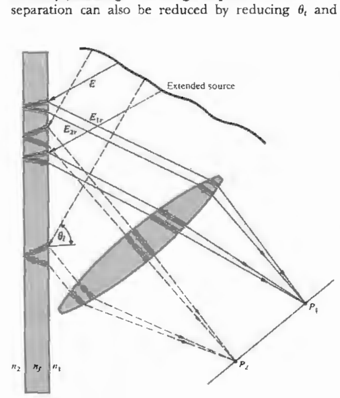


Figure 9.17 All rays inclined at the same angle arrive at the same point.

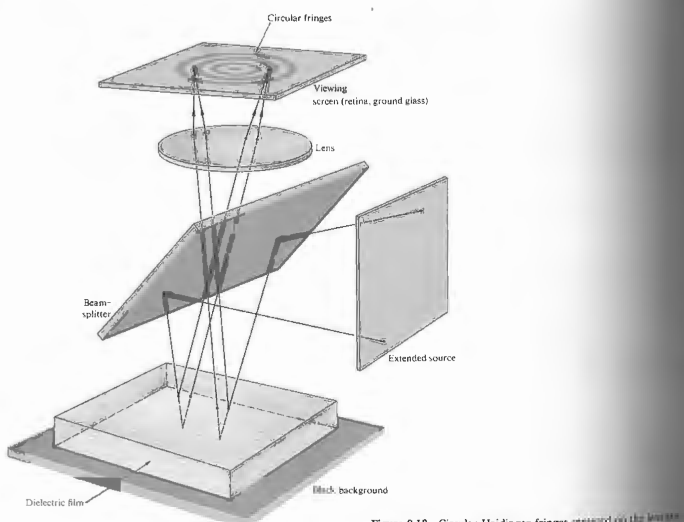


Figure 9.18 Circular Haidinger fringes centered on the lens.

therefore θ_i, that is, by viewing the film at nearly normal incidence. The equal-inclination fringes that are seen in this manner for thick plates are known as **Haidinger fringes, after the Austrian physicist Wilhelm Karl Haidinger (1795–1871). With an extended source, the symmetry of the setup requires that the interference pattern consists of a series of concentric circular bands centered on the perpendicular drawn from the eye to** the film (Fig. 9.18). As the observer moves, the interference pattern follows along.

Fringes of Equal Thickness

A whole class of interference fringes exis[redacted] which the optical thickness, $n_f d$, is the domina[redacted] rather than θ_i. These are referred to as fri[redacted] **thickness**. Under white-light illumination[redacted] cence of soap bubbles, oil slicks (a few wavele[redacted] thick), and even oxidized metal surfaces is the re[redacted] variations in film thickness. Interference bands o[redacted] kind are analogous to the constant-heig[redacted] of a topographical map. Each fringe is[redacted]

[redacted]he film for which the optical thickness is a [redacted]general, n_f does not vary, so that the fringes [redacted]espond to regions of constant film thick[redacted], they can be quite useful in determining [redacted] features of optical elements (lenses, prisms, [redacted]xample, a surface to be examined may be [redacted]act with an *optical flat.** The air in the space [redacted]two generates a thin-film interference pat[redacted]est surface is flat, a series of straight, equally [redacted]nds indicates a wedge-shaped air film, usually [redacted] from dust between the flats. Two pieces of [redacted]s separated at one end by a strip of paper will [redacted]atisfactory wedge with which to observe these bands.

[redacted]iewed at nearly normal incidence in the man[redacted]ated in Fig. 9.19, the contours arising from a [redacted]m film are called **Fizeau fringes**. For a thin wedge of small angle α, the optical path-length difference between two reflected rays may be approxi[redacted] by Eq. (9.33), where d is the thickness at a par[redacted]oint, that is,

$$d = x\alpha. \tag{9.38}$$

... small values of θ_i the condition for an interference [redacted]m becomes

$$(m + \tfrac{1}{2})\lambda_0 = 2n_f d_m$$

or

$$(m + \tfrac{1}{2})\lambda_0 = 2\alpha x_m n_f.$$

Since $\lambda_f = \lambda_0/n_f$, x_m may be written as

$$x_m = \left(\frac{m + 1/2}{2\alpha}\right)\lambda_f. \tag{9.39}$$

[redacted]at distances from the apex given by $\lambda_f/4\alpha$, [redacted]nd consecutive fringes are separated by a [redacted]ven by

$$\Delta x = \lambda_f/2\alpha. \tag{9.40}$$

[redacted]id to be optically flat when it deviates by not more [redacted]from a perfect plane. In the past, the best flats were [redacted]d quartz. Now glass-ceramic materials (e.g., CER-[redacted]mely small thermal coefficients of expansion (about [redacted]quartz) are available. Individual flats of $\lambda/200$ or a [redacted]ade.

Notice that the difference in film thickness between adjacent maxima is simply $\lambda_f/2$. Since the beam reflected from the lower surface traverses the film twice ($\theta_i \approx \theta_t \approx 0$), adjacent maxima differ in optical path length by λ_f. Note, too, that the film thickness at the various maxima is given by

$$d_m = (m + \tfrac{1}{2})\frac{\lambda_f}{2}, \tag{9.41}$$

which is an odd multiple of a quarter wavelength. Traversing the film twice yields a phase shift of π, which when added to the shift of π resulting from reflection, puts the two rays back in phase.

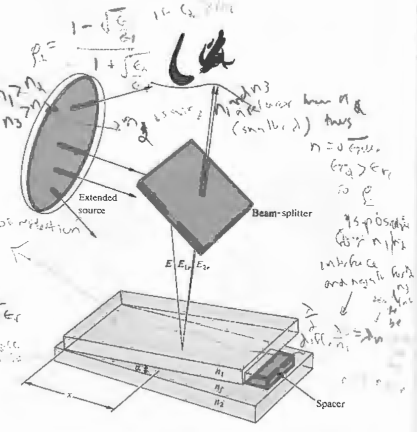


Figure 9.19 Fringes from a wedge-shaped film.

Figure 9.20 is a photograph of a soap film held vertically so that it settles into a wedge shape under the influence of gravity. When illuminated with white light, the bands are various colors. The black region at the top is a portion where the film is less than $\lambda_f/4$ thick. Twice this, plus an additional shift of $\lambda_f/2$ due to the reflection, is less than a whole wavelength. The reflected rays are therefore out of phase. As the thickness decreases still further, the total phase difference approaches π. The irradiance at the observer goes to a minimum (Eq. 9.16), and the film appears black in reflected light.*

Press two well-cleaned microscope slides together. The enclosed air film will usually not be uniform. In ordinary room light a series of irregular, colored bands (fringes of equal thickness) will be clearly visible across the surface (Fig. 9.21). The thin glass slides distort under pressure, and the fringes move and change accordingly. Indeed, if the two pieces of glass are forced together at a point, as might be done by pressing on them with a sharp pencil, a series of concentric, nearly [illegible] fringes is formed about that point (Fig. 9.22). [illegible] as **Newton's rings,*** this pattern is more [illegible] examined with the arrangement of Fig. 9[illegible] lens is placed on an optical flat and illuminated [illegible] incidence with quasimonochromatic light. [illegible] of uniformity in the concentric circular [illegible] measure of the degree of perfection [illegible] lens. With R as the radius of curvature of the convex lens, the relation between the distance x and the film thickness d is given by

$$x^2 = R^2 - (R - d)^2$$

or more simply by

$$x^2 = 2Rd - d^2.$$

Since $R \gg d$, this becomes

$$x^2 = 2Rd.$$

Figure 9.21 Fringes in an air film between [illegible] (Photo by E. H.)

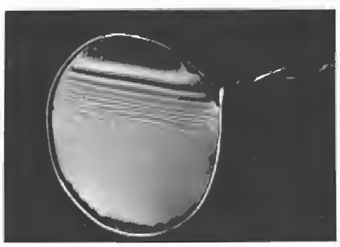
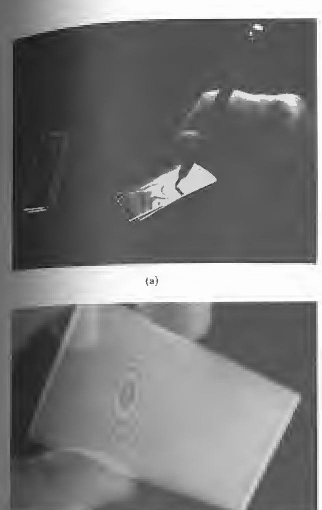


Figure 9.20 A wedge-shaped film made of liquid dishwashing soap. (Photo by E. H.)

* The relative phase shift of π between internal and external reflection is required if the reflected flux density is to go to zero smoothly, as the film gets thinner and finally disappears.

* Robert Hooke (1635–1703) and Isaac Newton [illegible] studied a whole range of thin-film phenomena, from [illegible] to the air film between lenses. Quoting from Newton [illegible]

> I took two Object-glasses, the one a Planoconvex for [illegible] Foot Telescope, and the other a large double [illegible] of about fifty Foot; and upon this, laying the [illegible] plane side downwards, I pressed them slowly to[illegible] the Colours successively emerge in the middle [illegible]



(a)

(b)

[illegible] rings with two microscope slides. (Photos by [illegible])

[illegible] approximate by assuming that we need only [illegible] the first two reflected beams E_{1r} and E_{2r}. The [illegible] interference maximum will occur in the thin [illegible] thickness is in accord with the relationship

$$2n_f d_m = (m + \tfrac{1}{2})\lambda_0.$$

[illegible] of the mth bright ring is therefore found by combining the last two expressions to yield

$$x_m = [(m + \tfrac{1}{2})\lambda_f R]^{1/2}. \tag{9.42}$$

Similarly, the radius of the mth dark ring is

$$x_m = (m\lambda_f R)^{1/2}. \tag{9.43}$$

If the two pieces of glass are in good contact (no dust), the central fringe at that point ($x_0 = 0$) will clearly be a minimum in irradiance, an understandable result since d goes to zero at that point. In transmitted light, the observed pattern will be the complement of the reflected one discussed above, so that the center will now appear bright.

Newton's rings, which are Fizeau fringes, can be distinguished from the circular pattern of Haidinger's fringes by the manner in which the diameters of the rings vary with the order m. The central region in the Haidinger pattern corresponds to the maximum value

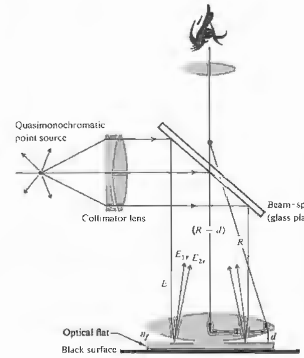


Figure 9.23 A standard setup to oberve Newton's rings.

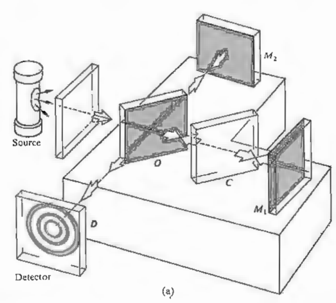
of m (Problem 9.25), whereas just the opposite applies to Newton's rings.

An optical shop, in the business of making lenses, will have a set of precision spherical test plates or gauges. A designer can specify the surface accuracy of a new lens in terms of the number and regularity of the Newton rings that will be seen with a particular test gauge. The use of test plates in the manufacture of high-quality lenses, however, is giving way to far more sophisticated techniques involving laser interferometers (Section 9.8.4).

9.4.2 Mirrored Interferometers

There are a good number of amplitude-splitting interferometers that utilize arrangements of mirrors and beam-splitters. By far the best known and historically the most important of these is the **Michelson interferometer**. Its configuration is illustrated in Fig. 9.24. An extended source (e.g., a diffusing ground-glass plate illuminated by a discharge lamp) emits a wave, part of which travels to the right. The beam-splitter at O divides the wave into two, one segment traveling to the right and one up into the background. The two waves are reflected by mirrors M_1 and M_2 and return to the beam-splitter. Part of the wave coming from M_2 passes through the beam-splitter going downward, and part of the wave coming from M_1 is deflected by the beam-splitter toward the detector. Thus the two waves are united, and interference can be expected.

Notice that one beam passes through O three times, whereas the other traverses it only once. Consequently, each beam will pass through equal thicknesses of glass only when a *compensator plate C* is inserted in the arm OM_1. The compensator is an exact duplicate of the



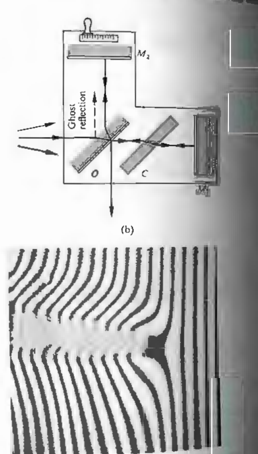
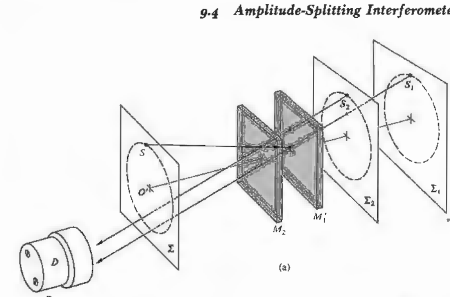


Figure 9.24 The Michelson interferometer. (c) The fringes with the tip of a hot soldering iron in one arm. (Photo by [illegible]



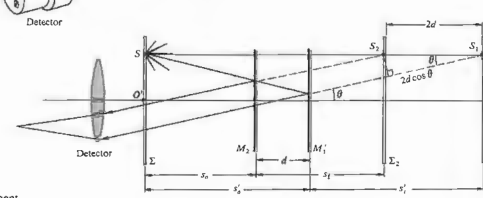


Figure 9.25 A conceptual rearrangement of the Michelson interferometer.

beam-splitter, with the exception of any possible silvered or thin film coating on the beam-splitter. It is positioned at an angle of 45°, so that O and C are parallel to each other. With the compensator in place, any optical path difference arises from the actual path difference. In addition, because of the dispersion of the beam-splitter, the optical path is a function of λ. Accordingly, for quantitative work, the interferometer without the compensator plate can be used only with a quasimonochromatic source. The inclusion of a compensator negates the effect of dispersion, so that even a source with a very broad bandwidth will generate discernible fringes.

To understand how fringes are formed, refer to the construction shown in Fig. 9.25, where the physical components are represented more as mathematical surfaces. An observer at the position of the detector will simultaneously see both mirrors M_1 and M_2 along with the source Σ in the beam-splitter. Accordingly, we can redraw the interferometer as if all the elements were in a straight line. Here M_1' corresponds to the image of mirror M_1 in the beam-splitter, and Σ has been swung over in line with O and M_2. The positions of these elements in the diagram depend on their relative distances from O (e.g., M_1' can be in front of, behind, or coincident with M_2 and can even pass through it). The surfaces Σ_1 and Σ_2 are the images of the source Σ in mirrors M_1 and M_2, respectively. Now consider a single point S on the source emitting light in all directions; let's follow the course of one emerging ray. In actuality a wave from S will be split at O, and its segments will thereafter be reflected by M_1 and M_2. In our schematic diagram we represent this by reflecting the ray off both M_2 and M_1'. To an observer at D the two reflected rays will appear to have come from the image points S_1 and S_2 [note that all rays shown in (a) and (b) of Fig. 9.25 share a common plane of incidence]. For all practical purposes, S_1 and S_2 are coherent point sources, and we can anticipate a flux-density distribution obeying Eq. (9.14). As the figure shows, the optical path difference for these rays is nearly $2d \cos \theta$, which represents a phase difference of $k_0 2d \cos \theta$. There is an additional phase term arising from the fact that the wave traversing the arm OM_2 is internally reflected in the beam-splitter, whereas the OM_1-wave is externally reflected at O. If the beam-splitter is simply an uncoated glass plate, the relative phase shift resulting from the two reflections will (Section 4.5, p. 119) be π radians. *Destructive*, rather than constructive, interference will then exist when

$$2d \cos \theta_m = m\lambda_0, \tag{9.44}$$

where m is an integer. If this condition is fulfilled for the point S, then it will be equally well fulfilled for any point on Σ that lies on the circle of radius $O'S$, where O' is located on the axis of the detector. As illustrated in Fig. 9.26, an observer will see a circular fringe system concentric with the central axis of her eye's lens. Because of the small aperture of the eye, the observer will not be able to see the entire pattern without the use of a large lens near the beam-splitter to collect most of the emergent light.

If we use a source containing a number of frequency

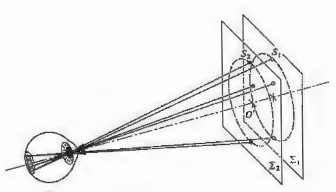


Figure 9.26 Formation of circular fringes.

components (e.g., a mercury discharge [illegible] dependence of θ_m on λ_0 in Eq. (9.44) require[illegible] such component generate a fringe system of its own. Note, too, that since $2d \cos \theta_m$ must be less than the coherence length of the source, it follows that [illegible] will be particularly easy to use in demonst[illegible] interferometer (see Section 9.5). This point [illegible] made strikingly evident were we to compare the [illegible] produced by laser light with those generated by [illegible] light from an ordinary tungsten bulb or a candle. In the latter case, the path difference must be very [illegible] zero, if we are to see any fringes at all, whereas [illegible] former instance a difference of 10 cm has little [illegible]able effect.

An interference pattern in quasimonochrom[illegible] typically consists of a large number of alternat[illegible] and dark rings. A particular ring correspond[illegible] *order m*. As M_2 is moved toward M_1', d dec[illegible] according to Eq. (9.44), $\cos \theta_m$ increases wh[illegible] θ_m [illegible] fore decreases. The rings shrink toward the cent[illegible] the highest-order one disappearing wh[illegible] decreases by $\lambda_0/2$. Each remaining ring b[illegible] more and more fringes vanish at the center [illegible] a few fill the whole screen. By the time d = [illegible] reached, the central fringe will have spread [illegible] the entire field of view. With a phase shift of [illegible] from reflection off the beam-splitter, the whole [illegible] will then be an interference minimum. (Lack of [illegible] tion in the optical elements can render this un[illegible] able.) Moving M_2 still farther causes the fri[illegible] reappear at the center and move outward.

Notice that a central dark fringe for which θ_m [illegible] Eq. (9.44) can be represented by

$$2d = m_0\lambda_0.$$

(Keep in mind that this is a special case. The [illegible] region might correspond to neither a maximum [illegible] minimum.) Even if d is 10 cm, which is fairly [illegible] in laser light, and $\lambda_0 = 500$ nm, m_0 will be quite large, namely 400,000. At a fixed value of d, successive [illegible] rings will satisfy the expressions

$$2d \cos \theta_1 = (m_0 - 1)\lambda_0$$
$$2d \cos \theta_2 = (m_0 - 2)\lambda_0$$
$$\vdots$$
$$2d \cos \theta_p = (m_0 - p)\lambda_0.$$

The angular position of any ring, for example, the pth ring, is determined by combining Eqs. (9.45) and (9.46) to yield

$$2d(1 - \cos \theta_p) = p\lambda_0. \tag{9.47}$$

Since $\theta_m \equiv \theta_p$, both are just the half-angle subtended at the detector by the particular ring, and since $m = m_0 - p$, Eq. (9.47) is equivalent to Eq. (9.44). The new form is somewhat more convenient, since (using the same example as above) with $d = 10$ cm, the sixth dark ring can be specified by stating that $p = 6$, or in terms of the *order* of the pth ring, that $m = 399{,}994$. If θ_p is small,

$$\cos \theta_p = 1 - \frac{\theta_p^2}{2},$$

and Eq. (9.47) yields

$$\theta_p = \left(\frac{p\lambda_0}{d}\right)^{1/2} \tag{9.48}$$

[illegible]gular radius of the pth fringe.

[illegible]struction of Fig. 9.25 represents one possible [illegible], the one in which we consider only pairs of parallel emerging rays. Since these rays do not [illegible] meet, they cannot form an image without a [illegible] lens of some sort. Indeed, that lens is most [illegible]ded by the observer's eye focused at infinity. [illegible] resulting *fringes of equal inclination* (θ_m = constant) [illegible]ed at infinity are also *Haidinger fringes*. A com[illegible]son of Figs. 9.25(b) and 9.3(a), both showing two [illegible] point sources, suggests that in addition to these [illegible] fringes at infinity, there might also be (real) [illegible] formed by converging rays. These fringes do [illegible]. Hence, if you illuminate the interferometer [illegible] *source* and shield out all extraneous light, [illegible] see the projected pattern on a screen in [illegible] room (see Section 9.5). The fringes will [illegible] space in front of the interferometer (i.e., [illegible]ector is shown), and their size will increase [illegible] distance from the beam-splitter. We will [illegible] (real) fringes arising from point-source [illegible] little later on.

[illegible] mirrors of the interferometer are inclined [illegible] respect to each other, making a small angle (i.e., [illegible] M_1 and M_2 are not quite perpendicular), *Fizeau* [illegible] are observed. The resultant wedge-shaped air film between M_2 and M_1' creates a pattern of straight parallel fringes. The interfering rays appear to diverge from a point behind the mirrors. The eye would have to focus on this point in order to make these *localized fringes* observable. It can be shown analytically* that by appropriate adjustment of the orientation of the mirrors M_1 and M_2, fringes can be produced that are straight, circular, elliptical, parabolic, or hyperbolic—this holds as well for the real and virtual fringes.

It is apparent that the Michelson interferometer can be used to make extremely accurate length measurements. As the moveable mirror is displaced by $\lambda_0/2$, each fringe will move to the position previously occupied by an adjacent fringe. Using a microscope arrangement, one need only count the number of fringes N, or portions thereof, that have moved past a reference point to determine the distance traveled by the mirror Δd, that is,

$$\Delta d = N\,(\lambda_0/2).$$

Of course, nowadays this can be done fairly easily by electronic means. Michelson used the method to measure the number of wavelengths of the red cadmium line corresponding to the standard meter in Sèvres near Paris.†

The Michelson interferometer can be used along with a few polaroid filters to verify the Fresnel–Arago laws. A polarizer inserted in each arm will allow the optical path-length difference to remain fairly constant, while the vector field directions of the two beams are easily changed.

A microwave Michelson interferometer can be constructed with sheet-metal mirrors and a chicken-wire beam splitter. With the detector located at the central fringe, it can easily measure shifts from maxima to minima as one of the mirrors is moved, thereby determining λ. A few sheets of plywood, plastic, or glass inserted in one arm will change the central fringe. Counting the number of fringe shifts yields a value for the index of refraction, and from that we can compute the dielectric constant of the material.

* See, for example, Valasek, *Optics*, p. 135.

† A discussion of the procedure he used to avoid counting the 3,106,327 fringes directly can be found in Strong, *Concepts of Classical Optics*, p. 238, or Williams, *Applications of Interferometry*, p. 51.

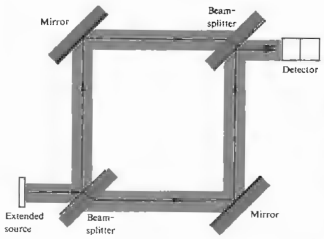


Figure 9.27 The Mach–Zehnder interferometer.

The **Mach–Zehnder interferometer** is another amplitude-splitting device. As shown in Fig. 9.27, it consists of two beam-splitters and two totally reflecting mirrors. The two waves within the apparatus travel along separate paths. A difference between the optical paths can be introduced by a slight tilt of one of the beam-splitters. Since the two paths are separated, the interferometer is relatively difficult to align. For the same reason, however, the interferometer finds myriad applications. It has even been used, in a somewhat altered yet conceptually similar form, to obtain electron interference fringes.*

An object interposed in one beam will alter the optical path-length difference, thereby changing the fringe pattern. A common application of the device is to observe the density variations in gas-flow patterns within research chambers (wind tunnels, shock tubes, etc.). One beam passes through the optically flat windows of the test chamber, while the other beam traverses appropriate compensator plates. The beam within the chamber will propagate through regions having a spatially varying index of refraction. The resulting distortions in the wavefront generate the fringe contours.

* L. Marton, J. Arol Simpson, and J. A. Suddeth, *Rev. Sci. Instr.* **25**, 1099 (1954), and *Phys. Rev.* **90**, 490 (1953).

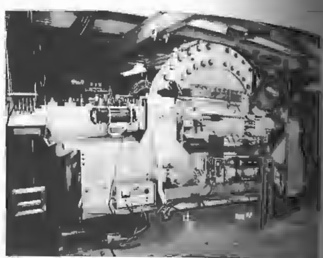


Figure 9.28 Scylla IV.

A particularly nice application is shown in Fig. 9.28, which is a photograph of the magnetic [illegible] device known as Scylla IV. It was used to study controlled thermonuclear reactions at the Los Alamos Scientific Laboratory. In this application the [illegible] Zehnder interferometer appears in the form of [illegible] parallelogram, as illustrated in Fig. 9.29. The two ruby laser *interferograms*, as these photographs are called, show (Fig. 9.30) the background pattern without a

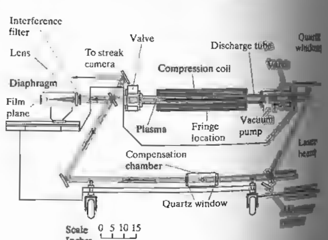
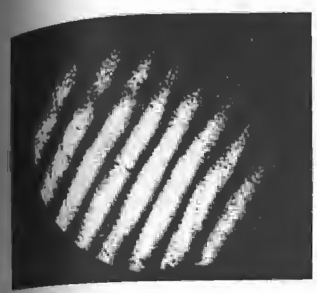


Figure 9.29 Schematic of Scylla IV.



[illegible]re 9.30 Interferogram without plasma.

Figure 9.31 Interferogram with plasma. (Photo courtesy Los Alamos Scientific Laboratory.)

[illegible] in the tube and the density contours within the [illegible] during a reaction (Fig. 9.31).

Another amplitude-splitting device, which differs [illegible] previous instrument in many respects, is the [illegible]erferometer. It is very easy to align and quite stable. An interesting application of the device is discussed in the last section of this chapter, where we consider its use as a gyroscope. One form of the Sagnac interferometer is shown in Fig. 9.32(a) and another in Fig. 9.32(b); still others are possible. Notice that the

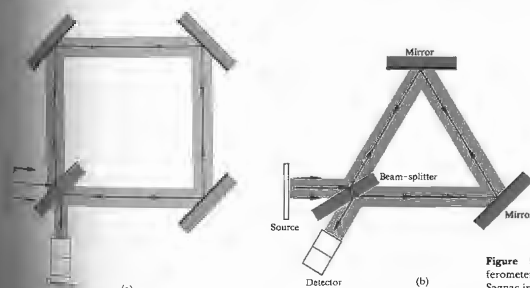


Figure 9.32 (a) A Sagnac interferometer. (b) Another variation of the Sagnac interferometer.

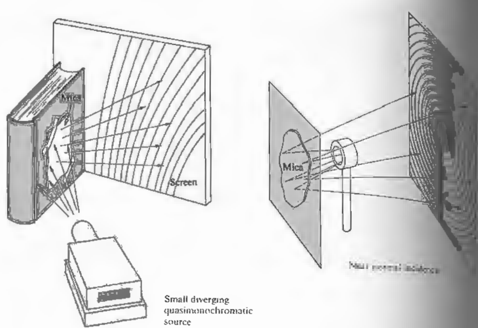


Figure 9.33 The Pohl interferometer.

main feature of the device is that there are two identical but oppositely directed paths taken by the beams and that both form closed loops before they are united to produce interference. A deliberate slight shift in the orientation of one of the mirrors will produce a path-length difference and a resulting fringe pattern. Since the beams are superimposed and therefore inseparable, the interferometer cannot be put to any of the conventional uses. These in general depend on the possibility of imposing variations on only one of the constituent beams.

Real Fringes

Before we examine the creation of real, as opposed to virtual, fringes, let's first consider another amplitude-splitting interferometric device, the **Pohl fringe-producing system**, illustrated in Fig. 9.33. It is simply a thin transparent film illuminated by the light coming from a point source. In this case, the fringes are real and can accordingly be intercepted on a screen placed anywhere in the vicinity of the interferometer without a condensing-lens system. A convenient light source to use is a mercury lamp covered with a shield having [illegible] small hole ($\approx\frac{1}{4}$ inch diameter) in it. As a thin film, [illegible] a piece of ordinary mica taped to a dark-colored bo[illegible] cover, which serves as an opaque backing. If yo[illegible] a laser, its remarkable coherence length and hi[illegible] density will allow you to perform this same [illegible] with almost anything smooth and transpa[illegible] the beam to about an inch or two in diamete[illegible] it through a lens (a focal length of 50 to [illegible] do). Then just reflect the beam off the surface [illegible] plate (e.g., a microscope slide), and the fring[illegible] evident within the illuminated disk whereve[illegible] strike[illegible] a screen.

The underlying physical principle involved with point-source illumination for all four [illegible] ferometric devices considered above can be [illegible] with the help of a construction, variations [illegible] shown in Figs. 9.34 and 9.35.* The two vertical [illegible] Fig. 9.34, or the inclined ones in Fig. 9.35, [illegible] either the positions of the mirrors or the two [illegible]

* A. Zajac, H. Sadowski, and S. Licht, "The Real Fri[illegible] and the Michelson Interferometers," *Am. J. Phys.* [illegible]

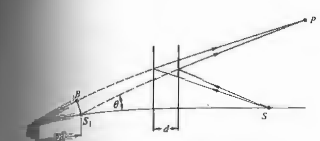


Figure 9.34 Point-source illumination of parallel surfaces.

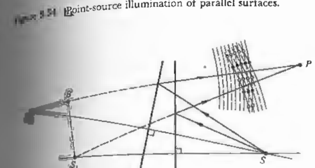


Figure 9.35 Point-source illumination of inclined surfaces.

[illegible] in the Pohl interferometer. Let's assume [illegible] P in the surrounding medium is a point at [illegible] is constructive interference. A screen placed [illegible] point would intercept this maximum, as well as [illegible] fringe pattern, without any condensing system. [illegible] erent virtual sources emitting the interfering [illegible] are mirror images S_1 and S_2 of the actual point [illegible] S. It should be noted that this kind of real fringe [illegible] can be observed with both the Michelson and [illegible] interferometers (Fig. 9.36). If either device is [illegible] ated with an expanded laserbeam, a real fringe pattern will be generated directly by the emerging [illegible] This is an extremely simple and beautiful [illegible]

9.5 [illegible] AND LOCALIZATION OF [illegible] FERENCE FRINGES

Often it [illegible] important to know where the fringes pro-[illegible] interferometric system will be located, since that is the region where we need to focus our detector (eye, camera, telescope). In general, the problem of locating fringes is characteristic of a given interferometer; that is, it has to be solved for each individual device.

Fringes can be classified, first, as either *real* or *virtual* and, second, as either *nonlocalized* or *localized*. Real fringes are those that can be seen on a screen without the use of an additional focusing system. The rays forming these fringes converge to the point of observation, all by themselves. Virtual fringes cannot be projected onto a screen without a focusing system. In this case the rays obviously do not converge.

Nonlocalized fringes are real and exist everywhere within an extended (three-dimensional) region of space. The pattern is literally nonlocalized, in that it is not restricted to some small region. Young's experiment, as illustrated in Fig. 9.5, fills the space beyond the secondary sources with a whole array of real fringes. Nonlocalized fringes of this sort are generally produced by small sources, that is, point or line sources, be they real or virtual. In contrast, localized fringes are clearly

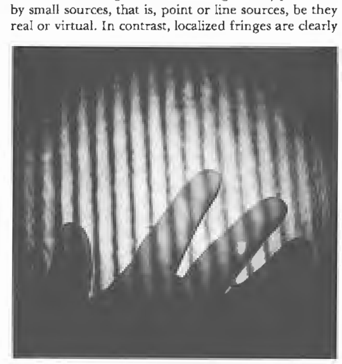


Figure 9.36 Real Michelson fringes using He–Ne laser light. (Photo by E. H.)

observable only over a particular surface. The pattern is literally localized, whether near a thin film or at infinity. This type of fringe will always result from the use of extended sources but can be generated with a point source as well.

The Pohl interferometer (Fig. 9.33) is particularly useful in illustrating these principles, since with a point source it will produce both real nonlocalized and virtual localized fringes. The real nonlocalized fringes (Fig. 9.37, upper half) can be intercepted on a screen almost anywhere in front of the mica film.

For the nonconverging rays, realize that since the aperture of the eye is quite small, it will intercept only those rays that are directed almost exactly at it. For this small pencil of rays, the eye, at a particular position, sees either a bright or dark spot but not much more.

To perceive an extended fringe pattern [redacted] parallel rays of the type shown in the [redacted] Fig. 9.37, a large lens will have to be [redacted] in light entering at other orientations[redacted] however, the source is usually somewhat [redacted] fringes can generally be seen by looking [redacted] with the eye focused at infinity. These [redacted] are localized at infinity and are equivalent[redacted] *inclination fringes* of Section 9.4. Similarly, [redacted] M_1 and M_2 in the Michelson interferometer[redacted] the usual circular, virtual, equal-inclina[redacted] localized at infinity will be seen. We can [redacted] air film between the surfaces of the mirrors [redacted] acting to generate these fringes. As with [redacted] ration of Fig. 9.37 for the Pohl device, real [redacted] fringes will also be present.

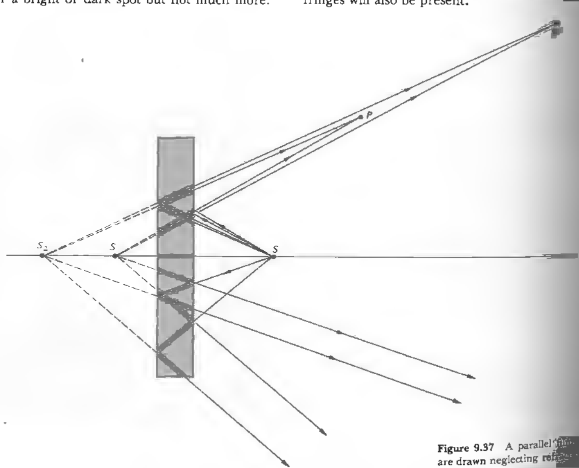


Figure 9.37 A parallel [redacted]he ray are drawn neglecting ref[redacted]

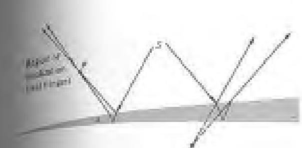


Figure 9.38 Fringes formed by a wedge-shaped film.

[redacted]metry of the fringe pattern seen in reflected [redacted]ransparent wedge of small angle α is shown [redacted] The fringe location P will be determined [redacted]ction of incidence of the incoming light. [redacted]ngs have this same kind of localization, as [redacted]helson, Sagnac, and other interferometers [redacted]e equivalent interference system consists of [redacted]g planes inclined slightly to each other. The [redacted]p of the Mach–Zehnder interferometer is [redacted]in that by rotating the mirrors, one can localize [redacted]sulting virtual fringes on any plane within the [redacted]enerally occupied by the test chamber (Fig. 9.39).

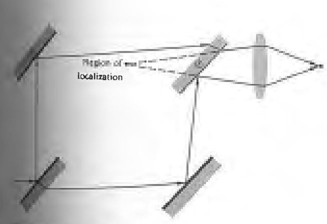


Figure 9.39 [redacted]inges in the Mach–Zehnder interferometer.

9.6 MULTIPLE-BEAM INTERFERENCE

Thus far we have examined a number of situations in which two coherent beams are combined under diverse conditions to produce interference patterns. There are, however, other circumstances under which a much larger number of mutually coherent waves are made to interfere. In fact, whenever the amplitude-reflection coefficients, the r's, for the parallel plate illustrated in Fig. 9.14 are not small, as was previously the case, the higher-order reflected waves $\mathbf{E}_{3r}$, $\mathbf{E}_{4r}$, ... become quite significant. A glass plate, slightly silvered on both sides so that the r's approach unity, will generate a large number of multiply internally reflected rays. For the moment, we will consider only situations in which the film, substrate, and surrounding medium are transparent dielectrics. This avoids the more complicated phase changes resulting from metal-coated surfaces.

To begin the analysis as simply as possible, let the film be nonabsorbing and let $n_1 = n_2$. The notation will be in accord with that of Section 4.5; in other words, the amplitude-transmission coefficients are represented by t, the fraction of the amplitude of a wave transmitted on entering into the film, and t', the fraction transmitted when a wave leaves the film. Keep in mind that the rays are actually lines drawn perpendicular to the wavefronts and therefore are also perpendicular to the optical fields $\mathbf{E}_{1r}$, $\mathbf{E}_{2r}$, and so forth. Since the rays will remain nearly parallel, the scalar theory will suffice as long as we are careful to account for any possible phase shifts. As shown in Fig. 9.40, the scalar amplitudes of the reflected waves $\mathbf{E}_{1r}$, $\mathbf{E}_{2r}$, $\mathbf{E}_{3r}$, ..., are respectively E_0r, $E_0tr't'$, $E_0tr'^3t'$, ..., where E_0 is the amplitude of the initial incoming wave and $r = -r'$ via Eq. (4.89). The minus sign indicates a phase shift, which we will consider later. Similarly, the transmitted waves $\mathbf{E}_{1t}$, $\mathbf{E}_{2t}$, $\mathbf{E}_{3t}$, ... will have amplitudes E_0tt', $E_0tr'^2t'$, $E_0tr'^4t'$, ... Consider the set of parallel reflected rays. Each ray bears a fixed phase relationship to all the other reflected rays. The phase differences arise from a combination of optical path-length differences and phase shifts occurring at the various reflections. Nonetheless, the waves are mutually coherent, and if they are collected and brought to focus at a point P by a lens, they will all interfere.

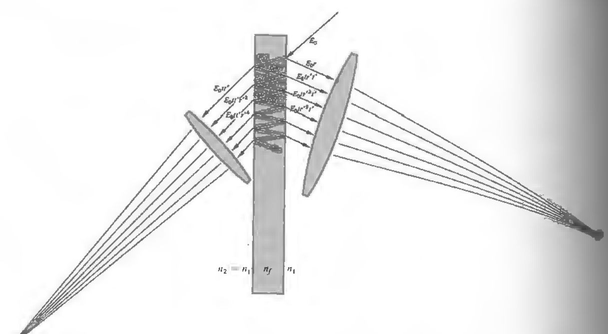


Figure 9.40 Multiple-beam interference from a [illegible]

The resultant irradiance expression has a particularly simple form for two special cases.

The difference in optical path length between adjacent rays is given by

$$\Lambda = 2n_f d \cos\theta_t. \qquad [9.33]$$

All the waves except for the first, $\mathbf{E}_{1r}$, undergo an odd number of reflections *within* the film. It follows from Fig. 4.25 that at each internal reflection the component of the field parallel to the plane of incidence changes phase by either 0 or π, depending on the internal incident angle, $\theta_i < \theta_c$. The component of the field perpendicular to the plane of incidence suffers no change in phase on internal reflection when $\theta_i < \theta_c$. Clearly then, no relative change in phase among these waves results from an odd number of such reflections (Fig. 9.41). As the *first special case*, if $\Lambda = m\lambda$, the second, third, fourth, and successive waves will all be in phase at P. The wave $\mathbf{E}_{1r}$, however, because of its reflection at the top surface of the film, will be out of phase by 180° with respect to all the other waves. The phase shift is embodied in the fact that $r = -r'$ and r' occurs only in odd powers. The sum of the scalar amplitudes, that is, the total *reflected amplitude* at point P, is then

$$E_{0r} = E_0 r - (E_0 t r t' + E_0 t r^3 t' + [illegible])$$

or

$$E_{0r} = E_0 r - E_0 t r t'(1 + r^2 + r^4 + \cdots),$$

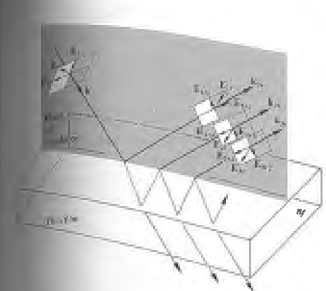
where since $\Lambda = m\lambda$, we've just replaced r' by [illegible]. The geometric series in parentheses converges to the finite sum $1/(1 - r^2)$ as long as $r^2 < 1$, so that

$$E_{0r} = E_0 r - \frac{E_0 t r t'}{(1 - r^2)}. \qquad (9.49)$$

It was shown in Section 4.5, when we consid[illegible] treatment of the principle of reversibility [illegible] that $tt' = 1 - r^2$, and it follows that

$$E_{0r} = 0.$$

Thus when $\Lambda = m\lambda$ the second, third, fourth, a[illegible] cessive waves exactly cancel the first reflected w[illegible] shown in Fig. 9.42. In this case no light is reflecte[illegible] the incoming energy is transmitted. The *secon*[illegible]



[illegible] Phase shifts arising purely from the reflections (internal [illegible]

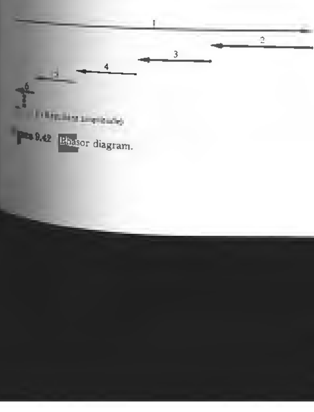
[illegible] when $\Lambda = (m + \frac{1}{2})\lambda$. Now the first and second [illegible] phase, and all other adjacent waves are $\lambda/2$ [illegible]phase; that is, the second is out of phase with [illegible], the third is out of phase with the fourth, and so on. The resultant *scalar amplitude* is then

$$E_{0r} = E_0 r + E_0 t r t' - E_0 t r^3 t' + E_0 t r^5 t' - \cdots$$

or

$$E_{0r} = E_0 r + E_0 r t t'(1 - r^2 + r^4 - \cdots).$$

[illegible] series in parentheses is equal to $1/(1 + r^2)$, in which



[illegible] 9.42 Phasor diagram.

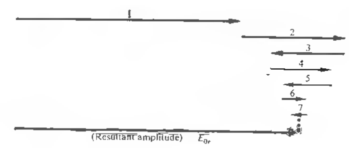


Figure 9.43 Phasor diagram.

case

$$E_{0r} = E_0 r\left[1 + \frac{tt'}{(1 + r^2)}\right].$$

Again, $tt' = 1 - r^2$; therefore, as illustrated in Fig. 9.43,

$$E_{0r} = \frac{2r}{(1 + r^2)} E_0.$$

Since this particular arrangement results in the addition of the first and second waves, which have relatively large amplitudes, it should yield a large reflected flux density. The irradiance is proportional to $E_{0r}^2/2$, so from Eq. (3.44)

$$I_r = \frac{4r^2}{(1 + r^2)^2}\left(\frac{E_0^2}{2}\right). \qquad (9.50)$$

That this is in fact the maximum, $(I_r)_{max}$, will be shown later.

We will now consider the problem of multiple-beam interference in a more general fashion, making use of the complex representation. Again let $n_1 = n_2$, thereby avoiding the need to introduce different reflection and transmission coefficients at each interface. The optical fields at point P are given by

$$E_{1r} = E_0 r e^{i\omega t}$$

$$E_{2r} = E_0 t r' t' e^{i(\omega t - \delta)}$$

$$E_{3r} = E_0 t r'^3 t' e^{i(\omega t - 2\delta)}$$

$$\vdots$$

$$E_{Nr} = E_0 t r'^{(2N-3)} t' e^{i[\omega t - (N-1)\delta]},$$

where $E_0 e^{i\omega t}$ is the incident wave.

The terms $\delta, 2\delta, \ldots, (N - 1)\delta$ are the contributions to the phase arising from an optical path-length difference between adjacent rays ($\delta = k_0\Lambda$). There is an additional phase contribution arising from the optical distance traversed in reaching point P, but this is common to each ray and has been omitted. The relative phase shift undergone by the first ray as a result of the reflection is embodied in the quantity r'. The resultant *reflected scalar wave* is then

$$E_r = E_{1r} + E_{2r} + E_{3r} + \cdots + E_{Nr},$$

or upon substitution (Fig. 9.44)

$$E_r = E_0 r e^{i\omega t} + E_0 t r' t' e^{i(\omega t - \delta)} + \cdots + E_0 t r'^{(2N-3)} t' \times e^{i[\omega t - (N-1)\delta]}.$$

This can be rewritten as

$$E_r = E_0 e^{i\omega t}\{r + r' t t' e^{-i\delta}[1 + (r'^2 e^{-i\delta}) + (r'^2 e^{-i\delta})^2 + \cdots + (r'^2 e^{-i\delta})^{N-2}]\}.$$

If $r'^2 e^{-i\delta} < 1$, and if the number of terms in the series approaches infinity, the series converges. The resultant wave becomes

$$E_r = E_0 e^{i\omega t}\left[r + \frac{r' t t' e^{-i\delta}}{1 - r'^2 e^{-i\delta}}\right]. \quad (9.51)$$

In the case of zero absorption, no energy being taken out of the waves, we can use the relations $r = -r'$ and $tt' = 1 - r^2$ to rewrite Eq. (9.51) as

$$E_r = E_0 e^{i\omega t}\left[\frac{r(1 - e^{-i\delta})}{1 - r^2 e^{-i\delta}}\right].$$

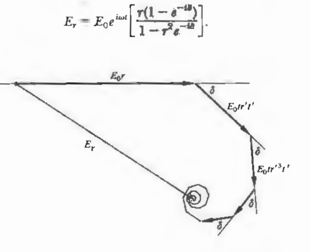


Figure 9.44 Phasor diagram.

The reflected flux density at P is then $I_r = E_r E_r^*/2$, that is,

$$I_r = \frac{E_0^2 r^2 (1 - e^{-i\delta})(1 - e^{+i\delta})}{2(1 - r^2 e^{-i\delta})(1 - r^2 e^{+i\delta})}$$

which can be transformed into

$$I_r = I_i \frac{2r^2(1 - \cos\delta)}{(1 + r^4) - 2r^2\cos\delta}. \quad (9.52)$$

The symbol $I_i = E_0^2/2$ represents the incident flux density, since, of course, E_0 was the ampli[illegible] incident wave. Similarly, the amplitudes of [illegible]ted waves given by

$$E_{1t} = E_0 t t' e^{i\omega t}$$
$$E_{2t} = E_0 t t' r'^2 e^{i(\omega t - \delta)}$$
$$E_{3t} = E_0 t t' r'^4 e^{i(\omega t - 2\delta)}$$
$$\vdots$$
$$E_{Nt} = E_0 t t' r'^{2(N-1)} e^{i[\omega t - (N-1)\delta]}$$

can be added to yield

$$E_t = E_0 e^{i\omega t}\left[\frac{tt'}{1 - r^2 e^{-i\delta}}\right]. \quad (9.53)$$

Multiplying this by its complex conjugate, we [illegible] (Problem 9.35) the irradiance of the transmitt[illegible]

$$I_t = \frac{I_i (tt')^2}{(1 + r^4) - 2r^2\cos\delta}. \quad (9.54)$$

Using the trigonometric identity $\cos\delta = 1 - 2\sin^2(\delta/2)$, Eqs. (9.52) and (9.54) become

$$I_r = I_i \frac{[2r/(1 - r^2)]^2 \sin^2(\delta/2)}{1 + [2r/(1 - r^2)]^2 \sin^2(\delta/2)} \quad (9.55)$$

and

$$I_t = I_i \frac{1}{1 + [2r/(1 - r^2)]^2 \sin^2(\delta/2)} \quad (9.56)$$

where energy is not absorbed, that is, $tt' + r^2 = 1$. If indeed none of the incident energy is abso[illegible] the flux density of the incoming wave should exa[illegible] the sum of the flux density reflected off the [illegible] the total transmitted flux density emerging [illegible] this film. It follows from Eqs. (9.55) and (9.56) [illegible] the case, namely,

$$I_i = I_r + I_t. \quad (9.57)$$

[illegible] be true, however, if the dielectric film is [illegible] thin layer of semitransparent metal. Sur[illegible] induced in the metal will dissipate a por[illegible]cident electromagnetic energy (see Section [illegible]

[illegible]ider the transmitted waves as described by Eq. (9.54). [illegible]aximum will exist when the denominator is [illegible] as possible, that is, when $\cos\delta = 1$, in which case [illegible] $2\pi m$ and

$$(I_t)_{max} = I_i.$$

Under these conditions Eq. (9.52) indicates that

$$(I_r)_{min} = 0,$$

[illegible] expect from Eq. (9.57). Again, from Eq. [illegible]ar that a minimum transmitted flux density [illegible] when the denominator is a maximum, that is, when $\cos\delta = -1$. In that case $\delta = (2m + 1)\pi$ and

$$(I_t)_{min} = I_i \frac{(1 - r^2)^2}{(1 + r^2)^2}. \quad (9.58)$$

The [illegible]esponding maximum in the reflected flux density is

$$(I_r)_{max} = I_i \frac{4r^2}{(1 + r^2)^2}. \quad (9.59)$$

Notice that the constant-inclination fringe pattern has [illegible] maxima when $\delta = (2m + 1)\pi$ or

$$\frac{4\pi n_f}{\lambda_0} d\cos\theta_t = (2m + 1)\pi,$$

which is the same as the result we arrived at previously, [illegible], by using only the first two reflected waves. [illegible] that Eq. (9.59) verifies that Eq. (9.50) was [illegible] a maximum.

[illegible]m of Eqs. (9.55) and (9.56) suggests that we [illegible] a new quantity, the *coefficient of finesse F*, such

$$F = \left(\frac{2r}{1 - r^2}\right)^2, \quad (9.60)$$

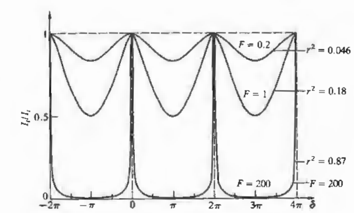


Figure 9.45 Airy function.

whereupon these equations can be written as

$$\frac{I_r}{I_i} = \frac{F\sin^2(\delta/2)}{1 + F\sin^2(\delta/2)} \quad (9.61)$$

and

$$\frac{I_t}{I_i} = \frac{1}{1 + F\sin^2(\delta/2)}. \quad (9.62)$$

The term $[1 + F\sin^2(\delta/2)]^{-1} \equiv \mathcal{A}(\theta)$ is known as the Airy function. It represents the transmitted flux density distribution and is plotted in Fig. 9.45. The complementary function $[1 - \mathcal{A}(\theta)]$, that is, Eq. (9.61), is plotted as well, in Fig. 9.46. When $\delta/2 = m\pi$ the Airy function is equal to unity for all values of F and therefore r. When r approaches 1, the transmitted flux density is very small, except within the sharp spikes centered about

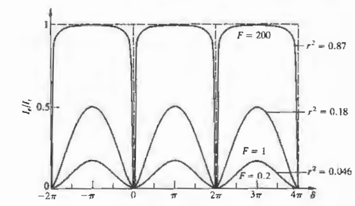


Figure 9.46 One minus the Airy function.

the points $\delta/2 = m\pi$. Multiple-beam interference has resulted in a redistribution of the energy density in comparison to the sinusoidal two-beam pattern (of which the curves corresponding to a small reflectance are reminiscent). This effect will be further demonstrated when we consider the diffraction grating. At that time we will clearly see this same peaking effect, resulting from an increased number of coherent sources contributing to the interference pattern. Remember that the Airy function is, in fact, a function of θ_i or θ_t by way of its dependence on δ, which follows from Eqs. (9.34) and (9.35), ergo the notation $\mathscr{A}(\theta)$. Each spike in the flux-density curve corresponds to a particular δ and therefore a particular θ_t. For a plane-parallel plate, the fringes, in transmitted light, will consist of a series of narrow bright rings on an almost completely dark background. In reflected light, the fringes will be narrow and dark on an almost uniformly bright background.

Constant-thickness fringes can also be made sharp and narrow by applying a light silver coating to the relevant reflecting surfaces to produce multiple-beam interference. This procedure has a number of practical applications, one of which will be discussed in Section 9.8.2, when we consider the use of multiple-beam Fizeau fringes to examine surface topography.

9.6.1 The Fabry–Perot Interferometer

The multiple-beam interferometer, first constructed by Charles Fabry and Alfred Perot in the late 1800s, is of considerable importance in modern optics. Besides being a spectroscopic device of extremely high resolving power, it serves as the basic laser resonant cavity. In principle, the device consists of two plane, parallel, highly reflecting surfaces separated by some distance d. This is the simplest configuration, and as we shall see, other forms are also widely in use. In practice, two semisilvered or aluminized glass optical flats form the reflecting boundary surfaces. The enclosed air gap generally ranges from several millimeters to several centimeters when the apparatus is used interferometrically, and often to considerably greater lengths when it serves as a laser resonant cavity. If the gap can be mechanically varied by moving one of the mirrors, it's an interferometer. When the mirrors a[redacted] and adjusted for parallelism by screwing [redacted] sort of spacer (invar or quartz is common[redacted] used), it's said to be an *etalon* (although it is, of course, still an interferometer in the broad sense). Indeed [redacted] surfaces of a single quartz plate are appro[redacted] ished and silvered, it too will serve as an eta[redacted] need not be air. The unsilvered sides of th[redacted] often made to have a slight wedge shape (a [redacted] of arc) to reduce the interference pattern aris[redacted] reflections off these sides. The etalon in Fig[redacted] shown illuminated by a broad source, which might be a mercury arc or a He–Ne laser beam spread out [redacted] diameter to several centimeters. This can be do[redacted] nicely by sending the beam into the back end of a telescope focused at infinity. The light can the[redacted] diffuse by passing it through a sheet of gro[redacted] Only one ray emitted from some point S_1 on[redacted] is traced through the etalon. Entering by [redacted] partially silvered plate, it is multiply reflec[redacted] the gap. The transmitted rays are collec[redacted] and brought to a focus on a screen, where [redacted] to form either a bright or dark spot. [redacted] particular plane of incidence, which contain[redacted] all the reflected rays. Any other ray emitted from a different point S_2, parallel to the original ray and in [redacted] plane of incidence, will form a spot at the same [redacted] the screen. As we shall see, the discussion of [redacted] section is again applicable, so that Eq. (9.54) [redacted] the transmitted flux density I_t. The m[redacted] generated in the cavity, arriving at P from [redacted] S_2, are coherent among themselves. But the [redacted]

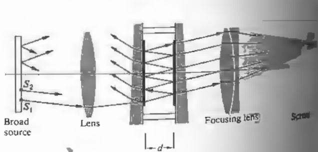
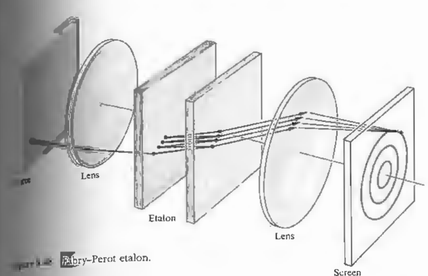


Figure 9.47 Fabry–Perot etalon.



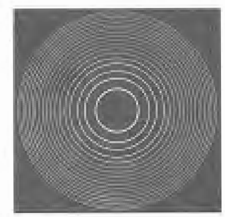


Figure 9.48 [redacted]bry–Perot etalon.

[redacted] completely incoherent with respect to those [redacted] that there is no sustained mutual interference [redacted] contribution to the irradiance I_t at P is just the sum of the two irradiance contributions.

[redacted] incident on the gap at a given angle will [redacted] single circular fringe of uniform irradiance [redacted] With a broad diffuse source, the interference [illegible] will be narrow concentric rings, corresponding [redacted]tiple-beam transmission pattern.

[redacted] system can be observed visually by looking [redacted] the etalon, while focusing at infinity. The [redacted]cusing lens, which is no longer needed, is done by the eye. At large values of d, the rings will be [redacted] together, and a telescope might be needed [redacted]gnify the pattern. A relatively inexpensive mon[redacted] will serve the same purpose and will allow [illegible]tographing the fringes localized at infinity. As [illegible] be expected from the considerations of Section [illegible] it is possible to produce real nonlocalized fringes [illegible] bright point source.

The partially transparent metal films that are often used to increase the reflectance ($R = r^2$) will absorb a fraction A of the flux density; this fraction is referred to as the absorptance.

The expression

$$tt' + r^2 = 1$$

or

$$T + R = 1, \qquad (9.60)$$

where T is the transmittance, must now be rewritten as

$$T + R + A = 1. \qquad (9.63)$$

One further complication introduced by the metallic films is an additional phase shift $\phi(\theta_i)$, which can differ from either zero or π. The phase difference between two successively transmitted waves is then

$$\delta = \frac{4\pi n_f}{\lambda_0} d \cos\theta_t + 2\phi. \qquad (9.64)$$

For the present conditions, θ_t is small and ϕ may be considered to be constant. In general, d is so large, and λ_0 so small, that ϕ can be neglected. We can now express Eq. (9.54) as

$$\frac{I_t}{I_i} = \frac{T^2}{1 + R^2 - 2R\cos\delta},$$

or equivalently

$$\frac{I_t}{I_i} = \left(\frac{T}{1-R}\right)^2 \frac{1}{1 + [4R/(1-R)^2]\sin^2(\delta/2)}. \qquad (9.65)$$

Making use of Eq. (9.63) and the definition of the Airy function, we obtain

$$\frac{I_t}{I_i} = \left[1 - \frac{A}{(1-R)}\right]^2 \mathscr{A}(\theta), \qquad (9.66)$$

as compared with the equation for zero absorption

$$\frac{I_t}{I_i} = \mathscr{A}(\theta). \qquad [9.62]$$

Inasmuch as the absorbed portion A is never zero, the transmitted flux-density maxima $(I_t)_{max}$ will always be somewhat less than I_i. [Recall that for $(I_t)_{max}$, $\mathscr{A}(\theta) = 1$.]

Accordingly, the *peak transmission* is defined as $(I_t/I_i)_{max}$:

$$\frac{(I_t)_{max}}{I_i} = \left[1 - \frac{A}{(1-R)}\right]^2. \qquad (9.67)$$

A silver film 50 nm thick would be approaching its maximum value of R (e.g., about 0.94), while T and A might be, respectively, 0.01 and 0.05. In this case, the peak transmission will be down to $\frac{1}{36}$. The relative irradiance of the fringe pattern will still be determined by the Airy function, since

$$\frac{I_t}{(I_t)_{max}} = \mathscr{A}(\theta). \qquad (9.68)$$

A measure of the sharpness of the fringes, that is, how rapidly the irradiance drops off on either side of the maximum, is given by the half-width γ. Shown in

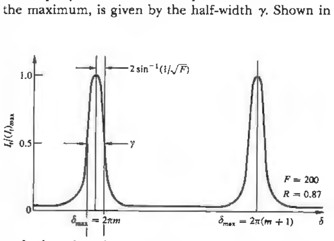


Figure 9.49 Fabry–Perot fringes.

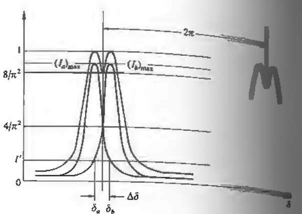


Figure 9.50 Overlapping fringes.

Fig. 9.49, γ is the width of the peak, in radian[redacted] when $I_t = (I_t)_{max}/2$.

Peaks in the transmission occur at specific [redacted]es of the phase difference $\delta_{max} = 2\pi m$. Accordi[redacted] the irradiance will drop to half its maximum va[redacted] (i.e., $\mathscr{A}(\theta) = \frac{1}{2}$) whenever $\delta = \delta_{max} \pm \delta_{1/2}$. Inasmuch[redacted]

$$\mathscr{A}(\theta) = [1 + F\sin^2(\delta/2)]^{-1},$$

then when

$$[1 + F\sin^2(\delta_{1/2}/2)]^{-1} = \tfrac{1}{2}$$

it follows that

$$\delta_{1/2} = 2\sin^{-1}(1/\sqrt{F}).$$

Since F is generally rather large, $\sin^{-1}(1/\sqrt{F}$[redacted] $\sqrt{F}$ and therefore the half-width, $\gamma = 2\delta_{1/2}$, be[redacted]

$$\gamma = 4/\sqrt{F}. \qquad (9.6$$

Recall that $F = 4R/(1-R)^2$, so that the large[redacted] is, the sharper the transmission peaks will be.

Another quantity of particular interest is[redacted] the separation of adjacent maxima to the [redacted] Known as the **finesse**, $\mathscr{F} = 2\pi/\gamma$ or, from Eq. (9.69),

$$\mathscr{F} = \frac{\pi\sqrt{F}}{2}. \qquad (9.7$$

Over the visible spectrum, the finesse of most ordinary Fabry–Perot instruments is about 30. The phys[redacted] tation on $\mathscr{F}$ is set by deviations in the mirro[redacted]

[redacted]allelism. Keep in mind that as the finesse [redacted] the half-width decreases, but so too does the [redacted]mission. Incidentally, finesse of about 1000 [redacted] curved-mirror systems using dielectric [redacted]ings.*

[redacted] Spectroscopy

[redacted]Perot interferometer is frequently used to [redacted] detailed structure of spectral lines. We will [redacted] a complete treatment of interference spec- [redacted] but rather will define the relevant ter- [redacted] briefly outlining appropriate derivations.† [redacted] have seen, a hypothetical, purely monochro- [redacted]matic [redacted]htwave generates a particular circular fringe [redacted] But δ is a function of λ_0, so that if the source [redacted]up of two such monochromatic components, [redacted]posed ring systems would result. When the [redacted] fringes partially overlap, a certain amount [redacted] exists in deciding when the two systems [redacted]vidually discernible, that is, when they are said [redacted] Lord Rayleigh's‡ criterion for resolving two [redacted]-irradiance overlapping slit images is well [redacted] if somewhat arbitrarily in the present [redacted] Its use, however, will allow a comparison [redacted] grating instruments. The essential feature [redacted]on is that the fringes are *just resolvable* when [redacted]ed irradiance of both fringes at the center, saddle point, of the resultant broad fringe is $8/\pi^2$ [redacted]maximum irradiance. This simply means that [redacted] see a broad bright fringe with a grey central region. [redacted] a bit more analytic about it, examine Fig. [redacted]ping in mind the previous derivation of the [redacted]h. Consider the case in which the two con- [redacted]ges have equal irradiances, $(I_a)_{max} = (I_b)_{max}$.

[redacted]ltiple Beam Interferometry," by H. D. Polster, *Appl.* [redacted] should be of interest. Also look at "The Optical [redacted] Abraham, C. Seaton, and S. Smith, *Sci. Am.* (Feb. [redacted] a discussion of the use of the Fabry–Perot inter- [redacted] optical transistor.

[redacted]plete treatment can be found in Born and Wolf, *Prin-* [redacted], and in W. E. Williams, *Applications of Interferometry,* [redacted]

[redacted] be reconsidered with respect to diffraction in the [redacted]Fig. 10.40).

The peaks in the resultant, occurring at $\delta = \delta_a$ and $\delta = \delta_b$, will have equal irradiances,

$$(I_t)_{max} = (I_a)_{max} + I'. \qquad (9.71)$$

At the saddle point, the irradiance, $(8/\pi^2)(I_t)_{max}$, is the sum of the two constituent irradiances, so that, recalling Eq. (9.68),

$$(8/\pi^2)\frac{(I_t)_{max}}{(I_a)_{max}} = [\mathscr{A}(\theta)]_{\delta=\delta_a+\Delta\delta/2} + [\mathscr{A}(\theta)]_{\delta=\delta_b+\Delta\delta/2}. \qquad (9.72)$$

Using $(I_t)_{max}$ given by Eq. (9.71), along with the fact that

$$\frac{I'}{(I_a)_{max}} = [\mathscr{A}(\theta)]_{\delta=\delta_a+\Delta\delta},$$

we can solve Eq. (9.72) for $\Delta\delta$. For large values of F,

$$(\Delta\delta) \approx \frac{4.2}{\sqrt{F}}. \qquad (9.73)$$

This then represents the smallest phase increment, $(\Delta\delta)_{min}$, separating two resolvable fringes. It can be related to equivalent minimum increments in wavelength $(\Delta\lambda_0)_{min}$, frequency $(\Delta\nu)_{min}$, and wave number $(\Delta\kappa)_{min}$. From Eq. (9.64), for $\delta = 2\pi m$, we have

$$m\lambda_0 = 2n_f d\cos\theta_t + \frac{\phi\lambda_0}{\pi}. \qquad (9.74)$$

Dropping the term $\phi\lambda_0/\pi$, which is clearly negligible, and then differentiating, yields

$$m(\Delta\lambda_0) + \lambda_0(\Delta m) = 0$$

or

$$\frac{\lambda_0}{(\Delta\lambda_0)} = -\frac{m}{(\Delta m)}.$$

The minus will be omitted, since it means only that the order increases when λ_0 decreases. When δ changes by 2π, m changes by 1, so

$$\frac{2\pi}{(\Delta\delta)} = \frac{1}{(\Delta m)}$$

and thus

$$\frac{\lambda_0}{(\Delta\lambda_0)} = \frac{2\pi m}{(\Delta\delta)}. \qquad (9.75)$$

The ratio of λ_0 to the least resolvable wavelength difference, $(\Delta\lambda_0)_{min}$, is known as the **chromatic resolving power** $\mathcal{R}$ of any spectroscope. At nearly normal incidence

$$\mathcal{R} \equiv \frac{\lambda_0}{(\Delta\lambda_0)_{min}} \approx \mathcal{F}\frac{2n_f d}{\lambda_0} \tag{9.76}$$

or

$$\mathcal{R} \approx \mathcal{F}m.$$

For a wavelength of 500 nm, $n_f d = 10$ mm, and $R = 90\%$, the resolving power is well over a million, a range only recently achieved by the finest diffraction gratings. It follows as well, in this example, that $(\Delta\lambda_0)_{min}$ is less than a millionth of λ_0. In terms of frequency, the *minimum resolvable bandwidth* is

$$(\Delta\nu)_{min} = \frac{c}{\mathcal{F}2n_f d}, \tag{9.77}$$

inasmuch as $|\Delta\nu| = |c\Delta\lambda_0/\lambda_0^2|$.

As the two components present in the source become increasingly different in wavelength, the peaks shown overlapping in Fig. 9.50 separate. As the wavelength difference increases, the mth-order fringe for one wavelength λ_0 will approach the $(m+1)$th-order for the other wavelength $(\lambda_0 - \Delta\lambda_0)$. The particular wavelength difference at which overlapping takes place, $(\Delta\lambda_0)_{fsr}$, is known as the **free spectral range**. From Eq. (9.75), a change in δ of 2π corresponds to $(\Delta\lambda_0)_{fsr} = \lambda_0/m$, or at near normal incidence,

$$(\Delta\lambda_0)_{fsr} \approx \lambda_0^2/2n_f d, \tag{9.78}$$

and similarly

$$(\Delta\nu)_{fsr} \approx c/2n_f d. \tag{9.79}$$

Continuing with the above example (i.e., $\lambda_0 = 500$ nm and $n_f d = 10$ mm), $(\Delta\lambda_0)_{fsr} = 0.0125$ nm. Clearly, if we attempt to increase the resolving power by merely increasing d, the free spectral range will decrease, bringing with it the resulting confusion from the overlapping of orders. What is needed is that $(\Delta\lambda_0)_{min}$ *be as small as possible and* $(\Delta\lambda_0)_{fsr}$ *be as large as possible.* But lo and behold,

$$\frac{(\Delta\lambda_0)_{fsr}}{(\Delta\lambda_0)_{min}} = \mathcal{F}. \tag{9.80}$$

This result should not be too surprising [illegible] view of the original definition of $\mathcal{F}$.

Both the applications and configurati[illegible] of the Fabry–Perot interferometer are nume[illegible] Etalons have been arranged in series with [illegible] as well as with grating and prism spect[illegible] multilayer dielectric films have been used [illegible] metallic mirror coatings.

Scanning techniques are now widely [illegible] take advantage of the superior linearity [illegible] detectors over photographic plates, to [illegible] reliable flux-density measurements. The basi[illegible] *central-spot scanning* is illustrated in Fig. 9.51 [illegible] is accomplished by varying δ, by changing [illegible] than cos θ_t. In some arrangements, n_f is s[illegible] by altering the air pressure within the etal[illegible] tively, mechanical vibration of one mirror with a di[illegible] placement of $\lambda_0/2$ will be enough to scan [illegible] tral range, corresponding as it does to $\Delta\delta$ [illegible] lar technique for accomplishing this utilize[illegible] tric mirror mount. This kind of material [illegible] length, and therefore d, as a voltage is applied to it. The voltage profile determines the mirror motion.

Instead of photographically recording [illegible] radiance over a large region in space, at a single po[illegible] in time, this method records irradiance over a large region in time, at a single point in space.

The actual configuration of the etalon itself has [illegible] undergone some significant variations. Pierre Connes in 1956 first described the *spherical-mirror* [illegible] *interferometer.* Since then, curved-mirror systems have become prominent as laser cavities and are [illegible] increasing use as spectrum analyzers.

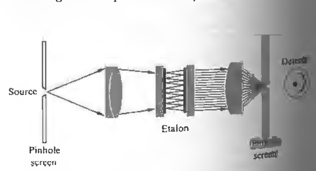
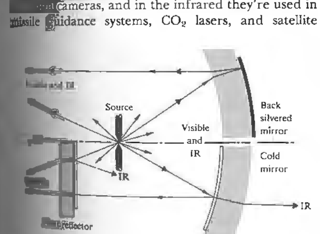


Figure 9.51 Central spot scanning.

9.7 [illegible]LICATIONS OF SINGLE AND [illegible]ULTILAYER FILMS

[illegible]ses to which coatings of thin dielectric films [illegible] in recent times are many indeed. Coatings [illegible] unwanted reflections off a diversity of sur[illegible] showcase glass to high-quality camera lenses, [illegible]monplace. Multilayer, nonabsorbing beam[illegible] and *dichroic* mirrors (color-selective beam-split[illegible] transmit and reflect particular wavelengths) [illegible] purchased commercially. Figure 9.52 is a seg[illegible] diagram illustrating the use of a *cold mirror* in [illegible] with a *heat reflector* to channel infrared [illegible] the rear of a motion-picture projector. The intense [illegible]wanted infrared radiation emitted by the [illegible] is [illegible] from the beam to avoid heating [illegible] the photographic film. The top half of Fig. [illegible]dinary back-silvered mirror shown for com[illegible] [illegible]ar cells, which are one of the prime power[illegible] systems for space vehicles, and even the astro[illegible] helmets and visors, are shielded with similar heat control coverings. Multilayer broad and narrow [illegible] filters, ones that transmit only over a specific [illegible]nge, can be made to span the region from [illegible] ultraviolet. In the visible, for example, they [illegible]portant part in splitting up the image in color [illegible] cameras, and in the infrared they're used in missile guidance systems, CO_2 lasers, and satellite horizon sensors. The applications of thin-film devices are manifold, as are their structures, which extend from the simplest single coatings to intricate arrangements of 100 or more layers.



[illegible] A composite drawing showing an ordinary system in [illegible] and a coated one in the bottom.

The treatment of multilayer film theory used here will deal with the *total* electric and magnetic fields and their boundary conditions in the various regions. This is a far more practical approach for many-layered systems than is the multiple-wave technique used earlier.*

9.7.1 Mathematical Treatment

Consider the linearly polarized wave shown in Fig. 9.53, impinging on a thin dielectric film between two semi-infinite transparent media. In practice, this might correspond to a dielectric layer a fraction of a wavelength thick, deposited on the surface of a lens, a mirror, or a prism. One point must be made clear at the outset: each wave $E_{r\text{I}}$, $E'_{r\text{II}}$, $E_{t\text{II}}$, and so forth, represents the resultant of all possible waves traveling in that direction, at that point in the medium. The summation process is therefore built in. As discussed in Section 4.3.2, the boundary conditions require that the tangential components of both the electric (**E**) and magnetic ($\mathbf{H} = \mathbf{B}/\mu$) fields be continuous across the boundaries (i.e., equal on both sides). At boundary I

$$E_\text{I} = E_{i\text{I}} + E_{r\text{I}} = E_{t\text{I}} + E'_{r\text{II}} \tag{9.81}$$

and

$$H_\text{I} = \sqrt{\frac{\epsilon_0}{\mu_0}}(E_{i\text{I}} - E_{r\text{I}})n_0 \cos\theta_{i\text{I}}$$
$$= \sqrt{\frac{\epsilon_0}{\mu_0}}(E_{t\text{I}} - E'_{r\text{II}})n_1 \cos\theta_{i\text{II}}, \tag{9.82}$$

where use is made of the fact that **E** and **H** in nonmagnetic media are related through the index of refraction and the unit propagation vector:

$$\mathbf{H} = \sqrt{\frac{\epsilon_0}{\mu_0}}\, n\hat{\mathbf{k}} \times \mathbf{E}.$$

* For a very readable nonmathematical discussion, see P. Baumeister and G. Pincus, "Optical Interference Coatings," *Sci. Amer.* **223**, 59 (December 1970).

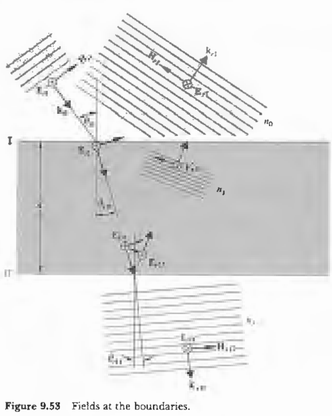


Figure 9.53 Fields at the boundaries.

At boundary II

$$E_{II} = E_{iII} + E_{rII} = E_{tII} \tag{9.83}$$

and

$$H_{II} = \sqrt{\frac{\epsilon_0}{\mu_0}}(E_{iII} - E_{rII})n_1 \cos\theta_{iII}$$

$$= \sqrt{\frac{\epsilon_0}{\mu_0}} E_{tII} n_s \cos\theta_{tII}, \tag{9.84}$$

the substrate having an index n_s. In accord with Eq. (9.33), a wave that traverses the film once undergoes a shift in phase of $k_0(2n_1 d\cos\theta_{iII})/2$, which will be denoted by k_0h, so that

$$E_{iII} = E_{tI} e^{-ik_0h} \tag{9.85}$$

and

$$E_{rII} = E'_{rII} e^{+ik_0h} \tag{9.86}$$

Equations (9.83) and (9.84) can now [illegible] as

$$E_{II} = E_{tI} e^{-ik_0h} + E'_{rII} e^{+ik_0h} \tag{9.87}$$

and

$$H_{II} = (E_{tI} e^{-ik_0h} - E_{rII} e^{+ik_0h})\sqrt{\frac{\epsilon_0}{\mu_0}}\, [illegible] \tag{9.88}$$

These last two equations can be solved for [illegible] which when substituted into Eqs. (9.81) and [illegible]

$$E_I = E_{II}\cos k_0h + H_{II}(i \sin [illegible]) \tag{9.89}$$

and

$$H_I = E_{II} Y_1 i \sin k_0h + H_{II}\cos k_0h \tag{9.90}$$

where

$$Y_1 = \sqrt{\frac{\epsilon_0}{\mu_0}}\, n_1 \cos\theta_{iII}.$$

When **E** is in the plane of incidence the [illegible] tions result in similar equations, provided [illegible]

$$Y_1 = \sqrt{\frac{\epsilon_0}{\mu_0}}\, n_1/\cos\theta_{iII}.$$

In matrix notation, the above linear [illegible] form

$$\begin{bmatrix} E_I \\ H_I \end{bmatrix} = \begin{bmatrix} \cos k_0h & (i \sin k_0h)/Y_1 \\ Y_1 i \sin k_0h & \cos k_0h \end{bmatrix} \begin{bmatrix} E_{II} \\ H_{II} \end{bmatrix} \tag{9.91}$$

or

$$\begin{bmatrix} E_I \\ H_I \end{bmatrix} = \mathcal{M}_I \begin{bmatrix} E_{II} \\ H_{II} \end{bmatrix}. \tag{9.92}$$

The *characteristic matrix* $\mathcal{M}_I$ relates the [illegible] two adjacent boundaries. It follows, [illegible] if two overlaying films are deposited on the [illegible] there will be three boundaries or interfaces, and now

$$\begin{bmatrix} E_{II} \\ H_{II} \end{bmatrix} = \mathcal{M}_{II} \begin{bmatrix} E_{III} \\ H_{III} \end{bmatrix}. \tag{9.93}$$

Multiplying both sides of this expression by $\mathcal{M}_I$, we obtain

$$\begin{bmatrix} E_I \\ H_I \end{bmatrix} = \mathcal{M}_I \mathcal{M}_{II} \begin{bmatrix} E_{III} \\ H_{III} \end{bmatrix}. \tag{9.94}$$

[illegible]eral, if p is the number of layers, each with a [illegible]ar value of n and h, then the first and the last [illegible] are related by

$$\begin{bmatrix} E_I \\ H_I \end{bmatrix} = \mathcal{M}_I \mathcal{M}_{II} \cdots \mathcal{M}_p \begin{bmatrix} E_{(p+1)} \\ H_{(p+1)} \end{bmatrix}. \tag{9.95}$$

[illegible] matrix of the entire system is the [illegible] the product (in the proper sequence) of the [illegible] 2 × 2 matrices, that is,

$$\mathcal{M} = \mathcal{M}_I \mathcal{M}_{II} \cdots \mathcal{M}_p = \begin{bmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{bmatrix}. \tag{9.96}$$

[illegible] see how all this fits together, we will derive [illegible]ions for the amplitude coefficients of reflection [illegible]ansmission using the above scheme. By reformu- [illegible] Eq. (9.92) in terms of the boundary conditions [illegible] and (9.84)] and setting

$$Y_0 = \sqrt{\frac{\epsilon_0}{\mu_0}}\, n_0 \cos\theta_{iI}$$

and

$$Y_s = \sqrt{\frac{\epsilon_0}{\mu_0}}\, n_s \cos\theta_{tII},$$

[illegible]

$$\begin{bmatrix} (E_{iI} + E_{rI}) \\ (E_{iI} - E_{rI})Y_0 \end{bmatrix} = \mathcal{M}_I \begin{bmatrix} E_{tII} \\ E_{tII} Y_s \end{bmatrix}.$$

When the matrices are expanded, the last relation [illegible]

$$1 + r = m_{11}t + m_{12}Y_s t$$

and

$$(1 - r)Y_0 = m_{21}t + m_{22}Y_s t,$$

[illegible]

$$r = E_{rI}/E_{iI} \quad \text{and} \quad t = E_{tII}/E_{iI}.$$

[illegible]

$$[illegible]\, \frac{[illegible]m_{11} + Y_0Y_s m_{12} - m_{21} - Y_s m_{22}}{[illegible]m_{11} + Y_0Y_s m_{12} + m_{21} + Y_s m_{22}} \tag{9.97}$$

and

$$t = \frac{2Y_0}{[illegible]m_{11} + Y_0Y_s m_{12} + m_{21} + Y_s m_{22}}. \tag{9.98}$$

To find either r or t for any configuration of films, we need only compute the characteristic matrices for each film, multiply them, and then substitute the resulting matrix elements into the above equations.

9.7.2 Antireflection Coatings

Now consider the extremely important case of normal incidence, that is,

$$\theta_{iI} = \theta_{iII} = \theta_{tII} = 0,$$

which in addition to being the simplest, is also quite frequently approximated in practical situations. If we put a subscript on r to indicate the number of layers present, the reflection coefficient for a single film becomes

$$r_1 = \frac{n_1(n_0 - n_s)\cos k_0h + i(n_0n_s - n_1^2)\sin k_0h}{n_1(n_0 + n_s)\cos k_0h + i(n_0n_s + n_1^2)\sin k_0h}. \tag{9.99}$$

Multiplying r_1 by its complex conjugate leads to the reflectance

$$R_1 = \frac{n_1^2(n_0 - n_s)^2\cos^2 k_0h + (n_0n_s - n_1^2)^2\sin^2 k_0h}{n_1^2(n_0 + n_s)^2\cos^2 k_0h + (n_0n_s + n_1^2)^2\sin^2 k_0h}. \tag{9.100}$$

This formula becomes particularly simple when $k_0h = \frac{1}{2}\pi$, which is equivalent to saying that the optical thickness h of the film is an odd multiple of $\frac{1}{4}\lambda_0$. In this case $d = \frac{1}{4}\lambda_f$, and

$$R_1 = \frac{(n_0n_s - n_1^2)^2}{(n_0n_s + n_1^2)^2}, \tag{9.101}$$

which, quite remarkably, will equal zero when

$$n_1^2 = n_0n_s. \tag{9.102}$$

Generally, d is chosen so that h equals $\frac{1}{4}\lambda_0$ in the yellow-green portion of the visible spectrum, where the eye is most sensitive. Cryolite (n = 1.35), a sodium aluminum fluoride compound, and magnesium fluoride (n = 1.38) are common low-index films. Since MgF_2 is by far the more durable, it is used more frequently. On a glass substrate, ($n_s \approx 1.5$), both these films have indices that are still somewhat too large to satisfy Eq. (9.102). Nonetheless, a single $\frac{1}{4}\lambda_0$ layer of MgF_2 will reduce the reflectance of glass from about 4% to a bit more than 1%, over the visible spectrum. It is now common practice to apply antireflection coatings to the elements of optical instruments. On camera lenses, such coatings produce a decrease in the haziness caused by stray internally scattered light, as well as a marked increase in image brightness. At wavelengths on either side of the central yellow-green region, R increases and the lens surface will appear blue-red in reflected light.

For a double-layer, quarter-wavelength antireflection coating,

$$\mathcal{M} = \mathcal{M}_{I}\mathcal{M}_{II}$$

or more specifically

$$\mathcal{M} = \begin{bmatrix} 0 & i/Y_1 \\ iY_1 & 0 \end{bmatrix}\begin{bmatrix} 0 & i/Y_2 \\ iY_2 & 0 \end{bmatrix} \qquad (9.103)$$

At normal incidence this becomes

$$\mathcal{M} = \begin{bmatrix} -n_2/n_1 & 0 \\ 0 & -n_1/n_2 \end{bmatrix}. \qquad (9.104)$$

Substituting the appropriate matrix elements into Eq. (9.97), yields r_2, which, when squared, leads to the reflectance

$$R_2 = \left[\frac{n_2^2 n_0 - n_s n_1^2}{n_2^2 n_0 + n_s n_1^2}\right]^2. \qquad (9.105)$$

For R_2 to be exactly zero at a particular wavelength, we need

$$\left(\frac{n_2}{n_1}\right)^2 = \frac{n_s}{n_0}. \qquad (9.106)$$

This kind of film is referred to as a *double-quarter, single-minimum* coating. When n_1 and n_2 are as small as possible, the reflectance will have its single broadest minimum equal to zero at the chosen frequency. It should be clear from Eq. (9.106) that $n_2 > n_1$; accordingly, it is now common practice to designate a (glass)–(high index)–(low index)–(air) system as *gHLa*. Zirconium dioxide ($n = 2.1$), titanium dioxide ($n = 2.40$), and zinc sulfide ($n = 2.32$) are commonly used for H-layers, and magnesium fluoride ($n = 1.38$) and cerium fluoride ($n = 1.63$) often serve as L-layers.

Other double- and triple-layer schemes can be designed to satisfy specific requirements for spectral response, incident angle, cost, and so on. Fig. 9.54 is a scene photographed through a 15-element [illegible] lens, with a 150-W lamp pointing directly into the [illegible] The lens elements were covered with a sin[illegible] MgF_2. For Fig. 9.55 a triple-layer antirefle[illegible] was used. The improved contrast and gl[illegible] are apparent.

Figure 9.54 Lens elements coated with a single layer of MgF_2.

Figure 9.55 Lens elements coated with a multilayer film [illegible] (Photos courtesy Optical Coating Laboratory, Inc., Sa[illegible] California.)

9.7.3 [illegible]tilayer Periodic Systems

[illegible]est kind of periodic system is the *quarter-wave* [illegible]ich is made up of a number of quarter-wave [illegible]e periodic structure of alternately high- and [illegible]index materials, illustrated in Fig. 9.56, is desig[illegible]d by

$$g(HL)^3a.$$

[illegible]57 illustrates the general form of a portion [illegible]tral reflectance for a few multilayer filters. [illegible] of the high-reflectance central zone increases [illegible]sing values of the index ratio $n_H/\bar{n}_L$, and its [illegible] increases with the number of layers. Note that [illegible]um reflectance of a periodic structure such [illegible] can be increased further by adding another [illegible] so that it has the form $g(HL)^mHa$. Mirror with very high reflectance can be produced [illegible] arrangement.

[illegible]mall peak on the short-wavelength side of the [illegible]e can be decreased by adding an eighth-wave [illegible] film to both ends of the stack, in which case [illegible] will be denoted by

$$g(0.5L)(HL)^mH(0.5L)a.$$

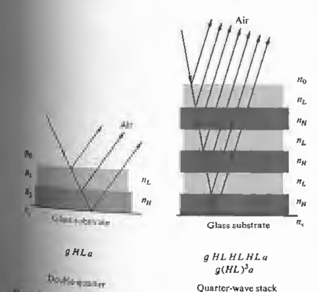


Figure 9.56 [illegible]eriodic structure.

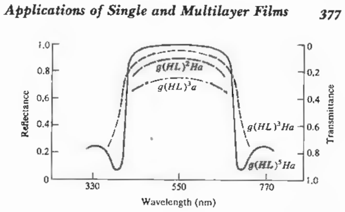


Figure 9.57 Reflectance and transmittance for several periodic structures.

This has the effect of increasing the short-wavelength high-frequency transmittance and is therefore known as a *high-pass filter*. Similarly, the structure

$$g(0.5H)L(HL)^m(0.5H)a$$

merely corresponds to the case in which the end H-layers are $\lambda_0/8$ thick. It has a higher transmittance at the long-wavelength, low-frequency range and serves as a *low-pass filter*.

At nonnormal incidence, up to about 30°, there is quite frequently little degradation in the response of thin-film coatings. In general, the effect of increasing the incident angle is a shift in the whole reflectance curve down to slightly shorter wavelengths. This kind of behavior is evidenced by several naturally occurring periodic structures, for example, peacock and hummingbird feathers, butterfly wings, and the backs of several varieties of beetles.

The last multilayer system to be considered is the *interference*, or more precisely the *Fabry–Perot, filter*. If the separation between the plates of an etalon is of the order of λ, the transmission peaks will be widely separated in wavelength. It will then be possible to block all the peaks but one by using absorbing filters of colored glass or gelatin. The transmitted light corresponds to a single sharp peak, and the etalon serves as a narrow band-pass filter. Such devices can be fabricated by depositing a semitransparent metal film onto a glass support, followed by a MgF_2 spacer and another metal coating.

All-dielectric, essentially nonabsorbing Fabry–Perot filters have an analogous structure, two possible examples of which are

$$g\ HLH\ LL\ HLH\ a$$

and

$$g\ HLHL\ HH\ LHLH\ a.$$

The characteristic matrix for the first of these is

$$\mathcal{M} = \mathcal{M}_H\mathcal{M}_L\mathcal{M}_H\mathcal{M}_L\mathcal{M}_L\mathcal{M}_H\mathcal{M}_L\mathcal{M}_H,$$

but from Eq. (9.104)

$$\mathcal{M}_L\mathcal{M}_L = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix},$$

or

$$\mathcal{M}_L\mathcal{M}_L = -\mathcal{I},$$

where $\mathcal{I}$ is the unity matrix. The central double layer, corresponding to the Fabry–Perot cavity, is a half-wavelength thick ($d = \frac{1}{2}\lambda_f$). It therefore has no effect on the reflectance *at the particular wavelength under consideration.* Thus, it is said to be an absentee layer, and as a consequence,

$$\mathcal{M} = -\mathcal{M}_H\mathcal{M}_L\mathcal{M}_H\mathcal{M}_H\mathcal{M}_L\mathcal{M}_H$$

The same conditions prevail over and over again at the center and will finally result in

$$\mathcal{M} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}.$$

At the special frequency for which the filter was designed, r at normal incidence, according to Eq. (9.97), reduces to

$$r = \frac{n_0 - n_s}{n_0 + n_s},$$

the value for the uncoated substrate. In particular, for glass ($n_s = 1.5$), in air ($n_0 = 1$) the theoretical peak transmission is 96% (neglecting reflections from the back surface of the substrate, as well as losses in both the blocking filter and the films themselves).

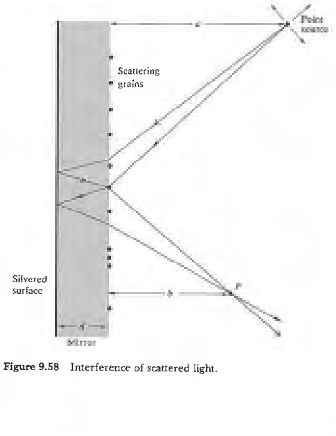


Figure 9.58 Interference of scattered light.

9.8 APPLICATIONS OF INTERFEROMETRY

There have been many physical applications of the principles of interferometry. Some of these are only of historical or pedagogical significance, whereas others are now being used extensively. The advent of the laser and the resultant availability of highly coherent quasimonochromatic light have made it particularly easy to create new interferometer configurations.

9.8.1 Scattered-Light Interference

Probably the earliest recorded study of interference fringes arising from scattered light is to be found in Sir Isaac Newton's *Optiks* (1704, Book Two, Part IV). Our present interest in this phenomenon is twofold. First, it provides an extremely easy way to see some rather beautiful colored interference fringes. Second, it is the basis for a remarkably simple and highly useful interferometer.

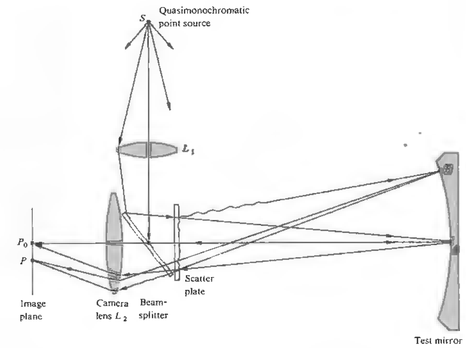


Figure 9.59 Scatter plate setup. Adapted from R. M. Scott, *Appl. Opt.* **8**, 531 (1969).

To see the fringes, lightly rub a thin layer of ordinary talcum powder onto the surface of any common back-silvered mirror (dew will do as well). Neither the thickness nor the uniformity of the coating is particularly important. The use of a bright point source, however, is crucial. A satisfactory source can be made by taping a heavy piece of cardboard having a hole about $\frac{1}{4}$ inch in diameter over a good flashlight. Initially, stand back from the mirror about 3 or 4 feet; the fringes will be too fine and closely spaced to see if you stand much nearer. Hold the flashlight alongside your cheek and illuminate the mirror so that you can see the brightest reflection of the bulb in it. The fringes will then be clearly seen as a number of alternately bright and dark bands.

In Fig. 9.58 two coherent rays leaving the point source are shown arriving at point P after traveling different routes. One ray is reflected from the mirror and then scattered by a single transparent talcum grain toward P. The second ray is first scattered downward by the grain, after which it crosses the mirror and is reflected back toward P. The resulting optical path-length difference determines the interference at P. At normal incidence, the pattern is a series of concentric rings of radius*

$$\rho \approx \left[\frac{nm\lambda a^2 b^2}{d(a^2 - b^2)}\right]^{1/2}.$$

Now consider a related device, which is very useful in testing optical systems. Known as a **scatter plate**, it generally consists of a slightly rough-surfaced, transparent sheet. In an arrangement such as the one shown in Fig. 9.59, it serves as an amplitude-splitting element. In this application it must have a center of symmetry; that is, each scattering site is required to have a duplicate, symmetrically located about a central point.

In the system under consideration, a point source of quasimonochromatic light S is imaged, by means of lens L_1 on the surface, at point A of the mirror being tested. A portion of the light coming from the source is scattered by the scatter plate and thereafter illuminates the entire surface of the mirror. The mirror, in turn, reflects light back to the scatter plate. This wave, as well as the

* For more of the details, see A. J. deWitte, "Interference in Scattered Light," *Am. J. Phys.* **35**, 301 (1967).

light forming the image of the pinhole at point A, passes through the scatter plate again and finally reaches the image plane (either on a screen or in a camera). Fringes are formed on this latter plane. The interference process, which is manifest in the formation of these fringes, occurs because each point in the final image plane is illuminated by light arriving via two dissimilar routes, one originating at A and the other at some point B, which reflects scattered light. Indeed, as strange as they may look at first sight, well-defined fringes do result, as shown in Fig. 9.60.

Examining the passage of light through the system in a bit more detail, consider the light initially incident on the scatter plate and assume that the wave is planar, as shown in Fig. 9.61. After it passes through the scatter plate, the incident plane wavefront $\mathbf{E}_i$ will be distorted into a transmitted wavefront $\mathbf{E}_T$. We envision this wave, in turn, split into a series of Fourier components consisting of plane waves, that is,

$$\mathbf{E}_T = \mathbf{E}_1 + \mathbf{E}_2 + \cdots. \tag{9.107}$$

Two of these constituents are shown in Fig. 9.61(a). Now suppose we attach a specific meaning to these components; namely, $\mathbf{E}_1$ is taken to represent the light traveling to the point A in Fig. 9.59, and $\mathbf{E}_2$ that traveling toward B. The analysis of the stages that follow could be continued in the same way. Let the portion of the wavefront returning from A be represented by the wavefront $\mathbf{E}_A$ in Fig. 9.61(b). The scatter plate will transform it into an irregular transmitted [illegible] by $\mathbf{E}_{AT}$ in the same figure. This again [illegible] a complicated configuration, but it can [illegible] Fourier components consisting of plane wa[illegible] above case. In Fig. 9.61(b), two of these [illegible] wavefronts have been drawn, one traveling [illegible] and the other inclined at an angle θ. The [illegible] wavefront, which is denoted by $\mathbf{E}_{A\theta}$, is focused by [illegible] the point P on the screen (Fig. 9.59).

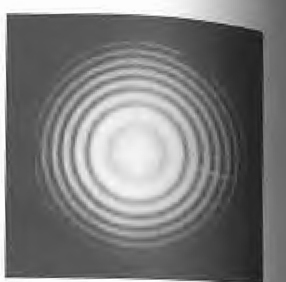


Figure 9.60 Fringes in scattered light.

The wavefront returning from B to the scatter plate [illegible] by $\mathbf{E}_B$ in Fig. 9.61(c). Upon traversing the [illegible] it will be reshaped into the wave $\mathbf{E}_{BT}$. One [illegible] components of this wavefront, denoted [illegible] inclined at the angle θ and will therefore be [illegible] the same point P on the screen.

[illegible] the waves arriving at P will be coherent in [illegible] that interference occurs. To obtain the resultant [illegible] I_P, first add the amplitudes of all the [illegible] at P, that is, $\mathbf{E}_P$, and then square and [illegible] $\mathbf{E}_P$.

[illegible] discussion above, only two point sources at the [illegible]. Actually, of course, the whole [illegible] the mirror is illuminated by the ongoing light, [illegible] point of it will serve as a secondary source [illegible] waves. All the waves will be deformed by [illegible] plate, and these, in turn, can be split into [illegible] components. In each series of component [illegible] will be one inclined at an angle θ, and all of these will be focused at the same point P on the screen. [illegible] resultant amplitude will then have the form

$$\mathbf{E}_P = \mathbf{E}_{A\theta} + \mathbf{E}_{B\theta} + \cdots.$$

[illegible] reaching the image plane can be envisioned [illegible] in part of two optical fields of special interest. [illegible] results from light that was scattered only [illegible] through the plate toward the mirror, and [illegible] results from light that was scattered only on the [illegible] toward the image plane. The former broadly [illegible] the test mirror and ultimately results in an [illegible] the screen. The latter, which was initially [illegible] to the region about A, scatters a diffuse blur [illegible] screen. The point A is chosen so that the [illegible] in the vicinity of it is free of aberrations. In [illegible] the wave reflected from it serves as a reference [illegible] to compare the wavefront corresponding [illegible] mirror surface. The interference pattern will show, as a series of contour fringes, any [illegible] perfection in the mirror surface.*

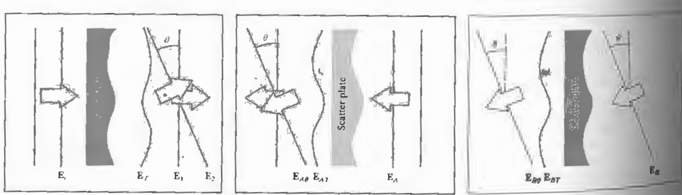


Figure 9.61 Wavefronts passing through the scatter plate.

* [illegible] discussion of the scatter plate, the reader might consult [illegible] papers by J. M. Burch, *Nature* **171**, 889 (1953), [illegible] *Am.* **52**, 600 (1962). Reference should be made to J. [illegible] *of Classical Optics*, p. 383. Also see R. M. Scott, "Scatter [illegible]metry," *Appl. Opt.* **8**, 531 (1969), and J. B. Houston, [illegible] Make and Use a Scatterplate Interferometer," *Optical* [illegible] p. 32.

9.8.2 Thin-Film Measurements by Multiple-Beam Interferometry

Return to Fig. 9.32 and now suppose that the wedge has a step in it. Figure 9.62 illustrates the fringe pattern that might be seen under these circumstances. If the wedge angle is the same for each surface, that is, if the top surfaces are parallel, the fringes will be equally spaced.

When the separation of the fringes is b and the shift is a, then the height of the step is given by

$$t = \frac{a}{b}\frac{\lambda_f}{2}.$$

If one of the boundaries of the film is an optical flat and the other boundary is a crystal surface or some other surface examined for flatness, then these Fizeau fringes are contours of the surface under examination.

An actual optical system for measuring the thickness of a thin film deposited on a glass substrate is shown in Fig. 9.63. The film whose thickness is to be determined is coated with an opaque layer of silver, about 70 nm thick, which accurately contours the undersurface. The

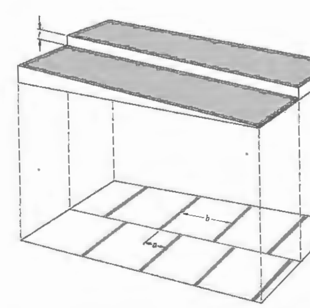


Figure 9.62 Fringes arising from a stepped wedge-shaped film.

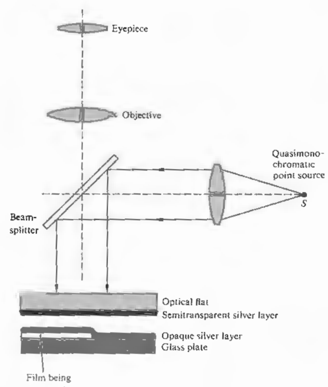


Figure 9.63 Arrangement for measuring film thickness.

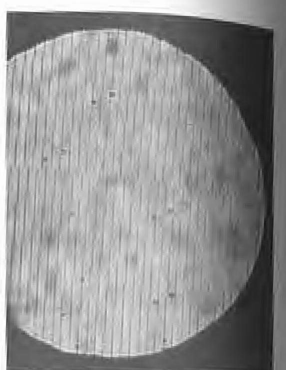


Figure 9.64 Actual fringes from a stepped wedge.

opposing silvered surfaces generate a sharp multiple-wave Fizeau pattern. The upper plate is tilted slightly to create an air film in the form of Fig. 9.62, so that the same arrangement of fringes is now observed (Fig. 9.64). Film thicknesses of about 2.0 nm can readily be determined in this manner. Such methods yield a resolution in depth comparable to the lateral resolution of an electron microscope. Tolansky, using the multiple-beam techniques that he invented, has measured height changes of 1×10^{-8} inches, nearly the size of a single atom.

9.8.3 The Michelson–Morley Experiment

Over the years since 1881, the Michelson interferometer has had innumerable applications, most of which are now mainly of historical interest. One of the most significant of these was its use in the Michelson–Morley experiment.

During the last century scientists common[illegible] that there existed a medium, the *luminife*[illegible] carrying) *aether*, which permeated all matter, pe[illegible] all space, was massless, and neither solid, liqu[illegible] gas. As James Maxwell wrote in the *Encyclo*[illegible] *Britannica*:

> Aethers were invented for the planets to swim in, to constitute electric atmospheres and magnetic [illegible] to convey sensations from one part of our bodies to another, and so on, until all space had been [illegible] or four times over with aethers. . . . The [illegible] which has survived is that which was invented by Huygens to explain the propagation of light.

It was well established that light was a wave [illegible] only natural to have a medium in which the dis[illegible]

[illegible]ed. With that assumption, the nature of the [illegible] had to match terrestrial and astronomical [illegible]ations. At the time, there was no denying the existence of aether; the debate centered on its properties. Was the aether stationary in space, providing a reference frame from which to [illegible] the absolute motion of all other objects? Or [illegible]ged along by the planets as they moved [illegible]ce? If the aether were stationary, an obser[illegible] Earth would be able to detect an aether wind [illegible] over its surface, as it moved in orbit. A. A. [illegible] later joined by E. W. Morley, set out to [illegible] effects of the aether wind, using his inter[illegible] which was designed specifically for that pur[illegible] oriented, as shown in Fig. 9.65, with the [illegible] parallel to the velocity **v** of the Earth through [illegible] The basic reasoning of the Michelson–Morley [illegible], derived from purely classical laws of physics, [illegible]ows: when the beam of light travels to the [illegible]ative speed with respect to the moving inter[illegible] is $c - v$, it is moving against the aether wind, [illegible]me to travel the length OM_1 is

$$t_1' = \frac{\ell_1}{c - v}.$$

For the return trip, M_1O, the beam travels with the

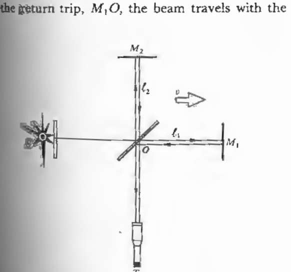


Figure 9.65 [illegible] Michelson–Morley experiment. Overall configuration.

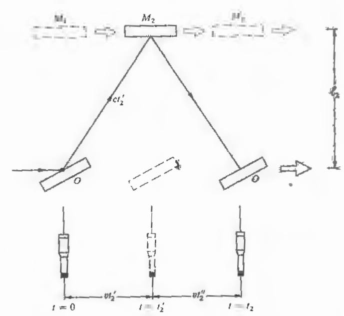


Figure 9.66 The Michelson–Morley experiment. Geometry for the transverse beam.

aether wind, and

$$t_1'' = \frac{\ell_1}{c + v}.$$

The total time, $t_1' + t_1''$, to traverse OM_1O is

$$t_1 = \frac{\ell_1}{c - v} + \frac{\ell_1}{c + v},$$

which can be written as

$$t_1 = \frac{2\ell_1}{c}\beta^2,$$

where

$$\beta = \frac{1}{\sqrt{1 - v^2/c^2}}.$$

The time of travel toward the second mirror can be determined with the help of Fig. 9.66. From the right triangle, where t_2' is the transit time to cover OM_2,

$$c^2 t_2'^2 = v^2 t_2'^2 + \ell_2^2,$$

from which it follows that

$$t_2' = \frac{\ell_2}{c}\beta.$$

But this is also the time t_2'' that it takes the beam of light to return from M_2 to O, and since $t_2 = t_2' + t_2''$,

$$t_2 = \frac{2\ell_2}{c}\beta.$$

Notice that even when $\ell_1 = \ell_2 = \ell$, $t_1 \neq t_2$ and

$$t_1 - t_2 = \frac{2\ell}{c}(\beta^2 - \beta).$$

Using the binomial expansion with $c \gg v$, we obtain

$$\beta^2 = (1 - v^2/c^2)^{-1} = 1 + v^2/c^2$$

and

$$\beta = (1 - v^2/c^2)^{-1/2}$$

or

$$\beta = 1 + \tfrac{1}{2}v^2/c^2.$$

We find that with $\Delta t = t_1 - t_2$

$$\Delta t = \frac{\ell}{c}\left(\frac{v}{c}\right)^2.$$

A time difference Δt in the two paths corresponds to a difference in the number of wavelengths fitting between OM_1O and OM_2O:

$$\Delta N = \Delta t/\tau \quad \text{or} \quad \Delta N = \nu\Delta t,$$

where τ is the period and ν the frequency. This is also the number of pairs of fringes (i.e., a maximum and a minimum) that would shift past the telescope cross hairs, if a time difference Δt were somehow introduced during the obervation. Suppose that the Earth were stationary in space and then started moving with a speed v, such that $\Delta N = \frac{1}{2}$. Furthermore, suppose the observer set the cross hairs initially at the center of a bright fringe. As the Earth began to move, the bright fringe would sweep by, and the cross hairs would shift to the center of the adjacent dark fringe. We cannot, of course, stop the world, but we can rotate the interferometer. If the instrument is rotated 90°, the new transit time difference, which can be determined by just interchanging the 1 and 2 subscripts, is equal to $-\Delta t$. This [illegible] that if the observer were to rotate the interfer[illegible] 90°, a time difference of $2\,\Delta t$ would be introduc[illegible] which, in that example, $\Delta N = 1$, and the cross hairs would end up on the next bright fringe.

This is essentially what Michelson and Morley did. Their apparatus was multimirrored to make [illegible] length as large as possible, $\ell_1 \approx \ell_2 \approx 11.0$ [illegible] on a massive stone, which floated on a troug[illegible] mercury (Fig. 9.67). Each man took tu[illegible] around with the slowly revolving stone, [illegible] tinuously observing the fringe pattern. Wi[illegible] assumed to be equal to the Earth's orbital sp[illegible] 30 km/s and $\lambda_0 = 550$ nm, the fringe shift [illegible] would be

$$\Delta N = \frac{2\ell}{\lambda}\left(\frac{v}{c}\right)^2$$

or

$$\Delta N = 0.4.$$

They made many observations at different [illegible] Earth's daily cycle and on different days durin[illegible] orbit. Even though they could have detected [illegible] a minute fraction of a fringe, they saw none whatev[illegible] There was no aether wind; Michelson and Morley [illegible] sounded the prelude to special relativity.

Ten years later, Michelson interferometricall[illegible] the possibility that the aether was being dragge[illegible]

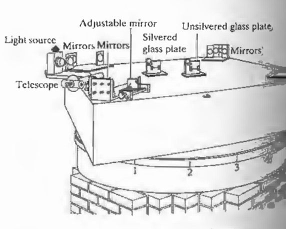


Figure 9.67 The Michelson–Morley experiment.

[illegible] Earth. His results showed that this too was not [illegible] the aether theory was doomed.

[illegible]ern version of the Michelson–Morley experi[illegible] own here in Fig. 9.68, compared the frequen[illegible] infrared lasers. (Recall that in Section 7.2.1 [illegible]red the application of lasers to the problem [illegible]rating beats.) The combined beam reaching the [illegible]ultiplier, being the resultant of two coplanar [illegible]ic waves, was *amplitude-modulated* by a relatively [illegible]iation. These *beats* had a frequency equal to the [illegible]erence between those of the two constituent laser [illegible] The precise frequency of the mode in which [illegible] operated was governed by the length of the [illegible] resonant cavity and the speed of light therein. [illegible]asers, functioning at about 3×10^{14} Hz, were [illegible] 90°, the *aether wind* would affect the speed of [illegible] in the cavities and therefore the frequency [illegible]erence between them. A relative change in ν of [illegible] would be expected from the aether wind [illegible]esis, because of the Earth's orbital velocity. No [illegible] in the beat frequency, to within an accuracy of [illegible] $\frac{1}{1000}$ of that predicted, was detected.

9.8.4 [illegible]e Twyman–Green Interferometer

[illegible]wyman–Green is essentially a variation of the [illegible]son interferometer. It's an instrument of great [illegible] in the domain of modern optical testing. [illegible] its distinguishing physical characteristics (illus[illegible] Fig. 9.69) are a quasimonochromatic point source and lens L_1, to provide a source of incoming [illegible] waves, and a lens L_2, which permits all the light [illegible]he aperture to enter the eye so that the entire [illegible] that is, any portion of M_1 and M_2. A [illegible] laser serves as a superior source in that it [illegible] of long path-length differen[illegible] [illegible] addition, short photographic exposure times. These tend to minimize unwanted vibration effects. Laser versions of the Twyman–Green are among the most effective testing tools in optics. As shown in the [illegible] the device is set up to examine a lens. The

[illegible] A. Javan, J. Murray, and C. H. Townes, "Test of Special [illegible] of the Isotropy of Space by Use of Infrared Masers," [illegible], A1221 (1964).

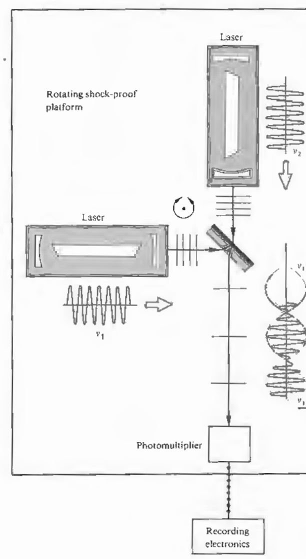


Figure 9.68 A variation of the Michelson–Morley experiment.

spherical mirror M_2 has its center of curvature coincident with the focal point of the lens. If the lens being tested is free of aberrations, the emerging reflected light returning to the beam-splitter will again be a plane wave. If, however, astigmatism, coma, or spherical aberration deforms the wavefront, a fringe pattern clearly manifesting these distortions can be seen and

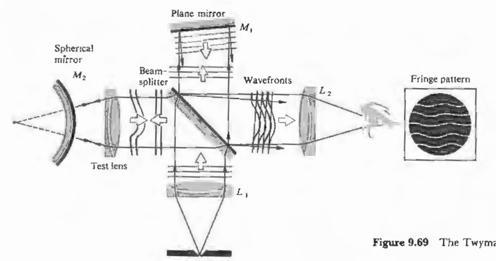


Figure 9.69 The Twyman–Green interferometer.

photographed. When M_2 is replaced by a plane mirror, a number of other elements (prisms, optical flats, etc.) can be tested equally well. The optician interpreting the fringe pattern can then mark the surface for further polishing to correct high or low spots. In the fabrication of the finest optical systems, telescopes, high-altitude cameras, and so forth, the interferograms may even be scanned electronically, and the resulting data analyzed by computer. Computer-controlled plotters can then automatically produce surface contour maps or perspective "three-dimensional" drawings of the distorted wavefront generated by the element being tested. These procedures can be used throughout the fabrication process to ensure the highest-quality optical instruments. Complex systems with wavefront aberrations in the fractional-wavelength range are the result of what might be called the *new technology*.*

9.8.5 The Rotating Sagnac Interferometer

Use of the Sagnac interferometer to measure the rotational speed of a system has generated interest in recent times. In particular, the *ring laser*, which is essentially a Sagnac interferometer containing a laser in one or more of its arms, was designed specifica[redacted] purpose. The first ring laser gyroscope was [redacted] in 1963, and work is continuing on various [redacted] this sort (Fig. 9.70). The initial experimen[redacted] impetus to these efforts were performed by [redacted] 1911. At that time he rotated the entire inter[redacted] mirrors, source, and detector, about a per[redacted] axis passing through its center (Fig. 9.71). R[redacted] Section 9.4.2, that two overlapping beams [redacted] interferometer, one clockwise, the other counter[redacted]wise. The rotation effectively shortens the pat[redacted] taken by one beam in comparison to that of the other. In the interferometer the result is a fringe shift proportional to the angular speed of rotation ω. In the ring laser, it is a frequency difference between the two beams that is proportional to ω.

Consider the arrangement depicted [redacted] Fig. 9.71[redacted] corner A (and every other corner) mo[redacted] with a li[redacted] speed $v = R\omega$, where R is half the d[redacted]gonal o[redacted] square. Using classical reasoning, we find that the [redacted] of travel of light along AB is

$$t_{AB} = \frac{R\sqrt{2}}{c - v/\sqrt{2}}$$

or

$$t_{AB} = \frac{2R}{\sqrt{2}c - \omega R}.$$

The time of travel of the light from A to D is

$$t_{AD} = \frac{2R}{\sqrt{2}c + \omega R}.$$

[redacted] for counterclockwise and clockwise travel [redacted]pectively by

$$t_{\circlearrowleft} = \frac{8R}{\sqrt{2}c + \omega R}$$

and

$$t_{\circlearrowright} = \frac{8R}{\sqrt{2}c - \omega R}.$$

[redacted] the difference between these two intervals is

$$\Delta t = t_{\circlearrowright} - t_{\circlearrowleft}$$

using the binomial series,

$$\Delta t = \frac{8R^2\omega}{c^2}.$$

[redacted]ing laser gyro. (Photo courtesy Autonetics, a Division [redacted] Rockwell Corp.)

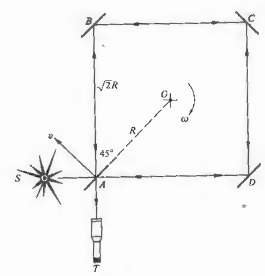


Figure 9.71 The rotating Sagnac interferometer. Originally it was 1 m × 1 m with ω = 120 rev/min.

This can be expressed in terms of the area $A = 2R^2$ of the square formed by the beams of light as

$$\Delta t = \frac{4A\omega}{c^2}.$$

Let the period of the monochromatic light used be $\tau = \lambda/c$; then the fractional displacement of the fringes, given by $\Delta N = \Delta t/\tau$, is

$$\Delta N = \frac{4A\omega}{c\lambda},$$

a result that has been verified experimentally. In particular, Michelson and Gale* used this method to determine the angular velocity of the Earth.

The preceding classical treatment is obviously lacking, inasmuch as it assumes speeds in excess of c, an assumption that is contrary to the dictates of special relativity. Furthermore, it would appear that since the system is accelerating, general relativity would prevail. In fact, all these formalisms yield the same results.

* Take a look at R. Berggren, "Analysis of Interferograms," *Optical Spectra*, (Dec. 1970), p. 22.

* Michelson and Gale, *Astrophys. J.* **61**, 140 (1925).

PROBLEMS

9.1 Returning to Section 9.1, let

$$\mathbf{E}_1(\mathbf{r}, t) = \boldsymbol{E}_1(\mathbf{r})e^{-i\omega t}$$

and

$$\mathbf{E}_2(\mathbf{r}, t) = \boldsymbol{E}_2(\mathbf{r})e^{-i\omega t},$$

where the wavefront shapes are not explicitly specified, and $\boldsymbol{E}_1$ and $\boldsymbol{E}_2$ are complex vectors depending on space and initial phase angle. Show that the interference term is then given by

$$I_{12} = \tfrac{1}{2}(\boldsymbol{E}_1 \cdot \boldsymbol{E}_2^* + \boldsymbol{E}_1^* \cdot \boldsymbol{E}_2). \qquad (9.108)$$

You will have to evaluate terms of the form

$$\langle \boldsymbol{E}_1 \cdot \boldsymbol{E}_2 e^{-2i\omega t} \rangle = \frac{\boldsymbol{E}_1 \cdot \boldsymbol{E}_2}{T} \int_t^{t+T} e^{-2i\omega t'} dt'$$

for $T \gg \tau$ (take another look at Problem 3.4). Show that Eq. (9.108) leads to Eq. (9.11) for plane waves.

9.2 In Section 9.1 we considered the spatial distribution of energy for two point sources. We mentioned that for the case in which the separation $a \gg \lambda$, I_{12} spatially averages to zero. Why is this true? What happens when a is much less than λ?

9.3 Will we get an interference pattern in Young's experiment (Fig. 9.5) if we replace the source slit S by a single long-filament light bulb? What would occur if we replaced the slits S_1 and S_2 by these same bulbs?

9.4* Two 1.0-MHz radio antennas emitting in phase are separated by 600 m along a north–south line. A radio receiver placed 2.0 km east is equidistant from both transmitting antennas and picks up a fairly strong signal. How far north should that receiver be moved if it is again to detect a signal nearly as strong?

9.5 An expanded beam of red light from a He–Ne laser ($\lambda_0 = 632.8$ nm) is incident on a screen containing two very narrow horizontal slits separated by 0.200 mm. A fringe pattern appears on a white screen held 1.00 m away.

a) How far (in radians and millimeters) above and below the central axis are the first zeros of irradiance?
b) How far (in mm) from the axis is the fifth bright band?
c) Compare these two results.

9.6* Red plane waves from a ruby laser ($\lambda_0 =$ 694.3 nm) in air impinge on two parallel slits in an opaque screen. A fringe pattern forms on a distant wall, and we see the fourth bright band 1.0° above the central axis. Kindly calculate the separation between the slits.

9.7* A 3 × 5 card containing two pinholes, 0.08 mm in diameter and separated center to center by 0.10 mm, is illuminated by parallel rays of blue light from an argon ion laser ($\lambda_0 = 487.99$ nm). If the fringes on an observing screen are to be 10 mm apart, how far away should the screen be?

9.8* White light falling on two long narrow slits emerges and is observed on a distant screen. If red light ($\lambda_0 = 780$ nm) in the first-order fringe overlaps violet in the second-order fringe, what is the latter's wavelength?

9.9* Considering the double-slit experiment, derive an equation for the distance $y_{m'}$ from the central axis to the m'th irradiance *minimum*, such that the first dark bands on either side of the central maximum correspond to $m' = \pm 1$. Identify and justify all your approximations.

9.10* With regard to Young's experiment, derive a general expression for the shift in the vertical position of the mth *maximum* as a result of placing a thin parallel sheet of glass of index n and thickness d directly over one of the slits. Identify your assumptions.

9.11* Plane waves of monochromatic light impinge at an angle θ_i on a screen containing two narrow slits separated by a distance a. Derive an equation for the angle measured from the central axis which locates the mth maximum.

9.12* Sunlight incident on a screen containing two long narrow slits 0.20 mm apart casts a pattern on a white sheet of paper 2.0 m beyond. What is the distance separating the violet ($\lambda_0 = 400$ nm) in the first-order band from the red ($\lambda_0 = 600$ nm) in the second-order band?

9.13 To examine the conditions under which the approximations of Eq. (9.23) are valid:

a) Apply the law of cosines to triangle S_1S_2P in Fig. 9.5(c) to get

$$\frac{r_2}{r_1} = \left[1 - 2\left(\frac{a}{r_1}\right)\sin\theta + \left(\frac{a}{r_1}\right)^2\right]^{1/2}.$$

b) Expand this in a Maclaurin series yielding

$$r_2 = r_1 - a\sin\theta + \frac{a^2}{2r_1}\cos^2\theta + \cdots.$$

c) In light of Eq. (9.17), show that if $(r_1 - r_2)$ is to equal $a\sin\theta$, it is required that $r_1 \gg a^2/\lambda$.

9.14 A stream of electrons, each having an energy of 0.5 eV, impinges on a pair of extremely thin slits separated by 10^{-2} mm. What is the distance between adjacent minima on a screen 20 m behind the slits? ($m_e = 9.108 \times 10^{-31}$ kg, 1 eV $= 1.602 \times 10^{-19}$ J.)

9.15* Show that a for the Fresnel biprism of Fig. 9.10 is given by $a = 2d(n - 1)\alpha$.

9.16* In the Fresnel double mirror $s = 2$ m, $\lambda_0 =$ [illegible] nm, and the separation of the fringes was found to be 0.5 mm. What is the angle of inclination of the mirrors, if the perpendicular distance of the actual point source to the intersection of the two mirrors is 1 m?

9.17* The Fresnel biprism is used to obtain fringes from a point source that is placed 2 m from the screen, and the prism is midway between the source and the screen. Let the wavelength of the light be $\lambda_0 = 500$ nm and the index of refraction of the glass be $n = 1.5$. What is the prism angle, if the separation of the fringes is 0.5 mm?

9.18 What is the general expression for the separation of the fringes of a Fresnel biprism of index n immersed in a medium having an index of refraction n'?

9.19 Using Lloyd's mirror, x-ray fringes were observed, the spacing of which was found to be 0.0025 cm. The wavelength used was 8.33 Å. If the source–screen distance was 3 m, how high above the mirror plane was the point source of x-rays placed?

9.20 Imagine that we have an antenna at the edge of a lake picking up a signal from a distant radio star (Fig. 9.72), which is just coming up above the horizon. Write expressions for δ and for the angular position of the star when the antenna detects its first maximum.

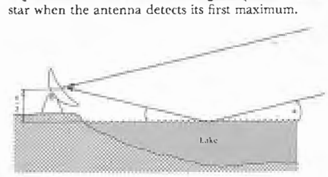


Figure 9.72

9.21* If the plate in Fig. 9.14 is glass in air, show that the amplitudes of E_{1r}, E_{2r}, and E_{3r} are respectively $0.2\,E_{0i}$, $0.192\,E_{0i}$, and $0.008\,E_{0i}$, where E_{0i} is the incident amplitude. Make use of the Fresnel coefficients at normal incidence, assuming no absorption. You might repeat the calculation for a water film in air.

9.22 A soap film surrounded by air has an index of refraction of 1.34. If a region of the film appears bright red ($\lambda_0 = 633$ nm) in normally reflected light, what is its minimum thickness there?

9.23* A thin film of ethyl alcohol ($n = 1.36$) spread on a flat glass plate and illuminated with white light shows a color pattern in reflection. If a region of the film reflects only green light (500 nm) strongly, how thick is it?

9.24* A soap film of index 1.34 has a region where it is 550.0 nm thick. Determine the vacuum wavelengths of the radiation that is not reflected when the film is illuminated from above with sunlight.

9.25 Consider the circular pattern of Haidinger's fringes resulting from a film with a thickness of 2 mm and an index of refraction of 1.5. For monochromatic illumination of $\lambda_0 = 600$ nm, find the value of m for the central fringe ($\theta_t = 0$). Will it be bright or dark?

9.26 Illuminate a microscope slide (or even better, a thin cover-glass slide). Colored fringes can easily be seen with an ordinary fluorescent lamp serving as a broad source or a mercury street light as a point source. Describe the fringes. Now rotate the glass. Does the pattern change? Duplicate the conditions shown in Figs. 9.15 and 9.16. Try it again with a sheet of plastic food wrap stretched across the top of a cup.

9.27 Figure 9.73 illustrates a setup used for testing lenses. Show that

$$d = x^2(R_2 - R_1)/2R_1R_2$$

when d_1 and d_2 are negligible in comparison with $2R_1$ and $2R_2$, respectively. (Recall the theorem from plane geometry that relates the products of the segments of intersecting chords.) Prove that the radius of the mth dark fringe is then

$$x_m = [R_1R_2m\lambda_f/(R_2 - R_1)]^{1/2}.$$

How does this relate to Eq. (9.43)?

Figure 9.73

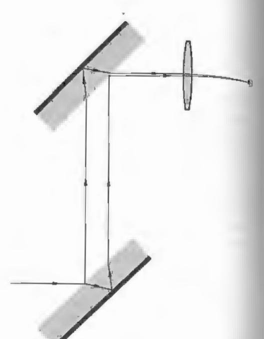


Figure 9.74

9.28* Newton rings are observed on a film with quasimonochromatic light that has a wavelength of 500 nm. If the 20th bright ring has a radius of 1 cm, what is the radius of curvature of the lens forming one part of the interfering system?

9.29 Fringes are observed when a parallel beam of light of wavelength 500 nm is incident perpendicularly onto a wedge-shaped film with an index of refraction of 1.5. What is the angle of the wedge if the fringe separation is $\frac{1}{3}$ cm?

9.30* Suppose a wedge-shaped air film is made between two sheets of glass, with a piece of paper 7.618×10^{-5} m thick used as the spacer at their very ends. If light of wavelength 500 nm comes down from directly above, determine the number of bright fringes that will be seen across the wedge.

9.31 A Michelson interferometer is illuminated with monochromatic light. One of its mirrors is then moved 2.53×10^{-5} m, and it is observed that 92 fringe-pairs, bright and dark, pass by in the process. Determine the wavelength of the incident beam.

9.32* One of the mirrors of a Michelson interferometer is moved, and 1000 fringe-pairs shift past the hairline in a viewing telescope during the process. If the device is illuminated with 500-nm light, how far was the mirror moved?

9.33* Suppose we place a chamber 10.0 cm long with flat parallel windows in one arm of a Michelson interferometer that is being illuminated by 600-nm light. If the refractive index of air is 1.00029 and all the air is pumped out of the cell, how many fringe-pairs will shift by in the process?

9.34* A form of the Jamin interferometer is illustrated in Fig. 9.74. How does it work? To what use might it be put?

9.35 Starting with Eq. (9.53) for the transmitted wave, compute the flux density, i.e. Eq. (9.54).

9.36 Given that the mirrors of a Fabry–Perot interferometer have an amplitude reflection coefficient of $r = 0.8944$, find

a) the coefficient of finesse,
b) the half-width,
c) the finesse, and,
d) the *contrast factor* defined by

$$C = \frac{(I_t/I_i)_{max}}{(I_t/I_i)_{min}}.$$

9.37 To fill in some of the details in the derivation of the smallest phase increment separating two resolvable Fabry–Perot fringes, that is,

$$(\Delta\delta) \approx 4.2/\sqrt{F}, \qquad [9.73]$$

satisfy yourself that

$$[\mathscr{A}(\theta)]_{\delta=\delta_n\pm\Delta\delta/2} = [\mathscr{A}(\theta)]_{\delta=\Delta\delta/2}.$$

Show that Eq. (9.72) can be rewritten as

$$2[\mathscr{A}(\theta)]_{\delta=\Delta\delta/2} = 0.81\{1 + [\mathscr{A}(\theta)]_{\delta=\Delta\delta}\}.$$

When F is large γ is small, and $\sin(\Delta\delta) \approx \Delta\delta$. Prove that Eq. (9.73) then follows.

9.38 Consider the interference pattern of the Michelson interferometer as arising from two beams of equal flux density. Using Eq. (9.17), compute the half-width. What is the separation, in δ, between adjacent maxima? What then is the finesse?

9.39* Satisfy yourself of the fact that a film of thickness $\lambda_f/4$ and index n_1 will always reduce the reflectance of the substrate on which it is deposited, as long as $n_s > n_1 > n_0$. Consider the simplest case of normal incidence and $n_0 = 1$. Show that this is equivalent to saying that the waves reflected back from the two interfaces cancel one another.

9.40 Verify that the reflectance of a substrate can be increased by coating it with a $\lambda_f/4$, high-index layer, that is, $n_1 > n_s$. Show that the reflected waves interfere constructively. The quarter-wave stack $g(HL)^mHa$ can be thought of as a series of such structures.

9.41 Determine the refractive index and thickness of a film to be deposited on a glass surface ($n_g = 1.54$) such that no normally incident light of wavelength 540 nm is reflected.

9.42 A glass microscope lens having an index of 1.55 is to be coated with a magnesium fluoride film to increase the transmission of normally incident yellow light ($\lambda_0 = 550$ nm). What minimum thickness should be deposited on the lens?

9.43* A glass camera lens with an index of 1.55 is to be coated with a cryolite film ($n \approx 1.30$) to decrease the reflection of normally incident green light ($\lambda_0 = 500$ nm). What thickness should be deposited on the lens?

10 DIFFRACTION

10.1 PRELIMINARY CONSIDERATIONS

An opaque body placed midway between a screen and a point source casts an intricate shadow made up of bright and dark regions quite unlike anything one might expect from the tenets of geometrical optics (Fig. 10.1).* The work of Francesco Grimaldi in the 1600s was the first published detailed study of this *deviation of light from rectilinear propagation*, something he called "*diffractio.*" *The effect is a general characteristic of wave phenomena occurring whenever a portion of a wavefront, be it sound, a matter wave, or light, is obstructed in some way.* If in the course of encountering an obstacle, either transparent or opaque, a region of the wavefront is altered in amplitude or phase, diffraction will occur.† The various segments of the wavefront that propagate beyond the obstacle interfere, causing the particular energy-density distribution referred to as the diffraction pattern. There is no significant physical distinction between *interference* and *diffraction*. It has, however, become somewhat customary, if not always appropriate, to speak of interference when considering the superposition of only a few waves and diffraction when treating a large number of waves. Even so, one refers to multiple-beam interference in one context and diffraction from a grating in another.

Figure 10.1 The shadow of a hand holding a dime, cast directly on 4 × 5 Polaroid A.S.A. 3000 film using a He–Ne beam and no lenses. (Photo by E.H.)

We might mention parenthetically that the wave theory, although the most natural, is not the only means for dealing with certain diffraction phenomena. For example, diffraction from a grating (Section 10.2.7) can be analyzed using a corpuscular quantum approach.* For our purposes, however, the classical wave theory, which provides the simplest effective formalism, will more than suffice throughout this chapter.

It should be emphasized that optical instruments make use of only a portion of the complete incident wavefront. Diffraction effects are accordingly of great significance in the detailed understanding of devices containing lenses, stops, source slits, mirrors, and so on. If all defects in a lens system were removed, the ultimate sharpness of an image would be limited by diffraction (Problem 10.23).

As an initial approach to the problem, let's reconsider Huygens's principle (Section 4.2.1). Each point on a wavefront can be envisaged as a source of secondary spherical wavelets. The progress through space of the wavefront or any portion thereof can then presumably be determined. At any particular time, the shape of the wavefront is supposed to be the envelope of the secondary wavelets (Fig. 4.3). The technique, however, ignores most of each secondary wavelet, retaining only that portion common to the envelope. As a result of this inadequacy, Huygens's principle by itself is unable to account for the details of the diffraction process. That this is indeed the case is borne out by everyday experience. Sound waves (e.g., $\nu = 500$ Hz, $\lambda \approx 68$ cm) easily "bend" around large objects like telephone poles and trees, yet these objects cast fairly distinct shadows when illuminated by light. Huygens's principle is independent of any wavelength considerations, however, and would predict the same wavefront configurations in both situations. The difficulty was resolved by Fresnel with his addition of the concept of interference. The corresponding **Huygens–Fresnel principle** states that *every unobstructed point of a wavefront, at a given instant in time, serves as a source of spherical secondary wavelets (with the same frequency as that of the primary wave). The amplitude of the optical field at any point beyond is the superposition of all these wavelets (considering their amplitudes and relative phases).* Applying these ideas on the very simplest qualitative level, refer to the ripple tank photographs in Fig. 10.2 and the illustration in Fig. 10.3. If each unobstructed point on the incoming plane wave acts as a coherent secondary source, the maximum optical path-length difference among them will be $\Lambda_{max} = |\overline{AP} - \overline{BP}|$, corresponding to a source point at each edge of the aperture. But Λ_{max} is less than or equal to $\overline{AB}$, the latter being the case when P is on

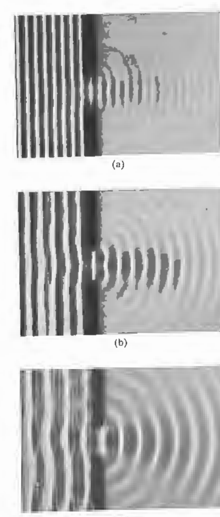


Figure 10.2 Diffraction through an aperture with varying λ as seen in a ripple tank. (Photo courtesy PSSC *Physics*, D. C. Heath, Boston, 1960.)

* The effect is easily seen, but you need a fairly strong source. A high-intensity lamp shining through a small hole works well. If you look at the shadow pattern arising from a pencil under point-source illumination, you will see an unusual bright region bordering the edge and even a faintly illuminated band down the middle of the shadow. Take a close look at the shadow cast by your hand in direct sunlight.

† Diffraction associated with transparent obstacles is not usually considered, although if you have ever driven an automobile at night with a few rain droplets on your eyeglasses, you are no doubt quite familiar with the effect. If you have not, put a droplet of water or saliva on a glass plate, hold it very close to your eye, and look directly through it at a point source. You'll see bright and dark fringes.

* W. Duane, *Proc. Nat. Acad. Sci.* **9**, 158 (1923).

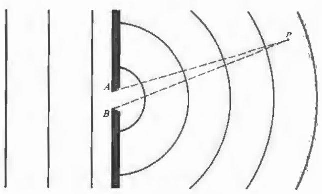


Figure 10.3 Diffraction at a small aperture.

the screen. When $\lambda \gg \overline{AB}$, as in Fig. 10.3, it follows that $\lambda \gg \Lambda_{max}$, and since the waves were initially in phase, they must all interfere constructively (to varying degrees) wherever P happens to be [see Fig. 10.2(c)]. The antithetic situation occurs when $\lambda \ll \overline{AB}$, as in Fig. 10.2(a). Now the area where $\lambda \gg \Lambda_{max}$ is limited to a small region extending out directly in front of the aperture, and it is only there that all the wavelets will interfere constructively. Beyond this zone some of the wavelets can interfere destructively, and the "shadow" begins. Keep in mind that the idealized *geometric shadow* corresponds to $\lambda \to 0$.

The Huygens–Fresnel principle has some shortcomings (which we will examine later), in addition to the fact that the whole thing at this point is rather hypothetical. Gustav Kirchhoff developed a more rigorous theory based directly on the solution of the differential wave equation. Kirchhoff, although a contemporary of Maxwell, did his work before Hertz's demonstration (and the resulting popularization) of the propagation of electromagnetic waves in 1887. Accordingly, Kirchhoff employed the older elastic-solid theory of light. His refined analysis lent credence to the assumptions of Fresnel and led to an even more precise formulation of Huygens's principle as an exact consequence of the wave equation. Even so, the Kirchhoff theory is itself an approximation that is valid for sufficiently small wavelengths, that is, when the diffracting apertures have dimensions that are large in comparison to λ. The difficulty arises from the fact that we require the solution of a partial differential equation that meets the boundary conditions imposed by the obstruction. This kind of rigorous solution is obtainable only in a few special cases. Kirchhoff's theory works fairly well, even though it deals only with scalar waves and is insensitive to the fact that light is a transverse vector field.*

It should be stressed that the problem of determining an exact solution for a particular diffracting configuration is among the most troublesome to be dealt with in optics. The first such solution, utilizing the electromagnetic theory of light, was published by Arnold Johannes Wilhelm Sommerfeld (1868–1951) in 1896. Although the problem was physically somewhat unrealistic, in that it involved an infinitely thin yet opaque, perfectly conducting plane screen, the result was nonetheless extremely valuable, providing a good deal of insight into the fundamental processes involved.

Rigorous solutions of this sort do not exist even today for many of the configurations of practical interest. We will therefore, out of necessity, rely on the approximate treatments of Huygens–Fresnel and Kirchhoff. In recent times, microwave techniques have been employed to conveniently study features of the diffraction field that might otherwise be almost impossible to examine optically. The Kirchhoff theory has held up remarkably well under this kind of scrutiny.† In many cases, the simpler Huygens–Fresnel treatment will prove adequate for our purposes.

10.1.1 Opaque Obstructions

Diffraction may be envisioned as arising from the interaction of electromagnetic waves with some sort of physical obstruction. We would therefore do well to reexamine briefly the processes involved; in other words, what actually takes place within the material of the opaque object?

One possible description is that a screen may be considered to be a continuum; that is, its microscopic structure may be neglected. For a nonabsorbing metal sheet (no joule heating, therefore infinite conductivity) we can write Maxwell's equations for the metal and for the surrounding medium, and then match the two at the boundaries. Precise solutions can thus be obtained for very simple configurations. The reflected and diffracted waves then result from the current distribution within the sheet.

Examining the screen on a submicroscopic scale, imagine the electron cloud of each atom set into vibration by the electric field of the incident radiation. The classical model, which speaks of electron-oscillators vibrating and reemitting at the source frequency (Section 3.5.1), serves quite well so that we need not be concerned with the quantum-mechanical description. The amplitude and phase of a particular oscillator within the screen are determined by the local electric field surrounding it. This in turn is a superposition of the incident field and the fields of all the other vibrating electrons. A large opaque screen with no apertures, be it made of black paper or aluminum foil, has one obvious effect: there is no optical field in the region beyond it. Electrons near the illuminated surface are driven into oscillation by the impinging light. They emit radiant energy, which is ultimately "reflected" backward, absorbed by the material in the form of heat, or both. In any case, the incident primary wave and the electron-oscillator fields superimpose in such a way as to yield zero light at any point beyond the screen. This might seem a remarkably special balance, but it actually is not. If the primary wave were not canceled completely, it would propagate deeper into the material of the screen, exciting more electrons to radiate. This in turn would further weaken the primary wave until it ultimately vanished (if the screen were thick enough). Even an opaque material such as silver, in the form of a sufficiently thin sheet, is transparent (recall the half-silvered mirror).

Now, remove a small disk-shaped segment from the center of the screen, so that light streams through the aperture. The oscillators that uniformly cover it are removed along with the disk, so the remaining electrons within the screen are no longer affected by them. As a first and certainly approximate approach, *assume that the mutual interaction of the oscillators is essentially negligible*; that is, the electrons in the screen are completely unaffected by the removal of the electrons in the disk. The field in the region beyond the aperture will then

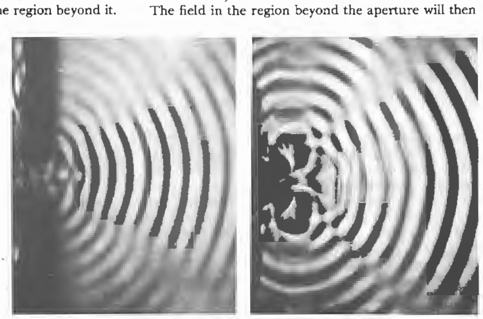


Figure 10.4 Ripple-tank photos. In one case the waves are simply diffracted by a slit; in the other a series of equally spaced point sources span the aperture and generate a similar pattern. (Photos courtesy PSSC *Physics*, D. C. Heath, Boston, 1960.)

* A vectorial formulation of the scalar Kirchhoff theory is discussed in J. D. Jackson, *Classical Electrodynamics*, p. 283. Also see Sommerfeld, *Optics*, p. 325. You might as well take a look at B. B. Baker and E. T. Copson, *The Mathematical Theory of Huygens' Principle*, as a general reference to diffraction. None of these texts is easy reading.

† C. L. Andrews, *Am. J. Phys.* **19**, 250 (1951); S. Silver, *J. Opt. Soc. Am.* **52**, 131 (1962).

be that which existed before the removal of the disk, namely zero, minus the contribution from the disk alone. Except for the sign, it is as if the source and screen had been taken away, leaving only the oscillators on the disk, rather than vice versa. In other words, the diffraction field, in this approximation, can be pictured as arising exclusively from a set of fictitious noninteracting oscillators distributed uniformly over the region of the aperture. This of course, is the essence of the Huygens–Fresnel principle.

We can expect, however, that instead of no interaction at all between electron-oscillators, there is a short-range effect, since the oscillator fields drop off with distance. In this physically more realistic view, the electrons within the vicinity of the aperture's edge are affected when the disk is removed. For large apertures, the number of oscillators in the disk is much greater than the number along the edge. In such cases, if the point of observation is far away and in the forward direction, the Huygens–Fresnel principle should, and does, work well (Fig. 10.4). For very small apertures, or at points of observation in the vicinity of the aperture, edge effects become important, and we can anticipate difficulties. Indeed, at a point within the aperture itself, the electron-oscillators on the edge are of the greatest significance because of their proximity. Yet these electrons were certainly not unaffected by the removal of the adjacent oscillators of the disk. Thus, the deviation from the Huygens–Fresnel principle should be appreciable.

10.1.2 Fraunhofer and Fresnel Diffraction

Imagine that we have an opaque shield, Σ, containing a single small aperture, which is being illuminated by plane waves from a distant point source, S. The plane of observation σ is a screen parallel with, and very close to, Σ. Under these conditions an image of the aperture is projected onto the screen, which is clearly recognizable despite some slight fringing around its periphery. If the plane of observation is moved farther away from Σ, the image of the aperture, although still easily recognizable, becomes increasingly more structured as the fringes become more prominent. This phenomenon is known as **Fresnel** or **near-field** diffraction. If the plane of observation is slowly moved out still farther, a continuous change in the fringes results. At a very great distance from Σ the projected pattern will have spread out considerably, bearing little or no resemblance to the actual aperture. Thereafter moving σ essentially changes only the size of the pattern and not its shape. This is **Fraunhofer** or **far-field** diffraction. If at that point we could sufficiently reduce the wavelength of the incoming radiation, the pattern would revert to the Fresnel case. If λ were decreased even more, so that it approached zero, the fringes would disappear, and the image would take on the limiting shape of the aperture, as predicted by geometrical optics. Returning to the original setup, if the point source was now moved toward Σ, spherical waves would impinge on the aperture, and a Fresnel pattern would exist, even on a distant plane of observation.

In other words, consider a point source S and a point of observation P, where both are very far from Σ and no lenses are present (Problem 10.1). *As long as both the incoming and outgoing waves approach being planar (differing therefrom by a small fraction of a wavelength) over the extent of the diffracting apertures (or obstacles), Fraunhofer diffraction obtains.* Another way to appreciate this is to realize that the *phase* of each contribution at P, due to differences in the path traversed, is crucial to the determination of the resultant field. Moreover, if the wavefronts impinging on, and emerging from, the aperture are planar, then these path differences will be describable by a linear function of the two aperture variables. *This linearity in the aperture variables is the definitive mathematical criterion of Fraunhofer diffraction.* On the other hand, when S or P or both are too near Σ for the curvature of the incoming and outgoing wavefronts to be negligible, Fresnel diffraction prevails.

Each point on the aperture is to be visualized as a source of Huygens wavelets, and we should be a little concerned about their relative strengths. When S is nearby, compared with the size of the aperture, a spherical wavefront will illuminate the hole. The distances from S to each point on the aperture will be different, and the strength of the incident electric field (which drops off inversely with distance) will vary from point to point over the diffracting screen. That would not be the case for incoming homogeneous plane waves.

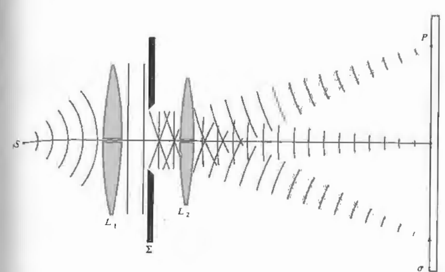


Figure 10.5 Fraunhofer diffraction.

Much the same thing is true for the diffracted waves going from the screen to P. Even if they are all emitted with the same amplitude (e.g., when the input beam is planar), if P is nearby, the waves converging on it are spherical and vary in amplitude, because of the different distances from various parts of the aperture to P. Ideally, for P at infinity the waves arriving there will be planar, and we need not worry about differences in field strength. That too contributes to the simplicity of the limiting Fraunhofer case.

As a practical rule of thumb, Fraunhofer diffraction will occur at an aperture (or obstacle) of greatest width a when

$$R > a^2/\lambda,$$

where R is the smaller of the two distances from S to Σ and Σ to P (Problem 10.1). Of course, when $R \equiv \infty$ the finite size of the aperture is of little concern. Moreover, an increase in λ clearly shifts the phenomenon toward the Fraunhofer extreme.

A practical realization of the Fraunhofer condition, where both S and P are effectively at infinity, is achieved by using an arrangement equivalent to that of Fig. 10.5. The point source S is located at F_1, the principal focus of lens L_1, and the plane of observation is the second focal plane of L_2. In the terminology of geometrical optics, the source plane and σ are conjugate planes.

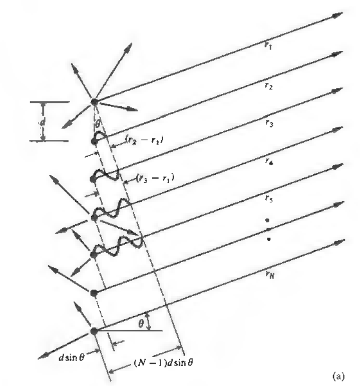
These same ideas can be generalized to any lens system forming an image of an extended source or object (Problem 10.5).* Indeed, the image would be a Fraunhofer diffraction pattern. It is because of these important practical considerations, as well as the inherent simplicity of Fraunhofer diffraction, that we will examine it before Fresnel diffraction, even though it is a special case of the latter.

10.1.3 Several Coherent Oscillators

As a simple yet logical bridge between the studies of interference and diffraction, consider the arrangement in Fig. 10.6. The illustration depicts a linear array of N coherent point oscillators (or radiating antennas), which are all identical, even to their polarization. For the moment, assume that the oscillators have no intrinsic phase difference; that is, they each have the same initial phase angle. The rays shown are all almost parallel, meeting at some very distant point P. If the spatial extent of the array is comparatively small, the separate wave amplitudes arriving at P will be essentially equal, having traveled nearly equal distances, that is,

$$E_0(r_1) = E_0(r_2) = \cdots = E_0(r_N) = E_0(r).$$

* A He–Ne laser can be set up to generate magnificent patterns without any auxiliary lenses, but this requires plenty of space.



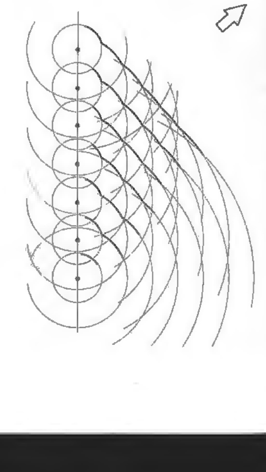


Figure 10.6 A linear array of in-phase coherent oscillators. (a) Note that at the angle shown $\delta = \pi$ while at $\theta = 0$, δ would be zero. (b) One of many sets of wavefronts emitted from a line of coherent point sources.

The sum of the interfering spherical wavelets yields an electric field at P, given by the real part of

$$E = E_0(r)e^{i(kr_1-\omega t)} + E_0(r)e^{i(kr_2-\omega t)} + \cdots + E_0(r)e^{i(kr_N-\omega t)}. \tag{10.1}$$

It should be clear, from Section 9.1, that we need not be concerned with the vector nature of the electric field for this configuration. Now then

$$E = E_0(r)e^{-i\omega t}e^{ikr_1} \times [1 + e^{ik(r_2-r_1)} + e^{ik(r_3-r_1)} + \cdots + e^{ik(r_N-r_1)}].$$

The phase difference between adjacent sources is obtained from the expression $\delta = k_0\Lambda$, and since $\Lambda = nd \sin\theta$, in a medium of index n, $\delta = kd \sin\theta$. Making use of Fig. 10.6, it follows that $\delta = k(r_2 - r_1)$, $2\delta = k(r_3 - r_1)$, and so on. Thus the field at P may be written as

$$E = E_0(r)e^{-i\omega t}e^{ikr_1} \times [1 + (e^{i\delta}) + (e^{i\delta})^2 + (e^{i\delta})^3 + \cdots + (e^{i\delta})^{N-1}]. \tag{10.2}$$

The bracketed geometric series has the value

$$(e^{i\delta N} - 1)/(e^{i\delta} - 1),$$

which can be rearranged into the form

$$\frac{e^{iN\delta/2}[e^{iN\delta/2} - e^{-iN\delta/2}]}{e^{i\delta/2}[e^{i\delta/2} - e^{-i\delta/2}]}$$

or equivalently

$$e^{i(N-1)\delta/2}\left[\frac{\sin N\delta/2}{\sin \delta/2}\right].$$

The field then becomes

$$E = E_0(r)e^{-i\omega t}e^{i[kr_1+(N-1)\delta/2]}\left(\frac{\sin N\delta/2}{\sin \delta/2}\right). \tag{10.3}$$

Notice that if we define R as the distance from the center of the line of oscillators to the point P, that is,

$$R = \tfrac{1}{2}(N-1)d\sin\theta + r_1,$$

then Eq. (10.3) takes on the form

$$E = E_0(r)e^{i(kR-\omega t)}\left(\frac{\sin N\delta/2}{\sin \delta/2}\right). \tag{10.4}$$

Finally, then, the flux-density distribution within the diffraction pattern due to N coherent, identical, distant point sources in a linear array is proportional to $EE^*/2$ for complex E or

$$I = I_0 \frac{\sin^2(N\delta/2)}{\sin^2(\delta/2)}, \tag{10.5}$$

where I_0 is the flux density from any single source arriving at P. (See Problem 10.2 for a graphic derivation of the irradiance.) For $N = 0$, $I = 0$, for $N = 1$, $I = I_0$, and for $N = 2$, $I = 4I_0\cos^2(\delta/2)$, in accord with Eq. (9.17). The functional dependence of I on θ is more apparent in the form

$$I = I_0 \frac{\sin^2[N(kd/2)\sin\theta]}{\sin^2[(kd/2)\sin\theta]}. \tag{10.6}$$

The $\sin^2[N(kd/2)\sin\theta]$ term undergoes rapid fluctuations, whereas the function that modulates it, $\{\sin[(kd/2)\sin\theta]\}^{-2}$, varies relatively slowly. The combined expression gives rise to a series of sharp principal peaks separated by small subsidiary maxima. The principal maxima occur in directions θ_m, such that $\delta = 2m\pi$, where $m = 0, \pm1, \pm2, \ldots$. Because $\delta = kd\sin\theta$,

$$d\sin\theta_m = m\lambda. \tag{10.7}$$

Since $[\sin^2 N\delta/2]/[\sin^2 \delta/2] = N^2$ for $\delta = 2m\pi$ (from L'Hospital's rule), the principal maxima have values of $N^2 I_0$. This is to be expected, inasmuch as all the oscillators are in phase at that orientation. The system will radiate a maximum in a direction perpendicular to the array ($m = 0$, $\theta_0 = 0$ and π). As θ increases, δ increases and I falls off to zero at $N\delta/2 = \pi$, its first minimum. Note that if $d < \lambda$ in Eq. (10.7), only the $m = 0$ or zero-order principal maximum exists. *If we were looking at an idealized line source of electron-oscillators separated by atomic distances, we could expect only that one principal maximum in the light field.*

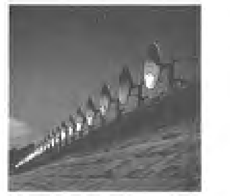


Figure 10.7 Interferometric radio telescope at the University of Sydney, Australia ($N = 32$, $\lambda = 21$ cm, $d = 7$ m, 2 m diameter, 700 ft. east–west base line). (Photo courtesy of Prof. W. N. Christiansen.)

The antenna array in Fig. 10.7 can transmit radiation in the narrow beam or lobe corresponding to a principal maximum. (The parabolic dishes shown reflect in the forward direction, and the radiation pattern is no longer symmetrical around the common axis.) Suppose that we have a system in which we can introduce an intrinsic phase shift of ε between adjacent oscillators. In that case

$$\delta = kd\sin\theta + \varepsilon;$$

the various principal maxima will occur at new angles

$$d\sin\theta_m = m\lambda - \varepsilon/k.$$

Concentrating on the central maximum $m = 0$, we can vary its orientation θ_0 at will by merely adjusting the value of ε.

The principle of reversibility, which states that without absorption, wave motion is reversible, leads to the same field pattern for an antenna used as either a transmitter or a receiver. The array, functioning as a radio telescope, can therefore be "pointed" by combining the output from the individual antennas with an appropriate phase shift, ε, introduced between each of them. For a given ε the output of the system corresponds to the signal impinging on the array from a specific direction in space.

Figure 10.7 is a photograph of the first multiple radio interferometer, designed by W. N. Christiansen and built in Australia in 1951. It consists of 32 parabolic antennas, each 2 m in diameter, designed to function in phase at the wavelength of the 21-cm hydrogen emission line. The antennas are arranged along an east–west base line with 7 m separating each one. This particular array utilizes the Earth's rotation as the scanning mechanism.*

Examine Fig. 10.8, which depicts an idealized line source of electron-oscillators (e.g., the secondary sources of the Huygens–Fresnel principle for a long slit whose width is much less than λ, illuminated by plane waves). Each point emits a spherical wavelet, which we write as

$$E = \left(\frac{\mathcal{E}_0}{r}\right) \sin(\omega t - kr),$$

explicitly indicating the inverse r-dependence of the amplitude. The quantity $\mathcal{E}_0$ is said to be the *source strength*. The present situation is distinct from that of Fig. 10.6, since now the sources are very weak, their number, N, is tremendously large, and the separation between them is vanishingly small. A minute but finite segment of the array Δy_i will contain $\Delta y_i(N/D)$ sources, where D is the entire length of the array. Imagine that the array is divided up into M such segments (i.e., i goes from 1 to M). The contribution to the electric field intensity at P from the ith segment is accordingly

$$E_i = \left(\frac{\mathcal{E}_0}{r_i}\right) \sin(\omega t - kr_i)\left(\frac{N\Delta y_i}{D}\right),$$

provided that Δy_i is so small that the oscillators within it have a negligible relative phase difference ($r_i =$ constant), and their fields simply add constructively. We can cause the array to become a continuous (coherent) line source by letting N approach infinity. This description, besides being fairly realistic on a macroscopic scale, also allows the use of the calculus for more complicated geometries. Certainly as N approaches infinity, the

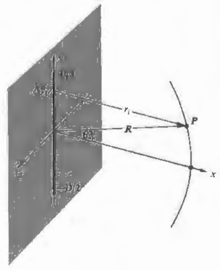


Figure 10.8 A coherent line source.

source strengths of the individual oscillators must diminish to nearly zero, if the total output is to be finite. We can therefore define a constant $\mathcal{E}_L$ as the *source strength per unit length* of the array, that is,

$$\mathcal{E}_L = \frac{1}{D} \lim_{N\to\infty} (\mathcal{E}_0 N). \tag{10.8}$$

The net field at P from all M segments is

$$E = \sum_{i=1}^{M} \frac{\mathcal{E}_L}{r_i} \sin(\omega t - kr_i)\Delta y_i.$$

For a continuous line source the Δy_i must become infinitesimal ($M \to \infty$), and the summation is then transformed into a definite integral

$$E = \mathcal{E}_L \int_{-D/2}^{+D/2} \frac{\sin(\omega t - kr)}{r}\, dy, \tag{10.9}$$

where $r = r(y)$. The approximations used to evaluate Eq. (10.9) must depend on the position of P with respect to the array and will therefore make the distinction between Fraunhofer and Fresnel diffraction. The coherent *optical* line source does not now exist as a physical entity, but we will make good use of it as a mathematical device.

* See E. Brookner, "Phased-Array Radars," *Sci. Am.* (Feb. 1985), p. 94.

10.2 FRAUNHOFER DIFFRACTION

10.2.1 The Single Slit

Return to Fig. 10.8, where now the point of observation is very distant from the coherent line source and $R \gg D$. Under these circumstances $r(y)$ never deviates appreciably from its midpoint value R, so that the quantity $(\mathcal{E}_L/R)$ at P is essentially constant for all elements dy. It follows from Eq. (10.9) that the field at P due to the differential segment of the source dy is

$$dE = \frac{\mathcal{E}_L}{R} \sin(\omega t - kr)\, dy, \tag{10.10}$$

where $(\mathcal{E}_L/R)\, dy$ is the amplitude of the wave. Notice that the phase is much more sensitive to variations in $r(y)$ than is the amplitude, so that we will have to be more careful about introducing approximations into it. We can expand $r(y)$, in precisely the same manner as was done in Problem (9.13), to make it an explicit function of y; thus

$$r = R - y \sin\theta + (y^2/2R)\cos^2\theta + \cdots, \tag{10.11}$$

where θ is measured from the xz-plane. The third term can be ignored so long as its contribution to the phase is insignificant even when $y = \pm D/2$; that is, $(\pi D^2/4\lambda R)\cos^2\theta$ must be negligible. This will be true for all values of θ when R is adequately large. We now have the **Fraunhofer condition**, where the distance r is linear in y: the distance to the point of observation and therefore the phase can be written as a linear function of the aperture variables. Substituting into Eq. (10.10) and integrating leads to

$$E = \frac{\mathcal{E}_L}{R} \int_{-D/2}^{+D/2} \sin[\omega t - k(R - y\sin\theta)]\, dy, \tag{10.12}$$

and finally

$$E = \frac{\mathcal{E}_L D}{R} \frac{\sin[(kD/2)\sin\theta]}{(kD/2)\sin\theta} \sin(\omega t - kR). \tag{10.13}$$

To simplify the appearance of things let

$$\beta = (kD/2)\sin\theta, \tag{10.14}$$

so that

$$E = \frac{\mathcal{E}_L D}{R}\left(\frac{\sin\beta}{\beta}\right) \sin(\omega t - kR). \tag{10.15}$$

The quantity most readily measured is the irradiance (forgetting the constants) $I(\theta) = \langle E^2 \rangle$ or

$$I(\theta) = \frac{1}{2}\left(\frac{\mathcal{E}_L D}{R}\right)^2 \left(\frac{\sin\beta}{\beta}\right)^2, \tag{10.16}$$

where $\langle \sin^2(\omega t - kR)\rangle = \frac{1}{2}$. When $\theta = 0$, $\sin\beta/\beta = 1$ and $I(\theta) = I(0)$, which corresponds to the *principal maximum. The irradiance resulting from an idealized coherent line source in the Fraunhofer approximation* is then

$$I(\theta) = I(0)\left(\frac{\sin\beta}{\beta}\right)^2 \tag{10.17}$$

or, using the *sinc function* (Section 7.9 and Table 1 of the Appendix),

$$I(\theta) = I(0)\,\mathrm{sinc}^2\,\beta.$$

There is symmetry about the y-axis, and this expression holds for θ measured in any plane containing that axis. Notice that since $\beta = (\pi D/\lambda)\sin\theta$, when $D \gg \lambda$, the irradiance drops extremely rapidly as θ deviates from zero. This arises from the fact that β becomes very large for large values of length D (a centimeter or so when using light). The phase of the line source is equivalent, by way of Eq. (10.15), to that of a point source located at the center of the array, a distance R from P. Finally, a relatively long coherent line source ($D \gg \lambda$) can be envisioned as a single point emitter radiating predominantly in the forward, $\theta = 0$, direction; in other words, its emission resembles a circular wave in the xz-plane. In contrast, notice that if $\lambda \gg D$, β is small, $\sin\beta \approx \beta$, and $I(\theta) \approx I(0)$. The irradiance is then constant for *all* θ, and the line source resembles a point source emitting spherical waves.

We can now turn our attention to the problem of Fraunhofer diffraction by a slit or elongated narrow rectangular hole (Fig. 10.9). An aperture of this sort might typically have a width of several hundred λ and a length of a few centimeters. The usual procedure to follow in the analysis is to divide the slit into a series of long differential strips (dz by ℓ) parallel to the y-axis,

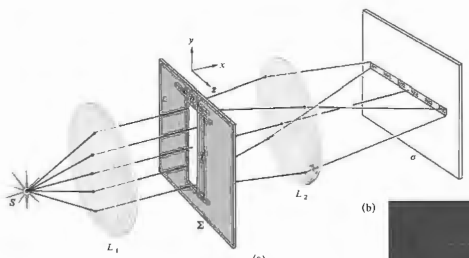


Figure 10.9 (a) Single-slit Fraunhofer diffraction. (b) Diffraction pattern of a single vertical slit under point-source illumination.

as shown in Fig. 10.10. We immediately recognize, however, that each strip is a long coherent line source and can therefore be replaced by a point emitter on the z-axis. In effect, each such emitter radiates a circular wave in the ($y = 0$ or) xz-plane. This is certainly reasonable, since the slit is long and the emerging wavefronts are practically unobstructed in the slit direction. There will thus be very little diffraction parallel to the edges of the slit. The problem has been reduced to that of finding the field in the xz-plane due to an infinite number of point sources extending across the width of the slit along the z-axis. We then need only evaluate the integral of the contribution dE from each element dz in the Fraunhofer approximation. But once again, this is equivalent to a coherent line source, so that the complete solution for the slit is, as we have seen,

$$I(\theta) = I(0)\left(\frac{\sin \beta}{\beta}\right)^2, \qquad [10.17]$$

provided that

$$\beta = (kb/2) \sin \theta \qquad (10.18)$$

and θ is measured from the xy-plane (see Problem 10.3). Note that here the line source is short, $D = b$, β is not large, and although the irradiance falls off rapidly, higher-order subsidiary maxima will be observable. The extrema of $I(\theta)$ occur at values of β that cause $dI/d\beta$ to be zero, that is,

$$\frac{dI}{d\beta} = I(0)\frac{2 \sin \beta(\beta \cos \beta - \sin \beta)}{\beta^3} = 0. \qquad (10.19)$$

The irradiance has minima, equal to zero, when $\sin \beta = 0$, whereupon

$$\beta = \pm\pi, \pm 2\pi, \pm 3\pi, \ldots . \qquad (10.20)$$

It also follows from Eq. (10.19) that when

$$\beta \cos \beta - \sin \beta = 0$$

$$\tan \beta = \beta. \qquad (10.21)$$

The solutions to this transcendental equation can be determined graphically, as shown in Fig. 10.11. The points of intersection of the curves $f_1(\beta) = \tan \beta$ with the straight line $f_2(\beta) = \beta$ are common to both and so satisfy Eq. (10.21). Only one such extremum exists between adjacent minima (10.20), so that $I(\theta)$ must have subsidiary maxima at these values of β ($\pm 1.4303\pi$, $\pm 2.4590\pi$, $\pm 3.4707\pi, \ldots$).

There is a particularly easy way to appreciate what's happening here with the aid of Fig. 10.12. We envision every point in the aperture emitting rays in all directions in the xz-plane. The light that continues to propagate directly forward in Fig. 10.12(a) is the undiffracted beam, all the rays arrive on the viewing screen in phase,

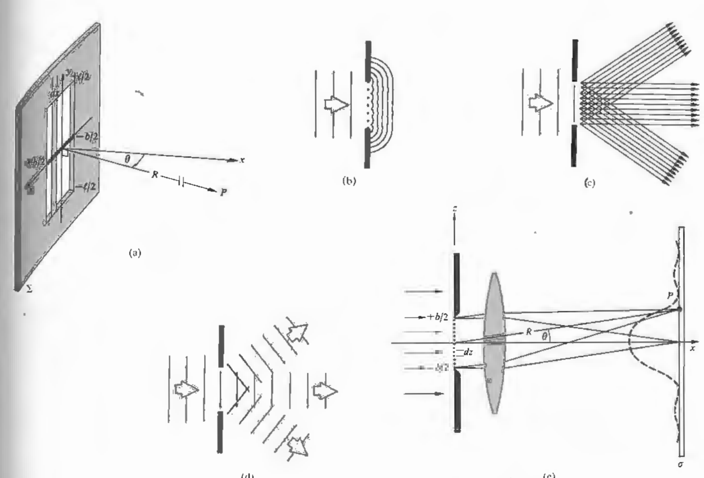


Figure 10.10 (a) Point P on σ is essentially infinitely far from Σ. (b) Huygens wavelets emitted across the aperture. (c) The equivalent representation in terms of rays. Each point emits rays in all directions. The parallel rays in various directions are seen. (d) These ray bundles correspond to plane waves, which can be thought of as the three-dimensional Fourier components. (e) A single slit illuminated by monochromatic plane waves.

and a central bright spot will be formed by them. If the screen is not actually at infinity, the rays that converge to it are not quite parallel but with it at infinity, or better still, with a lens in place, the rays are as drawn. Figure 10.12(b) shows the specific bundle of rays coming off at an angle θ_1 where the path-length difference between the rays from the very top and bottom, $b \sin \theta_1$, is made equal to one wavelength. A ray from the middle of the slit will then lag $\frac{1}{2}\lambda$ behind a ray from the top and exactly cancel it. Similarly, a ray from just below center will cancel a ray from just below the top, and so on; all across the aperture ray-pairs will cancel, yielding a minimum. The irradiance has dropped from its high central maximum to the first zero on either side at $\sin \theta_1 = \pm\lambda/b$.

As the angle increases further, some small fraction of the rays will again interfere constructively, and the irradiance will rise to form a subsidiary peak. A further increase in the angle produces another minimum, as shown in Fig. 10.12(c), when $b \sin \theta_2 = 2\lambda$. Now imagine the aperture divided into quarters. Ray by ray, the top quarter will cancel the one beneath it, and the next, the

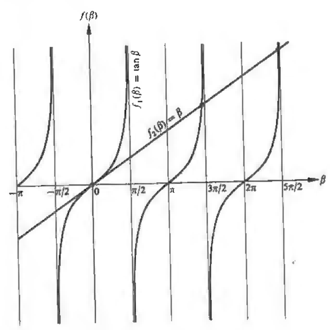


Figure 10.11 The points of intersection of the two curves are the solutions of Eq. (10.21).

third, will cancel the last quarter. Ray-pairs at the same locations in adjacent segments are $\lambda/2$ out of phase and destructively interfere. In general then, zeros of irradiance will occur when

$$b \sin \theta_m = m\lambda,$$

where $m = \pm 1, \pm 2, \pm 3, \ldots$, which is equivalent to Eq. (10.20), since $\beta = m\pi = (kb/2) \sin \theta_m$.

We should inject a note of caution at this point: one of the frailties of the Huygens–Fresnel principle is that it does not take proper regard of the variations in amplitude, with angle, over the surface of each secondary wavelet. We will come back to this when we consider the *obliquity factor* in Fresnel diffraction, where the effect is significant. In Fraunhofer diffraction the distance from the aperture to the plane of observation is so large that we need not be concerned about it, provided that θ remains small.

Figure 10.13 is a plot of the flux density, as expressed by Eq. (10.17). Envision some point on the curve, for example, the third subsidiary maximum at $\beta =$

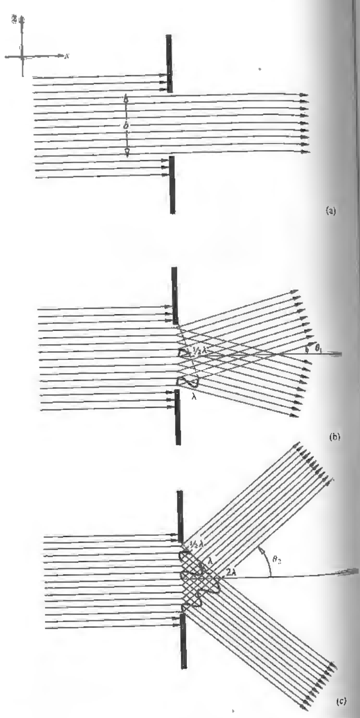


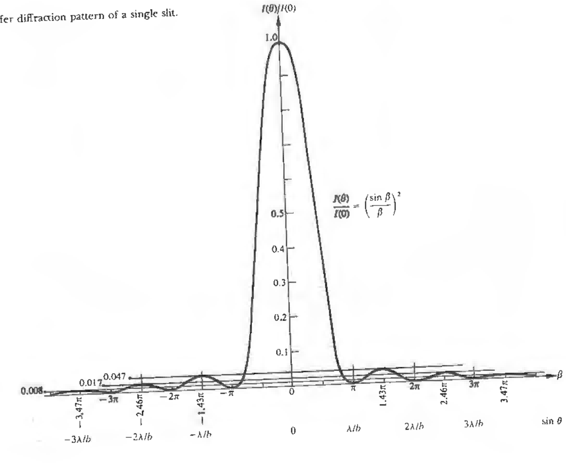
Figure 10.12 The diffraction of light in various directions. Here the aperture is a single slit, as in Fig. 10.10.

3.4707π; since $\beta = (\pi b/\lambda) \sin \theta$, an increase in the slit width b requires a decrease in θ, if β is to be constant. Under these conditions the pattern shrinks in toward the principal maximum, as it would if λ were decreased. If the source emits white light, the higher-order maxima show a succession of colors trailing off into red with increasing θ. Each different colored light component has its minima and subsidiary maxima at angular positions characteristic of that wavelength (Problem 10.6). Indeed, only in the region about $\theta = 0$ will all the constituent colors overlap to yield white light.

The point source S in Fig. 10.9 would be imaged at the position of the center of the pattern, if the diffracting screen Σ were removed. Under this sort of illumination, the pattern produced with the slit in place is a series of dashes in the yz-plane of the screen σ, much like a spread-out image of S [Fig. 10.9(b)]. An incoherent line source (in place of S) positioned parallel to the slit, in the focal plane of the collimator L_1, will broaden the pattern out into a series of bands. Any point on the line source generates an independent diffraction pattern, which is displaced, with respect to the others, along the y-direction. With no diffracting screen present, the image of the line source would be a line parallel to the original slit. With the screen in place the line is spread out, as was the point image of S (Fig. 10.14). Keep in mind that it's the small dimension of the slit that does the spreading out.

The single-slit pattern is easily observed without the use of special equipment. Any number of sources will do (e.g., a distant street light at night, a small incandescent lamp, sunlight streaming through a narrow space

Figure 10.13 The Fraunhofer diffraction pattern of a single slit.



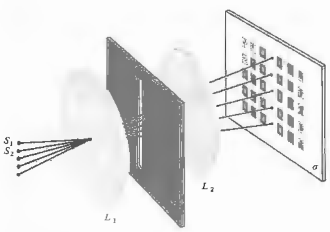


Figure 10.14 The single-slit pattern with a line source. See first photograph of Fig. 10.17.

in a window shade); almost anything that resembles a point or line source will serve. Probably the best source for our purposes is an ordinary clear, *straight-filament* display bulb (the kind in which the filament is vertical and about 3 inches long). You can use your imagination to generate all sorts of single-slit arrangements (e.g., a comb or fork rotated to decrease the projected space between the tines, or a scratch across a layer of india ink on a microscope slide). An inexpensive vernier caliper makes a remarkably good variable slit. Hold the caliper close to your eye with the slit, a few thousandths of an inch wide, parallel to the filament of the lamp. Focus your eye beyond the slit at infinity, so that its lens serves as L_2.

10.2.2 The Double Slit

It might at first seem from Fig. 10.10 that the location of the principal maximum is always to be in line with the center of the diffracting aperture; this, however, is not generally true. The diffraction pattern is actually centered about the axis of the lens and has exactly the same shape and location, regardless of the slit's position, as long as its orientation is unchanged and the approximations are valid (Fig. 10.15). All waves traveling parallel to the lens axis converge on the second focal point of L_2; this then is the image of S and the center of the diffraction pattern. Suppose now that we have two long slits of width b and center-to-center separation a (Fig. 10.16). Each aperture, by itself, would generate the same single-slit diffraction pattern on the viewing screen σ. At any point on σ, the contributions from the two slits overlap, and even though each must be essentially equal in amplitude, they may well differ significantly in phase. Since the same primary wave excites the secondary sources at each slit, the resulting wavelets will be coherent, and interference must occur. If the primary plane wave is incident on Σ at some angle θ (see Problem 10.3), there will be a constant relative phase difference between the secondary sources. At normal incidence, the wavelets are all emitted in phase. The interference fringe at a particular point of observation is determined by the differences in the optical path lengths traversed by the overlapping wavelets from the two slits. As we will see, the flux-density distribution (Fig. 10.17) is the result of a rapidly varying double-slit interference system modulated by a single-slit diffraction pattern.

To obtain an expression for the optical disturbance at a point on σ, we need only slightly reformulate the single-slit analysis. Each of the two apertures is divided into differential strips (dz by ℓ), which in turn behave like an infinite number of point sources aligned along

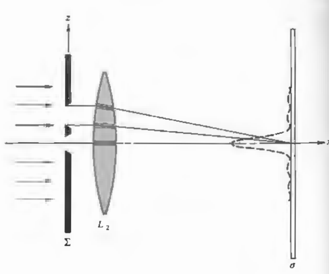


Figure 10.15 The double-slit setup.

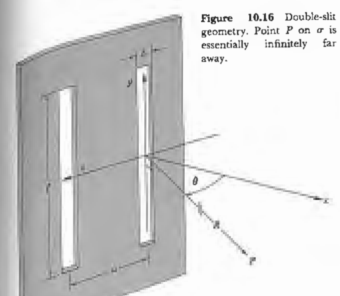


Figure 10.16 Double-slit geometry. Point P on σ is essentially infinitely far away.

the z-axis. The total contribution to the electric field, in the Fraunhofer approximation (10.12), is then

$$E = C\int_{-b/2}^{b/2} F(z)\,dz + C\int_{a-b/2}^{a+b/2} F(z)\,dz, \qquad (10.22)$$

where $F(z) = \sin[\omega t - k(R - z\sin\theta)]$. The constant-amplitude factor C is the secondary source strength per unit length along the z-axis (assumed to be independent of z over each aperture) divided by R, which is measured from the origin to P and is taken as constant. We will be concerned only with relative flux densities on σ, so that the actual value of C is of little interest to us now. Integration of Eq. (10.22) yields

$$E = bC\left(\frac{\sin\beta}{\beta}\right)[\sin(\omega t - kR) + \sin(\omega t - kR + 2\alpha)], \qquad (10.23)$$

Figure 10.17 Single- and double-slit Fraunhofer patterns. The faint cross-hatching arises entirely in the printing process. (Photos courtesy M. Cagnet, M. Francon, and J. C. Thrierr: *Atlas optischer Erscheinungen*, Berlin–Heidelberg–New York: Springer, 1962.)

with $\alpha = (ka/2)\sin\theta$ and, as before, $\beta = (kb/2)\sin\theta$. This is just the sum of the two fields at P, one from each slit, as given by Eq. (10.15). The distance from the first slit to P is R, giving a phase contribution of $-kR$. The distance from the second slit to P is $(R - a\sin\theta)$ or $(R - 2\alpha/k)$, yielding a phase term equal to $(-kR + 2\alpha)$, as in the second sine function. The quantity 2β is the phase difference $(k\Lambda)$ between two nearly parallel rays, arriving at a point P on σ, from the edges of one of the slits. The quantity 2α is the phase difference between two waves arriving at P, one having originated at any point in the first slit, the other coming from the corresponding point in the second slit. Simplifying Eq. (10.23) a bit further, it becomes

$$E = 2bC\left(\frac{\sin\beta}{\beta}\right)\cos\alpha\,\sin(\omega t - kR + \alpha),$$

which when squared and averaged over a relatively long interval in time is the irradiance

$$I(\theta) = 4I_0\left(\frac{\sin^2\beta}{\beta^2}\right)\cos^2\alpha. \qquad (10.24)$$

In the $\theta = 0$ direction (i.e., when $\beta = \alpha = 0$), I_0 is the flux-density contribution from either slit, and $I(0) = 4I_0$ is the total flux density. The factor of 4 comes from the fact that the amplitude of the electric field is twice what it would be at that point with one slit covered.

If in Eq. (10.24) b becomes vanishingly small ($kb \ll 1$), then $(\sin\beta)/\beta \approx 1$, and the equation reduces to the flux-density expression for a pair of long line sources, that is, Young's experiment, Eq. (9.17). If on the other hand $a = 0$, the two slits coalesce into one, $\alpha = 0$, and Eq. (10.24) becomes $I(0) = 4I_0(\sin^2\beta)/\beta^2$. This is the equivalent of Eq. (10.17) for single-slit diffraction with the source strength doubled. We might then envision the total expression as being generated by a $\cos^2\alpha$ interference term modulated by a $(\sin^2\beta)/\beta^2$ diffraction term. If the slits are finite in width but very narrow, the diffraction pattern from either slit will be uniform over a broad central region, and bands resembling the idealized Young's fringes will appear within that region. At angular positions (θ-values) where

$$\beta = \pm\pi, \pm 2\pi, \pm 3\pi, \ldots$$

diffraction effects are such that no light reaches σ, and

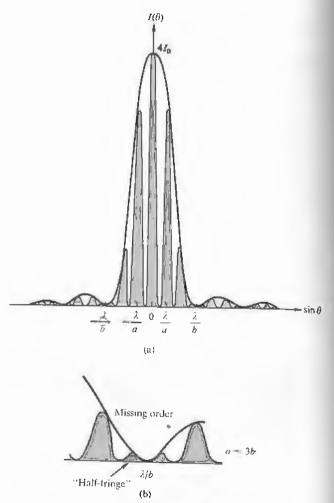


Figure 10.18 A double-slit pattern ($a = 3b$).

clearly none is available for interference. At points on σ where

$$\alpha = \pm\pi/2, \pm 3\pi/2, \pm 5\pi/2, \ldots$$

the various contributions to the electric field will be completely out of phase and will cancel, regardless of the actual amount of light made available from the diffraction process.

The irradiance distribution for a double-slit Fraunhofer pattern is illustrated in Fig. 10.18. Notice that it is a combination of Figs. 9.6 and 10.13. The curve is for the particular case in which $a = 3b$ (i.e., $\alpha = 3\beta$). You can get a rough idea of what the pattern will look like, since if $a = mb$, where m is any number, there will be $2m$ bright fringes (counting "fractional fringes" as well)* within the central diffraction peak (Problem 10.10). An interference maximum and a diffraction minimum (zero) may correspond to the same θ-value. In that case no light is available at that precise position to partake in the interference process, and the suppressed peak is said to be a *missing order*.

The double-slit pattern is also rather easily observed, and the seeing is well worth the effort. A straight-filament, tubular bulb is again the best line source. For slits, coat a microscope slide with India ink; if you happen to have some, a colloidal suspension of graphite in alcohol works even better (it's more opaque). Scratch a pair of slits across the dry ink with a razor blade and stand about 10 feet from the source. Hold the slits parallel to the filament and close to your eye, which, when focused at infinity, will serve as the needed lens. Interpose red or blue cellophane and observe the change in the width of the fringes. Find out what happens when you cover one and then both of the slits with a microscope slide. Move the slits slowly in the z-direction; then holding them stationary, move your eye in the z-direction. Verify that the position of the center of the pattern is indeed determined by the lens and not the aperture.

10.2.3 Diffraction by Many Slits

The procedure for obtaining the irradiance function for a monochromatic wave diffracted by many slits is essentially the same as that used when considering two slits. Here again, the limits of integration must be appropriately altered. Consider the case of N long, parallel, narrow slits, each of width b and center-to-center separation a, as illustrated in Fig. 10.19. With the origin of the coordinate system once more at the center of the first slit, the total optical disturbance at a point on the screen σ is given by

* Notice that m need not be an integer. Moreover, if m is an integer, there will be "half-fringes," as shown in Fig. 10.18(b).

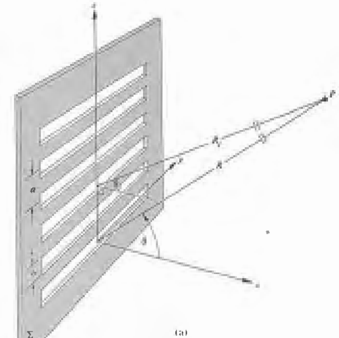


Figure 10.19(a) Multi-slit geometry. Again point P is on σ essentially infinitely far from Σ.

$$E = C\int_{-b/2}^{b/2} F(z)\,dz + C\int_{a-b/2}^{a+b/2} F(z)\,dz + C\int_{2a-b/2}^{2a+b/2} F(z)\,dz + \cdots + C\int_{(N-1)a-b/2}^{(N-1)a+b/2} F(z)\,dz, \qquad (10.25)$$

where as before, $F(z) = \sin[\omega t - k(R - z\sin\theta)]$. This applies to the Fraunhofer condition, so that the aperture configuration must be such that all the slits are close to the origin, and the approximation (10.11)

$$r = R - z\sin\theta \qquad (10.26)$$

applies over the entire array. The contribution from the jth slit (where the first one is numbered zero), obtained by evaluating only that one integral in Eq.

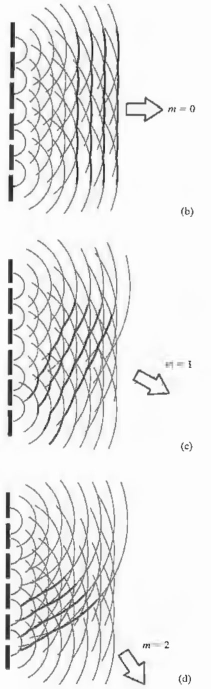


Figure 10.19(b, c, d)

(10.25), is then

$$E_j = \frac{C}{k \sin\theta}[\sin(\omega t - kR)\sin(kz\sin\theta) - \cos(\omega t - kR)\cos(kz \sin\theta)]_{ja-b/2}^{ja+b/2},$$

provided that we require $\theta_j \approx \theta$. After some manipula-tion this becomes,

$$E_j = bC\left(\frac{\sin\beta}{\beta}\right)\sin(\omega t - kR + 2\alpha j), \qquad (10.27)$$

recalling that $\beta = (kb/2)\sin\theta$ and $\alpha = (ka/2)$ sin
Notice that this is equivalent to the expression for a li
source (10.15) or, of course, a single slit, where in acco
with Eq. 10.26 and Fig. 10.19, $R_j = R - ja\sin\theta$, so th
$-kR + 2\alpha j = -kR_j$. The total optical disturbance as given by Eq. (10.25), is simply the sum of the contribu-tions from each of the slits; that is,

$$E = \sum_{j=0}^{N-1} E_j$$

or

$$E = \sum_{j=0}^{N-1} bC\left(\frac{\sin\beta}{\beta}\right)\sin(\omega t - kR + 2\alpha j). \qquad (10.28)$$

This in turn can be written as the imaginary part of a complex exponential:

$$E = \mathrm{Im}\left[bC\left(\frac{\sin\beta}{\beta}\right)e^{i(\omega t - kR)}\sum_{j=0}^{N-1}(e^{i2\alpha})^j\right]. \qquad (10.29)$$

But we have already evaluated this same geometric series in the process of simplifying Eq. (10.2). Equation (10.29) therefore reduces to the form

$$E = bC\left(\frac{\sin\beta}{\beta}\right)\left(\frac{\sin N\alpha}{\sin\alpha}\right)\sin[\omega t - kR + (N-1)\alpha]. \qquad (10.30)$$

The distance from the center of the array to the point P is equal to $[R - (N-1)(a/2)\sin\theta]$, and therefore the phase of E at P corresponds to that of a wave emitted from the midpoint of the source. The flux-density distri-bution function is

$$I(\theta) = I_0\left(\frac{\sin\beta}{\beta}\right)^2\left(\frac{\sin N\alpha}{\sin\alpha}\right)^2. \qquad (10.31)$$

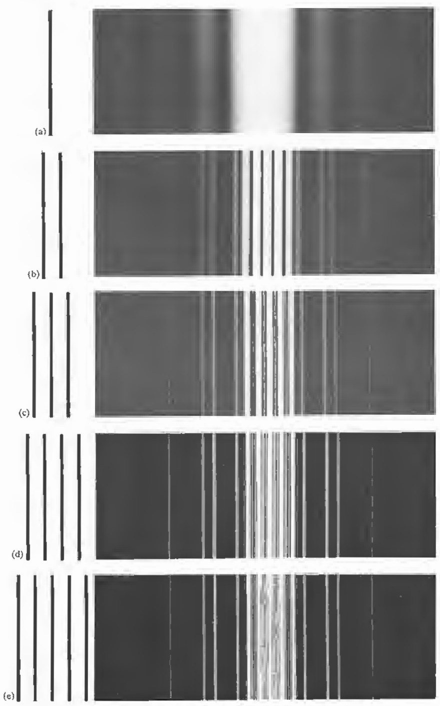


Figure 10.20 Diffraction patterns for slit systems shown at left.

Note that I_0 is the flux density in the $\theta = 0$ direction emitted by any one of the slits and that $I(0) = N^2 I_0$. In other words, the waves arriving at P in the forward direction are all in phase, and their fields add constructively. Each slit by itself would generate precisely the same flux-density distribution. Superimposed, the various contributions yield a multiple wave interference system modulated by the single-slit diffraction envelope. If the width of each aperture were shrunk to zero, Eq. (10.31) would become the flux-density expression (10.6) for a linear coherent array of oscillators. As in that earlier treatment (10.17), **principal maxima** occur when $(\sin N\alpha/\sin\alpha) = N$, that is, when

$$\alpha = 0, \pm\pi, \pm 2\pi, \ldots$$

or equivalently, since $\alpha = (ka/2)\sin\theta$,

$$a \sin\theta_m = m\lambda \tag{10.32}$$

with $m = 0, \pm 1, \pm 2, \ldots$. This is quite general and gives rise to the same θ-locations for these maxima, regardless of the value of $N \geq 2$. Minima, of zero flux density, exist whenever $(\sin N\alpha/\sin\alpha)^2 = 0$ or when

$$\alpha = \pm\frac{\pi}{N}, \pm\frac{2\pi}{N}, \pm\frac{3\pi}{N}, \ldots, \pm\frac{(N-1)\pi}{N}, \pm\frac{(N+1)\pi}{N}, \ldots \tag{10.33}$$

Between consecutive principal maxima (i.e., over the range in α of π) there will therefore be $N - 1$ minima. And of course between each pair of minima there will have to be a **subsidiary maximum**. The term $(\sin N\alpha/\sin\alpha)^2$, which we can think of as embodying the interference effects, has a rapidly varying numerator and a slowly varying denominator. The subsidiary maxima are therefore located approximately at points where $\sin N\alpha$ has its greatest value, namely,

$$\alpha = \pm\frac{3\pi}{2N}, \pm\frac{5\pi}{2N}, \ldots \tag{10.34}$$

The $N - 2$ *subsidiary maxima* between consecutive principal maxima are clearly visible in Fig. 10.20. We can get some idea of the flux density at these peaks by rewriting Eq. (10.31) as

$$I(\theta) = \frac{I(0)}{N^2}\left(\frac{\sin\beta}{\beta}\right)^2\left(\frac{\sin N\alpha}{\sin\alpha}\right)^2, \tag{10.35}$$

where at the points of interest $|\sin N\alpha| = 1$. For large N, α is small and $\sin^2\alpha \approx \alpha^2$. At the first subsidiary peak $\alpha = 3\pi/2N$, in which case

$$I \approx I(0)\left(\frac{\sin\beta}{\beta}\right)^2\left(\frac{2}{3\pi}\right)^2, \tag{10.36}$$

and the flux density has dropped to about $\frac{1}{22}$ of that at the adjacent principal maximum (see Problem 10.12). Since $(\sin\beta)/\beta$ for small β varies slowly, it will not differ from 1 appreciably, close to the zeroth-order principal maximum, so that $I/I(0) \approx \frac{1}{22}$. This flux-density ratio for the next secondary peak is down to $\frac{1}{61}$, and it continues to decrease as α approaches a value halfway between the principal maxima. At that symmetry point $\alpha \approx \pi/2$, $\sin\alpha \approx 1$, and the flux-density ratio has its lowest value, approximately $1/N^2$. Thereafter $\alpha > \pi/2$ and the flux densities of the subsidiary maxima begin to increase.

Try duplicating Fig. 10.20 using a tubular bulb and homemade slits. You'll probably have difficulty seeing the subsidiary maxima clearly, with the effect that the only perceptible difference between the double- and multiple-slit patterns may be an apparent broadening in the dark regions between principal maxima. As in Fig. 10.20, the dark regions will become wider than the bright bands as N increases and the secondary peaks fade out. If we consider each principal maximum to be bounded in width by two adjacent zeros, then each will extend over a length in θ, ($\sin\theta \approx \theta$) of approximately $2\lambda/Na$. As N increases, the principal maxima maintain their relative spacing (λ/a) while becoming increasingly narrow. Figure 10.21 shows the case of six slits, with $a = 4b$.

The multiple-slit interference term in Eq. 10.35 has the form $(\sin^2 N\alpha)/N^2\sin^2\alpha$; thus for large N, $(N^2\sin^2\alpha)^{-1}$ may be envisioned as the curve beneath which $\sin^2 N\alpha$ rapidly varies. Notice that for small α this interference term looks like $\text{sinc}^2 N\alpha$.

10.2.4 The Rectangular Aperture

Consider the configuration depicted in Fig. 10.22. A monochromatic plane wave propagating in the x-direction is incident on the opaque diffracting screen Σ. We

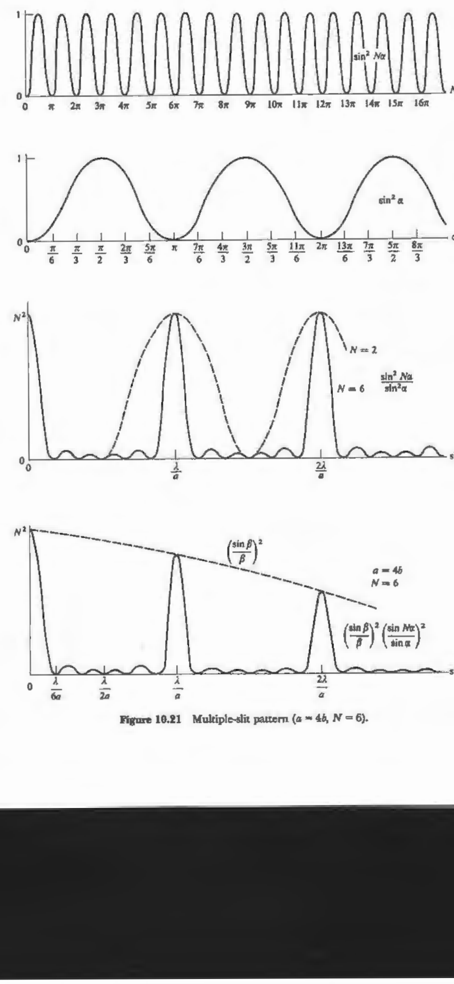


Figure 10.21 Multiple-slit pattern ($a = 4b$, $N = 6$).

wish to find the consequent (far-field) flux-density distribution in space or equivalently at some arbitrary distant point P. According to the Huygens–Fresnel principle, a differential area dS, within the aperture, may be envisioned as being covered with coherent secondary point sources. But dS is much smaller in extent than is λ, so that all the contributions at P remain in phase and interfere constructively. This is true regardless of θ: that is, dS emits a spherical wave (Problem 10.13). If $\mathcal{E}_A$ is the source strength per unit area, *assumed to be constant over the entire aperture*, then the optical disturbance at P due to dS is either the real or imaginary part of

$$dE = \left(\frac{\mathcal{E}_A}{r}\right) e^{i(\omega t - kr)}\, dS. \qquad (10.37)$$

The choice is yours and depends only on whether you like sine or cosine waves, there being no difference except for a phase shift. The distance from dS to P is

$$r = [X^2 + (Y - y)^2 + (Z - z)^2]^{1/2}, \qquad (10.38)$$

and as we have seen, the Fraunhofer condition occurs when this distance approaches infinity. As before, it will suffice to replace r by the distance $\overline{OP}$, that is, R, in the amplitude term, as long as the aperture is relatively small. But the approximation for r in the phase needs to be treated a bit more carefully; $k = 2\pi/\lambda$ is a large number. To that end we expand out Eq. (10.38) and by making use of

$$R = [X^2 + Y^2 + Z^2]^{1/2}, \qquad (10.39)$$

obtain

$$r = R[1 + (y^2 + z^2)/R^2 - 2(Yy + Zz)/R^2]^{1/2}. \qquad (10.40)$$

In the far-field case R is very large in comparison to the dimensions of the aperture, and the $(y^2 + z^2)/R^2$ term is certainly negligible. Since P is very far from Σ, θ can still be kept small, even though Y and Z are fairly large, and this mitigates any concern about the directionality of the emitters (the obliquity factor). Now

$$r = R[1 - 2(Yy + Zz)/R^2]^{1/2},$$

and dropping all but the first two terms in the binomial expansion, we have

$$r = R[1 - (Yy + Zz)/R^2].$$

The total disturbance arriving at P is

$$E = \frac{\mathcal{E}_A e^{i(\omega t - kR)}}{R} \iint_{\text{Aperture}} e^{ik(Yy + Zz)/R}\, dS. \qquad (10.41)$$

Consider the specific configuration shown in Fig. 10.23. Equation (10.41) can now be written as

$$E = \frac{\mathcal{E}_A e^{i(\omega t - kR)}}{R} \int_{-b/2}^{+b/2} e^{ikYy/R}\, dy \int_{-a/2}^{+a/2} e^{ikZz/R}\, dz,$$

where $dS = dy\, dz$. With $\beta' = kbY/2R$ and $\alpha' = kaZ/2R$, we have

$$\int_{-b/2}^{+b/2} e^{ikYy/R}\, dy = b\left(\frac{e^{i\beta'} - e^{-i\beta'}}{2i\beta'}\right) = b\left(\frac{\sin \beta'}{\beta'}\right)$$

and similarly

$$\int_{-a/2}^{+a/2} e^{ikZz/R}\, dz = a\left(\frac{e^{i\alpha'} - e^{-i\alpha'}}{2i\alpha'}\right) = a\left(\frac{\sin \alpha'}{\alpha'}\right),$$

so that

$$E = \frac{A\mathcal{E}_A e^{i(\omega t - kR)}}{R}\left(\frac{\sin \alpha'}{\alpha'}\right)\left(\frac{\sin \beta'}{\beta'}\right), \qquad (10.42)$$

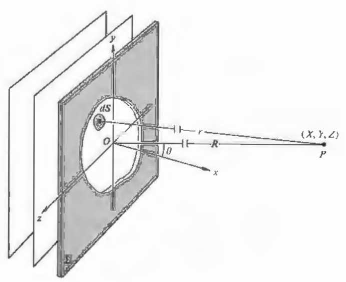


Figure 10.22 Fraunhofer diffraction from an arbitrary aperture, where r and R are very large compared to the size of the hole.

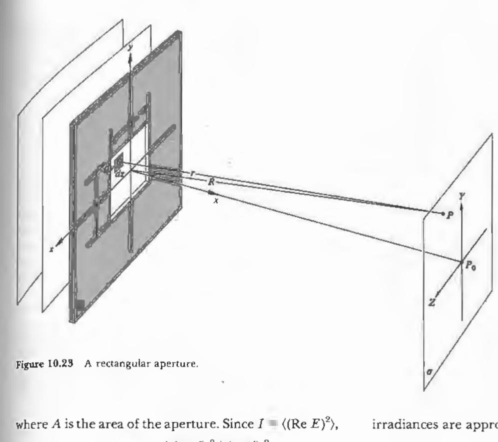


Figure 10.23 A rectangular aperture.

where A is the area of the aperture. Since $I = \langle(\text{Re}\, E)^2\rangle$,

$$I(Y, Z) = I(0)\left(\frac{\sin \alpha'}{\alpha'}\right)^2 \left(\frac{\sin \beta'}{\beta'}\right)^2, \qquad (10.43)$$

where $I(0)$ is the irradiance at P_0; that is, at $Y = 0$, $Z = 0$ (see Fig. 10.24). At values of Y and Z such that $\alpha' = 0$ or $\beta' = 0$, $I(Y, Z)$ assumes the familiar shape of Fig. 10.13. When β' or α' are nonzero integer multiples of π or equivalently when Y and Z are nonzero integer multiples of $\lambda R/b$ and $\lambda R/a$, respectively, $I(Y, Z) = 0$, and we have a rectangular grid of nodal lines, as indicated in Fig. 10.25. Notice that the pattern in the Y-, Z-directions varies *inversely* with the y-, z-aperture dimensions. A horizontal, rectangular opening will produce a pattern with a verticle rectangle at its center.

Along the β'-axis, $\alpha' = 0$ and the subsidiary maxima are located approximately halfway between zeros, that is, at $\beta'_m = \pm 3\pi/2, \pm 5\pi/2, \pm 7\pi/2, \ldots$. At each subsidiary maximum $\sin \beta'_m = 1$, and of course along the β'-axis, since $\alpha' = 0$, $(\sin \alpha')/\alpha' = 1$, so that the relative irradiances are approximated simply by

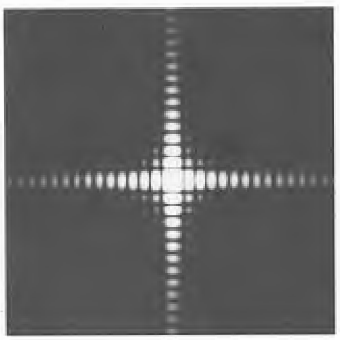
$$\frac{I}{I(0)} = \frac{1}{\beta'^2_m}. \qquad (10.44)$$

Similarly along the α'-axis

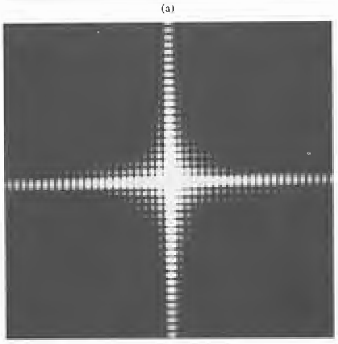
$$\frac{I}{I(0)} = \frac{1}{\alpha'^2_m}. \qquad (10.45)$$

The flux-density ratio* drops off rather rapidly from 1 to $\frac{1}{22}$ to $\frac{1}{62}$ to $\frac{1}{122}$, and so on. Even so, the off-axis secondary

* These particular photographs were taken during an undergraduate laboratory session. A 1.5-mW He–Ne laser was used as a plane-wave source. The apparatus was set up in a long darkened room, and the pattern was cast directly on 4 × 5 Polaroid (ASA 3000) film. The film was located about 30 feet from a small aperture, so that no focusing lens was needed. The shutter, placed directly in front of the laser, was a student-contrived cardboard guillotine arrangement, and therefore no exposure times are available. Any camera shutter (a single-lens reflex with the lens removed and the back open) will serve, but the cardboard one was more fun.



(a)



(b)

Figure 10.24 (a) Fraunhofer pattern of a square aperture. (b) The same pattern further exposed to bring out some of the faint terms. (Photos by E. H.)

peaks are still smaller; for example, the four corner peaks (whose coordinates correspond to appropriate combinations of $\beta' = \pm 3\pi/2$ and $\alpha' = \pm 3\pi/2$) nearest to the central maximum each have relative irradiances of $(\frac{1}{22})^2$.

10.2.5 The Circular Aperture

Fraunhofer diffraction at a circular aperture is an effect of great practical significance in the study of optical instrumentation. Envision a typical arrangement: plane waves impinging on a screen Σ containing a circular aperture and the consequent far-field diffraction pattern **spread** across a distant observing screen σ. By using a fo**cusing** lens L_2, we can bring σ in close to the aperture without changing the pattern. Now, if L_2 is positioned within and exactly fills the diffracting opening in Σ, the form of the pattern is essentially unaltered. The lightwave reaching Σ is cropped, so that only a circular segment propagates through L_2 to form an image in the focal plane. This is obviously the same process that takes place in an eye, telescope, microscope, or camera lens. The image of a distant point source, as formed by a perfectly aberration-free converging lens, is never a point but rather some sort of diffraction pattern. We are essentially collecting only a fraction of the incident wavefront and therefore cannot hope to form a perfect image. As shown in the last section, the expression for the optical disturbance at P, arising from an arbitrary aperture in the far-field case, is

$$E = \frac{\mathcal{E}_A e^{i(\omega t - kR)}}{R} \iint_{\text{Aperture}} e^{ik(Yy+Zz)/R}\, dS. \qquad [10.41]$$

For a circular opening, symmetry would suggest introducing spherical polar coordinates in both the plane of the aperture and the plane of observation, as shown in Fig. 10.26. Therefore, let

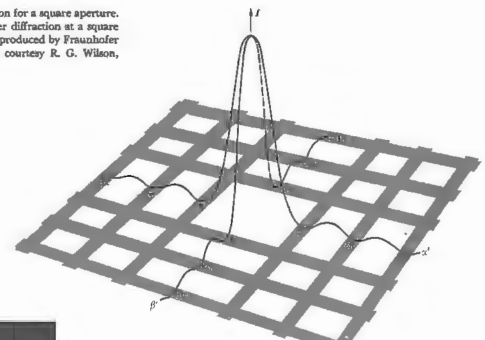
$$z = \rho \cos \phi \qquad y = \rho \sin \phi$$

$$Z = q \cos \Phi \qquad Y = q \sin \Phi.$$

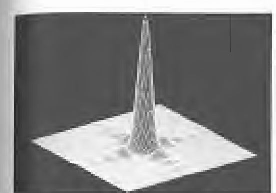
The differential element of area is now

$$dS = \rho\, d\rho\, d\phi.$$

Figure 10.25 (a) The irradiance distribution for a square aperture. (b) The irradiance produced by Fraunhofer diffraction at a square aperture. (c) The electric field distribution produced by Fraunhofer diffraction via a square aperture. (Photos courtesy R. G. Wilson, Illinois Wesleyan University.)



(a)



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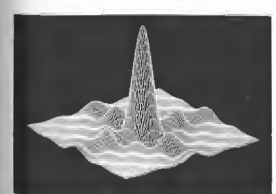


(c)

Substituting these expressions into Eq. (10.41), it becomes

$$E = \frac{\mathcal{E}_A e^{i(\omega t - kR)}}{R} \int_{\rho=0}^{a} \int_{\phi=0}^{2\pi} e^{i(k\rho q/R)\cos(\phi - \Phi)} \rho\, d\rho\, d\phi. \qquad (10.46)$$

Because of the complete axial symmetry, the solution must be independent of Φ. We might just as well solve Eq. (10.46) with $\Phi = 0$ as with any other value, thereby simplifying things slightly.

The portion of the double integral associated with the variable ϕ,

$$\int_0^{2\pi} e^{i(k\rho q/R)\cos\phi}\, d\phi,$$

is one that arises quite frequently in the mathematics of physics. It is a unique function in that it cannot be reduced to any of the more common forms, such as the various hyperbolic, exponential, or trigonometric functions, and indeed with the exception of these, it is

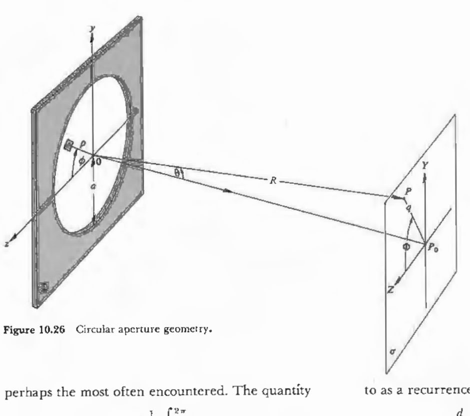


Figure 10.26 Circular aperture geometry.

perhaps the most often encountered. The quantity

$$J_0(u) = \frac{1}{2\pi}\int_0^{2\pi} e^{iu\cos v}\, dv \qquad (10.47)$$

is known as the *Bessel function* (of the first kind) of order zero. More generally,

$$J_m(u) = \frac{i^{-m}}{2\pi}\int_0^{2\pi} e^{i(mv+u\cos v)}\, dv \qquad (10.48)$$

represents the Bessel function of order m. Numerical values of $J_0(u)$ and $J_1(u)$ are tabulated for a large range of u in most mathematical handbooks. Just like sine and cosine, the Bessel functions have series expansions and are certainly no more esoteric than these familiar childhood acquaintances. As seen in Fig. 10.27, $J_0(u)$ and $J_1(u)$ are slowly decreasing oscillatory functions that do nothing particularly dramatic.

Equation (10.46) can be rewritten as

$$E = \frac{\mathcal{E}_A e^{i(\omega t - kR)}}{R} 2\pi \int_0^a J_0(k\rho q/R)\rho\, d\rho. \qquad (10.49)$$

Another general property of Bessel functions, referred to as a recurrence relation, is

$$\frac{d}{du}[u^m J_m(u)] = u^m J_{m-1}(u).$$

When $m = 1$, this clearly leads to

$$\int_0^u u' J_0(u')\, du' = uJ_1(u), \qquad (10.50)$$

with u' just serving as a dummy variable. If we now return to the integral in Eq. (10.49) and change the variable such that $w = k\rho q/R$, then $d\rho = (R/kq)\, dw$ and

$$\int_{\rho=0}^{\rho=a} J_0(k\rho q/R)\rho\, d\rho = (R/kq)^2 \int_{w=0}^{w=kaq/R} J_0(w)w\, dw.$$

Making use of Eq. (10.50), we get

$$E(t) = \frac{\mathcal{E}_A e^{i(\omega t - kR)}}{R} 2\pi a^2 (R/kaq) J_1(kaq/R). \qquad (10.51)$$

The irradiance at point P is $\langle(\text{Re } E)^2\rangle$ or $\frac{1}{2}EE^*$, that is,

$$I = \frac{2\mathcal{E}_A^2 A^2}{R^2}\left[\frac{J_1(kaq/R)}{kaq/R}\right]^2, \qquad (10.52)$$

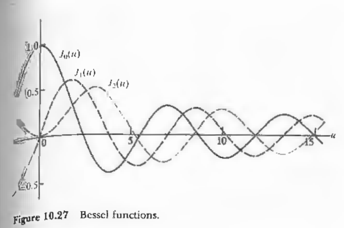


Figure 10.27 Bessel functions.

where A is the area of the circular opening. To find the irradiance at the center of the pattern (i.e., at P_0), set $q = 0$. It follows from the above recurrence relation ($m = 1$) that

$$J_0(u) = \frac{d}{du}J_1(u) + \frac{J_1(u)}{u}. \qquad (10.53)$$

From Eq. (10.47) we see that $J_0(0) = 1$, and from Eq. (10.48), $J_1(0) = 0$. The ratio of $J_1(u)/u$ as u approaches zero has the same limit (L'Hospital's rule) as the ratio of the separate derivatives of its numerator and denominator, namely, $dJ_1(u)/du$ over 1. But this means that the right-hand side of Eq. (10.53) is twice that limiting value, so that $J_1(u)/u = \frac{1}{2}$ at $u = 0$. The irradiance at P_0 is therefore

$$I(0) = \frac{\mathcal{E}_A^2 A^2}{2R^2}, \qquad (10.54)$$

which is the same result obtained for the rectangular opening (10.43). If R is assumed to be essentially constant over the pattern, we can write

$$I = I(0)\left[\frac{2J_1(kaq/R)}{kaq/R}\right]^2. \qquad (10.55)$$

Since $\sin\theta = q/R$, the irradiance can be written as a function of θ,

$$I(\theta) = I(0)\left[\frac{2J_1(ka\sin\theta)}{ka\sin\theta}\right]^2, \qquad (10.56)$$

and as such is plotted in Fig. 10.28. Because of the axial symmetry, the towering central maximum corresponds to a high-irradiance circular spot known as the **Airy disk**. It was Sir George Biddell Airy (1801–1892), Astronomer Royal of England, who first derived Eq. (10.56). The central disk is surrounded by a dark ring that corresponds to the first zero of the function $J_1(u)$. From Table 10.1 $J_1(u) = 0$ when $u = 3.83$, that is, $kaq/R = 3.83$. The radius q_1 drawn to the center of this first dark ring can be thought of as the extent of the Airy disk. It is given by

$$q_1 = 1.22\frac{R\lambda}{2a}. \qquad (10.57)$$

Table 10.1 Bessel functions.*

x	$J_1(x)$*	x	$J_1(x)$	x	$J_1(x)$
0.0	0.0000	3.0	0.3391	6.0	−0.2767
0.1	0.0499	3.1	0.3009	6.1	−0.2559
0.2	0.0995	3.2	0.2613	6.2	−0.2329
0.3	0.1483	3.3	0.2207	6.3	−0.2081
0.4	0.1960	3.4	0.1792	6.4	−0.1816
0.5	0.2423	3.5	0.1374	6.5	−0.1538
0.6	0.2867	3.6	0.0955	6.6	−0.1250
0.7	0.3290	3.7	0.0538	6.7	−0.0953
0.8	0.3688	3.8	0.0128	6.8	−0.0652
0.9	0.4059	3.9	−0.0272	6.9	−0.0349
1.0	0.4401	4.0	−0.0660	7.0	−0.0047
1.1	0.4709	4.1	−0.1033	7.1	0.0252
1.2	0.4983	4.2	−0.1386	7.2	0.0543
1.3	0.5220	4.3	−0.1719	7.3	0.0826
1.4	0.5419	4.4	−0.2028	7.4	0.1096
1.5	0.5579	4.5	−0.2311	7.5	0.1352
1.6	0.5699	4.6	−0.2566	7.6	0.1592
1.7	0.5778	4.7	−0.2791	7.7	0.1813
1.8	0.5815	4.8	−0.2985	7.8	0.2014
1.9	0.5812	4.9	−0.3147	7.9	0.2192
2.0	0.5767	5.0	−0.3276	8.0	0.2346
2.1	0.5683	5.1	−0.3371	8.1	0.2476
2.2	0.5560	5.2	−0.3432	8.2	0.2580
2.3	0.5399	5.3	−0.3460	8.3	0.2657
2.4	0.5202	5.4	−0.3453	8.4	0.2708
2.5	0.4971	5.5	−0.3414	8.5	0.2731
2.6	0.4708	5.6	−0.3343	8.6	0.2728
2.7	0.4416	5.7	−0.3241	8.7	0.2697
2.8	0.4097	5.8	−0.3110	8.8	0.2641
2.9	0.3754	5.9	−0.2951	8.9	0.2559

*$J_1(x) = 0$ for $x = 0$, 3.832, 7.016, 10.173, 13.324, . . .
Adapted from E. Kreyszig, *Advanced Engineering Mathematics*, Wiley.

For a lens focused on the screen σ, the focal length $f \approx R$, so

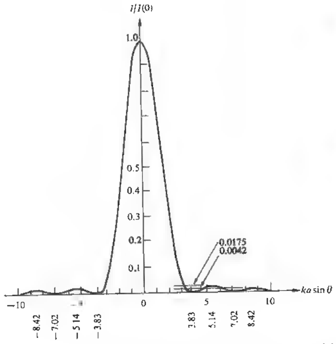
$$q_1 \approx 1.22\frac{f\lambda}{D}, \tag{10.58}$$

where D is the aperture diameter, in other words, $D = 2a$. (The *diameter* of the Airy disk in the visible spectrum is *very roughly* equal to the $f/\#$ of the lens in millionths of a meter.) As shown in Figs. 10.29 to 10.31, q_1 varies inversely with the hole's diameter. As D approaches λ, the Airy disk can be very large indeed, and the circular aperture begins to resemble a point source of spherical waves.

The higher-order zeros occur at values of kaq/R equal to 7.02, 10.17, and so forth. The secondary maxima are located where u satisfies the condition

$$\frac{d}{du}\left[\frac{J_1(u)}{u}\right] = 0,$$

which is equivalent to $J_2(u) = 0$. From the tables then,



(a)

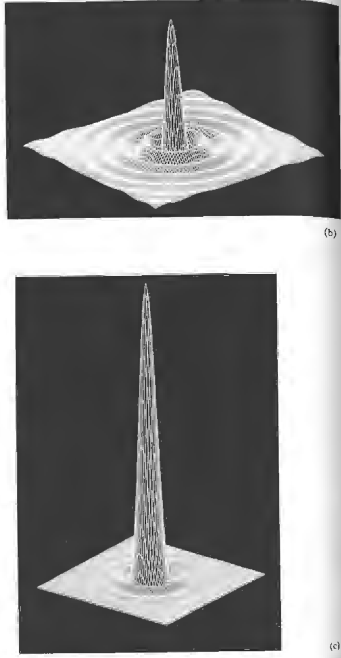

(b)
(c)

Figure 10.28 (a) The Airy pattern. (b) Electric field created by Fraunhofer diffraction at a circular aperture. (c) Irradiance resulting from Fraunhofer diffraction at a circular aperture. (Photos courtesy R. G. Wilson, Illinois Wesleyan University.)

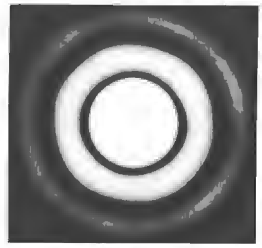


Figure 10.29 Airy rings (0.5-mm hole diameter). (Photo by E. H.)

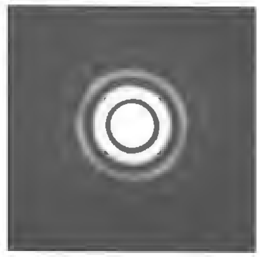
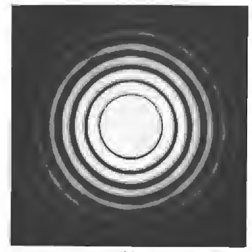


Figure 10.30 Airy rings (1.0-mm hole diameter). (Photo by E. H.)

these secondary peaks occur when kaq/R equals 5.14, 8.42, 11.6, and so on, whereupon $I/I(0)$ drops from 1 to 0.0175, 0.0042, and 0.0016, respectively (Problem 10.22).

Circular apertures are preferable to rectangular ones, as far as lens shapes go, since the circle's irradiance curve is broader around the central peak and drops off more rapidly thereafter. Exactly what fraction of the total light energy incident on σ is confined to within


(a)

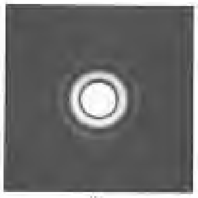

(b)

Figure 10.31 (a) Airy rings—long exposure (1.5-mm hole diameter). (b) Central Airy disc—short exposure with the same aperture. (Photos by E. H.)

the various maxima is a question of interest, but one somewhat too involved to solve here.* On integrating the irradiance over a particular region of the pattern, one finds that 84% of the light arrives within the Airy disk, and 91% within the bounds of the second dark ring.

* See Born and Wolf, *Principles of Optics*, p. 398, or the very fine elementary text by Towne, *Wave Phenomena*, p. 464.

10.2.6 Resolution of Imaging Systems

Imagine that we have some sort of lens system that forms an image of an extended object. If the object is self-luminous, it is likely that we can regard it as made up of an array of incoherent sources. On the other hand, an object seen in reflected light will surely display some phase correlation between its various scattering points. When the point sources are in fact incoherent, the lens system will form an image of the object, which consists of a distribution of partially overlapping, yet independent, Airy patterns. In the finest lenses, which have negligible aberrations, the spreading out of each image point due to diffraction represents the ultimate limit on image quality.

Suppose that we simplify matters somewhat and examine only two equal-irradiance, incoherent, distant point sources. For example, consider two stars seen through the objective lens of a telescope, where the entrance pupil corresponds to the diffracting aperture. In the previous section we saw that the radius of the Airy disk was given by $q_1 = 1.22f\lambda/D$. If $\Delta\theta$ is the corresponding angular measure, then $\Delta\theta = 1.22\lambda/D$, inasmuch as $q_1/f = \sin\Delta\theta \approx \Delta\theta$. The Airy disk for each star will be spread out over an angular half-width $\Delta\theta$ about its geometric image point, as shown in Fig. 10.32. If the angular separation of the stars is $\Delta\varphi$ and if $\Delta\varphi \gg \Delta\theta$, the images will be distinct and easily resolved. As the stars approach each other, their respective images come together, overlap, and commingle into a single blend of fringes. If Lord Rayleigh's criterion is applied, the stars are said to be *just resolved* when the center of one Airy disk falls on the first minimum of the Airy pattern of the other star. (We can certainly do a bit better than this, but Rayleigh's criterion, however arbitrary, has the virtue of being particularly uncomplicated.*) The *minimum resolvable angular separation* or *angular limit of resolution* is

$$(\Delta\varphi)_{min} = \Delta\theta = 1.22\lambda/D, \qquad (10.59)$$

as depicted in Fig. 10.33. If $\Delta\ell$ is the center-to-center separation of the images, the limit of resolution is

$$(\Delta\ell)_{min} = 1.22f\lambda/D. \qquad (10.60)$$

The resolving power for an image-forming system is generally defined as either $1/(\Delta\varphi)_{min}$ or $1/(\Delta\ell)_{min}$.

If the smallest resolvable separation between images is to be reduced (i.e., if the resolving power is to be increased), the wavelength, for instance, might be made smaller. Using ultraviolet rather than visible light in microscopy allows for the perception of finer detail. The electron microscope utilizes equivalent wavelengths of about 10^{-4} to 10^{-5} that of light. This makes it possible to examine objects that would otherwise be completely obscured by diffraction effects in the visible spectrum. On the other hand, the resolving power of a telescope can be increased by increasing the diameter of the objective lens or mirror. Besides collecting more of the incident radiation, this will also result in a smaller Airy disk and therefore a sharper, brighter image. The Mount Palomar 200-in telescope has a mirror 5 m in diameter (neglecting the obstruction of a small region at its center). At 550 nm it has an angular limit of resolution of 2.7×10^{-2} s of arc. In contrast, the Jodrell Bank radio telescope, with a 250-ft diameter, operates at a rather long, 21-cm wavelength. It therefore has a limit of resolution of only about 700 s of arc. The human eye has a pupil diameter that of course varies. Taking it, under bright conditions, to be about 2 mm, with $\lambda = 550$ nm, $(\Delta\varphi)_{min}$ turns out to be roughly 1 min of arc. With a focal length of about 20 mm, $(\Delta\ell)_{min}$ on the retina is 6700 nm. This is roughly twice the mean spacing between receptors. The human eye should therefore be able to resolve two points, an inch apart, at a distance of some 100 yards. You will probably not be able to do quite that well; one part in one thousand is more likely.

A more appropriate criterion for resolving power has been proposed by C. Sparrow. Recall that at the Rayleigh limit there is a central minimum or saddle point between adjacent peaks. A further decrease in the distance between the two point sources will cause the central dip to grow shallower and ultimately disappear. The angular separation corresponding to that configuration is Sparrow's limit. The resultant

* In Rayleigh's own words: "This rule is convenient on account of its simplicity and it is sufficiently accurate in view of the necessary uncertainty as to what exactly is meant by resolution." See Section 9.6.1. for further discussion.

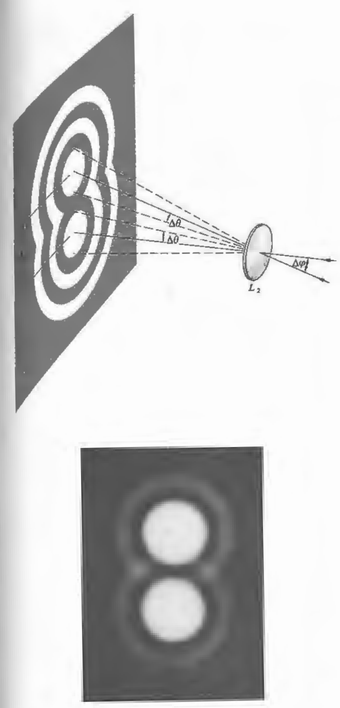


Figure 10.32 Overlapping images.

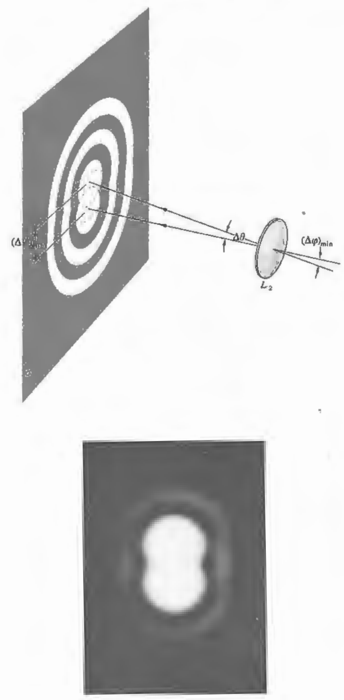


Figure 10.33 Overlapping images.

maximum has a broad flat top; in other words, at the origin, which is the center of the peak, the second derivative of the irradiance function is zero; there is no change in slope (Fig. 10.40).

Unlike the Rayleigh rule, which rather tacitly assumes incoherence, the Sparrow condition can readily be generalized to coherent sources. In addition, astronomical studies of equal-brightness stars have shown that Sparrow's criterion is by far the more realistic.

10.2.7 The Diffraction Grating

A repetitive array of diffracting elements, either apertures or obstacles, that has the effect of producing periodic alterations in the phase, amplitude, or both of an emergent wave is said to be a **diffraction grating**. One of the simplest such arrangements is the multiple-slit configuration of Section 10.2.3. It seems to have been invented by the American astronomer David Rittenhouse in about 1785. Some years later Joseph von Fraunhofer independently rediscovered the principle and went on to make a number of important contributions to both the theory and technology of gratings. The earliest devices were indeed multiple-slit assemblies, usually consisting of a grid of fine wire or thread wound about and extending between two parallel screws, which served as spacers. A wavefront, in passing through such a system, is confronted by alternate opaque and transparent regions, so that it undergoes a modulation in *amplitude*. Accordingly, a multiple-slit configuration is said to be a *transmission amplitude grating*. Another, more common form of transmission grating is made by ruling or scratching parallel notches into the surface of a flat, clear glass plate [Fig. 10.34(a)]. Each of the scratches serves as a source of scattered light, and together they form a regular array of parallel line sources. When the grating is totally transparent, so that there is negligible amplitude modulation, the regular variations in the optical thickness across the grating yield a modulation in *phase*, and we have what is known as a *transmission phase grating* (Fig. 10.35). In the Huygens–Fresnel representation you can envision the wavelets as radiated with different phases over the grating surface. An emerging wavefront therefore contains

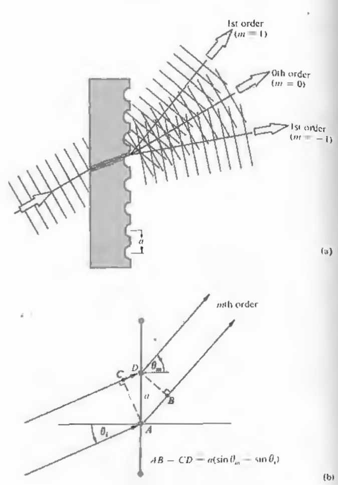


Figure 10.34 A transmission grating.

periodic variations in its shape rather than its amplitude. This in turn is equivalent to an angular distribution of constituent plane waves.

On reflection from this kind of grating, light scattered by the various periodic surface features will arrive at some point P with a definite phase relationship. The consequent interference pattern generated after reflection is quite similar to that arising from transmission. Gratings designed specifically to function in this fashion are known as *reflection phase gratings* (Fig. 10.36). Contemporary gratings of this sort are generally ruled in thin films of aluminum that have been evaporated onto optically flat glass blanks. The aluminum, being fairly

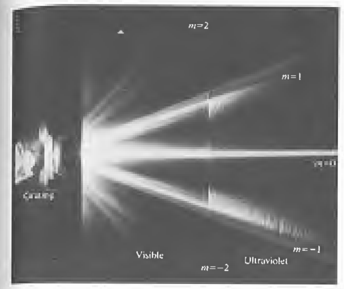


Figure 10.35 Light passing through a grating. The region on the left is the visible spectrum, that on the right, the ultraviolet. (Photo courtesy Klinger Scientific Apparatus Corp.)

soft, results in less wear on the diamond ruling tool and is also a better reflector in the ultraviolet region.

The manufacture of ruled gratings is extremely difficult, and relatively few are made. In actuality most gratings are exceedingly good plastic castings or *replicas* of fine, master ruled gratings.

If you were to look perpendicularly through a transmission grating at a distant parallel line source, your eye would serve as a focusing lens for the diffraction pattern. Recall the analysis of Section 10.2.3 and the expression

$$a \sin \theta_m = m\lambda, \qquad [10.32]$$

which is known as the **grating equation** for normal incidence. The values of m specify the *order* of the various principal maxima. For a source having a broad continuous spectrum, such as a tungsten filament, the $m = 0$, or zeroth-order, image corresponds to the undeflected, $\theta_0 = 0$, white-light view of the source. The grating equation is dependent on λ, and so for any value of $m \neq 0$ the various colored images of the source corresponding to slightly different angles (θ_m) spread out

into a continuous spectrum. The regions occupied by the faint subsidiary maxima will show up as bands seemingly devoid of any light. The first-order spectrum $m = \pm 1$ appears on either side of $\theta = 0$ and is followed, along with alternate intervals of darkness, by the higher-order spectra, $m = \pm 2, \pm 3, \ldots$. Notice that the smaller a becomes in Eq. (10.32), the fewer will be the number of visible orders.

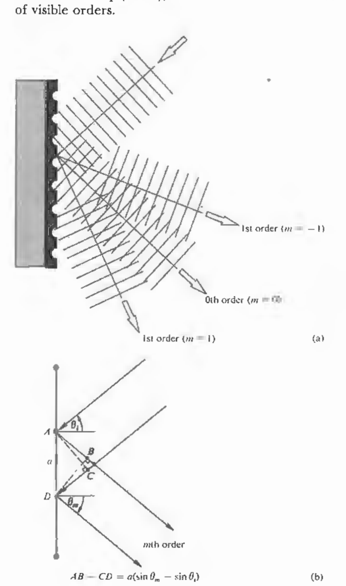


Figure 10.36 A reflection grating.

It should be no surprise that the grating equation is in fact Eq. (9.29), which describes the location of the maxima in Young's double-slit setup. The interference maxima, all located at the same angles, are now simply sharper (just as the multiple beam operation of the Fabry–Perot etalon made its fringes sharper). In the double-slit case when the point of observation is snme-what off the exact center of an irradiance maximum the two waves, one from each slit, will still be more or less in phase, and the irradiance, though reduced, will still be appreciable. Thus the bright regions are fairly broad. By contrast, with multiple-beam systems though all the waves interfere constructively at the centers of the maxima, even a small displacement will cause certain ones to arrive out of phase by $\frac{1}{2}\lambda$ with respect to others. For example, suppose P is slightly off from θ_1 so that $a \sin \theta = 1.010\lambda$ instead of 1.000λ. Each of the waves from successive slits will arrive at P shifted by 0.01λ with respect to the previous one. Then 50 slits down from the first, the path length will have shifted by $\frac{1}{2}\lambda$, and the light from slit 1 and slit 51 will essentially cancel. The same would be true for slit-pairs 2 and 52, 3 and 53, and so forth. The result is a rapid fall off in irradiance beyond the centers of the maxima.

Consider next the somewhat more general situation of oblique incidence, as depicted in Figs. 10.34 and 10.36. The grating equation, for both transmission and reflection, becomes

$$a(\sin \theta_m - \sin \theta_i) = m\lambda. \qquad (10.61)$$

This expression applies equally well, regardless of the refractive index of the transmission grating itself (Problem 10.37). One of the main disadvantages of the devices examined thus far, and in fact the reason for their obsolescence, is that they spread the available light energy out over a number of low-irradiance spectral orders. For a grating like that shown in Fig. 10.36, most of the incident light undergoes *specular reflection*, as if from a plane mirror. It follows from the grating equation that $\theta_m = \theta_i$ corresponds to the zeroth order, $m = 0$. All of this light is essentially wasted, at least for spectroscopic purposes, since the constituent wavelengths overlap.

In an article in the *Encyclopaedia Britannica* of 1888 Lord Rayleigh suggested that it was at least theoretically possible to shift energy out of the useless zeroth order into one of the higher-order spectra. So motivated, Robert Williams Wood (1868–1955) succeeded in 1910 in ruling grooves with a controlled shape, as shown in Fig. 10.37. Most modern gratings are of this shaped, or **blazed** variety. The angular positions of the nonzero orders, θ_m-values, are determined by a, λ, and, of more immediate interest, θ_i. But θ_i and θ_m are measured from the normal to the grating plane and not with respect to the individual groove surfaces. On the other hand, the location of the peak in the single-facet diffraction pattern corresponds to *specular reflection* off that face, for each groove. It is governed by the *blaze angle* γ and can be varied independently of θ_m. This is somewhat analogous to the antenna array of Section 10.1.3, where we were able to control the spatial position of the interference pattern (10.6) by adjusting the relative phase shift between sources without actually changing their orientations.

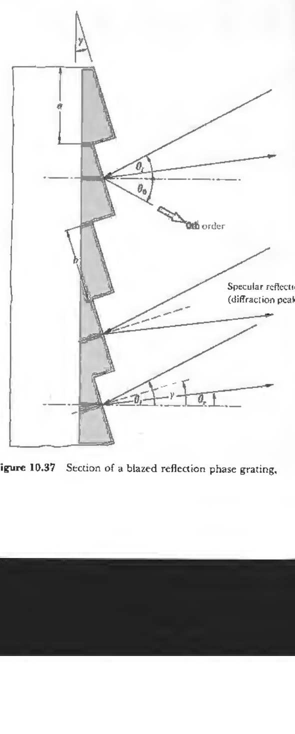


Figure 10.37 Section of a blazed reflection phase grating.

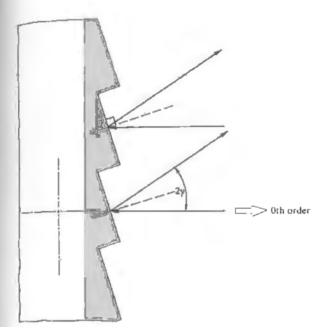


Figure 10.38 Blazed grating.

Consider the situation depicted in Fig. 10.38 when the incident wave is normal to the plane of a blazed reflection grating; that is, $\theta_i = 0$, so for $m = 0$, $\theta_0 = 0$. For *specular reflection* $\theta_i - \theta_r = 2\gamma$ (Fig. 10.37), most of the diffracted radiation is concentrated about $\theta_r = -2\gamma$. (θ_r is negative because the incident and reflected rays are on the same side of the grating normal.) This will correspond to a particular nonzero order, on one side of the central image, when $\theta_m = -2\gamma$; in other words, $a \sin(-2\gamma) = m\lambda$ for the desired λ and m.

Grating Spectroscopy

Quantum mechanics, which evolved in the early 1920s, had its initial thrust in the area of atomic physics. Predictions were made concerning the detailed structure of the hydrogen atom as manifested by its emitted radiation, and spectroscopy provided the vital proving

ground. The need for larger and better gratings became apparent. Grating spectrometers, used over the range from soft x-rays to the far infrared, have enjoyed continued interest. In the hands of the astrophysicist or rocket-borne, they yield information concerning the very origins of the universe, information as varied as the temperature of a star, the rotation of a galaxy, and the red shift in the spectrum of a quasar. In the mid-1900s George R. Harrison and George W. Stroke remarkably improved the quality of high-resolution gratings. They used a ruling engine* whose operation was contrnlled by an interferometrically guided servomechanism.

Let us now examine in some detail a few of the major features of the grating spectrum. Assume an infinitesimally narrow incoherent source. The effective width of an emergent spectral line may be defined as the angular distance between the zeros on either side of a principal maximum; in other words, $\Delta\alpha = 2\pi/N$, which follows from Eq. (10.33). At oblique incidence we can redefine α as $(ka/2)(\sin\theta - \sin\theta_i)$, and so a small change in α is given by

$$\Delta\alpha = (ka/2)\cos\theta(\Delta\theta) = 2\pi/N, \qquad (10.62)$$

where the angle of incidence is constant, that is, $\Delta\theta_i = 0$. Thus even when the incident light is monochromatic

$$\Delta\theta = 2\lambda/(Na\cos\theta_m) \qquad (10.63)$$

is the *angular width of a line*, due to *instrumental broadening*. Interestingly enough, the angular linewidth varies inversely with the width of the grating itself, Na. Another important quantity is the difference in angular position corresponding to a difference in wavelength. The **angular dispersion**, as in the case of a prism, is defined as

$$\mathscr{D} = d\theta/d\lambda. \qquad (10.64)$$

Differentiating the grating equation yields

$$\mathscr{D} = m/a\cos\theta_m. \qquad (10.65)$$

This means that the angular separation between two

* For more details about these marvelous machines see A. R. Ingalls, *Sci. Amer.* **186**, 45 (1952), or the article by E. W. Palmer and J. F. Verrill, *Contemp. Phys.* **9**, 257 (1968).

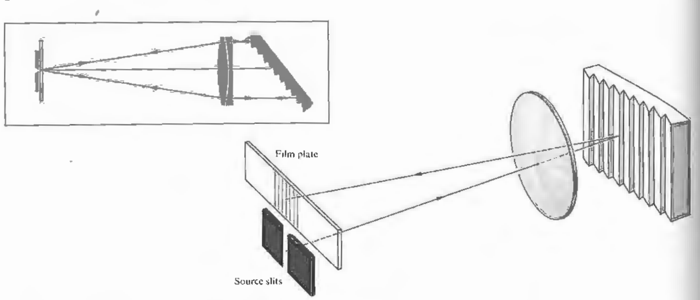


Figure 10.39 The Littrow autocollimation mounting.

different frequency lines will increase as the order increases.

Blazed plane gratings with nearly rectangular grooves are most often mounted so that the incident propagation vector is almost normal to either one of the groove faces. This is the condition of *autocollimation*, in which θ_i and θ_m are on the same side of the normal and $\gamma = \theta_i = -\theta_m$ (see Fig. 10.39), whereupon

$$\mathcal{D}_{auto} = 2 \tan \theta_i/\lambda, \quad (10.66)$$

which is independent of a.

When the wavelength difference between two lines is small enough so that they overlap, the resultant peak becomes somewhat ambiguous. The chromatic resolving power $\mathcal{R}$ of a spectrometer is defined as

$$\mathcal{R} \equiv \lambda/(\Delta\lambda)_{min}, \quad [9.76]$$

where $(\Delta\lambda)_{min}$ is the least resolvable wavelength difference, or limit of resolution, and λ is the mean wavelength. Lord Rayleigh's criterion for the resolution of two fringes with equal flux density requires that the principal maximum of one coincide with the first minimum of the other. (Compare this with the equivalent statement used in Section 9.6.1.) As shown in Fig. 10.40, at the limit of resolution the angular separation is half the linewidth, or from Eq. (10.63)

$$(\Delta\theta)_{min} = \lambda/Na \cos \theta_m.$$

Applying the expression for the dispersion, we get

$$(\Delta\theta)_{min} = (\Delta\lambda)_{min} m/a \cos \theta_m.$$

The combination of these two equations provides us with $\mathcal{R}$, that is,

$$\lambda/(\Delta\lambda)_{min} = mN \quad (10.67)$$

or

$$\mathcal{R} = \frac{Na(\sin \theta_m - \sin \theta_i)}{\lambda}. \quad (10.68)$$

The resolving power is a function of the grating width Na, the angle of incidence, and λ. A grating 6 inches wide and containing 15,000 lines per inch will have a total of 9×10^4 lines and a resolving power, in the second order, of 1.8×10^5. In the vicinity of 540 nm the grating could resolve a wavelength difference of 0.003 nm. Notice that the resolving power cannot exceed $2Na/\lambda$, which occurs when $\theta_i = -\theta_m = 90°$. The largest values of $\mathcal{R}$ are obtained when the grating is used in autocollimation, whereupon

$$\mathcal{R}_{auto} = \frac{2Na \sin \theta_i}{\lambda}, \quad (10.69)$$

and again θ_i and θ_m are on the same side of the normal. For one of Harrison's 260-mm–wide blazed gratings at about 75° in a Littrow mount, with $\lambda = 500$ nm, the resolving power just exceeds 10^6.

We now need to consider the problem of overlapping orders. The grating equation makes it quite clear that a line of 600 nm in the first order will have precisely the same position, θ_m, as a 300-nm line in the second order or a 200-nm line when $m = 3$. If two lines of wavelength λ and $(\lambda + \Delta\lambda)$ in successive orders $(m + 1)$ and m just coincide, then

$$a(\sin \theta_m - \sin \theta_i) = (m + 1)\lambda = m(\lambda + \Delta\lambda).$$

That precise wavelength difference is known as the **free spectral range**,

$$(\Delta\lambda)_{fsr} = \lambda/m, \quad (10.70)$$

as it was for the Fabry–Perot interferometer. In comparison with that device, whose resolving power was

$$\mathcal{R} = \mathcal{F}m, \quad [9.76]$$

we might take N to be the finesse of a diffraction grating (Problem 10.38).

A high-resolution grating blazed for the first order, so as to have the greatest free spectral range, will require a high groove density (up to about 1200 lines per millimeter) in order to maintain $\mathcal{R}$. Equation (10.68) shows that $\mathcal{R}$ can be kept constant by ruling fewer lines with increasing spacing, such that the grating width Na is constant. But this requires an increase in m and a subsequent decrease in free spectral range, characterized by overlapping orders. If this time N is held constant while a alone is made larger, $\mathcal{R}$ increases as does m, so that $(\Delta\lambda)_{fsr}$ again decreases. The angular width of a line is reduced (i.e., the spectral lines become sharper), the coarser the grating is, but the dispersion in a given order diminishes, with the effect that the lines in that spectrum approach each other.

Thus far we have considered a particular type of periodic array, namely, the *line grating*. A good deal more information is available in the literature* concern-

* See F. Kneubühl, "Diffraction Grating Spectroscopy", *Appl. Opt.* 8, 505 (1969); R. S. Longhurst, *Geometrical and Physical Optics*; and the extensive article by G. W. Stroke in the *Encyclopedia of Physics*, Vol. 29, edited by S. Flügge, p. 426.

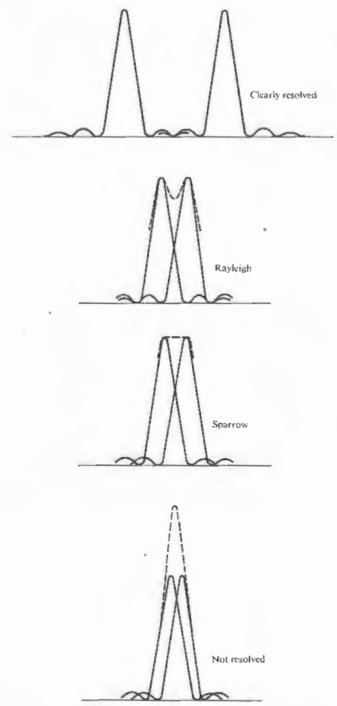


Figure 10.40 Overlapping point images.

ing their shapes, mountings, uses, and so forth.

There are a few unlikely household items that can be used as crude gratings, along with a small light source. The grooved surface of a phonograph record works nicely near grazing incidence. And surprisingly enough, under the same conditions an ordinary fine-toothed comb will separate out the constituent wavelengths of white light. This occurs in exactly the same fashion as it would with a more orthodox reflection grating. In a letter to a friend dated May 12, 1673, James Gregory pointed out that sunlight passing through a feather would produce a colored pattern, and he asked that his observations be conveyed to Mr. Newton. If you've got one, a feather makes a nice transmission grating.

Two- and Three-Dimensional Gratings

Suppose that the diffracting screen Σ contains a large number, N, of identical diffracting objects (apertures or obstacles). These are to be envisioned as distributed over the surface of Σ in a completely random manner. We also require that each and every one be similarly oriented. Imagine the diffracting screen to be illuminated by plane waves that are focused by a perfect lens L_2, after emerging from Σ (see Fig. 10.15). The individual apertures generate identical Fraunhofer diffraction patterns, all of which overlap on the image plane σ. If there is no regular periodicity in the location of the apertures, we cannot anticipate anything but a random distribution in the relative phases of the waves arriving at an arbitrary point P on σ. We have to be rather careful, however, because there is one exception, which occurs when P is on the central axis, that is, $P = P_0$. All rays, from all apertures, parallel to the central axis will traverse equal optical path lengths before reaching P_0. They will therefore arrive in phase and interfere constructively.

Now consider a group of arbitrarily directed parallel rays (not in the direction of the central axis), each one emitted from a different aperture. These will be focused at some point on σ, such that each corresponding wave will have an equal probability of arriving with any phase between 0 and 2π. What must be determined is the resultant field arising from the superposition of N equal-amplitude phasors all having random relative phases. The solution to this problem requires an elaborate analysis in terms of probability theory, which is a little too far afield to do here.* The important point is that the sum of a number of phasors taken at random angles is not simply zero, as might be thought. The general analysis begins, for statistical reasons, by assuming that there are a large number of individual aperture screens, each containing N random diffracting apertures and each illuminated, in turn, by a monochromatic wave. We shouldn't be surprised if there is some difference, however small, between the diffraction patterns of two different random distributions of, say, $N = 100$ holes—after all, they are different, and the smaller N is, the more obvious that becomes. Indeed, we can expect their similarities to show up statistically on considering a large number of such masks—ergo the general approach.

If the many individual resulting irradiance distributions are all averaged for a particular *off-axis* point on σ, it will be found that the average irradiance (I_{av}) there equals N times the irradiance (I_0) due to a single aperture: $I_{av} = NI_0$. Still, the irradiance at any point arising from any one aperture screen can differ from this average value by a fairly large amount, regardless of how great N is. These point-to-point fluctuations about the average manifest themselves in each particular pattern as a granularity that tends to show a radial fiberlike structure. If this fine-grained mottling is averaged over a small region of the pattern, which nonetheless contains many fluctuations, it will average out to NI_0.

Of course, in any real experiment the situation will not quite match the ideal—there is no such thing as monochromatic light or a truly random array of (nonoverlapping) diffracting objects. Nonetheless, with a screen containing N "random" apertures illuminated by quasimonochromatic, nearly plane-wave illumination, we can anticipate seeing a mottled flux-density distribution closely resembling that of an individual aperture but N times as strong. Moreover, a bright spot

* For a statistical treatment, consult J. M. Stone, *Radiation and Optics*, p. 146, and Sommerfeld, *Optics*, p. 194. Also take a look at "Diffraction Plates for Classroom Demonstrations," by R. B. Hoover, *Am. J. Phys.* **37**, 871 (1969), and T. A. Wiggins, "Hole Gratings for Optics Experiments," *Am. J. Phys.* **53**, 227 (1985).

will exist on-axis at its center, which will have a flux density of N^2 times that of a single aperture. If, for example, the screen contains N rectangular holes [Fig. 10.41(a)], the resultant pattern [Fig. 10.41(b)] will resemble Fig. 10.24. Similarly, the array of circular holes depicted in Fig. 10.41(c) will produce the diffraction rings of Fig. 10.41(d).

As the number of apertures increases, there will be a tendency for the central spot to become so bright as to obscure the rest of the pattern. Note as well that the above considerations apply when all the apertures are illuminated completely coherently. In actuality, the

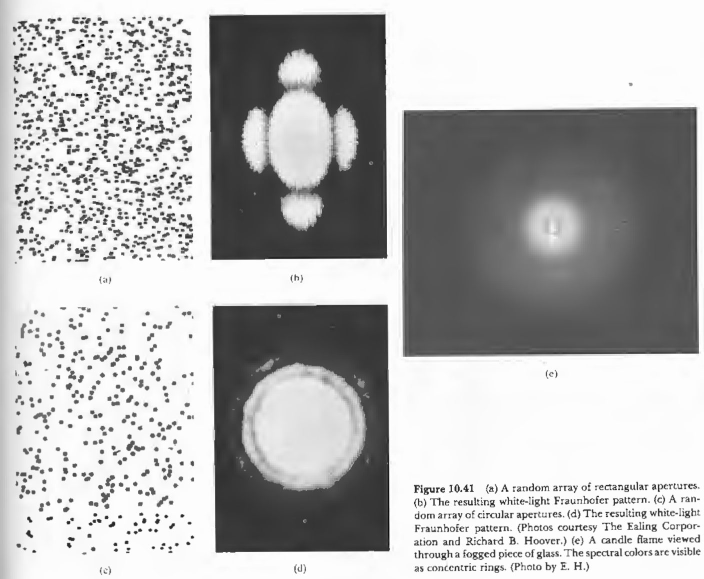


Figure 10.41 (a) A random array of rectangular apertures. (b) The resulting white-light Fraunhofer pattern. (c) A random array of circular apertures. (d) The resulting white-light Fraunhofer pattern. (Photos courtesy The Ealing Corporation and Richard B. Hoover.) (e) A candle flame viewed through a fogged piece of glass. The spectral colors are visible as concentric rings. (Photo by E. H.)

diffracted flux-density distribution will be determined by the degree of coherence (see Chapter 12). The pattern will run the gamut from no interference with completely incoherent light to the case discussed above for completely coherent illumination (Problem 10.40).

The same kind of effects arise from what we might call a two-dimensional *phase grating*. For example, the halo or corona often seen about the Sun or Moon results from diffraction by random droplets of water vapor (i.e., cloud particles). If you would like to duplicate the effect, rub a very thin film of talcum powder on a microscope slide and then fog it up with your breath. Look at a white-light point source. You should see a pattern of clear, concentric, colored rings (10.56) surrounding a white central disk. If you just see a white blur, you don't have a distribution of roughly equal sized droplets; have another try at the talcum. Strikingly beautiful patterns approximating concentric ring sys-

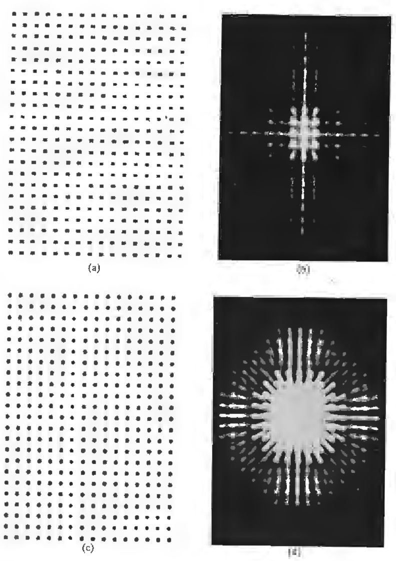


Figure 10.42 (a) An ordered array of rectangular apertures. (b) The resulting white-light Fraunhofer pattern. (c) An ordered array of circular apertures. (d) The resulting white-light Fraunhofer pattern. (Photos courtesy Richard B. Hoover.)

tems can be seen through an ordinary *mesh* nylon stocking. If you are fortunate enough to have mercury-vapor street lights, you'll have no trouble seeing all their constituent visible spectral frequencies. (If not, block out most of a fluorescent lamp, leaving something resembling a small source.) Notice the increased symmetry as you increase the number of layers of nylon. Incidentally, this is precisely the way Rittenhouse, the inventor of the grating, became interested in the problem, only he used a silk handkerchief.

Consider the case of a *regular* two-dimensional array of diffracting elements (Fig. 10.42) under normally incident plane-wave illumination. Each small element behaves as a coherent source. And because of the regular periodicity of the lattice of emitters, each emergent wave bears a fixed phase relation to the others. There will now be certain directions in which constructive interference prevails. Obviously, these occur when the distances from each diffracting element to P are such that the waves are nearly in phase at arrival. The phenomenon can be observed by looking at a point source through a piece of *square woven*, thin cloth (such as nylon curtain material) or the fine metal mesh of a tea strainer (Fig. 10.84). The diffracted image is effectively the superposition of two grating patterns at right angles. Examine the center of the pattern carefully to see its gridlike structure.

As for the possibility of a *three-dimensional grating*, there seems to be no particular conceptual difficulty. A regular spatial array of scattering centers would certainly yield interference maxima in preferred directions. In 1912 Max von Laue (1879–1960) conceived the ingenious idea of using the regularly spaced atoms within a crystal as a three-dimensional grating. It is apparent from the grating equation (10.61) that if λ is much greater than the grating spacing, only the zeroth order ($m = 0$) is possible. This is equivalent to $\theta_0 = \theta_i$, that is, specular reflection. Since the spacing between atoms in a crystal is generally several angstroms (1 Å = 10^{-1} nm), light can be diffracted only in the zeroth order.

Von Laue's solution to the problem was to probe the lattice, not with light but with x-rays whose wavelengths were comparable to the interatomic distances (Fig. 10.43). A narrow beam of white radiation (the broad

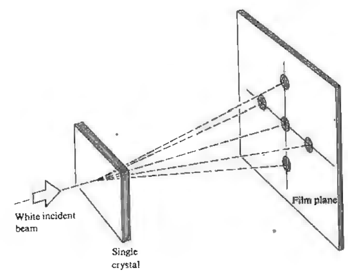


Figure 10.43 Transmission Laue pattern.

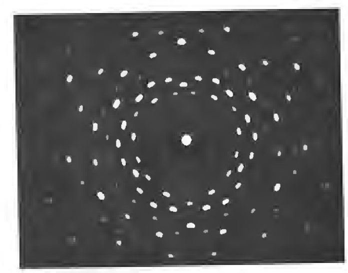


Figure 10.44 X-ray diffraction pattern for quartz (SiO_2).

continuous frequency range emitted by an x-ray tube) was directed onto a thin single crystal. The film plate (Fig. 10.44) revealed a Fraunhofer pattern consisting of an array of precisely located spots. These sites of constructive interference occurred whenever the angle between the beam and a set of atomic planes within the

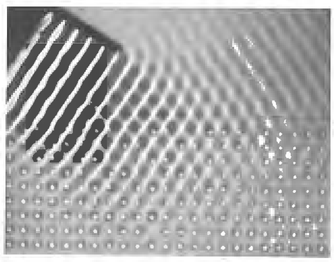


Figure 10.45 Water waves in a ripple tank reflecting off an array of pegs acting as point scatterers. (Photo courtesy PSSC *Physics*, D. C. Heath, Boston, 1960.)

crystal obeyed Bragg's law:

$$2d \sin \theta = m\lambda. \qquad (10.71)$$

Notice that in x-ray work θ is traditionally measured from the plane and not the normal to it. Each set of planes diffracts a particular wavelength into a particular direction. Figure 10.45 rather strikingly shows the analogous behavior in a ripple tank.

Instead of reducing λ to the x-ray range, we could have scaled everything up by a factor of about a billion and made a lattice of metal balls as a grating for microwaves.

10.3 FRESNEL DIFFRACTION

10.3.1 The Free Propagation of a Spherical Wave

In the Fraunhofer configuration, the diffracting system was relatively small, and the point of observation was very distant. Under these circumstances a few potentially problematic features of the Huygens–Fresnel principle could be completely passed over without concern. But we are now dealing with the near-field region, which extends right up to the diffracting element itself and any such approximations would be inappropriate. We therefore return to the Huygens–Fresnel principle in order to re-examine it more closely. At any instant every point on the primary wavefront is envisioned as a continuous emitter of spherical secondary wavelets. But if each wavelet radiated uniformly in all directions, in addition to generating an ongoing wave, there would also be a reverse wave traveling back toward the source. No such wave is found experimentally, so we must somehow modify the radiation pattern of the secondary emitters. We now introduce the function $K(\theta)$, known as the **obliquity** or **inclination factor**, in order to describe the directionality of the secondary emission. Fresnel recognized the need to introduce a quantity of this kind, but he did little more than conjecture about its form.* It remained for the more analytic Kirchhoff formulation to provide an actual expression for $K(\theta)$, which, as we will see in Section 10.4, turns out to be

$$K(\theta) = \tfrac{1}{2}(1 + \cos \theta). \qquad (10.72)$$

As shown in Fig. 10.46, θ is the angle made with the normal to the primary wavefront, **k**. This has its maximum value, $K(0) = 1$, in the forward direction and also dispenses with the back wave, since $K(\pi) = 0$.

Let us now examine the free propagation of a spherical monochromatic wave emitted from a *point source S*. If the Huygens–Fresnel principle is correct we should be able to add up the secondary wavelets arriving at a point P and thus obtain the unobstructed primary wave. In the process we will gain some insight, recognize a few shortcomings, and develop a very useful technique. Consider the construction shown in Fig. 10.47. The spherical surface corresponds to the primary wavefront at some arbitrary time t' after it has been emitted from S at $t = 0$. The disturbance, having a radius ρ, can be represented by any one of the mathematical expressions describing a harmonic spherical wave, for example,

$$E = \frac{\mathcal{E}_0}{\rho} \cos (\omega t' - k\rho). \qquad (10.73)$$

As illustrated, we have divided the wavefront into a number of annular regions. The boundaries of the various regions correspond to the intersections of the wavefront with a series of spheres centered at P of radius $r_0 + \lambda/2$, $r_0 + \lambda$, $r_0 + 3\lambda/2$, and so forth. These are the **Fresnel** or **half-period zones**. Notice that, for a secondary point source in one zone, there will be a

* It is interesting to read Fresnel's own words on the matter, keeping in mind that he was talking about light as an elastic vibration of the aether.

> Since the impulse communicated to every part of the primitive wave was directed along the normal, the motion which each tends to impress upon the aether ought to be more intense in this direction than in any other; and the rays which would emanate from it, if acting alone, would be less and less intense as they deviated more and more from this direction.
>
> The investigation of the law according to which their intensity varies about each center of disturbance is doubtless a very difficult matter; . . .

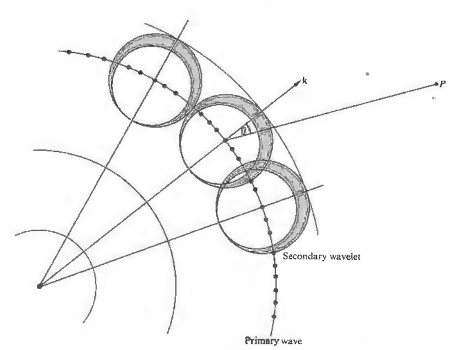


Figure 10.46 Secondary wavelets.

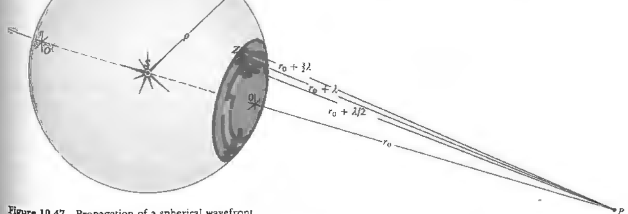


Figure 10.47 Propagation of a spherical wavefront.

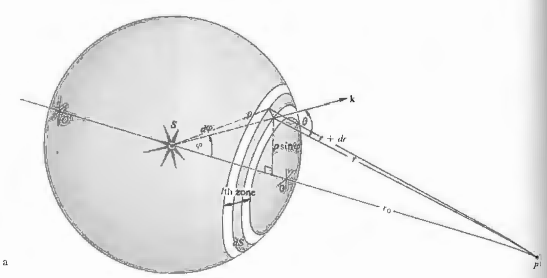


Figure 10.48 Propagation of a spherical wavefront.

point source in the adjacent zone that is further from P by an amount $\lambda/2$. Since each zone, although small, is finite in extent, we define a ring-shaped differential area element dS, as indicated in Fig. 10.48. All the point sources within dS are coherent, and *we assume that each radiates in phase with the primary wave* (10.73). The secondary wavelets travel a distance r to reach P, at a time t, all arriving there with the same phase, $\omega t - k(\rho + r)$. The amplitude of the primary wave at a distance ρ from S is $\mathcal{E}_0/\rho$. We assume, accordingly, that the source strength per unit area $\mathcal{E}_A$ of the secondary emitters on dS is proportional to $\mathcal{E}_0/\rho$ by way of a constant Q, that is, $\mathcal{E}_A = Q\mathcal{E}_0/\rho$. The contribution to the optical disturbance at P from the secondary sources on dS is, therefore,

$$dE = K\frac{\mathcal{E}_A}{r}\cos[\omega t - k(\rho + r)]\,dS. \qquad (10.74)$$

The obliquity factor must vary slowly and may be assumed to be constant over a single Fresnel zone. To get dS as a function of r, begin with

$$dS = \rho\, d\varphi\, 2\pi(\rho \sin\varphi).$$

Applying the law of cosines, we get

$$r^2 = \rho^2 + (\rho + r_0)^2 - 2\rho(\rho + r_0)\cos\varphi.$$

Upon differentiation this yields

$$2r\,dr = 2\rho(\rho + r_0)\sin\varphi\, d\varphi,$$

with ρ and r_0 held constant. Making use of the value of $d\varphi$, we find that the area of the element is therefore

$$dS = 2\pi\frac{\rho}{(\rho + r_0)}r\,dr. \qquad (10.75)$$

The disturbance arriving at P from the lth zone is

$$E_l = K_l 2\pi\frac{\mathcal{E}_A\rho}{(\rho + r_0)}\int_{r_{l-1}}^{r_l}\cos[\omega t - k(\rho + r)]\,dr.$$

Hence

$$E_l = \frac{-K_l\mathcal{E}_A\rho\lambda}{(\rho + r_0)}[\sin(\omega t - k\rho - kr)]_{r=r_{l-1}}^{r=r_l}.$$

Upon the introduction of $r_{l-1} = r_0 + (l-1)\lambda/2$ and $r_l = r_0 + l\lambda/2$, the expression reduces (Problem 10.42) to

$$E_l = (-1)^{l+1}\frac{2K_l\mathcal{E}_A\rho\lambda}{(\rho + r_0)}\sin[\omega t - k(\rho + r_0)]. \qquad (10.76)$$

Observe that the amplitude of E_l alternates between positive and negative values, depending on whether l is odd or even. This means that the contributions from adjacent zones are out of phase and tend to cancel. It is here that the obliquity factor makes a crucial difference. As l increases, θ increases and K decreases, so that successive contributions do not in fact completely cancel each other. It is interesting to note that E_l/K_l is independent of any position variables. Although the areas of each zone are almost equal, they do increase slightly as l increases, which means an increased number of emitters. But the mean distance from each zone to P also increases, such that E_l/K_l remains constant (see Problem 10.43).

The sum of the optical disturbances from all m zones at P is

$$E = E_1 + E_2 + E_3 + \cdots + E_m,$$

and since these alternate in sign, we can write

$$E = |E_1| - |E_2| + |E_3| - \cdots \pm |E_m|. \qquad (10.77)$$

If m is odd, the series can be reformulated in two ways, either as

$$E = \frac{|E_1|}{2} + \left(\frac{|E_1|}{2} - |E_2| + \frac{|E_3|}{2}\right) + \left(\frac{|E_3|}{2} - |E_4| + \frac{|E_5|}{2}\right) + \cdots + \left(\frac{|E_{m-2}|}{2} - |E_{m-1}| + \frac{|E_m|}{2}\right) + \frac{|E_m|}{2}, \qquad (10.78)$$

or as

$$E = |E_1| - \frac{|E_2|}{2} - \left(\frac{|E_2|}{2} - |E_3| + \frac{|E_4|}{2}\right) - \left(\frac{|E_4|}{2} - |E_5| + \frac{|E_6|}{2}\right) + \cdots + \left(\frac{|E_{m-3}|}{2} - |E_{m-2}| + \frac{|E_{m-1}|}{2}\right) - \frac{|E_{m-1}|}{2} + |E_m|. \qquad (10.79)$$

There are now two possibilities: either $|E_l|$ is greater than the arithmetic mean of its two neighbors $|E_{l-1}|$ and $|E_{l+1}|$, or it is less than that mean. This is really a question concerning the rate of change of $K(\theta)$. When

$$|E_l| > (|E_{l-1}| + |E_{l+1}|)/2$$

each bracketed term is negative. It follows from Eq. (10.78) that

$$E < \frac{|E_1|}{2} + \frac{|E_m|}{2} \qquad (10.80)$$

and from Eq. (10.79) that

$$E > |E_1| - \frac{|E_2|}{2} - \frac{|E_{m-1}|}{2} + |E_m|. \qquad (10.81)$$

Since the obliquity factor goes from 1 to 0 over a great many zones, we can neglect any variation between adjacent zones, that is, $|E_1| \approx |E_2|$ and $|E_{m-1}| \approx |E_m|$. Expression (10.81), to the same degree of approximation, becomes

$$E > \frac{|E_1|}{2} + \frac{|E_m|}{2} \qquad (10.82)$$

We conclude from (10.80) and (10.82) that

$$E \approx \frac{|E_1|}{2} + \frac{|E_m|}{2}. \qquad (10.83)$$

This same result is obtained when

$$|E_l| < (|E_{l-1}| + |E_{l+1}|)/2.$$

If the last term, $|E_m|$, in the series of Eq. (10.77) corresponds to an even m, the same procedure (Problem 10.44) leads to

$$E \approx \frac{|E_1|}{2} - \frac{|E_m|}{2}. \qquad (10.84)$$

Fresnel conjectured that the obliquity factor was such that the last contributing zone occurred at $\theta = 90°$, that is,

$$K(\theta) = 0 \quad \text{for } \pi/2 \le |\theta| \le \pi.$$

In that case Eqs. (10.83) and (10.84) both reduce to

$$E \approx \frac{|E_1|}{2} \qquad (10.85)$$

when $|E_m|$ goes to zero, because $K_m(\pi/2) = 0$. Alternatively, using Kirchhoff's correct obliquity factor, we divide the *entire* spherical wave into zones with the last or mth zone surrounding O'. Now θ approaches π, $K_m(\pi) = 0$, $|E_m| = 0$, and once again $E \approx |E_1|/2$. *The optical disturbance generated by the entire unobstructed wavefront is approximately equal to one half the contribution from the first zone.*

If the primary wave were simply to propagate from S to P in a time t, it would have the form

$$E = \frac{\mathcal{E}_0}{(\rho + r_0)}\cos[\omega t - k(\rho + r_0)]. \qquad (10.86)$$

Yet the disturbance synthesized from secondary wavelets, Eqs. (10.76) and (10.85), is

$$E = \frac{K_1 \mathcal{E}_A \rho \lambda}{(\rho + r_0)} \sin [\omega t - k(\rho + r_0)]. \qquad (10.87)$$

These two equations must, however, be exactly equivalent, and we interpret the constants in Eq. (10.87) to make them so. Note that there is some latitude in how we do this. We prefer to have the obliquity factor equal to 1 in the forward direction, that is, $K_1 = 1$ (rather than $1/\lambda$), from which it follows that Q must be equal to $1/\lambda$. In that case, $\mathcal{E}_A \rho \lambda = \mathcal{E}_0$, which is fine dimensionally. Keep in mind that $\mathcal{E}_A$ is the secondary-wavelet source strength per unit area over the primary wavefront of radius ρ, and $\mathcal{E}_0/\rho$ is the amplitude of that primary wave $E_0(\rho)$. Thus $\mathcal{E}_A = E_0(\rho)/\lambda$. There is one other problem, and that is the $\pi/2$ phase difference between Eqs. (10.86) and (10.87). This can be accounted for if we are willing to assume that the secondary sources radiate one quarter of a wavelength out of phase with the primary wave (see Section 3.5.2).

We have found it necessary to modify the initial statement of the Huygens–Fresnel principle, but this should not distract us from our rather pragmatic reasons for using it, which are twofold. First, the Huygens–Fresnel theory can be shown to be an approximation of the Kirchhoff formulation and as such is no longer merely a contrivance. Second, it yields, in a fairly simple way, many predictions that are in fine agreement with experimental observations. Don't forget that it worked quite well in the Fraunhofer approximation.

10.3.2 The Vibration Curve

We now develop a graphic method for qualitatively analyzing a number of diffraction problems that arise predominantly from circularly symmetric configurations.

Imagine that the first, or polar, Fresnel zone in Fig. 10.47 is divided into N subzones by the intersection of spheres, centered on P, of radii

$$r_0 + \lambda/2N,\ r_0 + \lambda/N,\ r_0 + 3\lambda/2N, \ldots, r_0 + \lambda/2.$$

Each subzone contributes to the disturbance at P, the resultant of which is of course just E_1. Since the phase difference across the entire zone, from O to its edge, is π rad (corresponding to $\lambda/2$), each subzone is shifted by π/N rad. Figure 10.49 depicts the vector addition of the subzone phasors, where, for convenience, $N = 10$. The chain of phasors deviates very slightly from the circle, because the obliquity factor shrinks each successive amplitude. When the number of subzones is increased to infinity (i.e., $N \to \infty$), the polygon of vectors blends into a segment of a smooth spiral called a **vibration curve**. For each additional Fresnel zone, the vibration curve swings through *one half-turn* and a phase of π as it spirals inward. As shown in Fig. 10.50, the points O_z, Z_{z1}, Z_{z2}, Z_{z3}, ..., O'_z on the spiral correspond to points $O, Z_1, Z_2, Z_3, \ldots, O'$, respectively, on the wavefront in Fig. 10.47. Each point $Z_1, Z_2, \ldots, Z_m$ lies on the periphery of a zone, so each point $Z_{z1}, Z_{z2}, \ldots, Z_{zm}$ is separated by a half-turn. We will see later, in Eq. (10.91), that the radius of each zone is proportional to the square root of its numerical designation, m. The radius of the hundredth zone will be only 10 times that

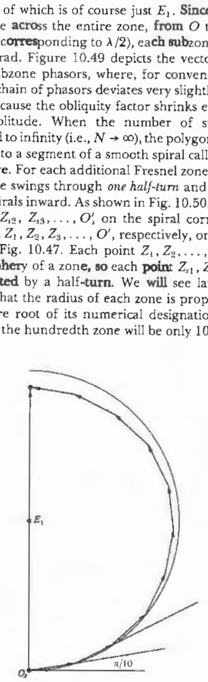


Figure 10.49 Phasor addition.

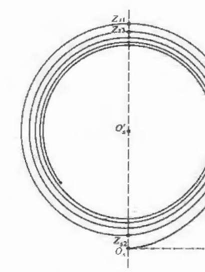


Figure 10.50 The vibration curve.

of the first zone. Initially, therefore, the angle θ increases rapidly, the thereafter it gradually slows down as m becomes larger. Accordingly, $K(\theta)$ decreases rapidly only for the first few zones. The result is that as the spiral circulates around with increasing m, it becomes tighter and tighter, deviating from a circle by a smaller amount for each revolution.

Keep in mind that the spiral is made up of an infinite number of phasors, each shifted by a small phase angle. The relative phase between any two disturbances at P, coming from two points on the wavefront, say O and A, can be depicted as shown in Fig. 10.51. The angle made by the tangents to the vibration curve, at points O_z and A_z, is β, and this is the desired phase difference. If the point A is considered to lie on the boundary of a cap-shaped region of the wavefront, the resultant at P from the whole region is $\overline{O_zA_z}$ at an angle δ.

The total disturbance arriving at P from an unimpeded wave is the sum of the contributions from all the zones between O and O'. The length of the vector from O_z to O'_z is therefore precisely that amplitude. Note that as expected, the amplitude $O_zO'_z$ is just about one half the contribution from the first zone, O_zZ_{z1}. Observe that $\overline{O_zO'_z}$ has a phase of 90° with respect to the wave arriving at P from O. A wavelet emitted at O in phase with the primary excitation gets to P still in phase with the primary wave. This means that $\overline{O_zO'_z}$ is 90° out of phase with the unobstructed primary wave. This, as we have seen, is one of the shortcomings of the Fresnel formulation.

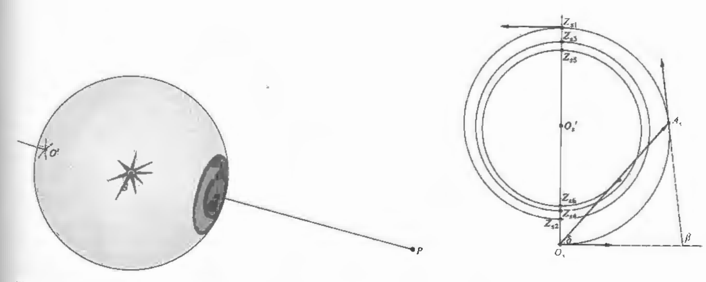


Figure 10.51 Wavefront and corresponding vibration curve.

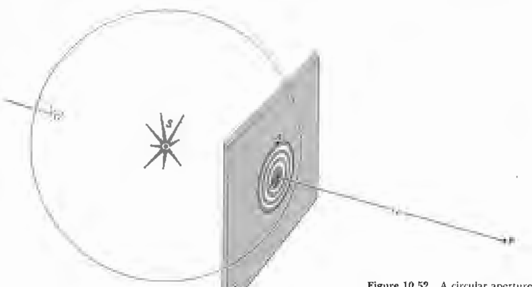


Figure 10.52 A circular aperture.

10.3.3 Circular Apertures

i) Spherical Waves

Fresnel's procedure, applied to a point source, can be used as a semiquantitative method to study diffraction at a circular aperture. Envision a monochromatic spherical wave impinging on a screen containing a small hole, as illustrated in Fig. 10.52. We first record the irradiance arriving at a very small sensor placed at point P on the symmetry axis. Our intention is to move the sensor around in space and so get a point-by-point map of the irradiance of the region beyond Σ.

Let us assume that the sensor at P "sees" an integral number of zones, m, filling the aperture. In actuality, the sensor merely records the irradiance at P, the zones having no reality. If m is even, then since $K_m = 0$,

$$E = (|E_1| - |E_2|) + (|E_3| - |E_4|) + \cdots + (|E_{m-1}| - |E_m|)$$

Because each adjacent contribution is nearly equal,

$$E = 0$$

and $I \approx 0$. If, on the other hand, m is odd,

$$E = |E_1| - (|E_2| - |E_3|) - (|E_4| - |E_5|) - \cdots - (|E_{m-1}| - |E_m|)$$

and

$$E \approx |E_1|,$$

which is roughly twice the amplitude of the unobstructed wave. This is truly an amazing result. By inserting a screen in the path of the wave, thereby blocking out most of the wavefront, we have increased the irradiance at P by a factor of four. Conservation of energy clearly demands that there be other points where the irradiance has decreased. Because of the complete symmetry of the setup, we can expect a circular ring pattern. If m is not an integer (i.e., a fraction of a zone appears in the aperture), the irradiance at P is somewhere between zero and its maximum value. You might see this all a bit more clearly if you imagine that the aperture is expanding smoothly from an initial value of nearly zero. The amplitude at P can be determined from the vibration curve, where A is any point on the edge of the hole. The phasor magnitude O_sA_s is the desired amplitude of the optical field. Return to Fig. 10.51; as the hole increases, A_s moves counterclockwise around the spiral toward Z_{s1} and a maximum. Allowing the second zone in reduces O_sA_s to O_sZ_{s2}, which is nearly zero, and P becomes a dark spot. As the aperture increases, O_sA_s oscillates in length from nearly zero to a number of successive maxima, which themselves gradually decrease. Finally, when the hole is fairly large, the wave is essentially unobstructed, A_s approaches O'_s, and further changes in O_sA_s are imperceptible.

To map the rest of the pattern, we now move the sensor along any line perpendicular to the axis, as shown in Fig. 10.53. At P we assume that two complete zones fill the aperture and $E \approx 0$. At P_1 the second zone has been partially obscured and the third begins to show; E is no longer zero. At P_2 a good fraction of the second zone is hidden, whereas the third is even more evident. Since the contributions from the first and third zones are in phase, the sensor, placed anywhere on the dotted circle passing through P_2, records a bright spot. As it moves radially outward and portions of successive zones are uncovered, the sensor detects a series of relative

maxima and minima. Figure 10.54 shows the diffraction patterns for a number of holes ranging in diameter from 1 mm to 4 mm as they appear on a screen 1 m away. Starting from the top left and moving right, the first four holes are so small that only a fraction of the first zone is uncovered. The sixth hole uncovers the first and second zones and is therefore black at its center. The ninth hole uncovers the first three zones and is once again bright at its center. Notice that even slightly beyond the geometric shadow at P_3, in Fig. 10.53, the first zone is partially uncovered. Each of the last few contributing segments is only a small fraction of its respective zone and as such is negligible. The sum of all the amplitudes of the fractional zones, although small, is therefore still finite. Further into the geometric shadow, however, the entire first zone is obscured, the last terms are again negligible, and this time the series does indeed go to zero and darkness.

We can gain a better appreciation of the actual size of the things we are dealing with by computing the number of zones in a given aperture. The area of each zone (from Problem 10.43) is given by

$$A = \frac{\rho}{(\rho + r_0)} \pi r_0 \lambda. \qquad (10.88)$$

Figure 10.53 Zones in a circular aperture.

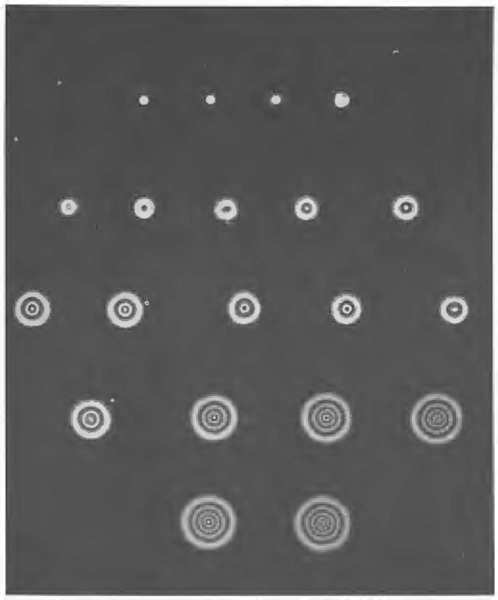


Figure 10.54 Diffraction patterns for circular apertures of increasing size.

If the aperture has a radius R, a good approximation of the number of zones within it is simply

$$\frac{\pi R^2}{A} = \frac{(\rho + r_0)R^2}{\rho r_0 \lambda}. \qquad (10.89)$$

For example, with a point source 1 m behind the aperture ($\rho \approx 1$ m), a plane of observation 1 m in front of it ($r_0 = 1$ m), and $\lambda = 500$ nm, there are 4 zones when $R = 1$ mm, and 400 zones when $R = 1$ cm. When both ρ and r_0 are increased to the point where only a small fraction of a zone appears in the aperture, Fraunhofer diffraction occurs. This is essentially a restatement of the Fraunhofer condition of Section 10.1.2; see Problem 10.1 as well.

It follows from Eq. (10.89) that the number of zones filling the aperture depends on the distance r_0 from P to O. As P moves in either direction along the central axis, the number of uncovered zones, whether increasing or decreasing, oscillates between odd and even integers. As a result, the irradiance goes through a series of maxima and minima. Clearly, this does not occur in the Fraunhofer configuration, where by definition, more than one zone cannot appear in the aperture.*

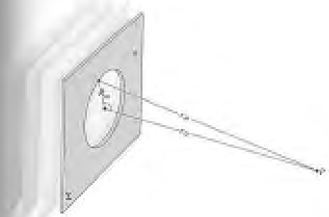


Figure 10.55 Plane waves incident on a circular hole.

(i) Plane Waves

Suppose now that the point source has been moved so far from the diffracting screen that the incoming light can be regarded as a plane wave ($\rho \to \infty$). Referring to Fig. 10.55, we derive an expression for the radius of the mth zone, R_m. Since $r_m = r_0 + m\lambda/2$,

$$R_m^2 = (r_0 + m\lambda/2)^2 - r_0^2,$$

and so

$$R_m^2 = m r_0 \lambda + m^2 \lambda^2/4. \qquad (10.90)$$

Under most circumstances the second term in Eq. (10.90) is negligible as long as m is not extremely large; consequently

$$R_m^2 = m r_0 \lambda, \qquad (10.91)$$

and *the radii are proportional to the square roots of integers.* Using a collimated He–Ne laser ($\lambda_0 = 632.8$ nm), the radius of the first zone is 1 mm when viewed from a distance of 1.58 m. Under these particular conditions Eq. (10.91) is applicable as long as $m \ll 10^7$, in which case $R_m = \sqrt{m}$ in millimeters. Figure 10.53 requires a slight modification in that now the lines $\overline{O_1P_1}$, $\overline{O_2P_2}$, and $\overline{O_3P_3}$ are perpendiculars dropped from the points of observation to Σ.

10.3.4 Circular Obstacles

In 1818 Fresnel entered a competition sponsored by the French Academy. His paper on the theory of diffraction ultimately won first prize and the title *Mémoire Couronné*, but not until it had provided the basis for a rather interesting story. The judging committee consisted of Pierre Laplace, Jean B. Biot, Siméon D. Poisson, Dominique F. Arago, and Joseph L. Gay-Lussac—a formidable group indeed. Poisson, who was an ardent critic of the wave description of light, deduced a remarkable and seemingly untenable conclusion from Fresnel's theory. He showed that a bright spot would be visible at the center of the shadow of a circular opaque obstacle, a result that he felt proved the absurdity of Fresnel's treatment. We can come to the same conclusion by considering the following, somewhat oversimplified argument. Recall that an unobstructed wave yields a disturbance (10.85) given by $E \approx |E_1|/2$. If some sort of obstacle precisely covers the first Fresnel zone, so that its contribution of $|E_1|$ is subtracted out, then $E \approx -|E_1|/2$. It is therefore possible that at some point P on the axis, the irradiance will be unaltered by the insertion of that obstruction. This surprising prediction, fashioned by Poisson as the death blow to the wave theory, was almost immediately verified experimentally

* R. S. Burch, "Fresnel Diffraction by a Circular Aperture," *Am. J. Phys.* 53, 255 (1985).

by Arago; the spot actually existed. Amusingly enough, Poisson's spot, as it is now called, had been observed many years earlier (1723) by Maraldi, but this work had long gone unnoticed.*

We now examine the problem a bit more closely, since it is quite evident from Fig. 10.56 that there is a good deal of structure in the actual shadow pattern. If the opaque obstacle, be it a disk or sphere, obscures the first ℓ zones, then

$$E = |E_{\ell+1}| - |E_{\ell+2}| + \cdots + |E_m|$$

(where, as before, there is no absolute significance to the signs other than that alternate terms must subtract). Unlike the analysis for the circular aperture, E_m now

* See J. E. Harvey and J. L. Forgham, "The Spot of Arago: New Relevance for an Old Phenomenon," *Am. J. Phys.* **52**, 243 (1984).

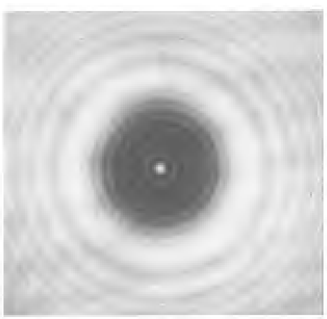


Figure 10.56 Shadow of a 1/8-inch diameter ball bearing. The bearing was glued to an ordinary microscope slide and illuminated with a He–Ne laserbeam. There are some faint extraneous nonconcentric fringes arising from both the microscope slide and a lens in the beam. (Photo by E. H.)

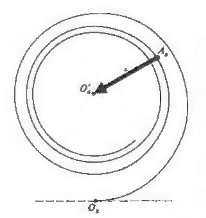


Figure 10.57 The vibration curve applied to a circular obstruction.

approaches zero, because $K_m \to 0$. The series must be evaluated in the same manner as that of the unobstructed wave (10.78 and 10.79). Repeating that procedure yields

$$E \approx \frac{|E_{\ell+1}|}{2}, \qquad (10.92)$$

and the irradiance on the central axis is generally only slightly less than that of the unobstructed wave. *There is a bright spot everywhere along the central axis except immediately behind the circular obstacle.* The wavelets propagating beyond the disk's circumference meet in phase on the central axis. Notice that as P moves closer to the disk, θ increases, $K_{\ell+1} \to 0$, and the irradiance gradually falls off to zero. If the disk is large, the $(\ell + 1)$th zone is very narrow, and any irregularities in the obstacle's surface may seriously obscure that zone. For Poisson's spot to be readily observable, the obstacle must be smooth and circular.

If A is a point on the periphery of the disk or sphere, A_s is the corresponding point on the vibration curve (Fig. 10.57). As the disk increases for a fixed P, A_s spirals in counterclockwise toward O'_s, and the amplitude $A_sO'_s$ gradually decreases. The same thing happens as P moves toward a disk of constant size.

Off the axis, the zones covered in Fig. 10.53 for the circular aperture will now be exposed and vice versa. Accordingly, a whole series of concentric bright and dark rings will surround the central spot.

The opaque disk images S at P and would similarly form a crude image of every point in an extended source. R. W. Pohl has shown that a small disk can therefore be used as a crude positive lens.

The diffraction pattern can be seen with little difficulty, but you need a telescope or binoculars. Glue a small ball bearing ($\approx\frac{1}{8}$ or $\frac{1}{4}$ inch in diameter) to a microscope slide, which then serves as a handle. Place the bearing a few meters beyond the point source and observe it from 3 or 4 meters away. Position it so that it is directly in front of and completely obscuring the source. You will need the telescope to magnify the image, since r_0 is so large. If you can hold the telescope steady, the ring system should be quite clear.

10.3.5 The Fresnel Zone Plate

In our previous considerations we utilized the fact that successive Fresnel zones tended to nullify each other. This suggests that we will observe a tremendous increase in irradiance at P, if we remove either all the even or all the odd zones. A screen that alters the light, either in amplitude or phase, coming from every other half-period zone is called a **zone plate.***

Suppose that we construct a zone plate that passes only the first 20 odd zones and obstructs the even zones.

$$E = E_1 + E_3 + E_5 + \cdots + E_{39},$$

and each of these terms is approximately equal. For an unobstructed wavefront, the disturbance at P would be $E_1/2$, whereas with the zone plate in place, $E = 20E_1$. The irradiance has been increased by a factor of 1600. The same result would obviously be true if the even zones were passed instead.

To calculate the radii of the zones shown in Fig. 10.58, refer to Fig. 10.59. The outer edge of the mth zone is marked by the point A_m. By definition, a wave that travels the path S–A_m–P must arrive out of phase by $m\lambda/2$ with a wave that traverses the path S–O–P, that is,

$$(\rho_m + r_m) - (\rho_0 + r_0) = m\lambda/2. \qquad (10.93)$$

Clearly $\rho_m = (R_m^2 + \rho_0^2)^{1/2}$ and $r_m = (R_m^2 + r_0^2)^{1/2}$. Expand both these expressions using the binomial series. Since R_m is comparatively small, retaining only the first two terms yields

$$\rho_m = \rho_0 + \frac{R_m^2}{2\rho_0} \quad \text{and} \quad r_m = r_0 + \frac{R_m^2}{2r_0}.$$

* Lord Rayleigh seems to have invented the zone plate, as witnessed by this entry of April 11, 1871, in his notebook: "The experiment of blocking out the odd Huygens zones so as to increase the light at centre succeeded very well . . . ."

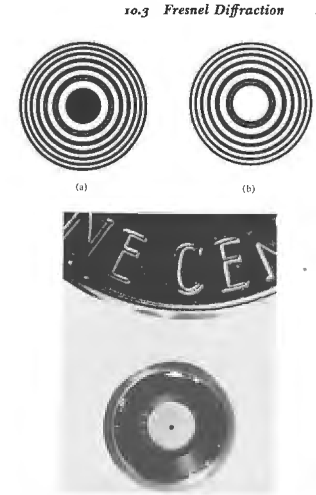


Figure 10.58 (a) and (b) Zone plates. (c) A zone plate used to image alpha particles coming from a target 1 cm in front, on photographic film 5 cm behind. The plate is 2.5 mm in diameter and contains 100 zones, the narrowest of which is 5.3 μm wide. (Photo courtesy Lawrence Livermore Laboratory.)

Finally, substituting into Eq. (10.93), we obtain

$$\left(\frac{1}{\rho_0}+\frac{1}{r_0}\right)=\frac{m\lambda}{R_m^2}. \tag{10.94}$$

Under plane-wave illumination ($\rho_0 \to \infty$), and Eq. (10.94) reduces to

$$R_m^2 = mr_0\lambda, \tag{10.91}$$

which is an approximation of the exact expression stated by Eq. (10.90). Equation (10.94) has a form identical to that of the thin-lens equation, which is not merely a coincidence, since S is actually imaged in converging diffracted light at P. Accordingly, the *primary focal length* is said to be

$$f_1 = \frac{R_m^2}{m\lambda}. \tag{10.95}$$

(Note that the zone plate will show extensive chromatic aberration.) The points S and P are said to be conjugate foci. With a collimated incident beam (Fig. 10.60) the image distance is the primary or *first-order* focal length, which in turn corresponds to a principal maximum in the irradiance distribution. In addition to this real image, there is also a virtual image formed of diverging light a distance f_1 in front of Σ. At a distance of f_1 from Σ each ring on the plate is filled by exactly one half-period zone on the wavefront. If we move a sensor along the S–P axis toward Σ, it registers a series of very small irradiance maxima and minima until it arrives at a point $f_1/3$ from Σ. At that *third-order focal point*, there is a pronounced irradiance peak. Additional focal points will exist at $f_1/5$, $f_1/7$, and so forth, unlike a lens but even more unlike a simple opaque disk.

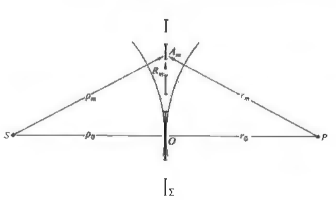


Figure 10.59 Zone-plate geometry.

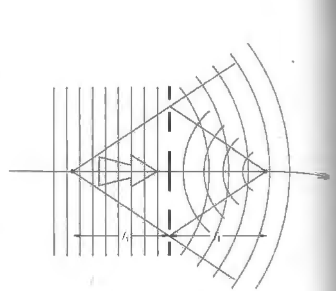


Figure 10.60 Zone-plate foci.

Following a suggestion by Lord Rayleigh, R. W. Wood constructed a *phase-reversal zone plate*. Instead of blocking out every other zone, he increased the thickness of alternate zones, thereby retarding their phase by π. Since the entire plate is transparent, the amplitude should double, and the irradiance increase by a factor of four. In actuality, the device does not work quite that well, because the phase is not really constant over each zone. Ideally, the retardation should be made to vary gradually over a zone, jumping back by π at the start of the next zone.*

The usual way to make an optical zone plate is to draw a large-scale version and then photographically reduce it. Plates with hundreds of zones can be made by photographing a Newton's ring pattern, in collimated quasimonochromatic light. Rings of aluminum foil on cardboard work very well for microwaves.

Zone plates can be made of metal with a self-supporting spoked structure, so that the transparent regions are devoid of any material. These will function as lenses in the range from ultraviolet to soft x-rays, where ordinary glass is opaque.

* See Ditchburn, *Light*, 2nd ed., p. 232; M. Sussman, "Elementary Diffraction Theory of Zone Plates," *Am. J. Phys.* **28**, 394 (1960); Ora E. Myers, Jr., "Studies of Transmission Zone Plates," *Am. J. Phys.* **19**, 359 (1951); and J. Higbie, "Fresnel Zone Plate: Anomalous Foci," *Am. J. Phys.* **44**, 929 (1976).

10.3.6 Fresnel Integrals and the Rectangular Aperture

We now consider a class of problems within the domain of Fresnel diffraction, which no longer have the circular symmetry of the previously studied configurations. Consider Fig. 10.61 where dS is an area element situated at some arbitrary point A whose coordinates are (y, z). The location of the origin O is determined by a perpendicular drawn to Σ from the position of the monochromatic point source. The contribution to the optical disturbance at P from the secondary sources on dS has the form given by Eq. (10.74). Making use of what we learned from the freely propagating wave ($\mathcal{E}_A\rho\lambda = \mathcal{E}_0$), we can rewrite that equation as

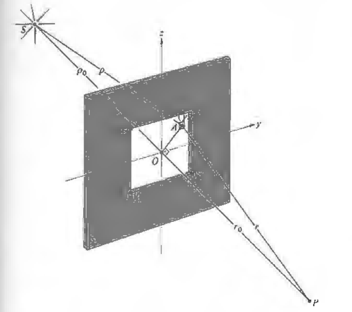


Figure 10.61 Fresnel diffraction at a rectangular aperture.

$$dE_p = \frac{K(\theta)\mathcal{E}_0}{\rho r\lambda}\cos\left[k(\rho+r)-\omega t\right]dS. \tag{10.96}$$

The sign of the phase has changed from that of Eq. (10.74) and is written in this way to conform with traditional treatment. *In the case where the dimensions of the aperture are small* in comparison to ρ_0 and r_0, we can set $K(\theta) = 1$ and let $1/\rho r$ equal $1/\rho_0 r_0$ in the amplitude coefficient. Being more careful about approximations introduced into the phase, apply the Pythagorean theorem to triangles SOA and POA to get

$$\rho = (\rho_0^2 + y^2 + z^2)^{1/2}$$

and

$$r = (r_0^2 + y^2 + z^2)^{1/2}.$$

Expand these using the binomial series and form

$$\rho + r = \rho_0 + r_0 + (y^2+z^2)\frac{\rho_0+r_0}{2\rho_0 r_0}. \tag{10.97}$$

Observe that this is a more sensitive approximation than that used in the Fraunhofer analysis (10.40), where the terms quadratic and higher in the aperture variables were neglected. The disturbance at P in the complex representation is

$$E_p = \frac{\mathcal{E}_0 e^{-i\omega t}}{\rho_0 r_0\lambda}\int_{y_1}^{y_2}\int_{z_1}^{z_2} e^{ik(\rho+r)}\,dy\,dz. \tag{10.98}$$

Following the usual form of derivation, we introduce the dimensionless variables u and v defined by

$$u = y\left[\frac{2(\rho_0+r_0)}{\lambda\rho_0 r_0}\right]^{1/2}, \qquad v = z\left[\frac{2(\rho_0+r_0)}{\lambda\rho_0 r_0}\right]^{1/2} \tag{10.99}$$

Substituting Eq. (10.97) into Eq. (10.98) and utilizing the new variables, we arrive at

$$E_p = \frac{\mathcal{E}_0}{2(\rho_0+r_0)}e^{i[k(\rho_0+r_0)-\omega t]}\int_{u_1}^{u_2} e^{i\pi u^2/2}\,du\int_{v_1}^{v_2} e^{i\pi v^2/2}\,dv. \tag{10.100}$$

The term in front of the integral represents the unobstructed disturbance at P divided by 2; let us call it $E_u/2$. The integral itself can be evaluated using two functions, $\mathscr{C}(w)$ and $\mathscr{S}(w)$, where w represents either u or v. These quantities, which are known as the **Fresnel integrals**, are defined by

$$\mathscr{C}(w) = \int_0^w \cos(\pi w'^2/2)\, dw',$$

$$\mathscr{S}(w) = \int_0^w \sin(\pi w'^2/2)\, dw'. \qquad (10.101)$$

Both functions have been extensively studied, and their numerical values are well tabulated. Their interest to us at this point derives from the fact that

$$\int_0^w e^{i\pi w'^2/2}\, dw' = \mathscr{C}(w) + i\mathscr{S}(w),$$

and this, in turn, has the form of the integrals in Eq. (10.100). The disturbance at P is then

$$E_p = \frac{E_u}{2}[\mathscr{C}(u) - i\mathscr{S}(u)]_{u_1}^{u_2}[\mathscr{C}(v) + i\mathscr{S}(v)]_{v_1}^{v_2}, \qquad (10.102)$$

which can be evaluated using the tabulated values of $\mathscr{C}(u_1)$, $\mathscr{C}(u_2)$, $\mathscr{S}(u_1)$, and so on. The mathematics becomes rather involved if we compute the disturbance at all points of the plane of observation, leaving the position of the aperture fixed. Instead we will fix the *S–O–P* line and imagine that we move the aperture through small displacements in the Σ-plane. This has the effect of translating the origin O with respect to the fixed aperture, thereby scanning the pattern over the point P. Each new position of O corresponds to a new set of relative boundary locations y_1, y_2, z_1, and z_2. These in turn mean new values of u_1, u_2, v_1, and v_2, which, when substituted into Eq. (10.102), yield a new E_p. The error encountered in such a procedure is negligible, as long as the aperture is displaced by distances that are small compared with ρ_0. This approach is therefore even more appropriate to incident plane waves. In that case if E_0 is the amplitude of the incoming plane wave at Σ, Eq. (10.96) becomes simply

$$dE_p = \frac{E_0 K(\theta)}{r\lambda}\cos(kr - \omega t)\, dS,$$

where, as before, $\mathcal{E}_A = E_0/\lambda$. This time, with

$$u = y\left(\frac{2}{\lambda r_0}\right)^{1/2}, \qquad v = z\left(\frac{2}{\lambda r_0}\right)^{1/2}, \qquad (10.103)$$

where we have divided the numerator and denomi in Eq. (10.99) by ρ_0 and then let it go to infini takes the same form as Eq. (10.102), where E_u is the unobstructed disturbance. The irradiance at $E_pE_p^*/2$ (keep in mind that E_u is complex); hence

$$I_p = \frac{I_0}{4}\{[\mathscr{C}(u_2) - \mathscr{C}(u_1)]^2 + [\mathscr{S}(u_2) - \mathscr{S}(u_1)]^2\}$$
$$\times \{[\mathscr{C}(v_2) - \mathscr{C}(v_1)]^2 + [\mathscr{S}(v_2) - \mathscr{S}(v_1)]^2\}, \qquad \text{[illegible]}$$

where I_0 is the unobstructed irradiance at P.

As a simple example, envision a square hole 2 on each side under plane-wave illumination at 500 If P is 4 m away and directly opposite point O at the center of the aperture, $u_2 = 1.0$, $u_1 = -1.0$, $v_2 = 1.0$, and $v_1 = -1.0$. The Fresnel integrals are both odd functions, that is,

$$\mathscr{C}(w) = -\mathscr{C}(-w) \quad \text{and} \quad \mathscr{S}(w) = -\mathscr{S}(-w);$$

consequently

$$I_p = \frac{I_0}{4}\{[2\mathscr{C}(1)]^2 + [2\mathscr{S}(1)]^2\}^2,$$

and a numerical value is easily obtained. To find the irradiance somewhere else in the pattern, for exam 0.1 mm to the left of center, move the aperture rela to the *OP*-line accordingly, whereupon $u_2 = 1.1$, $u_1 =$ -0.9, $v_2 = 1.0$, and $v_1 = -1.0$. The resultant I_p will al be equal to that found at 0.1 mm to the right of cent Indeed, because the aperture is square, the same va obtains 0.1 mm directly above and below center as (Fig. 10.62).

We can approach the limiting case of free propaga by allowing the aperture dimensions to incre indefinitely. Making use of the fact that $\mathscr{C}(\infty) = \mathscr{S}(\infty) = \frac{1}{2}$ and $\mathscr{C}(-\infty) = \mathscr{S}(-\infty) = -\frac{1}{2}$ the irradiance at P, oppo the center of the aperture, is

$$I_p = I_0,$$

which is exactly correct. This is rather remarkable, co sidering that when the length $\overline{OA}$ is large, all the approximations made in the derivation are no longer applicable. It should be realized, however, that a rela tively small aperture satisfying the approximations ca still be large enough to effectively show no diffractio

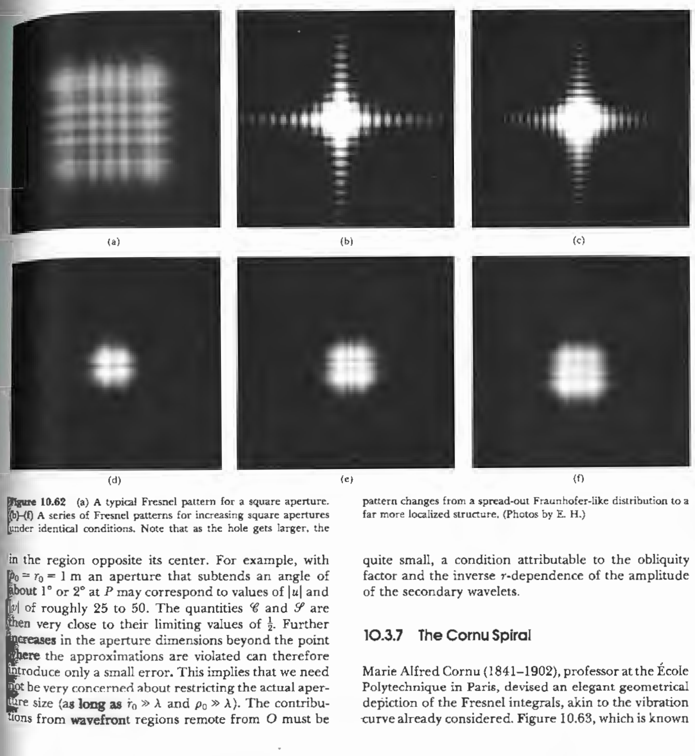


Figure 10.62 (a) A typical Fresnel pattern for a square aperture. (b)–(f) A series of Fresnel patterns for increasing square apertures under identical conditions. Note that as the hole gets larger, the pattern changes from a spread-out Fraunhofer-like distribution to a far more localized structure. (Photos by E. H.)

in the region opposite its center. For example, with $\rho_0 = r_0 = 1$ m an aperture that subtends an angle of about 1° or 2° at P may correspond to values of $|u|$ and $|v|$ of roughly 25 to 50. The quantities $\mathscr{C}$ and $\mathscr{S}$ are then very close to their limiting values of $\frac{1}{2}$. Further increases in the aperture dimensions beyond the point where the approximations are violated can therefore introduce only a small error. This implies that we need not be very concerned about restricting the actual aperture size (as long as $r_0 \gg \lambda$ and $\rho_0 \gg \lambda$). The contributions from wavefront regions remote from O must be quite small, a condition attributable to the obliquity factor and the inverse r-dependence of the amplitude of the secondary wavelets.

10.3.7 The Cornu Spiral

Marie Alfred Cornu (1841–1902), professor at the École Polytechnique in Paris, devised an elegant geometrical depiction of the Fresnel integrals, akin to the vibration curve already considered. Figure 10.63, which is known

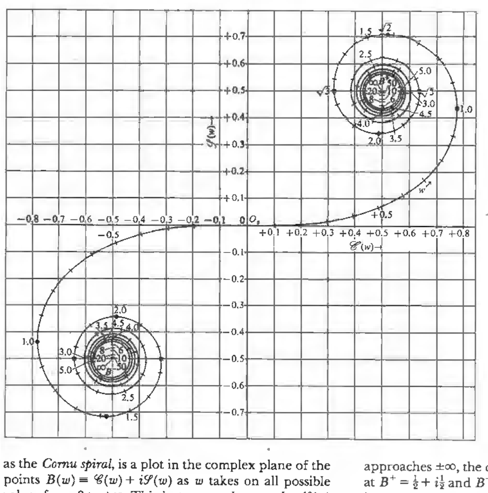


Figure 10.63 The Cornu spiral.

as the *Cornu spiral*, is a plot in the complex plane of the points $B(w) \equiv \mathscr{C}(w) + i\mathscr{S}(w)$ as w takes on all possible values from 0 to $\pm\infty$. This just means that we plot $\mathscr{C}(w)$ on the horizontal or real axis and $\mathscr{S}(w)$ on the vertical or imaginary axis. The appropriate numerical values are taken from Table 10.2. If $d\ell$ is an element of arc length measured along the curve, then

$$d\ell^2 = d\mathscr{C}^2 + d\mathscr{S}^2.$$

From the definitions (10.101),

$$d\ell^2 = (\cos^2 \pi w^2/2 + \sin^2 \pi w^2/2)\, dw^2$$

and

$$d\ell = dw.$$

Values of w correspond to the arc length and are marked off along the spiral in Fig. 10.63. As w approaches $\pm\infty$, the curve spirals into its limiting values at $B^+ = \frac{1}{2} + i\frac{1}{2}$ and $B^- = -\frac{1}{2} - i\frac{1}{2}$. The slope of the spiral is

$$\frac{d\mathscr{S}}{d\mathscr{C}} = \frac{\sin \pi w^2/2}{\cos \pi w^2/2} = \tan \frac{\pi w^2}{2}, \qquad (10.105)$$

and so the angle between the tangent to the spiral at any point and the $\mathscr{C}$-axis is $\beta = \pi w^2/2$.

The Cornu spiral can be used either as a convenient tool for quantitative determinations or as an aid to gaining a qualitative picture of a diffraction pattern (which was also the case with the vibration curve). As an example of its quantitative uses, reconsider the problem of a 2-mm-square hole, dealt with in the previous section (λ = 500 nm, r_0 = 4 m, and plane-wave illumination). We wish to find the irradiance at P directly opposite the aperture's center, where in this case u_1 = -1.0 and $u_2 = 1.0$. The variable u is measured along the arc; that is, w is replaced by u on the spiral. Place two points on the spiral at distances from O_s equal to u_1 and u_2. (These are symmetrical with respect to O_s, because P is now opposite the aperture's center.) Label the two points $B_1(u)$ and $B_2(u)$, respectively, as in Fig. 10.64. The phasor $\mathbf{B}_{12}(u)$ drawn from $B_1(u)$ to $B_2(u)$ is just the complex number $B_2(u) - B_1(u)$,

$$\mathbf{B}_{12}(u) = [\mathscr{C}(u) + i\mathscr{S}(u)]_{u_1}^{u_2},$$

and is the first term in the expression (10.102) for E_p. Similarly for $v_1 = -1.0$ and $v_2 = 1.0$, $B_2(v) - B_1(v)$ is

$$\mathbf{B}_{12}(v) = [\mathscr{C}(v) + i\mathscr{S}(v)]_{v_1}^{v_2},$$

which is the latter portion of E_p. The magnitudes of these two complex numbers are just the lengths of the appropriate $\mathbf{B}_{12}$-phasors, which can be read off the curve with a ruler, using either axis as a scale. The irradiance is then simply

$$I_p = \frac{I_0}{4} |\mathbf{B}_{12}(u)|^2 |\mathbf{B}_{12}(v)|^2, \qquad (10.106)$$

and the problem is solved. Notice that the arc lengths along the spiral (i.e., $\Delta u = u_2 - u_1$ and $\Delta v = v_2 - v_1$) are proportional to the aperture's overall dimensions in the y- and z-direction, respectively. *The arc lengths are therefore constant, regardless of the position of P in the plane*

Table 10.2 Fresnel integrals.

w	$\mathscr{C}(w)$	$\mathscr{S}(w)$	w	$\mathscr{C}(w)$	$\mathscr{S}(w)$
0.00	0.0000	0.0000	4.50	0.5261	0.4342
0.10	0.1000	0.0005	4.60	0.5673	0.5162
0.20	0.1999	0.0042	4.70	0.4914	0.5672
0.30	0.2994	0.0141	4.80	0.4338	0.4968
0.40	0.3975	0.0334	4.90	0.5002	0.4350
0.50	0.4923	0.0647	5.00	0.5637	0.4992
0.60	0.5811	0.1105	5.05	0.5450	0.5442
0.70	0.6597	0.1721	5.10	0.4998	0.5624
0.80	0.7230	0.2493	5.15	0.4553	0.5427
0.90	0.7648	0.3398	5.20	0.4389	0.4969
1.00	0.7799	0.4383	5.25	0.4610	0.4536
1.10	0.7638	0.5365	5.30	0.5078	0.4405
1.20	0.7154	0.6234	5.35	0.5490	0.4662
1.30	0.6386	0.6863	5.40	0.5573	0.5140
1.40	0.5431	0.7135	5.45	0.5269	0.5519
1.50	0.4453	0.6975	5.50	0.4784	0.5537
1.60	0.3655	0.6389	5.55	0.4456	0.5181
1.70	0.3238	0.5492	5.60	0.4517	0.4700
1.80	0.3336	0.4508	5.65	0.4926	0.4441
1.90	0.3944	0.3734	5.70	0.5385	0.4595
2.00	0.4882	0.3434	5.75	0.5551	0.5049
2.10	0.5815	0.3743	5.80	0.5298	0.5461
2.20	0.6363	0.4557	5.85,	0.4819	0.5513
2.30	0.6266	0.5531	5.90	0.4486	0.5163
2.40	0.5550	0.6197	5.95	0.4566	0.4688
2.50	0.4574	0.6192	6.00	0.4995	0.4470
2.60	0.3890	0.5500	6.05	0.5424	0.4689
2.70	0.3925	0.4529	6.10	0.5495	0.5165
2.80	0.4675	0.3915	6.15	0.5146	0.5496
2.90	0.5624	0.4101	6.20	0.4676	0.5398
3.00	0.6058	0.4963	6.25	0.4493	0.4954
3.10	0.5616	0.5818	6.30	0.4760	0.4555
3.20	0.4664	0.5933	6.35	0.5240	0.4560
3.30	0.4058	0.5192	6.40	0.5496	0.4965
3.40	0.4385	0.4296	6.45	0.5292	0.5398
3.50	0.5326	0.4152	6.50	0.4816	0.5454
3.60	0.5880	0.4923	6.55	0.4520	0.5078
3.70	0.5420	0.5750	6.60	0.4690	0.4631
3.80	0.4481	0.5656	6.65	0.5161	0.4549
3.90	0.4223	0.4752	6.70	0.5467	0.4915
4.00	0.4984	0.4204	6.75	0.5302	0.5362
4.10	0.5738	0.4758	6.80	0.4831	0.5436
4.20	0.5418	0.5633	6.85	0.4539	0.5060
4.30	0.4494	0.5540	6.90	0.4732	0.4624
4.40	0.4383	0.4622	6.95	0.5207	0.4591

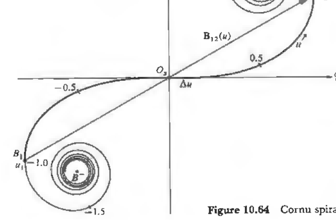


Figure 10.64 Cornu spiral.

of observation. On the other hand, the phasors $\mathbf{B}_{12}(u)$ and $\mathbf{B}_{12}(v)$, which span the arc lengths, are not constant, and they do depend on the location of P.

Maintaining the position of P opposite the center of the diffracting hole, now suppose that the aperture size is adjustable. As the square hole is gradually opened, Δv and Δu increase accordingly. The endpoints B_1 and B_2 of either of these arc lengths spiral around counterclockwise toward their limiting values of B^- and B^+, respectively. The phasors $\mathbf{B}_{12}(u)$ and $\mathbf{B}_{12}(v)$, which are identical in this instance because of the symmetry, pass through a series of extrema. The central spot in the pattern therefore gradually shifts from relative brightness to darkness and back. All the while, the entire irradiance distribution varies continually from one beautifully intricate display to the next (Fig. 10.62). For any particular aperture size, the off-center diffraction pattern can be computed by repositioning P. It is helpful to visualize the arc length as a piece of string, whose measure is equal to either Δv or Δu. Imagine it lying on the spiral, with O_s initially at its midpoint. As P is moved, for example, to the left along the y-axis (Fig. 10.61), y_1 and therefore u_1 both become less negative, and y_2 and u_2 increase positively. The result is that our Δu-string slides up the spiral. As the distance between the endpoints of the Δu-string changes, $|\mathbf{B}_{12}(u)|$ changes, and the irradiance (10.106) varies accordingly. When P is at the left edge of the geometric shadow, $y_1 = u_1 = 0$. As the point of observation moves into the geometric shadow, u_1 increases *positively*, and the Δu-string is now entirely on the upper half of the Cornu spiral. As u_1 and u_2 continue to increase, the string winds ever more tightly about the B^+-limit. Its ends, B_1 and B_2, become closer to each other, with the result that $|\mathbf{B}_{12}(u)|$ becomes quite small, and I_p decreases within the geometric shadow region. (We will come back to this point in more detail in the next section.) The same process applies when we scan in the z-direction; Δv is constant and $B_{12}(v)$ varies.

If the aperture is completely opened out, revealing an unobstructed wave, $u_1 = v_1 = -\infty$, which means that $B_1(u) = B_1(v) = B^-$ and $B_2(u) = B_2(v) = B^+$. The B^-B^+-line makes a 45° angle with the $\mathscr{C}$-axis and has a length equal to $\sqrt{2}$. Consequently, the phasors $\mathbf{B}_{12}(u)$ and $\mathbf{B}_{12}(v)$ each have magnitude $\sqrt{2}$ and phase $\pi/4$, that

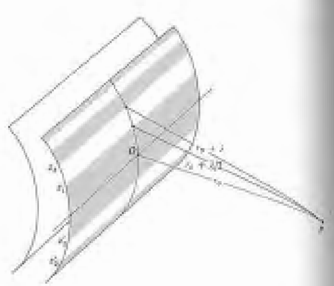


Figure 10.65 Cylindrical wavefront zones.

is, $\mathbf{B}_{12}(u) = \sqrt{2}\exp(i\pi/4)$ and $\mathbf{B}_{12}(v) = \sqrt{2}\exp(i\pi/4)$. It follows from Eq. (10.102) that

$$E_p = E_u e^{i\pi/2}, \tag{10.107}$$

and as in Section 10.3.1, we have the unobstructed amplitude, except for a $\pi/2$ phase discrepancy.* Finally, using (10.106), $I_p = I_0$.

We can construct a more palpable picture of what the Cornu spiral represents by considering Fig. 10.65, which depicts a cylindrical wavefront propagating from a coherent line source. The present procedure is exactly the same as that used in deriving the vibration curve, and the reader is referred back to Section 10.3.2 for a more leisurely discussion. Suffice it to say that the wavefront is divided into *half-period strip zones* by its intersection with a family of cylinders having a common axis and radii of $r_0 + \lambda/2$, $r_0 + \lambda$, $r_0 + 3\lambda/2$, and so on. *The contributions from these strip zones are proportional to their areas, which decrease rapidly.* This is in contrast to the circular zones, whose radii increase, thereby keeping the areas nearly constant. Each strip zone is similarly divided into N subzones, which have a relative phase

* The phase discrepancy will be resolved by the Kirchhoff theory in Section 10.4.

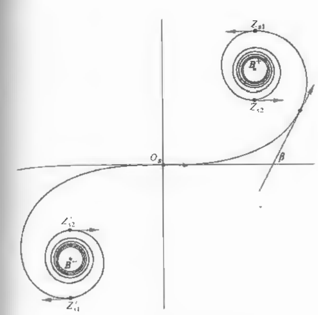


Figure 10.66 Cornu spiral related to the cylindrical wavefront.

difference of π/N. The vector sum of all the amplitude contributions from zones above the center line is a spiraling polygon. If N goes to ∞ and the contributions generated by the strip zones below the center line are included, the polygon smooths out into a continuous Cornu spiral. This is not surprising, since the coherent line source generates an infinite number of overlapping point-source patterns.

Figure 10.66 shows a number of unit tangent vectors at various positions along the spiral. The vector at O_s corresponds to the contribution from the central axis passing through O on the wavefront. The points associated with the boundaries of each strip zone can be located on the spiral, since at those positions the relative phase, β, is either an even or odd multiple of π. For example, the point Z_{s1} on the spiral (Fig. 10.66), which is related to z_1 (Fig. 10.65) on the wavefront, is by definition 180° out of phase with O_s. Therefore Z_{s1} must be located at the top of the spiral, where $w = \sqrt{2}$ inasmuch as there $\beta = \pi w^2/2 = \pi$.

It will be helpful as we go along in the treatment to visualize the blocking out of these strip zones when analyzing the effects of obstructions. Obviously one could even make an appropriate zone plate, which would accomplish this to some advantage, and such devices are in use.

10.3.8 Fresnel Diffraction by a Slit

We can treat Fresnel diffraction at a long slit as an extension of the rectangular-aperture problem. We need only elongate the rectangle by allowing y_1 and y_2 to move very far from O, as shown in Fig. 10.67. As the point of observation moves along the y-axis, so long as the vertical boundaries at either end of the slit are still essentially at infinity, $u_2 \approx \infty$, $u_1 \approx -\infty$, and $\mathbf{B}_{12}(u) \approx \sqrt{2}e^{i\pi/4}$. From Eq. (10.106), for either point-source or plane-wave illumination,

$$I_p = \frac{I_0}{2}|\mathbf{B}_{12}(v)|^2, \tag{10.108}$$

and the pattern is independent of y. The values of z_1 and z_2, which fix the slit width, determine the important parameter $\Delta v = v_2 - v_1$, which in turn governs $\mathbf{B}_{12}(v)$. Imagine once again that we have a string of length Δv

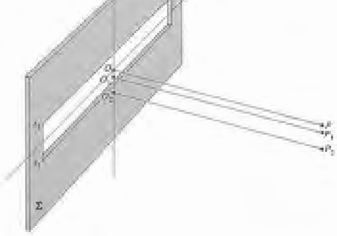


Figure 10.67 Single-slit geometry.

lying along the spiral. At P, opposite point O, the aperture is symmetrical, and the string is centered on O_s (Fig. 10.68). The chord $|\mathbf{B}_{12}(v)|$ need only be measured and substituted into Eq. (10.108) to find I_p. At point P_1, z_1 and therefore v_1 are smaller negative numbers, whereas z_2 and v_2 have increased positively. The arc length Δv (the string) moves up the spiral (Fig. 10.68), and the chord decreases. As the point of observation moves down into the geometric shadow, the string winds about B^+, and the chord goes through a series of relative extrema. If Δv is very small, our imaginary piece of string is small, and the chord $|\mathbf{B}_{12}(v)|$ decreases appreciably only when the radius of curvature of the spiral itself is small. This occurs in the vicinity of B^+ or B^-, that is, far out into the geometric shadow. There will therefore be light well beyond the edges of the aperture, as long as the aperture is relatively small. Note too that with small Δv there will be a broad central maximum. In fact, if Δv is much less than 1, $r_0\lambda$ is much greater than the aperture width, and the Fraunhofer condition prevails. This transition of Eq. (10.108) into the form of Eq. (10.17) is more plausible when we realize that

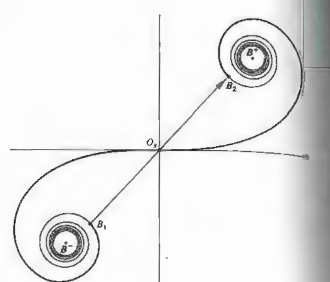


Figure 10.69 An irradiance minimum in the slit pattern.

for large w the Fresnel integrals have trigonometric representations (see Problem 10.46).

As the slit widens, Δv becomes larger, for a fixed r_0, until a configuration like that in Fig. 10.69 exists for a point opposite the slit's center. If the point of observation is moved vertically either up or down, Δv slides either down or up the spiral. Yet the chord increases in both cases, so that the center of the diffraction pattern must be a relative minimum. Fringes now appear within the geometric image of the slit, unlike the Fraunhofer pattern.

Figure 10.70 shows two curves of $|\mathbf{B}_{12}(w)|^2$ plotted against $(w_1 + w_2)/2$, which is the center point of the arc length Δw. (Recall that the symbol w stands for either u or v.) A family of such curves running the range in Δw from about 1 to 10 would cover the region of interest. The curves are computed by first choosing a particular Δw and then reading the appropriate $|\mathbf{B}_{12}(w)|$ values off the Cornu spiral as Δw slides along it. For a long slit

$$I_p = \frac{I_0}{2}|\mathbf{B}_{12}(v)|^2, \qquad [10.108]$$

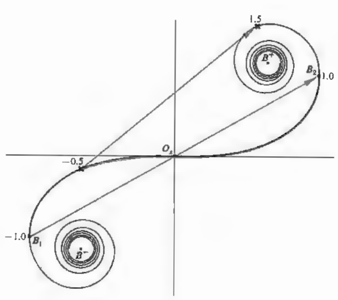


Figure 10.68 Cornu spiral for the slit.

and since Δz is the slit width that corresponds to Δv, each curve in Fig. 10.70 *is proportional to the irradiance distribution* for a given slit. For example, Fig. 10.70(a) can be read as $|\mathbf{B}_{12}(v)|^2$ versus $(v_1 + v_2)/2$ for $\Delta v = 2.5$. The abscissa relates to $(z_1 + z_2)/2$, that is, the displacement of the point of observation from the center of the slit. In Fig. 10.70(b) $\Delta w = 3.5$, which means that a slit having a $\Delta v = 3.5$ clearly has fringes appearing within the geometric image as expected (Problem 10.45). The curves could, of course, be plotted in terms of values of Δz or Δy explicitly, but that would unnecessarily limit them to one set of configuration parameters ρ_0, r_0, and λ.

As the slit is widened still further, Δv approaches and then surpasses 10. An increasing number of fringes appear within the geometric image, and the pattern no longer extends appreciably beyond that image.

The same kind of reasoning applies equally well to the analysis of the rectangular aperture, where use can also be made of the curves in Fig. 10.70.

To observe Fresnel slit diffraction, form a long narrow space between two fingers held at arm's length. Make a similar parallel slit close to your eye, using your other hand. With a *bright* source, such as the daytime sky or a large lamp, illuminating the far slit, observe it through the nearby aperture. After inserting the near slit the far slit will appear to widen, and rows of fringes will be evident.

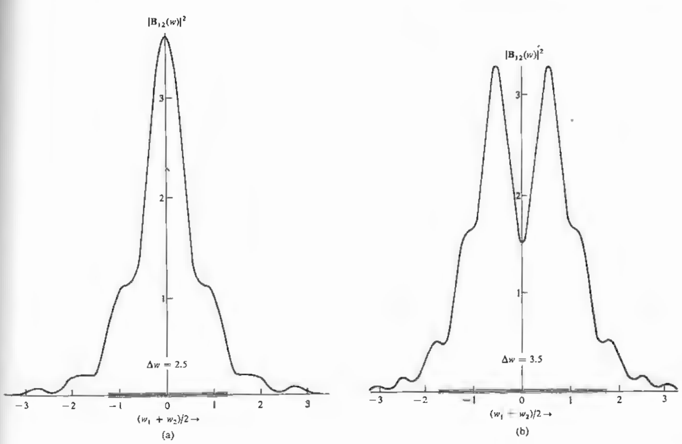


Figure 10.70 $|\mathbf{B}_{12}(w)|^2$ versus $(w_1 + w_2)/2$ for (a) $\Delta w = 2.5$ and (b) $\Delta w = 3.5$.

10.3.9 The Semi-Infinite Opaque Screen

We now form a semi-infinite planar opaque screen by removing the upper half of Σ in Fig. 10.67. This is done simply enough, by letting $z_2 = y_1 = y_2 = \infty$. Remembering the original approximations, we limit the geometry so that the point of observation is close to the screen's edge. Since $v_2 = u_2 = \infty$ and $u_1 = -\infty$, Eq. (10.104) or (10.108) leads to

$$I_p = \frac{I_0}{2}\{[\tfrac{1}{2} - \mathscr{C}(v_1)]^2 + [\tfrac{1}{2} - \mathscr{S}(v_1)]^2\}. \qquad (10.109)$$

When the point P is directly opposite the edge, $v_1 = 0$, $\mathscr{C}(0) = \mathscr{S}(0) = 0$, and $I_p = I_0/4$. This was to be expected, since half the wavefront is obstructed, the amplitude of the disturbance is halved, and the irradiance drops to one quarter. This occurs at point (3) in Figs. 10.71 and 10.72. Moving into the geometric shadow region to point (2) and then on to (1) and still further, the successive chords clearly decrease monotonically (Problem 10.46). No irradiance oscillations exist within that region; the irradiance merely drops off rapidly. At any point above (3) the screen's edge will be below it, in other words, $z_1 < 0$ and $v_1 < 0$. At about $v_1 = -1.2$ the chord reaches a maximum, and the irradiance is a maximum. Thereafter, I_p oscillates about I_0, gradually diminishing in magnitude. With sensitive electronic techniques, many hundreds of these fringes can be observed.*

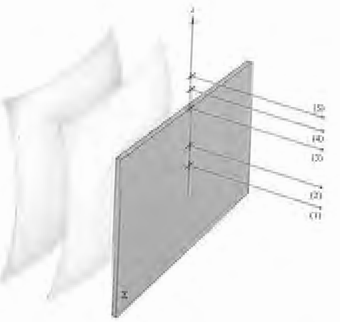


Figure 10.71 The semi-infinite opaque screen.

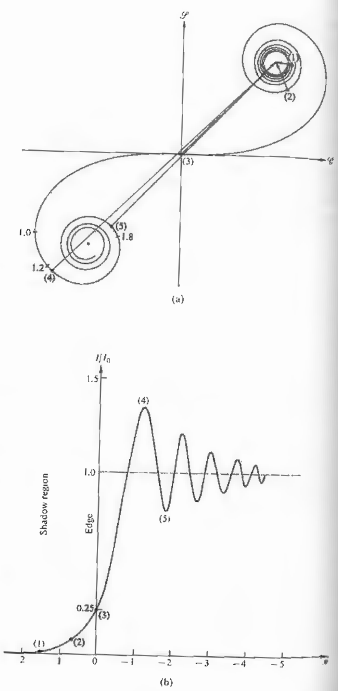


Figure 10.72 (a) The Cornu spiral for a semi-infinite screen. (b) The corresponding irradiance distribution.

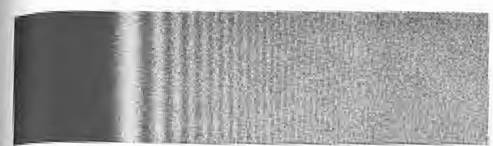


Figure 10.73 The fringe pattern for a half-screen.

It is evident that the diffraction pattern of Fig. 10.73 would appear in the vicinity of the edges of a wide *slit* (Δv greater than about 10) as a limiting case. The irradiance distribution suggested by geometrical optics is obtained only when λ goes to zero. Indeed as λ decreases, the fringes move closer to the edge and become increasingly fine in extent.

The straight-edge pattern can be observed using any kind of slit, held up in front of a broad lamp at arm's length, as a source. Introduce an opaque obstruction (e.g., a blackened microscope slide or a razor blade) very near your eye. As the edge of the obstruction passes in front of the source slit parallel to it, a series of fringes will appear.

10.3.10 Diffraction by a Narrow Obstacle

Refer back to the description of the single narrow slit; consider the complementary case in which the slit is opaque, and the screen transparent. Let's envision, for example, a vertical opaque wire. At a point directly opposite the wire's center there will be two separate contributing regions extending from y_1 to $-\infty$ and from y_2 to $+\infty$. On the Cornu spiral these correspond to two arc lengths from u_1 to B^- and from u_2 to B^+. The amplitude of the disturbance at a point P on the plane of observation is the magnitude of the *vector* sum of the two phasors $\overrightarrow{B^-u_1}$ and $\overrightarrow{u_2B^+}$, illustrated in Fig. 10.74. As with the opaque disk, the symmetry is such that there will always be an illuminated region along the central axis. This can be seen from the spiral, since when P is on the central axis, $\overrightarrow{B^-u_1} = \overrightarrow{u_2B^+}$ and their sum can never be zero. The arc length Δu represents the obscured region of the spiral, which increases as the diameter of the wire increases. For thick wires, u_1 approaches B^-, u_2 approaches B^+, the phasors decrease in length, and the irradiance on the shadow's axis drops off. This is evident in Fig. 10.75, which shows the pat-

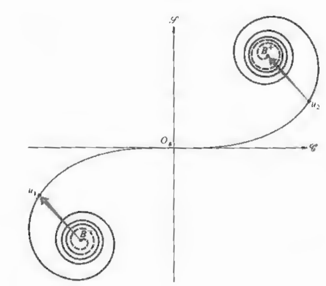
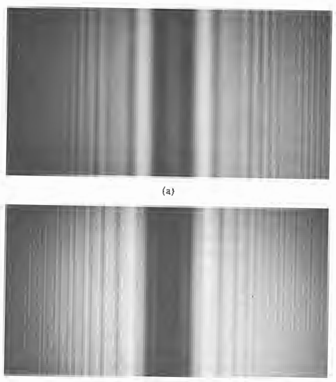


Figure 10.74 The Cornu spiral as applied to a narrow obstacle.

* J. D. Barnett and F. S. Harris, Jr., *J. Opt. Soc. Amer.* **52**, 637 (1962).



(a)

(b)

Figure 10.75 (a) The shadow pattern cast by the lead from a mechanical pencil. (b) The pattern cast by a 1/8-inch diameter rod. (Photos by E. H.)

terns actually cast by a thin piece of lead from a mechanical pencil and by a rod with a $\frac{1}{8}$-inch diameter. Imagine that we have a small irradiance sensor at point P on the plane of observation (or the film plate). As P moves off the central axis to the right, y_1 and u_1 increase negatively, whereas y_2 and u_2, which are positive, decrease. The opaque region, Δu, slides down the spiral. When the sensor is at the right edge of the geometric shadow $y_2 = 0$, $u_2 = 0$, in other words, u_2 is at O_s. Notice that if the wire is thin, that is, if Δu is small, the sensor will record a gradual decrease in irradiance as u_2 approaches O_s. On the other hand, if the wire is thick, Δu is large and u_1 and u_2 are large. As Δu slides down the spiral, the two phasors revolve through a number of complete rotations, going in and out of phase in the process. The resulting additional extrema appearing within the geometric shadow are evident in Fig. 10.75(b). In fact, the separation between inte[illegible] varies inversely with the width of the rod, [illegible] pattern arose from the interference of [illegible] (Young's experiment) reflected at the rod's edges.

10.3.11 Babinet's Principle

Two diffracting screens are said to be com[illegible] when the transparent regions on one exactly [illegible] to the opaque regions on the other and vice [illegible] two such screens are overlapped, the combinati[illegible] is obviously completely opaque. Now then, let E_1 [illegible] E_2 be the scalar optical disturbance arriving at P when either complementary screen Σ_1 or Σ_2, respectively, is in place. The total contribution from each aperture [illegible] determined by integrating over the area bo[illegible] that aperture. If both *apertures* are present at [illegible] are no opaque regions at all; the limits of [illegible] go to infinity, and we have the unobstructed [illegible] E_0, whereupon

$$E_1 + E_2 = E_0, \qquad (10.110)$$

which is the statement of **Babinet's principle**. Take a close look at Figs. 10.69 and 10.74, which depict the Cornu spiral configurations for a transparent slit and a narrow opaque obstacle. If the two arrange[illegible] made complementary, Fig. 10.76 illustrates [illegible]net's principle quite clearly. The phasor arising [illegible] narrow obstacle $(\overline{B^-B_1} + \overline{B_2B^+})$ added to that [illegible] a slit $\overline{B_1B_2}$ yields the unobstructed phasor $\overline{B^-B^+}$.

The principle implies that when $E_0 = 0$, E_1 [illegible] other words, these disturbances are precisely [illegible] magnitude and 180° out of phase. One would [illegible] observe exactly the same irradiance distrib[illegible] either Σ_1 or Σ_2 in place, an interesting result indeed. It is evident, however, that the principle cannot b[illegible] true, since for an unobstructed wave from [illegible] source, there are no zero-amplitude points [illegible] everywhere). Yet if the source is imaged at P [illegible] lenses, as in Fig. 10.9 (with neither Σ_1 nor Σ_2 [illegible] there will be a large, essentially zero-ampli[illegible] beyond the immediate vicinity of P_0 (beyond [illegible] disk) in which $E_1 + E_2 = E_0 = 0$. It is therefore [illegible] for the case of Fraunhofer diffraction that comple[illegible]

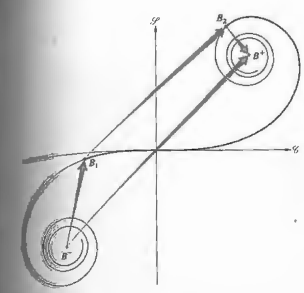


Figure 10.76 The Cornu spiral illustrating Babinet's principle.

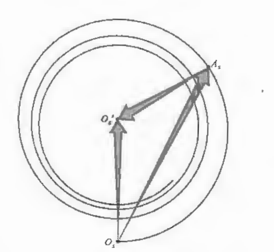


Figure 10.77 The vibration curve illustrating Babinet's principle.

[illegible]eens will generate equivalent irradiance distribu[illegible]ns, that is, $E_1 = -E_2$ (excluding point P_0). Nonetheless, Eq. (10.110) is valid in Fresnel diffraction, even [illegible] the irradiances obey no simple relationship. [illegible] exemplified by the slit and narrow obstacle of [illegible]76. Moreover, for a circular hole and disk, refer back to Figs. 10.52 and 10.58 and then examine Fig. [illegible] Equation (10.110) is again clearly applicable, even [illegible] the diffraction patterns are certainly not [illegible]

[illegible] beauty of Babinet's principle is most evident [illegible]plied to Fraunhofer diffraction, as shown in Fig. 10.78, where the patterns from complementary screens are almost identical.

10.4 [illegible]RCHHOFF'S SCALAR DIFFRACTION THEORY

We have described a number of diffracting configu[illegible]ions, quite satisfactorily, within the context of the [illegible]tively simple Huygens–Fresnel theory. Yet the [illegible]agery of surfaces covered with fictitious point [illegible] which was the basis of that analysis, was merely [illegible]ed rather than derived from fundamental principles. The Kirchhoff treatment shows that these results are actually derivable from the *scalar* differential wave equation.

The discussion to follow is rather formal and involved. Portions of it have therefore been relegated to an appendix, where we can indulge in succinctness and risk sacrificing readability for rigor.

In the past, when dealing with a distribution of monochromatic point sources, we computed the resultant optical disturbance at point P (i.e., E_p) by carrying out a superposition of the individual waves. There is, however, a completely different approach, which is founded in potential theory. Here one is concerned not with the sources themselves but rather with the scalar optical disturbance and its derivatives over an arbitrary closed surface surrounding P. We assume that a Fourier analysis can separate the constituent frequencies, so that we need only deal with one such frequency at a time. The monochromatic optical disturbance E is a solution of the differential wave equation

$$\nabla^2 E = \frac{1}{c^2}\frac{\partial^2 E}{\partial t^2}. \qquad (10.111)$$

Without specifying the precise spatial nature of the

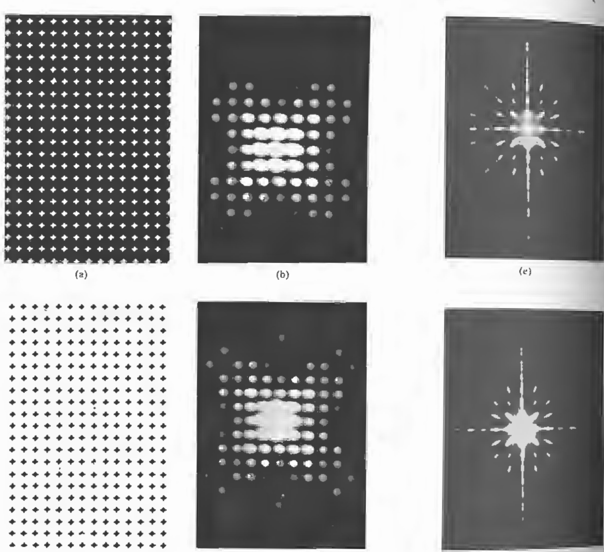


Figure 10.78 (a)–(d) White-light diffraction patterns for regular arrays of apertures and complementary obstacles in the form of rounded plus signs. (e) and (f) Diffraction patterns for a regular array of rectangular apertures and obstacles, respectively. (Photos courtesy The Ealing Corporation and Richard B. Hoover.)

[illegible] write it as

$$E = \mathscr{E}e^{-ikct}. \tag{10.112}$$

Here [illegible] represents the complex space part of the disturbance. Substituting this into the wave equation, we [illegible]

$$\nabla^2\mathscr{E} + k^2\mathscr{E} = 0. \tag{10.113}$$

[illegible] known as the *Helmholtz equation* and is solved, [illegible] the aid of Green's theorem, in Appendix 2. The [illegible] disturbance existing at a point P, expressed in [illegible] of the optical disturbance and its gradient evaluated on an arbitrary closed surface S, enclosing P, is

$$\mathscr{E}_p = \frac{1}{4\pi}\left[\iint_S \frac{e^{ikr}}{r}\nabla\mathscr{E}\cdot d\mathbf{S} - \iint_S \mathscr{E}\nabla\left(\frac{e^{ikr}}{r}\right)\cdot d\mathbf{S}\right]. \tag{10.114}$$

[illegible] as the *Kirchhoff integral theorem*, Eq. (10.114) [illegible] the geometric configuration illustrated in Fig. [illegible]

[illegible] apply the theorem to the specific instance of an unobstructed spherical wave originating at a point source s, as shown in Fig. 10.80. The disturbance has the form

$$E(\rho, t) = \frac{\mathcal{E}_0}{\rho}e^{i(k\rho-\omega t)}, \tag{10.115}$$

in which case

$$\mathscr{E}(\boldsymbol{\rho}) = \frac{\mathcal{E}_0}{\rho}e^{ik\rho}. \tag{10.116}$$

If we substitute this into Eq. (10.114), it becomes

$$\mathscr{E}_p = \frac{1}{4\pi}\left[\oint\!\!\!\oint_S \frac{e^{ikr}}{r}\frac{\partial}{\partial\rho}\left(\frac{\mathcal{E}_0}{\rho}e^{ik\rho}\right)\cos(\hat{\mathbf{n}},\hat{\boldsymbol{\rho}})\,dS - \oint\!\!\!\oint_S \frac{\mathcal{E}_0}{\rho}e^{-ik\rho}\frac{\partial}{\partial r}\left(\frac{e^{ikr}}{r}\right)\cos(\hat{\mathbf{n}},\hat{\mathbf{r}})\,dS\right],$$

where $d\mathbf{S} = \hat{\mathbf{n}}\,dS$, $\hat{\mathbf{n}}$, $\hat{\mathbf{r}}$ and $\hat{\boldsymbol{\rho}}$ are unit vectors,

$$\nabla\left(\frac{e^{ikr}}{r}\right) = \hat{\mathbf{r}}\frac{\partial}{\partial r}\left(\frac{e^{ikr}}{r}\right),$$

and

$$\nabla\mathscr{E}(\boldsymbol{\rho}) = \hat{\boldsymbol{\rho}}\,\partial\mathscr{E}/\partial\rho.$$

The differentiations under the integral signs are

$$\frac{\partial}{\partial\rho}\left(\frac{e^{ik\rho}}{\rho}\right) = e^{ik\rho}\left(\frac{ik}{\rho} - \frac{1}{\rho^2}\right)$$

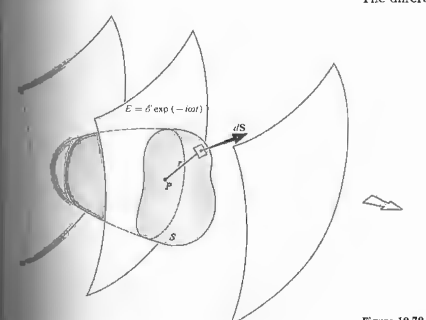
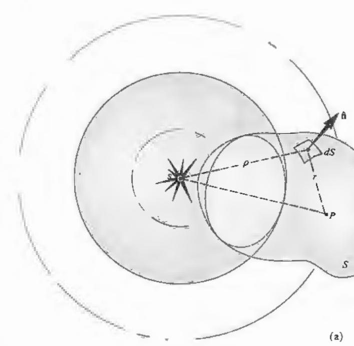


Figure 10.79 An arbitrary closed surface S enclosing point P.



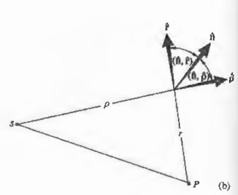


Figure 10.80 A spherical wave emitted from point

and

$$\frac{\partial}{\partial r}\left(\frac{e^{ikr}}{r}\right) = e^{ikr}\left(\frac{ik}{r} - \frac{1}{r^2}\right).$$

When $\rho \gg \lambda$ and $r \gg \lambda$ the $1/\rho^2$ and $1/r^2$ terms can be neglected. This approximation is fine in the optical spectrum but certainly need not be true for microwaves. Proceeding, we write

$$\mathscr{E}_p = -\frac{\mathcal{E}_0 i}{\lambda} \oiint_S \frac{e^{ik(\rho+r)}}{\rho r}\left[\frac{\cos(\hat{\mathbf{n}}, \hat{\mathbf{r}}) - \cos(\hat{\mathbf{n}}, \hat{\boldsymbol{\rho}})}{2}\right] dS, \tag{10.117}$$

which is known as the *Fresnel–Kirchhoff diffraction formula.*

Take a long look at Eq. (10.96), which represents the disturbance at P arising from an element dS in the Huygens–Fresnel theory, and compare it with Eq. (10.117). In Eq. (10.117) the angular dependence is contained in the single term $\frac{1}{2}[\cos(\hat{\mathbf{n}}, \hat{\mathbf{r}}) - \cos(\hat{\mathbf{n}}, \hat{\boldsymbol{\rho}})]$, which we shall call the obliquity factor $K(\theta)$, showing it to be equivalent to Eq. (10.72) later on. Notice as well that k can be replaced by $-k$ everywhere, since we certainly could have chosen the phase of Eq. (10.116) to have been $(\omega t - k\rho)$. Now multiply both sides of Eq. (10.117) by $\exp(-i\omega t)$; the differential element is then

$$dE_p = \frac{K(\theta)\mathcal{E}_0}{\rho r \lambda}\cos[k(\rho + r) - \omega t - \pi/2]\, dS. \tag{10.118}$$

This is the contribution to E_p arising from an element of surface area dS a distance r from P. The $\pi/2$ term in the phase results from the fact that $-i = \exp(-i\pi/2)$. The Kirchhoff formulation therefore leads to the same total result, with the exception that it includes the correct $\pi/2$ phase shift, which is lacking in the Huygens–Fresnel treatment (10.96).

We have yet to ensure that the surface S can be made to correspond to the unobstructed portion of the wavefront, as it does in the Huygens–Fresnel theory. For the case of a freely propagating spherical wave emanating from the point source s, we construct the doubly connected region shown in Fig. 10.81. The surface S_2 completely surrounds the small spherical surface S_1. At $\rho = 0$ the disturbance $E(\rho, t)$ has a singularity and is therefore properly excluded from the volume V between S_1 and S_2. The integral must now include both surfaces S_1 and S_2. But we can have S_2 increase outward indefinitely by requiring its radius to go to infinity. In that case, the contribution to the surface integral vanishes. (This is true whatever the form of the incoming disturbance, as long as it drops off at least as rapidly as a spherical wave.) The remaining surface S_1 is a sphere centered at the point source. Since, over S_1, $\hat{\mathbf{n}}$ and $\hat{\boldsymbol{\rho}}$ are anti-parallel, it is evident from Fig. 10.80(b) that the angles $(\hat{\mathbf{n}}, \hat{\mathbf{r}})$ and $(\hat{\mathbf{n}}, \hat{\boldsymbol{\rho}})$ are θ and 180°, respectively. The obliquity factor then becomes

$$K(\theta) = \frac{\cos\theta + 1}{2},$$

which is Eq. (10.72). Clearly, since the surface of integration S_1 is centered at s, it does indeed correspond to the spherical wavefront at some instant. *The Huygens–Fresnel principle is therefore directly traceable to the scalar differential wave equation.*

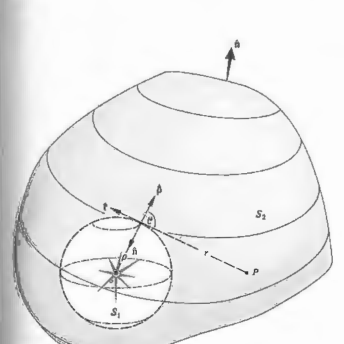


Figure 10.81 A doubly connected region surrounding point s.

We shan't pursue the Kirchhoff formulation any farther, other than to point out briefly how it is applied to diffracting screens. The single closed surface of integration surrounding the point of observation P is generally taken to be the entire screen Σ capped by an infinite hemisphere. There are then three distinct areas with which to be concerned. The contribution to the integral from the region of the infinite hemisphere is zero. Moreover, it is assumed that there is no disturbance immediately behind the opaque screen, so that this second region contributes nothing. The disturbance at P is therefore determined solely by the contributions arising from the aperture, and one need only integrate Eq. (10.117) over that area.

The fine results obtained by using the Huygens–Fresnel principle are now justified theoretically, the main limitations being that $\rho \gg \lambda$ and $r \gg \lambda$.

10.5 BOUNDARY DIFFRACTION WAVES

In Section 10.1.1 we said that the diffracted wave could be envisioned as arising from a fictitious distribution of secondary emitters spread across the unobstructed portion of the wavefront, namely, the Huygens–Fresnel principle. There is, however, another, completely different, and rather appealing possibility. Suppose that an incoming wave sets the electrons on the rear of the diffracting screen Σ into oscillation, and these in turn radiate. We anticipate a twofold effect. First, all the oscillators that are remote from the edge of the aperture radiate back toward the source in such a fashion as to cancel the incoming wave at all points, except within the projection of the aperture itself. In other words, if this were the only contributing mechanism, a perfect geometrical image of the aperture would appear on the plane of observation. There is, however, an additional contribution arising from those oscillators in the vicinity of the aperture's edge. A portion of the energy radiated by these secondary sources propagates in the forward direction. The superposition of this scattered wave (known as the *boundary diffraction wave*) and the unobstructed portion of the primary wave (known as the *geometrical wave*) yields the diffraction pattern. A rather cogent reason for contemplating such a scheme becomes apparent when one examines the following arrangement. Tear a small hole ($\approx\frac{1}{2}$ cm in diameter) of arbitrary shape in a piece of paper, and holding it at arm's length, view an ordinary light bulb some meters distant. Even with your eye in the shadow region, the edges of the aperture will be brightly illuminated. The ripple-tank photograph in Fig. 10.82 also illustrates the process. Notice how each edge of the slit seems to serve as a center for a circular disturbance, which then propagates beyond the aperture. There are no electron-oscillators here, which implies that these ideas have a certain generality, being applicable to elastic waves as well.

The formulation of diffraction in terms of the interference of a scattered edge wave and a geometrical wave is perhaps more physically appealing than the fictitious emitters of the Huygens–Fresnel principle. It is not, however, a new concept. Indeed it was first propounded by the ubiquitous Thomas Young even before Fresnel's

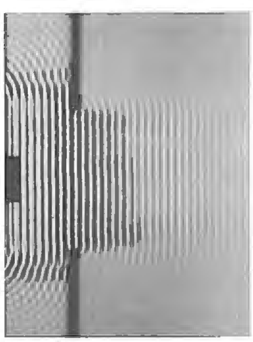


Figure 10.82 Ripple-tank waves passing through a slit. (Photo courtesy PSSC *Physics*, D. C. Heath, Boston, 1960.)

celebrated memoir on diffraction. But in time [illegible] brilliant successes unfortunately convinced [illegible] reject his own ideas, and he finally did so in [illegible] Fresnel in 1818. Strengthened by Kirchhoff's [illegible] Fresnel conception of diffraction became [illegible] accepted and has persisted (right up to Sectio[illegible] The resurrection of Young's theory began in [illegible] that time, Gian Antonio Maggi proved that Ki[illegible] analysis, for a point source at least, was equi[illegible] two contributing terms. One of these was a ge[illegible] wave, but the other, unhappily, was an integ[illegible] allowed no clear physical interpretation at th[illegible] his doctoral thesis (1893) Eugen Maey showe[illegible] edge wave could indeed be extracted from a[illegible] Kirchhoff formulation for a semi-infinite half-pla[illegible] Arnold Sommerfeld's rigorous solution of the half-plane problem (see Section 10.1) showed that [illegible] cylindrical wave actually does proceed from the screen's edge. It propagates into both the geometrical shadow region and the illuminated region. In the latter the boundary diffraction wave combines with the geometrical wave, in complete accord with Young's theory. In 1917 Adalbert (Wojciech) Rubinowicz was able to prove that Kirchhoff's formula for a plane or spherical wave can be appropriately decompo[illegible] the two desired waves, thereby revealing the [illegible] rectness of Young's ideas. He also later establi[illegible] the boundary diffraction wave, to a first approximation, was generated by reflection of the primary [illegible] from the aperture's edge. In 1923 Friedrich Kottle[illegible] pointed out the equivalence of the solutions of [illegible] Rubinowicz, and one now speaks of the Yo[illegible] Rubinowicz theory. Most recently, Kenro M[illegible] Emil Wolf (1962) have extended the boun[illegible] tion theory to the case of arbitrary inciden[illegible] very useful contemporary approach to the prob[illegible] been devised by Joseph B. Keller. He has deve[illegible] geometric theory of diffraction that is closely re[illegible] Young's edge wave picture. Along with the usual rays of geometrical optics, he hypothesizes the existence of diffracted rays. Rules governing these diff[illegible] rays, which are analogous to the laws of reflectio[illegible] tion, are employed to determine the resu[illegible]

* A fairly complete bibliography can be found in the article by [illegible] Rubinowicz in *Progress in Optics*, Vol. 4, p. 199.

PROBLEMS

10.1 A point source S is a perpendicular distance R from the center of a circular hole of radius a in [illegible]que screen. If the distance to the periphery is [illegible] show that Fraunhofer diffraction will occur on [illegible]stant screen when

$$\lambda R \gg a^2/2.$$

[illegible] smallest satisfactory value of R if the hole [illegible] radius of 1 mm, $\ell \le \lambda/10$, and $\lambda = 500$ nm?

10.2 [illegible]ing Fig. 10.83, derive the irradiance equation [illegible] oscillators, Eq. (10.5).

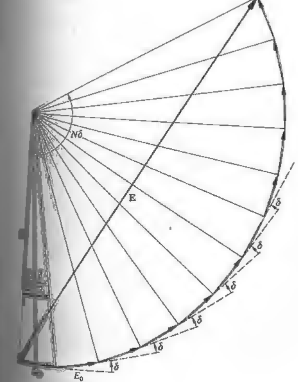


Figure 10.83

10.3* In Section 10.1.3 we talked about introducing an intrinsic phase shift ε between oscillators in a linear array. With this in mind show that Eq. (10.18) becomes

$$\beta = (kb/2)(\sin\theta - \sin\theta_i)$$

when the incident plane wave makes an angle θ_i with the plane of the slit.

10.4 Referring back to the multiple antenna system of Fig. 10.7, compute the angular separation between successive lobes or principal maxima and the width of the central maximum.

10.5 Examine the setup of Fig. 10.5 in order to determine what is happening in the image space of the lenses; in other words, locate the exit pupil and relate it to the diffraction process. Show that the configurations in Fig. 10.84 are equivalent to that of Fig. 10.5 and will therefore result in Fraunhofer diffraction. Design at least one more such arrangement.

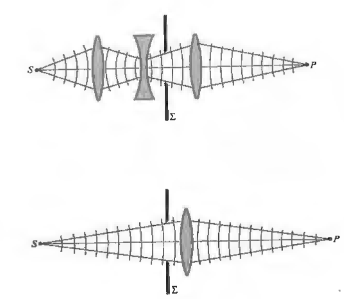


Figure 10.84

10.6 The angular distance between the center and the first minimum of a single-slit Fraunhofer diffraction pattern is called the *half-angular breadth;* write an expression for it. Find the corresponding *half-linear width* (a) when no focusing lens is present and the slit-viewing screen distance is L, and (b) when a lens of focal length f_2 is very close to the aperture. Notice that the half-linear width is also the distance between the successive minima.

10.7* A single slit in an opaque screen 0.10 mm wide is illuminated (in air) by plane waves from a krypton ion laser ($\lambda_0 = 461.9$ nm). If the observing screen is 1.0 m away, determine whether or not the resulting diffraction pattern will be of the far-field variety and then compute the angular width of the central maximum.

10.8* A narrow single slit (in air) in an opaque screen is illuminated by infrared from a He-Ne laser at 1152.2 nm, and it is found that the center of the tenth dark band in the Fraunhofer pattern lies at an angle of 6.2° off the central axis. Please determine the width of the slit. At what angle will the tenth minimum appear if the entire arrangement is immersed in water (n_w = 1.33) rather than air (n_a = 1.00029)?

10.9 A collimated beam of microwaves impinges on a metal screen that contains a long horizontal slit that is 20 cm wide. A detector moving parallel to the screen in the far-field region locates the first minimum of irradiance at an angle of 36.87° above the central axis. Determine the wavelength of the radiation.

10.10 Show that for a double-slit Fraunhofer pattern, if $a = mb$, the number of bright fringes (or parts thereof) within the central diffraction maximum will be equal to $2m$.

10.11* Two long slits 0.10 mm wide, separated by 0.20 mm, in an opaque screen are illuminated by light with a wavelength of 500 nm. If the plane of observation is 2.5 m away, will the pattern correspond to Fraunhofer or Fresnel diffraction? How many Young's [illegible] be seen within the central bright band?

10.12 What is the relative irradiance of the [illegible] maxima in a three-slit Fraunhofer diffraction [illegible] Draw a graph of the irradiance distribution [illegible] $2b$, for two and then three slits.

10.13* Starting with the irradiance expression for a finite slit, shrink the slit down to [illegible] area element and show that it emits equally [illegible] tions.

10.14* Show that Fraunhofer diffraction [illegible] have a center of symmetry [i.e., $I(Y, Z) = I(-Y, -Z)$], regardless of the configuration of the aperture, [illegible] as there are no phase variations in the field over the region of the hole. Begin with Eq. (10.41). We'll see later (Chapter 11) that this restriction is equivalent to saying that the aperture function is real.

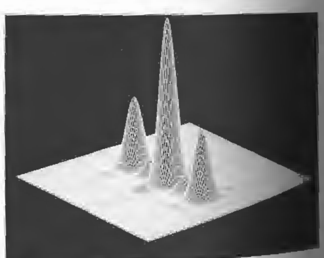
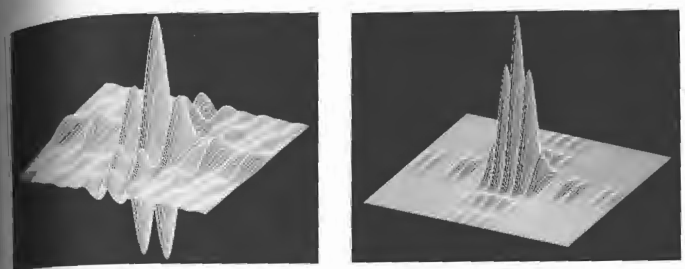


Fig. 10.85 Photo courtesy R. G. Wilson, Illinois Wesleyan [illegible]



[illegible] Photos courtesy R. G. Wilson, Illinois Wesleyan University.

10.15 With the results of Problem 10.14 in mind, [illegible] the symmetries that would be evident in the [illegible]nhofer diffraction pattern of an aperture that is [illegible] symmetrical about a line (assuming normally [illegible] quasimonochromatic plane waves).

10.16 From symmetry considerations, create a rough sketch of the Fraunhofer diffraction patterns of an [illegible] triangular aperture and an aperture in the [illegible] a plus sign.

[illegible]gure 10.85 is the irradiance distribution in [illegible] for a configuration of elongated rectangular [illegible] Describe the arrangement of holes that would [illegible] such a pattern and give your reasoning in [illegible]

[illegible] Fig. 10.86 (a) and (b) are the electric field [illegible]nce distributions, respectively, in the far field [illegible]guration of elongated rectangular apertures. [illegible] arrangement of holes that would give rise [illegible]terns and discuss your reasoning.

10.19 Figure 10.87 is a computer-generated Fraunhofer irradiance distribution. Describe the aperture that would give rise to such a pattern and give your reasoning in detail.

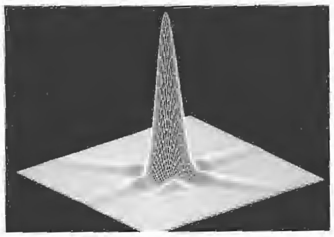
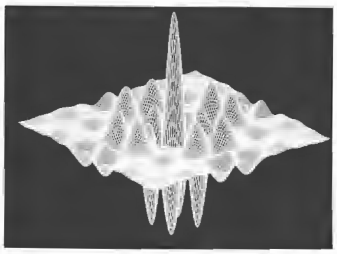


Figure 10.87 Photo courtesy R. G. Wilson, Illinois Wesleyan University.



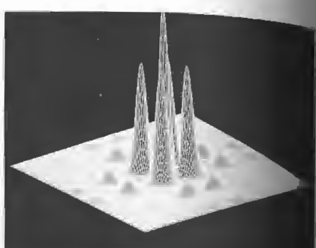


Figure 10.88 Photos courtesy R. G. Wilson, Illinois Wesleyan University.

10.20 In Fig. 10.88 (a) and (b) are the electric field and irradiance distributions, respectively, in the far field for a hole of some sort in an opaque screen. Describe the aperture that would give rise to such a pattern and give your reasoning in detail.

10.21 In light of the five previous questions, identify Fig. 10.89, explaining what it is and what aperture gave rise to it.

10.22* Verify that the peak irradiance I_1 of the first "ring" in the Airy pattern for far-field diffraction at a circular aperture is such that $I_1/I(0) = 0.0175$. You might want to use the fact that

$$J_1(u) = \frac{u}{2}\left[1 - \frac{1}{1!2!}(\tfrac{1}{2}u)^2 + \frac{1}{2!3!}(\tfrac{1}{2}u)^4 - \frac{1}{3!4!}(\tfrac{1}{2}u)^6 + \cdots\right].$$

10.23 No lens can focus light down to a perfect point, because there will always be some diffraction. Estimate the size of the minimum spot of light that can be expected at the focus of a lens. Discuss the relationship among the focal length, the lens diameter, and the spot size. Take the *f-number* of the lens to be roughly 0.8 or 0.9, which is just about what you can expect for the fastest lens.

10.24 Figure 10.90 shows several apertu[re] confi[gu]rations. Roughly sketch the Fraunhofer patterns [for] each. Note that the circular regions should generate Airy-like ring systems centered at the origin.

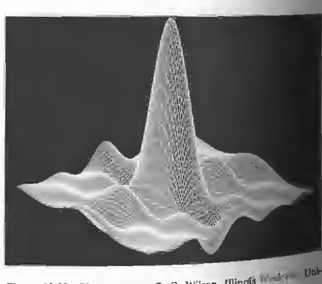


Figure 10.89 Photo courtesy R. G. Wilson, Illinois Wesleyan University.

...uppose that we have a laser emitting a diffrac-...d beam ($\lambda_0 = 632.84$ nm) with a 2-mm ... How big a light spot would be produced on ...e of the Moon a distance of 376×10^3 km away ... a device? Neglect any effects of the Earth's ...sphere.

...f you peered through a 0.75-mm hole at an ... you would probably notice a decrease in visual ... ompute the angular limit of resolution, assum-... it's determined only by diffraction; take $\lambda_0 =$ ... Compare your results with the value of $1.7 \times$ ... which corresponds to a 4.0-mm pupil.

10.27 The neoimpressionist painter Georges Seurat ... member of the pointillist school. His paintings ... of an enormous number of closely spaced small ... inch) of pure pigment. The illusion of color ... produced only in the eye of the observer. ... from such a painting should one stand in order ... e the desired blending of color?

L▲2ZS5

10.28* The Mount Palomar telescope has an objective ... with a 508-cm diameter. Determine its angular ... resolution at a wavelength of 550 nm, in radians, ... and seconds of arc. How far apart must two ... the surface of the Moon if they are to be ... able by the Palomar telescope? The Earth–Moon ... ce is 3.844×10^8 m; take $\lambda_0 = 550$ nm. How far ... must two objects be on the Moon if they are to ... tinguished by the eye? Assume a pupil diameter ... 00 mm.

A transmission grating whose lines are sepa-... 3.0×10^{-6} m is illuminated by a narrow beam ... ht ($\lambda_0 = 694.3$ nm) from a ruby laser. Spots of ... d light, on both sides of the undeflected beam, ... a screen 2.0 m away. How far from the central ... h of the two nearest spots?

10.30* A diffraction grating with slits 0.60×10^{-3} cm apart is illuminated by light with a wavelength of 500 nm. At what angle will the third-order maximum appear?

10.31* A diffraction grating produces a second-order spectrum of yellow light ($\lambda_0 = 550$ nm) at 25°. Determine the spacing between the lines on the grating.

10.32 White light falls normally on a transmission grating that contains 1000 lines per centimeter. At what angle will red light ($\lambda_0 = 650$ nm) emerge in the first-order spectrum?

10.33* Light from a laboratory sodium lamp has two strong yellow components at 589.5923 nm and 588.9953 nm. How far apart in the first-order spectrum will these two lines be on a screen 1.00 m from a grating having 10,000 lines per centimeter?

10.34* Sunlight impinges on a transmission grating that is formed with 5000 lines per centimeter. Does the third-order spectrum overlap the second-order spectrum? Take red to be 780 nm and violet to be 390 nm.

10.35 Light having a frequency of 4.0×10^{14} Hz is incident on a grating formed with 10,000 lines per centimeter. What is the highest-order spectrum that can be seen with this device? Explain.

10.36* Suppose that a grating spectrometer while in vacuum on Earth sends 500-nm light off at an angle of 20.0° in the first-order spectrum. By comparison, after landing on the planet Mongo, the same light is diffracted through 18.0°. Determine the index of refraction of the Mongoian atmosphere.

10.37 Prove that the equation

$$a(\sin\theta_m - \sin\theta_i) = m\lambda, \qquad [10.61]$$

when applied to a transmission grating, is independent of the refractive index.

10.38 A high-resolution grating 260 mm wide, with 300 lines per millimeter, at about 75° in autocollimation has a resolving power of just about 10^6 for $\lambda = 500$ nm. Find its free spectral range. How do these values of $\mathcal{R}$ and $(\Delta\lambda)_{fsr}$ compare with those of a Fabry–Perot etalon having a 1-cm air gap and a finesse of 25?

10.39 What is the total number of lines a grating must have in order just to separate the sodium doublet ($\lambda_1 = 5895.9$ Å, $\lambda_2 = 5890.0$ Å) in the third order?

10.40* Imagine an opaque screen containing 30 randomly located circular holes. The light source is such that every aperture is coherently illuminated by its own plane wave. Each wave in turn is completely incoherent with respect to all the others. Describe the resulting far-field diffraction pattern.

10.41 Imagine that you are looking through a piece of square woven cloth at a point source ($\lambda_0 = 600$ nm) 20 m away. If you see a square arrangement of bright spots located about the point source (Fig. 10.91), each separated by an apparent nearest-neighbor distance of 12 cm, how close together are the strands of cloth?

10.42* Perform the necessary mathematical operations needed to arrive at Eq. (10.76).

Figure 10.91 Photo by E.H.

10.43 Referring to Fig. 10.48, integrate the [illegible] $dS = 2\pi\rho^2 \sin\varphi\, d\varphi$ over the lth zone to get th[illegible] that zone,

$$A_l = \frac{\lambda\pi\rho}{\rho + r_0}\left[r_0 + \frac{(2l-1)\lambda}{4}\right].$$

Show that the mean distance to the lth zone is

$$r_l = r_0 + \frac{(2l-1)\lambda}{4},$$

so that the ratio A_l/r_l is constant.

10.44* Derive Eq. (10.84).

10.45 Use the Cornu spiral to make a rough sk[illegible] of $|\mathbf{B}_{12}(w)|^2$ versus $(w_1 + w_2)/2$ for $\Delta w = 5.5$. Com[illegible] your results with those of Fig. 10.70.

10.46 The Fresnel integrals have the asympt[illegible] (corresponding to large values of w) given by

$$\mathscr{C}(w) \approx \tfrac{1}{2} + \left(\frac{1}{\pi w}\right)\sin\left(\frac{\pi w^2}{2}\right),$$

$$\mathscr{S}(w) \approx \tfrac{1}{2} - \left(\frac{1}{\pi w}\right)\cos\left(\frac{\pi w^2}{2}\right).$$

Using this fact, show that the irradiance in the sha[illegible] of a semi-infinite opaque screen decreases in [illegible] to the inverse square of the distance to the edg[illegible] and therefore v_1 become large.

10.47 What would you expect to see on the [illegible] observation if the half-plane Σ in Fig. 10.71 [illegible] transparent?

10.48 Plane waves from a collimated He–Ne laser beam ($\lambda_0 = 632.8$ nm) impinge on a steel rod [illegible] 2.5-mm diameter. Draw a rough *graphic* repre[illegible] of the diffraction pattern that would be seen o[illegible] 3.16 m from the rod.

10.49 Make a rough sketch of the irradiance [illegible] for a Fresnel diffraction pattern arising from a [illegible] slit. What would the Cornu spiral picture look like at point P_0?

[illegible]0* Make a rough sketch of a possible Fresnel [illegible]action pattern arising from each of the indicated apertures (Fig. 10.92).

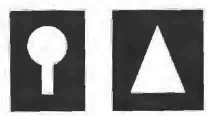


Figure 10.92

[illegible] Suppose the slit in Fig. 10.67 is made very [illegible] What will the Fresnel diffraction pattern look like?

10.52* Collimated light from a krypton ion laser at [illegible] nm impinges normally on a circular aperture. [illegible] viewed axially from a distance of 1.00 m, the hole uncovers the first half-period zone. Determine its diameter.

10.53* Plane waves impinge perpendicularly on a screen with a small circular hole in it. If is found that when viewed from some axial point P the hole uncovers $\frac{1}{2}$ of the first half-period zone. What is the irradiance at P in terms of the irradiance there when the screen is removed?

10.54* A collimated beam from a ruby laser (694.3 nm) having an irradiance of 10 W/m² is incident perpendicularly on an opaque screen containing a square hole 5.0 mm on a side. Compute the irradiance at a point on the central axis 250 cm from the aperture.

10.55* A long narrow slit 0.10 mm wide is illuminated by light of wavelength 500 nm coming from a point source 0.90 m away. Determine the irradiance at a point 2.0 m beyond the screen when the slit is centered on, and perpendicular to, the line from the source to the point of observation. Write your answer in terms of the unobstructed irradiance.

11 FOURIER OPTICS

11.1 INTRODUCTION

In what is to follow we will extend the discussion of Fourier methods introduced in Chapter 7. It is our intent to provide a strong basic introduction to the subject rather than a complete treatment. Besides its real mathematical power, Fourier analysis leads to a marvelous way of treating optical processes in terms of spatial frequencies.* It is always exciting to discover a new bag of analytic toys, but it's perhaps even more valuable to unfold yet another way of thinking about a broad range of physical problems—we shall do both.†

The primary motivation here is to develop an understanding of the way optical systems process light to form images. In the end we want to know all about the amplitudes and phases of the lightwaves reaching the image plane. Fourier methods are especially suited to that task, so we first extend the treatment of Fourier transforms begun earlier. Several transforms are particularly useful in the analysis and these will be considered first. Among them is the delta function, which will subsequently be used to represent a point source of light. How an optical system responds to [illegible] comprising a large number of delta-function [illegible] ces will be considered in Section 11.3.1. The [illegible] between Fourier analysis and Fraunhofer di[illegible] explored throughout the discussion, but sp[illegible] tion is given it in Section 11.3.3. The chapter end[illegible] a return to the problem of image evaluation, [illegible] from a different, though related, perspective [illegible] is treated not as a collection of point sour[illegible] scatterer of plane waves.

11.2 FOURIER TRANSFORMS

11.2.1 One-Dimensional Transforms

It was seen in Section 7.8 that a one-dimen[illegible] func- tion of some space variable $f(x)$ could be expre[illegible] a linear combination of an infinite number of ha[illegible] contributions:

$$f(x) = \frac{1}{\pi}\left[\int_0^\infty A(k)\cos kx\, dk + \int_0^\infty B(k)\sin kx\, dk\right]. \quad [illegible]$$

The weighting factors that determine the signifi[illegible] of the various angular spatial frequency (k) co[illegible] tions, that is, $A(k)$ and $B(k)$, are the *Fourier cos*[illegible] *sine transforms of* $f(x)$ given by

$$A(k) = \int_{-\infty}^{+\infty} f(x')\cos kx'\, dx'$$

* See Chapter 14 for a further nonmathematical discussion.

† As general references for this chapter, see R. C. Jennison, *Fourier Transforms and Convolutions for the Experimentalist*; N. F. Barber, *Experimental Correlograms and Fourier Transforms*; A. Papoulis, *Systems and Transforms with Applications in Optics*; J. W. Goodman, *Introduction to Fourier Optics*; *Linear Systems, Fourier Transforms, and Optics*, J. Gaskill; and the excellent series of booklets *Images and Information*, B. W. Jones, et al.

and

$$B(k) = \int_{-\infty}^{+\infty} f(x')\sin kx'\, dx', \quad [7.57]$$

[illegible]ely. Here the quantity x' is a dummy variable [illegible]ich the integration is carried out, so that neither [illegible] nor $B(k)$ is an explicit function of x', and the [illegible] of symbol used to denote it is irrelevant. The [illegible]and cosine transforms can be consolidated into a [illegible]e complex exponential expression as follows: sub- [illegible]ing Eq. (7.57) into Eq. (7.56), we obtain

$$f(x) = \frac{1}{\pi}\int_0^\infty \cos kx \int_{-\infty}^{+\infty} f(x')\cos kx'\, dx'\, dk$$
$$+ \frac{1}{\pi}\int_0^\infty \sin kx \int_{-\infty}^{+\infty} f(x')\sin kx'\, dx'\, dk.$$

But since $\cos k(x' - x) = \cos kx \cos kx' + \sin kx \sin kx'$, [illegible] can be rewritten as

$$f(x) = \frac{1}{\pi}\int_0^\infty \left[\int_{-\infty}^{+\infty} f(x')\cos k(x' - x)\, dx'\right] dk. \quad (11.1)$$

[illegible]uantity in the square brackets is an even function [illegible]and therefore changing the limits on the outer [illegible]gral leads to

$$f(x) = \frac{1}{2\pi}\int_{-\infty}^{+\infty}\left[\int_{-\infty}^{+\infty} f(x')\cos k(x' - x)\, dx'\right] dk. \quad (11.2)$$

[illegible] as we are looking for an exponential rep- [illegible]tation, Euler's theorem comes to mind. Con- [illegible]ently, observe that

$$\frac{i}{2\pi}\int_{-\infty}^{+\infty}\left[\int_{-\infty}^{+\infty} f(x')\sin k(x' - x)\, dx'\right] dk = 0,$$

[illegible] the factor in brackets is an odd function of k. [illegible]ing these last two expressions yields the complex [illegible] of the Fourier integral,

$$f(x) = \frac{1}{2\pi}\int_{-\infty}^{+\infty}\left[\int_{-\infty}^{+\infty} f(x')e^{ikx'}\, dx'\right] e^{-ikx}\, dk. \quad (11.3)$$

[illegible] can write

$$f(x) = \frac{1}{2\pi}\int_{-\infty}^{+\infty} F(k)e^{-ikx}\, dk, \quad (11.4)$$

provided that

$$F(k) = \int_{-\infty}^{+\infty} f(x)e^{ikx}\, dx, \quad (11.5)$$

having set $x' = x$ for Eq. (11.5). The function $F(k)$ is said to be the **Fourier transform** of $f(x)$, which is symbolically denoted by

$$F(k) = \mathscr{F}\{f(x)\}. \quad (11.6)$$

Actually there are several equivalent, slightly different ways of defining the transform that appear in the literature. For example, the signs in the exponentials could be interchanged or the factor of $1/2\pi$ could be split symmetrically between $f(x)$ and $F(k)$; each would then have a coefficient of $1/\sqrt{2\pi}$. Note that $A(k)$ is the real part of $F(k)$, while $B(k)$ is its imaginary part, that is,

$$F(k) = A(k) + iB(k). \quad (11.7a)$$

As was seen in Section 2.4, a complex quantity like this can also be written in terms of a real-valued amplitude, $|F(k)|$, the *amplitude spectrum*, and a real-valued phase, $\phi(k)$, the *phase spectrum:*

$$F(k) = |F(k)|e^{i\phi(k)}, \quad (11.7b)$$

and sometimes this form can be quite useful [see Eq. (11.96)].

Just as $F(k)$ is the transform of $f(x)$, $f(x)$ itself is said to be the **inverse Fourier transform** of $F(k)$, or symbolically

$$f(x) = \mathscr{F}^{-1}\{F(k)\} = \mathscr{F}^{-1}\{\mathscr{F}\{f(x)\}\}, \quad (11.8)$$

and $f(x)$ and $F(k)$ are frequently referred to as a Fourier-transform pair. It's possible to construct the transform and its inverse in an even more symmetrical form in terms of the spatial frequency $\kappa = 1/\lambda = k/2\pi$. Still, in whatever way it's expressed, the transform will not be precisely the same as the inverse transform, because of the minus sign in the exponential. As a result (Problem 11.10), in the present formulation,

$$\mathscr{F}\{F(k)\} = 2\pi f(-x) \quad \text{while} \quad \mathscr{F}^{-1}\{F(k)\} = f(x).$$

This is most often inconsequential, especially for even functions where $f(x) = f(-x)$, so we can expect a good deal of parity between functions and their transforms.

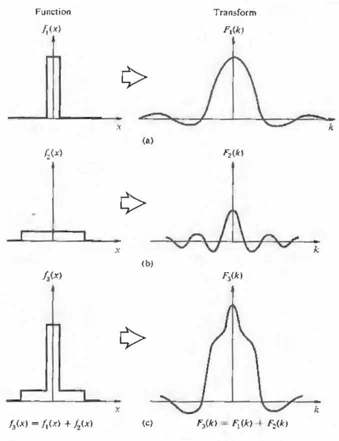


Figure 11.1 A composite function and its Fourier transform.

Obviously, if f were a function of time rather than space, we would merely have to replace x by t and then k, the angular spatial frequency, by ω, the angular temporal frequency, in order to get the appropriate transform pair in the time domain, that is,

$$f(t) = \frac{1}{2\pi}\int_{-\infty}^{+\infty} F(\omega)e^{-i\omega t}\, d\omega \qquad (11.9)$$

and

$$F(\omega) = \int_{-\infty}^{+\infty} f(t)e^{i\omega t}\, dt. \qquad (11.10)$$

It should be mentioned that if we write $f(x)$ as a sum of functions, its transform (11.5) will apparently be the sum of the transforms of the individual [illegible] functions. This can sometimes be quite a [illegible] way of establishing the transforms of complica[illegible] tions that can be constructed from well-k[illegible] stituents. Figure 11.1 makes this procedure fairly self-evident.

i) Transform of the Gaussian Function

As an example of the method, let's examine the Gaussian probability function,

$$f(x) = Ce^{-ax^2}, \qquad (11.11)$$

where $C = \sqrt{a/\pi}$ and a is a constant. If you like, you can imagine this to be the profile of a pulse at $t = 0$. The familiar bell-shaped curve [Fig. 11.2(a)] is quite frequently encountered in optics. It will be pertinent to a diversity of considerations, such as the wave packet representation of individual photons, the cro[illegible] irradiance distribution of a laser beam in the [illegible] mode, and the statistical treatment of thermal [illegible] coherence theory. Its Fourier transform, [illegible] obtained by evaluating

$$F(k) = \int_{-\infty}^{+\infty} (Ce^{-ax^2})e^{ikx}\, dx.$$

On completing the square, the exponent, $-ax^2 + ikx$, becomes $-(x\sqrt{a} - ik/2\sqrt{a})^2 - k^2/4a$, and letting $x\sqrt{a} - ik/2\sqrt{a} = \beta$ yields

$$F(k) = \frac{C}{\sqrt{a}}e^{-k^2/4a}\int_{-\infty}^{+\infty} e^{-\beta^2}\, d\beta.$$

The definite integral can be found in tables and equals $\sqrt{\pi}$; hence

$$F(k) = e^{-k^2/4a}, \qquad (11.12)$$

which is again a Gaussian function [Fig. 11.2(b)], this time with k as the variable. The standard deviation is defined as the range of the variable (x or k) over [illegible] the function drops by a factor of $e^{-1/2} = 0.607$ [illegible] maximum value. Thus the standard deviati[illegible] two curves are $\sigma_x = 1/\sqrt{2a}$ and $\sigma_k = \sqrt{2a}$ a[illegible] As a increases, $f(x)$ becomes narrower while [illegible] $F(k)$ broadens. In other words, the shorter [illegible] length, the broader the spatial frequency band[illegible]

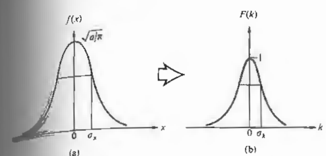


Figure 11.2 A Gaussian and its Fourier transform.

11.2.2 Two-Dimensional Transforms

Thus far the discussion has been limited to one-[illegible]ensional functions, but optics generally involves [illegible]dimensional signals: for example, the field across an aperture or the flux-density distribution over an image plane. The Fourier-transform pair can readily [illegible]eneralized to two dimensions, whereupon

$$f(x, y) = \frac{1}{(2\pi)^2}\iint_{-\infty}^{+\infty} F(k_x, k_y)e^{-i(k_x x + k_y y)}\, dk_x\, dk_y \qquad (11.13)$$

and

$$F(k_x, k_y) = \iint_{-\infty}^{+\infty} f(x, y)e^{i(k_x x + k_y y)}\, dx\, dy. \qquad (11.14)$$

[illegible]antities k_x and k_y are the angular spatial frequen-[illegible]ng the two axes. Suppose we were looking at the [illegible] a tiled floor made up alternately of black and [illegible]quares aligned with their edges parallel to the [illegible]directions. If the floor were infinite in extent, [illegible]hematical distribution of reflected light could [illegible]ded in terms of a two-dimensional Fourier [illegible]ith each tile having a length ℓ, the spatial period [illegible]her axis would be 2ℓ, and the associated funda-[illegible] angular spatial frequencies would equal π/ℓ. [illegible] and their harmonics would certainly be needed to [illegible]onstruct a function describing the scene. If the [illegible] was finite in extent, the function would no [illegible] truly periodic, and the Fourier integral would

have to replace the series. In effect, Eq. (11.13) says that $f(x, y)$ can be constructed out of a linear combination of elementary functions having the form $\exp[-i(k_x x + k_y y)]$, each appropriately weighted in amplitude and phase by a complex factor $F(k_x, k_y)$. The transform simply tells you how much of and with what phase each elementary component must be added to the recipe. In three dimensions, the elementary functions appear as $\exp[-i(k_x x + k_y y + k_z z)]$ or $\exp(-i\mathbf{k}\cdot\mathbf{r})$, which correspond to planar surfaces. Furthermore, if f is a wave function, that is, some sort of three-dimensional wave $f(\mathbf{r}, t)$, these elementary contributions become plane waves that look like $\exp[-i(\mathbf{k}\cdot\mathbf{r} - \omega t)]$. In other words, *the disturbance can be synthesized out of a linear combination of plane waves having various propagation numbers and moving in various directions.* Similarly, in two dimensions the elementary functions are "oriented" in different directions as well. That is to say, for a given set of values of k_x and k_y, the exponent or phase of the elementary functions will be constant along lines

$$k_x x + k_y y = \text{constant} \equiv A$$

or

$$y = -\frac{k_x}{k_y}x + \frac{A}{k_y}. \qquad (11.15)$$

The situation is analogous to one in which a set of planes normal to and intersecting the xy-plane does so along the lines given by Eq. (11.15) for differing values of A.

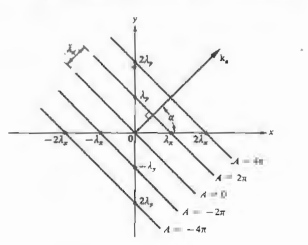


Figure 11.3 Geometry for Eq. (11.15).

A vector perpendicular to the set of lines, call it $\mathbf{k}_\alpha$, would have components k_x and k_y. Figure 11.3 shows several of these lines (for a given k_x and k_y), where $A = 0, \pm 2\pi, \pm 4\pi, \ldots$ The slopes are all equal to $-k_x/k_y$ or $-\lambda_y/\lambda_x$ while the y-intercepts equal $A/k_y = A\lambda_y/2\pi$. The orientation of the constant phase lines is

$$\alpha = \tan^{-1}\frac{k_y}{k_x} = \tan^{-1}\frac{\lambda_x}{\lambda_y} \qquad (11.16)$$

the wavelength, or spatial period λ_α, measured along $\mathbf{k}_\alpha$, is obtained from the similar triangles in the diagram, where $\lambda_\alpha/\lambda_y = \lambda_x/\sqrt{\lambda_x^2+\lambda_y^2}$ and

$$\lambda_\alpha = \frac{1}{\sqrt{\lambda_x^{-2}+\lambda_y^{-2}}} \qquad (11.17)$$

The angular spatial frequency k_α, being $2\pi/\lambda_\alpha$, is then

$$k_\alpha = \sqrt{k_x^2+k_y^2}, \qquad (11.18)$$

as expected. All of this just means that in order to construct a two-dimensional function, harmonic terms in addition to those of spatial frequency k_x and k_y will generally have to be included as well, and these are oriented in directions other than along the x- and y-axes.

Return for a moment to Fig. 10.10, which shows an aperture, with the diffracted wave leaving it represented by several different conceptions. One of these ways to envision the complicated emerging wavefront is as a superposition of plane waves coming off in a whole range of directions. These are the Fourier-transform components, which emerge in specific directions with specific values of angular spatial frequency—the zero spatial frequency term corresponding to the undeviated axial wave, the higher spatial frequency terms coming off at increasingly great angles from the central axis (Section 14.1.1). These Fourier components make up the diffracted field as it emerges from the aperture.

i) Transform of the Cylinder Function

The cylinder function

$$f(x, y) = \begin{cases} 1 & \sqrt{x^2+y^2} \le a \\ 0 & \sqrt{x^2+y^2} > a \end{cases} \qquad (11.19)$$

[Fig. 11.4(a)] provides an important practical example of the application of Fourier methods to two dimensions. The mathematics will not be [illegible] simple, but the relevance of the calculation [illegible] of diffraction by circular apertures and [illegible] justifies the effort. The evident circular sy[illegible] gests polar coordinates, and so let

$$k_x = k_\alpha \cos\alpha$$
$$k_y = k_\alpha \sin\alpha$$
$$x = r\cos\theta \qquad (11.20)$$
$$y = r\sin\theta,$$

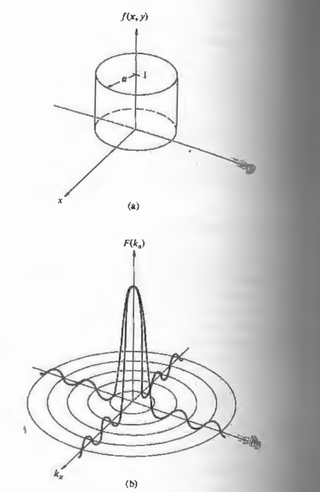


Figure 11.4 The cylinder, or top-hat, function and its transform.

in which case $dx\,dy = r\,dr\,d\theta$. The transform, $\mathscr{F}\{f(x)\}$, then reads

$$\mathscr{F}(k_\alpha, \alpha) = \int_{r=0}^{a}\left[\int_{\theta=0}^{2\pi} e^{ik_\alpha r\cos(\theta-\alpha)}\,d\theta\right] r\,dr. \qquad (11.21)$$

[illegible] as $f(x, y)$ is circularly symmetric, its transform [illegible] symmetrical as well. This implies that $F(k_\alpha, \alpha)$ [illegible]pendent of α. The integral can therefore be [illegible]fied by letting α equal some constant value, which [illegible]oose to be zero, whereupon

$$F(k_\alpha) = \int_0^a\left[\int_0^{2\pi} e^{ik_\alpha r\cos\theta}\,d\theta\right] r\,dr. \qquad (11.22)$$

It follows from Eq. (10.47) that

$$F(k_\alpha) = 2\pi\int_0^a J_0(k_\alpha r)\,r\,dr, \qquad (11.23)$$

[illegible] $J_0(k_\alpha r)$ being a Bessel function of order zero. [illegible]ducing a change of variable, namely, $k_\alpha r = w$, we [illegible] $dr = k_\alpha^{-1}\,dw$, and the integral becomes

$$\frac{1}{k_\alpha^2}\int_{w=0}^{k_\alpha a} J_0(w)\,w\,dw. \qquad (11.24)$$

Using Eq. (10.50), the transform takes the form of a [illegible]-order Bessel function (see Fig. 10.27), that is,

$$F(k_\alpha) = \frac{2\pi}{k_\alpha^2}\,k_\alpha a J_1(k_\alpha a)$$

or

$$F(k_\alpha) = 2\pi a^2\left[\frac{J_1(k_\alpha a)}{k_\alpha a}\right]. \qquad (11.25)$$

The similarity between this expression [Fig. 11.4(b)] [illegible] the formula for the electric field in the Fraunhofer [illegible]fraction pattern of a circular aperture (10.51) is, of course, not accidental.

[illegible]ns as a Fourier Transformer

Figure 11.5 shows a transparency, located in the front [illegible]lane of a converging lens, being illuminated by [illegible] light. This object, in turn, scatters plane waves, [illegible] are collected by the lens, and parallel bundles of [illegible] brought to convergence at its back focal plane.

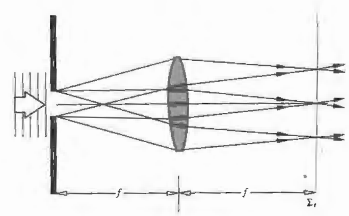


Figure 11.5 The light diffracted by a transparency at the front (or object) focal point of a lens converges to form the far-field diffraction pattern at the back (or image) focal point of the lens.

If a screen were placed there, at Σ_t, the so-called **transform plane**, we would see the far-field diffraction pattern of the object spread across it [this is essentially the configuration of Fig. 10.10(e)]. In other words, the electric field distribution across the object mask, which is known as the *aperture function*, is transformed by the lens into the far-field diffraction pattern. Remarkably, that Fraunhofer E-field pattern corresponds to the exact Fourier transform of the aperture function—a fact we shall confirm more rigorously in Section 11.3.3. Here the object is in the front focal plane, and all the various diffracted waves maintain their phase relationships traveling essentially equal optical path lengths to the transform plane. That doesn't quite happen when the object is displaced from the front focal plane. Then there will be a phase deviation, but that is actually of little consequence, since we are generally interested in the irradiance where the phase information is averaged out and the phase distortion is unobservable.

Thus if an otherwise opaque object mask contains a single circular hole, the E-field across it will resemble the top hat of Fig. 11.4(a), and the diffracted field, the Fourier transform, will be distributed in space as a Bessel function, looking very much like Fig. 11.4(b). Similarly, if the object transparency varies in density only along one axis, such that its amplitude transmission profile is triangular [Fig. 11.6(a)], then the amplitude of the electric field in the diffraction pattern will corre-

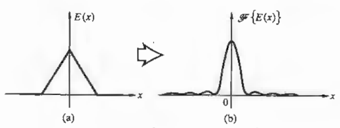


Figure 11.6 The transform of the triangle function is the sinc² function.

spond to Fig. 11.6(b)—the Fourier transform of the triangle function is the sinc-squared function.

11.2.3 The Dirac Delta Function

There are many physical phenomena that occur over very short durations in time with great intensity, and one is frequently concerned with the consequent response of some system to such stimuli. For example: How will a mechanical device, like a billiard ball, respond to being slammed with a hammer? Or how will a particular circuit behave if the input is a short burst of current? In much the same way we can envision some stimulus that is a sharp pulse in the space, rather than the time, domain. A bright minute source of light imbedded in a dark background is essentially a highly localized, two-dimensional, spatial pulse—a spike of irradiance. A convenient idealized mathematical representation of this sort of sharply peaked stimulus is the Dirac delta function $\delta(x)$. This is a quantity that is zero everywhere except at the origin, where it goes to infinity in a manner so as to encompass a *unit area*, that is,

$$\delta(x) = \begin{cases} 0 & x \neq 0 \\ \infty & x = 0 \end{cases} \tag{11.26}$$

and

$$\int_{-\infty}^{+\infty} \delta(x)\, dx = 1. \tag{11.27}$$

This is not really a function in the traditional mathematical sense. In fact, because it is so singular in nature, it remained the focus of considerable controversy after it was reintroduced and brought into prominence by P. A. M. Dirac in 1930. Yet physicists, pragmatic as they sometimes are, found it so highly useful that it soon became an established tool, despite whatever a lack of rigorous justification. The precise mathematical theory of the delta function evolved roughly [illegible] years later, in the early 1950s, principally at the [illegible] of Laurent Schwartz.

Perhaps the most basic operation to which $\delta(x)$ can be applied is the evaluation of the integral

$$\int_{-\infty}^{+\infty} \delta(x) f(x)\, dx.$$

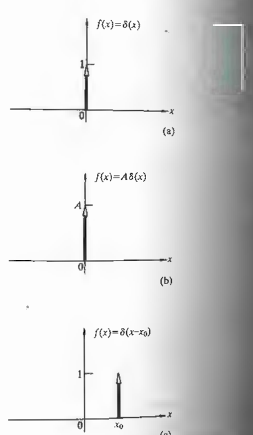


Figure 11.7 The height of the arrow representing the [illegible] corresponds to the area under the function.

Here the expression $f(x)$ corresponds to any continuous function. Over a tiny interval running from $x = -\gamma$ to $+\gamma$ centered about the origin, $f(x) \approx f(0) \approx$ constant, since the function is continuous at $x = 0$. From $x = -\infty$ to $-\gamma$ and from $x = +\gamma$ to $x = +\infty$, the integral is zero, simply because the δ-function is zero there. Thus the integral equals

$$f(0) \int_{-\gamma}^{+\gamma} \delta(x)\, dx.$$

Because $\delta(x) = 0$ for all x other than 0, the interval can be vanishingly small, that is, $\gamma \to 0$, and still

$$\int_{-\gamma}^{+\gamma} \delta(x)\, dx = 1,$$

from Eq. (11.27). Hence we have the exact result that

$$\int_{-\infty}^{+\infty} \delta(x) f(x)\, dx = f(0). \tag{11.28}$$

This is often spoken of as the **sifting property** of the δ-function, because it manages to extract only the one value of $f(x)$ taken at $x = 0$ from all its possible values. Similarly with a shift of origin of an amount x_0,

$$\delta(x - x_0) = \begin{cases} 0 & x \neq x_0 \\ \infty & x = x_0 \end{cases}, \tag{11.29}$$

[illegible] the spike resides at $x = x_0$ rather than $x = 0$, as shown in Fig. 11.7. The corresponding sifting property [illegible] appreciated by letting $x - x_0 = x'$, then with $f(x' + [illegible]) = g(x')$,

$$\int_{-\infty}^{+\infty} \delta(x - x_0) f(x)\, dx = \int_{-\infty}^{+\infty} \delta(x') g(x')\, dx' = g(0),$$

and since $g(0) = f(x_0)$,

$$\int_{-\infty}^{+\infty} \delta(x - x_0) f(x)\, dx = f(x_0). \tag{11.30}$$

Formally, rather than worrying about a precise definition of $\delta(x)$ for each value of x, it would be more [illegible] to continue along the lines of defining the effect of $\delta(x)$ on some other function $f(x)$. Accordingly, Eq. (11.28) is really the definition of an entire operation

that assigns a number $f(0)$ to the function $f(x)$. Incidentally, an operation that performs this service is called a *functional*.

It is possible to construct a number of sequences of pulses, each member of which has an ever-decreasing width and a concomitantly increasing height, such that any one pulse encompasses a unit area. A sequence of square pulses of height a/L and width L/a for which $a = 1, 2, 3, \ldots$ would fit the bill; so would a sequence of Gaussians (11.11),

$$\delta_a(x) = \sqrt{\frac{a}{\pi}}\, e^{-ax^2}, \tag{11.31}$$

as in Fig. 11.8, or a sequence of sinc functions

$$\delta_a(x) = \frac{a}{\pi} \operatorname{sinc}(ax). \tag{11.32}$$

Such strongly peaked functions that approach the sifting property, that is, for which

$$\lim_{a \to \infty} \int_{-\infty}^{+\infty} \delta_a(x) f(x)\, dx = f(0), \tag{11.33}$$

are known as *delta sequences*. It is often useful, but not actually rigorously correct, to imagine $\delta(x)$ as the convergence limit of such sequences as $a \to \infty$. The extension of these ideas into two dimensions is provided by the definition

$$\delta(x, y) = \begin{cases} \infty & x = y = 0 \\ 0 & \text{otherwise} \end{cases} \tag{11.34}$$

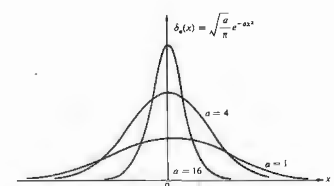


Figure 11.8 A sequence of Gaussians.

and

$$\iint_{-\infty}^{+\infty} \delta(x, y)\, dx\, dy = 1, \qquad (11.35)$$

and the sifting property becomes

$$\iint_{-\infty}^{+\infty} f(x, y)\delta(x - x_0)\delta(y - y_0)\, dx\, dy = f(x_0, y_0). \qquad (11.36)$$

Another representation of the δ-function follows from Eq. (11.3), the Fourier integral, which can be restated as

$$f(x) = \int_{-\infty}^{+\infty}\left[\frac{1}{2\pi}\int_{-\infty}^{+\infty} e^{-ik(x-x')}\, dk\right] f(x')\, dx',$$

and hence

$$f(x) = \int_{-\infty}^{+\infty} \delta(x - x')f(x')\, dx' \qquad (11.37)$$

provided that

$$\delta(x - x') = \frac{1}{2\pi}\int_{-\infty}^{+\infty} e^{-ik(x-x')}\, dk. \qquad (11.38)$$

Equation (11.37) is identical to Eq. (11.30), since by definition from Eq. (11.29) $\delta(x - x') = \delta(x' - x)$. The (divergent) integral of Eq. (11.38) is zero everywhere except at $x = x'$. Evidently, with $x' = 0$, $\delta(x) = \delta(-x)$ and

$$\delta(x) = \frac{1}{2\pi}\int_{-\infty}^{+\infty} e^{-ikx}\, dk = \frac{1}{2\pi}\int_{-\infty}^{+\infty} e^{ikx}\, dk. \qquad (11.39)$$

This implies, via (11.4), that the delta function can be thought of as the inverse Fourier transform of unity, that is, $\delta(x) = \mathscr{F}^{-1}\{1\}$ and so $\mathscr{F}\{\delta(x)\} = 1$. We can imagine a square pulse becoming narrower and taller as its transform, in turn, grows broader, until finally the pulse is infinitesimal in width, and its transform is infinite in extent, in other words, a constant.

i) Displacements and Phase Shifts

If the δ-spike is shifted off $x = 0$ to, say, $x = x_0$, its transform will change phase but not amplitude—that

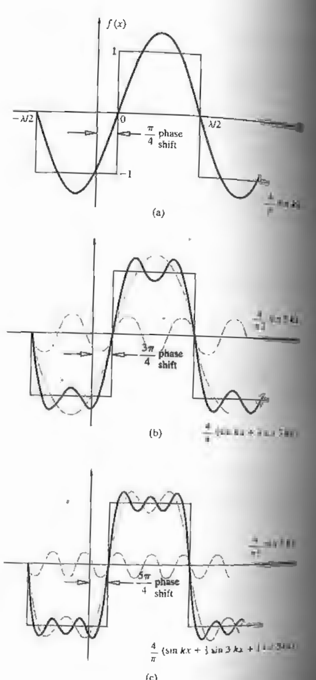


Figure 11.9 A shifted square wave showing the corresponding change in phase for each component wave.

remains equal to one. To see this, evaluate

$$\mathscr{F}\{\delta(x - x_0)\} = \int_{-\infty}^{+\infty} \delta(x - x_0)e^{ikx}\, dx.$$

From the sifting property (11.30) the expression becomes

$$\mathscr{F}\{\delta(x - x_0)\} = e^{ikx_0}, \qquad (11.40)$$

This should be compared with Eq. (11.76). What we see is that only the phase is affected, the amplitude being one as it was when $x_0 = 0$. This whole process can be appreciated somewhat more intuitively if we switch to the time domain and think of an infinitesimally narrow (such as a spark) occurring at $t = 0$. This results generation of an infinite range of frequency components, which are all initially in phase at the instant ation ($t = 0$). On the other hand, suppose the occurs at a time t_0. Again every frequency is duced, but in this situation the harmonic components are all in phase at $t = t_0$. Consequently, if we polate back, the phase of each constituent at $t = 0$ now have to be different, depending on the par- frequency. Besides, we know that all these com- its superimpose to yield zero everywhere except so that a frequency-dependent phase shift is quite able. This phase shift is evident in Eq. (11.40) the space domain. Note that it does vary with the lar spatial frequency k.

of this is quite general in its applicability, and we that *the Fourier transform of a function that is placed in space (or time) is the transform of the undisplaced tion multiplied by an exponential that is linear in phase* blem 11.14). This property of the transform will special interest presently, when we consider the of several point sources that are separated but wise identical. The process can be appreciated matically with the help of Figs. 11.9 and 7.13. To the square wave by $\pi/4$ to the right, the funda- must be shifted ⅛-wavelength (or, say, 1.0 mm), ery component must then be displaced an equal (i.e., 1.0 mm). Thus each component must be in phase by an amount specific to it that produces displacement. Here each is displaced, in turn, phase of $m\pi/4$.

ii) Sines and Cosines

We saw earlier (Fig. 11.1) that if the function at hand can be written as a sum of individual functions, its transform is simply the sum of the transforms of the component functions. Suppose we have a string of delta functions spread out uniformly like the teeth on a comb,

$$f(x) = \sum_j \delta(x - x_j). \qquad (11.41)$$

When the number of terms is infinite this periodic function is often called *comb*(x). In any event, the transform will simply be a sum of terms, such as that of Eq. (11.40):

$$\mathscr{F}\{f(x)\} = \sum_j e^{ikx_j}. \qquad (11.42)$$

In particular, if there are two δ-functions, one at $x_0 = d/2$ and the other at $x_0 = -d/2$,

$$f(x) = \delta[x - (+d/2)] + \delta[x - (-d/2)]$$

and

$$\mathscr{F}\{f(x)\} = e^{ikd/2} + e^{-ikd/2},$$

which is just

$$\mathscr{F}\{f(x)\} = 2\cos(kd/2), \qquad (11.43)$$

as in Fig. 11.10. Thus the transform of the sum of these two symmetrical δ-functions is a cosine function and vice versa. The composite is a real even function, and $F(k) = \mathscr{F}\{f(x)\}$ will also be real and even. This should be reminiscent of Young's experiment (p. 339) with infinitesimally narrow slits—we'll come back to it later.

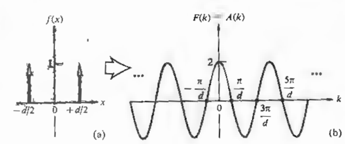


Figure 11.10 Two delta functions and their cosine-function transform.

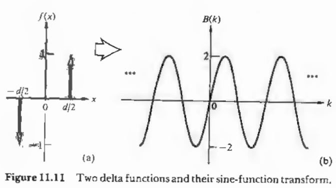


Figure 11.11 Two delta functions and their sine-function transform.

If the phase of one of the δ-functions is shifted, as in Fig. 11.11, the composite function is asymmetrical, it's odd,

$$f(x) = \delta[x - (+d/2)] - \delta[x - (-d/2)],$$

and

$$\mathscr{F}\{f(x)\} = e^{ikd/2} - e^{-ikd/2} = 2i \sin (kd/2). \quad (11.44)$$

The real sine transform (11.7) is then

$$B(k) = 2 \sin (kd/2), \quad (11.45)$$

and it too is an odd function.

This raises an interesting point. Recall that there are two alternative ways to consider the complex transform: either as the sum of a real and an imaginary part, from Eq. (11.7a), or as the product of an amplitude and a phase term, from Eq. (11.7b). It happens that the cosine and sine are rather special functions; the former is purely real and the latter is purely imaginary. Most functions, even harmonic ones, will usually be a blend of real and imaginary parts. For example, once a cosine is displaced a little, the new function, which is typically neither odd nor even, has both a real and an imaginary part. Moreover, it can be expressed as a cosinusoidal amplitude spectrum, which is appropriately phase-shifted (Fig. 11.12). Notice that when the cosine is shifted $\frac{1}{4}\lambda$ into a sine the relative phase difference between the two component delta functions is again π rad.

Figure 11.13 displays in summary form a number of transforms, mostly of harmonic functions. Observe how the functions and transforms in (a) and (b) combine to produce the function and its transform in (d). As a rule, each member of the pair of δ-pulses in the frequency spectrum of a harmonic function is located [illegible] k-axis at a distance from the origin equal to the [illegible] mental angular spatial frequency of $f(x)$. S[illegible] well-behaved periodic function can be expres[illegible] Fourier series, it can also be represented as an [illegible] pairs of delta functions, each weighted appro[illegible] and each a distance from the k-origin equal [illegible] angular spatial frequency of the particular [illegible] contribution—*the frequency spectrum of any periodic f[illegible] tion will be discrete.* One of the most remarkable of periodic functions is *comb*(x): as shown in Fig. 11[illegible] its transform is also a comb function.

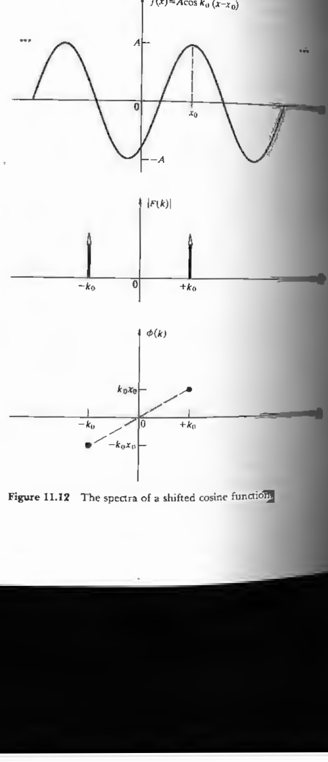


Figure 11.12 The spectra of a shifted cosine function.

11.3 OPTICAL APPLICATIONS

11.3.1 Linear Systems

[illegible]ier techniques provide a particularly elegant [illegible]ework from which to evolve a description of the [illegible]ation of images. And for the most part, this will [illegible] direction in which we shall be moving, although [illegible] side excursions are unavoidable in order to develop the needed mathematics.

A key point in the analysis is the concept of a **linear system**, which in turn is defined in terms of its input–output relations. Suppose then that an input signal [illegible] passing through some optical system results in an [illegible]ut $g(Y, Z)$. The system is linear if:

1. [illegible]lying $f(y, z)$ by a constant a produces an output [illegible] Z).
2. [illegible] the input is a weighted sum of two (or more) [illegible]ctions, $af_1(y, z) + bf_2(y, z)$, the output will similarly [illegible] the form $ag_1(Y, Z) + bg_2(Y, Z)$, where $f_1(y, z)$ and $f_2(y, z)$ generate $g_1(Y, Z)$ and $g_2(Y, Z)$ respectively.

[illegible]rmore, a linear system will be *space invariant* if [illegible]sses the property of *stationarity;* that is, in effect, [illegible]g the position of the input merely changes the [illegible] of the output without altering its functional [illegible] The idea behind much of this is that the output [illegible]d by an optical system can be treated as a linear [illegible]sition of the outputs arising from each of the [illegible]al points on the object. In fact, if we symbolically [illegible] the operation of the linear system as $\mathscr{L}\{\ \}$, the [illegible]ut and output can be written as

$$g(Y, Z) = \mathscr{L}\{f(y, z)\}. \quad (11.46)$$

[illegible]g the sifting property of the δ-function (11.36), [illegible] becomes

$$[illegible] = \mathscr{L}\left\{\iint_{-\infty}^{+\infty} f(y', z')\delta(y' - y)\delta(z' - z)\, dy'\, dz'\right\}.$$

[illegible] integral expresses $f(y, z)$ as a linear combination of [illegible]tary delta functions, each weighted by a number [illegible] It follows from the second linearity condition

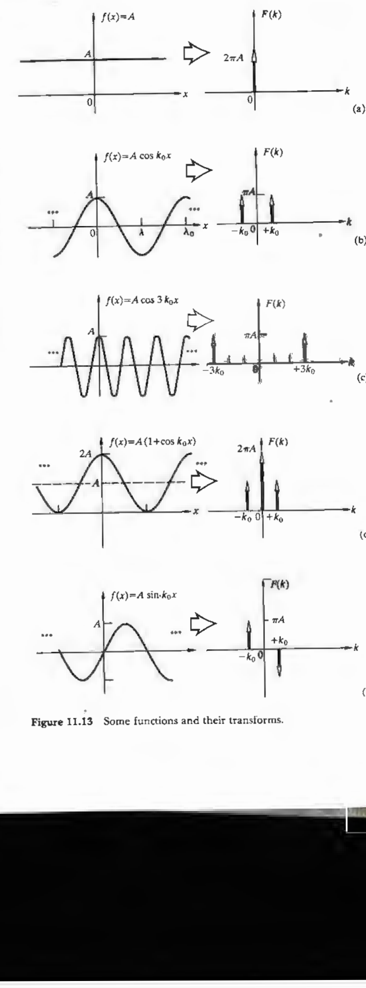


Figure 11.13 Some functions and their transforms.

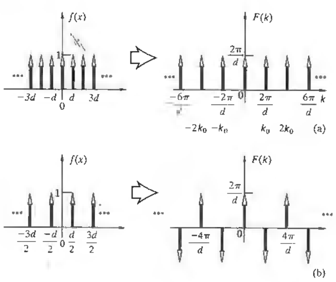


Figure 11.14 (a) The comb function and its transform. (b) A shifted comb function and its transform.

that the system operator can equivalently act on each of the elementary functions; thus

$$g(Y, Z) = \iint_{-\infty}^{+\infty} f(y', z')\mathscr{L}\{\delta(y' - y)\delta(z' - z)\}\, dy'\, dz'. \quad (11.47)$$

The quantity $\mathscr{L}\{\delta(y' - y)\delta(z' - z)\}$ is the response of the system (11.46) to a delta function located at the point (y', z') in the input space—it's called the **impulse response**. Apparently, if the impulse response of a system is known, the output can be determined directly from the input by means of Eq. (11.47). If the elementary sources are coherent, the input and output signals will have to be electric fields; if incoherent, they'll be flux densities.

Consider the self-luminous and, therefore, incoherent source depicted in Fig. 11.15. We can imagine that each point on the object plane, Σ_0, emits light that is processed by the optical system. It emerges to form a spot on the focal or image plane, Σ_i. In addition, *we assume that the magnification between object and image planes is one.* The image will be life-sized and erect, w... makes it a little easier to deal with for the time be... Notice that if the magnification (M_T) was great... one, the image would be larger than the object. Con... sequently, all of its structural details would be ... and broader, so the spatial frequencies of the har... contributions that go into synthesizing the image ... be lower than those of the object. For example, ... that is a transparency of a sinusoidally vary... and white linear pattern (a sinusoidal ampli... gra... ing) would be imaged having a greater space betwe... maxima and therefore a lower spatial frequen... Besides that, the image irradiance would be decre... by M_T^2, because the image area would be increa... by a factor of M_T^2.

If $I_0(y, z)$ is the irradiance distribution on the ... plane, an element $dy\,dz$ located at (y, z) will emit a ... flux of $I_0(y, z)\, dy\, dz$. Because of diffraction (an... possible presence of aberrations), this light is sm... out into some sort of blur spot over a finite area o... image plane rather than focused to a point. The ... of radiant flux is described mathematically by th... tion $\mathcal{S}(y, z; Y, Z)$, such that the flux density arr... the image point from $dy\,dz$ is

$$dI_i(Y, Z) = \mathcal{S}(y, z; Y, Z)I_0(y, z)\, dy\, dz. \quad (11.48)$$

This is the patch of light in the image plane at (Y, Z).

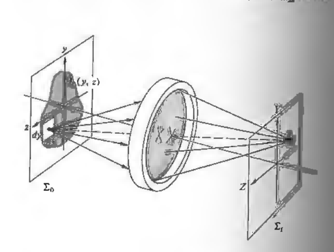


Figure 11.15 A lens system forming an image.

... $Y, Z)$ is known as the **point-spread function.** ...er words, when the irradiance $I_0(y, z)$ over the ...element $dy\,dz$ is 1 W/m², $\mathcal{S}(y, z; Y, Z)\, dy\, dz$ is the ... the resulting irradiance distribution in the ...ne. Because of the incoherence of the source, ...ensity contributions from each of its elements ...ve, so

$$I_i(Y, Z) = \iint_{-\infty}^{+\infty} I_0(y, z)\mathcal{S}(y, z; Y, Z)\, dy\, dz. \quad (11.49)$$

...ect," diffraction-limited optical system having ...ions, $\mathcal{S}(y, z; Y, Z)$ would correspond in shape ... diffraction figure of a point source at (y, z). ... if we set the input equal to a δ-pulse centered ... then $I_0(y, z) = A\delta(y - y_0)\delta(z - z_0)$. Here the ... A of magnitude one carries the needed units ... irradiance times area). Thus

$$I_i(Y, Z) = A \iint_{-\infty}^{+\infty} \delta(y - y_0)\delta(z - z_0)\mathcal{S}(y, z; Y, Z)\, dy\, dz,$$

... from the sifting property,

$$I_i(Y, Z) = A\mathcal{S}(y_0, z_0; Y, Z).$$

... point-spread function has a functional form ... to that of the image generated by a δ-pulse ...s the impulse response of the system [compare ...47) and (11.49)], whether optically perfect or ... a well-corrected system $\mathcal{S}$, apart from a multi... constant, is the Airy irradiance distribution ... centered on the Gaussian image point ... Fig. 11.16).

If the system is space invariant, a point-source input ... moved about over the object plane without any effect other than changing the location of its image. ...ently, one can say that the spread function is ...e for any point (y, z). In practice, however, the ... function will vary, but even so, the image plane ... divided into small regions, over each of which ... change appreciably. Thus if the object, and ... its image, is small enough, the system can be taken to be space invariant. We can imagine a spread ... sitting at every Gaussian image point on Σ_i, each multiplied by a different weighting factor $I_0(y, z)$ but all of the same general shape independent of (y, z). Since the magnification was set at one, the coordinates of any object and conjugate image point have the same magnitude.

If we were dealing with coherent light, we would have to consider how the system acted upon an input that was again a δ-pulse, but this time one representing the field amplitude. Once more the resulting image would be described by a spread function, although it would be an *amplitude* spread function. For a diffraction-limited circular aperture, the amplitude spread function looks like Fig. 10.28(b). And finally, we would have to be concerned about the interference that would take place on the image plane as the coherent fields interacted. By contrast, with incoherent object points the process occurring on the image plane is simply the summation of overlapping irradiances, as depicted in one dimension in Fig. 11.17. Each source point, with its own strength, corresponds to an appropriately scaled δ-pulse, and in the image plane each of these is smeared out, via the spread function. The sum of all the overlapping contributions is the image irradiance.

What kind of dependence on the image and object space variables will $\mathcal{S}(y, z; Y, Z)$ have? The spread func-

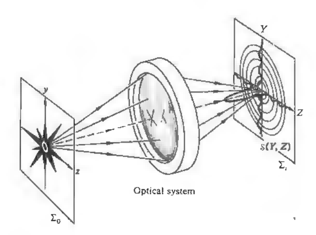


Figure 11.16 The point-spread function: the irradiance produced by the optical system with an input point source.

tion can only depend on (y, z) as far as the location of its center is concerned. Thus the value of $\mathcal{S}(y, z; Y, Z)$ anywhere on Σ_i merely depends on the displacement at that location from the particular Gaussian image point $(Y = y, Z = z)$ on which $\mathcal{S}$ is centered (Fig. 11.18). In other words,

$$\mathcal{S}(y, z; Y, Z) = \mathcal{S}(Y - y, Z - z). \qquad (11.50)$$

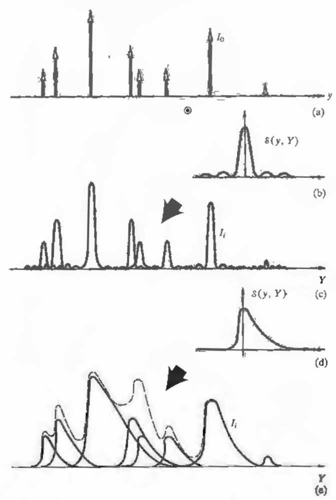


Figure 11.17 Here (a) is convolved first with (b) to produce (c) and then with (d) to produce (e). The resulting pattern is the sum of all the spread-out contributions as indicated by the dashed curve in (e).

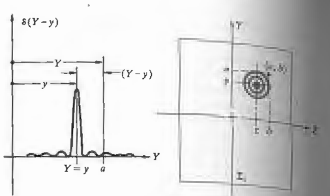


Figure 11.18 The point-spread function.

When the object point is on the central axis [illegible] z = 0), the Gaussian image point is as well [illegible] the spread function is then just $\mathcal{S}(Y, Z)$, as depic[illegible] 11.16. Under the circumstances of space inva[illegible] incoherence,

$$I_i(Y, Z) = \int\int_{-\infty}^{+\infty} I_0(y, z)\mathcal{S}(Y - y, Z - z)\, dy\, dz \qquad (11.51)$$

11.3.2 The Convolution Integral

Figure 11.17 shows a one-dimensional repr[illegible] of the distribution of point-source δ-function[illegible] up the object. The corresponding image is essen[illegible] obtained by "dealing out" an appropriately weight[illegible] point-spread function to the location of each ima[illegible] point on Σ_i and then adding up all the cont[illegible] at each point along Y. This dealing out of on[illegible] to every point of (and weighted by) another [illegible] a process known as **convolution**, and we say [illegible] function, $I_0(y)$, is convolved with another, $\mathcal{S}(y, Y)$, or vice versa.

This procedure can be carried out in two [illegible] as well, and that's essentially what is being [illegible] (11.51), the so-called *convolution integral* [illegible] corre[illegible] sponding one-dimensional expression de[illegible]ng the [illegible] of two functions $f(x)$ and $h(x)$,

$$g(X) = \int_{-\infty}^{+\infty} f(x)h(X - x)\, dx, \qquad (11.52)$$

[illegible] to visualize. In Fig. 11.17 one of the two func[illegible] a group of δ-pulses, and the convolution [illegible] was particularly easy to visualize. Still, we can [illegible] any function to be composed of a "densely [illegible]" continuum of δ-pulses and treat it in much the [illegible]shion. Let us now examine in some detail exactly [illegible] integral of Eq. (11.52) mathematically manages [illegible] the convolution. The essential features of

the process are illustrated in Fig. 11.19. The resulting signal $g(X_1)$, at some point X_1 in the output space, is a linear superposition of all the individual overlapping contributions that exist at X_1. In other words, each source element dx yields a signal of a particular strength $f(x)\, dx$, which is then smeared out by the system into a region centered about the Gaussian image point ($X = x$). The output at X_1 is then $dg(X_1) = f(x)h(X_1 - x)\, dx$. The integral sums up all of these contributions from each source element. Of couse the elements more remote from a given point on Σ_i contribute less, because the spread function generally drops off with displace-

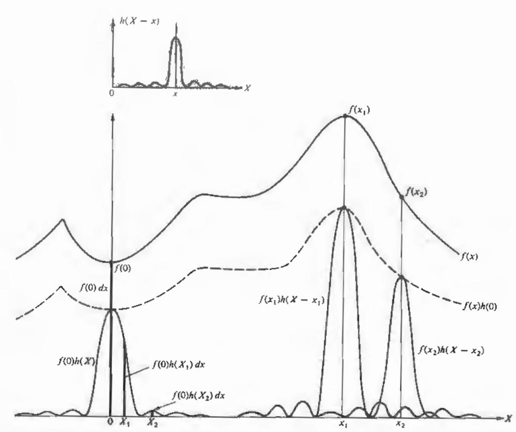


Figure 11.19 The overlapping of weighted spread functions.

ment. Thus we can imagine $f(x)$ to be a one-dimensional irradiance distribution, such as a series of vertical bands, as in Fig. 11.20. If the one-dimensional **line-spread function**, $h(X - x)$, is that of Fig. 11.20(d), the resulting image will simply be a somewhat blurred version of the input [Fig. 11.20(e)].

Let's now examine the convolution a bit more as a mathematical entity. Actually it's a rather subtle beast, performing a process that might certainly not be obvious at first glance, so let's approach it from a slightly different viewpoint. Accordingly, we will have two ways of thinking about the convolution integral, and we shall show that they are equivalent.

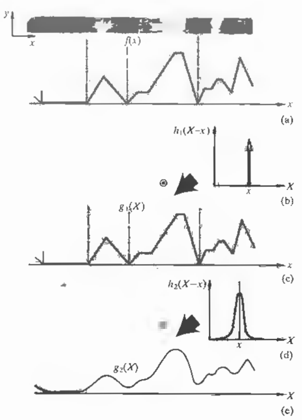
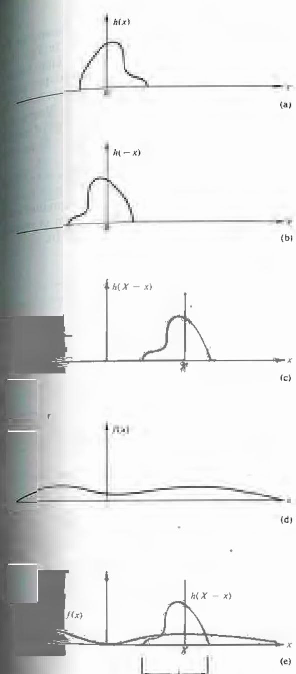


Figure 11.20 The irradiance distribution is converted to a function $f(x)$ shown in (a). This is convolved with a δ-function (b) to yield a duplicate of $f(x)$. By contrast, convolving $f(x)$ with the spread function h_2 in (d) yields a smoothed out curve represented by $g_2(x)$ in (e).

Suppose $h(x)$ looks like the asymmetrica... Fig. 11.21(a). Then $h(-x)$ appears in Fig. ... its shifted form $h(X - x)$ is shown in (c). ... lution of $f(x)$ [depicted in (d)] and $h(x)$ is $g(X)$ ... by Eq. (11.52). This is often written more co... $f(x) \circledast h(x)$. The integral simply says that the ... the product function $f(x)h(X - x)$ for all x is $g(X)$. Evidently the product is nonzero only over the range d wherein $h(X - x)$ is nonzero, that is, where ... two curves overlap [Fig. 11.21(e)]. At a particular ... in the output space, the area under the produ... $f(x)h(X_1 - x)$ is $g(X_1)$. This fairly direct inte... can be related back to the physically more plea... of the integral in terms of overlapping point ... tions, as depicted previously in Fig. 11.19. Remem... that there we said that each source element was ... out in a blur spot on the image plane having the ... of the spread function. Now suppose we take the ... approach and wish to compute the product area ... 11.21(e) at X_1, that is, $g(X_1)$. A differential ele... centered on any point in the region of ove... 11.22(a)], say x_1, will contribute an amount ... $x_1)\, dx$ to the area. This same differential ele... make an identical contribution when view... overlapping spread-function scheme. To see this, examine (b) and (c) in Fig. 11.22, which are *now dra... in the output space.* The latter shows the spread ... "centered" at $X = x_1$. A source element ... in this case located on the object at x_1, generates a sm... signal proportional to $f(x_1)h(X - x_1)$, as in ... $f(x_1)$ is just a number. The piece of this signal ... at X_1 is $f(x_1)h(X_1 - x_1)\, dx$, which indeed is ... the contribution made by dx at x_1 in (a). Simi... differential element of the product area (at an... in Fig. 11.22(a) has its counterpart in a curve ... of (d) but "centered" on a new point ($X = x$ ... beyond $x = x_2$ make no contribution, because ... not in the overlap region of (a) and, equiv... because they are too far from X_1 for the smear ... it, as shown in (e).

If the functions being convolved are simple en... $g(X)$ can be determined roughly without an... tions at all. The convolution of two identi...



...e 11.21 The geometry of the convolution process in the object ...dinates.

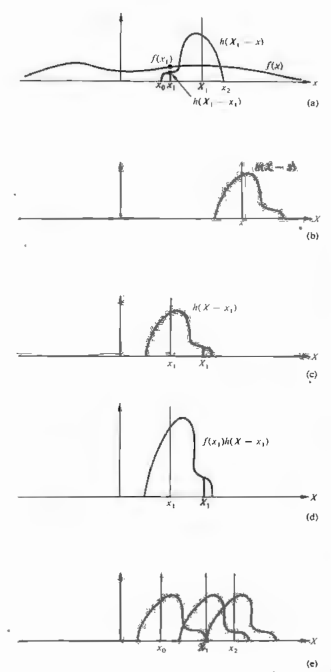


Figure 11.22 The geometry of the convolution process in the image coordinates.

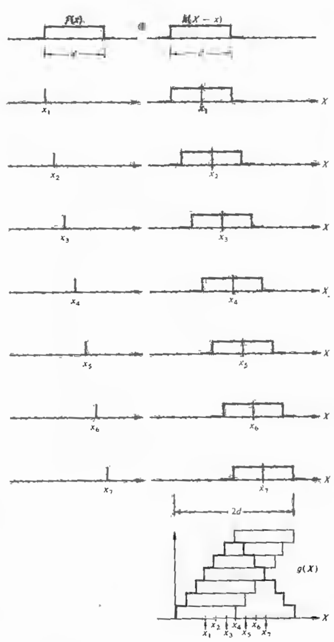


Figure 11.23 Convolution of two square pulses. The fact that we represented $f(x)$ by a finite number of delta functions (viz., 7) accounts for the steps in $g(X)$.

pulses is illustrated, from both of the viewpo[illegible] discussed above, in Figs. 11.23 and 11.24. In Fi[illegible] 1.23 each impulse constituting $f(x)$ is spread out in[illegible] pulse and summed. In Fig. 11.24 the overlap[illegible] as h varies, is plotted against X. In both ins[illegible] result is a triangular pulse. Incidentally, obse[illegible] that $(f \circledast h) = (h \circledast f)$, as can be seen by a change [illegible] $(x' = X - x)$ in Eq. (11.52), being careful wi[illegible] (see Problem 11.15).

Figure 11.25 illustrates the convolution of two [illegible]tions $I_0(y, z)$ and $\mathcal{S}(y, z)$ in two dimensions, a[illegible] Eq. (11.51). Here the volume under the [illegible] $I_0(y, z)\ \mathcal{S}(Y - y, Z - z)$, that is, the region of [illegible] equals $I_i(Y, Z)$ at (Y, Z); see Problem 11.16.

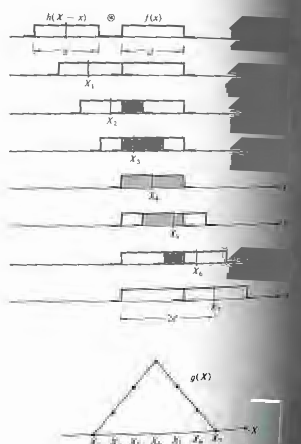


Figure 11.24 Convolution of two square pulses.

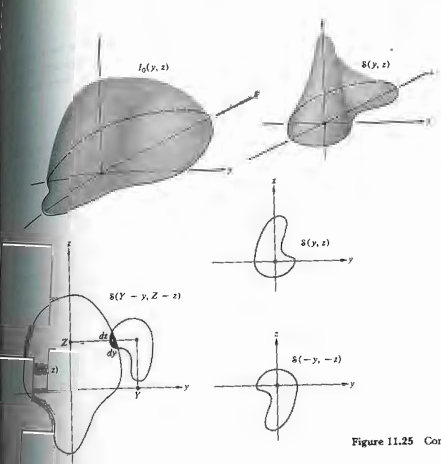


Figure 11.25 Convolution in two dimensions.

The Convolution Theorem

[illegible] have two functions $f(x)$ and $h(x)$ with Fourier [illegible]forms $\mathcal{F}\{f(x)\} = F(k)$ and $\mathcal{F}\{h(x)\} = H(k)$, [illegible]. The **convolution theorem** states that if [illegible]

$$\mathcal{F}\{g\} = \mathcal{F}\{f \circledast h\} = \mathcal{F}\{f\} \cdot \mathcal{F}\{h\} \qquad (11.53)$$

$$G(k) = F(k)H(k), \qquad (11.54)$$

[illegible] $= G(k)$. The proof is quite straightforward:

$$\mathcal{F}\{f \circledast h\} = \int_{-\infty}^{+\infty} g(X)e^{ikX}\,dX$$

$$= \int_{-\infty}^{+\infty} e^{ikX}\left[\int_{-\infty}^{+\infty} f(x)h(X - x)\,dx\right] dX.$$

Thus

$$G(k) = \int_{-\infty}^{+\infty}\left[\int_{-\infty}^{+\infty} h(X - x)e^{ikX}\,dX\right] f(x)\,dx.$$

If we put $w = X - x$ in the inner integral, then $dX = dw$ and

$$G(k) = \int_{-\infty}^{+\infty} f(x)e^{ikx}\,dx \int_{-\infty}^{+\infty} h(w)e^{ikw}\,dw.$$

Hence

$$G(k) = F(k)H(k),$$

which verifies the theorem. As an example of its application, refer to Fig. 11.26. Since the convolution of two identical square pulses $(f \circledast h)$ is a triangular pulse (g),

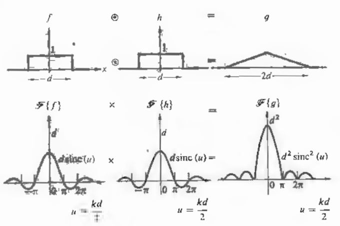


Figure 11.26 An illustration of the convolution theorem.

the product of their transforms (Fig. 7.17) must be the transform of g, namely,

$$\mathscr{F}\{g\} = [d \operatorname{sinc}(kd/2)]^2. \qquad (11.55)$$

As an additional example, convolve a square pulse with the two δ-functions of Fig. 11.11. The transform of the resulting double pulse (Fig. 11.27) is again the product of the individual transforms.

The k-space counterpart of Eq. (11.53), namely, the *frequency convolution theorem*, is given by

$$\mathscr{F}\{f \cdot h\} = \frac{1}{2\pi} \mathscr{F}\{f\} \circledast \mathscr{F}\{h\}; \qquad (11.56)$$

that is, the transform of the product is the convolution of the transforms.

Figure 11.28 makes the point rather nicely. Here an infinitely long cosine, $f(x)$, is multiplied by a rectangular pulse, $h(x)$, which truncates it into a short oscillatory wavetrain, $g(x)$. The transform of $f(x)$ is a pair of delta functions, the transform of the rectangular pulse is a sinc function, and the convolution of the two is the transform of $g(x)$. Compare this result with that of Eq. (7.60).

ii) Transform of the Gaussian Wave Packet

As a further example of the usefulness of the convolution theorem, let's evaluate the Fourier transform of a pulse of light in the configuration of the wave[illegible] of Fig. 11.29. Taking a rather general appro[illegible] that since a one-dimensional harmonic wa[illegible] form

$$E(x, t) = E_0 e^{-i(k_0 x - \omega t)},$$

one need only modulate the amplitude to get a pulse of the desired structure. Assuming the wave's profile to be independent of time, we can write it as

$$E(x, 0) = f(x) e^{-ik_0 x}.$$

Now, to determine $\mathscr{F}\{f(x)e^{-ik_0 x}\}$ evaluate

$$\int_{-\infty}^{+\infty} f(x) e^{-ik_0 x} e^{ikx}\, dx. \qquad (11.57)$$

Letting $k' = k - k_0$, we get

$$F(k') = \int_{-\infty}^{+\infty} f(x) e^{ik'x}\, dx = F(k - k_0) \qquad (11.58)$$

In other words, if $F(k) = \mathscr{F}\{f(x)\}$, then [illegible] $\mathscr{F}\{f(x)e^{-ik_0 x}\}$. For the specific case of [illegible] envelope (11.11), as in the figure, $f(x) = \sqrt{a/\pi}$ [illegible] is,

$$E(x, 0) = \sqrt{a/\pi}\, e^{-ax^2} e^{-ik_0 x}. \qquad (11.59)$$

From the foregoing discussion and Eq. (11.1[illegible] that

$$\mathscr{F}\{E(x, 0)\} = e^{-(k-k_0)^2/4a}. \qquad (11.60)$$

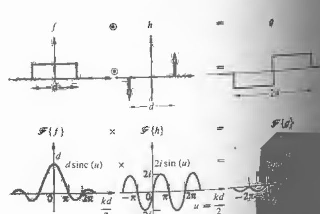
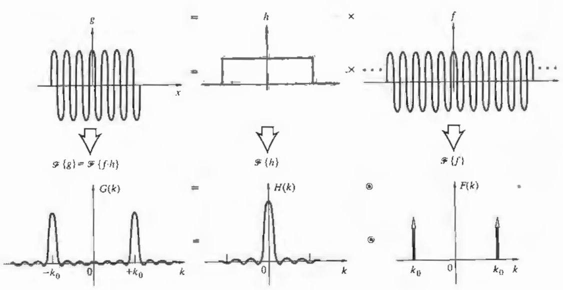
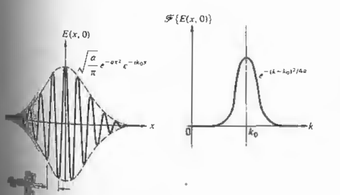


Figure 11.27 An illustration of the convolution th[illegible]



[illegible] 11.28 An example [illegible] the frequency convolution theorem.

In [illegible] different way, the transform can be deter[illegible] from Eq. (11.56). The expression $E(x, 0)$ is now [illegible] as the product of the two functions $f(x) =$ [illegible] $\exp(-ax^2)$ and $h(x) = \exp(-ik_0 x)$. One way to [illegible] $\mathscr{F}\{h\}$ is to set $f(x) = 1$ in Eq. (11.57). This yields the transform of 1 with k replaced by $k - k_0$. Since [illegible] $= 2\pi\delta(k)$ (see Problem 11.4), we have $\mathscr{F}\{e^{-ik_0 x}\} =$ [illegible] $- k_0)$. Thus $\mathscr{F}\{E(x, 0)\}$ is $1/2\pi$ times the convo[illegible] of $2\pi\delta(k - k_0)$, with the Gaussian $e^{-k^2/4a}$ centered on zero. The result* is once again a Gaussian centered on k_0, namely, $e^{-(k-k_0)^2/4a}$.



[illegible] 11.29 A Gaussian wave packet and its transform.

11.3.3 Fourier Methods in Diffraction Theory

i) Fraunhofer Diffraction

Fourier-transform theory provides a particularly beautiful insight into the mechanism of Fraunhofer diffraction. Let's go back to Eq. (10.41), rewritten as

$$E(Y, Z) = \frac{\mathcal{E}_A e^{i(\omega t - kR)}}{R} \iint_{\text{Aperture}} e^{ik(Yy + Zz)/R}\, dy\, dz. \qquad (11.61)$$

* We should actually have used the real part of $\exp(-ik_0 x)$ to start with in this derivation, since the transform of the complex exponential is different from the transform of $\cos k_0 x$ and taking the real part afterward is insufficient. This is the same sort of difficulty one always encounters when forming products of complex exponentials. The final answer (11.60) should, in fact, contain an additional $\exp[-(k + k_0)^2/4a]$ term, as well as a multiplicative constant of $\frac{1}{2}$. This second term is usually negligible in comparison, however. Even so, had we used $\exp(+ik_0 x)$ to start with (11.59), only the negligible term would have resulted! Using the complex exponential to represent the sine or cosine in this fashion is *rigorously incorrect*, albeit pragmatically common practice. As a short-cut device, it should be indulged in only with the greatest caution!

This formula refers to Fig. 10.22, which depicts an arbitrary diffracting aperture in the yz-plane upon which is incident a monochromatic plane wave. The quantity R is the distance from the center of the aperture to the output point where the field is $E(Y, Z)$. The source strength per unit area of the aperture is denoted by $\mathcal{E}_A$. We are talking about electric fields that are of course time-varying; the term $\exp i(\omega t - kR)$ just relates the phase of the net disturbance at the point (Y, Z) to that at the center of the aperture. The $1/R$ corresponds to the drop-off of field amplitude with distance from the aperture. The phase term in front of the integral is of little present concern, since we are interested in the relative amplitude distribution of the field, and it doesn't much matter what the resultant phase is at any particular output point. Thus if we limit ourselves to a small region of output space over which R is essentially constant, everything in front of the integral, with the exception of $\mathcal{E}_A$, can be lumped into a single constant. The $\mathcal{E}_A$ has thus far been assumed to be invariant over the aperture, but that certainly need not be the case. Indeed, if the aperture were filled with a bumpy piece of dirty glass, the field emanating from each area element $dy\,dz$ could differ in both amplitude and phase. There would be nonuniform absorption, as well as a position-dependent optical path length through the glass, which would certainly affect the diffracted field distribution. The variations in $\mathcal{E}_A$, as well as the multiplicative constant, can be combined into a single complex quantity

$$\mathcal{A}(y, z) = \mathcal{A}_0(y, z)e^{i\phi(y,z)}, \qquad (11.62)$$

which we call the **aperture function.** The amplitude of the field over the aperture is described by $\mathcal{A}_0(y, z)$, while the point-to-point phase variation is represented by $\exp[i\phi(y, z)]$. Accordingly, $\mathcal{A}(y, z)\,dy\,dz$ is proportional to the diffracted field emanating from the differential source element $dy\,dz$. Consolidating this much, we can reformulate Eq. (11.61) more generally as

$$E(Y, Z) = \iint_{-\infty}^{+\infty} \mathcal{A}(y, z)e^{ik(Yy+Zz)/R}\,dy\,dz. \qquad (11.63)$$

The limits on the integral can be extended to $\pm\infty$, because the aperture function is nonzero only over the region of the aperture.

Figure 11.30 A bit of geometry.

It might be helpful to envision $dE(Y, Z)$ at a given point P as if it were a plane wave propaga[illegible] direction of **k** as in Fig. 11.30, and having an [illegible] determined by $\mathcal{A}(y, z)\,dy\,dz$. To underscore th[illegible] ity between Eq. (11.63) and Eq. (11.14), let's define th[illegible] *spatial frequencies k_Y and k_Z* as

$$k_Y = kY/R = k\sin\phi = k\cos\beta \qquad (11.64)$$

and

$$k_Z = kZ/R = k\sin\theta = k\cos\gamma. \qquad (11.65)$$

For each point on the image plane, there is a corresponding spatial frequency. The diffracted field can now b[illegible] as

$$E(k_Y, k_Z) = \iint_{-\infty}^{+\infty} \mathcal{A}(y, z)e^{i(k_Y y+k_Z z)}\,dy\,dz. \qquad (11.66)$$

and we've arrived at the key point: *the fi[illegible] in the Fraunhofer diffraction pattern is the Fou[illegible] of the field distribution across the aperture (*[illegible]*function*). Symbolically, this is written as

$$E(k_Y, k_Z) = \mathcal{F}\{\mathcal{A}(y, z)\} \qquad (11.67)$$

The [illegible] distribution in the image plane is the spatial-[illegible] spectrum of the aperture function. The inverse [illegible]rm is then

$$\mathcal{A}(y, z) = \frac{1}{(2\pi)^2}\iint_{-\infty}^{+\infty} E(k_Y, k_Z)e^{-i(k_Y y+k_Z z)}\,dk_Y\,dk_Z, \qquad (11.68)$$

[illegible]

$$\mathcal{A}(y, z) = \mathcal{F}^{-1}\{E(k_Y, k_Z)\}. \qquad (11.69)$$

[illegible] have seen time and again, the more localized the [illegible] the more spread out is its transform—the same [illegible] two dimensions. The smaller the diffracting [illegible] the larger the angular spread of the diffracted [illegible] equivalently, the larger the spatial frequency [illegible].

[illegible] Single Slit

[illegible] illustration of the method, consider the long slit [illegible] direction of Fig. 10.10, illuminated by a plane wave. Assuming that there are no phase or amplitude variations across the aperture, $\mathcal{A}(y, z)$ has the form of a square pulse (Fig. 7.17):

$$\mathcal{A}(y, z) = \begin{cases} \mathcal{A}_0 & \text{when } |z| \leq b/2 \\ 0 & \text{when } |z| > b/2, \end{cases}$$

where $\mathcal{A}_0$ is no longer a function of y and z. If we take it as a one-dimensional problem,

$$E(k_Z) = \mathcal{F}\{\mathcal{A}(z)\} = \mathcal{A}_0 \int_{z=-b/2}^{+b/2} e^{ik_Z z}\,dz$$

$$= \mathcal{A}_0 b \operatorname{sinc} k_Z b/2.$$

With $k_Z = k\sin\theta$, this is precisely the form derived in Section 10.2.1. The far-field diffraction pattern of a **rectangular aperture** (Section 10.2.4) is the two-**dimensional counterpart** of the slit. **With** $\mathcal{A}(y, z)$ again equal to $\mathcal{A}_0$ over the aperture (Fig. 10.23),

$$E(k_Y, k_Z) = \mathcal{F}\{\mathcal{A}(y, z)\}$$

$$= \int_{y=-b/2}^{+b/2}\int_{z=-a/2}^{+a/2} \mathcal{A}_0 e^{i(k_Y y+k_Z z)}\,dy\,dz.$$

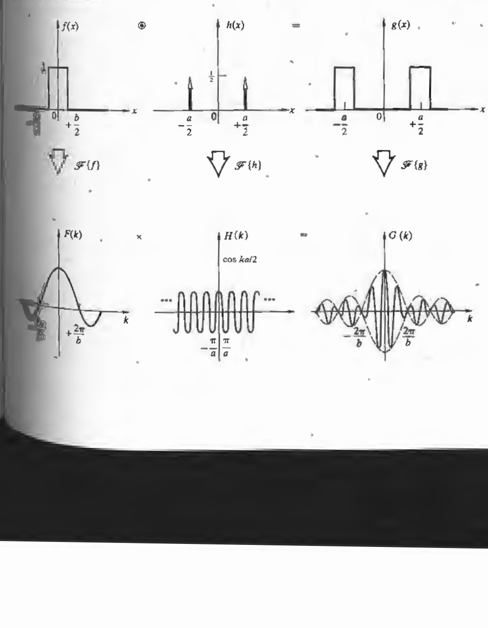


Figure 11.31 An illustration of the convolution theorem.

hence,

$$E(k_Y, k_Z) = \mathcal{A}_0 ba \operatorname{sinc}\frac{bkY}{2R} \operatorname{sinc}\frac{akZ}{2R}$$

just as in Eq. (10.42), where ba is the area of the hole.

Young's Experiment: The Double Slit

In our first treatment of Young's experiment (Section 9.3) we took the slits to be infinitesimally wide. The aperture function was then two symmetrical δ-pulses, and the corresponding idealized field amplitude in the diffraction pattern was the Fourier transform, namely, a cosine function. Squared, this yields the familiar cosine-squared irradiance distribution of Fig. 9.6. More realistically, each aperture actually has some finite shape, and the real diffraction pattern will never be quite so simple. Figure 11.31 shows the case in which the holes are actual slits. The aperture function, $g(x)$, is obtained by convolving the δ-function spikes, $h(x)$, that locate each slit with the rectangular pulse, $f(x)$, that corresponds to the particular opening. From the convolution theorem, the product of the transforms is the modulated cosine amplitude function representing the diffracted field as it appears on the image plane. Squaring that would produce the anticipated double-slit irradiance distribution shown in Fig. 10.17. The one-dimensional transform curves are plotted against k, but that's equivalent to plotting against image-space variables by means of Eq. (11.64). (The same reasoning applied to circular apertures yields the fringe pattern of Fig. 12.2.)

Three Slits

Looking at Fig. 11.13(d) it should be clear that the transform of the array of three δ-functio[illegible] in the diagram will generate a cosine that is raised [illegible] amount proportional to the zero-frequency te[illegible] **is, the δ-function at the origin.** When that delta [illegible] **has twice the amplitude of the** other two, the [illegible] **totally positive. Now** suppose we have thr[illegible] **narrow parallel slits uniformly illuminated.** [illegible] **ture function corresponds** to Fig. 11.32(a), [illegible] **central δ-function is half** its previous size. A[illegible] **the cosine transform** will drop one quarter [illegible] **down, as indicated in** Fig. 11.32(b). This [illegible] **to the diffracted electric field amplitude,** and [illegible] Fig. 11.32(c), is the three-slit irradiance pattern.

ii) Apodization

The term **apodization** derives from the Gre[illegible] away, and $\pi o \delta o \sigma$, meaning foot. It refers to the pro[illegible] of suppressing the secondary maxima (side lobes) [illegible] feet of a diffraction pattern. In the case o[illegible] pupil (Section 10.2.5), the diffraction pattern [illegible] spot surrounded by concentric rings. The fi[illegible] a flux density of 1.75% that of the central pea[illegible] small but it can be troublesome. About 16% of the [illegible] incident on the image plane is distributed in the [illegible] system. The presence of these side lobes ca[illegible] the resolving power of an optical system to a [illegible] apodization is called for, as is often the case in [illegible] and spectroscopy. For example, the star Si[illegible] appears as the brightest star in the sky (it's in the

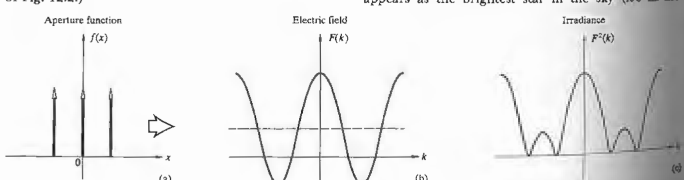


Figure 11.32 The Fourier transform of three equal δ-functions representing three slits.

[illegible]llation *Canis Major*—the big dog), is actually one [illegible]inary system. It's accompanied by a faint white [illegible] as they both orbit about their mutual center of [illegible] Because of the tremendous difference in brightness (10^4 to 1), the image of the faint companion, as [illegible] with a telescope, is generally completely [illegible] by the side lobes of the diffraction pattern of [illegible]in star.

[illegible]ization can be accomplished in several ways, for [illegible]le, by altering the shape of the aperture or its [illegible]mission characteristics.* We already know from [illegible]1.66) that the diffracted field distribution is the [illegible]orm of $\mathcal{A}(y, z)$. Thus we could effect a change in [illegible]obes by altering $\mathcal{A}_0(y, z)$ or $\phi(y, z)$. Perhaps the [illegible] approach is the one in which only $\mathcal{A}_0(y, z)$ is [illegible]ated. This can be accomplished physically by [illegible] the aperture with a suitably coated flat glass plate (or coating the objective lens itself). Suppose that [illegible]ting becomes increasingly opaque as it goes [illegible] out from the center (in the yz-plane) towards [illegible]es of a circular pupil. The transmitted field will [illegible]ondingly decrease off-axis until it is made to [illegible] negligible at the periphery of the aperture. In [illegible]lar, imagine that this drop-off in amplitude fol- [illegible] Gaussian curve. Then $\mathcal{A}_0(y, z)$ is a Gaussian func- [illegible] its transform $E(Y, Z)$, and consequently the [illegible] system vanishes. Even though the central peak is [illegible]dened, the side lobes are indeed suppressed (Fig. 11.33).

[illegible]other rather heuristic but appealing way to look at the process is to realize that the higher spatial [illegible]ency contributions go into sharpening up the [illegible] of the function being synthesized. As we saw [illegible] in one dimension (Fig. 7.13), the high frequen- [illegible] to fill in the corners on the square pulse. In [illegible] way, since $\mathcal{A}(y, z) = \mathcal{F}^{-1}\{E(k_Y, k_Z)\}$, sharp [illegible] on the aperture necessitate the presence of [illegible]eciable contributions of high spatial frequency in [illegible] diffracted field. It follows that making $\mathcal{A}_0(y, z)$ fall [illegible]dually will reduce these high frequencies, which [illegible] is manifest in a suppression of the side lobes.

[illegible]dization is one aspect of the more encompassing technique of *spatial filtering*, which is discussed in an extensive yet nonmathematical treatment in Chapter 14.

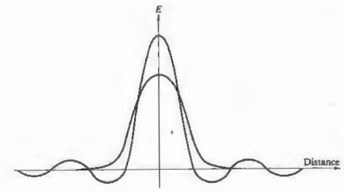


Figure 11.33 An Airy pattern compared with a Gaussian.

iii) The Array Theorem

Generalizing some of our previous ideas to two dimensions, imagine that we have a screen containing N identical holes, as in Fig. 11.34. In each aperture, at the same relative position, we locate a point $O_1, O_2, \ldots, O_N$ at $(y_1, z_1), (y_2, z_2), \ldots, (y_N, z_N)$, respectively. Each of these, in turn, fixes the origin of a local coordinate system (y', z'). Thus a point (y', z') in the local frame of the jth aperture has coordinates $(y_j + y', z_j + z')$ in the (y, z)-system. Under coherent monochromatic illumination, the resulting Fraunhofer diffraction field $E(Y, Z)$ at some point P on the image plane will be a superposition of the individual fields at P arising from each separate aperture; in other words,

$$E(Y, Z) = \sum_{j=1}^{N} \iint_{-\infty}^{+\infty} \mathcal{A}_j(y', z') e^{ik(Y(y_j+y')+Z(z_j+z'))/R}\, dy'\, dz' \tag{11.70}$$

or

$$E(Y, Z) = \iint_{-\infty}^{+\infty} \mathcal{A}_j(y', z') e^{ik(Yy'+Zz')/R}\, dy'\, dz' \times \sum_{j=1}^{N} e^{ik(Yy_j+Zz_j)/R}, \tag{11.71}$$

[illegible] extensive treatment of the subject, see P. Jacquinot and B. [illegible]Dossier, "Apodization," in Vol. III of *Progress in Optics.*

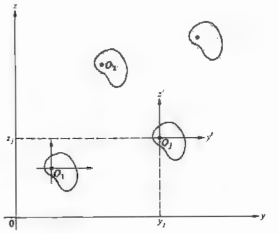


Figure 11.34 Multiple-aperture configuration.

where $\mathcal{A}_I(y', z')$ is the individual aperture function applicable to each hole. This can be recast, using Eqs. (11.64) and (11.65), as

$$E(k_Y, k_Z) = \iint_{-\infty}^{+\infty} \mathcal{A}_I(y', z')e^{i(k_Y y' + k_Z z')}\, dy'\, dz'$$

$$\times \sum_{j=1}^{N} e^{i(k_Y y_j)}\, e^{i(k_Z z_j)}. \qquad (11.72)$$

Notice that the integral is the Fourier transform of the individual aperture function, while the sum is the transform (11.42) of an array of delta functions

$$A_\delta = \sum_j \delta(y - y_j)\delta(z - z_j). \qquad (11.73)$$

Inasmuch as $E(k_Y, k_Z)$ itself is the transform $\mathcal{F}\{\mathcal{A}(y, z)\}$ of the total aperture function for the entire array, we have

$$\mathcal{F}\{\mathcal{A}(y, z)\} = \mathcal{F}\{\mathcal{A}_I(y', z')\} \cdot \mathcal{F}\{A_\delta\}. \qquad (11.74)$$

This equation is a statement of the **array theorem**, which says that *the field distribution in the Fraunhofer diffraction pattern of an array of similarly oriented identical apertures equals the Fourier transform of an individual aperture function (i.e., its diffracted field distribution) multiplied by the pattern that would result from a set of point sources arrayed in the same configuration (which is the transform of A_δ).*

This can be seen from a slightly different [illegible] view. The total aperture function may be [illegible]ed by convolving the individual aperture function [illegible]ith an appropriate array of delta functions, each [illegible] at one of the coordinate origins (y_1, z_1), (y_2, z_2), [illegible]. Hence

$$\mathcal{A}(y, z) = \mathcal{A}_I(y', z') \circledast A_\delta, \qquad (11.[illegible])$$

whereupon the array theorem follows directly from [illegible] convolution theorem (11.53).

As a simple example, imagine that we [illegible] Young's experiment with two slits along the [illegible] of width b and separation a. The individual [illegible] function for each slit is a step function,

$$\mathcal{A}_I(z') = \begin{cases} \mathcal{A}_{I0} & \text{when } |z'| \le b/2 \\ 0 & \text{when } |z'| > b/2, \end{cases}$$

and so

$$\mathcal{F}\{\mathcal{A}_I(z')\} = \mathcal{A}_{I0} b \,\text{sinc}\, k_Z b/2.$$

With the slits located at $z = \pm a/2$,

$$A_\delta = \delta(z - a/2) + \delta(z + a/2),$$

and from Eq. (11.43)

$$\mathcal{F}\{A_\delta\} = 2\cos k_Z a/2.$$

Thus

$$E(k_Z) = 2\mathcal{A}_{I0} b \,\text{sinc}\left(\frac{k_Z b}{2}\right)\cos\left(\frac{k_Z a}{2}\right)$$

which is the same conclusion arrived at [illegible] 11.31). The irradiance pattern is a set of [illegible] interference fringes modulated by a *sinc-squared* [illegible]tion envelope.

11.3.4 Spectra and Correlation

i) Parseval's Formula

Suppose that $f(x)$ is a pulse of finite extent, [illegible] is its Fourier transform (11.5). Thinking back to [illegible] 7.8, we recognize the function $F(k)$ as the [illegible] the spatial frequency spectrum of $f(x)$. [illegible] then connotes the amplitude of the contribu[illegible] pulse within the frequency range from k to [illegible]

[illegible] it seems that $|F(k)|$ serves as a spectral amplitude [illegible], and its square, $|F(k)|^2$, should be proportional [illegible] energy per unit spatial frequency interval. [illegible] in the time domain, if $f(t)$ is a radiated electric [illegible] $|f(t)|^2$ is proportional to the radiant flux or power, [illegible] the total emitted energy is proportional to [illegible] dt. With $F(\omega) = \mathcal{F}\{f(t)\}$ it appears that $|F(\omega)|^2$ [illegible] a measure of the radiated energy per unit [illegible] frequency interval. To be a bit more precise, [illegible] evaluate $\int_{-\infty}^{+\infty} |f(t)|^2\, dt$ in terms of the appropriate [illegible]urier transforms. Inasmuch as $|f(t)|^2 = f(t)f^*(t) = f(t)\{\mathcal{F}^{-1}[\mathcal{F}(\omega)]\}^*$,

$$\int_{-\infty}^{+\infty} |f(t)|^2\, dt = \int_{-\infty}^{+\infty} f(t)\left[\frac{1}{2\pi}\int_{-\infty}^{+\infty} F^*(\omega)e^{+i\omega t}\, d\omega\right] dt.$$

[illegible]anging the order of integration, we obtain

$$\int_{-\infty}^{+\infty} |f(t)|^2\, dt = \frac{1}{2\pi}\int_{-\infty}^{+\infty} F^*(\omega)\left[\int_{-\infty}^{+\infty} f(t)e^{i\omega t}\, dt\right] d\omega$$

and so

$$\int_{-\infty}^{+\infty} |f(t)|^2\, dt = \frac{1}{2\pi}\int_{-\infty}^{+\infty} |F(\omega)|^2\, d\omega, \qquad (11.76)$$

where $|F(\omega)|^2 = F^*(\omega)F(\omega)$. This is *Parseval's formula.* [illegible]ected, the total energy is proportional to the area [illegible] the $|F(\omega)|^2$ curve, and consequently $|F(\omega)|^2$ is [illegible]etimes called the **power spectrum** or *spectral energy* [illegible]*ibution.* The corresponding formula for the space domain is

$$\int_{-\infty}^{+\infty} |f(x)|^2\, dx = \frac{1}{2\pi}\int_{-\infty}^{+\infty} |F(k)|^2\, dk. \qquad (11.77)$$

ii) The Lorentzian Profile

As an indication of the manner in which these ideas are [illegible] in practice, consider the damped harmonic wave $f(t)$ at $x = 0$ depicted in Fig. 11.35. Here

$$f(t) = \begin{cases} 0 & \text{from } t = -\infty \text{ to } t = 0 \\ f_0 e^{-t/2\tau}\cos\omega_0 t & \text{from } t = 0 \text{ to } t = +\infty. \end{cases}$$

[illegible]ve exponential dependence arises, quite gen[illegible] whenever the rate of change of a quantity [illegible]on its instantaneous value. In this case, we [illegible]pose that the power radiated by an atom varies

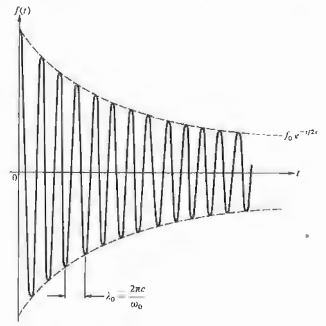


Figure 11.35 A damped harmonic wave.

as $(e^{-t/\tau})^{1/2}$. In any event, τ is known as the time constant of the oscillation, and $\tau^{-1} = \gamma$ is the damping constant. The transform of $f(t)$ is

$$F(\omega) = \int_0^{\infty} (f_0 e^{-t/2\tau}\cos\omega_0 t)e^{i\omega t}\, dt. \qquad (11.78)$$

The evaluation of this integral is explored in the problems. One finds on performing the calculation that

$$F(\omega) = \frac{f_0}{2}\left[\frac{1}{2\tau} - i(\omega + \omega_0)\right]^{-1} + \frac{f_0}{2}\left[\frac{1}{2\tau} - i(\omega - \omega_0)\right]^{-1}$$

When $f(t)$ is the radiated field of an atom, τ denotes the *lifetime* of the excited state (from around 1.0 ns to 10 ns). Now if we form the power spectrum $F(\omega)F^*(\omega)$, it will be composed of two peaks centered on $\pm\omega_0$ and thus separated by $2\omega_0$. At optical frequencies where $\omega_0 \gg \gamma$, these will be both narrow and widely spaced, with essentially no overlap. The shape of these peaks is determined by the transform of the modulation envelope in Fig. 11.35, that is, a negative exponential. The location of the peaks is fixed by the frequency of the modulated cosine wave, and the fact that there are two such peaks is a reflection of the spectrum of the cosine in this symmetrical frequency representation (Section 7.8). To determine the observable spectrum from $F(\omega)F^*(\omega)$, we need only consider the positive frequency term, namely,

$$|F(\omega)|^2 = \frac{f_0^2}{\gamma^2}\frac{\gamma^2/4}{(\omega-\omega_0)^2+\gamma^2/4}. \qquad (11.79)$$

This has a maximum value of f_0^2/γ^2 at $\omega = \omega_0$, as shown in Fig. 11.36. At the half-power points $(\omega - \omega_0) = \pm\gamma/2$, $|F(\omega)|^2 = f_0^2/2\gamma^2$, which is half its maximum value. The width of the spectral line between these points is equal to γ.

The curve given by Eq. (11.79) is known as the *resonance* or *Lorentz profile.* The frequency bandwidth arising from the finite duration of the excited state is called the *natural linewidth.*

If the radiating atom suffers a collision, it can lose energy and thereby further shorten the duration of emission. The frequency bandwidth increases in the process, which is known as *Lorentz broadening.* Here again, the spectrum is found to have a Lorentz profile. Furthermore, because of the random thermal motion of the atoms in a gas, the frequency bandwidth will be increased via the Doppler effect. *Doppler broadening,* as it is called, results in a Gaussian spectrum (Section 7.10). The Gaussian drops more slowly in the immediate vicinity of ω_0 and then more quickly away from it than does the Lorentzian profile. These effects can be combined mathematically to yield a single spectrum by convolving the Gaussian and Lorentzian functions. In a low-pressure gaseous discharge, the Gaussian profile is by far the wider and generally predominates.

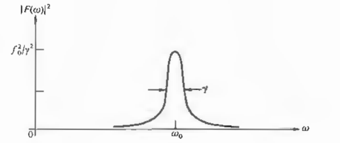


Figure 11.36 The resonance or Lorentz profile.

iii) Autocorrelation and Cross-Corre[redacted]

Let's now go back to the derivation of Parse[redacted] and follow it through again, this time [redacted] modification. We wish to evaluate $\int_{-\infty}^{+\infty} f(t[redacted]\tau)f^*(t)$[redacted] using much the same approach as befor[redacted] Thus[redacted] $F(\omega) = \mathcal{F}\{f(t)\}$,

$$\int_{-\infty}^{+\infty} f(t+\tau)f^*(t)\,dt = \int_{-\infty}^{+\infty} f(t+\tau) \times\left[\frac{1}{2\pi}\int_{-\infty}^{+\infty} F^*(\omega)e^{-i\omega t}\,d\omega\right] dt \qquad (11.80)$$

Changing the order of integration, we obtai[redacted]

$$\frac{1}{2\pi}\int_{-\infty}^{+\infty} F^*(\omega)\left[\int_{-\infty}^{+\infty} f(t+\tau)e^{i\omega t}\,dt\right] d\omega = \frac{1}{2\pi}\int_{-\infty}^{+\infty} F^*(\omega)\mathcal{F}\{f(t+\tau)\}\,d\omega.$$

To evaluate the transform within the last in[redacted] that

$$f(t+\tau) = \frac{1}{2\pi}\int_{-\infty}^{+\infty} F(\omega)e^{-i\omega(t+\tau)}\,d\omega$$

by a change of variable in Eq. (11.9). Hence,

$$f(t+\tau) = \mathcal{F}^{-1}\{F(\omega)e^{-i\omega\tau}\},$$

so as discussed earlier, $\mathcal{F}\{f(t+\tau)\} = F(\omega)e^{-i\omega\tau}$. Eq. (11.80) becomes

$$\int_{-\infty}^{+\infty} f(t+\tau)f^*(t)\,dt = \frac{1}{2\pi}\int_{-\infty}^{+\infty} F^*(\omega)F(\omega)e^{-i\omega\tau}\,d\omega, \qquad (11.81)$$

and both sides are functions of the para[redacted] left-hand side of this formula is said to be [redacted] **lation** of $f(t)$, denoted by

$$c_{ff}(\tau) = \int_{-\infty}^{+\infty} f(t+\tau)f^*(t)\,dt, \qquad (11.82)$$

which is often **written** symbolically as $f(t) \odot f^*(t)$. If we **take** the **transform** of both **sides**, Eq. (11.81) then becomes

$$\mathcal{F}\{c_{ff}(\tau)\} = |F(\omega)|^2. \qquad (11.83)$$

[redacted] a form of the *Wiener–Khintchine theorem.* It allows [redacted]termination of the spectrum by way of the [redacted]orrelation of the generating function. The [redacted] of $c_{ff}(\tau)$ **applies when the function has finite** [redacted]ergy. **When it doesn't, things will have to be changed** [redacted]htly. **The integral can also be restated as**

$$c_{ff}(\tau) = \int_{-\infty}^{+\infty} f(t)f^*(t-\tau)\,dt \qquad (11.84)$$

[redacted]ple change of variable ($t + \tau$ to t). Similarly, the [redacted]**orrelation** of the functions $f(t)$ and $h(t)$ is [redacted]

$$c_{fh}(\tau) = \int_{-\infty}^{+\infty} f^*(t)h(t+\tau)\,dt. \qquad (11.85)$$

[redacted]**lation** analysis is essentially a means for comparing [redacted] signals in order to determine the degree of [redacted]ty between them. In autocorrelation the original [redacted] is displaced in time by an amount τ, the product [redacted] displaced and undisplaced versions is formed, [redacted] area under that product (corresponding to the [redacted] of overlap) is computed by means of the integral. [redacted]**ocorrelation** function, $c_{ff}(\tau)$, provides the result [redacted] obtained in such a process for all values of [redacted]e reason for doing such a thing, for example, is [redacted]nal from a background of random noise. [redacted]see how the business works step by step, let's take the [redacted]**utocorrelation** of a simple function, such as [redacted]$(\omega t + \varepsilon)$, shown in Fig. 11.37. In each part of the [redacted] the function is shifted by a value of τ, the [redacted] $f(t) \cdot f(t+\tau)$ is formed, and then the area under [redacted]product function is computed and plotted in part [redacted]otice that the process is indifferent to the value of [redacted] final result is $c_{ff}(\tau) = \frac{1}{2}A^2 \cos \omega\tau$, where this func[redacted]**folds** through one cycle as τ goes through 2π, [redacted] the same frequency as $f(t)$. Accordingly, if we [redacted] process for generating the autocorrelation, we [redacted]**construct** from that both the original amplitude [redacted] angular frequency ω.

[redacted]**uming** the functions to be real, we can rewrite [redacted]

$$c_{fh}(\tau) = \int_{-\infty}^{+\infty} f(t)h(t+\tau)\,dt, \qquad (11.86)$$

[redacted] is obviously similar to the expression for the

convolution of $f(t)$ and $h(t)$. Equation (11.86) is written symbolically as $c_{fh}(\tau) = f(t) \odot h(t)$. Indeed, if either $f(t)$ or $h(t)$ is even, then $f(t) \circledast h(t) = f(t) \odot h(t)$, as we shall see by example presently. Recall that the convolution flips one of the functions over and then sums up the overlap area (Fig. 11.21), that is, the area under the product curve. In contrast, the correlation sums up the overlap without flipping the function, and thus if the function is even, $f(t) = f(-t)$, it isn't changed by being flipped (or folded about the symmetry axis), and the two integrands are identical. For this to obtain, either function must be even, since $f(t) \circledast h(t) = h(t) \circledast f(t)$. The autocorrelation of a square pulse is therefore equal to the convolution of the pulse with itself, which yields a triangular signal, as in Fig. 11.24. This same conclusion follows from Eq. (11.83) and Fig. 11.26. The transform of a square pulse is a sinc function, so that the power spectrum varies as $\text{sinc}^2 u$. The inverse transform of $|F(\omega)|^2$, that is, $\mathcal{F}^{-1}\{\text{sinc}^2 u\}$, is $c_{ff}(\tau)$, which as we have seen, is again a triangular pulse (Fig. 11.38).

It is clearly possible for a function to have infinite energy (11.76) over an integration ranging from $-\infty$ to $+\infty$ and yet still have a finite *average power*

$$\lim_{T\to\infty} \frac{1}{2T}\int_{-T}^{+T} |f(t)|^2\,dt.$$

Accordingly, we will define a correlation that is divided by the integration interval:

$$C_{fh}(\tau) = \lim_{T\to\infty} \frac{1}{2T}\int_{-T}^{+T} f(t)h(t+\tau)\,dt. \qquad (11.87)$$

For example, if $f(t) = A$ (i.e., a constant), its autocorrelation

$$C_{ff}(\tau) = \lim_{T\to\infty} \frac{1}{2T}\int_{-T}^{+T} (A)(A)\,dt = A^2,$$

and the power spectrum, which is the transform of the autocorrelation, becomes

$$\mathcal{F}\{C_{ff}(\tau)\} = A^2 2\pi\delta(\omega),$$

a single impulse at the origin ($\omega = 0$), which is sometimes referred to as a *dc*-term. Notice that $C_{fh}(\tau)$ can be thought of as the time average of a product of two functions, one of which is shifted by an interval τ. In the next chapter, expressions of the form $\langle f^*(t)h(t+\tau)\rangle$

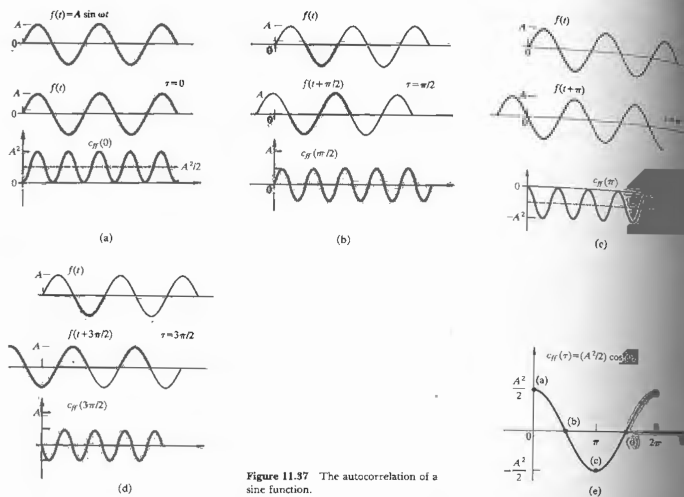


Figure 11.37 The autocorrelation of a sine function.

arise as coherence functions relating electric fields. They are also quite useful in the analysis of noise problems, for example, film grain noise.

We can obviously reconstruct a function from its transform, but once the transform is squared, as in Eq. (11.83), we lose information about the signs of the frequency contributions, that is, their relative phases. In the same way, the autocorrelation of a function contains no phase information and is not unique. To see this more clearly, imagine we have a number of harmonic functions of different amplitude and frequency. If their relative phases are altered, the resultant function changes, as does its transform [illegible] cases the amount of energy available at any [illegible] must be constant. Thus, whatever the form of [illegible] tant profile, its autocorrelation is unaltered. [illegible] is left as a problem to show analytically that [illegible] $A \sin(\omega t + \varepsilon)$, $C_{ff}(\tau) = (A^2/2)\cos\omega\tau$, which [illegible] loss of phase information.

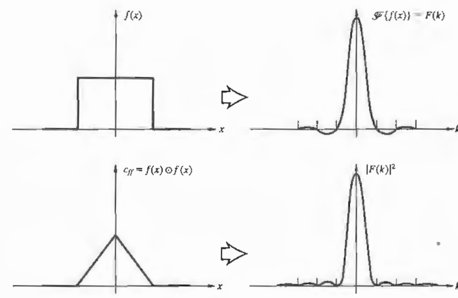
Figure 11.39 shows a means of optically [illegible] two two-dimensional spatial functions. Each of these signals is represented as a point-by-point variation in the irradiance transmission property of a pho[illegible] transparency (T_1 and T_2). For relatively sim[illegible] screens with appropriate apertures could serve [illegible] of transparencies (e.g., for square pulses).* The [illegible]ce at any point P on the image is due to a [illegible]ed bundle of parallel rays that has traversed both [illegible]parencies. The coordinates of P, $(\theta f, \varphi f)$, are fixed [illegible] orientation of the ray bundle, that is, the angles [illegible]. If the transparencies are identical, a ray passing [illegible] any point (x, y) on the first film with a transmittance $g(x, y)$ will pass through a corresponding point [illegible] $y + Y)$ on the second film where the transmittance is $g(x + X, y + Y)$. The shifts in coordinate are [illegible] $X = \ell\theta$ and $Y = \ell\varphi$, where ℓ is the separation [illegible] the transparencies. The irradiance at P is there[illegible] proportional to the autocorrelation of $g(x, y)$, that is,

$$[illegible]_{ff}(X, Y) = \iint_{-\infty}^{+\infty} g(x, y)g(x + X, y + Z)\,dx\,dy, \tag{11.88}$$

[illegible]ntire flux-density pattern is called a *correlogram*. [illegible] transparencies are different, the image is of course representative of the cross-correlation of the functions. Similarly, if one of the transparencies is rotated by 180° with respect to the other, the convolution can be obtained (see Fig. 11.25).

Before moving on, let's make sure that we actually do have a good physical feeling for the operation performed by the correlation functions. Accordingly, sup-

[illegible] The square of the Fourier [illegible] of the rectangular pulse $f(x)$ (i.e., [illegible] the Fourier transform of the [illegible] of $f(x)$).



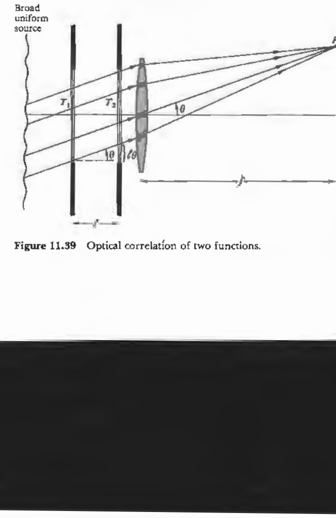


Figure 11.39 Optical correlation of two functions.

* [illegible] Kovasznay and A. Arman, *Rev. Sci. Instr.* **28**, 793 (1958), [illegible] Jr., *J. Opt. Soc. Am.* **52**, 454 (1962).

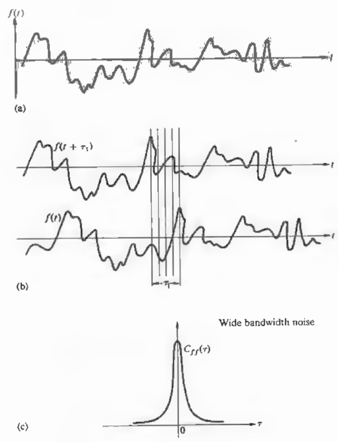


Figure 11.40 A signal $f(t)$ and its autocorrelation.

pose we have a random noise-like signal (e.g., [illegible] ing irradiance at a point in space or a tim[illegible] voltage or electric field), as in Fig. 11.4[illegible] autocorrelation of $f(t)$ in effect compares the [illegible] with its value at some other time, $f(t+\tau)$. For examp[illegible] with $\tau = 0$ the integral runs along the signal [illegible] summing up and averaging the product of [illegible] $f(t+\tau)$; in this case it's simply $f^2(t)$. Since at [illegible] of t, $f^2(t)$ is positive, $C_{ff}(0)$ will be a comparati[illegible] number. On the other hand, when the noise is [illegible] with itself shifted by an amount $+\tau_1$, $C_{ff}($[illegible] somewhat reduced. There will be points in [illegible] $f(t)f(t+\tau_1)$ is positive and other points where [illegible] negative, so that the value of the integral drops [illegible] 11.40(b)]. In other words, by shifting the sig[illegible] respect to itself, we have reduced the point-b[illegible] similarity that previously ($\tau = 0$) occurred at any [illegible] As this shift τ increases, what little correlation [illegible] quickly vanishes, as depicted in Fig. 11.40(c). [illegible] can assume from the fact that the autocorrelation [illegible] the power spectrum form a Fourier transform pai[illegible] that the broader the frequency bandwidth of [illegible] the narrower the autocorrelation. Thus for [illegible] width noise even a slight shift markedly redu[illegible] similarity between $f(t)$ and $f(t+\tau)$. Furthermore [illegible] signal comprises a random distribution of re[illegible] pulses, we can see intuitively that the similarity [illegible] of earlier persists for a time commensurate [illegible] width of the pulses. The wider (in time) the p[illegible] the more slowly the correlation decreases as τ [illegible] But this is equivalent to saying that reducing [illegible] bandwidth broadens $C_{ff}(\tau)$. All of this is in keepin[illegible] our previous observation that the autocorrelation [illegible] out any phase information, which in this case would

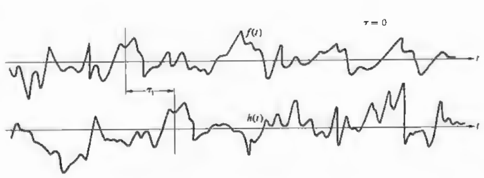
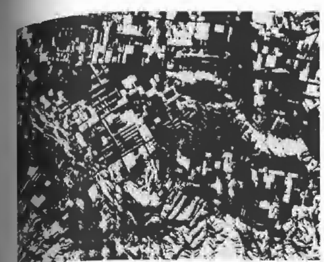
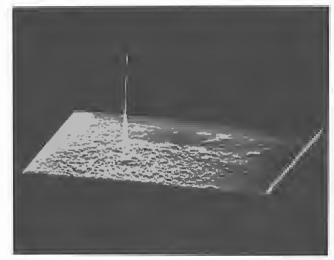


Figure 11.41 The cross-correl[illegible] of $f(t)$ and $h(t)$.


(a)


(c)


(b)

Figure 11.42 An example of optical pattern recognition. (a) Input signal, (b) reference data, (c) correlation pattern. (Reprinted with permission from the November 1980 issue of *Electro-Optical Systems Design*. David Casasent.)

[illegible]pond to the locations in time of the random pul- [illegible]early, $C_{ff}(\tau)$ shouldn't be affected by the position [illegible] pulses along t.

[illegible]very much the same way, the cross-correlation is a measure of the similarity between two different [illegible]orms, $f(t)$ and $h(t)$, as a function of the relative [illegible]ift τ. Unlike the autocorrelation, there is now [illegible]g special about $\tau = 0$. Once again, for each value [illegible]e average the product $f(t)h(t+\tau)$ to get $C_{fh}(\tau)$ [illegible] (11.87). For the functions shown in Fig. 11.41, [illegible] would have a positive peak at $\tau = \tau_1$.

[illegible]e the 1960s a great deal of effort has gone into [illegible] development of optical processors that can rapidly [illegible]e pictorial data. The potential uses range from [illegible]aring fingerprints to scanning documents for [illegible] or phrases; from screening aerial reconnaissance [illegible]es to creating terrain-following guidance systems [illegible]siles. An example of this kind of *optical pattern* [illegible]*ion*, accomplished using correlation techniques, [illegible] in Fig. 11.42. The input signal $f(x, y)$ depicted in photograph (a) is a broad view of some region that is to be searched for a particular group of structures [photograph (b)] isolated as the reference signal $h(x, y)$. Of course, that small frame is easy enough to scan directly by eye, so to make things more realistic, imagine the input to be a few hundred feet of reconnaissance film. The result of optically correlating these two signals is displayed in photograph (c), where we immediately see, from the correlation peak (i.e., the spike of light), that indeed the desired group of structures is in the input picture, and moreover its location is marked by the peak.

11.3.5 Transfer Functions

i) An Introduction to the Concepts

Until recent times, the traditional means of determining the quality of an optical element or system of elements was to evaluate its limit of resolution. The greater the

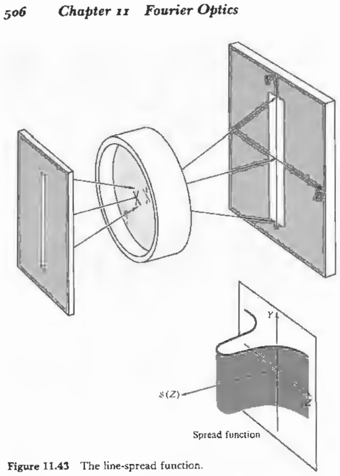


Figure 11.43 The line-spread function.

resolution, the better the system was presumed to be. In the spirit of this approach one might train an optical system on a resolution target consisting, for instance, of a series of alternating light and dark parallel rectangular bars. We have already seen that an object point is imaged as a smear of light described by the point-spread function $\mathcal{S}(Y, Z)$, as in Fig. 11.18. Under incoherent illumination these elementary flux-density patterns overlap and add linearly to create the final image. The one-dimensional counterpart is the *line-spread function* $\mathcal{S}(Z)$, which corresponds to the flux-density distribution across the image of a geometrical line source having infinitesimal width (Fig. 11.43). Because even an ideally perfect system is limited by diffraction effects, the image of a resolution target (Fig. 11.44) will be somewhat blurred (see Fig. 11.20). Thus, as the wi[illegible] of the bars on the target is made narrower, a limit [illegible] be reached where the fine-line structure (ak[illegible] *Ronchi ruling*) will no longer be discernible—[illegible] is the resolution limit of the system. We can [illegible] as a spatial frequency cutoff where each bright[illegible] bar pair constitutes one cycle on the object (a [illegible] measure of which is *line pairs per mm*). An [illegible] analogy which underscores the shortcomi[illegible] approach would be to evaluate a high-fide[illegible] system simply on the basis of its upper-freque[illegible] The limitations of this scheme became quite [illegible] with the introduction of detectors such as the pl[illegible] bicon, image orthicon, and vidicon. These tubes [illegible] a relatively coarse scanning raster, which fixes th[illegible] ution limit of the lens-tube system at a fairly low [illegible] frequency. Accordingly, it would seem reasona[illegible] design the optics preceding such detectors so that it provided the most contrast over this limited fre[illegible] range. It would clearly be unnecessary and perhaps [illegible] we shall see, even detrimental to select a mating l[illegible] system merely because of its own high limit of [illegible] ution. Evidently it would be more helpful to hav[illegible] figure of merit applicable to the entire operati[illegible] frequency range.

We have already represented the object as a[illegible] of point sources, each of which is imaged as [illegible] spread function by the optical system, and that patch

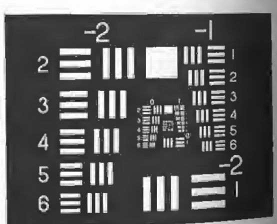
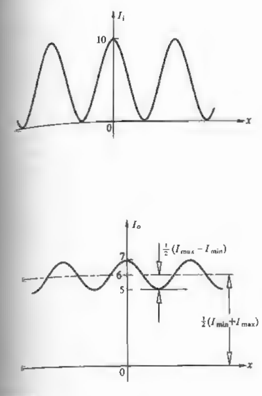


Figure 11.44 A bar target resolution chart.



[illegible] 11.45 The irradiance into and out of a system.

of light is then convolved into the image. Now we [illegible] the problem of image analysis from a different [illegible]related perspective. Consider the object to be [illegible]urce of an input lightwave, which itself is made [illegible] plane waves. These travel off in specific directions [illegible]nding, via Eqs. 11.64 and 11.65, to particular [illegible] of spatial frequency. How does the system modify [illegible]itude and phase of each plane wave as it trans- [illegible] from object to image?

[illegible]hly useful parameter in evaluating the perform- [illegible] a system is the **contrast** or **modulation**, defined by

$$\text{Modulation} = \frac{I_{max} - I_{min}}{I_{max} + I_{min}}. \tag{11.89}$$

[illegible]ple example, suppose the input is a cosinusoidal [illegible] distribution arising from an incoherently illuminated transparency (Fig. 11.45). Here the output is also a cosine, but one that's somewhat altered. The modulation, which corresponds to the amount the function varies about its mean value divided by that mean value, is a measure of how readily the fluctuations will be discernible against the dc background. For the input the modulation is a maximum of 1.0, but the output modulation is only 0.17. This is only the response of our hypothetical system to essentially one spatial frequency input—it would be nice to know what it does at all such frequencies. Moreover, here the input modulation was 1.0, and the comparison with the output was easy. In general it will not be 1.0, and so we define ***the ratio of the image modulation to the object modulation at all spatial frequencies*** as the **modulation transfer function**, or MTF.

Figure 11.46 is a plot of the MTF for two hypothetical lenses. Both start off with a zero-frequency (dc) value of 1.0, and both cross the zero axis somewhere where they can no longer resolve the data at that *cutoff frequency*. Had they both been diffraction-limited lenses, that cutoff would have depended only on diffraction and, hence, on the size of the aperture. In any event, suppose one of these is to be coupled to a detector whose cutoff frequency is indicated in the diagram. Despite the fact that lens 1 has a higher limit of resolution, lens 2 would certainly provide better performance when coupled to the particular detector.

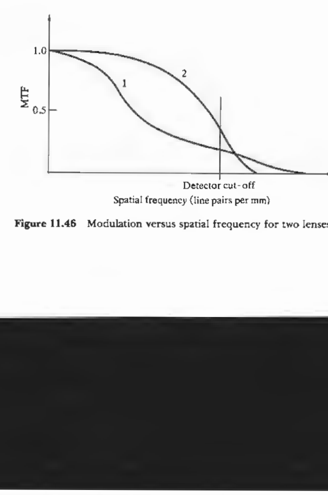


Figure 11.46 Modulation versus spatial frequency for two lenses.

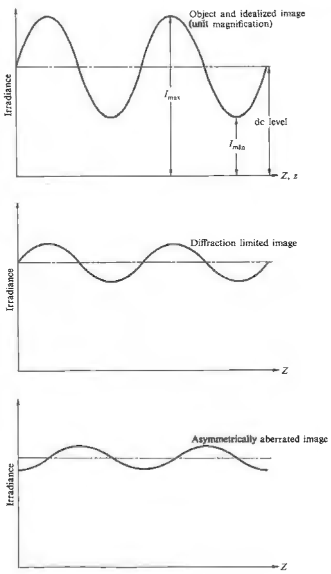
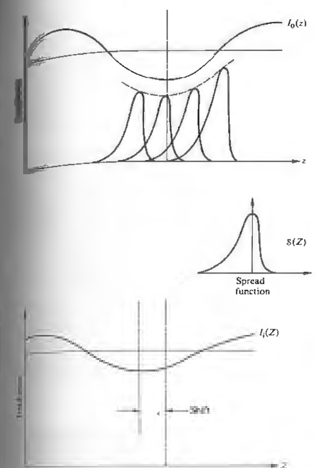


Figure 11.47 Harmonic input and resulting output.

It should be pointed out that a square bar target provides an input signal that is a series of square pulses, and the contrast in the image is actually a superposition of contrast variations due to the constituent Fourier components. Indeed, one of the key points in what is to follow is that *optical elements functioning as linear operators transform a sinusoidal input into an undistorted sinusoidal output.* Despite this, the input and out[illegible] irradiance distributions as a rule will not be identi[illegible] For example, the system's magnification affects [illegible] spatial frequency of the output (henceforth the [illegible] nification will be taken as one). Diffraction and [illegible] tions reduce the sinusoid's amplitude (contrast). [illegible] asymmetrical aberrations (e.g., coma) and poor c[illegible] ing of elements produce a shift in the position [illegible] output sinusoid corresponding to the introductio[illegible] phase shift. This latter point, which was consid[illegible] a Fig. 11.12, can be appreciated using a diagram [illegible] of Fig. 11.47.

If the spread function is symmetrical, the image irradiance will be an unshifted sinusoid, whereas an asymmetrical spread function will apparently p[illegible] output over a bit, as in Fig. 11.48. In either case, [illegible] *less of the form of the spread function, the image is h[illegible] if the object is harmonic.* Consequently, if we [illegible] object as being composed of Fourier components, the manner in which these individual harmonic com- ponents are transformed by the optical system into the corresponding harmonic constituents of the image is the quintessential feature of the process. The function that performs this service is known as the **op[illegible] fer function**, or OTF. It is a spatial **freque[illegible]** dent complex quantity whose modulus is the [illegible] *transfer function* (MTF) and whose phase, [illegible] enough, is the **phase transfer function** ([illegible] former is a measure of the reduction in contrast from object to image over the spectrum. The latter rep[illegible] the commensurate relative phase shift. Phase s[illegible] centered optical systems occur only off-axis, and often the PTF is of less interest than the MTF. Even so, each application of the transfer function must be studied carefully; there are situations wherein the PTF plays a crucial role. In point of fact, the MTF has become a widely used means of specifying the perfo[illegible] sorts of elements and systems, from lenses, magnetic tape, and films to telescopes, the atmosphere, a[illegible] eye, to mention but a few. Moreover, it has the [illegible] tage that if the MTFs for the individual independ[illegible] components in a system are known, the total MTF [illegible] often simply their product. This is inappli[illegible] to the cascading of lenses, since the aberrations [illegible]e lens can compensate for those of another lens in tandem,



[illegible]e 11.48 Harmonic input and output with an asymmetric spread [illegible]tion.

[illegible] and they are therefore not independent. Thus [illegible]hotograph an object having a modulation of 0.3 [illegible]ycles per mm, using a camera whose lens at the [illegible]priate setting has an MTF of 0.5 at 30 c/mm and [illegible] such as Tri-X with an MTF of 0.4 at 30 c/mm, [illegible] modulation will be $0.3 \times 0.5 \times 0.4 = 0.06$.

[illegible]ally, the whole idea of treating film as a noise-free linear [illegible] somewhat suspect. For further reading see J. B. De Velis [illegible]B. Parrent, Jr., "Transfer Function for Cascaded Optical [illegible]" *J. Opt. Soc. Am.* **57**, 1486 (1967).

(ii) A More Formal Discussion

We saw in Eq. (11.51) that the image (under the conditions of space invariance and incoherence) could be expressed as the convolution of the object irradiance and the point-spread function, in other words,

$$I_i(Y, Z) = I_0(y, z) \circledast S(y, z). \tag{11.90}$$

The corresponding statement in the spatial frequency domain is obtained by a Fourier transform, namely,

$$\mathscr{F}\{I_i(Y, Z)\} = \mathscr{F}\{I_0(y, z)\} \cdot \mathscr{F}\{S(y, z)\}, \tag{11.91}$$

where use was made of the convolution theorem (11.53). This says that *the frequency spectrum of the image irradiance distribution equals the product of the frequency spectrum of the object irradiance distribution and the transform of the spread function* (Fig. 11.49). Thus, it is multiplication by $\mathscr{F}\{S(y, z)\}$ that produces the alteration in the frequency spectrum of the object, converting it into that of the image spectrum. In other words, it is $\mathscr{F}\{S(y, z)\}$ that, in effect, transfers the object spectrum into the image spectrum. This is just the service performed by the OTF, and indeed we shall define the **unnormalized OTF** as

$$\mathscr{T}(k_Y, k_Z) = \mathscr{F}\{S(y, z)\}, \tag{11.92}$$

The modulus of $\mathscr{T}(k_Y, k_Z)$ will effect a change in the amplitudes of the various frequency components of the object spectrum, while its phase will, of course, appropriately alter the phase of these components to yield $\mathscr{F}\{I_i(Y, Z)\}$. Bear in mind that in the right-hand side of Eq. (11.90) the only quantity dependent on the actual optical system is $S(y, z)$, so it's not surprising that the spread function is the spatial counterpart of the OTF.

Let's now verify the statement made earlier that a harmonic input transforms into a somewhat altered harmonic output. To that end, suppose

$$I_0(z) = 1 + a \cos(k_Z z + \varepsilon), \tag{11.93}$$

where for simplicity's sake, we'll again use a one-dimensional distribution. The 1 is a dc bias, which makes sure the irradiance doesn't take on any unphysical negative values. Insofar as $f \circledast h = h \circledast f$, it will be more convenient here to use

$$I_i(Z) = S(z) \circledast I_0(z),$$

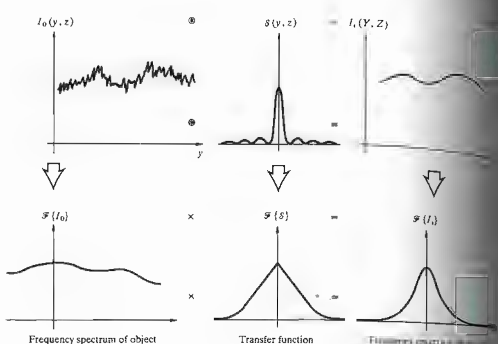


Figure 11.49 The relationships between the object and image spectra by way of the OTF, and the object and image irradiances by way of the point-spread function—all in incoherent illumination.

and so

$$I_i(Z) = \int_{-\infty}^{+\infty} \{1 + a\cos[k_Z(Z - z) + \varepsilon]\} S(z)\, dz.$$

Expanding out the cosine, we obtain

$$I_i(Z) = \int_{-\infty}^{+\infty} S(z)\, dz + a\cos(k_Z Z + \varepsilon) \int_{-\infty}^{+\infty} \cos k_Z z\, S(z)\, dz$$

$$+ a \sin(k_Z Z + \varepsilon) \int_{-\infty}^{+\infty} \sin k_Z z\, S(z)\, dz.$$

Referring back to Eq. (7.57), we recognize the second and third integrals as the Fourier cosine and sine transforms of $S(z)$, respectively, that is to say, $\mathscr{F}_c\{S(z)\}$ and $\mathscr{F}_s\{S(z)\}$. Hence

$$I_i(z) = \int_{-\infty}^{+\infty} S(z)\, dz + \mathscr{F}_c\{S(z)\} a \cos(k_Z Z + \varepsilon)$$

$$+ \mathscr{F}_s\{S(z)\} a \sin(k_Z Z + \varepsilon). \qquad (11.94)$$

Recall that the complex transform we've become so used to working with was defined such that

$$\mathscr{F}\{f(z)\} = \mathscr{F}_c\{f(z)\} + i\mathscr{F}_s\{f(z)\} \qquad (11.95)$$

or

$$F(k_Z) = A(k_Z) + iB(k_Z). \qquad [illegible]$$

In addition,

$$\mathscr{F}\{f(z)\} = |F(k_Z)| e^{i\varphi(k_Z)} = |F(k_Z)|[\cos\varphi + i \text{[illegible]}$$

where

$$|F(k_Z)| = [A^2(k_Z) + B^2(k_Z)]^{1/2} \qquad (11.[illegible])$$

and

$$\varphi(k) = \tan^{-1}\frac{B(k_Z)}{A(k_Z)}.$$

In precisely the same way, we apply this to [illegible] writing it as

$$\mathscr{F}\{S(z)\} = \mathscr{T}(k_Z) = \mathscr{M}(k_Z) e^{i\Phi(k_Z)},$$

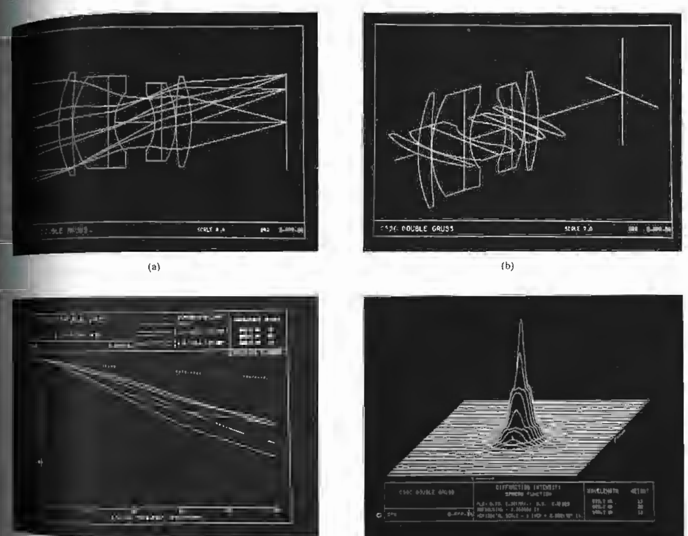
where $\mathscr{M}(k_Z)$ and $\Phi(k_Z)$ are the unnormalized [illegible] the PTF, respectively. It is left as a pro[illegible] that Eq. (11.94) can be recast as

$$I_i(Z) = \int_{-\infty}^{+\infty} S(z)\, dz + \text{[illegible]}$$

Notice that this is a function of the same form as the [illegible] signal (11.93), $I_0(z)$, which is just what we set out to determine. If the line-spread function is symmetrical (i.e., even), $\mathscr{F}_s\{S(z)\} = 0$, $\mathscr{M}(k_Z) = \mathscr{F}_c\{S(z)\}$, and $\Phi(k_Z) =$ [illegible] there is no phase shift, as was pointed out in the previous [illegible]. For an asymmetric (odd) spread function, [illegible] is nonzero, as is the PTF.

It has now become customary practice to define a set of ***normalized transfer functions*** by dividing $\mathscr{T}(k_Z)$ by its zero spatial frequency value, that is, $\mathscr{T}(0) = \int_{-\infty}^{+\infty} S(z)\, dz$. The normalized spread function becomes

$$S_n(z) = \frac{S(z)}{\int_{-\infty}^{+\infty} S(z)\, dz}, \qquad (11.100)$$



(a) (b) (c) (d)

Figure 11.[illegible] An example of the kind of lens design information [illegible] techniques. (Photos courtesy Optical Research [illegible].)

while the **normalized OTF** is

$$T(k_Z) = \frac{\mathcal{F}\{\mathcal{S}(z)\}}{\int_{-\infty}^{+\infty} \mathcal{S}(z)\,dz} = \mathcal{F}\{\mathcal{S}_n(z)\}, \tag{11.101}$$

or in two dimensions

$$T(k_Y, k_Z) = M(k_Y, k_Z)e^{i\Phi(k_Y, k_Z)}, \tag{11.102}$$

where $M(k_Y, k_Z) = \mathcal{M}(k_Y, k_Z)/\mathcal{T}(0,0)$. Therefore $I_i(Z)$ in Eq. (11.99) would then be proportional to

$$1 + aM(k_Z)\cos[k_Z Z + \varepsilon - \Phi(k_Z)].$$

The image modulation (11.89) becomes $aM(k_Z)$, the object modulation (11.93) is a, and the ratio is, as expected, the normalized MTF $= M(k_Z)$.

This discussion is really only an introductory one designed more as a strong foundation than a complete structure. There are many other insights to be explored, such as the relationship between the autocorrelation of the pupil function and the OTF, and from there, the means of computing and measuring transfer functions (Fig. 11.50)—but for this the reader is directed to the literature.†

PROBLEMS

11.1 Determine the Fourier transform of the function

$$E(x) = \begin{cases} E_0 \sin k_p x, & |x| < L \\ 0, & |x| > L. \end{cases}$$

Make a sketch of $\mathcal{F}\{E(x)\}$. Discuss its relationship to Fig. 11.11.

† See the series of articles "The Evolution of the Transfer Function," by F. Abbott, beginning in March 1970 in *Optical Spectra;* the articles "Physical Optics Notebook," by G. B. Parrent, Jr., and B. J. Thompson, beginning in December 1964, in the *S.P.I.E. Journal*, Vol. 3; or "Image Structure and Transfer," by K. Sayanagi, 1967, available from the Institute of Optics, University of Rochester. A number of books are worth consulting for practical emphasis, e.g. *Modern Optics*, by E. Brown; *Modern Optical Engineering*, by W. Smith; and *Applied Optics*, by L. Levi. In all of these, be careful of the sign convention in the transforms.

11.2* Determine the Fourier transform of

$$f(x) = \begin{cases} \sin^2 k_p x, & |x| < L \\ 0, & |x| > L. \end{cases}$$

Make a sketch of it.

11.3 Determine the Fourier transform of

$$f(t) = \begin{cases} \cos^2 \omega_p t, & |t| < T \\ 0, & |t| > T. \end{cases}$$

Make a sketch of $F(\omega)$, then sketch its limiting form as $T \to \pm\infty$.

11.4* Show that $\mathcal{F}\{1\} = 2\pi\delta(k)$.

11.5* Determine the Fourier transform of the function $f(x) = A \cos k_0 x$.

11.6 Given that $\mathcal{F}\{f(x)\} = F(k)$ and $\mathcal{F}\{h(x)\}$ = … if a and b are constants, determine $\mathcal{F}\{af(x) + b$…

11.7* Figure 11.51 shows two periodic fun… and $h(x)$, which are to be added to produce… $g(x)$, then draw diagrams of the real and… frequency spectra, as well as the amplitude spe… for each of the three functions.

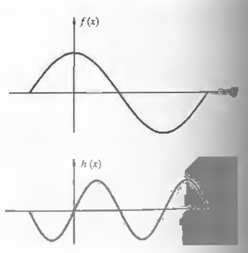


Figure 11.51

…ompute the Fourier transform of the triangular …own in Fig. 11.52. Make a sketch of your answer, …all the pertinent values on the curve.

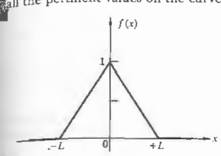


Figure 11.52

11.9* Given that $\mathcal{F}\{f(x)\} = F(k)$, introduce a constant …g factor $1/a$ and determine the Fourier transform …$/a)$. Show that the transform of $f(-x)$ is $F(-k)$.

11.10* Show that the Fourier transform of the trans… $\mathcal{F}\{F(k)\}$, equals $2\pi f(-x)$, and that this is not the …e transform of the transform, which equals $f(x)$. …problem was suggested by Mr. D. Chapman while …dent at the University of Ottawa.

11.11* The rectangular function is often defined as

$$\text{rect}\left|\frac{x - x_0}{a}\right| = \begin{cases} 0, & |(x - x_0)/a| > \frac{1}{2} \\ \frac{1}{2}, & |(x - x_0)/a| = \frac{1}{2} \\ 1, & |(x - x_0)/a| < \frac{1}{2}, \end{cases}$$

where it is set equal to $\frac{1}{2}$ at the discontinuities (Fig. 11.53). Determine the Fourier transform of

$$f(x) = \text{rect}\left|\frac{x - x_0}{a}\right|.$$

Notice that this is just a rectangular pulse, like that in Fig. 11.1(b), shifted a distance x_0 from the origin.

11.12* With the last two problems in mind, show that …$\text{sinc}(\frac{1}{2}x)\} = \text{rect}(k)$, starting with the knowl…at $\mathcal{F}\{\text{rect}(x)\} = \text{sinc}(\frac{1}{2}k)$, in other words, Eq. …with $L = a$, where $a = 1$.

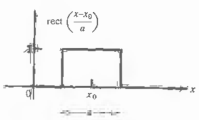


Figure 11.53

11.13* Utilizing Eq. (11.38), show that $\mathcal{F}^{-1}\{F\{f(x)\}\} = f(x)$.

11.14* Given $\mathcal{F}\{f(x)\}$, show that $\mathcal{F}\{f(x - x_0)\}$ differs from it only by a linear phase factor.

11.15 Prove that $f \circledast h = h \circledast f$ directly. Now do it using the convolution theorem.

11.16* **Suppose we have two functions, $f(x, y)$ and $h(x, y)$, where both have a value of 1 over a square region in the xy-plane and are zero everywhere else (Fig. 11.54). If $g(X, Y)$ is their convolution, make a plot of $g(X, 0)$.**

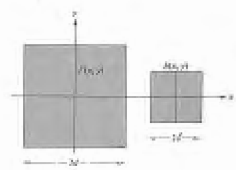


Figure 11.54

11.17 Referring to the previous problem, justify the fact that the convolution is zero for $|X| \geq d + \ell$ when h is viewed as a spread function.

11.18* Use the method illustrated in Fig. 11.23 to convolve the two functions depicted in Fig. 11.55.

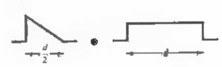


Figure 11.55

11.19 Given that $f(x) \circledast h(x) = g(X)$, show that after shifting one of the functions an amount x_0, we get $f(x - x_0) \circledast h(x) = g(X - x_0)$.

11.20* Prove analytically that the convolution of any function $f(x)$ with a delta function, $\delta(x)$, generates the original function $f(X)$. You might make use of the fact that $\delta(x)$ is even.

11.21 Prove that $\delta(x - x_0) \circledast f(x) = f(X - x_0)$ and discuss the meaning of this result. Make a sketch of two appropriate functions and convolve them. Be sure to use an asymmetrical $f(x)$.

11.22* Show that $\mathscr{F}\{f(x) \cos k_0x\} = [F(k - k_0) + F(k + k_0)]/2$ and that $\mathscr{F}\{f(x) \sin k_0x\} = [F(k - k_0) - F(k + k_0)]/2i$.

11.23* Figure 11.56 shows two functions. Convolve them graphically and draw a plot of the result.

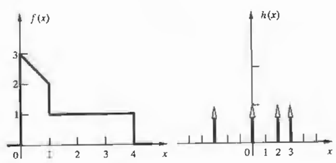


Figure 11.56

11.24 Given the function

$$f(x) = \text{rect}\left|\frac{x - a}{a}\right| + \text{rect}\left|\frac{x + a}{a}\right|$$

determine its Fourier transform. (See Proble[illegible] 11.11.)

11.25 Given the function $f(x) = \delta(x + 3) + \delta($[illegible]$) +$ $\delta(x - 5)$, convolve it with the arbitrary functio[illegible] $h(x)$.

11.26* Make a sketch of the function arisin[illegible] convolution of the two functions depicted in[illegible]

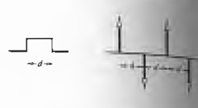


Figure 11.57

11.27* Figure 11.58 depicts a *rect* function (as [illegible] above) and a periodic *comb* function. Convolve [illegible] to get $g(x)$. Now sketch the transform of each of [illegible] functions against spatial frequency $k/2\pi =$ [illegible] your results with the convolution theorem. [illegible] relevant points on the horizontal axes in term[illegible] the zeros of the transform of $f(x)$.

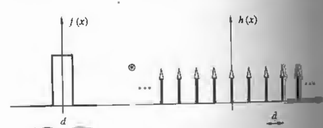


Figure 11.58

11.28 Figure 11.59 shows, in one dimension, [illegible] tric field across an illuminated aperture cons[illegible] several opaque bars forming a grating. Cons[illegible] to be created by taking the product of a per[illegible] tangular wave $h(x)$ and a unit rectangular fun[illegible] sketch the resulting electric field in the F[illegible] region.

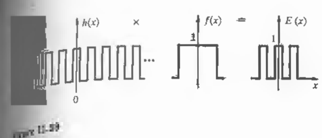


Figure 11.59

[illegible] Show (for normally incident plane waves) that [illegible] aperture has a center of symmetry (i.e., if the [illegible] function is even), then the diffracted field in [illegible]nhofer case also possesses a center of symmetry.

[illegible] Suppose a given aperture produces a Fraun[illegible]field pattern $E(Y, Z)$. Show that if the aperture's [illegible]ons are altered such that the aperture function [illegible] $\mathscr{A}(y, z)$ to $\mathscr{A}(\alpha y, \beta z)$, the newly diffracted field [illegible] given by

$$E'(Y, Z) = \frac{1}{\alpha\beta} E\left(\frac{Y}{\alpha}, \frac{Z}{\beta}\right).$$

[illegible] Show that when $f(t) = A \sin(\omega t + \varepsilon)$, $C_{ff}(\tau) =$ [illegible] $\omega\tau$, which confirms the loss of phase informa[illegible] the autocorrelation.

[illegible] Suppose we have a single slit along the y-direc[illegible] of width b where the aperture function is constant [illegible] at a value of $\mathscr{A}_0$. What is the diffracted field if [illegible] apodize the slit with a cosine function amplitude mask? In other words, we cause the aperture function to go from $\mathscr{A}_0$ at the center to 0 at $\pm b/2$ via a cosinusoidal drop-off.

11.33* Show, from the integral definitions, that $f(x) \odot g(x) = f(x) \circledast g(-x)$.

11.34* Figure 11.60 shows a transparent ring on an otherwise opaque mask. Make a rough sketch of its autocorrelation function, taking l to be the center-to-center separation against which you plot that function.

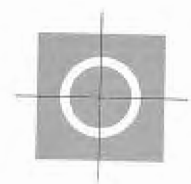


Figure 11.60

11.35* Consider the function in Fig. 11.35 as a cosine carrier multiplied by an exponential envelope. Use the frequency convolution theorem to evaluate its Fourier transform.

12 BASICS OF COHERENCE THEORY

Thus far in our discussion of phenomena involving the superposition of waves, we've restricted the treatment to that of either completely coherent or completely incoherent disturbances. This was done primarily as a mathematical convenience, since, as is quite often the case, the extremes in a physical situation are the easiest to deal with analytically. In fact, both of these limiting conditions are more conceptual idealizations than actual physical realities. There is a middle ground between these antithetic poles, which is of considerable contemporary concern—the domain of *partial coherence*. Even so, the need for extending the theoretical structure is not new; it dates back at least to the mid-1860s, when Emile Verdet demonstrated that a primary source commonly considered to be incoherent, such as the Sun, could produce observable fringes when it illuminated the closely spaced pinholes (≲0.05 mm) of Young's experiment (Section 9.3). Theoretical interest in the study of partial coherence lay dormant until it was revived in the 1930s by P. H. van Cittert and later by Fritz Zernike. And as the technology flourished, advancing from traditional light sources, which were essentially optical frequency noise generators, to the laser, a new practical impetus was given the subject. Moreover, the recent advent of individual-photon detectors has made it possible to examine related processes associated with the corpuscular aspects of the optical field.

Optical coherence theory is currently an area of active research. Thus, even though much of the excitement in the field is associated with material beyond the level of this book, we shall nonetheless introduce some of the basic ideas.

12.1 INTRODUCTION

Earlier (Section 7.10) we evolved the highly [illegible] ture of quasimonochromatic light as resemb[illegible] of randomly phased finite wavetrains (Fig. 7[illegible] a disturbance is nearly sinusoidal, alth[illegible] frequency does vary slowly (in comparison [illegible] of oscillation, 10^{15} Hz) about some mean value. Moreover, the amplitude fluctuates as well, but this [illegible] is a comparatively slow variation. The average constituent wavetrain exists roughly for a time [illegible] is the *coherence time* given by the inverse of th[illegible] bandwidth $\Delta\nu$.

It is often convenient, even if rather artificial, to divide coherence effects into two classificatio[illegible] and ***spatial****. The former relates directly to the fini[illegible] of the source, the latter to its finite extent in spa[illegible]*

To be sure, if the light were monochro[illegible] would be zero, and Δt_c infinite, but this [illegible] unattainable. However, over an interval much shorter than Δt_c an actual wave behaves essentially as [illegible] monochromatic. In effect the coherence time [illegible] *poral interval over which we can reasonably predic[illegible] of the lightwave at a given point in space.* This the[illegible] is meant by **temporal coherence**; namely, if Δt_c [illegible] the wave has a high degree of temporal cohere[illegible] vice versa.

The same characteristic can be viewed somewhat differently. To that end, imagine that we have two separate points P_1 and P_2 lying on the same radius

[illegible] from a quasimonochromatic point source. If the [illegible]ence length, $c\Delta t_c$, is much larger than the distance [illegible]etween P_1 and P_2, then a single wavetrain can [illegible]extend over the whole separation. The distur[illegible]at P_1 would then be highly correlated with the [illegible]bance occurring at P_2. On the other hand, if this [illegible]udinal separation were much greater than the [illegible]ence length, many wavetrains, each with an unre[illegible] phase, would span the gap r_{12}. In that case, the [illegible]bances at the two points in space would be [illegible]pendent at any given time. The degree to which a [illegible]elation exists is sometimes spoken of alternatively [illegible] the amount of *longitudinal coherence*. Whether we [illegible]ink in terms of coherence time (Δt_c) or coherence [illegible]th ($c\Delta t_c$), the effect still arises from the finite band[illegible]th of the source.

[illegible]he idea of **spatial coherence** is most often used to [illegible]be effects arising from the finite spatial extent of [illegible]dinary light sources. Suppose then that we have a [illegible]ssical broad monochromatic source. Two point [illegible]lators on it, separated by a lateral distance that is [illegible]compared with λ, will presumably behave quite [illegible]**ndently.** That is to say, there will be a lack of [illegible]**tion** existing between the phases of the two emit[illegible]**urbances.** Extended sources of this sort are gen[illegible] [illegible] to as incoherent, but this description is [illegible]ewhat misleading, as we shall see in a moment. [illegible] one is interested not so much in what is happen[illegible]on the source itself but rather in what is occurring [illegible]in some distant region of the radiation field. The [illegible]tion to be answered is really: How do the nature [illegible]e source and the geometrical configuration of the [illegible]uation relate to the resulting phase correlation [illegible]ween two laterally spaced points in the light field? [illegible] brings to mind Young's experiment, in which a [illegible] monochromatic source S illuminates two pin[illegible] an opaque screen. These in turn serve as secon[illegible]ources, S_1 and S_2, to generate a fringe pattern on [illegible] distant plane of observation, Σ_o (Fig. 9.5). We [illegible]y know that if S is an idealized point source, the [illegible]ets issuing from any set of apertures S_1 and S_2 on [illegible]ll maintain a constant relative phase; they will be [illegible]ely correlated and therefore coherent. A well-[illegible]d array of stable fringes results, and the field is [illegible]lly coherent. At the other extreme, if the pinholes

are illuminated by separate thermal sources (even with narrow bandwidths), no correlation exists; no fringes will be observable with existing detectors, and the fields at S_1 and S_2 are said to be incoherent. The generation of interference fringes is then seemingly a very convenient measure of the coherence.

We can gain some important insights into the process by returning to the general considerations of Section 9.1 and Eq. (9.7). Imagine two scalar waves $E_1(t)$ and $E_2(t)$ traveling toward, and overlapping at, point P, as in Fig. 9.2. If the light is monochromatic and both beams have the same frequency, the resulting interference pattern will depend on their relative phase at P. If the waves are in phase, $E_1(t)E_2(t)$ will be positive for all t as the fields rise and fall in together. Hence, $I_{12} = 2\langle E_1(t)E_2(t)\rangle$ will be a nonzero positive number, and the net irradiance I will exceed $I_1 + I_2$. Similarly, if the lightwaves are out of phase, one will be positive when the other is negative, with the result that the product $E_1(t)E_2(t)$ will always be negative, yielding a negative interference term I_{12}, and the result that I will be less than $I_1 + I_2$. In both these cases, the product of the two fields moment by moment is certainly oscillatory, but it is nonetheless either totally positive or negative and so averages in time to a nonzero value.

Now consider the more realistic case in which the two lightwaves are quasimonochromatic, resembling the disturbance in Fig. 7.21, which has a finite coherence length. If we again form the product $E_1(t)E_2(t)$, we see in Fig. 12.1(c) that it varies in time, drifting from negative to positive values. Accordingly, the interference term $\langle E_1(t)E_2(t)\rangle$, which is averaged over a relatively long interval compared with the periods of the waves, will be quite small, if not zero: $I \approx I_1 + I_2$. In other words, insofar as the two lightwaves are uncorrelated in their risings and fallings, they will not preserve a constant phase relationship, they will not be completely coherent, and they will not produce the ideal high-contrast interference pattern considered in Chapter 9. We should be reminded here of Eq. (11.87), which expresses the cross-correlation of two functions—with $\tau = 0$. Indeed, if P is shifted in space (e.g., along the plane of observation in Young's experiment), thereby introducing a relative time delay of τ between the two lightwaves, then the interference term becomes

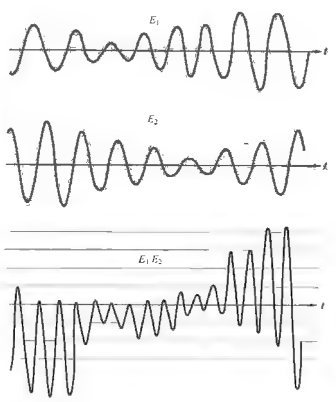
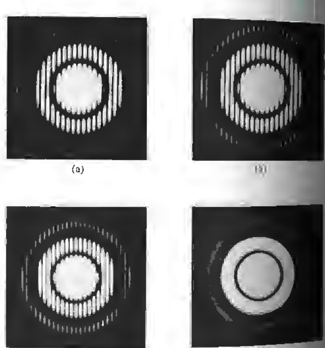


Figure 12.1 Two overlapping E-fields and their product as functions of time. The more uncorrelated the fields, the more nearly the product will average to zero.

$\langle E_1(t)E_2(t+\tau)\rangle$, which is the cross-correlation. Coherence is correlation, a point that will be made formally in Section 12.3.

Young's experiment can also be used to demonstrate temporal coherence effects with a finite bandwidth source. Figure 12.2(a) shows the fringe patterns obtained with two small circular apertures illuminated by a He–Ne laser. Before the photograph in Fig. 12.2(b) was taken, an optically flat piece of glass, 0.5 mm thick, was positioned over one of the pinholes (say S_1). No change in the form of the pattern (other than a shift in its location) is evident, because the coherence length of the laser light far exceeds the optical path-length difference introduced by the glass. On the other hand, when the same experiment is repeated using the light from a collimated mercury arc [(c) and (d) in Fig. 12.2] the fringes disappear. Here the coherence length is short enough and the additional optical path-length difference of the glass is long enough for [illegible] wavetrains from the two apertures to arrive at [illegible] of observation. In other words, of any two [illegible] wavetrains that leave S_1 and S_2, the one from [illegible] delayed so long in the glass that it falls completely behind the other and arrives at Σ_o to meet a totally different wavetrain from S_2.

In both cases of temporal and spatial coherence we are really concerned with one phenomenon, namely, the correlation between optical disturbances. That is, we are generally interested in determining the effects arising from relative fluctuations in the fields at two points in space–time. Admittedly, the term temporal coherence seems to imply an effect that is exclusively temporal. However, it relates back to the finite extent of the [illegible] in either space or time, and some people [illegible] prefer to refer to it as *longitudinal spatial* [illegible] than temporal coherence. Even so, it does depend intrinsically on the stability of phase in time, and accordingly we will continue to use the term temporal coherence. Spatial coherence, or if you will, *lateral* [illegible] *coherence*, is perhaps easier to appreciate, because [illegible] closely related to the concept of the wavefront. That if two laterally displaced points reside on the same wavefront at a given time, the fields at those points are said to be spatially coherent (see Section 12.3.1).



(a) (b) (c) (d)

Figure 12.2 Double-beam interference from a pair of [illegible] tures. (a) He–Ne laserlight illuminating the holes. (b) [illegible] again but now a glass plate, 0.5 mm thick, is covering one [illegible] (c) Fringes with collimated mercury-arc illumination [illegible] plate. (d) This time the fringes disappear when the [illegible] using mercury light. [From B. J. Thompson, *J. Soc.* [illegible] 4, 7 (1965).]

12.2 VISIBILITY

The quality of the fringes produced by an interferometric system can be described quantitatively using the visibility $\mathcal{V}$, which, as first formulated by Michelson, is given by

$$\mathcal{V}(\mathbf{r}) = \frac{I_{max} - I_{min}}{I_{max} + I_{min}} \qquad (12.1)$$

Of course, this is identical to the *modulation* of Eq. [illegible]. Here I_{max} and I_{min} are the irradiances corresponding to the maximum and adjacent minimum in the fringe system. If we set up Young's experiment, we [illegible] vary the separation of the apertures or the size [illegible] primary incoherent quasimonochromatic source, [illegible] $\mathcal{V}$ as it changes in turn, and then relate all this [illegible] idea of coherence. An analytic expression can be [illegible] for the flux-density distribution with the aid of Fig. 12.3.* Here we use a lens L to localize the fringe [illegible] more effectively, that is, to make the cones of [illegible] diffracted by the finite pinholes more completely [illegible] on the plane Σ_o. A point source S' located on [illegible] central axis would generate the usual pattern given by

$$I = 4I_0 \cos^2\left(\frac{Ya\pi}{s\lambda}\right) \qquad (12.2)$$

from Section 9.3. Similarly, a point source above or below S' and lying on a line normal to the line $\overline{S_1S_2}$, would generate the same straight band fringe system slightly displaced in a direction parallel to the fringes. Thus replacing S' by an incoherent line source (normal to the plane of the drawing) effectively just increases the amount of light available. This is something we presumably already knew. In contrast, an off-axis point source, at say S'', will generate a pattern centered about P'', its image point on Σ_o in the absence of the aperture screen. A "spherical" wavelet leaving S'' is focused at P''; thus all rays from S'' to P'' traverse equal optic paths, and the interference must be constructive; in other words, the central maximum appears at P''. The path difference $\overline{S_1P''} - \overline{S_2P''}$ accounts for the displacement $\overline{P'P''}$. Consequently, S'' produces a fringe system identical to that of S' but shifted by an amount $\overline{P'P''}$ with respect to it. Since these source points are incoherent, their irradiances add on Σ_o rather than their field amplitudes [Fig. 12.3(e)].

The pattern arising from a broad source having a rectangular aperture of width b can be determined by finding the irradiance due to an incoherent continuous line source parallel to $\overline{S_1S_2}$. Notice, in Fig. 12.3(b), that the variable Y_0 describes the location of any point on the image of the source when the aperture screen is absent. With Σ_a in place, each differential element of the line source will contribute a fringe system centered about its own image point, a distance Y_0 from the origin on Σ_o. Moreover, its contribution to the flux-density pattern dI is proportional to the differential line element or, more conveniently, to its image, dY_0, on Σ_o. Thus, using Eq. (9.31), the contribution to the total irradiance arising from dY_0 is

$$dI \quad A\, dY_0 \cos^2\left[\frac{a\pi}{s\lambda}(Y - Y_0)\right], \qquad (12.3)$$

where A is an appropriate constant. This, in analogy to Eq. (12.2), is the expression for an entire fringe system of minute irradiance centered at Y_0 contributed by the tiny piece of the source whose image corresponds

* [illegible] part follows that given by Towne in Chapter 11 [illegible]. See Klein, *Optics*, Section 6.3, or Problem 12.6 for different [illegible].

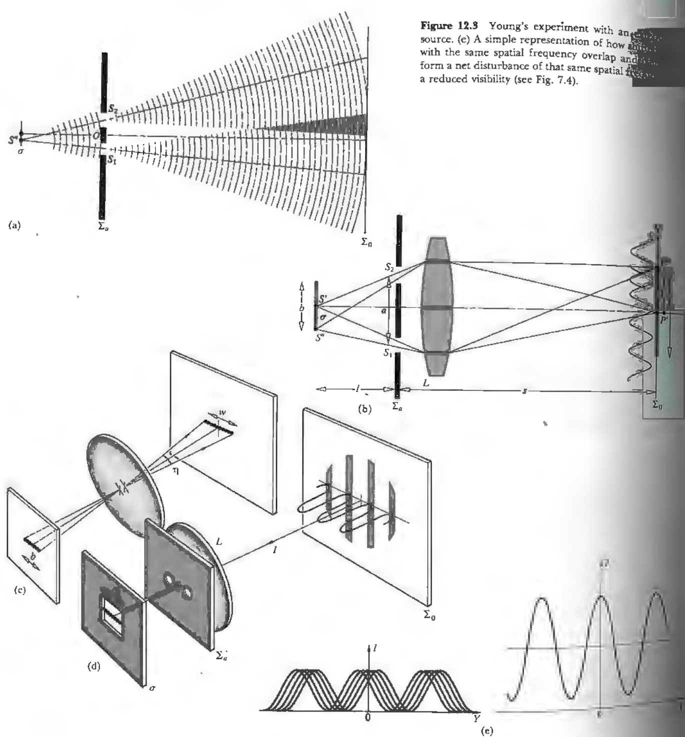


Figure 12.3 Young's experiment with an ... source. (c) A simple representation of how ... with the same spatial frequency overlap and ... form a net disturbance of that same spatial ... a reduced visibility (see Fig. 7.4).

... Y_0. By integrating over the extent w of the ...ge of the line source, we effectively integrate over ...source and get the entire pattern:

$$I(Y) = A\int_{-w/2}^{+w/2} \cos^2\left[\frac{a\pi}{s\lambda}(Y - Y_0)\right] dY_0. \qquad (12.4)$$

After a good bit of straightforward trigonometric manipulation, this becomes

$$I(Y) = \frac{Aw}{2} + \frac{A}{2}\frac{s\lambda}{a\pi}\sin\left(\frac{a\pi}{s\lambda}w\right)\cos\left(2\frac{a\pi}{s\lambda}Y\right). \qquad (12.5)$$

The irradiance oscillates about an average value of $\bar{I} = Aw/2$, which increases with w, which in turn increases with the width of the source slit. Accordingly,

$$\frac{I(Y)}{\bar{I}} = 1 + \left(\frac{\sin a\pi w/s\lambda}{a\pi w/s\lambda}\right)\cos\left(2\frac{a\pi}{s\lambda}Y\right) \qquad (12.6)$$

or

$$\frac{I(Y)}{\bar{I}} = 1 + \operatorname{sinc}\left(\frac{a\pi w}{s\lambda}\right)\cos\left(2\frac{a\pi}{s\lambda}Y\right). \qquad (12.7)$$

...llows that the extreme values of the relative irradi-...are given by

$$\frac{I_{max}}{\bar{I}} = 1 + \left|\operatorname{sinc}\left(\frac{a\pi w}{s\lambda}\right)\right| \qquad (12.8)$$

and

$$\frac{I_{min}}{\bar{I}} = 1 - \left|\operatorname{sinc}\left(\frac{a\pi w}{s\lambda}\right)\right| \qquad (12.9)$$

When w is very small in comparison to the fringe width $(s\lambda/a)$, the sinc function (p. 624) approaches 1 and $I_{max}/\bar{I} = 2$, while $I_{min}/\bar{I} = 0$ (see Fig. 12.4). As w increases, I_{min} begins to differ from zero, and the fringes ... contrast until they finally vanish entirely at w ... Between the arguments of π and 2π (i.e., $w = s\lambda/a$ ... $w = 2s\lambda/a$), the sinc is negative. As the primary slit source widens beyond $w = s\lambda/a$, the fringes reappear shifted in phase; in other words, previously there ... maximum at $Y = 0$, now there will be a minimum. ... actuality, the light diffracted by the apertures is ... (Section 10.2) so that the fringe system does not continue ... uniformly indefinitely as Y increases.

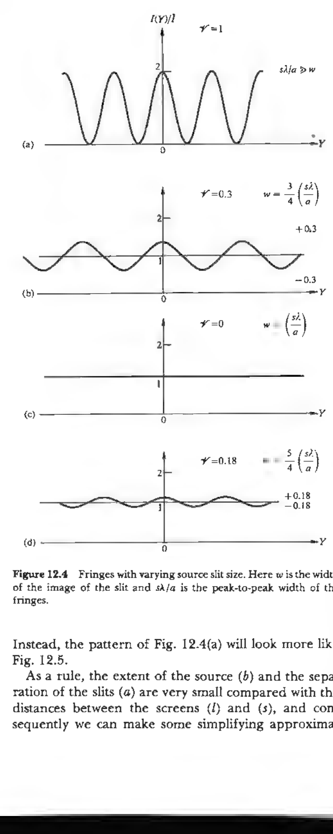


Figure 12.4 Fringes with varying source slit size. Here w is the width of the image of the slit and $s\lambda/a$ is the peak-to-peak width of the fringes.

Instead, the pattern of Fig. 12.4(a) will look more like Fig. 12.5.

As a rule, the extent of the source (b) and the separation of the slits (a) are very small compared with the distances between the screens (l) and (s), and consequently we can make some simplifying approxima-

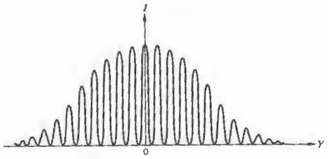


Figure 12.5 Double-beam interference fringes showing the effect of diffraction.

tions. While the above considerations were expressed in terms of w and s, it follows from Fig. 12.3(c), using the central angle η, that $b \approx l\eta$ and $w \approx s\eta$; hence $w/s \approx b/l$. Accordingly, $(a\pi w/s\lambda) \approx (a\pi\eta/\lambda) \approx (a\pi b/l\lambda)$. The visibility of the fringes follows from Eq. (12.1):

$$\mathcal{V} = \left|\operatorname{sinc}\left(\frac{a\pi w}{s\lambda}\right)\right| = \left|\operatorname{sinc}\left(\frac{a\pi b}{l\lambda}\right)\right|, \qquad (12.10)$$

which is plotted in **Fig. 12.6**. Observe that $\mathcal{V}$ is a function of both the source breadth and the aperture separation a. Holding either one of these parameters constant and varying the other will cause $\mathcal{V}$ to change in precisely the same way. Note that the visibilities in both Figs. 12.4(a) and 12.5 are equal to one, because $I_{min} = 0$. Clearly then, the visibility of the fringe system on the plane of observation is linked to the way the light is distributed over the aperture screen. If the primary

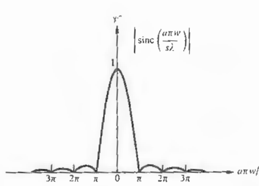


Figure 12.6 The visibility as given by Eq. (12.10).

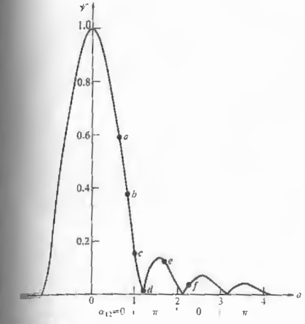
source were in fact a point, b would equal zero [illegible] visibility would be a perfect 1. Shy of that, th[illegible] $(a\pi b/l\lambda)$ is, the better, that is, the bigger $\mathcal{V}$ i[illegible] clearer the fringes are. We can think of $\mathcal{V}$ as [illegible] of the degree of coherence of the light from th[illegible] source as spread over the aperture screen. Ke[illegible] that we have encountered the sinc function [illegible] connection wtih the diffraction pattern resulting from a rectangular aperture.

When the primary source is circular, the [illegible] a good deal more complicated to calculate. I[illegible] to be proportional to a first-order Bessel fun[illegible] 12.7). This too is quite reminiscent of diffraction this time at a circular aperture (10.56). These similarit[illegible] between expressions for $\mathcal{V}$ and the correspon[illegible] diffraction patterns for an aperture of the same s[illegible] are not merely fortuitous but rather are a ma[illegible] of something called the van Cittert–Zernike [illegible] as we will see presently.

Figure 12.8 shows a sequence of fringe [illegible] which the circular incoherent primary sourc[illegible] in size but the separation a between S[illegible] increased. The visibility decreases from (a) to [illegible] figure, then increases for (e) and decreases ag[illegible] All the associated $\mathcal{V}$-values are plotted in Fig [illegible] the shift in the peaks, that is, the change i[illegible] the center of the pattern for each point on the second lobe of Fig. 12.7 (the Bessel function is negative over that range). In other words, (a), (b), and (c) have a central maximum, while (d) and (e) have a central minimum, and (f) on the third lobe is back to a maximum. In the same way, for a slit source [illegible] where sinc $(a\pi w/s\lambda)$ in Eq. (12.7) is positive [illegible] will yield a maximum or minimum, respectively, in $I(0)/\bar{I}$. These in turn correspond to the odd or even lobes of the visibility curve of Fig. 12.6. Bear in mind that we could define a complex visibility of ma[illegible] $\mathcal{V}$, having an argument corresponding to the [illegible] shift—we'll come back to this idea later.

Since the width of the fringes is inversely p[illegible] to a, the spatial frequency of the bright and [illegible] increases accordingly from (a) to (f) in Fig. [illegible] 12.9 results when the separation a is held co[illegible] the primary incoherent source diameter i[illegible]

We should also mention that the effects [illegible]



[illegible] 12.7 The visibility for a circular source.

[illegible]width will show up in a given fringe pattern as a [illegible]ally decreasing value of $\mathcal{V}$ with Y, as in Fig. 12.10 [illegible]roblem 12.3). When the visibility is determined in these cases, using the central region of each of a [illegible] of patterns, the dependence of $\mathcal{V}$ on aperture [illegible] will again match Fig. 12.7.

12.3 [illegible]HE MUTUAL COHERENCE FUNCTION AND THE DEGREE OF COHERENCE

[illegible] carry the discussion a bit further in a more [illegible]fashion. Again suppose we have a broad, narrow [illegible]dth source, which generates a light field whose [illegible]plex representation* is $\tilde{E}(\mathbf{r}, t)$. We'll overlook [illegible]ization effects, and therefore a scalar treatment [illegible]o. The disturbances at two points in space S_1 and [illegible] are then $\tilde{E}(S_1, t)$ and $\tilde{E}(S_2, t)$ or, more succinctly, $\tilde{E}_1(t)$ and $\tilde{E}_2(t)$. If these two points are then isolated using an opaque screen with two circular apertures (Fig. 12.11), we're back to Young's experiment. The two apertures serve as sources of secondary wavelets, which propagate out to some point P on Σ_o. There the resultant field is

$$\tilde{E}_P(t) = \tilde{K}_1\tilde{E}_1(t - t_1) + \tilde{K}_2\tilde{E}_2(t - t_2), \qquad (12.11)$$

where $t_1 = r_1/c$ and $t_2 = r_2/c$. This says that the field at the space–time point (P, t) can be determined from the fields that existed at S_1 and S_2 at t_1 and t_2, respectively, these being the instants when the light, which is now overlapping, first emerged from the apertures. The quantities $\tilde{K}_1$ and $\tilde{K}_2$, which are known as *propagators*, depend on the size of the apertures and their relative locations with respect to P. They mathematically affect the alterations in the field resulting from its having traversed either of the apertures. For example, the secondary wavelets issuing from the pinholes in this setup are out of phase by $\pi/2$ rad with the primary wave incident on the aperture screen, Σ_a (Section 10.3.1). Clearly someone is going to have to tell $\tilde{E}(\mathbf{r}, t)$ to shift phase beyond Σ_a—that's just what the $\tilde{K}$ factors are for. Moreover, they reflect a reduction in the field that might arise from a number of physical causes: absorption, diffraction, and so forth. Here, since there is a $\pi/2$ phase shift in the field, which can be introduced by multiplying by $\exp i\pi/2$, $\tilde{K}_1$ and $\tilde{K}_2$ are purely imaginary numbers.

The resultant irradiance at P measured over some finite time interval, which is long compared with the coherence time, is

$$I = \langle \tilde{E}_P(t)\tilde{E}_P^*(t)\rangle. \qquad (12.12)$$

It should be remembered that Eq. (12.12) is written sans several multiplicative constants. Hence using Eq. (12.11),

$$\begin{aligned} I = {} & \tilde{K}_1\tilde{K}_1^*\langle\tilde{E}_1(t - t_1)\tilde{E}_1^*(t - t_1)\rangle \\ & + \tilde{K}_2\tilde{K}_2^*\langle\tilde{E}_2(t - t_2)\tilde{E}_2^*(t - t_2)\rangle \\ & + \tilde{K}_1\tilde{K}_2^*\langle\tilde{E}_1(t - t_1)\tilde{E}_2^*(t - t_2)\rangle \\ & + \tilde{K}_1^*\tilde{K}_2\langle\tilde{E}_1^*(t - t_1)\tilde{E}_2(t - t_2)\rangle. \end{aligned} \qquad (12.13)$$

It is now assumed that the wave field is *stationary*, as is almost universally the case in classical optics; in other

*[illegible]t a wavy line over quantities that are complex just as a [illegible]ng reminder.

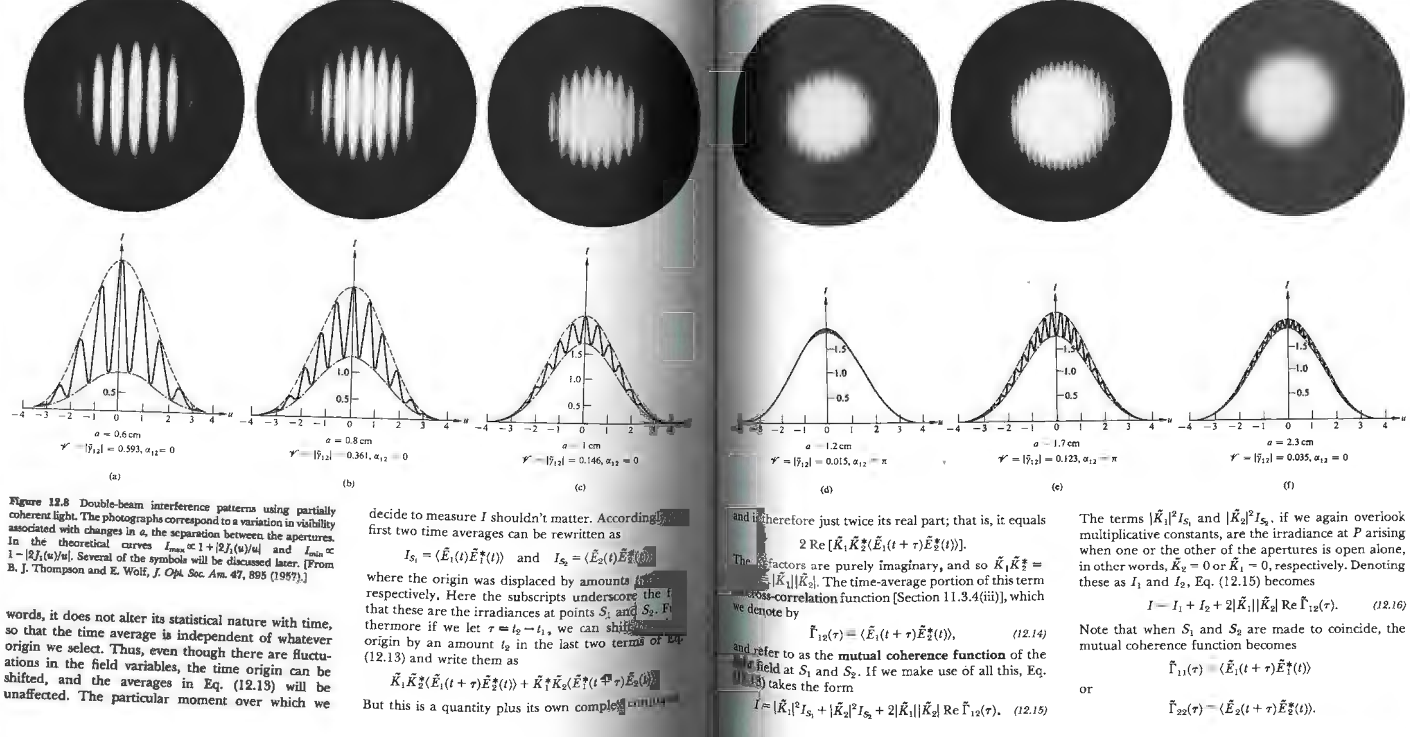


Figure 12.8 Double-beam interference patterns using partially coherent light. The photographs correspond to a variation in visibility associated with changes in a, the separation between the apertures. In the theoretical curves $I_{max} \propto 1 + |2J_1(u)/u|$ and $I_{min} \propto 1 - |2J_1(u)/u|$. Several of the symbols will be discussed later. [From B. J. Thompson and E. Wolf, *J. Opt. Soc. Am.* **47**, 895 (1957).]

words, it does not alter its statistical nature with time, so that the time average is independent of whatever origin we select. Thus, even though there are fluctuations in the field variables, the time origin can be shifted, and the averages in Eq. (12.13) will be unaffected. The particular moment over which we decide to measure I shouldn't matter. Accordingly, [illegible] first two time averages can be rewritten as

$$I_{S_1} = \langle \tilde{E}_1(t)\tilde{E}_1^*(t)\rangle \quad \text{and} \quad I_{S_2} = \langle \tilde{E}_2(t)\tilde{E}_2^*(t)\rangle$$

where the origin was displaced by amounts [illegible] respectively. Here the subscripts underscore the [illegible] that these are the irradiances at points S_1 and S_2. F[illegible]thermore if we let $\tau = t_2 - t_1$, we can shift [illegible] origin by an amount t_2 in the last two terms of Eq. (12.13) and write them as

$$\tilde{K}_1\tilde{K}_2^*\langle \tilde{E}_1(t+\tau)\tilde{E}_2^*(t)\rangle + \tilde{K}_1^*\tilde{K}_2\langle \tilde{E}_1^*(t+\tau)\tilde{E}_2(t)\rangle$$

But this is a quantity plus its own complex conjugate and is therefore just twice its real part; that is, it equals

$$2\,\mathrm{Re}\,[\tilde{K}_1\tilde{K}_2^*\langle \tilde{E}_1(t+\tau)\tilde{E}_2^*(t)\rangle].$$

The [illegible] factors are purely imaginary, and so $\tilde{K}_1\tilde{K}_2^* = |\tilde{K}_1||\tilde{K}_2|$. The time-average portion of this term [illegible] cross-correlation function [Section 11.3.4(iii)], which we denote by

$$\tilde{\Gamma}_{12}(\tau) = \langle \tilde{E}_1(t+\tau)\tilde{E}_2^*(t)\rangle, \qquad (12.14)$$

and refer to as the **mutual coherence function** of the [illegible] field at S_1 and S_2. If we make use of all this, Eq. (12.13) takes the form

$$I = |\tilde{K}_1|^2 I_{S_1} + |\tilde{K}_2|^2 I_{S_2} + 2|\tilde{K}_1||\tilde{K}_2|\,\mathrm{Re}\,\tilde{\Gamma}_{12}(\tau). \qquad (12.15)$$

The terms $|\tilde{K}_1|^2 I_{S_1}$ and $|\tilde{K}_2|^2 I_{S_2}$, if we again overlook multiplicative constants, are the irradiance at P arising when one or the other of the apertures is open alone, in other words, $\tilde{K}_2 = 0$ or $\tilde{K}_1 = 0$, respectively. Denoting these as I_1 and I_2, Eq. (12.15) becomes

$$I = I_1 + I_2 + 2|\tilde{K}_1||\tilde{K}_2|\,\mathrm{Re}\,\tilde{\Gamma}_{12}(\tau). \qquad (12.16)$$

Note that when S_1 and S_2 are made to coincide, the mutual coherence function becomes

$$\tilde{\Gamma}_{11}(\tau) = \langle \tilde{E}_1(t+\tau)\tilde{E}_1^*(t)\rangle$$

or

$$\tilde{\Gamma}_{22}(\tau) = \langle \tilde{E}_2(t+\tau)\tilde{E}_2^*(t)\rangle.$$

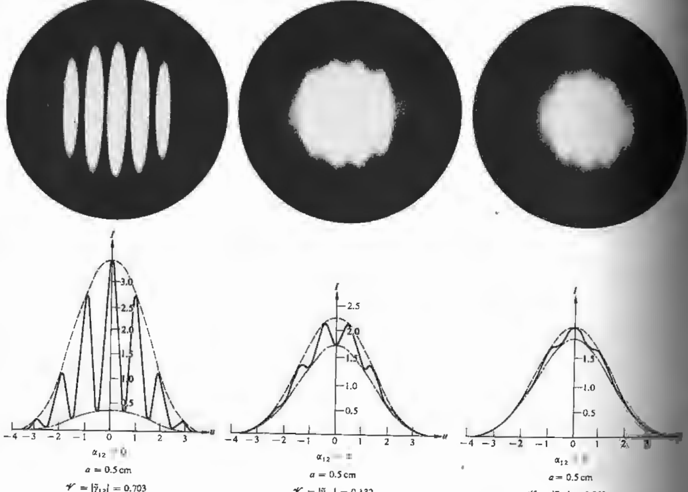


Figure 12.9 Double-beam interference patterns. Here the aperture separation was held constant, thereby yielding a constant number of fringes per unit displacement in each photo. The visibility was altered by varying the size of the primary incoherent source. [From B. J. Thompson, *J. Soc. Photo. Inst. Engr.* **4**, 7 (1965).]

We can imagine that two wavetrains emerge from this coalesced source point and somehow pick up a relat[illegible] phase delay proportional to τ. In the present si[illegible] τ becomes zero (since the optical path differenc[illegible] to zero), and these functions are reduced to the corresponding irradiances $I_{S_1} = \langle \tilde{E}_1(t)\tilde{E}_1^*(t)\rangle$ and $I_{S_2} = \langle \tilde{E}_2(t)\tilde{E}_2^*(t)\rangle$ on Σ_a. Hence

$$\Gamma_{11}(0) = I_{S_1} \quad \text{and} \quad \Gamma_{22}(0) = I_{S_2},$$

and these are called *self-coherence functi[illegible]* Thus

$$I_1 = |\tilde{K}_1|^2\Gamma_{11}(0) \quad \text{and} \quad I_2 = |\tilde{K}_2|^2\Gamma_{2[illegible]}$$

Keeping Eq. (12.16) in mind, observe that

$$|\tilde{K}_1||\tilde{K}_2| = \sqrt{I_1}\sqrt{I_2}/\sqrt{\Gamma_{11}(0)}\sqrt{\Gamma_{22}(0)}.$$

Hence the normalized form of the mutual coherence function is defined as

$$\tilde{\gamma}_{12}(\tau) \equiv \frac{\tilde{\Gamma}_{12}(\tau)}{\sqrt{\Gamma_{11}(0)\Gamma_{22}(0)}} = \frac{\langle \tilde{E}_1(t+\tau)\tilde{E}_2^*(t)\rangle}{\sqrt{\langle|\tilde{E}_1|^2\rangle\langle|\tilde{E}_2|^2\rangle}}, \quad (12.17)$$

and it's spoken of as the **complex degree of coherence,** [illegible] which will be clear imminently. Equation [illegible] then be recast as

$$I = I_1 + I_2 + 2\sqrt{I_1 I_2}\,\text{Re}\,\tilde{\gamma}_{12}(\tau), \quad (12.18)$$

[illegible] the *general interference law for partially coherent* [illegible]

[illegible] quasimonochromatic light the phase angle [illegible]ence concomitant with the optical path difference [illegible] given by

$$\varphi = \frac{2\pi}{\bar{\lambda}}(r_2 - r_1) = 2\pi\bar{\nu}\tau, \quad (12.19)$$

[illegible] $\bar{\lambda}$ and $\bar{\nu}$ are the mean wavelength and frequency. [illegible] $\tilde{\gamma}_{12}(\tau)$ is a complex quantity expressible as

$$\tilde{\gamma}_{12}(\tau) = |\tilde{\gamma}_{12}(\tau)|e^{i\Phi_{12}(\tau)}. \quad (12.20)$$

[illegible] phase angle of $\tilde{\gamma}_{12}(\tau)$ relates back to Eq. (12.14) [illegible] the phase angle between the fields. If we set [illegible] $= \alpha_{12}(\tau) - \varphi$, then

$$\text{Re}\,\tilde{\gamma}_{12}(\tau) = |\tilde{\gamma}_{12}(\tau)|\cos[\alpha_{12}(\tau) - \varphi].$$

[illegible]uation (12.18) is then expressible as

$$I = I_1 + I_2 + 2\sqrt{I_1 I_2}|\tilde{\gamma}_{12}(\tau)|\cos[\alpha_{12}(\tau) - \varphi]. \quad (12.21)$$

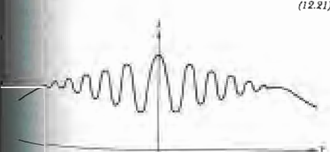


Figure 12.10 A finite bandwidth results in a decreasing value of $\mathcal{V}$ with increasing Y.

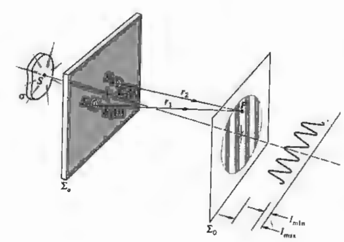


Figure 12.11 Young's experiment.

It can be shown from Eq. (12.17) and the Schwarz inequality that $0 \le |\tilde{\gamma}_{12}(\tau)| \le 1$. In fact, a comparison of Eqs. (12.21) and (9.14), the latter having been derived for the case of complete coherence, makes it evident that if $|\tilde{\gamma}_{12}(\tau)| = 1$, I is the same as that generated by two *coherent* waves out of phase at S_1 and S_2 by an amount $\alpha_{12}(\tau)$. If at the other extreme $|\tilde{\gamma}_{12}(\tau)| = 0$, $I = I_1 + I_2$, there is no interference, and the two disturbances are said to be *incoherent*. When $0 < |\tilde{\gamma}_{12}(\tau)| < 1$ we have *partial coherence*, the measure of which is $|\tilde{\gamma}_{12}(\tau)|$ itself; this is known as the **degree of coherence**. In summary then,

$|\tilde{\gamma}_{12}| = 1$ coherent limit

$|\tilde{\gamma}_{12}| = 0$ incoherent limit

$0 < |\tilde{\gamma}_{12}| < 1$ partial coherence.

The basic statistical nature of the entire process must be underscored. Clearly $\tilde{\Gamma}_{12}(\tau)$ and, therefore, $\tilde{\gamma}_{12}(\tau)$ are the key quantities in the various expressions for the irradiance distribution; they are the essence of what we previously called the interference term. It should be pointed out that $\tilde{E}_1(t+\tau)$ and $\tilde{E}_2(t)$ are in fact two disturbances occurring at different points in both space and time. We anticipate, as well, that the amplitudes and phases of these disturbances will somehow fluctuate in time. If these fluctuations at S_1 and S_2 are completely independent, then $\tilde{\Gamma}_{12}(\tau) = \langle \tilde{E}_1(t+\tau)\tilde{E}_2^*(t)\rangle$ will go to zero, since $\tilde{E}_1$ and $\tilde{E}_2$ can be either positive or negative with equal likelihood, and their product averages to zero. In that case no correlation exists, and $\tilde{\Gamma}_{12}(\tau) = \tilde{\gamma}_{12}(\tau) = 0$. If the field at S_1 at a time $(t+\tau)$ were perfectly correlated with the field at S_2 at a time t, their relative phase would remain unaltered despite individual fluctuations. The time average of the product of the fields would certainly not be zero, just as it would not be zero even if the two were only slightly correlated.

Both $|\tilde{\gamma}_{12}(\tau)|$ and $\alpha_{12}(\tau)$ are slowly varying functions of τ in comparison to $\cos 2\pi\bar{\nu}\tau$ and $\sin 2\pi\bar{\nu}\tau$. In other words, as P is moved across the resultant fringe system, the point-by-point spatial variations in I are predominantly due to the changes in φ as $(r_2 - r_1)$ changes.

The maximum and minimum values of I occur when the cosine term in Eq. (12.21) is +1 and −1, respectively. The visibility at P (Problem 12.7) is then

$$\mathscr{V} = \frac{2\sqrt{I_1}\sqrt{I_2}}{I_1 + I_2}|\tilde{\gamma}_{12}(\tau)|. \qquad (12.22)$$

Perhaps the most common arrangement occurs when things are adjusted so that $I_1 = I_2$, whereupon

$$\mathscr{V} = |\tilde{\gamma}_{12}(\tau)|; \qquad (12.23)$$

that is, *the modulus of the complex degree of coherence is identical to the visibility of the fringes* (take another look at Fig. 12.8).

It is essential to realize that Eqs. (12.17) and (12.18) clearly suggest the way in which the real parts of $\tilde{\Gamma}_{12}(\tau)$ and $\tilde{\gamma}_{12}(\tau)$ can be determined from direct measurements. When the flux densities of two disturbances are adjusted to be equal, Eq. (12.23) provides an experimental means of obtaining $|\tilde{\gamma}_{12}(\tau)|$ from the resultant fringe pattern. Furthermore, the off-axis shift in the location of the central fringe (from $\varphi = 0$) is a measure of $\alpha_{12}(\tau)$, the apparent relative retardation of the phase of the disturbances at S_1 and S_2. Thus, measurements of the visibility and fringe position yield both the amplitude and phase of the complex degree of coherence.

By the way, it can be shown* that $|\tilde{\gamma}_{12}(\tau)|$ will equal 1 for all values of τ and any pair of spatial points, if and only if the optical field is strictly monochro[illegible] and therefore such a situation is unattain[illegible] Moreover, a nonzero radiation field for which $|\tilde{\gamma}_{12}($[illegible] 0 for all values of τ and any pair of spatial points [illegible] exist in free space either.

12.3.1 Temporal and Spatial Coherence

Let's now relate the ideas of temporal and spa[illegible] ence to the above formalism.

If the primary source S in Fig. 12.11 shrinks down to a point source on the central axis having [illegible] frequency bandwidth, temporal coherence [illegible] predominate. The optical disturbances at S_1 [illegible] then be identical. In effect, the mutual coheren[illegible] between the two points will be the **self-coherence** [illegible] field. Hence $\tilde{\Gamma}(S_1, S_2, \tau) = \tilde{\Gamma}_{12}(\tau) = \tilde{\Gamma}_{11}(\tau)$ or [illegible] $\tilde{\gamma}_{11}(\tau)$. The same thing obtains when S_1 and S_2 co[illegible] and $\tilde{\gamma}_{11}(\tau)$ is sometimes referred to as the **comple[illegible] degree of temporal coherence** at that point for two instances of time separated by an interval τ. This wo[illegible] be the case in an amplitude-splitting interferom[illegible] such as Michelson's, in which τ equals the path-len[illegible] difference divided by c. The expression for [illegible] Eq. (12.18), would then contain $\tilde{\gamma}_{11}(\tau)$ rather th[illegible]

Suppose a lightwave is divided into two [illegible] disturbances of the form

$$\tilde{E}(t) = E_0 e^{i\phi(t)} \qquad (12.24)$$

by an amplitude-splitting interferometer, which later recombines them to generate a fringe pattern. Then

$$\tilde{\gamma}_{11}(\tau) = \frac{\langle \tilde{E}(t+\tau)\tilde{E}^*(t)\rangle}{|\tilde{E}|^2} \qquad (12.25)$$

or

$$\tilde{\gamma}_{11}(\tau) = \langle e^{i\phi(t+\tau)}e^{-i\phi(t)}\rangle.$$

Hence

$$\tilde{\gamma}_{11}(\tau) = \lim_{T\to\infty}\frac{1}{T}\int_0^T e^{i[\phi(t+\tau)-\phi(t)]}\,dt \qquad (12.26)$$

and

$$\tilde{\gamma}_{11}(\tau) = \lim_{T\to\infty}\frac{1}{T}\int_0^T (\cos\Delta\phi + i\sin\Delta\phi)\,dt$$

[illegible] $\Delta\phi = \phi(t+\tau) - \phi(t)$. For a strictly monochro[illegible] plane wave of infinite coherence length, $\phi(t) =$ [illegible] $\Delta\phi = -\omega\tau$, and

$$\tilde{\gamma}_{11}(\tau) = \cos\omega\tau - i\sin\omega\tau = e^{-i\omega\tau}.$$

[illegible] $|\tilde{\gamma}_{11}| = 1$; the argument of $\tilde{\gamma}_{11}$ is just $-2\pi\nu\tau$, and [illegible] complete coherence. In contradistinction, for [illegible] monochromatic wave where τ is greater than the [illegible] time, $\Delta\phi$ will be random, varying between 0 [illegible] such that the integral averages to zero, $|\tilde{\gamma}_{11}(\tau)| =$ [illegible] responding to complete incoherence. A path [illegible] ence of 60 cm, produced when the two arms of a [illegible] helson interferometer differ in length by 30 cm, [illegible] sponds to a time delay between the recombining [illegible] ms of $\tau \approx 2$ ns. This is roughly the coherence time [illegible] good isotope discharge lamp, and the visibility of [illegible] ttern under this sort of illumination will be quite [illegible] If white light is used instead, $\Delta\nu$ is large, Δt_c is [illegible] small, and the coherence length is less than one [illegible] elength. In order for τ to be less than Δt_c (i.e., in [illegible] er that the visibility be good), the optical path [illegible] erence will have to be a small fraction of a [illegible] elength. The other extreme is laserlight, in which [illegible] can be so long that a value of $c\tau$ that will cause an [illegible] able decrease in visibility would require an [illegible] ically large interferometer.

[illegible] see that $\tilde{\Gamma}_{11}(\tau)$, being a measure of temporal [illegible] ence, must be intimately related to the coherence [illegible] and therefore the bandwidth of the source. Indeed, [illegible] *rier transform of the self-coherence function, $\tilde{\Gamma}_{11}(\tau)$,* [illegible] *power spectrum, which describes the spectral energy* [illegible] *ution of the light* (Section 11.3.4).

[illegible] go back to Young's experiment (Fig. 12.11) with [illegible] narrow-bandwidth extended source, spatial [illegible] ence effects will predominate. The optical disturbances at S_1 and S_2 will differ, and the fringe pattern will depend on $\tilde{\Gamma}(S_1, S_2, \tau) = \tilde{\Gamma}_{12}(\tau)$. By examining the [illegible] about the central fringe where $(r_2 - r_1) = 0$, $\tau = 0$ [illegible] $\tilde{\Gamma}_{12}(0)$ and $\tilde{\gamma}_{12}(0)$ can be determined. This latter [illegible] tity is the **complex degree of spatial coherence** of [illegible] two points at the same instant in time. $\tilde{\Gamma}_{12}(0)$ plays [illegible] tral role in the description of the Michelson stellar [illegible] ferometer to be discussed forthwith.

[illegible] ere is a very convenient relationship between the [illegible] lex degree of coherence in a region of space and the corresponding irradiance distribution across the extended source giving rise to the light fields. We shall make use of that relationship, the **van Cittert–Zernike theorem**, as a calculational aid without going through its formal derivation. Indeed, the analysis of Section 12.2 already suggests some of the essentials. Figure 12.12 represents an extended quasimonochromatic incoherent source, S, located on the plane σ and having an irradiance given by $I(y, z)$. Also shown is an observa-

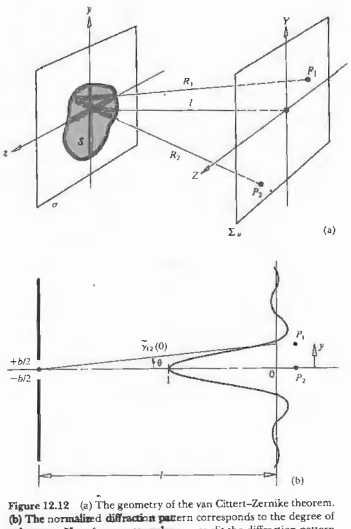


Figure 12.12 (a) The geometry of the van Cittert–Zernike theorem. (b) The normalized diffraction pattern corresponds to the degree of coherence. Here for a rectangular source slit the diffraction pattern is sinc $(\pi by/l\lambda)$.

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*The proofs are given in Beran and Parrent, *Theory of Partial Coherence*, Section 4.2.

tion screen on which are two points, P_1 and P_2. These are at distances R_1 and R_2, respectively, from a tiny element of S. It is on this plane that we wish to determine $\tilde{\gamma}_{12}(0)$, which describes the correlation of the field vibrations at the two points. Note that although the source is incoherent, the light reaching P_1 and P_2 will generally be correlated to some degree, since each source element contributes to the field at each such point.

Calculation of $\tilde{\gamma}_{12}(0)$ from the fields at P_1 and P_2 results in an integral that has a familiar structure. The integral has the same form and will yield the same results as a well-known diffraction integral, provided we reinterpret each term appropriately. For instance, $I(y, z)$ appears in that coherence integral where an aperture function would be if it were, in fact, a diffraction integral. Thus, suppose that S is not a source but an aperture of identical size and shape, and suppose that $I(y, z)$ is not a description of irradiance, but instead its functional form corresponds to the field distribution across that aperture. In other words, imagine that there is a transparency at the aperture with amplitude transmission characteristics that correspond functionally to $I(y, z)$. Furthermore, imagine that the aperture is illuminated by a spherical wave converging toward the fixed point P_2 (see Fig. 12.12b), so that *there will be a diffraction pattern centered on* P_2. This diffracted field distribution, normalized to unity at P_2, is everywhere (i.e., at P_1) equal to the value of $\tilde{\gamma}_{12}(0)$ at that point. This is the van Cittert–Zernike theorem.

When P_1 and P_2 are close together and S is small compared with l, the complex degree of coherence equals the normalized Fourier transform of the irradiance distribution across the source. Furthermore, if the source has a uniform irradiance, then $\tilde{\gamma}_{12}(0)$ is simply a sinc function when the source is a slit and a Bessel function when it's circular. Observe that in Fig. 12.12 the sinc function corresponds to that of Fig. 10.1, where $\beta = (kb/2)\sin\theta$ and $\theta \approx \sin\theta$. Thus if P_1 is a distance y from P_2, $\beta \approx kb\theta/2$ and $\theta \approx y/l$, and $|\tilde{\gamma}_{12}(0)| = |\text{sinc}\,(\pi by/l\lambda)|$. This result is explored further in the problem set.

12.4 COHERENCE AND STELLAR INTERFEROMETRY

12.4.1 The Michelson Stellar Interferometer

In 1890 A. A. Michelson, following an earlier suggestion by Fizeau, proposed an interferometric device (Fig. 12.13) that is of interest here both because it was the precursor of some important modern techniques and because it lends itself to an interpretation in terms of coherence theory. The function of the *stellar interferometer*, as it is called, is to measure the small angular dimensions of remote astronomical bodies.

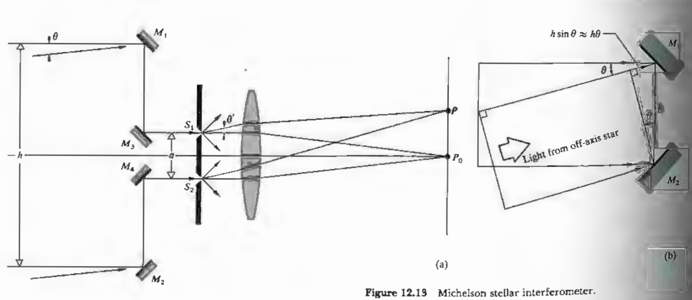


Figure 12.13 Michelson stellar interferometer.

Two widely spaced movable mirrors, M_1 and M_2, collect rays, assumed to be parallel, from a very distant star. The light is then channeled via mirrors M_3 and M_4 through apertures S_1 and S_2 of a mask and thence into the objective of a telescope. The optical paths $M_1M_3S_1$ and $M_2M_4S_2$ are made equal, so that the relative phase-angle difference between a disturbance at M_1 and M_2 is the same as that between S_1 and S_2. The two apertures generate the usual Young's experiment fringe system in the focal plane of the objective. Actually, the mask and openings are not really necessary; the mirrors alone could serve as apertures. Suppose we now point the device so that its central axis is directed toward one of the stars in a closely spaced double-star configuration. Because of the tremendous distances involved, the rays reaching the interferometer from either star are well collimated. Furthermore, we assume, at least for the moment, that the light has a narrow linewidth centered about a mean wavelength of $\bar{\lambda}_0$. The disturbances arising at S_1 and S_2 from the axial star are in phase, and a pattern of bright and dark bands results, centered on P_0. Similarly, rays from the other star arrive at some angle θ, but this time the disturbances at M_1 and M_2 (and therefore at S_1 and S_2) are out of phase by approximately $\bar{k}_0 h\theta$ or, if you will, retarded by a time $h\theta/c$, as indicated in Fig. 12.13(b). The resulting fringe system is centered about a point P shifted by an angle θ' from P_0 such that $h\theta/c = a\theta'/c$. Since the stars behave as though they were incoherent point sources, the individual irradiance distributions simply add. The separation between the fringes set up by either star is equal and dependent solely on a. Yet the visibility varies with h. Thus if h is increased from nearly zero until $\bar{k}_0 h\theta = \pi$, that is, until

$$h = \frac{\bar{\lambda}_0}{2\theta}, \tag{12.27}$$

the two fringe systems take on an increasing relative displacement, until finally the maxima from one star overlap the minima from the other, at which point, if the irradiances are equal, $\mathcal{V} = 0$. Hence, when the fringes vanish, one need only measure h to determine the angular separation between the stars, θ. Notice that the appropriate value of h varies inversely with θ.

Note that even though the source points, the two stars, are assumed to be completely uncorrelated, the resulting optical fields at any two points (M_1 and M_2) are not necessarily incoherent. For that matter, as h becomes very small, the light from each point source arrives with essentially zero relative phase at M_1 and M_2; $\mathcal{V}$ approaches 1, and the fields at those locations are highly coherent.

In much the same way as with a double star system, the angular diameter (θ) of certain single stars can be measured. Once again the fringe visibility corresponds to the degree of coherence of the optical field at M_1 and M_2. If the star is assumed to be a circular distribution of incoherent point sources such that it has a uniform brilliance, its visibility is equivalent to that already plotted in Fig. 12.7. Earlier, we alluded to the fact that $\mathcal{V}$ for this sort of source was given by a first-order Bessel function, and in fact it is expressible as

$$\mathcal{V} = |\tilde{\gamma}_{12}(0)| = 2\left|\frac{J_1(\pi h\theta/\bar{\lambda}_0)}{\pi h\theta/\bar{\lambda}_0}\right|. \tag{12.28}$$

Recall that $J_1(u)/u = \frac{1}{2}$ at $u = 0$, and the maximum value of $\mathcal{V}$ is 1. The first zero of $\mathcal{V}$ occurs when $\pi h\theta/\bar{\lambda}_0 = 3.83$, as in Fig. 10.28. Equivalently, the fringes disappear when

$$h = 1.22\frac{\bar{\lambda}_0}{\theta}, \tag{12.29}$$

and as before, one simply measures h to find θ.

In Michelson's arrangement, the two outrigged mirrors were movable on a long girder, which was mounted on the 100-inch reflector of the Mt. Wilson Observatory. Betelgeuse (α Orionis) was the first star whose angular diameter was measured with the device. It's the orange-looking star in the upper left of the constellation Orion. In fact, its name is a contraction for the Arabic phrase meaning *the armpit of the central one* (i.e., Orion). The fringes formed by the interferometer, one cold December night in 1920, were made to vanish at $h = 121$ inches, and with $\bar{\lambda}_0 = 570$ nm, $\theta = 1.22(570 \times 10^{-9})/121(2.54 \times 10^{-2}) = 22.6 \times 10^{-8}$ rad, or 0.047 seconds of arc. Using its known distance, determined from parallax measurements, the star's diameter turned out to be about 240 million miles, or roughly

280 times that of the Sun. Actually, Betelgeuse is an irregular variable star whose maximum diameter is so tremendous that it's larger than the orbit of Mars about the Sun. The main limitation on the use of the stellar interferometer is due to the inconveniently long mirror separations required for all but the largest stars. This is true as well in radio astronomy, where an analogous setup has been widely used to measure the extent of celestial sources of radiofrequency emissions.

Incidentally, we assume, as is often done, that "good" coherence means a visibility of 0.88 or better. For a disk source this occurs when $\pi h\theta/\bar{\lambda}_0$ in Eq. (12.28) equals one, that is when

$$h = 0.32\frac{\bar{\lambda}_0}{\theta}. \qquad (12.30)$$

For a narrow-bandwidth source of diameter D a distance R away, there is an **area of coherence** equal to $\pi(h/2)^2$ over which $|\tilde{\gamma}_{12}| \geq 0.88$. Since $D/R = \theta$,

$$h = 0.32\frac{R\bar{\lambda}_0}{D}. \qquad (12.31)$$

These expressions are very handy for estimating the required physical parameters in an interference or diffraction experiment. For example, if we put a red filter over a 1-mm-diameter disk-shaped flashlight source and stand back 20 m from it, then

$$h = 0.32(20)(600 \times 10^{-9})/10^{-3} = 3.8 \text{ mm},$$

where the mean wavelength is taken as 600 nm. This means that a set of apertures spaced at about h or less should produce nice fringes. Evidently the area of coherence increases with R, and this is why you can always find a distant bright street light to use as a convenient source.

12.4.2 Correlation Interferometry

Let's return for a **moment** to the representation of a disturbance emanating from a thermal source, as discussed in Section 7.10. Here the word *thermal* connotes a light field arising predominantly from the superposition of spontaneously emitted waves issuing from a great many independent atomic sources.* A quasimono[illegible] matic optical field can be represented by

$$E(t) = E_0(t)\cos[\varepsilon(t) - 2\pi\bar{\nu}t]. \qquad [illegible]$$

The amplitude is a relatively slowly varying fun[illegible] time, as is the phase. For that matter, the wave[illegible] undergo tens of thousands of oscillations before[illegible] the amplitude (i.e., the envelope of the field vibratio[illegible] or the phase would change appreciably. Thus[illegible] the coherence time is a measure of the fluctua[illegible] val of the phase, it is also a measure of the interv[illegible] which $E_0(t)$ is fairly predictable. Large fluctuatio[illegible] are generally accompanied by correspondingly[illegible] fluctuations of E_0. Presumably, a knowledge o[illegible] amplitude fluctuations of the field could be relate[illegible] the phase fluctuations and therefore to the correla[illegible] (i.e., coherence) functions. Accordingly, at two poi[illegible] in space–time where the phases of the field are corre[illegible] lated, we could expect the amplitudes to be related [illegible] well.

When a fringe pattern exists for the Michel[illegible] interferometer, it is because the fields at M_1 [illegible] the apertures, are somehow correlated, that is, Γ_{12}[illegible] $\langle \tilde{E}_1(t)\tilde{E}_2^*(t)\rangle \neq 0$. If we could measure the field am[illegible] tudes at these points, their fluctuations would like[illegible] show an interrelationship. Since this isn't practi[illegible] because of the high frequencies involved, we [illegible] instead measure and compare the fluctuations in [illegible] ance at the locations of M_1 and M_2 and [illegible] some as yet unknown way, infer $|\tilde{\gamma}_{12}(0)|$. In o[illegible] words if there are values of τ for which $\tilde{\gamma}_{12}(\tau)$ is n[illegible]ro, the field at the two points is partially coherent, a[illegible] correla tion between the irradiance fluctuations [illegible] locations is implied. This is the essential id[illegible] series of remarkable experiments conducted [illegible] 1952 to 1956 by R. Hanbury-Brown in co[illegible] with R. Q. Twiss and others. The culminati[illegible] work was the so-called *correlation interferomete*[illegible]

Thus far we have evolved only an intui[illegible] tification for the phenomenon rather than a firm[illegible] retical treatment. Such an analysis, however, is beyo[illegible]

* Thermal light is sometimes spoken of as *Gaussian* [illegible] amplitude of the field follows a Gaussian probability [illegible]

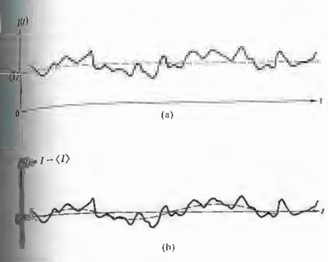


Figure 12.14 Irradiance variations.

[illegible]ope of this discussion, and we shall have to content [illegible]ves with merely outlining its salient features.* Just [illegible] (12.14), we are interested in determining the [illegible]correlation function, this time, of the irradiances [illegible] points in a partially coherent field, $\langle I_1(t+\tau)I_2(t)\rangle$. [illegible]tributing wavetrains, which are again represen[illegible] complex fields, are assumed to have been randomly emitted in accord with Gaussian statistics, with the fi[illegible] result that

$$\langle I_1(t+\tau)I_2(t)\rangle = \langle I_1\rangle\langle I_2\rangle + |\tilde{\Gamma}_{12}(\tau)|^2 \qquad (12.32)$$

or

$$\langle I_1(t+\tau)I_2(t)\rangle = \langle I_1\rangle\langle I_2\rangle[1 + |\tilde{\gamma}_{12}(\tau)|^2]. \qquad (12.33)$$

The [illegible]stantaneous irradiance fluctuations $\Delta I_1(t)$ and [illegible] given by the variations of the instantaneous [illegible] $I_1(t)$ and $I_2(t)$ about their mean values $\langle I_1(t)\rangle$ and $\langle I$[illegible]$\rangle$, as in Fig. 12.14. Consequently if we use

$$[illegible](t) = I_1(t) - \langle I_1\rangle, \qquad \Delta I_2(t) = I_2(t) - \langle I_2\rangle$$

[illegible] fact that

$$\langle \Delta I_1(t)\rangle = 0 \quad \text{and} \quad \langle \Delta I_2(t)\rangle = 0,$$

[illegible] for example, L. Mandel, "Fluctu[illegible]," [illegible] *Optics*, Vol. II, p. 193, or Françon, [illegible] p. 182.

Eqs. (12.32) and (12.33) become

$$\langle \Delta I_1(t+\tau)\Delta I_2(t)\rangle = |\tilde{\Gamma}_{12}(\tau)|^2 \qquad (12.34)$$

or

$$\langle \Delta I_1(t+\tau)\Delta I_2(t)\rangle = \langle I_1\rangle\langle I_2\rangle|\tilde{\gamma}_{12}(\tau)|^2 \qquad (12.35)$$

(Problem 12.11). These are the desired cross-correlations of the irradiance fluctuations. They exist as long as the field is partially coherent at the two points in question. Incidentally, these expressions correspond to linearly polarized light. When the wave is unpolarized, a multiplicative factor of $\frac{1}{2}$ must be introduced on the right-hand side.

The validity of the principle of correlation interferometry was first established in the radiofrequency region of the spectrum, where signal detection was a fairly straightforward matter. Soon afterward, in 1956, Hanbury-Brown and Twiss proposed the optical stellar interferometer illustrated in Fig. 12.15. But the only suitable detectors that could be used at optical frequencies were photoelectric devices whose very operation is keyed to the quantized nature of the light field. Thus

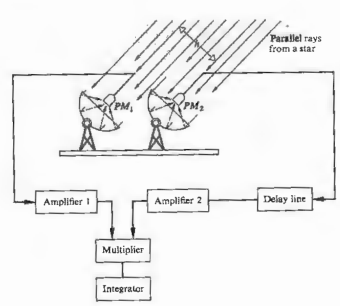


Figure 12.15 Stellar correlation interferometer.

> . . . it was by no means certain that the correlation would be fully preserved in the process of photo-electric emission. For these reasons a laboratory experiment was carried out as described below.*

That experiment is shown in Fig. (12.16). Filtered light from a Hg arc was passed through a rectangular aperture, and different portions of the emerging wavefront were sampled by two photomultipliers, PM_1 and PM_2. The degree of coherence was altered by moving PM_1, that is, by varying h. The signals from the two photomultipliers were presumably proportional to the incident irradiances $I_1(t)$ and $I_2(t)$. These were then filtered and amplified, such that the steady, or dc, component of each of the signals (being proportional to $\langle I_1\rangle$ and $\langle I_2\rangle$) was removed, leaving only the fluctuations, in other words, $\Delta I_1(t) = I_1(t) - \langle I_1\rangle$ and $\Delta I_2(t) = I_2(t) - \langle I_2\rangle$. The two signals were then multiplied together in the correlator, and the time average of the product, which was proportional to $\langle \Delta I_1(t)\Delta I_2(t)\rangle$, was finally recorded. The values of $|\tilde{\gamma}_{12}(0)|^2$ for various separations, h, as deduced experimentally via Eq. (12.35), were in fine agreement with those calculated from theory. For the given geometry, the correlation definitely existed; moreover, it was preserved through photoelectric detection.

The irradiance fluctuations have a frequency bandwidth roughly equivalent to the bandwidth ($\Delta\nu$) of the incident light, in other words, $(\Delta t_c)^{-1}$, which is about 100 MHz or more. This is much better than trying to follow the field alternations at 10^{15} Hz. Even so, fast circuitry with roughly a 100-MHz pass bandwidth is required. In actuality the detectors have a finite resolving time T, so that the signal currents $\mathcal{I}_1$ and $\mathcal{I}_2$ are actually proportional to averages of $I_1(t)$ and $I_2(t)$ over T and not their instantaneous values. In effect, the measured fluctuations are smoothed out, as illustrated by the dashed curve of Fig. 12.14(b). For $T > \Delta t_c$, which is normally the case, this just leads to a reduction, by a factor of $\Delta t_c/T$, in the correlation actually observed:

$$\langle \Delta\mathcal{I}_1(t)\Delta\mathcal{I}_2(t)\rangle = \langle \mathcal{I}_1\rangle\langle \mathcal{I}_2\rangle \frac{\Delta t_c}{T}|\tilde{\gamma}_{12}(0)|^2 \qquad (12.36)$$

* Taken from R. Hanbury-Brown and R. Q. Twiss, "Correlation Between Photons in Two Coherent Beams of Light," *Nature* 127, 27 (1956).

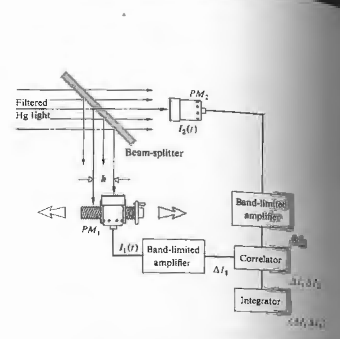


Figure 12.16 Hanbury-Brown and Twiss experiment.

For example, in the preceding laboratory arra[illegible] the filtered mercury light had a coherence time [illegible] 1 ns, while the electronics had a reciprocal pass ban[illegible] width or effective integration time of ≈40 ns. Note th[illegible] Eq. (12.36) isn't any different conceptually from Eq. (12.35)—it's just been made a bit more realis[illegible]

Shortly after their successful laboratory ex[illegible] Hanbury-Brown and Twiss constructed the [illegible] ferometer shown in Fig. 12.15. Searchlight mirro[illegible] used to collect starlight and focus it onto two [illegible] multipliers. One arm contained a delay line, so [illegible] mirrors could physically be located at the same heig[illegible] with compensation for any differences in the arr[illegible] times of the light. The measurement of $\langle \Delta\mathcal{I}_1(t)\Delta$[illegible] at various separations of the detectors allowed [illegible] square of the modulus of the degree of coherence, $|\tilde{\gamma}_{12}(0)|^2$, to be deduced, and this in turn yielded the angular diameter of the source, just as it did with the Michelson stellar interferometer. This time, however, the separation h could be very large, because one no longer had to worry about messing up the phase of waves, as was the case in the Michelson device. T[illegible] a slight shift in a mirror of a fraction of a [illegible] was fatal. Here, in contrast, the phase was [illegible] so that the mirrors didn't even have to be of [illegible]

[illegible] The star Sirius was the first to be examined, [illegible]was found to have an angular diameter of 0.0069 [illegible] of arc. More recently, a correlation inter[illegible]ter with a baseline of 618 feet has been constructed at Narrabri, Australia. For certain stars, angular [illegible]meters of as little as 0.0005 seconds of arc can be [illegible]red with this instrument—that's a long way from [illegible] angular diameter of Betelgeuse (0.047 seconds of [illegible]).†

The electronics involved in irradiance correlation [illegible] be greatly simplified if the incident light were [illegible]early monochromatic and of considerably higher [illegible]nsity. Laser light isn't thermal and doesn't display [illegible] statistical fluctuations, but it can nonetheless be used to generate *pseudothermal*‡ light. A pseudo[illegible] source is composed of an ordinary bright source (a laser is most convenient) and a moving [illegible] of *nonuniform* optical thickness, such as a rotat[illegible]ound glass disk. If the scattered beam emerging from a stationary piece of ground glass is examined [illegible] *sufficiently slow detector*, the inherent irradiance [illegible]tions will be smoothed out completely. By setting [illegible]round glass in motion, irradiance fluctuations [illegible] with a simulated coherence time commensurate [illegible]he disk's speed. In effect, one has an extremely [illegible]t thermal source of variable Δt_c (from, say, 1 s [illegible]s), which can be used to examine a whole range [illegible]herence effects. For example, Fig. 12.17 shows the [illegible]lation function, which is proportional to [illegible]$/(u)]^2$, for a pseudothermal circular aperture [illegible] determined from irradiance fluctuations. The [illegible]ment setup resembles that of Fig. 12.16, although [illegible]ctronics is considerably simpler.§

[illegible]cussion of the photon aspects of irradiance correlation, see [illegible] *Optical Physics*, Section 6.2.5.2, or Klein, *Optics*, Section 6.4.

[illegible]Martienssen and E. Spiller, "Coherence and Fluctuations in [illegible]ms," *Am. J. Phys.* 32, 919 (1964), and A. B. Haner and [illegible]nor, "Intensity Correlations from Pseudothermal Light [illegible] *Am. J. Phys.* 38, 748 (1970). Both of these articles are well [illegible]udying.

[illegible]overall reference for this chapter is the review article by L. [illegible] E. Wolf, "Coherence Properties of Optical Fields," *Revs.* [illegible] 37, 231 (1965); this is rather heavy reading. Take a look [illegible]ermann, "Intercontinental Radio Astronomy," *Sci. Am.* [illegible]bruary 1972).

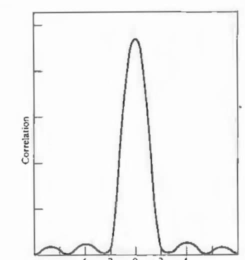


Figure 12.17 A correlation function for a pseudothermal source. [From A. B. Haner and N. R. Isenor, *Am. J. Phys.*, 38, 748 (1970).]

PROBLEMS

12.1 Suppose we set up a fringe pattern using a Michelson interferometer with a mercury vapor lamp as the source. Switch on the lamp in your mind's eye and discuss what will happen to the fringes as the mercury vapor pressure builds to its steady state value.

12.2* We wish to examine the irradiance produced on the plane of observation in Young's experiment when the slits are illuminated simultaneously by two monochromatic plane waves of somewhat different frequency, E_1 and E_2. Sketch these against time, taking $\lambda_1 = 0.8\,\lambda_2$. Now draw the product E_1E_2 (at a point P) against time. What can you say about its average over a relatively long interval? What does $(E_1 + E_2)^2$ look like? Compare it with $E_1^2 + E_2^2$. Over a time that is long compared with the periods of the waves, approximate $\langle (E_1 + E_2)^2\rangle$.

12.3* With the previous problem in mind, now consider things spread across space at a given moment in time. Each wave separately would result in an irradiance distribution I_1 and I_2. Plot both on the same space axis and then draw their sum $I_1 + I_2$. Discuss the meaning of your results. Compare your work with Fig. 7.9. What happens to the net irradiance as more waves of different frequency are added in? Explain in terms of the coherence length. Hypothetically, what would happen to the pattern as the frequency bandwidth approached infinity?

12.4 With the previous problem in mind, return to the autocorrelation of a sine function, shown in Fig. 11.37. Now suppose we have a signal composed of a great many sinusoidal components. Imagine that you take the autocorrelation of this complicated signal and plot the result (use three or four components to start with), as in part (e) of Fig. 11.37. What will the autocorrelation function look like when the number of waves is very large and the signal resembles random noise? What is the significance of the $\tau = 0$ value? How does this compare with the previous problem?

12.5* Imagine that we have the arrangement depicted in Fig. 12.3. If the separation between fringes (max. to max.) is 1 mm and if the projected width of the source slit on the screen is 0.5 mm, compute the visibility.

12.6 Referring to the slit source and pinhole screen arrangement of Fig. 12.18, show by integration over the source that

$$I(Y) \propto b + \frac{\sin(\pi a/\lambda l)b}{\pi a/\lambda l}\cos(2\pi a Y/\lambda s).$$

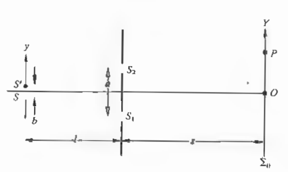


Figure 12.18

12.7 Carry out the details leading to the expression for the visibility given by Eq. (12.22).

12.8 Under what circumstances will the irradiance on Σ_o in Fig. 12.19 be equal to $4I_0$, where I_0 is the irradiance due to either incoherent point source alone?

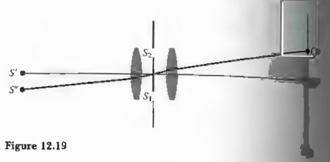


Figure 12.19

12.9* Suppose we set up Young's experiment with a small circular hole of diameter 0.1 mm in front of a sodium lamp ($\bar{\lambda}_0 = 589.3$ nm) as the source. If the distance from the source to the slits is 1 m, how far apart will the slits be when the fringe pattern disappears?

12.10 Taking the angular diameter of the S[illegible] from the Earth to be about 1/2°, determine the [illegible] of the corresponding area of coherence, neg[illegible] variations in brightness across the surface.

12.11 Show that Eqs. (12.34) and (12.35) follow from Eqs. (12.32) and (12.33).

12.12* Return to Eq. (12.21) and separate it into [illegible] terms representing a coherent and an incoherent [illegible] bution, the first arising from the superposition of [illegible] coherent waves with irradiances of $|\tilde{\gamma}_{12}(\tau)|I_1$ and $|\tilde{\gamma}_{12}(\tau)|I_2$ having a relative phase of $\alpha_{12}(\tau) - \varphi$, and the second from the superposition of incoherent waves of irradiance $[1 - |\tilde{\gamma}_{12}(\tau)|]I_1$ and $[1 - |\tilde{\gamma}_{12}(\tau)|]I_2$. N[illegible] derive expressions for I_{coh}/I_{incoh} and for I[illegible]. Discuss the physical significance of this alternative [illegible] mulation and how we might view the visibility of [illegible] in terms of it.

12.13 Imagine that we have Young's experiment, where one of the two pinholes is now covered by a neutral-density filter that cuts the irradiance by a factor of 10, and the other hole is covered by a transparent sheet of glass, so there is no relative phase shift introduced. Compute the visibility in the hypothetical case of completely coherent illumination.

12.14* Suppose that Young's double-slit apparatus is illuminated by sunlight with a mean wavelength of 550 nm. Determine the separation of the slits that would cause the fringes to vanish.

12.15 We wish to construct a double-pinhole setup [illegible]inated by a uniform, quasimonochromatic, inco[illegible] slit source of mean wavelength 500 nm and width [illegible] distance of 1.5 m from the aperture screen. If the [illegible] are 0.50 mm apart, how wide can the source [illegible] visibility of the fringes on the plane of observation is not to be less than 85%?

12.16* Suppose that we have an incoherent, quasi[illegible]chromatic, uniform slit source, such as a dis[illegible] lamp with a mask and filter in front of it. We [illegible] illuminate a region on an aperture screen 10.0 m [illegible] such that the modulus of the complex degree of [illegible]nce everywhere within a region 1.0 mm wide is [illegible] or greater than 90% when the wavelength is 500 nm. How wide can the slit be?

12.17* Figure 12.20 shows two incoherent quasimonochromatic point sources illuminating two pinholes in a mask. Show that the fringes formed on the plane of observation have minimum visibility when

$$a(\alpha_2 - \alpha_1) = \tfrac{1}{2}m,$$

where $m = \pm 1, \pm 3, \pm 5, \ldots$

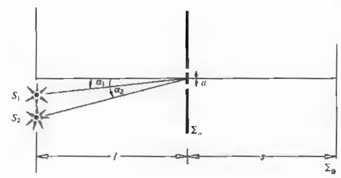


Figure 12.20

12.18 Imagine that we have a wide quasimonochromatic source ($\lambda = 500$ nm) consisting of a series of vertical, incoherent, infinitesimally narrow line sources, each separated by 500 μm. This is used to illuminate a pair of exceedingly narrow vertical slits in an aperture screen 2.0 m away. How far apart should the apertures be to create a fringe system of maximum visibility?

13 SOME ASPECTS OF THE QUANTUM NATURE OF LIGHT

Our understanding of the physical world has changed in a most profound manner since the beginning of this century. We have come to appreciate fundamental similarities between all of the various forms of radiant energy and matter. Optics, which was traditionally the study of light, has broadened its domain to encompass the entire electromagnetic spectrum. Moreover, the advent of quantum mechanics has brought with it yet another extension into what might be called *matter optics* (e.g., electron and neutron diffraction).

Our main purpose in this chapter conceptually is to weave some of the basic ideas of quantum mechanics into the fabric of optics.

13.1 QUANTUM FIELDS

The nineteenth-century physicist envisioned the electromagnetic field as a disturbance of the all-pervading aether medium. If two charges interacted, it was because the aether in which they were imbedded was distorted by their presence, and the resulting *strain* was transmitted from one to the other. Maxwell's field equations described this measurable disturbance of the medium without explicitly discussing the aether itself. Light was then simply a wavetrain consisting of oscillatory mechanical stresses within the aether. Since there were electromagnetic waves, there had to be a transmitting medium—it was as clear as that. Yet curiously enough, even after the Michelson-Morley experiment (Section 9.10.3) and Einstein's special theory of relativity had put aside the aether hypothesis, Maxwell's equations remained. Even though the entire imagery had to be changed, the validity of those equations persisted. There seemed little conceptual alternative; the field itself had to be a physical entity, independent of any medium and capable of traversing otherwise empty space. An electromagnetic wave was seen as a disturbance propagated in the electromagnetic field.

In the early part of this century it became evident that although Maxwell's equations seemed to be the truth, they could not be the whole truth. The field was real enough, but experiments were starting to reveal behavior inconsistent with the representation of the field exclusively as a fluid-like continuum. The electromagnetic field displayed particle-like properties in that it was emitted and absorbed in lumps [illegible] and not at all continuously. Even in the [illegible] the formative years of quantum theory, field [illegible] cles were envisioned as separate entities. [illegible] became evident, with the melding of quantum [illegible] and relativity, that each particle, material or [illegible] could be envisioned as a quantized manifest[illegible] distinct field (e.g., the photon is a quantum [illegible] electromagnetic field). As with the photon, [illegible] particles can be created and destroyed. Their corresponding fields can transport all observable physical characteristics, such as energy, charge, and [illegible] advancing through space as waves. Within the con[illegible] of quantum field theory, as this description is cal[illegible] particles are viewed essentially as localized packet[illegible]

field energy. Another far-reaching distinction between this and the classical picture is in the consideration of interactions. Quantum field theory maintains that all interactions arise from the creation and annihilation of particles. To wit, forces, in the classical sense, are envisioned as due to the exchange of quanta or lumps of the field in question. Charged particles can interact by absorbing and emitting, in a mutual exchange, quanta of the electromagnetic field, that is, photons. [illegible] the gravitational interaction is similarly the [illegible] of an exchange of quanta of the gravitational field, gravitons.

[illegible] then is something of a cursory view of the direction taken by contemporary quantum field theory. In the next few sections we will consider some of the [illegible]ments that led to the development of the quantum-mechanical photon picture.

13.2 BLACKBODY RADIATION—PLANCK'S QUANTUM HYPOTHESIS

[illegible] the turn of the nineteenth century, the electromag[illegible] theory of light, fashioned by Maxwell and meticulously verified by Hertz, was firmly established as one of the cornerstones of science. But periods of [illegible]ment in physics are usually short-lived, and Max [illegible] in 1900 unleashed a conceptual whirlwind that [illegible] led to a radical change in the picture of the [illegible]cal universe. Planck, who had been a student of [illegible]holtz and Kirchhoff, was working on a theoretical [illegible]sis of a seemingly obscure phenomenon known as [illegible]*body radiation*. We know that if an object is in ther[illegible] equilibrium with its environment, it must emit as [illegible] radiant energy as it absorbs. It follows that a good [illegible]er is a good emitter. *A perfect absorber, one which [illegible] all radiant energy incident upon it, regardless of [illegible]ngth, is said to be a blackbody.* Generally, one [illegible]imates a blackbody in the laboratory by a hollow [illegible]ed enclosure (an oven) that contains a small hole [illegible] the wall. Radiant energy entering the hole has little [illegible] of being reflected out again, so that the enclosure [illegible] as a nearly perfect absorber. The "black" pupil of the eye suggests the mechanism. On the other hand, if the oven is heated, it can serve as a source emitting energy through the hole. In accord with common experience, we can anticipate that the spectral distribution of the emitted radiant energy will be dependent on the oven's absolute temperature T. As the temperature increases, the hole will initially radiate predominantly infrared, and then gradually it will take on a faint reddish glow that gets brighter and brighter, shifting to yellow, white, and finally blue-white. Experimental investigations (notably by O. Lummer and E. Pringsheim, 1899) resulted in spectral curves similar to those of Fig. 13.1. The quantity $I_{e\lambda}$, which is plotted as the ordinate, is known as the *spectral flux density* or *spectral exitance*. It corresponds to the emitted power per unit area per unit wavelength interval leaving the hole. Were we to make such measurements, at least in principle, we could determine the exitance (in W/m^2) from the blackbody at a given wavelength λ, using some sort of power meter. But in actuality, any such meter would accept a range of wavelengths $\Delta\lambda$ centered about λ, so we introduce the notion of *spectral* exitance. The curves of $I_{e\lambda}$ versus λ can be plotted so that the area beneath them is measured in W/m^2. Notice how the peaks in the curves shift toward the shorter wavelengths as T increases.

In 1879 Josef Stefan (1835–1893) observed that the total radiant flux density (or exitance, I_e) of a blackbody

Figure 13.1 Blackbody radiation curves. The hyperbola passing through peak points corresponds to Wen's law.

was proportional to the fourth power of its absolute temperature. A few years later, Ludwig Boltzmann (1844–1906) derived that relationship in a combined application of Maxwell's theory and thermodynamic arguments. The *Stefan–Boltzmann law*, as it is now called, is

$$I_e = \sigma T^4, \qquad (13.1)$$

where the Stefan–Boltzmann constant σ is equal to $(5.6697 \pm 0.0029) \times 10^{-8}$ W m^{-2} K^{-4}. The last notable success in applying classical theory to the problem of blackbody radiation came in 1893 at the hands of the German physicist and Nobel laureate Wilhelm Carl Werner Otto Fritz Franz Wien (1864–1928), known to his friends as Willy. He was able to show that the wavelength, λ_{max}, at which $I_{e\lambda}$ (the flux density *per unit wavelength interval* emerging from the blackbody) is a maximum, varies as

$$\lambda_{max} T = 2.8978 \times 10^{-3} \text{ m K}. \qquad (13.2)$$

As T increases, λ_{max} decreases, and the peaks are displaced, as we have already pointed out in connection with Fig. 13.1. Accordingly, the expression (13.2) is known as *Wien's displacement law.*

It was at this point in time that classical theory began to falter. All attempts to fit the entire radiation curve (Fig. 13.1) with some theoretical expression based on electromagnetism led only to the most limited successes. Wien produced a formula that agreed with the observed data fairly well in the short wavelength region but deviated from it substantially at large λ. Lord Rayleigh [John William Strutt (1824–1919)] and later Sir James Jeans (1877–1946) developed a description in terms of the standing wave modes of the field within the enclosure. But the resulting *Rayleigh–Jeans formula* matched the experimental curves only in the very long wavelength region. The failure of classical theory was totally inexplicable; a turning point in the history of physics had arrived.

Planck's approach to the problem was a rather systematic and practical one. He first matched the observed data with an empirical expression. Then he set about finding a physical justification for that expression within the framework of thermodynamics. In effect his model pictured the atoms in the walls of the oven to be in thermal equilibrium with the enclosed rad[illegible] field. He presumed that the atoms behaved lik[illegible] oscillators, absorbing and emitting radiant en[illegible] further assumed that all oscillator frequencie[illegible] possible, and thus every frequency should b[illegible] in the emitted spectrum. All else having [illegible] regretfully turned to the method of Boltzm[illegible] which he had little familiarity and less confid[illegible] apply this statistical analysis he introduced a [illegible] unprecedented *ad hoc* assumption whose [illegible] tification was a pragmatic one—it worked. [illegible] ted that *an atomic resonator could absorb or emit* [illegible] *amounts of energy that were proportional to its* [illegible] *frequency. Moreover, each such energy value had* [illegible] *an integral multiple of what he called an* "*energy elem*[illegible] *hν.* Thus all possible oscillator energies $\mathscr{E}_m$ are given by

$$\mathscr{E}_m = mh\nu, \qquad (13.3)$$

where m is a positive integer and h is a constan[illegible] determined by fitting the actual data. After bring[illegible] bear statistical arguments, which are of little con[illegible] here (and not actually correct anyhow),* Plan[illegible] the following formula for the spectral exitan[illegible] he had already arrived at by fitting curves to [illegible]

$$I_{e\lambda} = \frac{2\pi hc^2}{\lambda^5}\left[\frac{1}{e^{hc/\lambda kT} - 1}\right]. \qquad (13.4)$$

Here k is Boltzmann's constant. Planck's r[illegible] on law as given by Eq. (13.4), is in extremely good [illegible] eement with experimental results when h is chosen [illegible] ately. The currently accepted value of Planck's [illegible] is

$$h = (6.6256 \pm 0.0005) \times 10^{-34} \text{ J s}.$$

The hypothesis that energy was emitted a[illegible] in quanta of $h\nu$ (which initially seemed only [illegible] tional contrivance) has proved to be a fun[illegible] statement of the nature of things. Moreover, [illegible] tity h, rather than simply being a particular c[illegible] parameter, has shown itself to be a univers[illegible] of the greatest importance. Nonetheless, we shou[illegible] point out that the true significance of Planck's work went unappreciated for several years, and even he was rather cautious, as witnessed by this commentary on the derivation:*

> It is true that we shall not thereby prove that this hypothesis represents the only possible or even the most adequate expression of the elementary dynamical law of the vibration of oscillators. On the contrary I think it very probable that it may be greatly improved as regards form and contents . . . and as long as no contradiction in itself or with experiment is discovered in it, and as long as no more adequate hypothesis can be advanced to replace it, it may justly claim a certain importance.

* Planck's original derivation leads to erroneous p[illegible] *mhν*, but it was later correctly reformulated by Bose [illegible] Einstein.

† Don't confuse this with spectral energy density, which [illegible] uals $4I_{e\lambda}$

13.3 THE PHOTOELECTRIC EFFECT — EINSTEIN'S PHOTON CONCEPT

[illegible]ather ironical that Heinrich Hertz, who helped to [illegible]lish the classical wave picture of radiant energy, [illegible] unwitting contributor to its ultimate reformula-[illegible] This came by way of his discovery of the **photoelectric** [illegible] whose description first appeared in 1887 in a [illegible] entitled "On an Effect of Ultraviolet Light upon [illegible] Electric Discharge." While engaged in his now [illegible] experiments on electromagnetic waves (Section [illegible] noticed that the spark induced in his receiving [illegible] was stronger when the terminals of the gap were [illegible]ated by the light coming from the primary spark. [illegible] able to establish that the effect was most pro-[illegible]nced when ultraviolet impinged on the negative [illegible]inal of the gap, but he did not pursue the work [illegible]ther. Later, in 1889, Wilhelm Hallwachs (1859–[illegible] showed that negative particles were released from [illegible] illuminated metal surfaces, such as zinc, [illegible]ium, and potassium. Thereafter Philipp Eduard [illegible]on von Lenard (1862–1947), who was a colleague [illegible] Hertz, measured the charge-to-mass ratio of these [illegible]ticles, thus confirming that the spark enhancement [illegible]rved by Hertz was the result of the emission of [illegible] (now referred to as *photoelectrons*). Using [illegible]vices that were similar in principle to the one depicted in Fig. 13.2, a number of researchers began to accrue data on the **photoelectric effect, that is, *the process whereby electrons are liberated from materials under the action of radiant energy.*** It soon became apparent that the photoelectric effect was another instance in which classical electromagnetic theory was paradoxically impotent. This protracted dilemma was finally resolved by Einstein in a brilliant paper appearing in the *Annalen der Physik* of 1905.* It was there that he boldly extended Planck's quantum hypothesis and in so doing gave impetus to the sweeping reinterpretation of classical physics that was to take place later in the 1920s. Let's

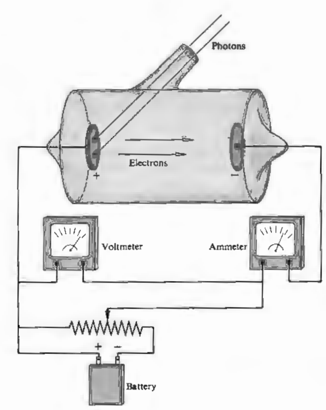


Figure 13.2 Setup to observe the photoelectric effect.

* M. Pla[illegible] and M. Masius, *The Theory of Heat Radiation.*

* 1905 was a good year for Einstein. It was then, at the age of about 26, that he published his theories of special relativity, Brownian motion, and the photoelectric effect. Nonetheless, he once confided in a friend that his theory of the photoelectric effect was the result of five years of thinking about Planck's hypothesis.

now set the scene (c. 1905) so that we can appreciate how insightful Einstein's work actually was in light of the limited existent data.

The early experiments of J. Elster and H. Geitel in 1889 had revealed that photoelectrons were frequently forcibly ejected from the illuminated metal surfaces under study. Electrons apparently emerged with small but finite speeds ranging from zero to some maximum value, v_{max}. By making the collecting plate negative with respect to the illuminated plate, a retarding force could be exerted on the electrons. The retarding voltage, which would stop even the most energetic electrons from reaching the collector, thereby bringing the photocurrent to zero, is known as the *stopping potential* V_0. Thus

$$\tfrac{1}{2}m_0 v_{max}^2 = q_e V_0, \qquad (13.5)$$

where m_0 is the rest mass of the electron. Figure 13.3(a) depicts the manner in which the *photocurrent* i_p varies as the retarding voltage V is altered. There is nothing about Fig. 13.3(a) that is at variance with the classical picture. The distribution in energy of the emerging electrons, which manifests itself in the gradual drop-off of the curve, can satisfactorily be attributed to differences in the energy binding the various electrons to the metal. Electrons do not spontaneously escape from metal surfaces, so that such binding is quite reasonable.

In 1893 it was observed that i_p was directly proportional to the incident irradiance, I, as indicated in Fig. 13.3(b). This too represented no departure from the classical scheme. Increasing I increases the total energy absorbed by the surface and should thus yield a proportionately larger number of emitted photoelectrons.

In contrast, it had early been established that there was no discernible time delay between the instant the plate was illuminated and the initiation of photoemission. This behavior is completely incomprehensible within the context of the classical description. For example, if $I = 10^{-10}$ W/m² (at $\lambda_0 = 500$ nm), theory predicts (Problem 13.10) that it might take about 10 hours before electrons could accumulate the amount of energy they had been observed to possess. To the contrary, Elster and Geitel, working with an even smaller irradiance, found no measurable time lag whatever.

In 1902 Lenard discovered that for a given metal the

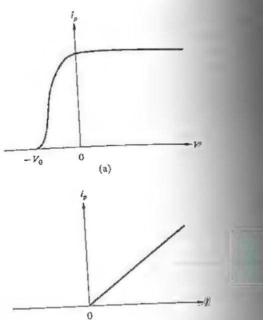


Figure 13.3 (a) Photocurrent versus voltage. (b) Photo[illegible] irradiance.

stopping potential, and therefore the maxim[illegible] energy, was independent of the radiant [illegible] arriving at the plate, as shown schematically in [illegible] He determined that even though the incident [illegible] was varied 70-fold, it did not alter V_0 by even [illegible] result led to yet another conundrum. It was w[illegible] that the maximum kinetic energy of the photo[illegible] depended on the source being used. Yet Lena[illegible] showed that this energy was independent o[illegible] could only conclude that the maximum kinetic [illegible] varied in some way with the frequency of the [illegible] and not with the total incident energy—a perp[illegible] result indeed. Furthermore, recall that Hertz, [illegible] original experiment, pointed out that ultravio[illegible] ation rather than visible light was the effective [illegible] This implied that as the frequency of the radia[illegible] increased, a threshold value was reached, a[illegible] photoelectrons were emitted. But this too wa[illegible] inexplicable; whether or not emission takes p[illegible] depend on I and not on ν.

The quintessence of Planck's original hyp[illegible] that the energy of the radiation field could only *change* by discrete quanta, that is, integer multiples of $h\nu$. This was a consequence of the fact that he had quantized the energy of the electric oscillators. Going far beyond this, Einstein proposed that *the radiation field itself was quantized, and thus energy could be absorbed from it only in quanta of* $h\nu$ (later called *photons*). The mechanism of the photoelectric effect now becomes quite clear. Envision an electron, within the interior of the material, which has absorbed a photon $h\nu$. In rising to the surface it will lose some of that energy, and in escaping from the surface it will lose even more. Let the total energy spent in leaving the material be Φ. The difference between $h\nu$ and Φ appears in the form of kinetic energy:

$$h\nu = \frac{mv^2}{2} + \Phi. \qquad (13.6)$$

[illegible] the electron happens to be at the surface, Φ has its minimum value Φ_0. Known as the *work function*, Φ_0 simply corresponds to the energy needed by an electron [illegible] free of the surface (see Table 13.1). In that special case

$$h\nu = \frac{mv_{max}^2}{2} + \Phi_0, \qquad (13.7)$$

[illegible]being a statement of *Einstein's photoelectric equation.* The lowest or *threshold frequency* (ν_0) capable of promoting emission would just barely eject the electrons. To wit, $v_{max} \approx 0$ and

$$\nu_0 = \Phi_0/h. \qquad (13.8)$$

Table 13.1 Photoelectric threshold frequencies and work functions for a few metals.

Metal		ν_0(THz)	Φ_0(eV)
Cesium	Cs	460	1.9
Beryllium	Be	940	3.9
Titanium	Ti	990	~4.1
Mercury	Hg	1100	4.5
Nickel	Ni	1210	5.0
Platinum	Pt	1530	6.3

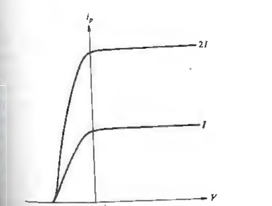


Figure 13.4 The stopping potential is independent of the irradiance.

In the photon picture, an electron literally absorbs a blast of energy as opposed to a gradual trickle. Accordingly, there will be no appreciable time delay in the emission. The interrelationship between irradiance and photocurrent is also quite understandable. An increase in I corresponds to more photons of the same energy and thus an increase in i_p but not in V_0.

The quantum theory rather neatly accounts for the existence of a threshold frequency, the dependence of $(mv_{max}^2/2)$ on ν, the lack of a time lag, the independence of V_0 on I, and the relationship of I to i_p. Even so, since quantitative data were scanty and the photon so radical an idea it remained unaccepted by many.

The photoelectric equation went even further than accounting for all of the known observations; it also represented one of the great prognostications of all times. After it had been published, a great flurry of experimental work brought with it all sorts of confirmation. The proportionality between I and i_p was extended over a range of 5×10^7 in irradiance. Ernest O. Lawrence and J. W. Beams (1928) used a Kerr cell to create pulses of light and therewith found that if a time lag existed in the emission of electrons, it had to be less than* 3×10^{-9} s. In 1916 the American physicist Robert Andrews Millikan (1868–1953) published an extensive and remarkably accurate study of the relationship of Einstein's equation and the photoelectric effect. His own

* E. O. Lawrence and J. W. Beams, "The Element of Time in the Photoelectric Effect," *Phys. Rev.* 32, 478 (1928).

words on the subject are quite enlightening:

> I spent ten years of my life testing the 1905 equation of Einstein's and contrary to all my expectations, I was compelled in 1915 to assert its unambiguous experimental verification in spite of its unreasonableness since it seemed to violate everything that we knew about the interference of light.

A representation of Millikan's results is shown in Fig. 13.5. Note that since $\nu_0 = \Phi_0/h$, we can write

$$\frac{mv_{\max}^2}{2} = h(\nu - \nu_0), \qquad (13.9)$$

which means that a plot of maximum kinetic energy (q_eV_0) versus ν for any given material should be a straight line having a slope h and an intercept of $-\Phi_0$. These predictions were completely confirmed by Millikan.* The amazing fact that the slope actually turned out to be equal to h is a tribute to the insight of Planck and the genius of Einstein. Different metals have characteristic values of Φ_0 and ν_0, but in all cases the slope of the line remained constant at h, as predicted.

The quantization of the electromagnetic field had been established; all of physics, and particularly optics, would never quite be the same again.†

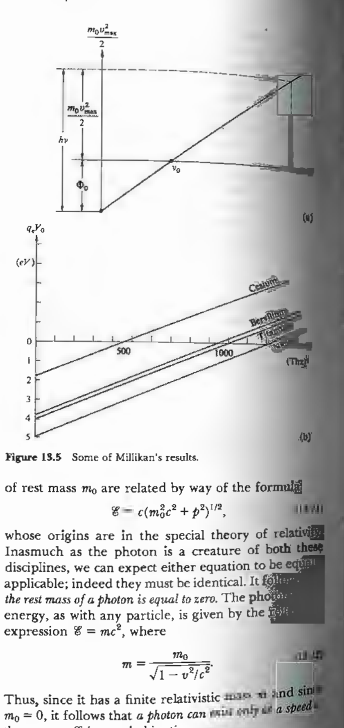


Figure 13.5 Some of Millikan's results.

13.4 PARTICLES AND WAVES

According to Maxwell's electromagnetic theory (see Chapter 3), the energy $\mathscr{E}$ and momentum p of an electromagnetic wave are related by the expression

$$\mathscr{E} = cp. \qquad (13.10)$$

Alternatively, the energy and momentum of a particle of rest mass m_0 are related by way of the formula

$$\mathscr{E} = c(m_0^2c^2 + p^2)^{1/2}, \qquad (13.11)$$

whose origins are in the special theory of relativity. Inasmuch as the photon is a creature of both these disciplines, we can expect either equation to be equally applicable; indeed they must be identical. It follows that *the rest mass of a photon is equal to zero.* The photon's energy, as with any particle, is given by the [illegible] expression $\mathscr{E} = mc^2$, where

$$m = \frac{m_0}{\sqrt{1 - v^2/c^2}}. \qquad (13.12)$$

Thus, since it has a finite relativistic mass m and since $m_0 = 0$, it follows that *a photon can exist only at a speed* [illegible] the energy $\mathscr{E}$ is purely kinetic.

* In 1923, two years after Einstein received the Nobel prize for his work on the photoelectric effect, Millikan was awarded the same honor, in part for his experimental efforts on that subject.

† Notwithstanding the great influence the photoelectric effect had on the photon historically, it is nonetheless possible to explain that effect without resorting to a quantization of the electromagnetic field. Indeed one can treat the field classically, imparting the quantum nature to the matter alone. See the article by W. E. Lamb, Jr., and M. O. Scully in *Polarization, Matter and Radiation, Jubilee Volume in Honor of Alfred Kastler.*

The fact that the photon possesses inertial mass leads to some rather interesting results, for example, the gravitational *red shift* (Problem 13.13) and the deflection of starlight by the Sun (Problem 13.16). The red shift was actually observed under laboratory conditions in [illegible] by R. V. Pound and G. A. Rebka, Jr., at Harvard University. In brief, if a particle of mass m moves upward a height d in the Earth's gravitational field, it will do work in overcoming the field and thus decrease in energy by an amount mgd. Therefore, if the photon's initial energy is $h\nu_i$, its final energy after traveling a vertical distance d will be given by

$$h\nu_f = h\nu_i - mgd, \qquad (13.13)$$

and so $\nu_f < \nu_i$, ergo the name red shift. Pound and Rebka, using gamma-ray photons, were able to confirm that quanta of the electromagnetic field behave as if they had a mass $m = \mathscr{E}/c^2$.

From Eq. (13.10) the momentum of a photon can be written as

$$p = \frac{\mathscr{E}}{c} = \frac{h\nu}{c} \qquad (13.14)$$

or

$$p = h/\lambda. \qquad (13.15)$$

If we had a perfectly monochromatic beam of light of wavelength λ, each constituent photon would possess a momentum of h/λ, or equivalently

$$\mathbf{p} = \hbar\mathbf{k}. \qquad [3.53]$$

We can arrive at this same end by way of a somewhat different route. Momentum quite generally is the product of mass and speed, thus

$$p = mc = \frac{\mathscr{E}}{c},$$

and we're back to Eq. (13.14). The momentum relationship, $p = h/\lambda$, for photons was confirmed in 1923 by Arthur Holly Compton (1892–1962). In a classic experiment he irradiated electrons with x-ray quanta and studied the frequency of the scattered photons. By applying the laws of conservation of momentum and energy relativistically, as if the collisions were between particles, Compton was able to account for an otherwise inexplicable decrease in the frequency of the scattered radiant energy.

A few years later in France, Louis Victor, Prince de Broglie (b. 1891), in his doctoral thesis drew a marvelous analogy between photons and matter particles. He proposed that every particle, and not just the photon, should have an associated wave nature. Thus since $p = h/\lambda$, *the wavelength of a particle having a momentum mv would then be*

$$\lambda = h/mv. \qquad (13.16)$$

Because $h = 6.6 \times 10^{-34}$ is small and because of the relative enormity of the momenta of macroscopic entities, such bodies have miniscule wavelengths. For example, a 1-g pebble moving at 1 cm/s has a wavelength of 6.6×10^{-29} m, roughly 10^{22} times shorter than that of red light. In contrast, let's compute the voltage needed to impart a wavelength of 1 Å to an electron; this is of the order of the spacing between atoms. Starting from rest, the electron has a kinetic energy of $mv^2/2$ after traversing a potential difference of V, that is,

$$q_eV = \frac{mv^2}{2}.$$

Using Eq. (13.14), we can write

$$V = \frac{h^2}{2mq_e\lambda^2}$$

$$= \frac{(6.6 \times 10^{-34}\,\mathrm{J\,s})^2}{2(9.1 \times 10^{-31}\,\mathrm{kg})(1.6 \times 10^{-19}\,\mathrm{C})(10^{-10}\,\mathrm{m})^2}$$

or

$$V = 150\ \mathrm{V}.$$

An electron so accelerated has an energy of 150 eV ($1\ \mathrm{eV} = 1.602 \times 10^{-19}$ J) and a wavelength of 1 Å, which is just about that of a typical x-ray photon.

Experimental verification of de Broglie's hypothesis came in the years 1927–1928 as a result of the efforts of Clinton Joseph Davisson (1881–1958) and Lester Germer (b. 1896) in the United States and Sir George Paget Thomson (1892–1975) in Great Britain. Davisson and Germer used a nickel crystal (face-centered cubic structure) as a three-dimensional diffraction grating for electrons. When a 54-eV beam was incident, perpen-

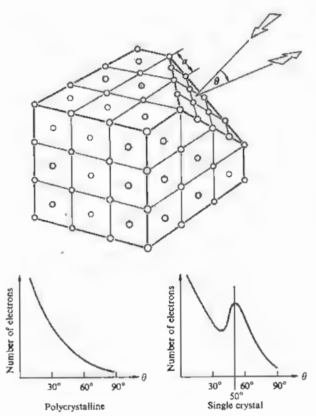


Figure 13.6 The Davisson–Germer experiment.

dicular to the cut face of the crystal, as shown in Fig. 13.6, a strong reflection appeared at 50° to the normal. Making use of the grating equation,

$$a \sin \theta_m = m\lambda, \qquad [10.32]$$

we find that the first-order ($m = 1$) maximum corresponds to

$$a \sin \theta_1 = \lambda.$$

In this instance the lattice spacing a is 2.15 Å, and so $\lambda = 2.15 \sin 50°$ or 1.65 Å, in fine agreement with the value of 1.67 Å computed from the de Broglie equation (13.16). Amazingly enough, a beam of electrons had thus been diffracted in a manner completely analogous to a lightwave bouncing off a reflection grating. The first observation of electron diffraction that was made by Davisson and Germer was quite accidental; they were not looking for it, nor did they at first realiz[e] happened. In contrast, Thomson had set out ately to verify diffraction. Taking a somewhat approach, he passed a beam of high-speed through a thin polycrystalline foil (100 nm th observed a diffraction pattern made up of co

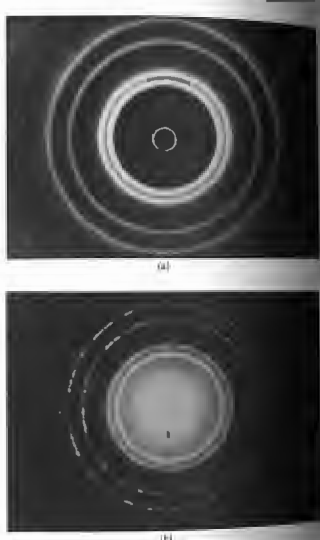
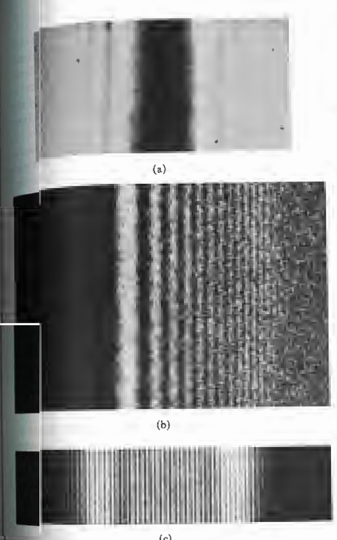


Figure 13.7 (a) Diffraction pattern arising from through a thin polycrystalline aluminum foil. (b) D arising from electrons passing through the same al the PSSC film *Matter Waves*.)



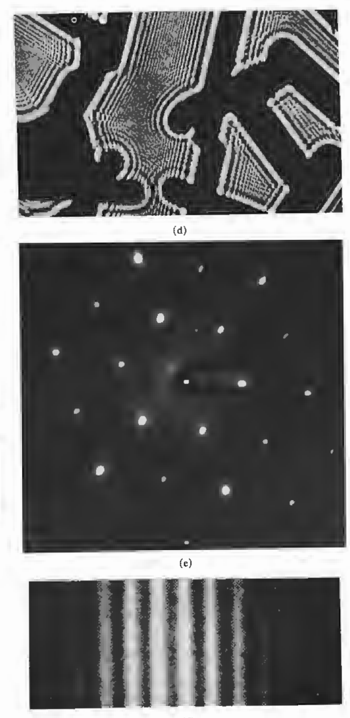


Figure 13.8 Matter-wave diffraction. (a) Fresnel electron diffraction of a 2-μm diameter metallized quartz filament. [Photo from Klemperer, *Electron Physics*, Butterworths and Co. (Publishers) London (1972).] (b) Fresnel electron diffraction at a half plane crystal). (c) Interference fringes observed with an electron arrangement by G. Möllenstedt. (d) Fresnel diffraction of by zinc oxide crystals (After H. Boersch). (The last three are from *Handbuch der Physik*, edited by S. Flügge, Springer-Heidelberg.) (e) Electron diffraction by a UO_2 crystal. (Photo of University of California's Los Alamos Scientific Labora-) Double-beam interference of electrons. [Photo by C. Jönsson, from J. Orear, *Fundamental Physics*, John Wiley, New York The faint cross hatching in this photo arises purely in the printing process; it's a moiré effect from rescreening.

(a)

(b)

Figure 13.9 Diffraction patterns generated by (a) neutrons, (b) x-ray photons incident on a single crystal of NaCl. A polycrystalline specimen would produce a great many randomly oriented dot patterns of this sort which would blend into the ring systems of Fig. 13.7. [Photo (a) by E. O. Wollan, which along with (b) is from Lapp and Andrews, *Nuclear Radiation Physics* 3rd ed., Prentice-Hall, Inc., Englewood Cliffs, N.J. (1963).]

rings (Fig. 13.7). In 1928 E. Rupp diffracted [illegible] slow electrons (70 eV) at grazing incidence o[illegible] optical grating (1300 lines per cm) and observed [illegible] second-, and third-order images. Two years [illegible] 1930, I. Estermann and Otto Stern demonst[illegible] in [illegible] occurrence of diffraction effects using beams [illegible] helium atoms and molecular hydrogen.

In recent times it has become possible t[illegible] remarkable range of interference and diff[illegible] terns using electrons, as witness the photog[illegible] 13.8.

Out of the long list of material particles that hav[illegible] been observed to display wave properties, neu[illegible] amongst the most useful. Because they carry n[illegible] slow or *thermal neutrons* can have long waveleng[illegible] yet be immune to the electrical forces that strongly disturb low-momentum electrons. The diffractio[illegible] of thermal neutrons (generally originating from nuclear reactors) is now a routinely used procedure in [illegible] of atomic structure (Fig. 13.9).

Not very long ago (1969), a beam of neutral po[illegible] atoms was used to observe diffraction arising from a macroscopic slit (23×10^{-6} m wide). The resulti[illegible] tern was in accord with de Broglie's hypothesis [illegible] scalar Fresnel diffraction theory.*

We are limited by our language to a list of words [illegible] much as our worldly experiences limit th[illegible] those words bring to mind. Our senses ha[illegible] read th[illegible] environment and in so doing provided the [illegible]s for ou[illegible] understanding of it. In what seemed a logical [illegible] we have tried, a bit naively, to use macroscopic [illegible] to describe submicroscopic entities. But elec[illegible] not behave like miniscule billiard balls any more than light can be pictured in terms of scaled-dow[illegible] ocean waves. *Particles and waves are macroscopic [illegible] which gradually lose their relevance as we approach [illegible] microscopic domain.*

13.5 PROBABILITY AND WAVE OPTICS

The fundamental wave nature of optical [illegible] was established well over a hundred years ag[illegible] [illegible] the work of Young, Fresnel, and many others [illegible] studied the processes of interference, diffraction, [illegible] polarization. During the intervening century, our [illegible]ception of light has metamorphosed from that of a [illegible]mentary mechanical aether wave to the contemporary photon description. Yet the concept that light is somehow inherently oscillatory has persisted throughout this transition period. And so we might again press the point and ask, *what is it that oscillates when we envisage light as a stream of photons*; or for that matter, what aspect of an electron vibrates? The answer [illegible] this will obviously give us some clue as to how quanta [illegible]play interference effects.

[illegible] Danish physicist Niels Henrik David Bohr (1885–[illegible]) provided an essential link between classical and [illegible]tum physics in what has become known as the [illegible]spondence *principle*. Briefly stated, *any new theory must [illegible] with the results of the classical theory it supersedes in [illegible] domain where the latter is known to be effective.** Thus [illegible] quantum theory can explain blackbody radiation, [illegible] photoelectric effect, Compton scattering, electron [illegible]action, and a myriad of other observations, it must [illegible]ccount for what might be called classical behavior. [illegible]ntire range of familiar effects, such as Snell's law, [illegible]flection law, and the Doppler formula,† which are [illegible] treated in terms of electromagnetic theory, must [illegible] understandable within the context of the photon [illegible]cription. The quantum theory is not just an esoteric [illegible]endum; it must encompass all confirmed observa[illegible] that have gone before it, no matter how mundane. [illegible]gine, if you will, a monochromatic light source [illegible]nating an optical element of some kind followed [illegible] observation screen. Presumably, in many cases [illegible]uld calculate, using classical wave optics, the flux-[illegible]sity distribution appearing on the screen. Suppose [illegible] that we have such a case, for example, a plane [illegible] incident on a double-slit arrangement. The irradi[illegible] $I(\theta)$ represents the average energy density per unit [illegible] at the plane of observation, in this instance, the familiar fringe pattern of Young's experiment. Thus the average number of photons impinging on a small area element dA, in a time interval dt, will be $(I\,dA\,dt)/h\nu$, where I, of course, varies from one point to the next over the surface of the screen. Keep in mind that we can only detect the emission or absorption of a photon, that is, its interaction with matter. There is no way to predict where a particular photon will arrive on the plane of observation, although some regions are more likely sites than others. Accordingly, if a total of N photons strike the screen in each interval dt, we can say that each photon has a probability equal to $(I\,dA\,dt)/h\nu N$ of arriving at the given area element dA. *The irradiance, as computed classically, is therefore related to the probability of finding a photon somewhere on the screen.* It is convenient at this point to introduce, at least conceptually, a complex quantity known as the **probability amplitude**, that is, a quantity whose absolute value squared (the so-called *wave-intensity*) yields the probability distribution. It is this probability amplitude propagating as a wave that describes the whole range of interference effects. For example, in Young's experiment the photon's probability amplitude for reaching its final state is the sum of two amplitudes, each of these being associated with the photon's passage through one of the slits. The various contributing amplitudes in a given situation overlap and thereby effectively interfere, yielding the resultant probability amplitude and from that the irradiance. In answer to our initial question, we can say that it is the probability amplitude associated with the photon that is oscillating. Bear in mind that the same kind of discomforting reinterpretation of familiar ideas that we are encountering now had to be made when Maxwell's electromagnetic theory first emerged on the scene.

Let's now briefly examine the implications of a rather famous statement made by the renowned British physicist and Nobel laureate Paul Adrien Maurice Dirac (1902–1984):

> ... each photon interferes only with itself. Interference between different photons never occurs.*

This is in accord with the conclusion that each photon possesses a distinct wave nature. Evidently the wave

* J. Leavitt and F. Bills, "Single-Slit Diffraction Pattern [illegible] Atomic Potassium Beam," *Am. J. Phys.* 37, 905 (1969).

* [illegible] process. [illegible] classical [illegible] is the corre[illegible] of quantum [illegible] h is [illegible] to approach [illegible] phenomena continuous.

† See [illegible] *Optics* p. 82.

* P. A. M. Dirac, *Quantum Mechanics*, 4th ed., p. 9.

properties of light are not attributable to the beam **acting as** a **whole. In Young's experiment** each **photon somehow simultaneously interacts with** both slits; **close** either one and the fringes will disappear. Presumably, **since each photon interferes with itself, the same fringe pattern would gradually occur, one flash at a time, even if we shone a single photon a day at the slits. This remarkable conclusion was actually confirmed experimentally by Geoffrey I. Taylor, a student at the University of Cambridge in 1909. Using a light-proof box, a gas flame illuminating an entrance slit, and a number of attenuating smoked glass screens, he set about photographing the diffraction pattern in the shadow of a needle. By drastically reducing the incoming flux density, he was able to obtain exposure times of up to about 3 months. In such cases the energy density in the** box was so low that there was usually only one photon at a time in the region beyond the entrance slit. Nonetheless, the customary array of diffraction fringes appeared, and moreover,

> In no case was there any diminution in the sharpness of the pattern. . .*

Much of the foregoing discussion can be applied to material particles as well. In fact, the same dynamical equations determine the interrelationship of ν, λ, and v with p and $\mathscr{E}$ for all particles, material or otherwise. Consequently from Eq. (13.11) we find that

$$p = (\mathscr{E}^2 - m_0^2c^4)^{1/2}/c, \tag{13.17}$$

while $\lambda = h/p$ leads to

$$\lambda = hc/(\mathscr{E}^2 - m_0^2c^4)^{1/2}. \tag{13.18}$$

Since $p = mv$, $v = pc^2/(mc^2) = pc^2/\mathscr{E}$ and

$$v = c[1 - (m_0^2c^4/\mathscr{E}^2)]^{1/2}. \tag{13.19}$$

Evidently one of **the main distinguishing characteristics of the photon is just its zero rest mass. In that case,** the **above equations** simply **become $p = \mathscr{E}/c$, $\lambda = hc/\mathscr{E} = c/\nu$** and $v = c$.

In **a way analogous** to that of the photon, the probability **amplitude** or de Broglie wave for a *matter field* is represented by the function $\psi(x, y, z, t)$ (also refe[illegible] to as the *wave function*). The **probability** of findi[illegible] particle of finite rest mass is **then proportional** [illegible] wave-intensity $|\psi|^2$. One determines the wave func[illegible] for a particular circumstance involving material [illegible] cles from the *Schrödinger equation*. Once again [illegible] probability amplitude of the particle that is [illegible] propagates through space as a wave, and [illegible] takes i[illegible] interference.

* G. I. Taylor, "Interference Fringes with Feeble Light," *Proc. Camb. Phil. Soc.* **15**, 114 (1909).

13.6 FERMAT, FEYNMAN, AND PHOTONS

In classically treating interference and **diffrac**[illegible] lems with coherent waves, one generally **sum**[illegible] electric field contributions at a given **point**—[illegible] frequently being written in complex form. [illegible] of the absolute value of this sum is **proportio**[illegible] irradiance and is consequently proportional to [illegible] ability of finding a photon at the point in **que**[illegible] will now qualitatively generalize these **rem**[illegible] the lines of Richard Feynman's elegant **varia**[illegible] mulation of quantum mechanics.* Suppose [illegible] particle (photon, electron, etc.) is emitted **fro**[illegible] point S and is later detected at point A. The [illegible] of arrival, P, is equal to the square of the **abso**[illegible] of a complex quantity Φ, which, as before, is [illegible] the probability amplitude, that is, $P = |\Phi|^2$. [illegible] classical treatment, where the field was expresse[illegible] in complex form as a convenience, Φ must be comple[illegible] the quantum-mechanical formulation. **Conse**[illegible] has an amplitude and a phase, the latter being [illegible] of both the spatial position of A and time, [illegible] can occur by several alternative routes 1, 2, [illegible] it was postulated by Feynman that in such cases [illegible] *path contributes to the total probability amplitude.* In other words,

$$\Phi = \Phi_1 + \Phi_2 + \Phi_3 + \cdots \tag{13.20}$$

and so

$$P = |\Phi_1 + \Phi_2 + \Phi_3 + \cdots|^2. \tag{13.21}$$

* R. P. Feynman "Space–Time Approach to Non-Rela[illegible] tum Mechanics," *Rev. Mod. Phys.* 20, 367 (1948).

It was further postulated that *the magnitudes of these individual probability amplitudes are all equal*, that is,

$$|\Phi_1| = |\Phi_2| = |\Phi_3| = \cdots, \tag{13.22}$$

whereas **their phases are not equal and indeed depend** on the **particular paths. Note that a value of $P = 1$ means** that the **particle will arrive at A with complete certainty,** while **$P = 0$ means that it will most definitely not reach** A. Quite **generally then, P will range in value between** 0 and 1. **Equation (13.21) evidently introduces the** phenom**enon of interference into the scheme, whether** [illegible] for **photons or electrons. In contrast, if we were** [illegible]ing **with classical particles, such as a stream of BB** [illegible]lets, **P would equal $|\Phi_1|^2 + |\Phi_2|^2 + |\Phi_3|^2 + \cdots$, and** [illegible] **would be no interference; in other words, P would** [illegible] **independent of the individual phases. As with inco**[illegible]**rent light, one then adds irradiances rather than** amp**litudes.**

Let's now turn to the idealized Young's experiment of Fig. 13.10, consisting of two extremely small slits. In [illegible] case

$$P = |\Phi_1 + \Phi_2|^2, \tag{13.23}$$

[illegible] there are effectively two paths, one through each [illegible]ture. If the phases of the probability amplitudes at [illegible] differ by an odd multiple of π, they will interfere [illegible]ructively, that is,

$$P = (|\Phi_1| - |\Phi_2|)^2 = 0. \tag{13.24}$$

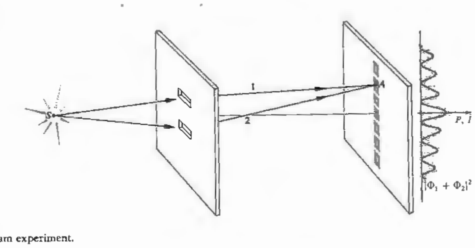


Figure 13.10 Double-beam experiment.

On the other hand, if they are in phase, constructive interference results at A, whereupon

$$P = (|\Phi_1| + |\Phi_2|)^2 = 4|\Phi_1|^2, \tag{13.25}$$

which is equivalent to

$$I = 4I_0 \cos^2 \frac{\delta}{2} \tag{9.6}$$

for $\delta = 0, \pi, 2\pi, \ldots$. The **phases** of the **probability** amplitudes at A depend on **the path** length**s traversed** along each route, so P can **clearly** have **any value** between these extremes as well. In the same way, if we were shooting BB pellets through two small holes, the **probability of their** arriving **at** A would **be the** sum $|\Phi_1|^2 + |\Phi_2|^2$. **Here** $|\Phi_1|^2$ **and** $|\Phi_2|^2$ are **simply** the **individual probabilities** of **arrival** with either **hole** 1 or hole 2 open, respectively, as indicated in Figs. 13.11 and 13.12. The resulting distribution of BB pellets is just the superposition of the two separate patterns for each aperture; there are **no fringes and no interference.**

If the screen had N **such apertures, rather than just** two, the probability of a **photon reaching A would be**

$$P = \left|\sum_{i=1}^{N} \Phi_i\right|^2. \tag{13.26}$$

For a large aperture, for example, a lens or mirror, the **summation becomes an integral over the area of** the **aperture. Incidentally, Feynman has shown that,** for **material particles, the total value of the probability**

Figure 13.11 Lower hole covered in double-beam setup.

amplitude for all paths is the wave function satisfying Schrödinger's equation.*

We now go back to the picture of a single ray of light leaving a source and reflecting off a mirror, ultimately to arrive at a sensor. The probability of a photon encountering the sensor is determined by Φ, which in turn is composed of contributions from each of the possible paths. All of this talk about paths should bring to mind Fermat's principle (Section 4.2.4), which maintains that the actual path taken by a ray is stationary. Everything fits together rather nicely when we realize that the relative differences in path length and phase of the corresponding probability amplitudes at the sensor are small only for paths near the stationary one ($\theta_i = \theta_r$). These probability amplitudes interfere constructively, thereby providing the predominant contribution to P. This is then the quantum-mechanical basis for Fermat's principle. Probability amplitudes associated with paths remote from the stationary one will have large phase-angle differences resulting in relatively little cumulative effect on P. This discussion is reminiscent of the Cornu spiral (Section 10.3.7), which in quite an analogous fashion can be thought of as the diagrammatic sum of a great number of phasors, each of different amplitude but the same phase angle. Suppose that we wish to determine I or equivalently P at a point on the central axis of, say, a long slit. In that case contributions from remote areas of the aperture correspond to the tightly wound regions of the spiral and therefore contribute little to the complex number (phasor) $\mathbf{B}_{12}$. Recall [Eqs. (10.106) or (10.108)] that I is proportional to $|\mathbf{B}_{12}|^2$ just as it is proportional to $|\Phi|^2$. Equation (13.20) can similarly be envisioned pictorially in terms of the addition of a number of equal-amplitude phasors, in which case P is proportional to the square of the magnitude of the resultant. Phasors corresponding to probability amplitudes for paths in the vicinity of a stationary one differ in phase by very little and therefore add almost along a straight line, thus making a major contribution. Where the relative phase of successive phasors is large, the curve spirals around, having little effect on $|\Phi|$. The analogy can even be extended if we now visualize the Cornu spiral as if it were composed of a great number of equal-amplitude phasors whose phase angles are ever increasing as they get farther from the center of the spiral [from Eq. (10.[illegible]), $\beta = \pi w^2/2$]. In any event the phasor representation of the contributing probability amplitudes is a handy device to keep in mind.

* To see how these ideas are related to Hamilton's principle function, the principle of least action, and the WKB approximation, refer, for example, to D. B. Beard and G. B. Beard, *Quantum Mechanics with Applications*, p. 44, and S. Borowitz, *Fundamentals of Quantum Mechanics*, p. 165.

13.7 ABSORPTION, EMISSION, AND SCATTERING

Let's now take a brief look at the quantum-mechanical aspects of a few important interactions occurring between light and matter. Suppose that a photon of frequency ν_i collides with and is absorbed by an atom. Energy is transmitted to a bound electron, resulting in the excitation of the atom. The absorption probability is greatest when the frequency of the incident photon is equal to an excitation energy of the atom (see Section [illegible]). In dense gases, liquids, and solids, absorption occurs over a range or band of frequencies, and the energy is generally dissipated by way of intermolecular collisions. In contrast, the excited atoms of a low-pressure gas can reradiate a photon of the same frequency (ν_i) in a random direction, a process first observed by R. W. Wood in 1904 and known as **resonance radiation**. Accordingly, there is preponderant scattering at frequencies coincident with the excitation energies of the atoms. The effect is easily demonstrated using Wood's technique, which incorporates an evacuated glass bulb containing a bit of pure metallic sodium. Gradually heating the bulb increases the sodium vapor pressure within it. If a region of the vapor is then illuminated with a strong beam of light from a sodium arc, that portion will glow with the characteristic yellow resonance radiation of Na.

Figure 13.12 Upper hole covered in double-beam setup.

Scattering can also occur at frequencies other than those corresponding to the atom's stable energy levels. In such cases a photon will be reradiated without any appreciable time delay and most often with the same energy as that of the absorbed quantum. The process is known as **elastic** or **coherent scattering**, because there is a phase relationship between the incident and scattered fields. This is the *Rayleigh scattering* we talked about in Section 8.5.1.

It is also possible that an excited atom will not return to its initial state after the emission of a photon. This kind of behavior had been observed and studied extensively by George Stokes prior to the advent of quantum theory. Since the atom drops down to an interim state, it emits a photon of lower energy than the incident primary photon, in what is usually referred to as a *Stokes transition*. If the process takes place rapidly (roughly 10^{-7} s), it is called **fluorescence**, whereas if there is an appreciable delay (in some cases seconds, minutes, or even many hours), it is known as **phosphorescence**. Using ultraviolet quanta to generate a fluorescent emission of visible light has become an accepted occurrence in our everyday lives. Any number of common materials (e.g., detergents, organic dyes, and tooth enamel), will emit characteristic visible photons so that they appear to glow under ultraviolet illumination, ergo the widespread use of the phenomenon for commercial display purposes and for "whitening" cloths.

13.7.1 The Spontaneous Raman Effect

If quasimonochromatic light is scattered from a substance, it will thereafter consist mainly of light of the same frequency. Yet it is possible to observe very weak additional components having higher and lower frequencies (side bands). Moreover, the difference between the side bands and the incident frequency ν_i is found to be characteristic of the material and therefore suggests an application to spectroscopy. The *spontaneous Raman effect*, as it is now called, was predicted in 1923 by Adolf Smekal and observed experimentally in 1928 by Sir Chandrasekhara Vankata Raman (1888–1970), then professor of physics at the University of Calcutta. The effect was difficult to put to actual use, because one needed strong sources (usually Hg discharges were used) and large samples. Often the ultraviolet from the source would further complicate matters by decomposing the specimen. And so it is not surprising that little sustained interest was aroused by the promising practical aspects of the Raman effect. The situation was changed dramatically when the laser

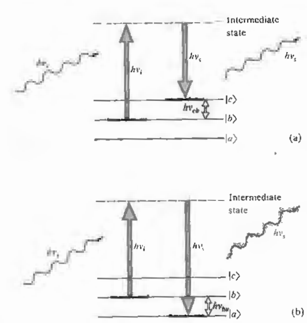


Figure 13.13 Spontaneous Raman scattering.

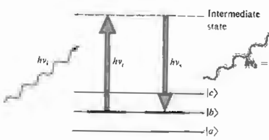


Figure 13.14 Rayleigh scattering.

became a reality. *Raman spectroscopy* is now a unique and powerful analytical tool.

To appreciate how the phenomenon operates, let's review the germane features of molecular spectra. A molecule can absorb radiant energy in the far-infrared and microwave regions, converting it to rotational kinetic energy. Furthermore, it can absorb infrared photons (i.e., ones within a wavelength range from roughly 10 mm^{-2} down to about 700 nm), transforming that energy into vibrational motion of the molecule. Finally a molecule can absorb energy in the visible and ultraviolet regions through the mechanism of [illegible] transitions, much like those of an atom. Suppose that we have a molecule in some vibrational state, which, using quantum-mechanical notation, we call $|b\rangle$, as indicated diagrammatically in Fig. 13.13(a). This need not necessarily be an excited state. An incident photon of energy $h\nu_i$ is absorbed, raising the system to some intermediate or virtual state, whereupon it immediately makes a Stokes transition, emitting a (scattered) photon of energy $h\nu_s < h\nu_i$. In conserving energy, the difference $h\nu_i - h\nu_s = h\nu_{cb}$ goes into exciting the molecule to a higher vibrational energy level $|c\rangle$. It is possible that electronic or rotational excitation [illegible] as well. Alternatively, if the initial state is an [illegible] one (just heat the sample), the molecule, after [illegible] and emitting a photon, may drop back to an even lower state [Fig. 13.13(b)], thereby making an *anti-Stokes* transition. In this instance $h\nu_s > h\nu_i$, which means [illegible] some vibrational energy of the molecule ($h\nu_{bd} =$ [illegible]) has been converted into radiant energy. In either case the resulting differences between ν_s and ν_i correspond to specific energy-level differences for the substance under study and as such yield insights into its molecular structure. Figure 13.14, for comparison's sake, depicts Rayleigh scattering where $\nu_s = \nu_i$.

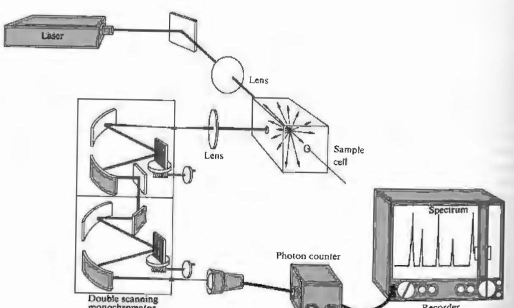


Figure 13.15 A laser–Raman system.

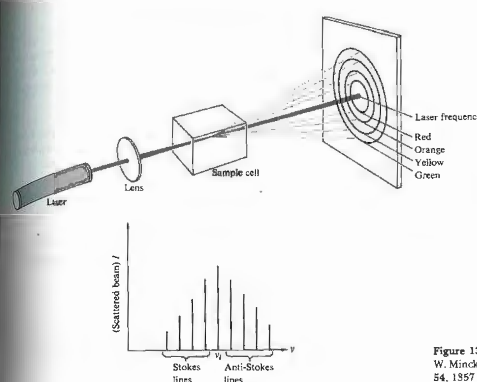


Figure 13.16 Stimulated Raman scattering. [See R. W. Minck, R. W. Terhune, and C. C. Wang, *Proc. IEEE* 54, 1357 (1966).]

The laser is an ideal source for spontaneous Raman scattering. It is bright, quasimonochromatic, and available in a wide range of frequencies. Figure 13.15 illustrates a typical laser-Raman system. Complete research instruments of this sort are commercially available, including the laser (usually helium–neon, argon, or krypton), focusing lens systems, and photon-counting electronics. The double scanning monochromator provides the needed discrimination between ν_i and ν_s, since unshifted laser light (ν_i) is scattered along with the Raman spectra (ν_s). Although Raman scattering associated with molecular rotation was observed prior to the use of the laser, the increased sensitivity now available makes the process easier and allows even the effects of electron motion to be examined.

13.7.2 The Stimulated Raman Effect

In 1962 Eric J. Woodbury and Won K. Ng rather fortuitously discovered a remarkable related effect known as *stimulated Raman scattering*. They had been working with a million-watt pulsed ruby laser incorporating a nitrobenzene Kerr cell shutter (see Section 8.11.3). They found that about 10% of the incident energy at 694.3 nm was shifted in wavelength and appeared as a *coherent* scattered beam at 766.0 nm. It was subsequently determined that the corresponding frequency shift of about 40 THz was characteristic of one of the vibrational modes of the nitrobenzene

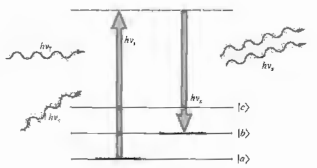


Figure 13.17 Energy-level diagram of stimulated Raman scattering.

molecule, as were other new frequencies also present in the scattered beam. Stimulated Raman scattering can occur in solids, liquids, or dense gases under the influence of focused high-energy laser pulses (Fig. 13.16). The effect is schematically depicted in Fig. 13.17. Here two photon beams are simultaneously incident on a molecule, one corresponding to the laser frequency ν_i, the other having the scattered frequency ν_s. In the original setup the scattered beam was reflected back and forth through the specimen, but the effect can occur without a resonator. The laser beam loses a photon $h\nu_i$, while the scattered beam gains a photon $h\nu_s$ and is subsequently *amplified*. The remaining energy ($h\nu_i - h\nu_s = h\nu_{ba}$) is transmitted to the sample. The chain reaction in which a large portion of the incident beam is converted into stimulated Raman light can only occur above a certain high-threshold flux density of the exciting laser beam.

Stimulated Raman scattering provides a whole new range of high–flux-density coherent sources extending from the infrared to the ultraviolet. It should be mentioned that in principle each spontaneous scattering mechanism (e.g., Rayleigh and Brillouin scattering) has its stimulated counterpart.*

* For further reading on these subjects you might try the review-tutorial paper by Nicolaas Bloembergen, "The Stimulated Raman Effect," *Am. J. Phys.* **35**, 989 (1967). It contains a fairly good bibliography as well as a historical appendix. Many of the papers in *Lasers and Light* also deal with this material and are highly recommended reading.

PROBLEMS

13.1 Suppose that we measure the emitted [illegible] from a small hole in a furnace to be 22.8 W/[illegible] an optical pyrometer of some sort. Compute [illegible] temperature of the furnace.

13.2* When the Sun's spectrum is photog[illegible] using rockets to range above the Earth's atmos[illegible] it is found to have a peak in its spectral exitan[illegible] at roughly 465 nm. Compute the Sun's surface [illegible]perature, assuming it to be a blackbody. This app[illegible]mation yields a value that is about 400 K too high[illegible]

13.3 Beginning with Eq. (13.4), show that the [illegible] per unit frequency interval for a blackbody is give[illegible] by

$$I_{e\nu} = \frac{2\pi h\nu^3}{c^2}\left[\frac{1}{e^{h\nu/kT} - 1}\right]. \qquad (13.2[illegible])$$

13.4 Compute the wavelength of a 0.15-kg b[illegible] moving at 25 m/s. Compare this with the wavelen[illegible] a hydrogen atom ($m_0 = 1.673 \times 10^{-27}$ kg) hav[illegible] speed of 10^3 m/s.

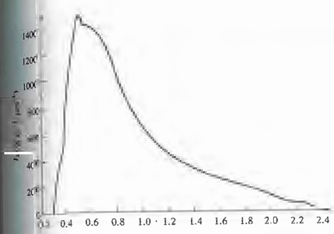
13.5* Determine the energy of a 500-nm ([illegible] photon in both joules and electron volts. Make the [illegible] calculation for a 1-MHz radio wave.

13.6 Write an expression for the waveleng[illegible] of a photon in angstroms (1 Å $= 10^{-10}$ m) in term[illegible] of its energy in eV.

13.7 Figure 13.18 shows the *spectral irradian*[illegible] ing on a horizontal surface, for a clear day, a[illegible] with the Sun at the zenith. What is the most ener[illegible] photon we can expect to encounter (in eV and an[illegible]

13.8* Suppose we have a 100-W yellow [illegible]t bulb (550 nm) 100 m away from a 3-cm–diameter [illegible]uttered aperture. Assuming the bulb to have a 2.5% [illegible] to radiant power, how many photons will pa[illegible] the aperture if the shutter is opened for [illegible]

13.9 The *solar constant* is the radiant flux densi[illegible] spherical surface centered on the Sun having [illegible] radiu[illegible]



Figur[illegible]

equal [illegible] that of the Earth's mean orbital radius; it has [illegible] of 0.133–0.14 W/cm^2. If we assume an average [illegible]length of about 700 nm, how many photons at most [illegible] arrive on each square meter per second of a solar cell [illegible] just above the atmosphere?

13.1[illegible] With respect to the photoelectric effect, imagine [illegible] we have an incident beam with an irradiance of [illegible] W/m^2 at a wavelength of 500 nm. What is the [illegible]rgy per quantum? Supposing the target atoms to [illegible] radii of 10^{-10} m, how long would it take for any [illegible] them to accumulate the energy of a single photon, [illegible] the classical wave picture? In 1916 Rayleigh [illegible] classically that an atomic oscillator absorbs [illegible]nt energy with an effective area of the order of λ^2 [illegible]onance. How does this help?

[illegible] The work function for outgassed polycrystalline [illegible] is 2.28 eV. What is the minimum frequency a [illegible] must have in order to liberate an electron? What [illegible] the maximum kinetic energy of an electron [illegible] a 400-nm photon?

[illegible]* Suppose that we have a beam of light of a given [illegible]density incident on a photoelectric tube. Draw a [illegible] of i_p versus V showing what we might expect to [illegible]pen to the stopping potential as the frequency is [illegible]ased from ν_1 to ν_2 to ν_3.

13.13 To examine the *gravitational red shift* consider a photon of frequency ν, which is emitted from a star having a mass M and a radius R. Show that at the star's surface the energy of the photon is given by

$$\mathscr{E} = h\nu\left(1 - \frac{GM}{c^2R}\right).$$

When it arrives at the Earth, having essentially escaped the gravitational pull of the star, the photon will have a lower frequency. Show that the frequency shift is then

$$\Delta\nu = \frac{GM}{c^2R}\,\nu.$$

The effect is quite noticeable for the class of stars known as *white dwarfs*. (This problem should have been analyzed using general relativity, but the answer would have been the same.)

13.14 Compute the fractional gravitational red shift, that is, $\Delta\nu/\nu$, for the Sun ($M = 1.991 \times 10^{30}$ kg and $R = 6.960 \times 10^8$ m). How much of a change would occur in the frequency and wavelength of a photon of $\lambda_0 = 650$ nm emitted from the Sun? (See previous problem.)

13.15 Show that a photon moving upward a distance d in the Earth's gravitational field (Section 13.4) will undergo a frequency decrease equal to

$$\Delta\nu = -gd\nu/c^2.$$

Compute the value of $\Delta\nu/\nu$ if $d = 20$ m. Pound and Rebka actually measured that shift in a vertical tower at Harvard University, using the extreme sensitivity of the Mössbauer effect.

13.16 This problem concerns itself with the bending of a beam of light as it passes a massive body, such as the Sun. It should actually be solved using general rather than special relativity because of the presence of gravity. As a result, our simple approach yields half the correct answer. Be that as it may, let us plunge on. Show that the force component acting on the photon transverse to its initial direction of motion (Fig. 13.19) is given by

$$F = \frac{GMm}{R^2}\cos^3\theta.$$

Since $c\,dt = ds = d(R \tan \theta)$, show that the total transverse component of momentum received by the photon is

$$p_{\perp} = \frac{2GMm}{cR}.$$

Inasmuch as $p_{\parallel} = mc$, compute ϕ for the Sun ($R = 6.960 \times 10^8$ m and $M = 1.991 \times 10^{30}$ kg).

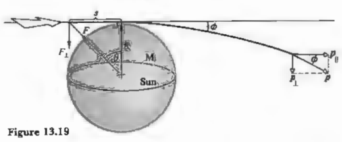


Figure 13.19

13.17* Imagine that we accelerate a beam of electrons through a potential difference of 100 V and then cause it to pass through a slit 0.1 mm wide. Determine the angular width of the central diffraction maximum ($m_0 = 9.108 \times 10^{-31}$ kg). How do things change if we decrease the beam's energy?

13.18 A thermal neutron is one that is in thermal equilibrium with matter at a given temperature. Compute the wavelength of such a neutron at 25°C (≈room temperature). Recall from kinetic theory that the average kinetic energy would be equal to $\frac{3}{2}kT$. (Boltzmann's constant $k = 1.380 \times 10^{-23}$ J/K and $m_0 = 1.675 \times 10^{-27}$ kg.)

13.19 In Young's experiment can we imagine that an incident photon splits and passes through both slits? Discuss your conclusion.

13.20* Suppose we have a laserbeam of radius [illegible] and wavelength λ. Using the uncertainty principle [illegible] Δp_x [illegible] h), make an approximate calculation of the radius q of the smallest spot the beam will make on a screen [illegible] distance R away.

13.21 What is the *photon flux* Π of a 1000-W continuous CO$_2$ laser emitting at 10,600 nm in the IR?

13.22 Derive the dispersion relation, that is, ω = [illegible] for the de Broglie wave of a particle of mass m_0 [illegible] tivistically in a region where it has constant potential energy U.

13.23* Derive an expression for the dispersion [illegible] tion of a free ($U = 0$), relativistically moving particle [illegible] rest mass m_0.

13.24 Assuming that the de Broglie wave for a [illegible] in a region where its potential energy is constant is [illegible] by

$$\psi(x, t) = C_1 e^{-i(\omega t + kx)} + C_2 e^{[illegible]},$$

use the results of Problem (13.22) to show that

$$i\hbar \frac{\partial \psi}{\partial t} = -\frac{\hbar^2}{2m} \frac{\partial^2 \psi}{\partial x^2} + U\psi.$$

This is a form of the famous Schrödinger equation of quantum mechanics.

14 SUNDRY TOPICS FROM CONTEMPORARY OPTICS

14.1 IMAGERY — THE SPATIAL DISTRIBUTION OF OPTICAL INFORMATION

The manipulation of all sorts of data via optical techniques has already become a technological *fait accompli.* [illegible] literature since the 1960s reflects, in a diversity of [illegible], this far-reaching interest in the methodology of optical data processing. Practical applications have been made in the fields of television and photographic image enhancement, radar and sonar signal processing (phased and synthetic array antenna analysis), as well as in pattern recognition (e.g., aerial photointerpretation and fingerprint studies), to list only a very few.

Our concern here is to develop the nomenclature and [illegible] of the ideas necessary for an appreciation of this contemporary thrust in optics.

14.1.1 Spatial Frequencies

[illegible] processes one is most frequently concerned [illegible] signal variations in time, that is, the moment-by-moment alteration in voltage that might appear across [illegible] of terminals at some fixed location in space. By comparison, in optics we are most often concerned with [illegible] spread across a region of space at a fixed [illegible] in time. For example, we can think of the scene [illegible] in Fig. 14.1(a) as a two-dimensional flux-density distribution. It might be an illuminated transparency, a television picture, or an image projected on a screen; in any event there is presumably some function $I(y, z)$, which assigns a value of I to each point in the picture. To simplify matters a bit, suppose we scan across the screen on a horizontal line ($z = 0$) and plot point-by-point variations in irradiance with distance, as in Fig. 14.1(b). The function $I(y, 0)$ can be synthesized out of harmonic functions, using the techniques of Fourier analysis treated in Chapters 7 and 11. In this instance, the function is rather complicated, and it would take many terms to represent it adequately. Yet if the functional form of $I(y, 0)$ is known, the procedure is straightforward enough. Scanning across another line, for example, $z = a$, we get $I(y, a)$, which is drawn in Fig. 14.1(c) and which just happens to turn out to be a series of equally spaced square pulses. This function is one that was considered at length in Section 7.7, and a few of its constituent Fourier components are roughly sketched in Fig. 14.1(d). If the peaks in (c) are separated, center to center, by say, 1-cm intervals, the spatial period equals 1 cm per cycle, and its reciprocal, which is the spatial frequency, equals 1 cycle per cm.

Quite generally we can transform the information associated with any scan line into a series of sinusoidal functions of appropriate amplitude and spatial frequency. In the case of either of the simple sine- or square-wave targets of Fig. 14.2, each such horizontal scan line is identical, and the patterns are effectively one-dimensional. The spatial frequency spectrum of Fourier components needed to synthesize the square wave is shown in Fig. 7.15. On the other hand, $I(y, z)$ for the wine bottle candelabra scene is two-dimensional,

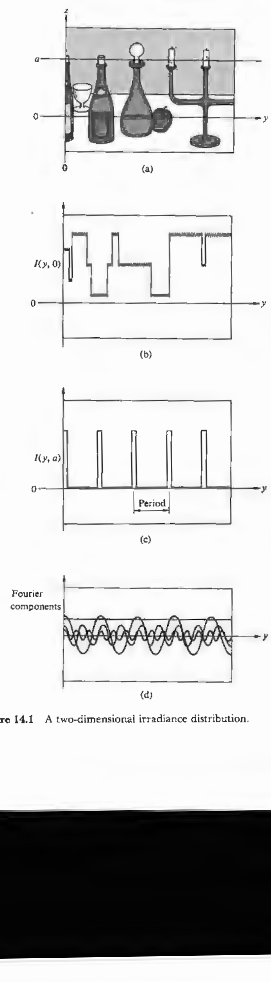


Figure 14.1 A two-dimensional irradiance distribution.

and we have to think in terms of two-dimensional Fourier transforms (Section 11.2.2). We might mention as well that, at least in principle, we could have recorded the amplitude of the electric field at each point of the scene and then performed a similar decomposition of that signal into its Fourier components.

Recall (Section 11.3.3) that the far-field or Fraunhofer diffraction pattern is, in fact, identical to the Fourier transform of the aperture function $\mathscr{A}(y, z)$. The aperture function is proportional to $\mathcal{E}_A(y, z)$, the source strength per unit area (10.37) over the input or object plane. In other words, if the field distribution on the object plane is given by $\mathscr{A}(y, z)$, its two-dimensional Fourier transform will appear as the field distribution $E(Y, Z)$ on a very distant screen. As in Fig. 10.10 we

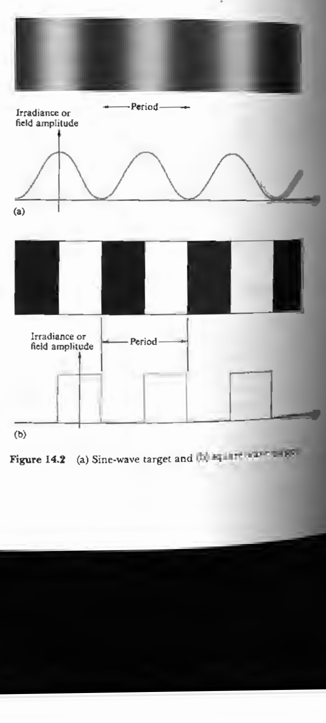


Figure 14.2 (a) Sine-wave target and (b) square-wave target.

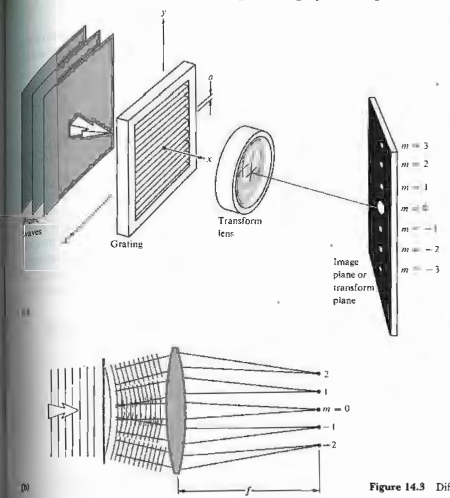


Figure 14.3 Diffraction pattern of a grating. (Source unknown.)

can introduce a lens (L_t) after the object in order to shorten the distance to the image plane. That objective lens is commonly referred to as the *transform lens*, since we can imagine it as if it were an *optical computer* capable of generating instant Fourier transforms. Now, suppose we illuminate a somewhat idealized transmission grating with a spatially coherent, quasimonochromatic wave, such as the plane wave emanating from a laser or a collimated, filtered Hg arc source (Fig. 14.3). In either case, the amplitude of the field is assumed to be fairly constant over the incident wavefront. The aperture function is then a periodic step function (Fig. 14.4); in other words, as we move from point to point on the object plane, the amplitude of the field is either zero or a constant. If a is the grating spacing, it is also the spatial period of the step function, and its reciprocal is the fundamental spatial frequency of the grating. The central spot ($m = 0$) in the diffraction pattern is the dc term corresponding to a zero spatial frequency—it's the bias level that arises from the fact that the input $\mathscr{A}(y)$ is everywhere positive. This bias level can be shifted by constructing the step-function pattern on a uniform gray background. As the spots in the image (or in this case the transform) plane get farther from the central axis, their associated spatial frequencies (m/a) increase in accord with the grating equation $\sin \theta_m = \lambda(m/a)$. A

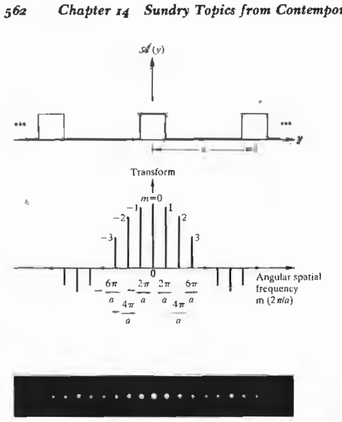


Figure 14.4 Square wave and its transform.

coarser grating would have a larger value of a, so that a given order (m) would be concomitant with a lower frequency, (m/a), and the spots would all be closer to the central or optical axis.

Had we used as an object a transparency resembling the sine target [Fig. 14.2(a)], such that the aperture function varied sinusoidally, there would ideally have only been three spots on the transform plane, these being the zero-frequency central peak and the first order or fundamental ($m = \pm 1$) on either side of the center. Extending things into two dimensions, a crossed grating (or mesh) yields the diffraction pattern shown in Fig. 14.5. Note that in addition to the obvious periodicity horizontally and vertically across the mesh, it is also repetitive, for example, along diagonals. A more involved object, such as a transparency of the surface of the moon, would generate an extremely complex diffraction pattern. Because of the simple [illegible] nature of the grating, we could think of its Fo[illegible] components, but now we will certainly have [illegible] terms of Fourier transforms. In any case [illegible] *light in the diffraction pattern denotes the presence [illegible] spatial frequency, which is proportional to its di[illegible] the optical axis (zero-frequency location).* Frequenc[illegible] ponents of positive and negative sign appear di[illegible] cally opposite each other about the central axi[illegible] could measure the electric field at each point in the transform plane, we would indeed observe the tran[illegible] form of the aperture function, but this is not p[illegible] Instead, what will be detected is the flux-dens[illegible] bution, where at each point the irradiance is propor[illegible] tional to the time average of the electric field squa[illegible] or equivalently to the square of the amplitude [illegible] the particular spatial frequency contribution at that point.

14.1.2 Abbe's Theory of Image Formation

Consider the system depicted in Fig. 14.6(a), which is just an elaborated version of Fig. 14.3(b). Plane monochromatic wavefronts emanating from the collimating lens (L_c) are diffracted by a grating. The result is a distorted wavefront, which we resolve into a set of plane waves, each corresponding to a given [illegible]

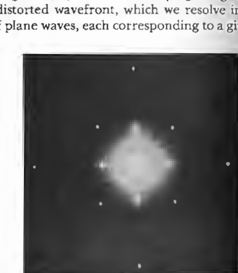


Figure 14.5 Diffraction pattern of a crossed grating. (Source of photo unknown.)

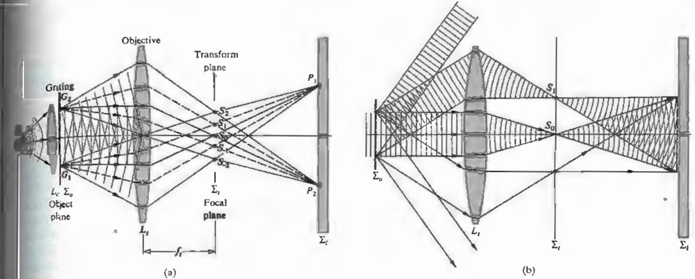


Figure 14.6 Image formation.

[illegible] ±2, ... or spatial frequency and each travel[illegible] a specific direction [Fig. 14.6(b)]. The objective [illegible] (L_t) serves as a *transform lens*, forming the Fraun[illegible] diffraction pattern of the grating on the transform [illegible] Σ_t (which is also the back focal plane of L_t). The [illegible], of course, propagate beyond Σ_t and arrive at the image plane Σ_i. There they overlap and interfere to form an inverted image of the grating. Accordingly, [illegible]ts G_1 and G_2 are imaged at P_1 and P_2, respectively. [illegible] objective lens forms two distinct patterns of interest. One is the Fourier transform on the focal plane [illegible]gate to the plane of the source, and the other is [illegible] image of the object, formed on the plane conjugate [illegible] object plane. Figure 14.7 shows the same setup [illegible] a long, narrow, horizontal slit coherently illuminated.

We can envision the points S_0, S_1, S_2, and so forth [illegible] Fig. 14.6(a) as if they were point emitters of Huygens [illegible]lets, and the resulting diffraction pattern on Σ_i is [illegible] the grating's image. In other words, *the image arises* [illegible] *a double diffraction process.* Alternatively, we can [illegible]gine that the incoming wave is diffracted by the [illegible], and the resulting diffracted wave is then diffrac[illegible] once again by the objective lens. If that lens were not there, a diffraction pattern of the object would appear on Σ_i in place of the image.

These ideas were first propounded by Professor Ernst Abbe (1840–1905) in 1873.* His interest at the time concerned the theory of microscopy, whose relationship to the above discussion is clear if we consider L_t as a microscope objective. Moreover, if the grating is replaced by a piece of some thin translucent material (i.e., the specimen being examined), which is illuminated by light from a small source and condenser, the system certainly resembles a microscope.

Carl Zeiss (1816–1888), who in the mid-1800s was running a small microscope factory in Jena, realized the shortcomings of the trial-and-error development techniques of that era. In 1866 he enlisted the services of Ernst Abbe, then lecturer at the University of Jena, to establish a more scientific approach to microscope

* An alternative and yet ultimately equivalent approach was put forth in 1896 by Lord Rayleigh. He envisaged each point on the object as a coherent source whose emitted wave was diffracted by the lens into an Airy pattern. Each of these in turn was centered on the ideal image point (on Σ_i) of the corresponding point source. Thus Σ_i was covered with a distribution of somewhat overlapping and interfering Airy patterns.

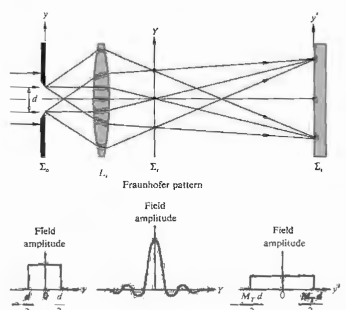


Figure 14.7 The image of a slit.

design. Abbe soon found by experimentation that a larger aperture resulted in higher resolution, even though the apparent cone of incident light filled only a small portion of the objective. Somehow the surrounding "dark space" contributed to the image. Consequently, he took the approach that the then well-known diffraction process that occurs at the edge of a lens (leading to the Airy pattern for a point source) was not operative in the same sense as it was for an incoherently illuminated telescope objective. Specimens, whose size was of the order of λ, were apparently scattering light into the "dark space" of the microscope objective. Observe that if, as in Fig. 14.6(b), the aperture of the objective is not large enough to collect all of the diffracted light, the image does not correspond exactly to that object. Rather it relates to a fictitious object whose complete diffraction pattern matches the one collected by L_t. We know from the previous section that these lost portions of the outer region of the Fraunhofer pattern are associated with the higher spatial frequencies. And, as we shall see presently, their removal will result in a loss in image sharpness and resolution.

Practically speaking, unless the grating con[illegible] earlier has an infinite width, it cannot actually be [illegible] periodic. This means that it has a continuous [illegible] spectrum dominated by the usual discrete Fourier [illegible] terms, the other being much smaller in amplitude [illegible] plicated, irregular objects clearly display the con[illegible] nature of their Fourier transforms. In any [illegible] should be emphasized that *unless the objective lens [illegible] infinite aperture, it functions as a low-pass filter [illegible] spatial frequencies above a given value and passing [illegible] below* (the former being those that extend beyond the physical boundary of the lens). Consequently, all [illegible] tical lens systems will be limited in their ability to [illegible] duce the high spatial frequency content of an [illegible] object under coherent illumination.* It might [illegible] tioned as well that there is a basic nonlinearity [illegible] with optical imaging systems operating at high [illegible] frequencies.†

14.1.3 Spatial Filtering

Suppose we actually set up the system shown in Fig. 14.6(a), using a laser as a plane-wave source. If the points S_0, S_1, S_2, and so on are to be the sources of [illegible] Fraunhofer pattern, the image screen must presu[illegible] be located at $x = \infty$ (although 30 or 40 ft will offer [illegible] At the risk of being repetitious, recall that the reason for using L_t originally was to bring the diffraction pattern of the object in from infinity. We now intro[illegible] an *imaging lens* L_i (Figs. 14.8 and 14.9) in order [illegible] in from infinity the diffraction pattern of [illegible] source points S_0, S_1, S_2, and so forth, thereby [illegible] Σ_i at a convenient distance. The transform [illegible] the light from the object to converge in the form of [illegible] diffraction pattern on the plane Σ_t; that is, [illegible] on Σ_t a two-dimensional Fourier transform of [illegible] To wit, the spatial frequency spectrum of the [illegible] spread across the transform plane. Thereaf[illegible]

* Refer to H. Volkmann, "Ernst Abbe and His Work, [illegible] 1720 (1966), for a more detailed account of Abbe's m[illegible] ments in optics.

† R. J. Becherer and G. B. Parrent, Jr., "Nonlinea[illegible] Imaging Systems," *J. Opt. Soc. Am.* **57**, 1479 (1967).

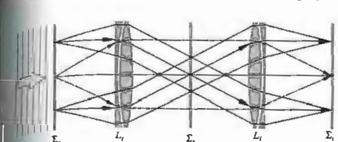


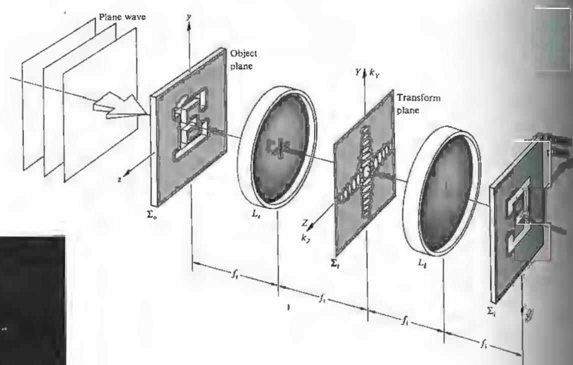
Figure 14.8 Object, transform, and image planes.

"*inverse*" *transform lens*) projects the diffraction pattern of the light distributed over Σ_t onto the image plane. In other words, it diffracts the diffracted beam, which effectively means that it generates an (inverted) inverse transform. Thus essentially an inverse transform of the data on Σ_t appears as the final image. Quite frequently in practice L_t and L_i are identical ($f_t = f_i$) well-corrected multielement lenses [for quality work these might have resolutions of about 150 line pairs/mm—one line pair being a period in Fig. 14.2(b)]. For less demanding applications two projector objectives of large aperture (about 100 mm) having convenient focal lengths of roughly 30 or 40 cm serve quite nicely. One of these lenses is then merely turned around so that both their back focal planes coincide with Σ_t. Incidentally, the [illegible]t or object plane need not be located a focal length [illegible] from L_t; the transform still appears on Σ_t. Moving [illegible] affects only the phase of the amplitude distribution, [illegible] that is generally of little interest. The device shown [illegible] Figs. 14.8 and 14.9 is often referred to as a *coherent [illegible] computer.* It allows us to insert obstructions (i.e., [illegible] or filters) into the tranform plane and in so doing partially or completely block out certain spatial frequen[illegible], stopping them from reaching the image plane. *This process of altering the frequency spectrum of the image is known as* **spatial filtering.** And herein lie some of the [illegible] beautiful, exciting, and promising aspects of con[illegible]orary optics.

[illegible] our earlier discussion of Fraunhofer diffraction [illegible]w that a long narrow slit at Σ_0, regardless of its [illegible]ation and location, generates a transform at Σ_t [illegible]sisting of a series of dashes of light lying along a [illegible]ight line perpendicular to the slit (Fig. 10.11) and passing through the *origin.* Consequently, if the straight-line object is described by $y = mz + b$, the diffraction pattern lies along the line $Y = -Z/m$ or equivalently, from Eqs. (11.64) and (11.65), $k_Y = -k_Z/m$. With this and the Airy pattern in mind we should be able to anticipate some of the gross structure of the transforms of various objects. Be aware as well that these transforms are centered about the zero-frequency optical axis of the system. For example, a transparent plus sign whose horizontal line is thicker than its vertical one has a two-dimensional transform again shaped more or less like a plus sign. The thick horizontal line generates a series of short vertical dashes, while the thin vertical element produces a line of long horizontal dashes. Remember that object elements with small dimensions diffract through relatively large angles. Along with Abbe, one could think of this entire subject in these terms rather than using the concepts of spatial frequency filtering and transforms, which represent the more modern influence of communication theory.

The vertical portions of the symbol E in Fig. 14.9 generate the broad frequency spectrum appearing as the horizontal pattern. Note that all parallel line sources on a given object correspond to a single linear array on the transform plane. This, in turn, passes through the origin on Σ_t (the intercept is zero), just as in the case of the grating. A transparent figure 5 will generate a pattern consisting of both a horizontal and vertical distribution of spots extending over a relatively large frequency range. There will also be a comparatively low-frequency, concentric ring-like structure. The transforms of disks and rings and the like will obviously be circularly symmetric. Similarly a horizontal elliptical aperture will generate vertically oriented concentric elliptical bands. Most often, far-field patterns possess a center of symmetry (see Problems 10.14 and 11.29).

We are now in a better position to appreciate the process of spatial filtering and to that end will consider an experiment very similar to one published in 1906 by A. B. Porter. Figure 14.10(a) shows a fine wire mesh whose periodic pattern is disrupted by a few particles of dust. With the mesh at Σ_0, Fig. 14.10(b) shows the transform as it would appear on Σ_t. Now the fun starts—since the transform information relating to the dust is located in an irregular cloud-like distribution about the center point, we can easily eliminate it by inserting an opaque mask at Σ_t. If the mask has holes at each of the principal maxima, thus passing on only those frequen-

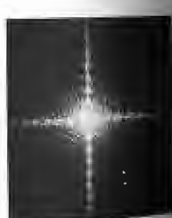


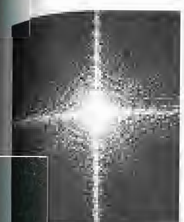

(a)

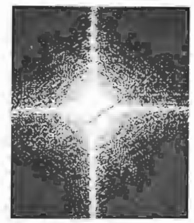
Figure 14.9 The Fourier transform of the letter E via an optical computer, [illegible] through (g) show more and more of the detail of the transform as the exposure [illegible] increased. (Photos by E. H.)


(b)


(c)


(d)


(e)


(f)

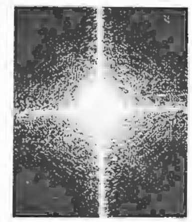
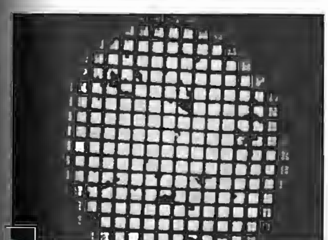

(g)

Figure 14.9 (continued)

cies, the image appears dustless [Fig. 14.11(a)]. At the [illegible] extreme, if we just pass the cloud-like pattern [illegible] center, very little of the periodic structure appears, [illegible]ing an image consisting of essentially just the dust [illegible]cles [14.11(b)]. Passing only the zero-order central [illegible] generates a uniformly illuminated (dc) field, just as if the mesh were no longer in position. Observe that as more and more of the higher frequencies are eliminated, the detail of the image deteriorates markedly [(d), (e), and (f) in Fig. 14.11]. This can be understood quite simply by remembering how a function, with what we might call "sharp edges," was synthesized out of


(a)

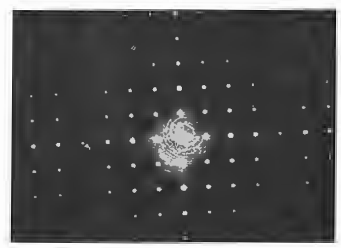

(b)

Figure 14.10 A fine, slightly dusty mesh and its transform. (Photos from D. Dutton, M. P. Givens, and R. E. Hopkins, *Spectra-Physics Laser Technical Bulletin Number 3*.)

harmonic components. The square wave of Fig. 7.13 serves to illustrate the point. It is evident that the addition of higher harmonics serves predominantly to square up the corners and flatten out the peaks and troughs of the profile. In this way, the high spatial frequencies contribute to the sharp edge detail between light and dark regions of the image. The removal of the high-frequency terms causes a rounding out of the step function and a consequent loss of resolution in the two-dimensional case.

What would happen if we took out the dc component [Fig. 14.11(c)] by passing everything but the central spot? A point on the original image that appears black in the photo denotes a near-zero irradiance and perforce a near-zero field amplitude. Presumably, all of the various optical field components cancel each other at that point—ergo, no light. Yet with the removal of the dc term the point in question must certainly then have a nonzero field amplitude. When squared ($I \propto E_0^2/2$) this will generate a nonzero irradiance. It follows that regions that were originally black in the photo will now appear whitish, while regions that were white will become grayish, as in Fig. 14.12.

Let's now examine some of the possible applications of this technique. Figure 14.13(a) shows a composite photograph of the Moon consisting of film strips pieced together to form a single mosaic. The video data were telemetered to Earth by *Lunar Orbiter I*. Clearly the grating-like regular discontinuities between adjacent strips in the object photograph generate the broad-bandwidth, vertical-frequency distribution evident in Fig. 14.13(c). When these frequency components are blocked, the enhanced image shows no sign of having been a mosaic. In very much the same way, one can suppress extraneous data in bubble chamber photographs of subatomic particle tracks.* These photographs are made difficult to analyze because of the presence of the unscattered beam tracks (Fig. 14.14), which, since they are all parallel, are easily [illegible]ved by spatial filtering.

Consider the familiar half-tone or facsimile [illegible] by which a printer can create the illusion of va[illegible] tones of gray while using only black ink and [illegible] paper (take a close look at a newspaper photog[illegible]h). If a transparency* of such a facsimile is inserte[illegible] at Σ_0 [illegible] Fig. 14.8, its frequency spectrum will appear on Σ_t. Once again the relatively high-frequency comp[illegible] arising from the half-tone mesh can easily be elimi[illegible]. This yields an image in shades of gray (Fig. [illegible]) showing none of the discontinuous nature of the original. One could construct a precise filter to ob[illegible] only the square mesh frequencies by actually [illegible] a negative transparency of the transform of th[illegible] checkerboard array. Alternatively, it usually [illegible] use a low-pass circular aperture filter, and in [illegible] inadvertently discard some of the high-frequen[illegible] of the original scene, at least as long as th[illegible] frequency is comparatively high. The same p[illegible] can be used to remove the graininess of highly [illegible] photographs, which is of value, for example, [illegible] photo reconnaissance. In contrast, we could sh[illegible] the details in a slightly blurred photograph by e[illegible]ing its high-frequency components. This could [illegible] with a filter that preferentially absorbed the low-frequency portion of the spectrum. A great deal of effort, beginning in the 1950s has gone into the study of photographic image enhancement, and the ensuing successes have been notable indeed. Promin[illegible] among these contributors is A. Maréchal of th[illegible] Institut d'Optique, Université de Paris, who has [illegible] absorbing and phase-shifting filters to recons[illegible] detail in badly blurred photographs. These [illegible]ters are transparent coatings deposited on optical fla[illegible] so as to retard the phase of various portions of the [illegible]pectrum (Section 14.1.4).

As this work in optical data processing continues [illegible]

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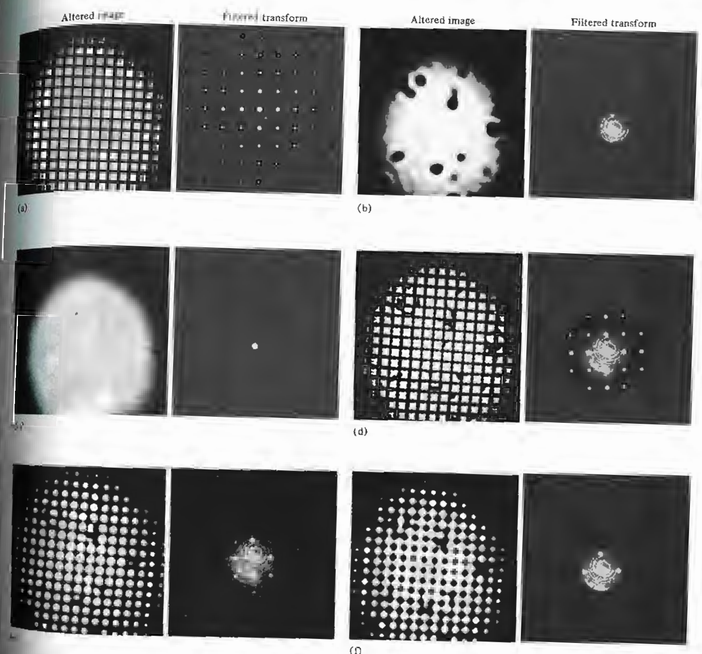
* D. G. Falconer, "Optical Processing of Bubble Chamber Photographs," *Appl. Opt.* 5, 1365 (1966), includes some additional uses for the coherent optical computer.

* Polaroid 55 P/N film is satisfactory for medium[illegible] while Kodak 649 plates are good where higher resolu[illegible] of the transparency.



[illegible]re 14.11 Images resulting when various portions of the diffraction pattern of Fig. 14.10(b) are obscured by the accompanying masks or [illegible]al filters. (Photos from D. Dutton, M. P. Givens, and R. E. Hopkins, *Spectra-Physics Laser Technical Bulletin Number 5*.)

the coming decades, we will surely see the replacement of the photographic stages, in increasingly many applications, by real-time electro-optical devices (e.g., arrays of ultrasonic light modulators forming a multichannel input are already in use).* The coherent optical computer will reach a certain maturity, becoming an even more powerful tool when the input, filtering, and output functions are performed electro-optically. A continuous stream of real-time data could flow into and out of such a device.

14.1.4 Phase Contrast

It was mentioned rather briefly in the last section that the reconstructed image could be altered by introducing a phase-shifting filter. Probably the best-known example of this technique dates back to 1934 and the work of the Dutch physicist Fritz Zernike, who invented the method of phase contrast and applied it in the *phase-contrast microscope.*

An object can be "seen" because it stands out from its surroundings—it has a color, tone, or lack of color, which provides contrast with the background. This kind of structure is known as an *amplitude object,* because it is observable by dint of variations that it causes in the amplitude of the lightwave. The wave that is either reflected or transmitted by such an object becomes *amplitude modulated* in the process. In contradistinction, it is often desirable to "see" *phase objects,* that is, ones that are transparent, thereby providing practically no contrast with their environs and altering only the phase of the detected wave. The optical thickness of such objects generally varies from point to point as either the refractive index or the actual thickness or both vary.

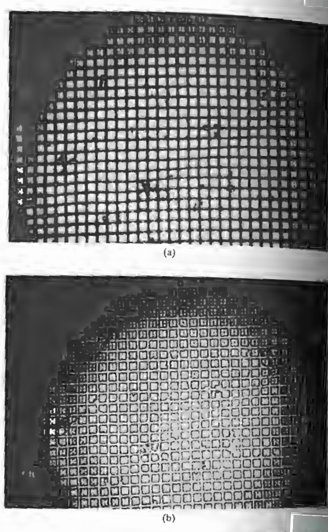


Figure 14.12 Part (b) is a filtered version of (a) [illegible] the zeroth order was removed. (Photos from D. Dutton, M. [illegible] E. Hopkins, *Spectra-Physics Laser Technical Bulletin* [illegible]

Obviously, since the eye cannot detect phase va[illegible] such objects are invisible. This is the problem [illegible] biologists to develop techniques for staining [illegible] microscope specimens and in so doing to con[illegible] objects into amplitude objects. But this [illegible] unsatisfactory in many respects, [illegible] the

* We have only touched on the subject of optical data processing; a more extensive discussion of these matters is given, for example, by Goodman in *Introduction to Fourier Optics,* Chapter 7. That text also includes a good reference list for further reading in the journal literature. Also see P. F. Mueller, "Linear Multiple Image Storage," *Appl. Opt.* 8, 267 (1969). Here, as in much of modern optics, the frontiers are fast moving, and obsolescence is a hard rider.

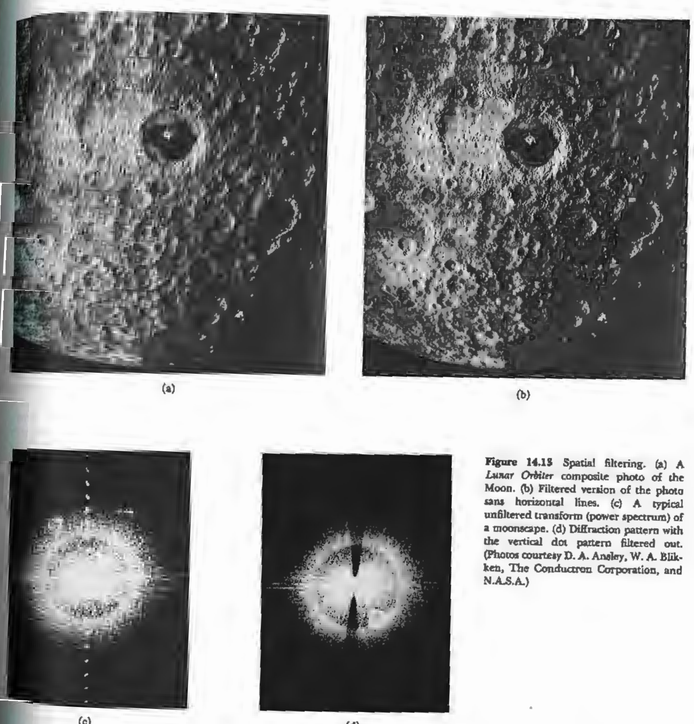


Figure 14.13 Spatial filtering. (a) A *Lunar Orbiter* composite photo of the Moon. (b) Filtered version of the photo sans horizontal lines. (c) A typical unfiltered transform (power spectrum) of a moonscape. (d) Diffraction pattern with the vertical dot pattern filtered out. (Photos courtesy D. A. Ansley, W. A. Blikken, The Conductron Corporation, and N.A.S.A.)

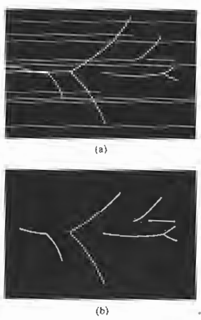


Figure 14.14 Unfiltered and filtered bubble-chamber tracks.

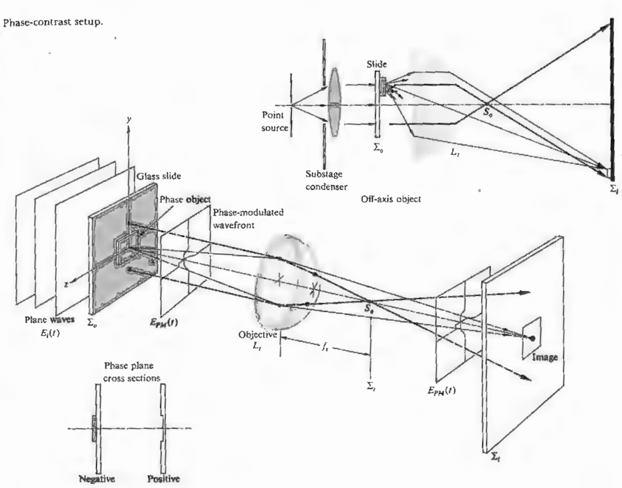
stain kills the specimen whose life processes are under study, as is all too often the case.

Recall that diffraction occurs when a portion of the surface of constant phase is obstructed in some way, that is, when a region of the wavefront is altered (either in amplitude or phase, i.e., shape). Suppose then that a plane wave passes through a transparent particle, which retards the phase of a region of the [illegible] emerging wave is no longer perfectly planar [illegible]ut contains a small indentation corresponding to [illegible]he area retarded by the specimen; the wave is *phase*[illegible]*odulated.*

Taking a rather simplistic view of things, [illegible] imagine the phase-modulated wave $E_{PM}(\mathbf{r}, t)$ (Fig. 14.16) to consist of the original incident plane wave $E_i(x, t)$ plus a localized disturbance $E_d(\mathbf{r}, t)$. (The sym[illegible] $\mathbf{r}$ means that E_{PM} and E_d depend on x, y, and [illegible]; i.e., they vary over the yz-plane, whereas E_i is uniform and does not.) Indeed, if the phase retardation is very [illegible] the localized disturbance is a wave of very small [illegible]tude, E_{0d}, lagging by just about $\lambda_0/4$, as in Fig. [illegible] There the difference between $E_{PM}(\mathbf{r}, t)$ and [illegible] shown to be $E_d(\mathbf{r}, t)$. The disturbance $E_i(x, t)$ [illegible] the direct or *zeroth-order wave,* while $E_d(\mathbf{r}, t)$ is the [illegible]*ted wave.* The former produces a uniformly illu[illegible] field at Σ_i, which is unaffected by the object, [illegible] latter carries all of the information about the [illegible] structure of the particle. After broadly diverg[illegible] the object, these higher-order spatial freque[illegible] (see Section 14.1.2) are caused to converge on [illegible] plane. The direct and diffracted waves recom[illegible] of phase by $\pi/2$, again forming the phase-modu[illegible] wave. Since the amplitude of the reconstructed wave $E_{PM}(\mathbf{r}, t)$ is everywhere the same on Σ_i, even [illegible] the phase varies from point to point, the flux density is uniform, and no image is perceptible. [illegible]se, the

Figure 14.15 A self-portrait of K. E. Beth[illegible] of only black and white regions as in a halftone. [illegible] the high frequencies are filtered out, sh[illegible]des of [illegible] appear and the sharp boundaries vanish. [illegible] Phillips, *Am. J. Phys.* **37**, 536 (1969).]

Figure 14.16 Phase-contrast setup.



[illegible]th-order spectrum of a phase grating will be $\pi/2$ [illegible]f phase with the higher-order spectra.

[illegible]e could somehow shift the relative phase between [illegible] diffracted and direct beams by an additional $\pi/2$ [illegible] to their recombination, they would still be coherent and could then interfere either constructively or [illegible]uctively (Fig. 14.18). In either case, the reconstructed [illegible]avefront over the region of the image would then be [illegible]plitude modulated—the image would be visible. [illegible]an see this in a very simple analytical way where

$$E_i(x, t)|_{x=0} = E_0 \sin \omega t \tag{14.1}$$

[illegible]ncoming monochromatic lightwave at Σ_o without the specimen in place. The particle will induce a position-dependent phase variation $\phi(y, z)$ such that the wave just leaving it is

$$E_{PM}(\mathbf{r}, t)|_{x=0} = E_0 \sin [\omega t + \phi(y, z)]. \tag{14.2}$$

This is a constant-amplitude wave, which is essentially the same on the conjugate image plane. That is, there are some losses, but if the lens is large and aberration-free and we neglect the orientation and size of the image, Eq. (14.2) will suffice to represent the PM wave on either Σ_o or Σ_i. Reformulating that disturbance as

$$E_{PM}(y, z, t) = E_0 \sin \omega t \cos \phi + E_0 \cos \omega t \sin \phi \tag{14.3}$$

and limiting ourselves to *very small values* of ϕ, we obtain

$$E_{PM}(y, z, t) = E_0 \sin \omega t + E_0 \phi(y, z) \cos \omega t.$$

The first term is independent of the object, while the second term obviously isn't. Thus, as above, if we change their relative phase by $\pi/2$, that is, either change the cosine to sine or vice versa, we get

$$E_{AM}(y, z, t) = E_0[1 + \phi(y, z)] \sin \omega t, \qquad (14.4)$$

which is an amplitude-modulated wave. Observe that $\phi(y, z)$ can be expressed in terms of a Fourier expansion, thereby introducing the spatial frequencies associated with the object. Incidentally, this discussion is precisely analogous to the one proposed in 1936 by E. H. Armstrong for converting AM radio waves to FM [$\phi(t)$ could be thought of as a frequency modulation wherein the

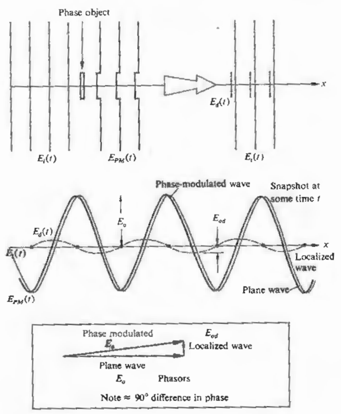


Figure 14.17 Wavefronts in the phase-contrast process.

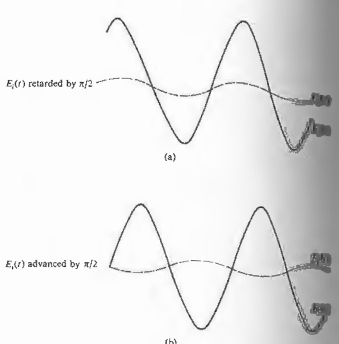


Figure 14.18 Effect of phase shifts.

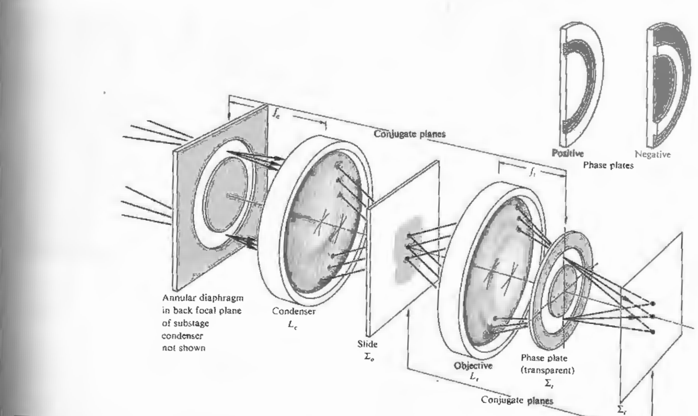
zeroth-order term is the carrier]. An electrical ba[illegible] filter was used to separate the carrier from the [illegible] ing information spectrum so that the $\pi/2$ phase shift could be accomplished. Zernike's method of doing essentially the same thing is as follows. He inserted [illegible] spatial filter in the transform plane Σ_t of the objecti[illegible] (Fig. 14.16), which was capable of inducing th[illegible] phase shift. Observe that the direct light actually [illegible] a small image of the source on the optical axis [illegible] location of Σ_t. The filter could then be a small ci[illegible] indentation of depth d etched in a transparent gl[illegible] plate of index n_g. Ideally, only the direct beam would pass through the indentation, and in so doing it w[illegible] take on a *phase advance* with respect to the diffra[illegible] wave of $(n_g - 1)d$, which is made to equal $\lambda_0/4$. A[illegible] of this sort is known as a *phase plate*, and since its effe[illegible] corresponds to Fig. 14.18(b), that is, destructive inter- ference, phase objects that are thicker or have hi[illegible] indices appear dark against a bright background.

[illegible]stead, the phase plate had a small raised disk at its [illegible]nter, the opposite would be true. The former case is [illegible]lled *positive-phase contrast;* the latter, *negative-phase* [illegible]*ntrast.*

In actual practice a brighter image is obtained by [illegible]ing a broad, rather than a point, source along with a [illegible]bstage condenser. The emerging plane waves illumi- [illegible] an annular diaphragm (Fig. 14.19), which, since it [illegible] source plane, is conjugate to the transform plane [illegible]the objective. The zeroth-order waves, shown in the [illegible]gure, pass through the object according to the tenets [illegible] geometrical optics. They then traverse the thin [illegible]nular region of the phase plate located at Σ_t. That [illegible]gion of the plate is quite small, and so the cone of [illegible]ffracted rays, for the most part, misses it. By making [illegible] annular region absorbing as well (a thin metal film [illegible]ll do), the very large uniform zeroth-order term (Fig. 14.20) is reduced with respect to the higher orders, and the contrast improves. Or, if you like, E_0 is reduced to a value comparable with that of the diffracted wave E_{0d}. Generally a microscope will come with an assortment of these phase plates having different absorptions.

In the parlance of modern optics (the still-blushing bride of communications theory), phase contrast is simply the process whereby we introduce a $\pi/2$ phase shift in the zeroth-order spectrum of the Fourier transform of a phase object (and perhaps attenuate its amplitude as well) through the use of an appropriate spatial filter.

The phase-contrast microscope, which earned Zernike the Nobel prize in 1953, has found extensive applications (Fig. 14.21), perhaps the most fascinating of which is the study of the life functions of otherwise invisible organisms.



[illegible]re 14.19 Phase contrast (only zeroth order shown).

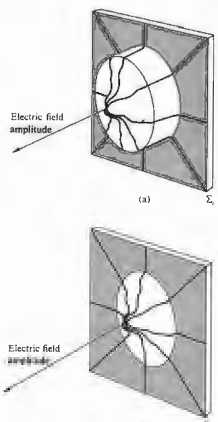


Figure 14.20 Field amplitude over a circular region on the image plane. In one case there is no absorption in the phase plate and the irradiance would be a small ripple on a great plateau. With the zeroth order attenuated the contrast increases.

14.1.5 The Dark-Ground and Schlieren Methods

Suppose we go back to Fig. 14.16, where we were examining a phase object, and this time rather than retard and attenuate the central zeroth order, we remove it completely with an opaque disk at S_o. Without the object in place the image plane will be completely dark—ergo the name *dark ground.* With the object in position only the localized diffracted wave will appear at Σ_i to form the image. (This can also be accomplished in microscopy by illuminating the object obliquely so that no direct light enters the objective lens.) Obse[illegible] that by eliminating the dc contribution, the amplit[illegible] distribution (as in Fig. 14.20), will be lowered [illegible] tions that were near zero prior to filtering will [illegible] negative. Inasmuch as irradiance is proportio[illegible] amplitude squared, this will result in somewhat of a contrast reversal from that which would have been seen in phase contrast (see Section 4.1.3). In general this technique has not been as satisfactory as the phase-contrast method, which generates a flux-density distribution across the image that is directly proportional to the phase variations induced across the object.

(a)

(b)

Figure 14.21 (a) A conventional photomicrograph of [illegible] and bacteria. (b) A phase photomicrograph of the same scene. [illegible] by T. J. Lowery and R. Hawley.)

In 1864 A. Toepler introduced a procedure for examining defects in lenses, which has come to be known as the **schlieren** method.* We will discuss it here because of the widespread current usage of the method in a broad range of fluid dynamics studies and furthermore because it is another beautiful example of the application of spatial filtering. Schlieren systems are particularly useful in ballistics, aerodynamics, and ultrasonic wave analysis (Fig. 14.22), indeed wherever it is desirable to examine pressure variations as revealed by refractive-index mapping.

Suppose that we set up any one of the possible arrangements for viewing Fraunhofer diffraction (e.g., Fig. 10.5 or 10.84). But now, instead of using an aperture of some sort as the diffracting amplitude object, we insert a phase object, for example, a gas-filled chamber (Fig. 14.23). Again a Fraunhofer pattern is formed in Σ_t, and if that plane is followed by the objective lens of a camera, an image of the chamber is formed on the film plane. We could then photograph any amplitude objects within the test area, but, of course, phase objects would still be invisible. Imagine that we now introduce a knife edge at Σ_t, raising it from below until it obstructs (sometimes only partially) the zeroth-order light and therefore all the higher orders on the bottom side as well. Just as in the dark-ground method, phase objects are then perceptible. Inhomogeneities in the test chamber windows and flaws in the lenses are also noticeable. For this reason and because of the large field of view usually required, mirror systems (Fig. 14.24) have now become commonplace.

Quasimonochromatic illumination is generally made use of when resulting data are to be analyzed electronically, for example, with a photodetector. Sources with a broad spectrum, on the other hand, allow us to exploit the considerable color sensitivity of photographic emulsions, and a number of color schlieren systems have been devised.

* [illegible] word *Schlieren* in German means streaks or striae. It's frequently [illegible] because all nouns are in German and not because there [illegible] Mr. Schlieren.

Figure 14.22 A schlieren photo of a spoon in a candle flame. (Photo by E. H.)

14.2 LASERS AND LASERLIGHT

During the early 1950s a remarkable device known as the *maser* came into being through the efforts of a number of scentists. Principal amongst these people were Charles Hard Townes of the U.S.A. and Alexandr Mikhailovich Prokhorov and Nikolai Gennadievich Basov of the U.S.S.R., all of whom shared the 1964 Nobel Prize in Physics for their work. The maser, which is an acronym for Microwave Amplification by Stimulated Emission of Radiation, is, as the name implies, an extremely low-noise, microwave amplifier.* It func-

* See James P. Gorden, "The Maser," *Sci. Am.* **199**, 42 (December 1958).

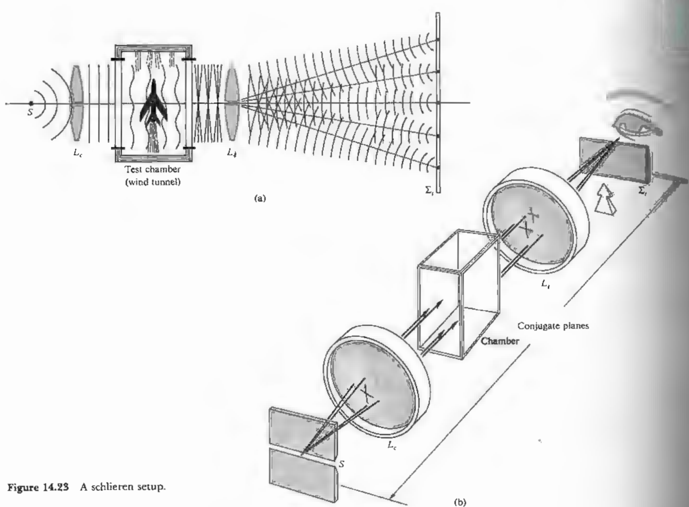


Figure 14.23 A schlieren setup.

tioned in what was then a rather unconventional way, making direct use of the quantum-mechanical interaction of matter and radiant energy. Almost immediately after its inception speculation arose as to whether or not the same technique could be extended into the optical region of the spectrum. In 1958 Townes and Arthur L. Schawlow prophetically set forth the general physical conditions that would have to be met in order to achieve Light Amplification by Stimulated Emission of Radiation. And then in July of 1960 Theodore H. Maiman announced the first successful operation of an optical maser or **laser**—certainly one of the great milestones in the history of optics, and indeed in the history of science, had been achieved.

14.2.1 The Laser

Speaking first in generalities, suppose we have a collection of atoms, as for example, in a solid, gas, or liquid. Recall that each atom (taken as a system composed of

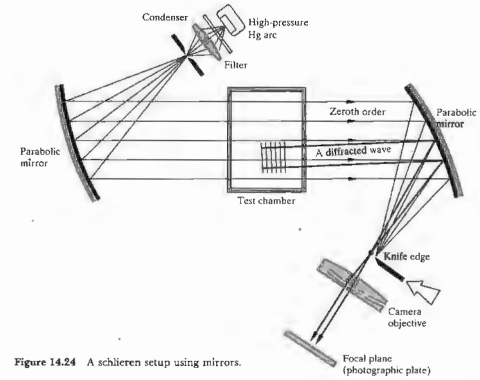


Figure 14.24 A schlieren setup using mirrors.

a nucleus and electron cloud) possesses a certain amount of internal energy, and each tends to maintain its lowest energy configuration. This is the *ground state* for that particular kind of atom. Furthermore, each atom can exist in specific, well-defined configurations corresponding to higher energies than the ground state. Any of these are termed *excited states.*

In a conventional light source, such as a tungsten lamp, energy is *pumped* into the reacting atoms, in this case located within the filament. These are consequently "raised" into excited states. Each can then drop back *spontaneously* (i.e., without external inducement) to the ground state, emitting the absorbed energy in the form of a randomly directed photon. Atoms in this kind of source radiate essentially independently. The photons in the emitted stream bear no particular phase relationship with each other, and the light is incoherent. It varies in phase from point to point and moment to moment.

Now imagine that light impinges on an atomic system of some sort. If an incident photon is energetic enough, it may be absorbed by an atom, raising the latter to an excited state. It was pointed out by Einstein in 1917 that an excited atom can revert to a lower state (which need not necessarily be the ground state) through photon emission via two distinctive mechanisms. In one instance the atom emits energy spontaneously, while in the other it is triggered into emission by the presence of electromagnetic radiation of the proper frequency. The latter process is known as **stimulated emission**, and it is a key to the operation of the laser. In either situation the emerging photon will carry off the energy difference ($h\nu_{if}$) between the initial higher state $|i\rangle$ and the final lower state $|f\rangle$, that is,

$$\mathscr{E}_i - \mathscr{E}_f = h\nu_{if}, \tag{14.5}$$

where $\mathscr{E}_i$ and $\mathscr{E}_f$ are the energies of the two states.

If an incident electromagnetic wave is to trigger an excited atom into stimulated emission, it must have the frequency ν_{if}. A remarkable feature of this process is that *the emitted photon is in phase with, has the polarization of, and propagates in the same direction as, the stimulating radiation.* Thus the photon is said to be in the same *radiation mode* as the incident wave and tends to add to it, increasing its flux density. However, since most of the atoms are ordinarily in the ground state, absorption is usually far more likely than stimulated emission. But this raises an intriguing point: What would happen if a substantial percentage of the atoms could somehow be excited into an upper state, leaving the lower state all but empty? For obvious reasons this is known as **population inversion**. An incident photon of the proper frequency could then trigger an avalanche of stimulated photons—*all in phase.* The initial wave would continue to build, so long as there were no dominant competitive processes (such as scattering) and provided the population inversion could be maintained. In effect, energy (electrical, chemical, optical, etc.) would be pumped in to sustain the inversion, and a beam of light would be extracted after sweeping across the active medium.

i) The First (Pulsed Ruby) Laser

To see how all of this is accomplished in practice, let's take a look at Maiman's original device (Fig. 14.25). The first operative laser had as its active medium a small, cylindrical, synthetic, pale pink ruby, that is, an Al_2O_3 crystal containing about 0.05 percent (by weight) of Cr_2O_3. Ruby, which is still one of the most common of the crystalline laser media, had been used earlier in maser applications and was suggested for use in the laser by Schawlow. The rod's end faces were polished flat, parallel and normal to the axis. Then both were silvered (one only partially) to form a **resonant cavity**. It was surrounded by a helical gaseous discharge flashtube, which provided broadband **optical pumping**. Ruby appears red because the chromium atoms have absorption bands in the blue and green regions of the spectrum [Fig. 14.26(a)]. Firing the flashtube generated an intense burst of light lasting for a few milliseconds. Much of this energy is lost in heat, but many of the Cr^{3+} ions are excited into the absorption bands. A simplified energy-level diagram appears in Fig. 14.26(b). The excited ions rapidly relax (in about 100 ns), giving up energy to the crystal lattice and making nonradiative transitions, they preferentially drop "down" to a pair of closely spaced, especially long-lived, interim states. They remain in these so-called **metastable states** for up to several milliseconds (~3 ms at room temperature) before randomly, and in most cases spontaneously, dropping down to the ground state. This is accompanied by the emission of the characteristic red fluorescent radiation of ruby. The lower-level transition dominates, and the resulting emission occurs in a [illegible] broad spectral range centered about 694.3 nm; it emerges in all directions and is incoherent. However, when the pumping rate is increased somewhat, a population inversion occurs, and the first few spontaneously emitted photons stimulate a chain reaction. One quantum triggers the rapid, in-phase emission of another, drawing energy from the metastable atoms into the evolving lightwave. The wave continues to grow as it sweeps back and forth across the active medium (provided enough energy is available to overcome losses at the [illegible] ends). Since one of those reflecting surfaces was only partially silvered, an intense pulse of red laser light (lasting about 0.5 ms and having a linewidth of about 0.01 nm) emerges from that end of the ruby rod. Notice how neatly everything works out. The broad **absorption** bands make the initial excitation rather easy, while the long lifetime of the metastable state facilitates the population inversion. The atomic system in effect consists of (1) the absorption bands, (2) the metastable state, and (3) the ground state. Accordingly it is spoken of as a [illegible] laser.

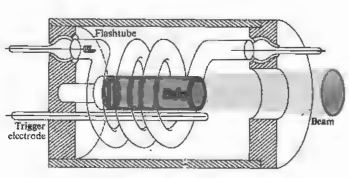


Figure 14.25 The first ruby-laser configuration, just about life-sized.

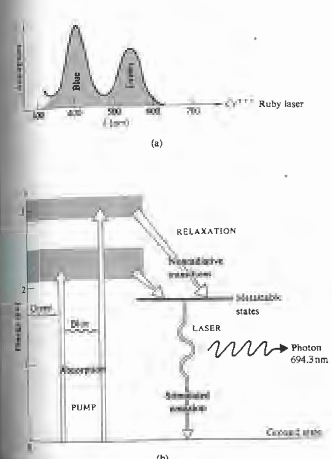


Figure 14.26 Ruby-laser energy levels.

Today's ruby laser is generally a high-power source of pulsed coherent radiation used extensively in work on **interferometry**, plasma diagnostics, holography, and so forth. Such devices operate with coherence lengths of from 0.1 m to 10 m. Modern configurations usually have flat external mirrors, one totally and the other partially reflecting. As an oscillator, the ruby laser generates millisecond pulses in the energy range from around 50 J to upwards of 100 J, but by using a tandum **oscillator-amplifier** setup, energies well in excess of 100 J can be produced. The commercial ruby laser typically operates at a modest overall efficiency of less than 1%, producing a beam that has a diameter ranging from 1 mm to about 25 mm, with a divergence of from 0.25 mrad to about 7 mrad.

ii) Optical Resonant Cavities

The resonant cavity, which in this case is of course a Fabry–Perot etalon, plays a most significant role in the operation of the laser. In the early stages of the laser process, spontaneous photons are emitted in every direction, as are the concommitant stimulated photons. But all of these, with the singular exception of those propagating very nearly along the cavity axis, quickly pass out of the sides of the ruby. In contrast, the axial beam continues to build as it bounces back and forth across the active medium. This accounts for the amazing degree of collimation of the issuing laserbeam, which is then effectively a coherent plane wave. Though the medium acts to amplify the wave, the *optical feedback* provided by the cavity converts the system into an oscillator and hence into a light generator—the acronym is thus somewhat of a misnomer.

In addition, the disturbance propagating within the cavity takes on a standing-wave configuration determined by the separation (L) of the mirrors. The cavity resonates (i.e., standing waves exist within it) when there is an integer number (m) of half wavelengths spanning the region between the mirrors. The idea is simply that there must be a node at each mirror, and this can only happen when L equals a whole number multiple of $\lambda/2$ (where $\lambda = \lambda_0/n$). Thus

$$m = \frac{L}{\lambda/2}$$

and

$$\nu_m = \frac{mv}{2L}. \qquad (14.6)$$

There are therefore an infinite number of possible oscillatory **longitudinal cavity modes**, each with a distinctive frequency ν_m. Consecutive modes are separated by a constant difference,

$$\nu_{m+1} - \nu_m = \Delta\nu = \frac{v}{2L}, \qquad (14.7)$$

which is the free spectral range of the etalon [Eq. (9.79)] and, incidentally, the inverse of the round-trip time. For a gas laser 1 m long, $\Delta\nu \approx 150$ MHz. The resonant modes of the cavity are considerably narrower in frequency than the bandwidth of the normal spontaneous atomic transition. These modes, whether the device is constructed so that there is one or more, will be the ones that are sustained in the cavity, and hence the emerging beam is restricted to a region close to those frequencies (Fig. 14.27). In other words, the radiative transition makes available a relatively broad range of frequencies out of which the cavity will select and amplify only certain narrow bands and, if desired, even only one such band. This is the origin of the laser's extreme quasimonochromaticity. Thus while the bandwidth of the ruby transition to the ground state is roughly a rather broad 0.53 nm (330 GHz)—because of interactions of the chromium ions with the lattice—the corresponding laser cavity bandwidth, the frequency spread of the radiation of a single resonant mode, is a much narrower 0.00005 nm (30 MHz). This situation is depicted in Fig. 14.27(b), which shows a typical transition lineshape and a series of corresponding cavity spikes—in this case each is separated by $v/2L$, and each is 30 MHz wide.

A possible way to generate only a single mode in the cavity would be to have the mode separation, as given by Eq. (14.7), exceed the transition bandwidth. Then only one mode would fit within the range of available frequencies provided by the transition. For a ruby laser (with an index of refraction of 1.76) a cavity length of a few centimeters will easily insure single longitudinal mode operation. The drawback of this particular approach is that it limits the length of the active region contributing energy to the beam and so limits the output power of the laser.

In addition to the longitudinal or axial modes of oscillation, which correspond to standing waves set up along the cavity or z-axis, **transverse modes** can be sustained as well. Since the fields are very nearly normal to z, these are known as TEM_{mn} modes (transverse electric and magnetic). The m and n subscripts are the integer number of transverse nodal lines in the x- and y-directions across the emerging beam. That is to say,

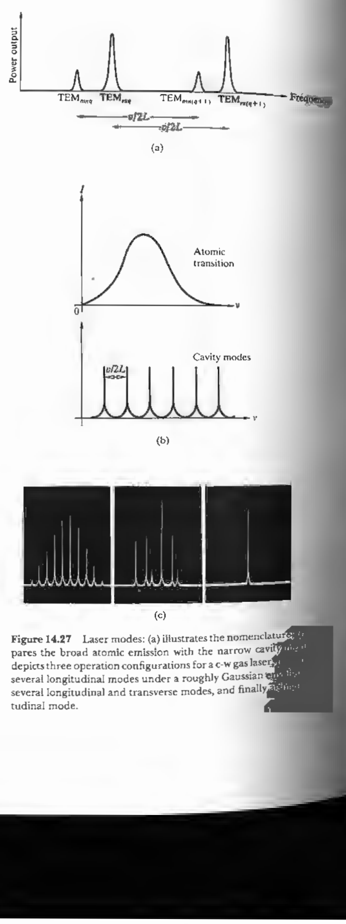


Figure 14.27 Laser modes: (a) illustrates the nomenclature; [illegible] pares the broad atomic emission with the narrow cavity [illegible] depicts three operation configurations for a c-w gas laser, [illegible] several longitudinal modes under a roughly Gaussian [illegible] several longitudinal and transverse modes, and finally, [illegible] tudinal mode.

the beam is segmented in its cross section into one or more regions. Each such array is associated with a given TEM mode, as shown in Figs. 14.28 and 14.29. The lowest order or TEM_{00} transverse mode is perhaps the most widely used, and this for several compelling reasons: the flux density is ideally Gaussian over the beam's cross section (Fig. 14.30); there are no phase shifts in the electric field across the beam, as there are in other modes, and so it is completely spatially coherent; the

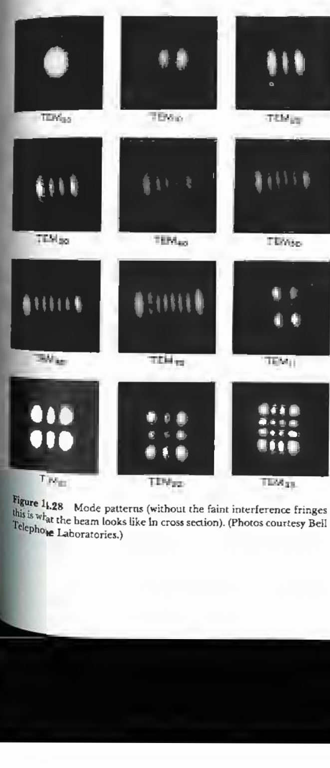


Figure 14.28 Mode patterns (without the faint interference fringes this is what the beam looks like in cross section). (Photos courtesy Bell Telephone Laboratories.)

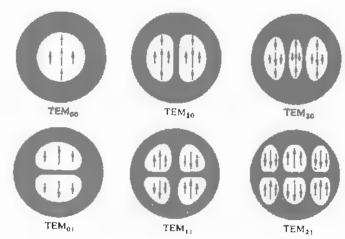


Figure 14.29 Mode configurations (rectangular symmetry). Circularly symmetric modes are also observable, but any slight asymmetry (such as Brewster windows) destroys them.

beam's angular divergence is the smallest; and it can be focused down to the smallest-sized spot. Note that the amplitude in this mode is actually not constant over the wavefront, and it is consequently an inhomogeneous wave.

A complete specification of each mode has the form TEM_{mnq}, where q is the longitudinal mode number. For each transverse mode (m, n) there can be many longitudinal modes (i.e., values of q). Often, however, it's unnecessary to work with a particular longitudinal mode, and the q subscript is usually simply dropped.*

There are several additional cavity arrangements that are of considerably more practical significance than is the original plane-parallel setup (Fig. 14.31). For example, if the planar mirrors are replaced by identical concave spherical mirrors separated by a distance very nearly equal to their radius of curvature, we have the *confocal* resonator. Thus the focal points are almost coincident on the axis midway between mirrors—ergo

* Take a look at R. A. Phillips and R. D. Gehrz, "Laser Mode Structure Experiments for Undergraduate Laboratories," *Am. J. Phys.* **38**, 429 (1970).

the name confocal. If one of the spherical mirrors is made planar, the cavity is termed a *hemispherical* or *hemiconcentric*, resonator. Both these congfigurations are considerably easier to align than is the plane-parallel form. Laser cavities are said to be either *stable* or *unstable* to the degree that the beam tends to retrace itself and so remain relatively close to the optical axis (Fig. 14.32). A beam in an unstable cavity will "walk out," going farther from the axis on each reflection until it quickly leaves the cavity altogether. By contrast, in a stable configuration (with mirrors that are, say, 100% and 98% reflective) the beam might traverse the resonator 50 times or more. Unstable resonators are commonly used in high-power lasers, where the fact that the beam traces across a wide region of the active medium enhances the amplification and allows for more energy to be extracted. This approach will be especially useful for media (like carbon dioxide or argon) wherein the beam gains a good deal of energy on each sweep of the cavity. In other words, the needed number of sweeps is determined by the so-called *small-signal gain* of the active medium. The actual selection of a resonator configuration is governed by the specific requirements of the system—there is no universally best arrangement.

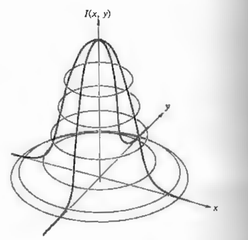


Figure 14.30 Gaussian irradiance distribution.

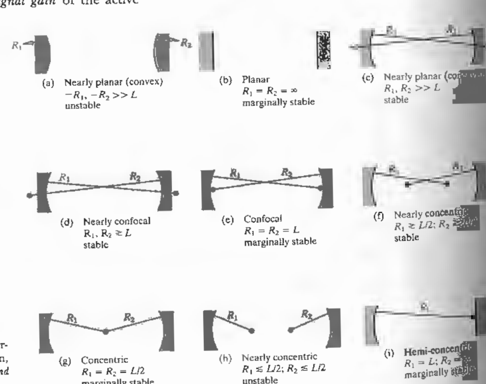


Figure 14.31 Laser cavity configurations. (Adapted from O'Shea, Callen, and Rhodes, *An Introduction to Lasers and Their Applications*.)

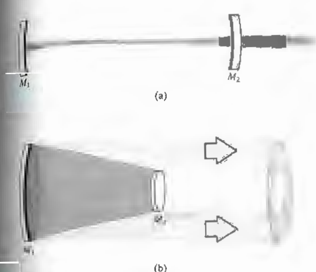


Figure 14.32 Stable and unstable laser resonators. (Adapted from O'Shea, Callen, and Rhodes, *An Introduction to Lasers and Their Applications*.)

As can be seen in Fig. 14.32(a), when curved mirrors form the cavity there is a tendency to "focus" the beam, giving it a minimum cross section or *waist* of diameter D_0. Under such circumstances the external divergence of the laserbeam is essentially a continuation of the divergence out from this waist. Thus while two plane mirrors will produce a beam that is aperture limited via diffraction, this will not now be the case. Recall Eq. (10.58), which describes the radius of the Airy disk, and divide both sides by f to get the half-angular width of the diffracted circular beam of diameter D. Doubling this yields Φ, the full-angular width or divergence of an aperture-limited laserbeam:

$$\Phi \approx 2.44\lambda/D.$$

By comparison, far from the region of minimum cross section, the full-angular width of a waisted laserbeam is

$$\Phi \approx 1.27\lambda/D_0, \qquad (14.8)$$

where D_0 can be calculated from the particular cavity configuration.

The decay of energy in a cavity is expressed in terms of the Q or **quality factor** of the resonator. The origin of the expression dates back to the early days of radio engineering, when it was used to describe the performance of an oscillating (tuning) circuit. A high-Q, low-loss circuit meant a narrow bandpass and a sharply tuned radio. If an optical cavity is somehow disrupted, as for example by the displacement or removal of one of the mirrors, the laser action generally ceases. When this is done deliberately in order to delay the onset of oscillation in the laser cavity, it's known as *Q-spoiling* or **Q-switching**. The power output of a laser is self-limited in the sense that the population inversion is continuously depleted through stimulated emission by the radiation field within the cavity. However, if oscillation is prevented, the number of atoms pumped into the (long-lived) metastable state can be considerably increased, thereby creating a very extensive population inversion. When the cavity is switched on at the proper moment, a tremendously powerful *giant pulse* (perhaps up to several hundred megawatts) will emerge as the atoms drop down to the lower state almost in unison. A great many *Q-switching* arrangements utilizing various control schemes, for example, bleachable absorbers that become transparent under illumination, rotating prisms and mirrors, mechanical choppers, ultrasonic cells, or electro-optic shutters such as Kerr or Pockels cells, have all been used.

iii) The Helium–Neon Laser

Maiman's announcement of the first operative laser came at a New York news conference on July 7, 1960.* By February of 1961 Ali Javan and his associates W. R. Bennett, Jr., and D. R. Herriott had reported the successful operation of a *continuous-wave* (c-w) helium–neon, gas laser at 1152.3 nm. The He–Ne laser (Fig. 14.33) is currently the most popular device of its kind, most often providing a few milliwatts of continuous power in the visible (632.8 nm). Its appeal arises primarily because it's easy to construct, relatively inex-

* His initial paper, which would have made his findings known in a more traditional fashion, was rejected for publication by the editors of *Physical Review Letters*—this to their everlasting chagrin.

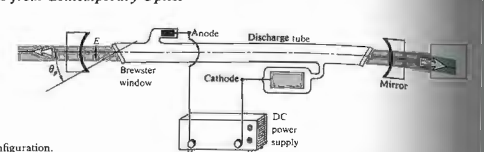


Figure 14.33 A simple, early He–Ne laser configuration.

pensive, and fairly reliable and in most cases can be operated by a flick of a single switch. Pumping is usually accomplished by electrical discharge (via either dc, ac, or electrodeless rf excitation). Free electrons and ions are accelerated by an applied field and, as a result of collisions, cause further ionization and excitation of the gaseous medium (typically a mixture of about 0.8 torr of He and about 0.1 torr of Ne). Many helium atoms, after dropping down from several upper levels, accumulate in the long-lived 2^1S- and 2^3S-states. These are metastable states (Fig. 14.34) from which there [illegible] no allowed radiative transitions. The excited He atoms inelastically collide with and transfer energy to [illegible] state Ne atoms, raising them in turn to the [illegible] 4s-states. These are the upper laser levels, and there then exists a population inversion with respect to the lower 4p- and 3p-states. Transitions between the [illegible] and 4s-states are forbidden. Spontaneous photons [illegible] ate stimulated emission, and the chain reaction be[illegible]. The dominant laser transitions correspond [illegible] 1152.3 nm and 3391.2 nm in the infrared and [illegible] course, the ever-popular 632.8 nm in the visible (b[illegible] red). The p-states drain off into the 3s-state, thus the[illegible] selves remaining uncrowded and thereby continuously sustaining the inversion. The 3s-level is metastable [illegible] that 3s-atoms return to the ground state after losing energy to the walls of the enclosure. This is why [illegible] plasma tube's diameter inversely affects the gain and [illegible] accordingly, a significant design parameter. In contr[illegible] to the ruby, where the laser transition is down to the ground state, stimulated emission in the He–Ne laser occurs between two upper levels. The significance of this, for example, is that since the 3p-state is ordinarily only sparsely occupied, a population inversion is very easily obtained, and this without having to half empty the ground state.

Return to Fig. 14.33, which pictures the relevant features of a basic early He–Ne laser. The mirrors are coated with a multilayered dielectric film having a reflectance of over 99%. The laser output is made linearly polarized by the inclusion of Brewster end windows (i.e., plates tilted at the polarization angle) terminating the discharge tube. If these end faces [illegible] instead normal to the axis, reflection losses (4% at [illegible] interface) would become unbearable. By tilting them to the polarization angle, the windows presumably have 100% transmission for light whose electic field component is parallel to the plane of incidence (the plane of the drawing). This polarization state rapidly becomes dominant, since the normal component is partially reflected off-axis at each transit of the windows. Linearly polarized light in the plane of incidence soon becomes the preponderant stimulating mechanism in the cavity, to the ultimate exclusion of the orthogonal polarization.*

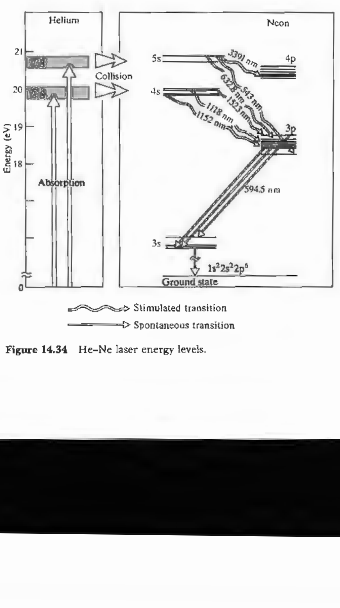


Figure 14.34 He–Ne laser energy levels.

Epoxying the windows to the ends of the laser tube and mounting the mirrors externally was a typical though dreadful approach used commercially until the mid-1970s. Inevitably, the epoxy leaked, allowing water vapor in and helium out. Today, such lasers are *hard sealed;* the glass is bonded directly to metal (Kovar) mounts, which support the mirrors within the tube. The mirrors (one of which is generally ≈100% reflective) have modern resistive coatings so they can tolerate the discharge environment within the tube. Operating lifetimes of 20,000 hours and more are now the rule (up from only a few hundred hours in the 1960s). Brewster windows are usually optional, and most commercial He–Ne lasers generate more or less "unpolarized" beams. The typical mass-produced He–Ne laser (with an output of from 0.5 mW to 5 mW) operates in the TEM_{00} mode, has a coherence length of around 25 cm, a beam diameter of approximately 1 mm, and a low overall efficiency of only 0.01% to about 0.1%. Though there are infrared He-Ne lasers, and even a new green (543.5 nm) He–Ne laser, the bright red 632.8-nm version remains the most popular.

A Survey of Laser Developments

Laser technology is so dynamic a field that what was a laboratory breakthrough a year of two ago may be a commonplace off-the-shelf item today. The whirlwind will certainly not pause to allow descriptive terms like "the smallest," "the largest," "the most powerful," and so on to be applicable for very long. With this in mind, we briefly survey the existing scene without trying to anticipate the wonders that will surely come after this type is set. Laserbeams have already been bounced off the Moon; they have spot welded detached retinas, generated fusion neutrons, stimulated seed growth, served as communications links, guided milling machines, missiles, ships, and grating engines, carried color television pictures, drilled holes in diamonds, levitated tiny objects,* and intrigued countless amongst the curious.

Along with ruby there are a great many other **solid-state lasers** whose outputs range in wavelength from roughly 170 nm to 3900 nm. For example, the trivalent rare earths Nd^{3+}, Ho^{3+}, Gd^{3+}, Tm^{3+}, Er^{3+}, Pr^{3+}, and Eu^{3+} undergo laser action in a host of hosts, such as $CaWO_4$, Y_2O_3, $SrMoO_4$, LaF_3, yttrium aluminum garnet (YAG for short), and glass, to name only a few. Of these, neodymium-doped glass and neodymium-doped YAG are of particular importance. Both constitute high-powered laser media operating at approximately 1060 nm. Nd: YAG lasers generating in excess of a kilowatt of continuous power have been constructed. Tremendous power outputs in pulsed systems have been obtained by operating several lasers in tandem. The first laser in the train serves as a Q-switched oscillator that fires into the next stage, which functions as an amplifier; and there may be one or more such amplifiers in the system. By reducing the feedback of the cavity, a laser will no longer be self-oscillatory, but it will amplify an incident wave that has triggered stimulated emission. Thus the amplifier is, in effect, an active medium, which is pumped, but for which the end faces are only partially reflecting or even nonreflecting. Ruby systems of this kind, delivering a few GW (gigawatts, i.e., 10^9 W) in the form of pulses lasting several nanoseconds, are available commercially. On December 19, 1984, the largest laser in existence, the Nova, fired all 10 of its beams at once for the first time, producing a warm-up shot of a mere 18 kJ of 350-nm radiation in

* Half of the output power of the laser is *not* lost in reflections at the Brewster windows when the transverse $\mathcal{P}$-state light is scattered. Energy simply isn't continuously channeled into that polarization component by the cavity. If it's reflected out of the plasma tube, it's not present to stimulate further emission.

* See M. Lubin and A. Fraas, "Fusion by Laser," *Sci. Am.* **224**, 21 (June 1971); R. S. Craxton, R. L. McCrory, and J. M. Soures, "Progress in Laser Fusion," *Sci. Am.* **255**, 69 (August 1986); and A. Ashkin, "The Pressure of Laser Light," *Sci. Am.* **226**, 63 (February 1972).

Figure 14.35 Nova, the world's most powerful laser. (Photo courtesy Lawrence Livermore National Laboratory.)

a 1-ns pulse (Fig. 14.35). When fully operational this immense neodymium-doped glass laser will focus up to 100 TW of green (530 nm) or blue (350 nm) light onto a fusion pellet—that's roughly 500 times more power than all the electrical generating stations in the United States—albeit only for about 10^{-9} s.

A large group of **gas lasers** operate across the spectrum from the far IR to the UV (1 mm to 150 nm). Primary amongst these are helium–neon, argon, and krypton, as well as several molecular gas systems, such as carbon dioxide, hydrogen fluoride, and molecular nitrogen (N_2). Argon lases mainly in the green, blue-green, and violet (predominantly at 488.0 and 514.5 nm) in either pulsed or continuous operation. Although its output is usually several watts c-w, it has gone as high as 150 W c-w. The argon ion laser is similar in some respects to the He–Ne laser, although it evidently differs in its usually greater power, shorter wavelength, broader linewidth, and higher price. All of the noble gases (He, Ne, A, Kr, Xe) have been made to lase individually, as have the gaseous ions of many other elements, but the former grouping has been studied most extensively.

The CO_2 molecule, which lases between vibrational modes, emits in the IR at 10.6 μm, with typical c-w power levels of from watts to several kilowatts. Its efficiency can be an unusually high 15% when aided [illegible] additions of N_2 and He. While it once took a disch[illegible] tube nearly 200 m long to generate 10 kW c-w, consi[illegible]ably smaller "table models" are now available com[illegible]cially. For a while in the 1970s, the record o[illegible] belonged to an experimental gas-dynamic laser [illegible] thermal pumping on a mixture of CO_2, N_2, and [illegible] to generate 60 kW c-w at 10.6 μm in mul[illegible]ode operation.

The pulsed nitrogen laser operates at 337.1 [illegible] the UV, as does the c-w helium–cadmium laser. A [illegible]ber of metal vapors (e.g., Zn, Hg, Sn, Pb) have di[illegible] laser transitions in the visible, but problems [illegible] maintaining uniformity of the vapor in the discharge region have handicapped their exploitation. The He-Cd laser emits at 325.0 nm and 441.6 nm. These are transitions of the cadmium ion arising after excitation resulting from collisions with metastable helium atoms.

The **semiconductor laser**—alternatively known [illegible] junction or diode laser—was invented in 1962, [illegible] after the development of the light-emitting diode (LED). Today it serves a central role in electro-opti[illegible] primarily because of its spectral purity, high efficien[illegible] (≈100%), ruggedness, ability to be modulated [illegible] extremely rapid rates, long lifetimes, and mode[illegible] power (as much as 200 mW) despite its pinhead size. Junction lasers have already been used in the millions in fiberoptic communications, laser disk audio sy[illegible] and so forth.

The first such lasers were made of one material, gallium arsenide, appropriately doped to form [illegible] junction. The associated high lasing threshold o[illegible] so-called homostructures limited them to pulsed operation and cryogenic temperatures; other[illegible] heat developed in their small structures would [illegible] them. The first tunable lead–salt diode laser was developed in 1964, but it was not until almost [illegible] dozen years later that it became commercially ava[illegible] operates at liquid nitrogen temperatures, whic[illegible] tainly inconvenient, but it can scan from 2 μm [illegible]

Later advances have since allowed a reductio[illegible] [illegible]reshold and resulted in the advent of the continuous-[illegible]ve (c-w), room temperature diode laser. Transitions [illegible]cur between the conduction and valence bands, and stimulated emission results in the immediate vicinity of the p–n junction (Fig. 14.36). Quite generally, as a [illegible]rrent flows in the forward direction through a semi-[illegible]ductor diode, electrons from the n-layer conduction [illegible]d will recombine with p-layer holes, thereupon emit-[illegible]ng energy in the form of photons. This radiative process, which competes for energy with the existing [illegible]sorption mechanisms (such as phonon production) [illegible]mes to predominate when the recombination layer is [illegible]all and the current is large. To make the system lase, the light emitted from the diode is retained within a resonant cavity, and that's usually accomplished by simply polishing the end faces perpendicular to the junction channel.

Nowadays semiconductor lasers are created to meet specific needs, and there are many designs producing wavelengths ranging from around 700 nm to about 30 μm. The early 1970s saw the introduction of the c-w GaAs/GaAlAs laser. Operating at room temperature in the 750-nm to 900-nm region (depending on the relative amounts of aluminum and gallium), the tiny diode chip is usually about a sixteenth of a cubic centimeter in volume. Figure 14.36(b) shows a typical heterostructure (a device formed of different materials) diode laser of this kind. Here the beam emerges in two directions from the 0.2-μm–thick active layer of GaAs. These little lasers usually produce upward of 20 mW of continuous wave power. To take advantage of the low loss region (λ ≈ 1.3 μm) in fiberoptic glass (p. 170) the GaInAsP/InP laser was devised in the mid-1970s with an output of 1.2 μm to 1.6 μm. The cleaved–coupled-cavity laser is a still more recent (1983) development (Fig. 14.37). In it the number of axial modes is controlled in order to produce very-narrow-bandwidth tunable radiation. Two cavities coupled together across a small gap restrict the radiation to the extremely narrow bandwidth that can be sustained in both resonant chambers.*

* [illegible]Y. Suematsu, "Advances in Semiconductor Lasers," *Phys. Today* [illegible]ay 1985). For a discussion of heterostructure diode lasers refer [illegible]B. Panish and I. Hayashi, "A New Class of Diode Lasers," *Sci.* [illegible] 225, 32 (July 1971).

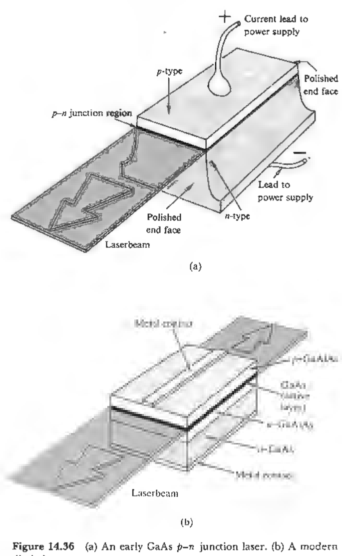


Figure 14.36 (a) An early GaAs p–n junction laser. (b) A modern diode laser.

The first **liquid laser** was operated in January of 1963.* All of the early devices of this sort were exclusively *chelates* (i.e., metallo-organic compounds formed of a metal ion with organic radicals). That original liquid laser contained an alcohol solution of europium benzoylacetonate emitting at 613.1 nm. The discovery of laser action in nonchelate organic liquids was made

* See Adam Heller, "Laser Action in Liquids," *Phys. Today* (November 1967), p. 35, for a more detailed account.

in 1966. It came with the fortuitous lasing (at 755.5 nm) of a chloroaluminum phthalocyanine solution during a search for stimulated Raman emission in that substance.* A great many fluorescent dye solutions of such families as the fluoresceins, coumarins, and rhodamines have since been made to lase at frequencies from the IR into the UV. These have usually been pulsed, although c-w operation has been obtained. There are so many organic dyes that it would seem possible to build such a laser at any frequency in the visible. Moreover, these devices are distinctive in that they inherently can be tuned continuously over a range of wavelengths (of perhaps 70 nm or so, although a pulsed system tunable over 170 nm exists). Indeed, there are other arrangements that will vary the frequency of a primary laserbeam (i.e., the beam enters with one color and emerges with another, Section 14.4), but in the case of the dye laser, the primary beam itself is tuned internally. This is accomplished, for example, by changing the concentration or the length of the dye cell or by adjusting a diffraction grating reflector at the end of the cavity. Several multicolor dye laser systems, which can easily be switched from one dye to another and thereby operate over a very broad frequency range, are available commercially.

A **chemical laser** is one that is pumped with energy released via a chemical reaction. The first of this kind was operated in 1964, but it was not until 1969 that a continuous-wave chemical laser was developed. One of the most promising of these is the deuterium fluoride–carbon dioxide (DF–CO_2) laser. It is self-sustaining, in that it requires no external power source. In brief, the reaction $F_2 + D_2 \rightarrow 2DF$, which occurs on the mixing of these two fairly common gases, generates enough energy to pump a CO_2 laser.

There are solid-state, gaseous, liquid, and vapor (e.g., H_2O) lasers; there are semiconductor lasers, free electron (600 nm to 3 mm) lasers, x-ray lasers, and lasers with very special properties, such as those that generate extremely short pulses, or those that have extraordinary frequency stability. These latter devices are very useful in the field of high-resolution spectroscopy, but there is a growing need for them in other research areas as well (e.g., in the interferometers used to attempt to detect gravity waves). In any event, these lasers must have precisely controlled cavity configurations despite the disturbing influences of temperature variations, vibrations, and even sound waves. To date the record is held by a laser at the Joint Institute for Laboratory Astrophysics in Boulder, Colorado, which maintains a frequency stability (p. 265) of nearly one part in

* P. Sorokin, "Organic Lasers," *Sci. Amer.* **220**, 30 (February 1969).

Figure 14.37 The cleaved–coupled-cavity laser. (Photos ... Bell Laboratories.)

14.2.2 The Light Fantastic

Laserbeams differ somewhat in nature from one type of laser to another; yet there are several remarkable features that are displayed, to varying degrees, by all such radiation. Quite apparent is the fact that most laser-beams are exceedingly directional, or if you will, highly collimated. One need only blow some smoke into an otherwise invisible, visible-laserbeam to see (via scattering) a fantastic thread of light stretched across a room. A He–Ne beam in the TEM_{00} mode generally has a divergence of only about one minute of arc or less. Recall that in that mode the emission closely approximates a Gaussian irradiance distribution; that is, the flux density drops off from a maximum at the central axis of the beam and has no side lobes. The typical laserbeam is quite narrow, usually issuing at no more than a few millimeters in diameter. Since the beam resembles a truncated plane wave, it is of course *spatially coherent*. In fact, its directionality may be thought of as a manifestation of that coherence. Laserlight is quasimonochromatic, generally having an exceedingly narrow frequency bandwidth (see Section 7.10). In other words, it is *temporally coherent*.

Another attribute is the high flux or *radiant power* that can be delivered in that narrow frequency band. As we've seen, the laser is distinctive in that it emits all its energy in the form of a narrow beam. In contrast, a 100-W incandescent light bulb may pour out considerably more radiant energy in toto than a low-power c-w laser, but the emission is incoherent, spread over a large solid angle, and it has a broad bandwidth as well. A good lens* can totally intercept a laserbeam and focus essentially all of its energy into a minute spot (whose diameter varies directly with λ and the focal length and inversely with the beam diameter). Spot diameters of a few thousandths of an inch can readily be attained with lenses that have a conveniently short focal length. And a spot diameter of a few hundred-millionths of an inch is possible in principle. Thus flux densities can readily be generated in a focused laserbeam of over 10^{17} W/cm^2, in contrast to, say, an oxyacetylene flame having roughly 10^3 W/cm^2. To get a better feel for these power levels, note that a focused CO_2 laserbeam of a few kilowatts c-w can burn a hole through a quarter-inch stainless steel plate in about 10 seconds. By comparison, a pinhole and filter positioned in front of an ordinary source will certainly produce spatially and temporally coherent light, but only at a minute fraction of the total power output.

* Spherical aberration is usually the main problem, since laserbeams are, as a rule, both quasimonochromatic and incident along the axis of the lens.

Femtosecond Optical Pulses

The advent of the mode-locked dye laser in the early part of the 1970s gave a great boost to the efforts then being made at generating extremely short pulses of light.* Indeed, by 1974 subpicosecond (1 ps = 10^{-12} s) optical pulses were already being produced, although the remainder of the decade saw little significant progress. In 1981 two separate advances resulted in the creation of femtosecond laser pulses (i.e., <0.1 ps or <100 fs)—a group at Bell Labs developed a colliding-pulse ring dye laser, and a team at IBM devised a new pulse-compression scheme. Above and beyond the implications in the practical domain of electro-optical communications, these accomplishments have firmly established a new field of research known as *ultrafast phenomena*. The most effective way to study the progression of a process that occurs exceedingly rapidly (e.g., carrier dynamics in semiconductors, fluorescence, photochemical biological processes, and molecular configuration changes) is to examine it on a time scale that is comparatively short with respect to what's happening. Pulses lasting ≈10 fs allow an entirely new access into previously obscure areas in the study of matter.

At the moment, the shortest pulses on record each lasted a mere 8 fs (10^{-15} s), which corresponds to wavetrains only about 4 wavelengths of red light in length. One of the new techniques that makes these femtosecond wavegroups possible is based on an idea used in radar work in the 1950s called *pulse compression*. Here an initial laser pulse has its frequency spectrum

* Take a look at "Ultrafast laser pulses" by A. De Maria, W. Glenn and M. Mack, *Phys. Today* (July 1971), p. 19.

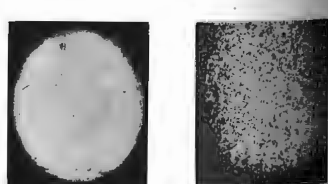
broadened, thereby allowing the inverse or temporal pulse width to be shortened—remember that $\Delta\nu$ and Δt are conjugate Fourier quantities (Eq. 7.63). The input pulse (several picoseconds long) is passed into a nonlinear dispersive medium, namely, a single-mode optical fiber. When the light intensity is high enough the index of refraction has an appreciable nonlinear term (Section 14.4), and the carrier frequency of the pulse experiences a time-dependent shift. On traversing perhaps 30 m of fiber, the frequency of the pulse is drawn out or "chirped." That is, a spread occurs in the spectrum of the pulse, with the low frequencies leading and the high frequencies trailing. Next the spectrally broadened pulse is passed through another dispersive system (a delay line), such as a pair of diffraction gratings. By traveling different paths, the blue-shifted trailing edge of the pulse is made to catch up to the red-shifted leading edge, creating a time-compressed output pulse.

The Speckle Effect

A rather striking and easily observable manifestation of the spatial coherence of laserlight is its granular appearance on reflection from a diffuse surface. Using a He–Ne laser (632.8 nm), expand the beam a bit by passing it through a simple lens and project it onto a wall or a piece of paper. The illuminated disk appears speckled with bright and dark regions that sparkle and shimmer in a dazzling psychedelic dance. Squint and the grains grow in size; step toward the screen and they shrink; take off your eyeglasses and the pattern stays in perfect focus. In fact, if you are nearsighted, the diffraction fringes caused by dust on the lens blur out and disappear, but the speckles do not. Hold a pencil at varying distances from your eye so that the disk appears just above it. At each position, focus on the pencil; wherever you focus, the granular display is crystal clear. Indeed, look at the pattern through a telescope; as you adjust the scope from one extreme to the other, the ubiquitous granules remain perfectly distinct, even though the wall is completely blurred.

The spatially coherent light scattered from a diffuse surface fills the surrounding region with a *stationary* interference pattern (just as in the case of the wavefront-splitting arrangements of Section 9.3). At the suface the granules are exceedingly small, and they increa[illegible] size with distance. At any location in space the re[illegible] field is the superposition of many contributing [illegible] wavelets. These must have a constant relativ[illegible] determined by the optical path length from [illegible] terer to the point in question, if the interference [illegible] is to be sustained. Figure 14.38 illustrates [illegible] rather nicely. It shows a cement block illuminated [illegible] one case by laserlight and in the other by collima[illegible] light from a Hg arc lamp, both of about the same [illegible] coherence. Yet while the laser's coherence length [illegible] much greater than the height of the surface featur[illegible] the coherence length of the Hg light is not. In [illegible] former case, the speckles in the photograph are [illegible] and they obscure the surface structure; in the [illegible] despite its spatial coherence, the speckle pattern is [illegible] observable in the photograph, and the surface featu[illegible] predominate. Because of the rough texture the [illegible] path-length difference between two wavelets arriv[illegible] a point in space, scattered from different surface [illegible] is generally greater than the coherence length [illegible] mercury light. This means that the relative [illegible] the overlapping wavetrains change rapidly and [illegible] domly in time, washing out the large-scale interfe[illegible] pattern.

A real system of fringes is formed of the scattered waves that converge in front of the screen. The fring[illegible]



(a) (b)

Figure 14.38 Speckle patterns. (a) A cement block [illegible] ated by a mercury arc and (b) a He–Ne laser. [From B. J. [illegible] n, *J. Soc. Phot. Inst. Engr.* **4**, 7 (1965).]

can be viewed by intersecting the interference pattern with a sheet of paper at a convenient location. After forming the real image in space, the rays proceed to diverge, and any region of the image can therefore be viewed directly with the eye appropriately focused. In contrast, rays that initially diverge appear to the eye as if they had originated behind the scattering screen and thus form a virtual image.

[illegible] seems that as a result of chromatic aberration, normal and farsighted eyes tend to focus red light behind the screen. Contrarily, a nearsighted person observes the real field in front of the screen (regardless of wavelength). Thus if the viewer moves her head to the right, the pattern will move to the right in the first instance (where the focus is beyond the screen) and to the left in the second (focus in front). The pattern will follow the motion of your head, if you're viewing a very close to the surface. The same apparent parallax motion can be seen by looking through a window; outside objects will seem to move with your head, inside ones opposite to it. The brilliant, narrow-bandwidth, spatially coherent laserbeam is ideally suited for observing the granular effect, although other means are certainly possible.* In unfiltered sunlight the grains are minute, on the surface, and multicolored. The effect is easy to observe on a smooth, flat-black material (e.g., poster-painted paper), but you can see it on a fingernail or a worn coin as well.

Although it provides a marvelous demonstration, both aesthetically and pedagogically, the granular effect can be a real practical nuisance in coherently illuminated systems. For example, in holographic imagery the [illegible]eckle pattern corresponds to troublesome back[illegible] [illegible]ound noise. Incidentally, very much the same kind [illegible] thing is observable when listening to a mobile radio [illegible]here the signal strength ffuctuates from one location [illegible] the next, depending on the environment and the [illegible]ulting interference pattern.

[illegible] further reading on this effect, see L. I. Goldfischer, *J. Opt. Soc.* [illegible] 55, 247 (1965); D. C. Sinclair, *J. Opt. Soc. Am.* **55**, 575 (1965); [illegible] Rigden and E. I. Gordon, *Proc. IRE* **50**, 2367 (1962); B. M. [illegible]r, *Proc. IEEE* **51**, 220 (1963).

14.3 HOLOGRAPHY

The technology of photography has been with us for a long time, and we've all grown accustomed to seeing the three-dimensional world compressed into the flatness of a scrapbook page. The depthless television pitchman who smiles out of a myriad of phosphorescent flashes, although inescapably there, seems no more palpable than a postcard image of the Eiffel Tower. Both share the severe limitation of being simply irradiance mappings. In other words, when the image of a scene is ordinarily reproduced, by whatever traditional means, what we ultimately see is not an accurate reproduction of the light field that once inundated the object, but rather a point-by-point record of just the square of the field's amplitude. The light reflecting off a photograph carries with it information about the irradiance but nothing about the phase of the wave that once emanated from the object. Indeed, if both the amplitude and phase of the original wave could be reconstructed somehow, the resulting light field (assuming the frequencies are the same) would be indistinguishable from the original. This means that you would then see (and could photograph) the re-formed image in perfect three-dimensionality, exactly as if the object were there before you, actually generating the wave.

14.3.1 Methods

Dennis Gabor had been thinking along these lines for a number of years prior to 1947, when he began conducting his now famous experiments in holography at the Research Laboratory of the British Thomson–Houston Company. His original setup, depicted in Fig. 14.39, was a two-step lensless imaging process in which he first photographically recorded an interference pattern, generated by the interaction of scattered quasi-monochromatic light from an object and a coherent reference wave. The resulting pattern was something he called a **hologram**, after the Greek word *holos*, meaning whole. The second step in the procedure was the *reconstruction* of the optical field or image, and this was done through the diffraction of a coherent beam by a

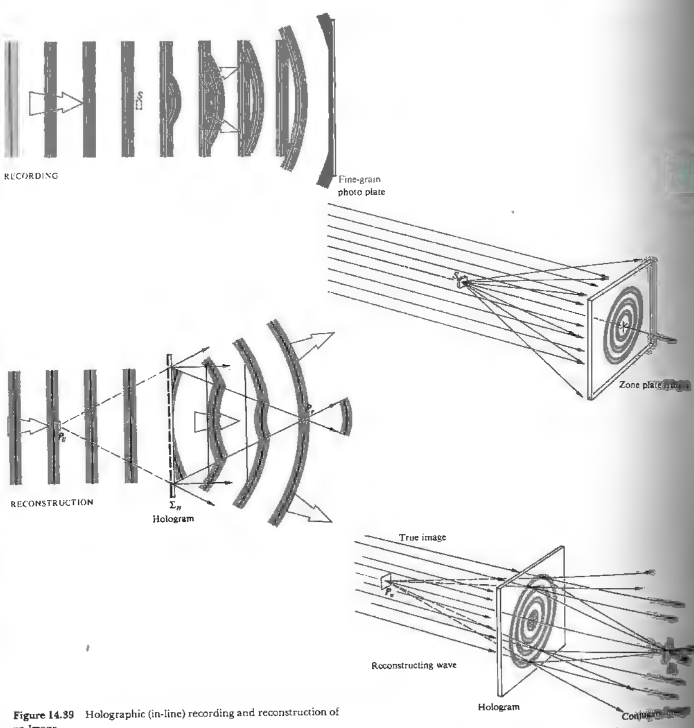


Figure 14.39 Holographic (in-line) recording and reconstruction of an image.

transparency, which was the developed hologram. In a way quite reminiscent of Zernike's phase-contrast technique (Section 14.1.4), the hologram was formed when the unscattered *background* or *reference wave* interfered with the diffracted wave from the small semitransparent object, S—which was, in those early days, often a piece of microfilm. The key point is that the interference pattern or hologram contains, by way of the fringe configuration, information corresponding to both the amplitude and phase of the wave scattered by the object.

Admittedly, it's not at all obvious that by now shining a plane wave through the processed hologram one could reconstruct an image of the original object. Suffice it to say for the moment that if the object were very small, the scattered wave would be nearly spherical, and the interference pattern a series of concentric rings (centered about an axis through the object and normal to the plane wave). Except for the fact that the circular fringes would vary gradually in irradiance from one to the next, the resulting flux-density distribution would correspond to a conventional Fresnel zone plate (Section 10.3.5). Recall that a zone plate functions somewhat like a lens in that it diffracts collimated light into a beam converging to a real focal point, P_r. In addition, it produces a diverging wave, which appears to come from the point P_r and constitutes a virtual image. Thus we can imagine, albeit rather simplistically, that each point on an extended object generates its own zone plate displaced from the others and that the ensemble of all such partially overlapping zone plates forms the hologram.* During the reconstruction step, each constituent zone plate forms both a real and virtual image of a single object point, and in this way, point by point, the hologram regenerates the original light field. When the reconstructing beam has the same wavelength as the initail recording beam (which need not necessarily be the case, and quite often isn't), the virtual image is undistorted and appears at the location formerly occupied by the object. Thus it is the virtual image field that actually corresponds to the original object field. As such, the virtual image is sometimes spoken of as the *true image*, while the other is the real or, perhaps more fittingly, the *conjugate image*. In any event, we envision the hologram as a composite of interference patterns, and at least for this very simple configuration, those patterns resemble zone plates. As we will see presently, the sinusoidal grating is an equally fundamental fringe system making up complex holograms.

Gabor's research, which won him the 1971 Nobel Prize in Physics, had as its motivation an improvement in electron microscopy. His work initially generated some interest, but all in all it remained in a state of quasi-unnoticed oblivion for about 15 years. In the early 1960s there was a resurgence of interest in Gabor's **wavefront reconstruction** process and, in particular, in its relation to certain radar problems. Soon, aided by an abundance of the new coherent laserlight and extended by a number of technological advances, holography became a subject of widespread research and tremendous promise. This rebirth had its origin in the Radar Laboratory of the University of Michigan, with the work of Emmett N. Leith and Juris Upatnieks. Among other things, they introduced an improved arrangement for generating holograms, which is illustrated in Fig. 14.40. Unlike Gabor's *in line*-configuration, where the conjugate image was inconveniently located in front of the true image, the two were now satisfactorily separated off-axis, as shown in the diagram. Once again, the hologram is an interference pattern arising from a coherent reference wave and a wave scattered from the object (this type is sometimes referred to as a **side-band Fresnel hologram).** Figure 14.41 shows the equivalent arrangement for producing side-band Fresnel holograms from transparent objects.

What's happening here can be appreciated in two ways—an essentially pictorial, Fourier-optical way and, alternatively, a direct mathematical way. We will look from both perspectives, because they complement each other. First, this is at heart an interference (or, if you like, a diffraction) problem, and we can again return to the notion of the complicated object wavefront being composed of Fourier-component plane waves (Fig. 10.10) traveling in directions associated with the different spatial frequencies of the object's light field, reflected or transmitted. Each one of these Fourier plane waves interferes with the reference wave on the photographic plate and thus preserves the information

* See M. P. Givens, "Introduction to Holography," *Am. J. Phys.* **35**, 1056 (1967).

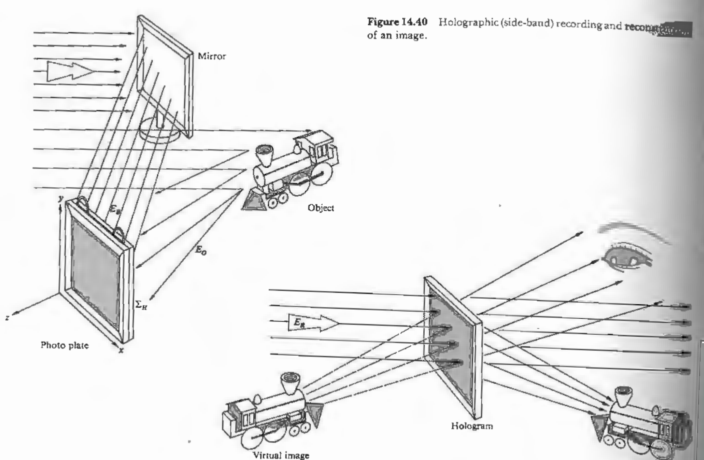


Figure 14.40 Holographic (side-band) recording and [illegible] of an image.

associated with that particular spatial frequency in the form of a characteristic fringe pattern.

To see how this occurs examine the simplified two-wave version depicted in Fig. 14.42. At the moment shown the reference wave happens to have a crest along the face of the film plane, and the scattered object wavelet, coming in at an angle θ, similarly has crests at points A, B, and C. These correspond to points where interference maxima will occur at the moment shown. But as both waves progress to the right, they will remain in phase at these points, trough will overlap trough, and the maxima will remain fixed at A, B, and C. Similarly, between these points, trough overlaps crest, and minima exist. The relative phase (ϕ) of these two waves, which varies from point to point along the film, can be written as a function of x. Since ϕ changes [illegible] 2π as x goes the length of $\overline{AB}$, $\phi/2\pi = x/\overline{AB}$. No[illegible] that $\sin\theta = \lambda/\overline{AB}$, and so getting rid of the specific length $\overline{AB}$, the phase in general becomes

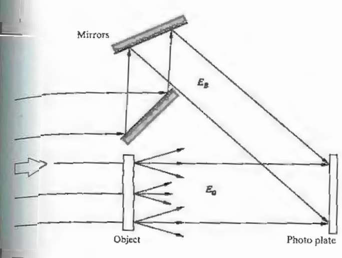
$$\phi(x) = (2\pi x \sin\theta)/\lambda. \tag{14.9}$$

If the two waves are assumed to have the same [illegible] E_0, the resultant field follows from Eq. (7.1[illegible]

$$E = 2E_0 \cos \tfrac{1}{2}\phi \sin(\omega t - kx - \tfrac{1}{2}\phi),$$

and the irradiance distribution, which is proport[illegible] to the field amplitude squared, by way of Eq. ([illegible] has the form

$$I(x) = \tfrac{1}{2}c\epsilon_0(2E_0\cos\tfrac{1}{2}\phi)^2 = 2c\epsilon_0 E_0^2 \cos^2 [illegible]$$



[illegible]ure 14.41 A side-band Fresnel holographic setup for a trans[illegible]rent object.

[illegible]

$$I(x) = 2c\epsilon_0 E_0^2 + 2c\epsilon_0 E_0^2 \cos\phi. \tag{14.10}$$

What we have is a cosinusoidal irradiance distribution across the film plane with a spatial period of $\overline{AB}$ and a spatial frequency ($1/\overline{AB}$) of $\sin\theta/\lambda$.

Upon processing the film so that the amplitude transmission profile corresponds to $I(x)$, the result is a cosinusoidal grating. When this simple hologram (which essentially corresponds to a structureless object with no information) is illuminated by a plane wave identical to the original reference wave [Fig. 14.42(c)] three beams will emerge: one zeroth and two first order. One of these first-order beams will travel in the direction of the original object beam and corresponds to its reconstructed wavefront.

Now suppose we go one step beyond this most basic hologram and examine an object that has some optical structure. Accordingly, let's use as the object a transparency with a simple periodic structure that has a single spatial frequency—a cosine grating. A slightly idealized representation (which leaves out the weak higher-order [illegible]ms due to the finite size of the beam and grating) is depicted in Fig. 14.43, which shows the illuminated [illegible], the three transmitted beams, and the reference [illegible]. What results is three slightly different versions

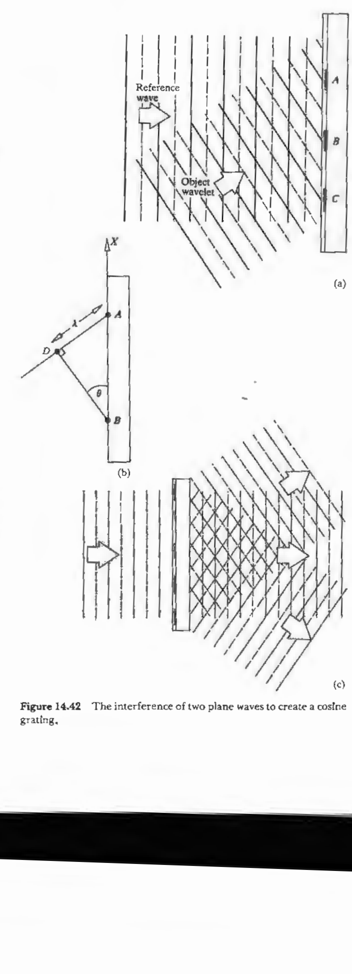


Figure 14.42 The interference of two plane waves to create a cosine grating.

of Fig. 14.42, where each of the three transmitted waves makes a slightly different angle (θ) with the reference wave. Consequently, each of the three overlap areas will correspond to a set of cosine fringes of a slightly different spatial frequency, from Eq. (14.9). Again when we play back the resulting hologram, Fig. 14.43(b), we have three pieces of business: the undiffracted wave, the virtual image, and the real image. Observe that it is only where the three beams come together to contribute their spatial frequency content that images of the original grating are formed.

When a still more complex object is used we can anticipate that the relative phase between the object and reference waves (ϕ) will vary from point to point in a complicated way, thereby modulating the basic carrier signal (Fig. 14.44) produced by two plane waves when no object is present. In other words, we can generalize from Fig. 14.43 and conclude that the phase angle difference ϕ (which varies with θ) is encoded in the configuration of the fringes. Furthermore, had the amplitudes of the reference and object waves been different, the irradiance of those fringes would have been altered accordingly. Thus we can guess that the amplitude of the object wave at every point on the film plane will be encoded in the visibility of the resulting fringes.

The process depicted in Fig. 14.40 can be treated analytically as follows. Suppose that the xy-plane is the plane of the hologram, Σ_H. Then

$$E_B(x, y) = E_{0B} \cos[2\pi ft + \phi(x, y)] \qquad (14.11)$$

describes the planar background or reference wave at Σ_H, overlooking considerations of polarization. Its amplitude, E_{0B}, is constant, while the phase is a function of position. This just means that the reference wavefront is tilted in some known manner with respect to Σ_H. For example, if the wave were oriented such that it could be brought into coincidence with Σ_H by a single rotation through an angle of θ about y, the phase at any point on the hologram plane would depend on its value of x. Thus ϕ would again have the form

$$\phi = \frac{2\pi}{\lambda} x \sin\theta = kx \sin\theta,$$

being, in that particular case, independent of y and

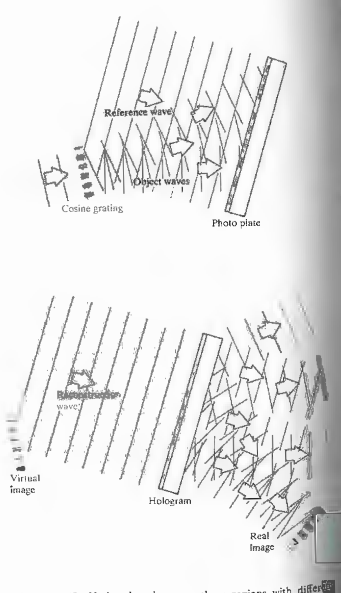


Figure 14.43 Notice that there are three regions with different spatial frequencies. Each of these on the re-illuminate hologram generates three waves.

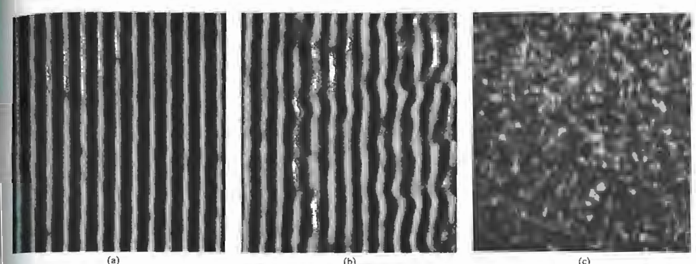


Figure 14.44 Various degrees of modulation of hologram fringes. (Photo courtesy Emmett N. Leith and *Scientific American*.)

varying linearly with x. For the sake of simplicity, we'll just write it, quite generally, as $\phi(x, y)$ and keep in mind that it's a simple known function. The wave scattered from the object can, in turn, be expressed as

$$E_O(x, y) = E_{0O}(x, y) \cos[2\pi ft + \phi_O(x, y)], \qquad (14.12)$$

where both the amplitude and phase are now complicated functions of position corresponding to an irregular wavefront. From the communications-theoretic point of view, this is an amplitude- and phase-modulated carrier wave bearing all of the available information about the object. Note that this information is encoded in spatial rather than temporal variations of the wave. The two disturbances E_B and E_O superimpose and interfere to form an irradiance distribution, which is recorded by the photographic emulsion. The resulting irradiance, except for a multiplicative constant, is $I(x, y) = \langle (E_B + E_O)^2 \rangle$, which, from Section 9.1, is given by

$$I(x, y) = \frac{E_{0B}^2}{2} + \frac{E_{0O}^2}{2} + E_{0B}E_{0O} \cos(\phi - \phi_O). \qquad (14.13)$$

Observe once again that the phase of the object wave determines the location on Σ_H of the irradiance maxima and minima. Moreover, the contrast or fringe visibility

$$\mathcal{V} \equiv (I_{max} - I_{min})/(I_{max} + I_{min}) \qquad (12.1)$$

across the hologram plane, which is

$$\mathcal{V} = 2E_{0B}E_{0O}/(E_{0B}^2 + E_{0O}^2), \qquad (14.14)$$

contains the appropriate information about the object wave's amplitude.

Once more, in the parlance of communications theory, we might observe that the film plate serves as both the storage device and detector or mixer. It produces, over its surface, a distribution of opaque regions corresponding to a modulated spatial waveform. Accordingly, the third or difference frequency term in Eq. (14.13) is both amplitude and phase modulated by way of the position dependence of $E_{0O}(x, y)$ and $\phi_O(x, y)$.

Figure 14.44(b) is an enlarged view of a portion of the fringe pattern that constitutes the hologram for a simple, essentially two-dimensional, semitransparent object. Were the two interfering waves perfectly planar [as in Fig. 14.44(a)], the evident variations in fringe position and irradiance, which represent the information, would be absent, yielding the traditional Young's pattern (Section 9.3). The sinusoidal transmission-grating configuration [Fig. 14.44(a)] may be thought of as the carrier waveform, which is then modulated by the signal. Furthermore, we can imagine that the coherent superposition of countless zone-plate patterns, one arising from each point on a large object, have metamorphosed into the modulated fringes of Fig. 14.44(b). When the amount of modulation is further greatly increased, as it would be for a large, three-dimensional, diffusely reflecting object, the fringes lose the kind of symmetry still discernible in Fig. 14.44(b) and become considerably more complicated. Incidentally, holograms are often covered with extraneous swirls and concentric ring systems that arise from diffraction by dust and the like on the optical elements.

The amplitude transmission profile of the processed hologram can be made proportional to $I(x, y)$. In that case, the *final emerging wave*, $E_F(x, y)$, is proportional to the product $I(x, y)E_R(x, y)$, where $E_R(x, y)$ is the *reconstructing wave* incident on the hologram. Thus if the reconstructing wave, of frequency ν, is incident obliquely on Σ_H, as was the background wave, we can write

$$E_R(x, y) = E_{0R} \cos [2\pi\nu t + \phi(x, y)]. \qquad (14.15)$$

The final wave (except for a multiplicative constant) is the product of Eqs. (14.13) and (14.15):

$$\begin{aligned} E_F(x, y) = {} & \tfrac{1}{2}E_{0R}(E_{0B}^2 + E_{0O}^2) \cos [2\pi\nu t + \phi(x, y)] \\ & + \tfrac{1}{2}E_{0R}E_{0B}E_{0O} \cos (2\pi\nu t + 2\phi - \phi_O) \\ & + \tfrac{1}{2}E_{0R}E_{0B}E_{0O} \cos (2\pi\nu t + \phi_0). \qquad (14.16) \end{aligned}$$

Three terms describe the light issuing from the hologram; the first can be rewritten as

$$\tfrac{1}{2}(E_{0B}^2 + E_{0O}^2)E_R(x, y),$$

and is an amplitude-modulated version of the reconstructing wave. In effect, each portion of the hologram functions as a diffraction grating, and this is again the *zeroth-order*, undeflected, direct beam. Since it contains no information about the phase of the object wave, ϕ_O, it is of little concern here.

The next two or *side-band waves* are the sum and difference terms, respectively. These are the two *first-order waves* diffracted by the grating-like hologram. The first of these (i.e., the sum term) represents a wa[illegible] except for a multiplicative constant, has the same [illegible] tude as the object wave $E_{0O}(x, y)$. Moreover, its [illegible] contains a $2\phi(x, y)$ contribution, which, as you [illegible] arose from tilting the background and recon[illegible] wavefronts with respect to Σ_H. It's this phase fa[illegible] provides the angular separation between the real [illegible] virtual images. Furthermore, rather than contain[illegible] phase of the object wave, the sum term con[illegible] negative. Thus it's a wave carrying all of the app[illegible] information about the object but in a way that [illegible] quite right. Indeed, this is the real image fo[illegible] converging light in the space beyond the hologram, [illegible] is, between it and the viewer. The negative [illegible] manifest in an inside-out image something like [illegible] pseudoscopic effect occurring when the elements [illegible] a photographic stereo pair are interchanged. B[illegible] appear as indentations, and object points that we[illegible] front of and nearer to Σ_H are now imaged nearer to but beyond Σ_H. Thus a point on the original subj[illegible] closest to the observer appears farthest away in the re[illegible] image. The scene is turned in on itself along one axis in a way that perhaps must be seen to be appreciate[illegible] For example, imagine you are looking down the holo[illegible] graphic conjugate image of a bowling alley. The "bac[illegible] row of pins, even though partially obscured by the "front" rows, are nonetheless imaged closer to the viewer than is the one-pin. Despite this, bear in mind that it's not as if you were looking at the array from behind. No light from the very backs of the pins was ever recorded—you're seeing an inside-out fro[illegible] As a consequence, the conjugate image is [illegible] limited utility, although it can be made to have a[illegible] configuration by forming a second hologram [illegible] real image as the object.

The difference term in Eq. (14.16), except for [illegible] plicative constant, has precisely the form of [illegible] wave $E_{0O}(x, y)$. If you were to peer into (not at) [illegible] illuminated hologram, as if it were a window looki[illegible] out onto the scene beyond, you would "see" the obj[illegible] exactly as if it were truly sitting there. You could move your head a bit and look around an item in the foreground in order to see the view it had previously [illegible] obstructing. In other words, in addition to co[illegible] three-dimensionality, parallax effects are appare[illegible]

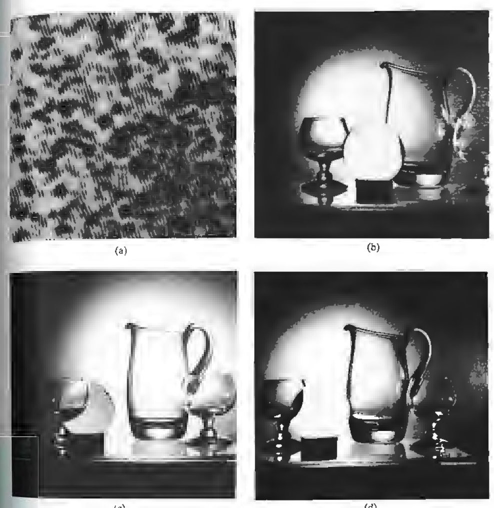


Figure 14.45 Parts (b) through (d) are three different views photographed from the same holographic image generated by the hologram in (a). (Photos from Smith, *Principles of Holography*.)

they are in no other reproducing technique (Fig. 14.45). [illegible]ine that you are viewing the holographic image of a [illegible]gnifying glass focused on a page of print. As you mo[illegible] your eye with respect to the hologram plane, the wo[illegible] being magnified by the lens (which is itself just an [illegible]age) actually change, just as they would in "real" [illegible] with a "real" lens and "real" print. In the case of [illegible]xtended scene having considerable depth, your eyes [illegible]ld have to refocus as you viewed different regions [illegible] various distances. In precisely the same way, a [illegible]mera lens would have to be readjusted if you were photographing different regions of the virtual image (Fig. 14.46).

There are other extremely important and interesting features that holograms display. For example, if you were standing close to a window, you could obscure all of it with, say, a piece of cardboard, except for a tiny area through which you could then peer and still see the objects beyond. The same is true of a hologram, since each small fragment of it contains information about the entire object, at least as seen from the same vantage point, and each fragment can repropattern (Section 9.3). The sinusoidal transmission-grating configuration [Fig. 14.44(a)] may be thought of as the carrier waveform, which is then modulated by the signal. Furthermore, we can imagine that the coherent superposition of countless zone-plate patterns, one arising from each point on a large object, have metamorphosed into the modulated fringes of Fig. 14.44(b). When the amount of modulation is further greatly increased, as it would be for a large, three-dimensional, diffusely reflecting object, the fringes lose the kind of symmetry still discernible in Fig. 14.44(b) and become considerably more complicated. Incidentally, holograms are often covered with extraneous swirls and concentric ring systems that arise from diffraction by dust and the like on the optical elements.

The amplitude transmission profile of the processed hologram can be made proportional to $I(x, y)$. In that case, the *final emerging wave*, $E_F(x, y)$, is proportional to the product $I(x, y)E_R(x, y)$, where $E_R(x, y)$ is the *reconstructing wave* incident on the hologram. Thus if the reconstructing wave, of frequency ν, is incident obliquely on Σ_H, as was the background wave, we can write

$$E_R(x, y) = E_{0R} \cos [2\pi\nu t + \phi(x, y)]. \qquad (14.15)$$

The final wave (except for a multiplicative constant) is the product of Eqs. (14.13) and (14.15):

$$E_F(x, y) = \tfrac{1}{2}E_{0R}(E_{0B}^2 + E_{0O}^2) \cos [2\pi\nu t + \phi(x, y)] + \tfrac{1}{2}E_{0R}E_{0B}E_{0O} \cos (2\pi\nu t + 2\phi - \phi_O) + \tfrac{1}{2}E_{0R}E_{0B}E_{0O} \cos (2\pi\nu t + \phi_0). \qquad (14.16)$$

Three terms describe the light issuing from the hologram; the first can be rewritten as

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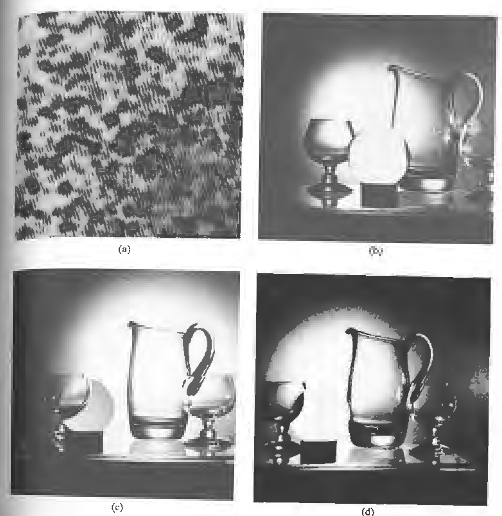


Figure 14.45 Parts (b) through (d) are three different views photographed from the same holographic image generated by the hologram in (a). (Photos from Smith, *Principles of Holography*.)

[illegible]y are in no other reproducing technique (Fig. 14.45). Imagine that you are viewing the holographic image of a magnifying glass focused on a page of print. As you move your eye with respect to the hologram plane, the words being magnified by the lens (which is itself just an image) actually change, just as they would in "real" life with a "real" lens and "real" print. In the case of an extended scene having considerable depth, your eyes would have to refocus as you viewed different regions [illegible] at various distances. In precisely the same way, a camera lens would have to be readjusted if you were photographing different regions of the virtual image (Fig. 14.46).

There are other extremely important and interesting features that holograms display. For example, if you were standing close to a window, you could obscure all of it with, say, a piece of cardboard, except for a tiny area through which you could then peer and still see the objects beyond. The same is true of a hologram, since each small fragment of it contains information about the entire object, at least as seen from the same vantage point, and each fragment can reproduce, albeit with diminishing resolution, the entire image.

Figure 14.47 summarizes pictorially much of what's been said so far while also providing a convenient setup for actually making and viewing a hologram. Here the photographic emulsion is shown having some depth, as compared with Fig. 14.42, where it was treated as though it were purely two-dimensional. Of course, any emulsion must certainly have a finite thickness. Typically it would be about 10 μm thick, as compared with the spatial period of the fringes, which might average around 1 μm or so. Figure 14.48(a) is closer to the point, showing the kind of three-dimensional fringes that actually exist throughout the emulsion. For plane waves these straight parallel fringe-planes are oriented so as to bisect the angle between the reference and object waves. Realize that all the holograms considered up to now have been viewed by looking through them; they're all **transmission holograms**, and in each case they were made by causing the reference wave and the object wave to traverse the film from the same side.

Something similar happens when the reference and object waves traverse the emulsion from opposite sides as in Fig. 14.48(b). If for simplicity we again let both waves be planar, the resulting pattern can be visualized by sliding two pencils along with the fronts; it should then be clear that the fringes are straight bands (planes) lying parallel to the face of the film plate. When the actual, highly contorted, object wave is made to overlap a planar, coherent, reference wave, these fringes become modulated with the information describing the object. The corresponding three-dimensional diffraction grating is called a **reflection hologram.** During playback it scatters the reilluminating beam back out toward the viewer, and one sees a virtual image behind the hologram (as if looking into a mirror).

The zone-plate interpretation has been applicable to the various holographic schemes we've considered so far, and this regardless of whether the diffracted wave was of the *near*- or *far*-field variety (i.e., whether we had Fresnel or Fraunhofer holograms, respectively). Indeed it applies generally where the interferogram results from the superpositioning of the scattered, spherical wavelets from each object point and a coherent

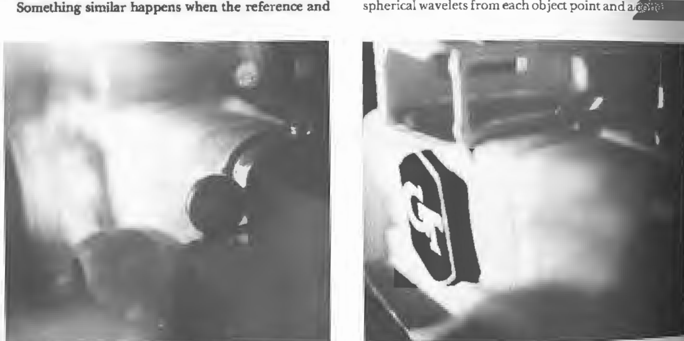
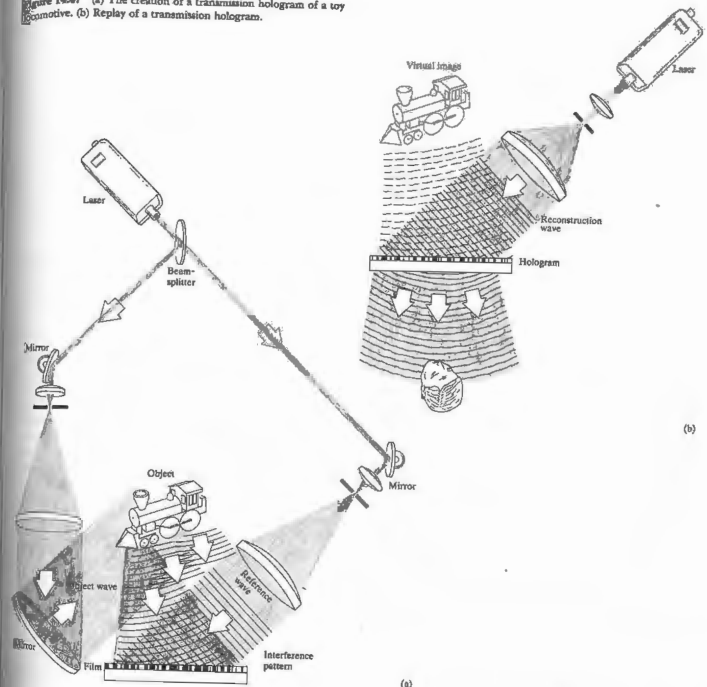


Figure 14.46 A reconstructed holographic image of a model automobile. The camera position and plane of focus were changed between (a) and (b). (Photos from O'Shea, Callen, and Rhodes, *An Introduction to Lasers and Their Applications*.)

Figure 14.47 (a) The creation of a transmission hologram of a toy locomotive. (b) Replay of a transmission hologram.



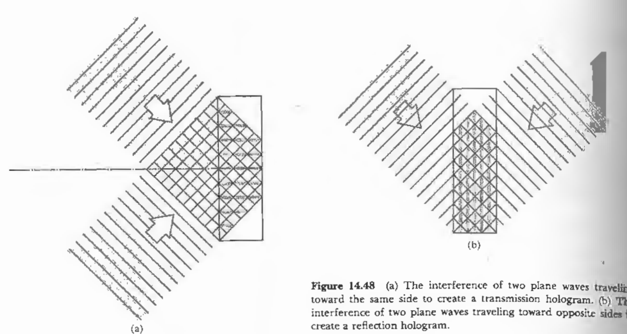


Figure 14.48 (a) The interference of two plane waves traveling toward the same side to create a transmission hologram. (b) The interference of two plane waves traveling toward opposite sides to create a reflection hologram.

plane or even spherical reference wave (provided the latter's curvature is different from that of the wavelets). An inherent problem, which these schemes therefore have in common, arises from the fact that the zone-plate radii, R_m, vary as $m^{1/2}$ from Eq. (10.91). Thus the zone fringes are more densely packed farther from the center of each zone lens (i.e., at larger values of m). This is tantamount to an increasing spatial frequency of bright and dark rings, which must be recorded by the photographic plate. The same thing can be appreciated in the cosine-grating representation, where the spatial frequency increases with θ. Since film, no matter how fine-grained, is limited in its spatial frequency response, there will be a cutoff beyond which it cannot record data. All of this represents a built-in limitation on resolution. In contrast, if the mean frequency of the fringes could be made constant, the limitations imposed by the photographic medium would be considerably reduced, and the resolution correspondingly increased. So long as it could record the average spatial fringe frequency, even a coarse emulsion, such as Polaroid P/N, could be used without extensive loss of resolution. Figure 14.49 shows an arrangement that accomplishes just this by having the diffracted object wavelets interfere with a spherical reference wave of about the same curvature. The resulting interferogram is known as a **Fourier transform** hologram (in this specific instance, it's of the high-resolution *lensless* variety). This scheme is designed to have the reference wave cancel the quadratic (i.e., lens type) dependence of the phase with position on Σ_H. But that will occur precisely only for a planar two-dimensional object. In the case of a three-dimensional object (Fig. 14.50) this only happens over one plane, and the resulting hologram is therefore a composite of both types, that is, a zone lens and Fourier transform. Unlike the other arrangements, both images generated by a Fourier-transform hologram are real, in the same plane, and oriented as if reflected through the origin (Fig. 14.51).

The grating-like nature of all previous holograms is evident here as well. In fact, if you look through a Fourier-transform hologram at a small white-light source (a flashlight in a dark room works beautifully), you see the two mirror images, but they are extremely vague and surrounded by bands of spectral colors. The similarity with white light that has passed through a grating is unmistakable.*

*See DeVelis and Reynolds, *Theory and Applications of Holography;* Stroke, *An Introduction to Coherent Optics and Holography;* Goodman, *Introduction to Fourier Optics;* Smith, *Principles of Holography;* or perhaps *The Engineering Uses of Holography,* edited by E. R. Robertson and J.M. Harvey.

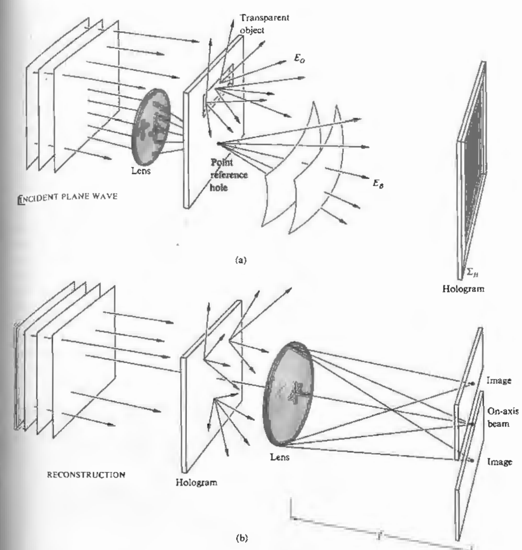


Figure 14.49 Lensless Fourier transform holography (a transparent object).

14.3.2 Developments and Applications

For years holography was an invention in search of application, that notwithstanding certain obvious possibilities, such as the all too inevitable 3-D billboard. Fortunately, several significant technological developments have in recent times begun what will surely be an ongoing extension of the scope and utility of holography. The early efforts in the field were typified by countless images of toy cars and trains, chess pieces and

Figure 14.50 Lensless Fourier transform holography (an opaque object).

statuettes—small objects resting on giant blocks of granite. They had to be small because of limited laser power and coherence length, while the ever-present massive granite platform served to isolate the slightest vibrations that might blur the fringes and thereby degrade or obliterate the stored data. A loud sound or gust of air could result in deterioration of the reconstructed image by causing the photographic plate, object, or mirrors to shift several millionths of an inch during the exposure, which itself might last of the order of a minute or so. That was the still-life era of holography. But now, with the use of new, more sensitive films and the short duration (~40 ns) high-power light flashes from a single-mode pulsed ruby laser, even portraiture and stop-action holography have become a reality* (Fig. 14.52).

Throughout the 1960s and much of the 1970s the emphasis in the field was on the obvious visual wonders of holography. This continues in the 1980s with the mass production of over a hundred million inexpensive plastic reflection holograms (bonded to credit cards; tucked in candy packages; decorating magazine covers, jewelry, and record albums). Indeed, the recent (198[illegible]) development of a photopolymer that is stable, cheap, and able to produce high-quality images will stimulate the manufacture of even more of these throwaway holograms. Still there is now a widespread recognition of the potential of holography as a nonpictorial instrumentality, and that new direction is finding increasingly important applications.

i) Volume Holograms

Yuri Nikolayevitch Denisyuk of the Soviet Union, in 1962, introduced a scheme for generating holograms that was conceptually similar to the early (1891) color photographic process of Gabriel Lippmann. In brief, the object wave is reflected from the subject and propagates backward, overlapping the incoming coherent background wave. In so doing, the two waves set up a three-dimensional pattern of standing waves, as in Fig. 14.48. The spatial distribution of fringes is recorded by the photoemulsion throughout its entire thickness to form what has become known as a **volume hologram.** Several variations have since been introduced, but the basic ideas are the same; rather than generating a two-dimensional grating-like scattering structure, the volume hologram is a three-dimensional grating. In other words, it's a three-dimensional, modulated, periodic array of phase or amplitude objects, which represent the data. It can be recorded in several media, for example, in thick photoemulsions wherein the amplitude objects are grains of deposited silver; in photochromic glass; with halogen crystals, such as KBr, which respond to irradiation via color-center variations; or with a ferroelectric crystal, such as lithium niobate, which undergoes local alterations in its index of refraction, thus forming what might be called a phase volume hologram. In any event, one is left with a volume array of data, however stored in the medium, which in the reconstruction process behaves very much like a crystal being irradiated by x-rays. It scatters the incident (reconstructing) wave according to Bragg's law (Section 10.2.7). This isn't very surprising, since both the scattering centers and λ have simply been scaled up proportionately.

One important feature of volume holograms is the interdependence [via Bragg's law, $2d \sin\theta = m\lambda$ (10.71)] of the wavelength and the scattering angle; that is, only a given color light will be diffracted at a particular angle by the hologram. Another significant property is that by successively altering the incident angle (or the wavelength), a single volume medium can store a great many coexisting holograms at one time. This latter property makes such systems extremely appealing as densely packed memory devices. For example, an 8-mm-thick hologram has been used to store 550 pages of information, each individually retrievable. In theory a single lithium niobate crystal is capable of easily storing thousands of holograms, and any one of them could be replayed by addressing the crystal with a laserbeam at the appropriate angle. Current research is also focusing on potassium tantalate niobate (KTN) as a potential photorefractive crystal-storage medium. Imagine a 3-D holographic motion picture; a library; or everyone's vital statistics—beauty marks, credit cards, taxes, bad habits, income, life history, and so on, all recorded on a handful of small transparent crystals.

Multicolored reconstructions have been formed using (black and white) volume holographic plates. Two, three, or more different colored and mutually incoherent overlapping laserbeams are used to generate separate, cohabitating, component holograms of the object, and this can be done one at a time or all at once. When these are illuminated simultaneously by the various constituent beams, a multicolored image results.

Another important and highly promising scheme, devised by G. W. Stroke and A. E. Labeyrie, is known as **white-light reflection holography**. Here, the reconstructing wave is an ordinary white-light beam from, say, a flashlight or projector, having a wavefront similar to the original quasimonochromatic background wave. When illuminated on the same side as the viewer, only the specific wavelength that enters the volume hologram at the proper Bragg angle is reflected off to form a reconstructed 3-D virtual image. Thus if the scene were recorded in red laserlight, only red light would presumably be reflected as an image. It is of pedagogical interest to point out, however, that the emulsion may shrink during the fixing process, and if it is not swollen back to its original form chemically (with say triethylnolamine), the spacing of the Bragg planes, d, decreases. That means that at a given angle θ, the reflected

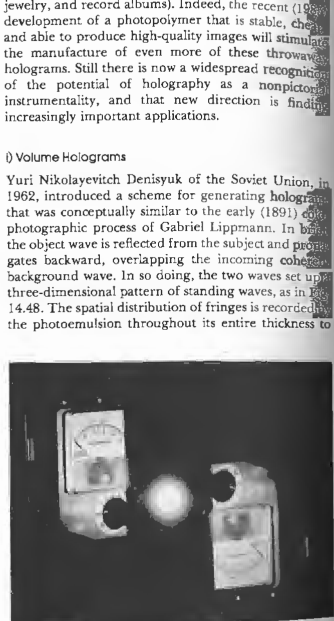


Figure 14.51 A reconstruction of a Fourier transform hologram. [From G. W. Stroke, D. Brumm, and A. Funkhauser, *J. Opt. Soc. Am.* **55**, 1327 (1965).]

Figure 14.52 A reconstruction of a holographic portrait. (Photo courtesy L. D. Siebert.)

* L. D. Siebert, *Appl. Phys. Letters* **11**, 326 (1967), and R. G. Zech and L. D. Siebert, *Appl. Phys. Letters* **13**, 417 (1968).

wavelength will decrease proportionately. Hence, a scene recorded in He–Ne red might play back in orange or even green when reconstructed by a beam of white light.

If several overlapping holograms corresponding to different wavelengths are stored, a mutlicolored image will result. The advantages of using an ordinary source of white light to reconstruct full-color 3-D images are obvious and far-reaching.

ii) Holographic Interferometry

One of the most innovative and practical of recent holographic advances is in the area of interfernmetry. Three distinctive approaches have proved to be quite useful in a wealth of nondestructive testing situations where, for example, one might wish to study microinch distortions in an object resulting from strain, vibration, heat, etc. In the *double exposure* technique, one simply makes a hologram of the undisturbed object and then, before processing, exposes the hologram for a second time to the light coming from the now distorted object. The ultimate result is two overlapping reconstructed waves, which proceed to form a fringe pattern indicative of the displacements suffered by the object, that is, the changes in optical path length (Fig. 14.53). Variations in index such as those arising in wind tunnels and the like will generate the same sort of pattern.

In the *real-time* method, the subject is left in its original position throughout; a processed hologram is formed, and the resulting virtual image is made to overlap the object precisely (Fig. 14.54). Any distortions that arise during subsequent testing show up, on looking through the hologram, as a system of fringes, which can be studied as they evolve in real time. The method applies to both opaque and transparent objects. Motion pictures can be taken to form a continuous record of the response.

The third method is the *time-average* approach and is particularly applicable to rapid, small-amplitude, oscillatory systems. Here the film plate is exposed for a relatively long duration, during which time the vibrating object has executed a numbr of oscillations. The resulting hologram can be thought of as a superposition of a multiplicity of images, with the effect that a standing-wave pattern emerges. Bright areas reveal undeflected or stationary nodal regions, while contour lines trace out areas of constant vibrational amplitude.

Figure 14.53 Double exposure holographic interferogram. [illegible] S. M. Zivi and G. H. Humberstone, "Chest Motion Visualized [illegible] Holographic Interferometry," *Medical Research Eng.* p. 5 (June 19[illegible])

Especially promising in the field of nondestructive testing is the commercial availability (1983) of a holographic system that records on erasable thermoplastic film. The holograms are produced in less than [illegible] seconds after exposure, and the plate can be reused hundreds of times. Today holographic testing of mechanical systems is already a well established practice in industry. It continues to serve in a broad range of applications, from noise reduction in automobile transmissions to routine jet engine inspections.

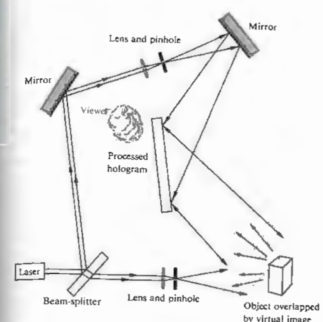


Figure 14.54 Real-time holographic interferometry.

iii) Acoustical Holography

In acoustical holography, an ultra-high-frequency sound wave (ultrasound) is used to create the hologram initially, and a laserbeam then serves to form a recognizable reconstructed image. In one application, the stationary ripple pattern on the surface of a water body produced by submerged coherent transducers corresponds to a hologram of the object beneath (Fig. 14.55). Photographing it creates a hologram that can be illuminated optically to form a visual image. Alternatively, the ripples can be irradiated from above with a laserbeam to produce an instantaneous reconstruction in reflected light.

The advantages of acoustical techniques reside in the fact that sound waves can propagate considerable distances in dense liquids and solids where light cannot. Thus acoustical holograms can record such diverse things as underwater submarines and internal body organs.* In the case of Fig. 14.55, one would see something that resembled an x-ray motion picture of the fish. Figure 14.56 is the image of a penny formed via acoustical holography using ultrasound at a frequency of 48 MHz. In water that corresponds to a wavelength of roughly 30 μm, and so each fringe contour reveals a change in elevation of $\frac{1}{2}\lambda$ or 15 μm.

* See A. F. Metherell, "Acoustical Holography," *Sci. Am.* **221**, 36 (October 1969). Refer to A. L. Dalisa et al., "Photoanodic Engraving of Holograms on Silicon," *Appl. Phys. Letters* **17**, 208 (1970), for another interesting use of surface relief patterns.

iv) Holographic Optical Elements

Evidently when two plane waves overlap, as in Fig. 14.42, they produce a cosine grating. This suggests the rather obvious notion that holography can be used for nonpictorial purposes, like making diffraction gratings. Indeed the *holographic optical element* (HOE) is any diffractive device consisting of a "fringe" system (i.e., a distribution of diffracting amplitude or phase objects) created either directly by interferometry or by computer simulation thereof. Holographic diffraction gratings, both blazed and sinusoidal, are available commercially (with up to around 3600 lines/mm). Although still less efficient than ruled gratings, they do produce far less stray light, which can be important in many applications.

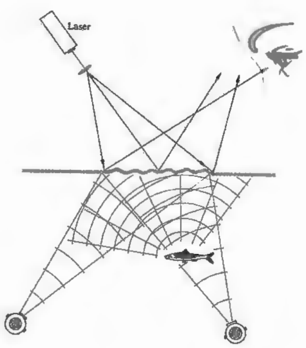


Figure 14.55 Acoustical holography.

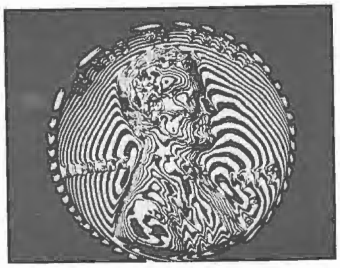


Figure 14.56 Interferometric image of a penny via acoustical holography. (Photo courtesy Holosonics, Inc.)

Suppose we record the interference pattern of a converging beam using a planar reference wave. Upon reilluminating the resulting transmission hologram with a matching plane wave, out will come a recreated converging wave—the hologram will function like a lens (see Fig. 14.39). Similarly, if the reference beam is a diverging wave from a point source and the object is a plane wave, the resulting hologram, reilluminated by the point source, will play back a plane wave. In this way a holographic optical element can perform the tasks of a complex lens with the added benefit of allowing for an inexpensive, lightweight, compact system design. Holographic optical elements are already in use inside supermarket check-out scanners that automatically read the bar patterns of the Universal Product Code (UPC) on merchandise. A laserbeam passes through a rotating disk composed of a number of holographic lens-prism facets. These rapidly refocus, shift, and scan the beam across a volume of space, ensuring that the code will be read on the first pass across the device. HOEs are used in so-called heads-up displays in airplane cockpits. These allow reflected data to appear on an otherwise transparent screen in front of the pilot's face and yet not obscure the view. They're also in office copy machines and solar concentrators.

As *matched spatial filters*, HOEs are used in optical correlators (p. 505) to spot defects in semiconductors and tanks in reconnaissance pictures. In such cases the HOE is a hologram formed using the Fourier transform of the target (e.g., a picture of a tank or perhaps a printed word) as the object. Suppose the problem is to find a word on a printed page automatically, using an optical computer like that in Fig. 14.8, that is, to cross-correlate the word and the page of words. The target transform hologram is placed in the transform plane and illuminated with the transform of an entire page of print. The field amplitude emerging from this HOE filter will then be proportional to the product of the transforms of the page and the word. The transform of this product, generated by the last lens and displayed on the image plane, is the desired cross-correlation (recall the Wiener–Khintchine theorem). If the word is on the page, there will be a high correlation, and a bright spot of light will appear superimposed in the final image everywhere the target word occurs.*

It is possible to synthesize, point by point, a hologram of a fictitious object. In other words, in the most direct approach holograms can be produced by calculating, with a digital computer, the irradiance distribution that would arise were some object appropriately illuminated in a hypothetical recording session. A computer-controlled plotter drawing or cathode ray tube readout of the interferogram is then photographed, thence to serve as the actual hologram. The result upon illumination is a three-dimensional reconstructed image of an object that never had any real existence in the first place. More practically, computer-generated HOEs are now routinely being produced, often to serve as references for optical testing. Since this mating of technologies can in principle generate wavefronts otherwise essentially impossible to produce, the future is very promising.

14.4 NONLINEAR OPTICS

Generally, the domain of *nonlinear optics* is understood to encompass those phenomena for which electric and magnetic field intensities of higher powers than the first play a dominant role. The Kerr effect (Section 8.11.3), which is a quadratic variation of refractive index with applied voltage, and thereby electric field, is typical of several long-known nonlinear effects.

The usual classical treatment of the propagation of light—superposition, reflection, refraction, and so forth—assumes a linear relationship between the electromagnetic light field and the responding atomic system constituting the medium. But just as an oscillatory mechanical device (e.g., a weighted spring) can be overdriven into nonlinear response through the application of large enough forces, so too we might anticipate that an extremely intense beam of light could generate appreciable nonlinear optical effects. The electric fields associated with light beams from ordinary or, if you will, traditional sources are far too small for such behavior to be easily observable. It was for this reason, coupled with an initial lack of technical prowess, that the subject had to await the advent of the laser in order that sufficient brute force could be brought to bear in the optical region of the spectrum. As an example of the kinds of fields readily obtainable with the current technology, consider that a good lens can focus a laserbeam down to a spot having a diameter of about 10^{-3} inch or so, which corresponds to an area of roughly 10^{-9} m^2. A 200-megawatt pulse from, say, a Q-switched ruby laser would then produce a flux density of 20×10^{16} W/m^2. It follows (Problem 14.18) from Section 3.3.1 that the corresponding electric field amplitude is given by

$$E_0 = 27.4\left(\frac{I}{n}\right)^{1/2}. \qquad (14.17)$$

In this particular case, for $n \approx 1$, the field amplitude is about 1.2×10^8 V/m. This is more than enough to cause the breakdown of air (roughly 3×10^6 V/m) and just several orders of magnitude less than the typical fields holding a crystal together, the latter being roughly about the same as the cohesive field on the electron in a hydrogen atom (5×10^{11} V/m). The availability of these and even greater (10^{12} V/m) fields has made possible a wide range of important new nonlinear phenomena and devices. We shall limit this discussion to the consideration of several nonlinear phenomena associated with passive media (i.e., media that act essentially as catalysts without making their own characteristic frequencies evident). Specifically, we'll consider optical rectification, optical harmonic generation, frequency mixing, and self-focusing of light. In contrast, stimulated Raman, Rayleigh, and Brillouin scattering (Section 13.8) exemplify nonlinear optical phenomena arising in active media that do impose their characteristic frequencies on the lightwave.*

As you may recall (Section 3.5.1), the electromagnetic field of a lightwave propagating through a medium exerts forces on the loosely bound outer or valence electrons. Ordinarily these forces are quite small, and in a linear isotropic medium the resulting electric polarization is parallel with and directly proportional to the applied field. In effect, the polarization follows the field; if the latter is harmonic, the former will be harmonic as well. Consequently, one can write

$$P = \epsilon_0 \chi E, \qquad (14.18)$$

where χ is a dimensionless constant known as the electric susceptibility, and a plot of P versus E is a straight line. Quite obviously in the extreme case of very high fields, we can expect that P will become saturated; in other words, it simply cannot increase linearly indefinitely with E (just as in the familiar case of ferromagnetic materials, where the magnetic moment becomes saturated at fairly low values of H). Thus we can anticipate a gradual increase of the ever-present, but usually insignificant, nonlinearity as E increases. Since the directions of **P** and **E** coincide in the simplest case of an isotropic medium, we can express the polarization more effectively as a series expansion:

$$P = \epsilon_0(\chi E + \chi_2 E^2 + \chi_3 E^3 + \cdots). \qquad (14.19)$$

The usual linear susceptibility, χ, is much greater than the coefficients of the nonlinear terms χ_2, χ_3, and so on, and hence the latter contribute noticeably only at high-amplitude fields. Now suppose that a lightwave of the form

$$E = E_0 \sin \omega t$$

is incident on the medium. The resulting electric

* See A. Ghatak and K. Thyagarajan, *Contemporary Optics*, p. 212.

* For a more extensive treatment than is possible here, see N. Bloembergen, *Nonlinear Optics*, or G. C. Baldwin, *An Introduction to Nonlinear Optics*.

polarization

$$P = \epsilon_0\chi E_0 \sin \omega t + \epsilon_0\chi_2 E_0^2 \sin^2 \omega t + \epsilon_0\chi_3 E_0^3 \sin^3 \omega t + \cdots \quad (14.20)$$

can be rewritten as

$$P = \epsilon_0\chi E_0 \sin \omega t + \frac{\epsilon_0\chi_2}{2} E_0^2(1 - \cos 2\omega t) + \frac{\epsilon_0\chi_3}{4} E_0^3(3 \sin \omega t - \sin 3\omega t) + \cdots. \quad (14.21)$$

As the harmonic lightwave sweeps through the medium, it creates what might be thought of as a polarization wave, that is, an undulating redistribution of charge within the material in response to the field. If only the linear term were effective, the electric polarization wave would correspond to an oscillatory current following along with the incident light. The light thereafter reradiated in such a process would be the usual refracted wave generally propagating with a reduced speed v and having the same frequency as the incident light. In contrast, the presence of higher-order terms in Eq. (14.20) implies that the polarization wave certainly does have the same harmonic profile as the incident field. In fact, Eq. (14.21) can he likened to a Fourier series representatiton of the distored profile of $P(t)$.

14.4.1 Optical Rectification

The second term in Eq. (14.21) has two components of great interest. First there is a *dc* or *constant bias polarization* varying as E_0^2. Consequently, if an intense plane-polarized beam traverses an appropriate (piezoelectric) crystal, the presence of the quadratic nonlinearity will, in part, be manifest by a constant electric polarization of the medium. A voltage difference, proportional to the beam's flux density, will accordingly appear across the crystal. This effect, in analogy to its radiofrequency counterpart, is known as **optical rectification**.

14.4.2 Harmonic Generation

The $\cos 2\omega t$ term (14.21) corresponds to a variation in electric polarization at twice the fundamental frequency (i.e., at twice that of the incident wave). The reradiated light that arises from the driven oscillators also has a component at this same frequency, 2ω, and the process is spoken of as **second-harmonic generation**, or SHG for short. In terms of the photon representation we can envision two identical photons of energy $\hbar\omega$ coalescing within the medium to form a single photon of energy $\hbar 2\omega$. Peter A. Franken and several coworkers at the University of Michigan in 1961 were the first to observe SHG experimentally. They focused a 3-kW pulse of red (694.3 nm) ruby laserlight onto a quartz crystal. Just about one part in 10^8 of this incident wave was converted to the 347.15-nm ultraviolet second harmonic.

Notice that, for a given material, if $P(E)$ is an odd function, that is, if reversing the direction of the **E**-field simply reverses the direction of **P**, the even powers of E in Eq. 14.19 must vanish. But this is just what happens in an isotropic medium, such as glass or water—there are no special directions in a liquid. Morover, in crystals like calcite, which are so structured as to have what's known as a *center of symmetry* or an *inversion center*, a reversal of all of the coordinate axes must leave the interrelationships between physical quantities unaltered. Thus no even harmonics can be produced by materials of this sort. Third-harmonic generation (THG), however, can exist and has been observed, for example, in calcite. The requirement for SHG that a crystal not have inversion symmetry is also necessary for it to be piezoelectric. Under pressure a piezoelectric crystal [such as quartz, potassium dihydrogen phosphate (KDP), or ammonium dihydrogen phosphate (ADP)] undergoes an asymmetric distortion of its charge distribution, thus producing a voltage. Of the 32 crystal classes, 20 are of this kind and may therefore be used in SHG. The simple scalar expression (14.19) is actually not an adequate description of a typical dielectric crystal. Things are a good deal more complicated, because the field components in several different directions in a crystal can affect the electric polarization in any one direction. A complete treatment requires that **P** and **E** be related not by a single scalar but by a group of quantities arranged in the particular form of a tensor, namely, the susceptibility tensor.*

* Incidentally, there is nothing extraordinary about this kind of behavior—it comes up all the time. There are inertia tensors, demagnetization coefficient tensors, stress tensors, and so forth.

A major difficulty in generating copious amounts of second-harmonic light arises from the frequency dependence of the refractive index, that is, dispersion. At some initial point where the incident or ω-wave, generates the second-harmonic or 2ω-wave, the two are coherent. As the ω-wave propagates through the crystal, it continues to generate additional contributions of second-harmonic light, which all combine totally constructively only if they maintain a proper phase relationship. Yet the ω-wave travels at a phase velocity v_ω, which is ordinarily different from the phase velocity, $v_{2\omega}$, of the 2ω-wave. Thus the newly emitted second harmonic periodically falls out of phase with some of the previously generated 2ω-waves. When the irradiance of the second harmonic, $I_{2\omega}$, emerging from a plate of thickness ℓ is computed* it turns out to be

$$I_{2\omega} \propto \frac{\sin^2 [2\pi(n_\omega - n_{2\omega})\ell/\lambda_0]}{(n_\omega - n_{2\omega})^2} \quad (14.22)$$

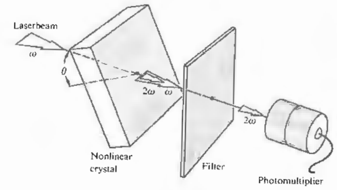
(see Fig. 14.57). This yields the result that $I_{2\omega}$ has its maximum value when $\ell = \ell_c$, where

$$\ell_c = \frac{1}{4}\frac{\lambda_0}{|n_\omega - n_{2\omega}|}. \quad (14.23)$$

This is quite commonly known as the *coherence length* (although a different name would perhaps be better), and it's usually of the order of only about $20\lambda_0$. Despite this, efficient SHG can be accomplished by a procedure known as *index matching*, which negates the undesirable effects of dispersion; in short, one arranges things so that $n_\omega = n_{2\omega}$. A commonly used SHG material is KDP. It is piezoelectric, transparent, and also negatively uniaxially birefringent. Furthermore, it has the interesting property that if the fundamental light is a linear polarized *ordinary wave*, the resulting second harmonic will be an *extraordinary wave*. As can be seen from Fig. 14.58, if light propagates within a KDP crystal at the specific angle θ_0 with respect to the optic axis, the index, $n_{0\omega}$, of the ordinary fundamental wave will precisely equal the index of the extraordinary second harmonic $n_{e2\omega}$. The second-harmonic wavelets will then interfere constructively, thereupon increasing the conversion efficiency by several orders of magnitude. Second-harmonic genrators, which are simply appropriately cut and oriented crystals, are available commercially, but do keep in mind that θ_0 is a function of λ, and each such device performs at one frequency. Not long ago, a continuous 1-W second-harmonic beam at 532.3 nm was obtained by placing a barium sodium niobate crystal within the cavity of a 1-W 1.06μ laser. The fact that the ω-wave sweeps back and forth through the crystal increases the net conversion efficiency.

Optical harmonic generation soon lost its initial exotic quality and became a routine commercial process

* See, for example, B. Lengyel, *Introduction to Laser Physics*, Chapter VII. This is a fine elementary treatment.



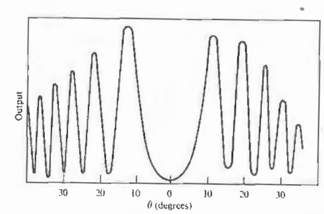


Figure 14.57 Second harmonic generation as a function of θ for a 0.78-mm thick quartz plate. Peaks occur when the effective thickness is an even multiple of ℓ_c. [From P. D. Maker, R. W. Terhune, M. Nisenoff, and C. M. Savage, *Phys. Rev. Letters* 8, 21 (1962).]

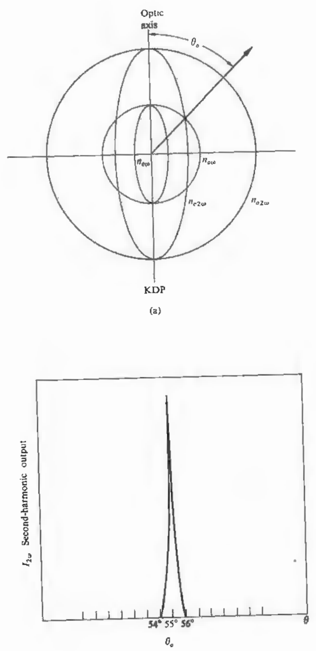


Figure 14.58 Refractive index surface for KDP. (b) $I_{2\omega}$ versus crystal orientation in KDP. (From Maker et al.)

by the early 1980s. Still, there continue to be exciting technical accomplishments, such as the 74-cm-diameter harmonic conversion array (Fig. 14.59) built for the Nova laser-fusion program. Its function is to convert upwards of 80% of the infrared (1.05 μm) emission from the neodymium–glass laser (Fig. 14.37) into more efficient high-frequency radiation. Because of its great size the converter is an aligned mosaic of smaller KDP single-crystal panels forming two layers, one behind the other. To generate the second harmonic (green light at 0.53 μm), the array is positioned so that each layer functions independently to produce two overlapping frequency-shifted components. These arise one from each crystal layer and are orthogonally polarized. The third harmonic (blue light at 0.35 μm) is created by reorienting the assembly to the appropriate phase-matching angle so as to shift about two thirds of the beam energy into the second harmonic as it traverses the first crystal layer. The second layer mixes the remaining IR and the second-harmonic green light to produce third-harmonic blue.

14.4.3 Frequency Mixing

Another situation of considerable practical interest involves the *mixing* of two or more primary beams of different frequencies within a nonlinear dielectric. The process can most easily be appreciated by substituting a wave of the form

$$E = E_{01} \sin \omega_1 t + E_{02} \sin \omega_2 t \qquad (14.24)$$

into the simplest expression for P given by Eq. [illegible]. The second-order contribution is then

$$\epsilon_0 \chi_2 (E_{01}^2 \sin^2 \omega_1 t + E_{02}^2 \sin^2 \omega_2 t + 2E_{01}E_{02} \sin \omega_1 t \sin \omega_2 t).$$

The first two terms can be expressed as functions of $2\omega_1$ and $2\omega_2$, respectively, while the last quantity gives rise to sum and difference terms, $\omega_1 + \omega_2$ and $\omega_1 - \omega_2$.

As for the quantum picture, the photon of frequency $\omega_1 + \omega_2$ simply corresponds to a coalescing of the two original photons into a new photon, just as it did in the case of SHG, where both quanta had the same frequency. The energy and momentum of the annihilated photons are carried off by the created sum photon. The generation of an $\omega_1 - \omega_2$ difference-photon is a little more involved. Conservation of energy and momentum requires that on interacting with an ω_2-photon, only the higher-frequency ω_1-photon vanishes, thereby creating two new quanta, one an ω_2-photon and the other a difference-photon.

As an application of this phenomenon, suppose we beat, within a nonlinear crystal, a strong wave of

Figure 14.59 The KDP frequency converter for the Nova laser. (Photo courtesy Lawrence Livermore National Laboratory.)

frequency ω_p, called the *pump light*, with a weak *signal wave* of lower frequency ω_s, which is to be amplified. Pump light is thereby converted into both signal light and a difference wave, called *idler light*, of frequency $\omega_i = \omega_p - \omega_s$. If the idler light is then made to beat with the pump light, the latter is converted into additional amounts of idler and signal light. In this way both the signal and idler waves are amplified. This is actually an extension into the optical-frequency region of the well-known concept of *parametric amplification*, whose use in the microwave spectrum dates back to the late 1940s. The first *optical-parametric oscillator*, which was operated in 1965, is depicted in Fig. 14.60. The flat parallel end faces of a nonlinear crystal (lithium niobate) were coated to form an optical Fabry–Perot cavity. The signal and idler frequencies (both about 1000 nm) corresponded to two of the resonant frequencies of the cavity. When the flux density of the pumping light was high enough, energy was transferred from it into the signal and idler oscillatory modes, with the consequent build-up of those modes and emission of coherent radiant energy at those frequencies. This transfer of energy from one wave to another within a lossless medium typifies parametric processes. By changing the refractive index of the crystal (via temperature, electric field, etc.), the oscillator becomes tunable. Various oscillator configurations have since evolved, with other nonlinear materials used as well, such as barium sodium niobate. The optical parametric oscillator is a laser-like, broadly tunable source of coherent radiant energy in the IR to the UV.

14.4.4 Self-Focusing of Light

When a dielectric is subjected to an electric field that varies in space, in other words, when there is a gradient of the field parallel to **P**, an internal force will result. This has the effect of altering the density, changing the permittivity, and thereby varying the refractive index, and this in both linear and nonlinear isotropic media. Suppose then that we shine an intense laserbeam with a transverse Gaussian flux-density distribution onto a specimen. The induced refractive-index variations will cause the medium in the region of the beam to function much as if it were a positive lens. Accordingly, the beam

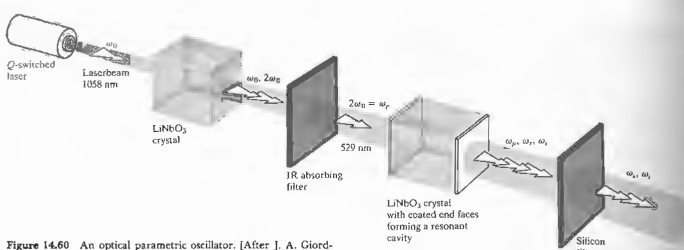


Figure 14.60 An optical parametric oscillator. [After J. A. Giordmaine and R. C. Miller, *Phys. Rev. Letters* **4**, 973 (1965).]

contracts, the flux density increases even more, and the contraction continues in a process known as **self-focusing**. The effect can be sustained until the beam reaches a limiting filament diameter (of about 5×10^{-6} m), being totally internally reflected as if it were in a fiberoptic element imbedded within the medium.†

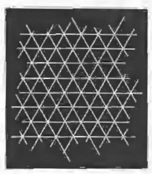


Figure 14.61

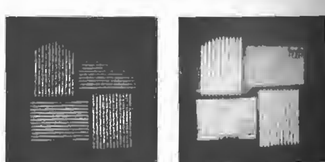
PROBLEMS

14.1 What would the pattern look like for a laserbeam diffracted by the three crossed gratings of Fig. 14.61?

14.2 Make a rough sketch of the Fraunhofer diffraction pattern that would arise if a transparency of Fig. 14.62(a) served as the object. How would you filter it to get Fig. 14.62(b)?

14.3 Repeat the previous problem using Fig. 14.63 instead.

† See J. A. Giordmaine, "Nonlinear Optics," *Phys. Today*, 39 (January 1969).



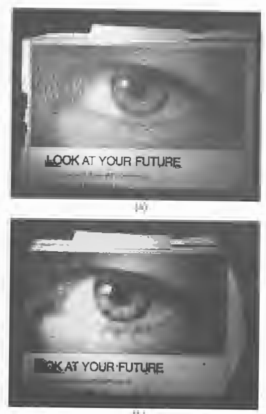
(a) (b)

Figure 14.62 Photos courtesy R. A. Phillips.

(a) (b)

Figure 14.63 Photos courtesy R. A. Phillips.

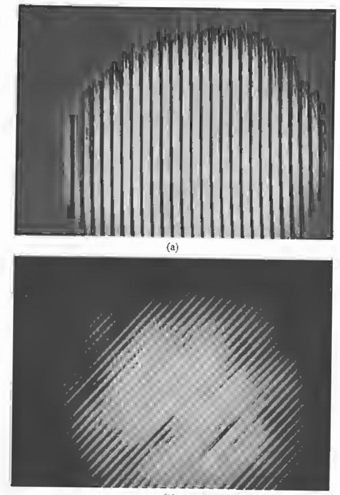
14.4* Repeat the previous problem using Fig. 14.64 this time.



(a) (b)

Figure 14.64 Photos courtesy R. A. Phillips.

14.5 Returning to Fig. 14.10, what kind of spatial filter would produce each of the patterns shown in Fig. 14.65?



(a) (b)

Figure 14.65 Photos courtesy D. Dutton, M. P. Givens, and R. E. Hopkins.

14.6 With Fig. 14.9 in mind, show that the transverse magnification of the system is given by $-f_i/f_t$ and draw the appropriate ray diagram. Draw a ray up through the center of the first lens at an angle θ with the axis. From the point where that ray intersects Σ_t, draw a ray downward that passes through the center of the second lens at an angle Φ. Prove that $\Phi/\theta = f_t/f_i$. Using the notion of spatial frequency, from Eq. (11.64), show that k_O at the object plane is related to k_I at the image plane by

$$k_I = k_O(f_i/f_t)$$

What does this mean with respect to the size of the image when $f_i > f_t$? What can then be said about the spatial periods of the input data as compared with the image output?

14.7 A diffraction grating having a mere 50 grooves per cm is the object in the optical computer shown in Fig. 14.9. If it is coherently illuminated by plane waves of green light (543.5 nm) from a He-Ne laser and each lens has a 100-cm focal length, what will be the spacing of the diffraction spots on the transform plane?

14.8* Imagine that you have a cosine grating (i.e., a transparency whose *amplitude* transmission profile is cosinusoidal) with a spatial period of 0.01 mm. The grating is illuminated by quasimonochromatic plane waves of $\lambda = 500$ nm, and the setup is the same as that of Fig. 14.9, where the focal lengths of the transform and imaging lenses are 2.0 m and 1.0 m, respectively.

a) Discuss the resulting pattern and design a filter that will pass *only* the first-order terms. Describe it in detail.
b) What will the image look like on Σ_i with that filter in place?
c) How might you pass only the dc term, and what would the image look like then?

14.9 Suppose we insert a mask in the transform plane of the previous problem, which obscures everything but the $m = +1$ diffraction contribution. What will the re-formed image look like on Σ_i? Explain your reasoning. Now suppose we remove *only* the $m = +1$ or the $m = -1$ term. What will the re-formed image look like?

14.10* Referring to the previous two problems with the cosine grating oriented horizontally, make a sketch of the electric field amplitude along y' with no filtering. Plot the corresponding image irradiance distribution. What will the electric field of the image look like if the dc term is filtered out? Plot it. Now plot the new irradiance distribution. What can you say about the spatial frequency of the image with and without the filter in place? Relate your answers to Fig. 11.13.

14.11 Replace the cosine grating in the previous problem with a "square" bar grating, that is, a series of fine alternating opaque and transparent bands of equal width. We now filter out all terms in the transform plane but the zeroth and the two first-order diffraction spots. These we determine to have relative irradiances of 1.00, 0.36, and 0.36: compare them with Figs. 7.15(a) and 7.16. Derive an expression for the general shape of the irradiance distribution on the image plane—make a sketch of it. What will the resulting fringe system look like?

14.12 A fine square wire mesh with 50 wires per cm is placed vertically in the object plane of the optical computer of Fig. 14.8. If the lenses each have 1.00-m focal lengths, what must be the illuminating wavelength if the diffraction spots on the transform plane are to have a horizontal and vertical separation of 2.0 mm? What will be the mesh spacing as it appears on the image plane?

14.13* Imagine that we have an opaque mask into which are punched an ordered array of circular holes, all of the same size, located as if at the corners of the boxes of a checkerboard. Now suppose our robot puncher goes mad and makes an additional batch of holes essentially randomly all across the mask. If this screen is now made the object in Problem. 14.11, what will the diffraction pattern look like? Given that the ordered holes are separated from their nearest neighbors on the object by 0.1 mm, what will be the spatial frequency of the corresponding dots in the image? Describe a filter that will remove the random holes from the final image.

14.14* Imagine that we have a large photographic transparency on which there is a picture of a student made up of a regular array of small circular dots, all the same size, but each with its own density, so that it passes a spot of light with a particular field amplitude. Considering the transparency to be illuminated by a

plane wave, discuss the idea of representing the electric field amplitude just beyond it as the product (on average) of a regular two-dimensional array of top-hat functions (Fig. 11.4, p. 476) and the continuous two-dimensional picture function: the former like a dull bed of nails, the latter an ordinary photograph. Applying the frequency convolution theorem, what does the distribution of light look like on the transform plane? How might it be filtered to produce a continuous output image?

14.15* Given that a ruby laser operating at 694.3 nm has a frequency bandwidth of 50 MHz, what is the corresponding linewidth?

14.16* Determine the frequency difference between adjacent axial resonant cavity modes for a typical gas laser 25 cm long ($n \approx 1$).

14.17* A He-Ne c-w laser has a Doppler-broadened transition bandwidth of about 1.4 GHz at 632.8 nm. Assuming $n = 1.0$, determine the maximum cavity length for single-axial-mode operation. Make a sketch of the transition linewidth and the corresponding cavity modes.

14.18 Show that the maximum electric field intensity, E_{max}, that exists for a given irradiance I is

$$E_{max} = 27.4\left(\frac{I}{n}\right)^{1/2} \text{ in units of V/m,}$$

where n is the refractive index of the medium.

14.19* The arrangement shown in Fig. 14.66 is used to convert a collimated laserbeam into a spherical wave. The pinhole cleans up the beam; that is, it eliminates diffraction effects due to dust and the like on the lens. How does it manage it?

14.20 What would happen to the speckle pattern if a laserbeam were projected onto a suspension such as milk rather than onto a smooth wall?

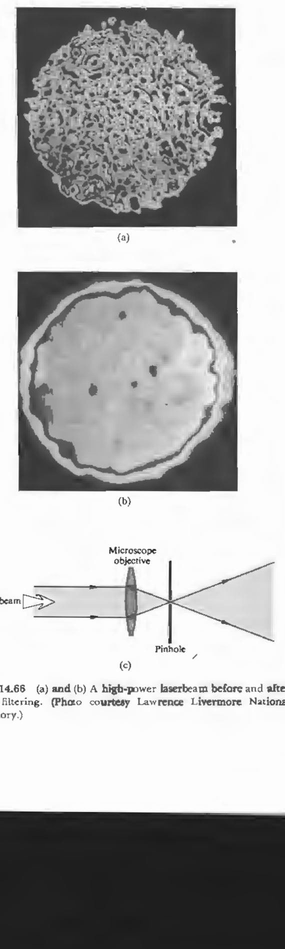


Figure 14.66 (a) and (b) A high-power laserbeam before and after spatial filtering. (Photo courtesy Lawrence Livermore National Laboratory.)

Appendix 1 Electromagnetic Theory

MAXWELL'S EQUATIONS IN DIFFERENTIAL FORM

The set of integral expressions that have come to be known as Maxwell's equations are

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = -\iint_A \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S} \qquad [3.5]$$

$$\oint_C \frac{\mathbf{B}}{\mu} \cdot d\mathbf{l} = \iint_A \left(\mathbf{J} + \epsilon \frac{\partial \mathbf{E}}{\partial t}\right) \cdot d\mathbf{S} \qquad [3.13]$$

$$\oiint_A \epsilon \mathbf{E} \cdot d\mathbf{S} = \iiint_V \rho \, dV \qquad [3.7]$$

and

$$\oiint_A \mathbf{B} \cdot d\mathbf{S} = 0, \qquad [3.9]$$

where the units, as usual, are SI.

Maxwell's equations can be written in a differential form, which is more useful for deriving the wave aspects of the electromagnetic field. This transition can readily be accomplished by making use of two theorems from vector calculus, namely, Gauss's divergence theorem,

$$\oiint_A \mathbf{F} \cdot d\mathbf{S} = \iiint_V \nabla \cdot \mathbf{F} \, dV \qquad (A1.1)$$

and Stokes's theorem

$$\oint_C \mathbf{F} \cdot d\mathbf{l} = \iint_A \nabla \times \mathbf{F} \cdot d\mathbf{S}. \qquad (A1.2)$$

Here the quantity **F** is not one fixed vector, but a function that depends on the position variables. It is a rule that associates a single vector, for example, in Cartesian coordinates, $\mathbf{F}(x, y, z)$, with each point (x, y, z) in space. Vector-valued functions of this kind, such as **E** and **B**, are known as vector fields.

Applying Stokes's theorem to the electric field intensity, we have

$$\oint \mathbf{E} \cdot d\mathbf{l} = \iint \nabla \times \mathbf{E} \cdot d\mathbf{S}. \qquad (A1.3)$$

If we compare this with Eq. (3.5), it follows that

$$\iint \nabla \times \mathbf{E} \cdot d\mathbf{S} = -\iint \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S}. \qquad (A1.4)$$

This result must be true for all surfaces bounded by the path *C*. This can only be the case if the integrands are themselves equal, that is, if

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}. \qquad (A1.5)$$

A similar application of Stokes's theorem to **B**, using Eq. (3.13), results in

$$\nabla \times \mathbf{B} = \mu\left(\mathbf{J} + \epsilon \frac{\partial \mathbf{E}}{\partial t}\right). \qquad (A1.6)$$

Gauss's divergence theorem applied to the electric field intensity yields

$$\oiint \mathbf{E} \cdot d\mathbf{S} = \iiint \nabla \cdot \mathbf{E} \, dV. \qquad (A1.7)$$

If we make use of Eq. (3.7), this becomes

$$\iiint_V \nabla \cdot \mathbf{E} \, dV = \frac{1}{\epsilon} \iiint_V \rho \, dV, \qquad (A1.8)$$

and since this is to be true for any volume (i.e., for an arbitrary closed domain), the two integrands must be equal. Consequently, at any point (x, y, z, t) in space–time

$$\nabla \cdot \mathbf{E} = \rho/\epsilon. \qquad (A1.9)$$

In the same fashion Gauss's divergence theorem applied to the **B**-field and combined with Eq. (3.9) yields

$$\nabla \cdot \mathbf{B} = 0. \qquad (A1.10)$$

Equations (A1.5), (A1.6) (A1.9), and (A1.10) are Maxwell's equations in differential form. Refer back to Eqs. (3.18) through (3.21) for the simple case of Cartesian coordinates and *free space* ($\rho = J = 0$, $\epsilon = \epsilon_0$, $\mu = \mu_0$).

ELECTROMAGNETIC WAVES

To derive the electromagnetic wave equation in its most general form, we must again consider the presence of some medium. We saw in Section 3.5.1 that there is a need to introduce the *polarization* vector **P**, which is a measure of the overall behavior of the medium, in that it is the resultant electric dipole moment per unit volume. Since the field within the material has been altered, we are led to define a new field quantity, the *displacement* **D**:

$$\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P}. \qquad (A1.11)$$

Clearly then,
$$\mathbf{E} = \frac{\mathbf{D}}{\epsilon_0} - \frac{\mathbf{P}}{\epsilon_0}.$$

The internal electric field **E** is the difference between the field $\mathbf{D}/\epsilon_0$, which would exist in the absence of polarization, and the field $\mathbf{P}/\epsilon_0$ arising from polarization.

For a homogeneous, linear, isotropic dielectric, **P** and **E** are in the same direction and are mutually proportional. It follows that **D** is therefore also proportional to **E**:

$$\mathbf{D} = \epsilon \mathbf{E}. \qquad (A1.12)$$

Like **E**, **D** extends throughout space and is in no way limited to the region occupied by the dielectric, as is **P**. The lines of **D** begin and end on free, movable charges. Those of **E** begin and end on either *free* charges or bound polarization charges. If no free charge is present, as might be the case in the vicinity of a polarized dielectric or in free space, the lines of **D** close on themselves.

Since in general the response of optical media to **B**-fields is only slightly different from that of a vacuum, we need not describe the process in detail. Suffice it to say that the material will become polarized. We can define a *magnetic polarization* or *magnetization* vector **M** as the magnetic dipole moment per unit volume. In order to deal with the influence of the magnetically polarized medium, we introduce an auxiliary vector **H**, traditionally known as the *magnetic field intensity*

$$\mathbf{H} = \mu_0^{-1}\mathbf{B} - \mathbf{M}. \qquad (A1.13)$$

For a homogeneous, linear (nonferromagnetic), isotropic medium, **B** and **H** are parallel and proportional:

$$\mathbf{H} = \mu^{-1}\mathbf{B}. \qquad (A1.14)$$

Along with Eqs. (A1.12) and (A1.14), there is one more *constitutive equation*,

$$\mathbf{J} = \sigma \mathbf{E}. \qquad (A1.15)$$

Known as *Ohm's law*, it is a statement of an experimentally determined rule that holds for conductors at constant temperatures. The electric field intensity, and therefore the force acting on each electron in a conductor, determines the flow of charge. The constant of proportionality relating **E** and **J** is the conductivity of the particular medium, σ.

Consider the rather general environment of a linear (nonferroelectric and nonferromagnetic), homogeneous, istropic medium, which is physically at rest. By making use of the constitutive relations, we can rewrite Maxwell's equations as

$$\nabla \cdot \mathbf{E} = \rho/\epsilon \qquad [A1.9]$$

$$\nabla \cdot \mathbf{B} = 0 \qquad [A1.10]$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \qquad [A1.5]$$

and

$$\nabla \times \mathbf{B} = \mu\sigma\mathbf{E} + \mu\epsilon\frac{\partial \mathbf{E}}{\partial t}. \qquad (A1.16)$$

If these expressions are somehow to yield a wave equation (2.61), we had best form some second derivatives with respect to the space variables. Taking the curl of Eq. (A1.16), we obtain

$$\nabla \times (\nabla \times \mathbf{B}) = \mu\sigma(\nabla \times \mathbf{E}) + \mu\epsilon\frac{\partial}{\partial t}(\nabla \times \mathbf{E}), \tag{A1.17}$$

where, since **E** is assumed to be a well-behaved function, the space and time derivatives can be interchanged. Equation (A1.5) can be substituted to obtain the needed second derivative with respect to time:

$$\nabla \times (\nabla \times \mathbf{B}) = -\mu\sigma\frac{\partial \mathbf{B}}{\partial t} - \mu\epsilon\frac{\partial^2 \mathbf{B}}{\partial t^2}. \tag{A1.18}$$

The vector triple product can be simplified by making use of the operator identity

$$\nabla \times (\nabla \times\ ) = \nabla(\nabla \cdot\ ) - \nabla^2 \tag{A1.19}$$

so that

$$\nabla \times (\nabla \times \mathbf{B}) = \nabla(\nabla \cdot \mathbf{B}) - \nabla^2\mathbf{B},$$

where in Cartesian coordinates

$$(\nabla \cdot \nabla)\mathbf{B} = \nabla^2\mathbf{B} = \frac{\partial^2 \mathbf{B}}{\partial x^2} + \frac{\partial^2 \mathbf{B}}{\partial y^2} + \frac{\partial^2 \mathbf{B}}{\partial z^2}.$$

Since the divergence of **B** is zero, Eq. (A1.18) becomes

$$\nabla^2\mathbf{B} = \mu\epsilon\frac{\partial^2 \mathbf{B}}{\partial t^2} - \mu\sigma\frac{\partial \mathbf{B}}{\partial t} = 0. \tag{A1.20}$$

A similar equation is satisfied by the electric field intensity. Following essentially the same procedure as above, take the curl of Eq. (A1.5):

$$\nabla \times (\nabla \times \mathbf{E}) = -\frac{\partial}{\partial t}(\nabla \times \mathbf{B}).$$

Eliminating **B** this becomes

$$\nabla \times (\nabla \times \mathbf{E}) = -\mu\sigma\frac{\partial \mathbf{E}}{\partial t} - \mu\epsilon\frac{\partial^2 \mathbf{E}}{\partial t^2},$$

and then by making use of Eq. (A1.19), we arrive at

$$\nabla^2\mathbf{E} - \mu\epsilon\frac{\partial^2 \mathbf{E}}{\partial t^2} - \mu\sigma\frac{\partial \mathbf{E}}{\partial t} = \nabla(\rho/\epsilon),$$

having utilized the fact that

$$\nabla(\nabla \cdot \mathbf{E}) = \nabla(\rho/\epsilon).$$

For an uncharged medium ($\rho = 0$) and

$$\nabla^2\mathbf{E} - \mu\epsilon\frac{\partial^2 \mathbf{E}}{\partial t^2} - \mu\sigma\frac{\partial \mathbf{E}}{\partial t} = 0. \tag{A1.21}$$

Equations (A1.20) and (A1.21) are known as the *equations of telegraphy.**

In nonconducting media $\sigma = 0$, and these equations become

$$\nabla^2\mathbf{B} - \mu\epsilon\frac{\partial^2 \mathbf{B}}{\partial t^2} = 0 \tag{A1.22}$$

$$\nabla^2\mathbf{E} - \mu\epsilon\frac{\partial^2 \mathbf{E}}{\partial t^2} = 0 \tag{A1.23}$$

and similarly

$$\nabla^2\mathbf{H} - \mu\epsilon\frac{\partial^2 \mathbf{H}}{\partial t^2} = 0 \tag{A1.24}$$

and

$$\nabla^2\mathbf{D} - \mu\epsilon\frac{\partial^2 \mathbf{D}}{\partial t^2} = 0. \tag{A1.25}$$

In the special nonconducting medium of a vacuum (free space) where

$$\rho = 0, \qquad \sigma = 0, \qquad K_e = 1, \qquad K_m = 1,$$

these equations become simply

$$\nabla^2\mathbf{E} = \mu_0\epsilon_0\frac{\partial^2 \mathbf{E}}{\partial t^2} \tag{A1.26}$$

and

$$\nabla^2\mathbf{B} = \mu_0\epsilon_0\frac{\partial^2 \mathbf{B}}{\partial t^2}. \tag{A1.27}$$

Both of these expressions describe coupled space- and time-dependent fields, and both have the form of the **differential wave equation (see Section 3.2 for further** discussion).

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* For a pair of parallel wires that might serve as a telegraph line, the finite wire resistance results in a power loss and joule heating. The electromagnetic wave advancing along the line has less and less energy available to it. The first-order time derivatives in Eqs. (A1.20) and (A1.21) arise from the conduction current and lead to the dissipation or damping.

Appendix 2 The Kirchhoff Diffraction Theory

To solve the Helmholtz equation (10.113) suppose that we have two scalar functions U_1 and U_2 for which Green's theorem is

$$\iiint_V (U_1\nabla^2 U_2 - U_2\nabla^2 U_1)dV = \oiint_S (U_1\nabla U_2 - U_2\nabla U_1)\cdot d\mathbf{S}. \tag{A2.1}$$

It is clear that if U_1 and U_2 are solutions of the Helmholtz equation, that is, if

$$\nabla^2 U_1 + k^2 U_1 = 0$$

and

$$\nabla^2 U_2 + k^2 U_2 = 0,$$

then

$$\oiint_S (U_1\nabla U_2 - U_2\nabla U_1)\cdot d\mathbf{S} = 0. \tag{A2.2}$$

Let $U_1 = \mathscr{E}$, the space portion of an unspecified scalar optical disturbance (10.112). And let

$$U_2 = \frac{e^{ikr}}{r}$$

where r is measured from a point P. Both of these choices clearly satisfy the Helmholtz equation. There is a singularity at point P, where $r = 0$, so that we surround it by a small sphere in order to exclude P from the region enclosed by S (see Fig. A2.1). Equation (A2.2) now becomes

$$\oiint_S \left[\mathscr{E}\nabla\left(\frac{e^{ikr}}{r}\right) - \frac{e^{ikr}}{r}\nabla\mathscr{E}\right]\cdot d\mathbf{S} + \oiint_{S'} \left[\mathscr{E}\nabla\left(\frac{e^{ikr}}{r}\right) - \frac{e^{ikr}}{r}\nabla\mathscr{E}\right]\cdot d\mathbf{S} = 0. \tag{A2.3}$$

Now expand out the portion of the integral corresponding to S'. On the small sphere, the unit normal $\hat{\mathbf{n}}$ points toward the origin at P, and

$$\nabla\left(\frac{e^{ikr}}{r}\right) = \left(\frac{1}{r^2} - \frac{ik}{r}\right)e^{ikr}\hat{\mathbf{n}},$$

since the gradient is directed radially outward. In terms of the solid angle ($dS = r^2\,d\Omega$) measured at P, the integral over S' becomes

$$\oiint_{S'} \left(\mathscr{E} - ik\mathscr{E}r + r\frac{\partial\mathscr{E}}{\partial r}\right)e^{ikr}\,d\Omega, \tag{A2.4}$$

where $\nabla\mathscr{E}\cdot d\mathbf{S} = -(\partial\mathscr{E}/\partial r)r^2\,d\Omega$. As the sphere surrounding P shrinks, $r \to 0$ on S' and $\exp(ikr) \to 1$. Because of the continuity of $\mathscr{E}$ its value at any point on S' approaches its value at P, that is, $\mathscr{E}_p$. The last two terms in Eq. (A2.4) go to zero, and the integral becomes $4\pi\mathscr{E}_p$. Finally then, Eq. (A2.3) becomes

$$\mathscr{E}_p = \frac{1}{4\pi}\left[\oiint_S \frac{e^{ikr}}{r}\nabla\mathscr{E}\cdot d\mathbf{S} - \oiint_S \mathscr{E}\nabla\left(\frac{e^{ikr}}{r}\right)\cdot d\mathbf{S}\right], \tag{10.114}$$

which is known as the *Kirchhoff integral theorem.*

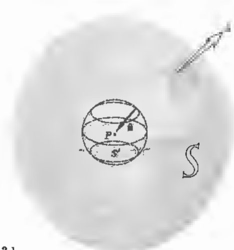


Figure A2.1

Table 1

The Sinc Function

(Sin u)/u

u	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
0.0	1.000000	0.999983	0.999933	0.999850	0.999733	0.999583	0.999400	0.999184	0.998934	[illegible]
0.1	0.998334	[illegible]	[illegible]	0.997186	0.996737	0.996254	0.995739	0.995190	0.994609	0.993994
0.2	0.993347	0.992666	0.991953	0.991207	0.990428	0.989616	0.988771	0.987894	0.986984	0.986042
0.3	0.985067	0.984060	0.983020	0.981949	0.980844	0.979708	0.978540	0.977339	0.976106	0.974842
0.4	0.973546	0.972218	0.970858	0.969467	0.968044	0.966590	0.965105	0.963588	0.962040	0.960461
0.5	0.958851	0.957210	0.955539	0.953836	0.952104	0.950340	0.948547	0.946723	0.944869	0.942985
0.6	0.941071	0.939127	0.937153	0.935150	0.933118	0.931056	0.928965	0.926845	0.924696	0.922518
0.7	0.920311	0.918076	0.915812	0.913520	0.911200	0.908852	0.906476	0.904072	0.901640	0.899181
0.8	0.896695	0.894182	0.891641	0.889074	0.886480	0.883859	0.881212	0.878539	0.875840	0.873114
0.9	0.870363	0.867587	0.864784	0.861957	0.859104	0.856227	0.853325	0.850398	0.847446	0.844471
1.0	0.841471	0.838447	0.835400	0.832329	0.829235	0.826117	0.822977	0.819814	0.816628	0.813419
1.1	0.810189	0.806936	0.803661	0.800365	0.797047	0.793708	0.790348	0.786966	0.783564	0.780142
1.2	0.776699	0.773236	0.769754	0.766251	0.762729	0.759188	0.755627	0.752048	0.748450	0.744833
1.3	0.741199	0.737546	0.733875	0.730187	0.726481	0.722758	0.719018	0.715261	0.711488	0.707698
1.4	0.703893	0.700071	0.696234	0.692381	0.688513	0.684630	0.680732	0.676819	0.672892	0.668952
1.5	0.664997	0.661028	0.657046	0.653051	0.649043	0.645022	0.640988	0.636942	0.632885	0.628815
1.6	0.624734	0.620641	0.616537	0.612422	0.608297	0.604161	0.600014	0.595858	0.591692	0.587517
1.7	0.583332	0.579138	0.574936	0.570725	0.566505	0.562278	0.558042	0.553799	0.549549	0.545291
1.8	0.541026	0.536755	0.532478	0.528194	0.523904	0.519608	0.515307	0.511001	0.506689	0.502373
1.9	0.498053	0.493728	0.489399	0.485066	0.480729	0.476390	0.472047	0.467701	0.463353	0.459002
2.0	0.454649	0.450294	0.445937	0.441579	0.437220	0.432860	0.428499	0.424137	0.419775	0.415414
2.1	0.411052	0.406691	0.402330	0.397971	0.393612	0.389255	0.384900	0.380546	0.376194	0.371845
2.2	0.367498	0.363154	0.358813	0.354475	0.350141	0.345810	0.341483	0.337161	0.332842	0.328529
2.3	0.324220	0.319916	0.315617	0.311324	0.307036	0.302755	0.298479	0.294210	0.289947	0.285692
2.4	0.281443	0.277202	0.272967	0.268741	0.264523	0.260312	0.256110	0.251916	0.247732	0.243556
2.5	0.239389	0.235231	0.231084	0.226946	0.222817	0.218700	0.214592	0.210495	0.206409	0.202334
2.6	0.198270	0.194217	0.190176	0.186147	0.182130	0.178125	0.174132	0.170152	0.166185	0.162230
2.7	0.158289	0.154361	0.150446	0.146546	0.142659	0.138786	0.134927	0.131083	0.127253	0.123439
2.8	0.119639	0.115854	0.112084	0.108330	0.104592	0.100869	0.097163	0.093473	0.089798	0.086141
2.9	0.082500	0.078876	0.075268	0.071678	0.068105	0.064550	0.061012	0.057492	0.053990	0.050506
3.0	0.047040	0.043592	0.040163	0.036753	0.033361	0.029988	0.026635	0.023300	0.019985	0.016689
3.1	0.013418	0.010157	0.006920	0.003704	0.000507	−0.002669	−0.005825	−0.008960	−0.012075	−0.015169
3.2	−0.018242	−0.021294	−0.024325	−0.027335	−0.030324	−0.033291	−0.036236	−0.039160	−0.042063	−0.044943
3.3	−0.047802	−0.050638	−0.053453	−0.056245	−0.059014	−0.061762	−0.064487	−0.067189	−0.069868	−0.072525
3.4	−0.075159	−0.077770	−0.080358	−0.082923	−0.085465	−0.087983	−0.090478	−0.092950	−0.095398	−0.097823
3.5	−0.100224	−0.102601	−0.104955	−0.107285	−0.109591	−0.111873	−0.114131	−0.116365	−0.118575	−0.120761
3.6	−0.122922	−0.125060	−0.127173	−0.129262	−0.131326	−0.133366	−0.135382	−0.137373	−0.139339	−0.141282
3.7	−0.143199	−0.145092	−0.146960	−0.148803	−0.150622	0.152416	−0.154186	−0.155930	−0.157650	−0.159345
3.8	−0.161015	−0.162661	−0.164281	−0.165877	−0.167448	−0.168994	−0.170515	−0.172011	−0.173482	−0.174929
3.9	−0.176350	−0.177747	−0.179119	−0.180466	−0.181788	−0.183086	−0.184358	−0.185606	−0.186829	−0.188027

Table 1 *(continued)*

(Sin u)/u

u	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
4.0	−0.189201	−0.190349	−0.191473	−0.192573	−0.193647	−0.194698	−0.195723	−0.196724	−0.197700	−0.198652
4.1	−0.199580	−0.200483	−0.201361	−0.202216	−0.203046	−0.203851	−0.204633	−0.205390	−0.206124	−0.206833
4.2	−0.207518	−0.208179	−0.208817	−0.209430	−0.210020	−0.210586	−0.211128	−0.211647	−0.212142	−0.212614
4.3	−0.213062	−0.213487	−0.213888	−0.214267	−0.214622	−0.214955	−0.215264	−0.215550	−0.215814	−0.216055
4.4	−0.216273	−0.216469	−0.216642	−0.216793	−0.216921	−0.217028	−0.217112	−0.217174	−0.217214	−0.217232
4.5	−0.217229	−0.217204	−0.217157	−0.217089	−0.217000	−0.216889	−0.216757	−0.216604	−0.216430	−0.216235
4.6	−0.216020	−0.215784	−0.215527	−0.215250	−0.214953	−0.214635	−0.214298	−0.213940	−0.213563	−0.213166
4.7	−0.212750	−0.212314	−0.211858	−0.211384	−0.210890	−0.210377	−0.209846	−0.209296	−0.208727	−0.208140
4.8	−0.207534	−0.206911	−0.206269	−0.205609	−0.204932	−0.204236	−0.023524	−0.202794	−0.202046	−0.201282
4.9	−0.200501	−0.199702	−0.198887	−0.198056	−0.197208	−0.196344	−0.195464	−0.194568	−0.193656	−0.192728
5.0	−0.191785	−0.190826	−0.189853	−0.188864	−0.187860	−0.186841	−0.185808	−0.184760	−0.183699	−0.182622
5.1	−0.181532	−0.180428	−0.179311	−0.178179	−0.177035	−0.175877	−0.174706	−0.173522	−0.172326	−0.171117
5.2	−0.169895	−0.168661	−0.167415	−0.166158	−0.164888	−0.163607	−0.162314	−0.161010	−0.159695	−0.158369
5.3	−0.157032	−0.155684	−0.154326	−0.152958	−0.151579	−0.150191	−0.148792	−0.147384	−0.145967	−0.144540
5.4	−0.143105	−0.141660	−0.140206	−0.138744	−0.137273	−0.135794	−0.134307	−0.132812	−0.131309	−0.129798
5.5	−0.128280	−0.126755	−0.125222	−0.123683	−0.122137	−0.120584	−0.119024	−0.117459	−0.115887	−0.114310
5.6	−0.112726	−0.111137	−0.109543	−0.107943	−0.106338	−0.104728	−0.103114	−0.101495	−0.099871	−0.098243
5.7	−0.096611	−0.094976	−0.093336	−0.091693	−0.090046	−0.088396	−0.086743	−0.085087	−0.083429	−0.081768
5.8	−0.080104	−0.078438	−0.076770	−0.075100	−0.073428	−0.071755	−0.070080	−0.068404	−0.066726	−0.065048
5.9	−0.063369	−0.061689	−0.060009	−0.058329	−0.056648	−0.054967	−0.053287	−0.051606	−0.049927	−0.048248
6.0	−0.046569	−0.044892	−0.043216	−0.041540	−0.039867	−0.038195	−0.036524	−0.034856	−0.033189	−0.031525
6.1	−0.029863	−0.028203	−0.026546	−0.024892	−0.023240	−0.021592	−0.019947	−0.018305	−0.016667	−0.015032
6.2	−0.013402	−0.011775	−0.010152	−0.008533	−0.006919	−0.005309	−0.003703	−0.002103	−0.000507	0.001083
6.3	0.002669	0.004249	0.005824	0.007393	0.008956	0.010514	0.012066	0.013612	0.015151	0.016684
6.4	0.018211	0.019731	0.021244	0.022751	0.024250	0.025743	0.027228	0.028706	0.030177	0.031640
6.5	0.033095	0.034543	0.035983	0.037414	0.038838	0.040253	0.041661	0.043059	0.044449	0.045831
6.6	0.047203	0.048567	0.049922	0.051268	0.052604	0.053931	0.055249	0.056558	0.057857	0.059146
6.7	0.060425	0.061695	0.062955	0.064204	0.065444	0.066673	0.067892	0.069101	0.070299	0.071487
6.8	0.072664	0.073830	0.074986	0.076130	0.077264	0.078386	0.079498	0.080598	0.081688	0.082765
6.9	0.083832	0.084887	0.085930	0.086962	0.087982	0.088991	0.089987	0.090972	0.091945	0.092906
7.0	0.093855	0.094792	0.095717	0.096629	0.097530	0.098418	0.099293	0.100157	0.101008	0.101846
7.1	0.102672	0.103485	0.104286	0.105074	0.105849	0.106611	0.107361	0.108098	0.108822	0.109533
7.2	0.110232	0.110917	0.111589	0.112249	0.112895	0.113528	0.114149	0.114756	0.115350	0.115931
7.3	0.116498	0.117053	0.117594	0.118122	0.118637	0.119138	0.119627	0.120102	0.120563	0.121012
7.4	0.121447	0.121869	0.122277	0.122673	0.123055	0.123423	0.123779	0.124121	0.124449	0.124765
7.5	0.125067	0.125355	0.125631	0.125893	0.126142	0.126378	0.126600	0.126809	0.127005	0.127188
7.6	0.127358	0.127514	0.127658	0.127788	0.127905	0.128009	0.128100	0.128178	0.128243	0.128295
7.7	0.128334	0.128360	0.128373	0.128373	0.128361	0.128335	0.128297	0.128247	0.128183	0.128107
7.8	0.128018	0.127917	0.127803	0.127677	0.127539	0.127388	0.127224	0.127049	0.126861	0.126661
7.9	0.126448	0.126224	0.125988	0.125739	0.125479	0.125207	0.124923	0.124627	0.124320	0.124000

Table 1 *(continued)*

(Sin u)/u

u	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
8.0	0.123670	0.123328	0.122974	0.122609	0.122232	0.121845	0.121446	0.121036	0.120615	0.120183
8.1	0.119739	0.119286	0.118821	0.118345	0.117859	0.117363	0.116855	0.116338	0.115810	0.11527[illegible]
8.2	0.114723	0.114165	0.113596	0.113018	0.112429	0.111831	0.111223	0.110605	0.109978	0.109341
8.3	0.108695	0.108040	0.107376	0.106702	0.106019	0.105327	0.104627	0.103918	0.103200	0.102473
8.4	0.101738	0.100994	0.100243	0.099483	0.098714	0.097938	0.097154	0.096362	0.095562	0.094755
8.5	0.093940	0.093117	0.092287	0.091450	0.090606	0.089755	0.088896	0.088031	0.087159	0.086280
8.6	0.085395	0.084503	0.083605	0.082701	0.081790	0.080874	0.079951	0.079023	0.078089	0.077149
8.7	0.076203	0.075253	0.074296	0.073335	0.072369	0.071397	0.070421	0.069439	0.068453	0.067463
8.8	0.066468	0.065468	0.064465	0.063457	0.062445	0.061429	0.060410	0.059386	0.058359	0.057328
8.9	0.056294	0.055257	0.054217	0.053173	0.052127	0.051077	0.050025	0.048970	0.047913	0.046853
9.0	0.045791	0.044727	0.043660	0.042592	0.041521	0.040449	0.039375	0.038300	0.037223	0.036145
9.1	0.035066	0.033985	0.032904	0.031821	0.030738	0.029654	0.028569	0.027484	0.026399	0.025313
9.2	0.024227	0.023141	0.022055	0.020970	0.019884	0.018799	0.017714	0.016630	0.015547	0.014464
9.3	0.013382	0.012301	0.011222	0.010143	0.009066	0.007990	0.006916	0.005843	0.004772	0.003703
9.4	0.002636	0.001570	0.000507	−0.000554	−0.001612	−0.002669	−0.003722	−0.004774	−0.005822	−0.006868
9.5	−0.007911	−0.008950	−0.009987	−0.011021	−0.012051	−0.013078	−0.014101	−0.015121	−0.016138	−0.017150
9.6	−0.018159	−0.019164	−0.020165	−0.021161	−0.022154	−0.023142	−0.024126	−0.025106	−0.026081	−0.027051
9.7	−0.028017	−0.028977	−0.029933	−0.030884	−0.031830	−0.032771	−0.033707	−0.034637	−0.035562	−0.036482
9.8	−0.037396	−0.038304	−0.039207	−0.040104	−0.040995	−0.041881	−0.042760	−0.043633	−0.044500	−0.045361
9.9	−0.046216	−0.047064	−0.047906	−0.048741	−0.049570	−0.050392	−0.051208	−0.052017	−0.052819	−0.053614
10.0	−0.054402	−0.055183	−0.055957	−0.056724	−0.057484	−0.058237	−0.058982	−0.059720	−0.060450	−0.061173
10.1	−0.061888	−0.062596	−0.063296	−0.063988	−0.064673	−0.065350	−0.066019	−0.066680	−0.067333	−0.067978
10.2	−0.068615	−0.069244	−0.069865	−0.070477	−0.071082	−0.071678	−0.072266	−0.072845	−0.073416	−0.073979
10.3	−0.074533	−0.075078	−0.075615	−0.076143	−0.076663	−0.077174	−0.077677	−0.078170	−0.078655	−0.079131
10.4	−0.079599	−0.080057	−0.080507	−0.080947	−0.081379	−0.081802	−0.082216	−0.082620	−0.083016	−0.083403
10.5	−0.083781	−0.084149	−0.084509	−0.084859	−0.085200	−0.085532	−0.085855	−0.086169	−0.086473	−0.086768
10.6	−0.087054	−0.087331	−0.087599	−0.087857	−0.088106	−0.088346	−0.088576	−0.088797	−0.089009	−0.089212
10.7	−0.089405	−0.089589	−0.089764	−0.089929	−0.090085	−0.090232	−0.090370	−0.090498	−0.090617	−0.090727
10.8	−0.090827	−0.090919	−0.091001	−0.091073	−0.091137	−0.091191	−0.091236	−0.091272	−0.091299	−0.091316
10.9	−0.091324	−0.091324	−0.091314	−0.091295	−0.091267	−0.091229	−0.091183	−0.091128	−0.091064	−0.090990
11.0	−0.090908	−0.090817	−0.090717	−0.090608	−0.090490	−0.090364	−0.090228	−0.090084	−0.089931	−0.089770
11.1	−0.089599	−0.089420	−0.089233	−0.089037	−0.088832	−0.088619	−0.088397	−0.088167	−0.087929	−0.087682
11.2	−0.087427	−0.087163	−0.086891	−0.086612	−0.086324	−0.086027	−0.085723	−0.085411	−0.085091	−0.084763
11.3	−0.084426	−0.084083	−0.083731	−0.083371	−0.083004	−0.082630	−0.082247	−0.081857	−0.081460	−0.081055
11.4	−0.080643	−0.080223	−0.079796	−0.079362	−0.078921	−0.078473	−0.078017	−0.077555	−0.077086	−0.076609
11.5	−0.076126	−0.075636	−0.075140	−0.074637	−0.074127	−0.073611	−0.073088	−0.072559	−0.072023	−0.071481
11.6	−0.070934	−0.070379	−0.069819	−0.069253	−0.068681	−0.068103	−0.067519	−0.066929	−0.066334	−0.065733
11.7	−0.065127	−0.064515	−0.063898	−0.063275	−0.062647	−0.062014	−0.061376	−0.060733	−0.060084	−0.059431
11.8	−0.058773	−0.058111	−0.057443	−0.056771	−0.056095	−0.055414	−0.054728	−0.054039	−0.053345	−0.052646
11.9	−0.051944	−0.051238	−0.050528	−0.049814	−0.049096	−0.048375	−0.047650	−0.046921	−0.046189	−0.045453

Table 1 *(continued)*

(Sin u)/u

u	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
12.0	−0.044714	−0.043972	−0.043227	−0.042479	−0.041727	−0.040973	−0.040216	−0.039456	−0.038694	−0.037929
12.1	−0.037161	−0.036391	−0.035618	−0.034844	−0.034067	−0.033288	−0.032506	−0.031723	−0.030938	−0.030152
12.2	−0.029363	−0.028573	−0.027781	−0.026988	−0.026193	−0.025398	−0.024600	−0.023802	−0.023003	−0.022202
12.3	−0.021401	−0.020599	−0.019796	−0.018992	−0.018188	−0.017384	−0.016578	−0.015773	−0.014967	−0.014161
12.4	−0.013355	−0.012549	−0.011743	−0.010937	−0.010131	−0.009326	−0.008521	−0.007716	−0.006912	−0.006109
12.5	−0.005306	−0.004504	−0.003702	−0.002902	−0.002103	−0.001304	−0.000507	0.000289	0.001083	0.001877
12.6	0.002668	0.003459	0.004248	0.005035	0.005820	0.006603	0.007385	0.008164	0.008942	0.009717
12.7	0.010491	0.011262	0.012030	0.012797	0.013560	0.014321	0.015080	0.015836	0.016589	0.017339
12.8	0.018087	0.018831	0.019572	0.020311	0.021046	0.021778	0.022506	0.023231	0.023953	0.024671
12.9	0.025386	0.026097	0.026804	0.027507	0.028207	0.028903	0.029594	0.030282	0.030966	0.031645
13.0	0.032321	0.032992	0.033658	0.034321	0.034978	0.035632	0.036281	0.036925	0.037564	0.038199
13.1	0.038829	0.039454	0.040075	0.040690	0.041300	0.041905	0.042506	0.043101	0.043690	0.044275
13.2	0.044854	0.045428	0.045996	0.046559	0.047117	0.047669	0.048215	0.048756	0.049291	0.049820
13.3	0.050344	0.050861	0.051373	0.051879	0.052379	0.052873	0.053361	0.053843	0.054319	0.054788
13.4	0.055252	0.055709	0.056160	0.056605	0.057043	0.057476	0.057901	0.058321	0.058733	0.059140
13.5	0.059540	0.059933	0.060320	0.060700	0.061073	0.061440	0.061800	0.062154	0.062500	0.062840
13.6	0.063174	0.063500	0.063820	0.064132	0.064438	0.064737	0.065029	0.065314	0.065593	0.065864
13.7	0.066128	[illegible]	0.066636	0.066879	0.067115	0.067344	0.067566	0.067781	0.067989	0.068190
13.8	0.068384	0.068570	0.068750	0.068922	0.069087	0.069245	[illegible]	0.069540	0.069677	0.069806
13.9	0.069929	0.070044	0.070152	0.070253	0.070346	0.070433	0.070512	0.070584	0.070649	0.070707
14.0	0.070758	0.070801	0.070838	0.070867	0.070889	0.070904	0.070912	0.070913	0.070907	0.070893
14.1	0.070873	0.070846	0.070811	0.070770	0.070721	0.070666	0.070603	0.070534	0.070457	0.070374
14.2	0.070284	0.070186	0.070082	0.069971	0.069854	0.069729	0.069598	0.069460	0.069315	0.069163
14.3	0.069005	0.068840	0.068668	0.068490	0.068305	0.068114	0.067916	0.067712	0.067501	0.067283
14.4	0.067060	0.066829	0.066593	0.066350	0.066101	0.065845	0.065584	0.065316	0.065042	0.064762
14.5	0.064476	0.064183	[illegible]	0.063581	0.063271	0.062954	0.062633	0.062305	0.061971	0.061632
14.6	0.061287	0.060936	0.060580	0.060218	0.059851	0.059478	0.059100	0.058717	0.058328	0.057933
14.7	0.057534	0.057129	0.056719	0.056304	0.055884	0.055459	0.055029	0.054594	0.054154	0.053710
14.8	0.053260	0.052806	0.052347	0.051884	0.051416	0.050944	0.050467	0.049985	0.049500	0.049010
14.9	0.048516	0.048017	0.047515	0.047008	0.046497	0.045983	0.045464	0.044942	0.044416	0.043886
15.0	0.043353	0.042815	0.042275	0.041730	0.041183	0.040632	0.040077	0.039520	0.038959	0.038395
15.1	0.037828	0.037257	0.036684	0.036108	0.035529	0.034948	0.034363	0.033776	0.033187	0.032595
15.2	0.032000	0.031403	0.030803	0.030202	0.029598	0.028992	0.028383	0.027773	0.027161	0.026547
15.3	0.025931	0.025313	0.024693	0.024072	0.023450	0.022825	0.022199	0.021572	0.020944	0.020314
15.4	0.019683	0.019051	0.018418	0.017783	0.017148	0.016512	0.015875	0.015237	0.014599	0.013960
15.5	0.013320	0.012680	0.012040	0.011399	0.010758	0.010116	0.009475	0.008833	0.008191	0.007549
15.6	0.006907	0.006266	0.005624	0.004983	0.004342	0.003702	0.003062	0.002422	0.001783	0.001145
15.7	0.000507	−0.000130	−0.000766	−0.001401	−0.002035	−0.002668	−0.003300	−0.003931	−0.004561	−0.005190
15.8	−0.005817	−0.006443	−0.007067	−0.007690	−0.008311	−0.008931	−0.009549	−0.010166	−0.010780	−0.011393
15.9	−0.012004	−0.012613	−0.013219	−0.013824	−0.014427	−0.015027	−0.015625	−0.016221	−0.016814	−0.017405

Table 1 *(continued)*

(Sin *u*)/*u*

u	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
16.0	−0.017994	−0.018580	−0.019163	−0.019744	−0.020322	−0.020898	−0.021470	−0.022040	−0.022607	−0.023170
16.1	−0.023731	−0.024289	−0.024843	−0.025395	−0.025943	−0.026488	−0.027030	−0.027568	−0.028103	−0.028634
16.2	−0.029162	−0.029686	−0.030207	−0.030724	−0.031237	−0.031747	−0.032252	−0.032754	−0.033252	−0.033746
16.3	−0.034236	−0.034722	−0.035204	−0.035682	−0.036156	−0.036626	−0.037091	−0.037552	−0.038009	−0.038461
16.4	−0.038909	−0.039352	−0.039792	−0.040226	−0.040656	−0.041081	−0.041502	−0.041918	−0.042330	−0.042737
16.5	−0.043139	−0.043536	−0.043928	−0.044315	−0.044698	−0.045076	−0.045448	−0.045816	−0.046179	−0.046536
16.6	−0.046889	−0.047236	−0.047578	−0.047915	−0.048247	−0.048574	−0.048895	−0.049212	−0.049522	−0.049828
16.7	−0.050128	−0.050423	−0.050713	−0.050997	−0.051275	−0.051548	−0.051816	−0.052078	−0.052335	−0.052586
16.8	−0.052831	−0.053071	−0.053306	−0.053535	−0.053758	−0.053975	−0.054187	−0.054393	−0.054594	−0.054789
16.9	−0.054978	−0.055161	−0.055339	−0.055511	−0.055677	−0.055837	−0.055992	−0.056141	−0.056284	−0.056421
17.0	−0.056553	−0.056678	−0.056798	−0.056912	−0.057021	−0.057123	−0.057220	−0.057310	−0.057395	−0.057475
17.1	0.057548	−0.057615	−0.057677	−0.057732	−0.057782	−0.057826	−0.057865	−0.057897	−0.057924	−0.057944
17.2	−0.057959	−0.057968	−0.057972	−0.057969	−0.057961	−0.057947	−0.057927	−0.057902	−0.057870	−0.057833
17.3	−0.057790	−0.057742	−0.057688	−0.057628	−0.057562	−0.057491	−0.057414	−0.057331	−0.057243	−0.057149
17.4	−0.057049	−0.056944	−0.056834	−0.056717	−0.056596	−0.056468	−0.056336	−0.056197	−0.056054	−0.055905
17.5	−0.055750	−0.055590	−0.055425	−0.055254	−0.055078	−0.054897	−0.054710	−0.054518	−0.054321	−0.054119
17.6	−0.053912	−0.053699	−0.053481	−0.053258	−0.053031	−0.052798	−0.052560	−0.052317	−0.052069	−0.051816
17.7	−0.051558	−0.051296	−0.051028	−0.050756	−0.050479	−0.050198	−0.049911	−0.049620	−0.049324	−0.049024
17.8	−0.048719	−0.048410	−0.048096	−0.047778	−0.047455	−0.047128	−0.046796	−0.046461	−0.046121	−0.045776
17.9	−0.045428	−0.045075	−0.044718	−0.044358	−0.043993	−0.043624	−0.043251	−0.042875	−0.042494	−0.042110
18.0	−0.041722	−0.041330	−0.040934	−0.040535	−0.040132	−0.039726	−0.039316	−0.038902	−0.038485	−0.038065
18.1	−0.037642	−0.037215	−0.036785	−0.036351	−0.035915	−0.035475	−0.035033	−0.034587	−0.034139	−0.033687
18.2	−0.033233	−0.032775	−0.032315	−0.031853	−0.031387	−0.030919	−0.030449	−0.029976	−0.029500	−0.029022
18.3	−0.028541	−0.028059	−0.027574	−0.027086	−0.026597	−0.026105	−0.025612	−0.025116	−0.024619	−0.024119
18.4	−0.023618	−0.023114	−0.022610	−0.022103	−0.021594	−0.021085	−0.020573	−0.020060	−0.019546	−0.019030
18.5	−0.018512	−0.017994	−0.017474	−0.016953	−0.016431	−0.015908	−0.015384	−0.014859	−0.014333	−0.013806
18.6	−0.013278	−0.012750	−0.012220	−0.011691	−0.011160	−0.010629	−0.010098	−0.009566	−0.009033	−0.008501
18.7	−0.007968	−0.007435	−0.006901	−0.006368	−0.005834	−0.005301	−0.004767	−0.004234	−0.003701	−0.003168
18.8	−0.002635	−0.002102	−0.001570	−0.001038	−0.000507	0.000024	0.000554	0.001083	0.001612	0.002140
18.9	0.002668	0.003194	0.003720	0.004245	0.004769	0.005292	0.005813	0.006334	0.006853	0.007371
19.0	0.007888	0.008404	0.008918	0.009431	0.009942	0.010452	0.010960	0.011466	0.011971	0.012474
19.1	0.012976	0.013475	0.013973	0.014468	0.014962	0.015454	0.015944	0.016431	0.016917	0.017400
19.2	0.017881	0.018360	0.018836	0.019310	0.019782	0.020251	0.020717	0.021181	0.021643	0.022102
19.3	0.022558	0.023011	0.023462	0.023910	0.024355	0.024797	0.025236	0.025672	0.026105	0.026535
19.4	[illegible]	0.027386	0.027807	0.028224	0.028638	0.029049	0.029457	0.029861	0.030262	0.030659
19.5	0.031053	0.031444	0.031831	0.032214	0.032594	0.032970	0.033342	0.033711	0.034076	0.034437
19.6	0.034794	0.035148	0.035497	0.035843	0.036185	0.036522	0.036856	0.037186	0.037512	0.037833
19.7	0.038151	0.038464	0.038774	0.039079	0.039379	0.039676	0.039968	0.040256	0.040540	0.040820
19.8	0.041095	0.041365	0.041632	0.041893	0.042151	0.042404	0.042652	0.042896	0.043135	0.043370
19.9	0.043600	0.043826	0.044047	0.044263	0.044475	0.044682	0.044885	0.045082	0.045275	0.045464

Adapted from L. Levi, *Applied Optics*.

Solutions to Selected Problems

CHAPTER 2

2.1 (0.003) $(2.54 \times 10^{-2})/580 \times 10^{-9}$ = number of waves = 131 $c = \nu\lambda$, $\lambda = c/v = 3 \times 10^8/10^{10}$, $\lambda = 3$ cm. Waves extend 3.9 m.

2.7 $\psi = A \sin 2\pi(\kappa x - \nu t)$, $\psi_1 = 4 \sin 2\pi(0.2x - 3t)$

a) $\nu = 3$ b) $\lambda = 1/0.2$ c) $\tau = 1/3$
d) $A = 4$ e) $v = 15$ f) positive x

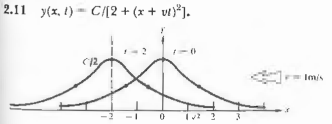
$$\psi = A \sin (kx + \omega t), \qquad \psi_2 = (1/2.5) \sin (7x + 3.5t)$$

a) $\nu = 3.5/2\pi$ b) $\lambda = 2\pi/7$ c) $\tau = 2\pi/3.5$
d) $A = 1/2.5$ e) $v = \frac{1}{2}$ f) negative x

2.9 $v_y = -\omega A \cos (kx - \omega t + \varepsilon)$, $a_y = -\omega^2 y$. Simple harmonic motion since $a_y \propto y$.

2.10 $\tau = 2.2 \times 10^{-15}$ s; therefore $\nu = 1/\tau = 4.5 \times 10^{14}$ Hz; $v = \nu\lambda$, 3×10^8 m/s $= (4.5 \times 10^{14}$ Hz$)\lambda$; $\lambda = 6.6 \times 10^{-7}$ m and $k = 2\pi/\lambda = 9.5 \times 10^6$ m^{-1}. $\psi(x, t) = (10^3$ V/m$) \cos [9.5 \times 10^6$ m$^{-1}(x + 3 \times 10^8$ m/s $t)]$. It's cosine because cos 0 = 1.

2.11 $y(x, t) = C/[2 + (x + vt)^2]$.



2.13 No, not twice differentiable (in a nontrivial way) and not a solution of the differential wave equation.

2.15

$$\psi(z, 0) = A \sin (kz + \varepsilon);$$

$$\psi(-\lambda/12, 0) = A \sin (-\pi/6 + \varepsilon) = 0.866;$$

$$\psi(\lambda/6, 0) = A \sin (\pi/3 + \varepsilon) = 1/2;$$

$$\psi(\lambda/4, 0) = A \sin (\pi/2 + \varepsilon) = 0.$$

$$A \sin (\pi/2 + \varepsilon) = A (\sin \pi/2 \cos \varepsilon + \cos \pi/2 \sin \varepsilon)$$

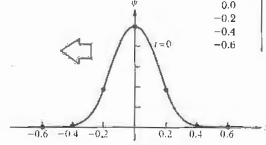
$$= A \cos \varepsilon = 0, \varepsilon = \pi/2.$$

$$A \sin (\pi/3 + \pi/2) = A \sin (5\pi/6) = 1/2;$$

therefore $A = 1$, hence $\psi(z, 0) = \sin (kz + \pi/2)$.

2.18 $\psi(x, t) = 5.0 \exp [-a(x + \sqrt{b/a}\, t)^2]$, the propagation direction is negative x; $v = \sqrt{b/a} = 0.6$ m/s. $\psi(x, 0) = 5.0 \exp (-25x^2)$;

x	ψ
0.6	0.0006
0.4	0.09
0.2	1.8
0.0	5.0
−0.2	1.8
−0.4	0.09
−0.6	0.0006



2.19 $\psi = A \exp i(k_x x + k_y y + k_z z)$

$$k_x = k\alpha \qquad k_y = k\beta \qquad k_z = k\gamma$$

$$|\mathbf{k}| = [(k\alpha)^2 + (k\beta)^2 + (k\gamma)^2]^{1/2} = k[\alpha^2 + \beta^2 + \gamma^2]^{1/2}.$$

2.20 30° corresponds to $\frac{1}{12}\lambda$ or $(1/12)3 \times 10^8/6 \times 10^{14} = 42$ nm.

2.21
$$\psi = A \sin 2\pi\left(\frac{x}{\lambda} \pm \frac{t}{\tau}\right)$$

$$\psi = 60 \sin 2\pi\left(\frac{x}{400 \times 10^{-9}} - \frac{t}{1.33 \times 10^{-15}}\right)$$

$$\lambda = 400 \text{ nm}$$

$$v = 400 \times 10^{-9}/1.33 \times 10^{-15} = 3 \times 10^8 \text{ m/s}$$

$$\nu = (1/1.33) \times 10^{+15} \text{ Hz}, \qquad \tau = 1.33 \times 10^{-15} \text{ s}.$$

2.23 $\lambda = h/mv = 6.6 \times 10^{-34}/6(1) = 1.1 \times 10^{-34}$ m.

2.24 **k** can be constructed by forming a unit vector in the proper direction and multiplying it by k. The unit vector is

$$[(4 - 0)\hat{\mathbf{i}} + (2 - 0)\hat{\mathbf{j}} + (1 - 0)\hat{\mathbf{k}}]/\sqrt{4^2 + 2^2 + 1^2}$$
$$= (4\hat{\mathbf{i}} + 2\hat{\mathbf{j}} + \hat{\mathbf{k}})/\sqrt{21}$$

and $\mathbf{k} = k(4\hat{\mathbf{i}} + 2\hat{\mathbf{j}} + \hat{\mathbf{k}})/\sqrt{21}$.

$$\mathbf{r} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$

hence $\psi(x, y, z, t) = A \sin [(4k/\sqrt{21})x + (2k/\sqrt{21})y + (k/\sqrt{21})z - \omega t]$.

2.26
$$\psi(\mathbf{r}_1, t) = \psi[\mathbf{r}_2 - (\mathbf{r}_2 - \mathbf{r}_1), t] = \psi(\mathbf{k} \cdot \mathbf{r}_1, t)$$
$$= \psi[\mathbf{k} \cdot \mathbf{r}_2 - \mathbf{k} \cdot (\mathbf{r}_2 - \mathbf{r}_1), t]$$
$$= \psi(\mathbf{k} \cdot \mathbf{r}_2, t) = \psi(\mathbf{r}_2, t)$$

since $\mathbf{k} \cdot (\mathbf{r}_2 - \mathbf{r}_1) = 0$.

CHAPTER 3

3.1 $E_y = 2 \cos [2\pi \times 10^{14}(t - x/c) + \pi/2]$

$E_y = A \cos [2\pi\nu(t - x/v) + \pi/2]$ from Eq. (2.26)

a) $\nu = 10^{14}$ Hz, $v = c$, and $\lambda = c/\nu = 3 \times 10^8/10^{14} = 3 \times 10^{-6}$ m, moves in **positive** x-**direction,** $A = 2$ V/m, $\varepsilon = \pi/2$ linearly **polarized** in y-**direction**.

b) $B_x = 0$, $B_y = 0$, $B_z = \dfrac{2}{c} \cos [2\pi \times 10^{14}(t - x/c) + \pi/2]$.

3.2 $E_z = 0$, $E_y = E_x = E_0 \sin (kz - \omega t)$ or cosine; $B_z = 0$, $B_y = -B_x = E_y/c$, or if you like,

$$\mathbf{E} = \frac{E_0}{\sqrt{2}}(\hat{\mathbf{i}} + \hat{\mathbf{j}}) \sin (kz - \omega t), \quad \mathbf{B} = \frac{E_0}{c\sqrt{2}}(\hat{\mathbf{j}} - \hat{\mathbf{i}}) \sin (kz - \omega t).$$

3.4 $\langle \cos^2 (\mathbf{k} \cdot \mathbf{r} - \omega t)\rangle = \dfrac{1}{T}\displaystyle\int_t^{t+T} \cos^2 (\mathbf{k} \cdot \mathbf{r} - \omega t')\, dt'$.

Let $\mathbf{k} \cdot \mathbf{r} - \omega t' = x$; then

$$\langle \cos^2 (\mathbf{k} \cdot \mathbf{r} - \omega t)\rangle = \frac{1}{-\omega T}\int \cos^2 x dx$$
$$= \frac{1}{-\omega T}\int \frac{1 + \cos 2x}{2} dx$$
$$= -\frac{1}{\omega T}\left[\frac{x}{2} + \frac{\sin 2x}{4}\right]_{\mathbf{k}\cdot\mathbf{r}-\omega t}^{\mathbf{k}\cdot\mathbf{r}-\omega(t+T)}$$

3.6 $\mathbf{E}_0 = (-E_0/\sqrt{2})\hat{\mathbf{i}} + (E_0/\sqrt{2})\hat{\mathbf{j}}$; $\mathbf{k} = (2\pi/\lambda)(\hat{\mathbf{i}}/\sqrt{2} + \hat{\mathbf{j}}/\sqrt{2})$; hence $\mathbf{E} = (1/\sqrt{2})(-10\hat{\mathbf{i}} + 10\hat{\mathbf{j}}) \cos [(\sqrt{2}\pi/\lambda)(x + y) - \omega t]$ and $I = \frac{1}{2}c\epsilon_0 E_0^2 = 0.13$ W/m².

3.7

a) $l = c\,\Delta t = (3.00 \times 10^8 \text{ m/s})(2.00 \times 10^{-9} \text{ s}) = 0.600$ m.

b) The volume of one pulse is $(0.600 \text{ m})(\pi R^2) = 2.945 \times 10^{-6}$ m³; therefore $(6.0 \text{ J})/2.945 \times 10^{-6} \text{ m}^3 = 2.0 \times 10^6$ J/m³.

3.8 $u = \dfrac{(\text{power})(t)}{(\text{volume})} = \dfrac{(10^{-3} \text{ W})(t)}{(\pi r^2)(ct)} = \dfrac{10^{-3} \text{ W}}{\pi(10^{-3})^2(3 \times 10^8)}$

$$u = \frac{10^{-5}}{3\pi} \text{ J/m}^3 = 1.06 \times 10^{-6} \text{ J/m}^3.$$

3.10 $h = 6.63 \times 10^{-34}$, $E = h\nu$

$$\frac{I}{h\nu} = \frac{19.88 \times 10^{-2}}{(6.63 \times 10^{-34})(100 \times 10^6)}$$
$$= 3 \times 10^{24} \text{ photons/m}^2 \text{ s}.$$

All photons in volume V cross unit area in one second

$$V = (ct)(1 \text{ m}^2) = 3 \times 10^8 \text{ m}^3$$
$$3 \times 10^{24} = V(\text{density})$$
$$\text{density} = 10^{16} \text{ photons/m}^3.$$

3.12 $P_e = iV = (0.25)(3.0) = 0.75$ W. This is the electrical power dissipated. The power available as light is

$$P_l = (0.01)P_e = 75 \times 10^{-4} \text{ W}.$$

a) Photon flux

$$= P_l/h\nu = 75 \times 10^{-4}\lambda/hc$$
$$= 75 \times 10^{-4}(550 \times 10^{-9})/(6.63 \times 10^{-34})3 \times 10^8$$
$$= 2.08 \times 10^{16} \text{ photons/s}.$$

b) There are 2.08×10^{16} in volume $(3 \times 10^8)(1\text{s}) \times (10^{-3} \text{ m}^2)$;

$$\therefore \quad \frac{2.08 \times 10^{16}}{3 \times 10^5} = \text{photons/m}^3 = 0.69 \times 10^{11}.$$

c) $I = 75 \times 10^{-4} \text{ W}/10 \times 10^{-4} \text{ m}^2 = 7.5$ W/m².

3.14 Imagine two concentric cylinders of radius r_1 and r_2 surrounding the wave. The energy flowing per second through the first cylinder must pass through the second cylinder; that is, $\langle S_1\rangle 2\pi r_1 = \langle S_2\rangle 2\pi r_2$, and so $\langle S\rangle 2\pi r =$ constant and $\langle S\rangle$ varies inversely with r. Therefore, since $\langle S\rangle \propto E_0^2$, E_0 varies as $\sqrt{1/r}$.

3.16
$$\left\langle\frac{dp}{dt}\right\rangle = \frac{1}{c}\left\langle\frac{dW}{dt}\right\rangle,$$

$A =$ area. $\quad \langle\mathcal{P}\rangle = \dfrac{1}{A}\left\langle\dfrac{dp}{dt}\right\rangle = \dfrac{1}{Ac}\left\langle\dfrac{dW}{dt}\right\rangle = \dfrac{I}{c}.$

3.18 $\mathscr{E} = 300 \text{ W}(100 \text{ s}) = 3 \times 10^4$ J,

$p = \mathscr{E}/c = 3 \times 10^4/3 \times 10^8 = 10^{-4}$ kg · m/s.

3.19

a) $\langle\mathcal{P}\rangle = 2\langle S\rangle/c = 2(1.4 \times 10^3 \text{ W/m}^2)/(3 \times 10^8 \text{ m/s}) = 9 \times 10^{-6}$ N/m².

b) S, and therefore $\mathcal{P}$, drops off with the inverse square of the distance, and hence $\langle S\rangle = [(0.7 \times 10^9 \text{ m})^{-2}/(1.5 \times 10^{11} \text{ m})^{-2}](1.4 \times 10^3 \text{ W/m}^2) = 6.4 \times 10^7$ W/m², and $\langle\mathcal{P}\rangle = 0.21$ N/m².

3.20
$$\langle S\rangle = 1400 \text{ W/m}^2,$$
$$\langle\mathcal{P}\rangle = 2(1400 \text{ W/m}^2/3 \times 10^8 \text{ m/s}) = 9.3 \times 10^{-6} \text{ N/m}^2,$$
$$\langle F\rangle = A\langle\mathcal{P}\rangle = 2000 \text{ m}^2(9.3 \times 10^{-6} \text{ N/m}^2) = 1.9 \times 10^{-2} \text{ N}.$$

3.21 $\langle S\rangle = (200 \times 10^3 \text{ W})(500 \times 2 \times 10^{-6} \text{ s})/A(1s)$,

$\langle F\rangle = A\langle\mathcal{P}\rangle = A\langle S\rangle/c = 6.7 \times 10^{-7}$ N.

3.22 $\langle F\rangle = A\langle\mathcal{P}\rangle = A\langle S\rangle/c = \dfrac{10 W}{3 \times 10^8} = 3.3 \times 10^{-8}$ N

$$a = 3.3 \times 10^{-8}/100 \text{ kg} = 3.3 \times 10^{-10} \text{ m/s}^2$$
$$v = at = \tfrac{1}{3} \times 10^{-9}(t) = 10 \text{ m/s}$$
$$t = 3 \times 10^{10} \text{ s}, \qquad 1 \text{ year} = 3.2 \times 10^7 \text{ s}.$$

3.23 **B** surrounds **v** in circles, and **E** is radial, hence **E** × **B** is tangent to the sphere, and no energy radiates outward from it.

3.25 Thermal agitation of the molecular dipoles causes a marked reduction in K_e but has little effect on n. At optical frequencies n is predominantly due to electronic polarization, rotations of the molecular dipoles having ceased to be effective at much lower frequencies.

3.26 From Eq. (3.70), for a single resonant frequency we get

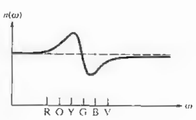
$$n = \left[1 + \frac{Nq_e^2}{\epsilon_0 m_e}\left(\frac{1}{\omega_0^2 - \omega^2}\right)\right]^{1/2};$$

since for low-density materials $n \approx 1$, the second term is $\ll 1$, and we need only retain the first two terms of the binomial expansion of n. Thus $\sqrt{1 + x} \approx 1 + x/2$ and

$$n \approx 1 + \frac{1}{2}\frac{Nq_e^2}{\epsilon_0 m_e}\left(\frac{1}{\omega_0^2 - \omega^2}\right).$$

3.28 $x_0(-\omega^2 + \omega_0^2 + i\gamma\omega) = (q_e E_0/m_e)e^{i\alpha} = (q_e E_0/m_e) \times (\cos\alpha + i \sin\alpha)$; squaring both sides yields $x_0^2[(\omega_0^2 - \omega^2)^2 + \gamma^2\omega^2] = (q_e E_0/m_e)^2(\cos^2\alpha + \sin^2\alpha)$, x_0 follows immediately. As for α, **divide** the imaginary parts of both sides of the first **equation** above, namely, $x_0\gamma\omega = (q_e E_0/m_e)\sin\alpha$, by the real parts, $x_0(\omega_0^2 - \omega^2) = (q_e E_0/m_e)\cos\alpha$ to get $\alpha = \tan^{-1}[\gamma\omega/(\omega_0^2 - \omega^2)]$. α ranges continuously from 0 to $\pi/2$ to π.

3.29 The normal order of the spectrum for a glass prism is R, O, Y, G, B, V, with red (R) deviated the least and violet (V) deviated the most. For a fuchsin prism, there is an absorption band in the green, and so the indices for yellow and blue on either side (n_Y and n_B) of it are extremes, as in Fig. 3.26, that is, n_Y is the maximum, n_B the minimum, and $n_Y > n_O > n_R > n_V > n_B$. Thus the spectrum in order of increasing deviation is B, V, black band, R, O, Y.



3.30 The phase angle is retarded by an amount $(n\,\Delta y\,2\pi/\lambda) - \Delta y\,2\pi/\lambda$ or $(n-1)\,\Delta y\,\omega/c$. Thus

$$E_p = E_0 \exp i\omega[t - (n-1)\Delta y/c - y/c]$$

or $E_p = E_0 \exp[-i\omega(n-1)\,\Delta y/c]\exp i\omega(t - y/c)$

if $n \approx 1$ or $\Delta y \ll 1$. Since $e^x \approx 1 + x$ for small x,

$$\exp[-i\omega(n-1)\Delta y/c] \approx 1 - i\omega(n-1)\Delta y/c$$

and since $\exp(-i\pi/2) = -i$,

$$E_p = E_u + \frac{\omega(n-1)\Delta y}{c} E_u e^{-i\pi/2}.$$

3.32 With ω in the visible, $(\omega_0^2 - \omega^2)$ is smaller for lead glass and larger for fused silica. Hence $n(\omega)$ is larger for the former and smaller for the latter.

3.33 C_1 is the value that n approaches as λ gets larger.

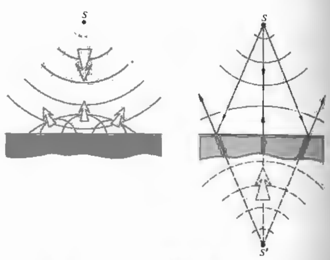
3.34 The horizontal values of $n(\omega)$ approached in each **region** between absorption bands increase as ω de**creases**.

CHAPTER 4

4.1

$$n_i \sin\theta_i = n_t \sin\theta_t$$
$$\sin 30° = 1.52 \sin\theta_t$$
$$\theta_t = \sin^{-1}(1/3.04)$$
$$\theta_t = 19°\,13'.$$

4.3

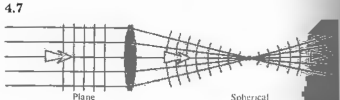


4.5 $n_{ti} = \dfrac{n_t}{n_i} = \dfrac{c/v_t}{c/v_i} = \dfrac{v_i}{v_t} = \dfrac{\nu\lambda_i}{\nu\lambda_t} = \dfrac{\lambda_i}{\lambda_t}$

therefore $\lambda_t = \lambda_i 3/4 = 9$ cm

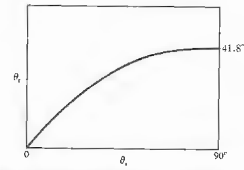
$$\sin\theta_i = n_{ti}\sin\theta_t$$
$$\sin^{-1}[\tfrac{3}{4}(0.707)] = \theta_t = 32°.$$

4.7



4.8

θ_i (degrees)	θ_t (degrees)
0	0
10	6.7
20	13.3
30	19.6
40	25.2
50	30.7
60	35.1
70	38.6
80	40.6
90	41.8



4.9 The number of waves per unit length along $\overline{AC}$ on the interface equals **$(\overline{BC}/\lambda_i)/\overline{BC}\sin\theta_i) = (\overline{AD}/\lambda_t) \times (\overline{AD}/\sin\theta_t)$. Snell's law follows on multiplying both** sides **by c/ν.**

4.12 Let τ be the time for the wave to move along a **ray from** b_1 **to b_2, from a_1 to** a_2, and from a_1 to a_3. **Thus $\overline{a_1a_2} = \overline{b_1b_2} = v_i\tau$ and $\overline{a_1a_3}$** $= v_t\tau$.

$$\sin\theta_i = \overline{b_1b_2}/\overline{a_1b_2} = v_i/\overline{a_1b_2}$$
$$\sin\theta_t = \overline{a_1a_3}/\overline{a_1b_2} = v_t/\overline{a_1b_2}$$
$$\sin\theta_r = \overline{a_1a_2}/\overline{a_1b_2} = v_i/\overline{a_1b_2}$$
$$\frac{\sin\theta_i}{\sin\theta_t} = \frac{v_i}{v_t} = \frac{n_t}{n_i} = n_{ti} \quad \text{and} \quad \theta_i = \theta_r.$$

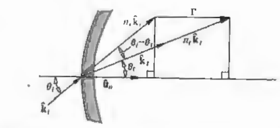
4.13

$$n_i \sin\theta_i = n_t \sin\theta_t$$
$$n_i(\hat{\mathbf{k}}_i \times \hat{\mathbf{u}}_n) = n_t(\hat{\mathbf{k}}_t \times \hat{\mathbf{u}}_n),$$

where $\hat{\mathbf{k}}_i$, $\hat{\mathbf{k}}_t$ are unit propagation vectors. Thus

$$n_t(\hat{\mathbf{k}}_t \times \hat{\mathbf{u}}_n) - n_i(\hat{\mathbf{k}}_i \times \hat{\mathbf{u}}_n) = 0$$
$$(n_t\hat{\mathbf{k}}_t - n_i\hat{\mathbf{k}}_i) \times \hat{\mathbf{u}}_n = 0.$$

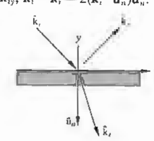
Let $n_t\hat{\mathbf{k}}_t - n_i\hat{\mathbf{k}}_i = \boldsymbol{\Gamma} = \Gamma\hat{\mathbf{u}}_n$.



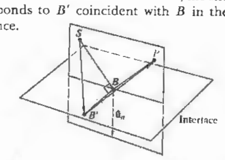
Γ is often referred to as **the** ***astigmatic constant***; Γ = the **difference between** the **projections of $n_t\hat{\mathbf{k}}_t$** and $n_i\hat{\mathbf{k}}_i$ on **$\hat{\mathbf{u}}_n$; in other words,** take **dot product $\boldsymbol{\Gamma}\cdot\hat{\mathbf{u}}_n$**:

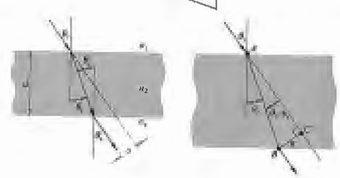
$$\Gamma = n_t\cos\theta_t - n_i\cos\theta_i.$$

4.14 Since $\theta_i = \theta_r$, $\hat{\mathbf{k}}_{ix} = \hat{\mathbf{k}}_{rx}$ and $\hat{\mathbf{k}}_{iy} = -\hat{\mathbf{k}}_{ry}$, and since $(\hat{\mathbf{k}}_i \cdot \hat{\mathbf{u}}_n)\hat{\mathbf{u}}_n = \hat{\mathbf{k}}_{iy}$, $\hat{\mathbf{k}}_i - \hat{\mathbf{k}}_r = 2(\hat{\mathbf{k}}_i \cdot \hat{\mathbf{u}}_n)\hat{\mathbf{u}}_n$.



4.15 Since $\overline{SB'} > \overline{SB}$ and $\overline{B'P} > \overline{BP}$, the shortest path corresponds to B' coincident with B in the plane of incidence.





4.18
$$n_1 \sin\theta_i = n_2 \sin\theta_t \qquad \theta_t = \theta_i'$$
$$n_2 \sin\theta_i' = n_1 \sin\theta_t'$$
$$n_1 \sin\theta_i = n_1 \sin\theta_t' \quad \text{and} \quad \theta_i = \theta_t'.$$
$$\cos\theta_t = d/\overline{AB}$$
$$\sin(\theta_i - \theta_t) = a/\overline{AB}$$
$$\sin(\theta_i - \theta_t) = \frac{a}{d}\cos\theta_t$$
$$\frac{d\sin(\theta_i - \theta_t)}{\cos\theta_t} = a.$$

4.20 Rather than propagating from point S to point P in a straight line, the ray traverses a path that crosses the plate at a sharper angle. Although in so doing the path lengths in air are slightly increased, the decrease in time spent within the plate more than compensates. This being the case, we might expect the displacement a to increase with n_{21}. As n_{21} gets larger for a given θ_i, θ_t decreases, $(\theta_i - \theta_t)$ increases, and from the results of Problem 4.18, a clearly increases.

4.21 From Eq. (4.40)
$$r_\parallel = \frac{1.52\cos 30^\circ - \cos 19^\circ 13'}{\cos 19^\circ 13' + 1.52\cos 30^\circ}$$
where from Problem 4.1 $\theta_t = 19^\circ 13'$. Similarly
$$t_\parallel = \frac{2\cos 30}{\cos 19^\circ 13' + 1.52\cos 30^\circ}$$
$$r_\parallel = \frac{1.32 - 0.944}{0.944 + 1.32} = 0.165$$
$$t_\parallel = \frac{1.732}{0.944 + 1.32} = 0.766.$$

4.22
$$\oint_C \mathbf{E}\cdot d\mathbf{l} = -\iint_A \frac{\partial \mathbf{B}}{\partial t}\cdot d\mathbf{S}. \qquad [3.5]$$
This reduces in the limit to $E_{2x}(\overline{BC}) - E_{1x}(\overline{AD}) = 0$, since area $\rightarrow 0$ and $\partial\mathbf{B}/\partial t$ is finite. Thus $E_{2x} = E_{1x}$.

4.23 Starting with Eq. (4.34), divide top and bottom by n_i and replace n_{ti} with $\sin\theta_i/\sin\theta_t$ to get
$$r_\perp = \frac{\sin\theta_t\cos\theta_i - \sin\theta_i\cos\theta_t}{\sin\theta_t\cos\theta_i + \sin\theta_i\cos\theta_t},$$
which is equivalent to Eq. (4.42). Equation (4.44) follows in exactly the same way. To find $r_\parallel$ start the same way with Eq. (4.40) and get
$$r_\parallel = \frac{\sin\theta_i\cos\theta_i - \cos\theta_t\sin\theta_t}{\cos\theta_t\sin\theta_t + \sin\theta_i\cos\theta_i}.$$
There are several routes that can be taken now: one is to rewrite $r_\parallel$ as
$$r_\parallel = \frac{(\sin\theta_i\cos\theta_t - \sin\theta_t\cos\theta_i)(\cos\theta_i\cos\theta_t - \sin\theta_i \ldots)}{(\sin\theta_i\cos\theta_t + \sin\theta_t\cos\theta_i)(\cos\theta_i\cos\theta_t + \sin\theta_i\sin \ldots)}$$
$$\text{and so } r_\parallel = \frac{\sin(\theta_i - \theta_t)\cos(\theta_i + \theta_t)}{\sin(\theta_i + \theta_t)\cos(\theta_i - \theta_t)} = \frac{\tan(\theta_i - \theta_t)}{\tan(\theta_i + \theta_t)}.$$
We can find $t_\parallel$, which has the same denominator, in a similar way.

4.24 $[E_{0r}]_\perp + [E_{0i}]_\perp = [E_{0t}]_\perp$; tangential field in incident medium equals that in transmitting medium,
$$[E_{0t}/E_{0i}]_\perp - [E_{0r}/E_{0i}]_\perp = 1, \qquad t_\perp - r_\perp = 1.$$
Alternatively, from Eqs. (4.42) and (4.44),
$$\frac{+\sin(\theta_i - \theta_t) + 2\sin\theta_t\cos\theta_i}{\sin(\theta_i + \theta_t)} \overset{?}{=} 1$$
$$\frac{\sin\theta_i\cos\theta_t - \cos\theta_i\sin\theta_t + 2\sin\theta_t\cos\theta_i}{\sin\theta_i\cos\theta_t + \cos\theta_i\sin\theta_t} = 1.$$

4.27 From Eq. (4.73) we see that the exponential will be in the form $k(x - vt)$, provided that we factor out $k_t\sin\theta_i/n_{ti}$, leaving the second term as $\omega n_{ti}t/k_t\sin\theta_i$ which must be $v_t t$. Hence $\omega n_t/(2\pi/\lambda_t)n_i\sin\theta_i = v_t$, and so $v_t = c/n_i\sin\theta_i = v_i/\sin\theta_i$.

4.28 From the defining equation (p. 107) $\beta = k_t[(\sin^2\theta_i/n_{ti}^2) - 1]^{1/2} = 3.702 \times 10^6\ \text{m}^{-1}$, and since $y\beta = 1$, $y = 2.7 \times 10^{-7}$ m.

4.29 The beam scatters off the wet paper and is mo… transmitted until the critical angle is attained, at wh… point the light is reflected back toward the source. $\tan\theta_c = (R/2)/d$, and so $n_{ti} = 1/n_i = \sin[\tan^{-1}(R/2d)]$

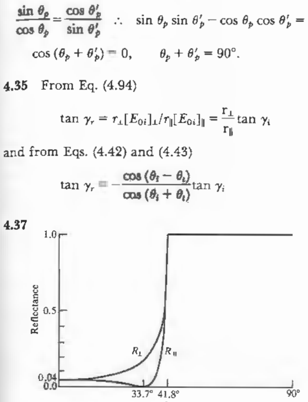
4.30 $1.00029\sin 88.7^\circ = n\sin 90^\circ$
$$(1.00029)(0.99974) = n; \qquad n = 1.00003.$$

4.32
$$\theta_i + \theta_t = 90^\circ \text{ when } \theta_i = \theta_p$$
$$n_i\sin\theta_p = n_t\sin\theta_t = n_t\cos\theta_p$$
$$\tan\theta_p = n_t/n_i = 1.52, \qquad \theta_p = 56^\circ 40' \qquad [8.25]$$

4.34
$$\tan\theta_p = n_t/n_i = n_2/n_1,$$
$$\tan\theta_p' = n_1/n_2, \qquad \tan\theta_p = 1/\tan\theta_p'.$$
$$\frac{\sin\theta_p}{\cos\theta_p} = \frac{\cos\theta_p'}{\sin\theta_p'} \quad \therefore \quad \sin\theta_p\sin\theta_p' - \cos\theta_p\cos\theta_p' = 0$$
$$\cos(\theta_p + \theta_p') = 0, \qquad \theta_p + \theta_p' = 90^\circ.$$

4.35 From Eq. (4.94)
$$\tan\gamma_r = r_\perp[E_{0i}]_\perp/r_\parallel[E_{0i}]_\parallel = \frac{r_\perp}{r_\parallel}\tan\gamma_i$$
and from Eqs. (4.42) and (4.43)
$$\tan\gamma_r = -\frac{\cos(\theta_i - \theta_t)}{\cos(\theta_i + \theta_t)}\tan\gamma_i$$

4.37



4.38 $T_\perp = \left(\dfrac{n_t\cos\theta_t}{n_i\cos\theta_i}\right)t_\perp^2$. From Eq. (4.44) and Snell's law,
$$T_\perp = \left(\frac{\sin\theta_i\cos\theta_t}{\sin\theta_t\cos\theta_i}\right)\left(\frac{4\sin^2\theta_t\cos^2\theta_i}{\sin^2(\theta_i + \theta_t)}\right) = \frac{\sin 2\theta_i\sin 2\theta_t}{\sin^2(\theta_i + \theta_t)}.$$
Similarly for $T_\parallel$.

4.40 If Φ_i is the incident radiant flux or power and T is the transmittance across the first air–glass boundary, the transmitted flux is then $T\Phi_i$. From Eq. (4.68) at normal incidence the transmittance from glass to air is also T. Thus a flux $T\Phi_i T$ emerges from the first slide, and $\Phi_i T^{2N}$ from the last one. Since $T = 1 - R$, $T_t = (1 - R)^{2N}$ from Eq. (4.67).
$$R = (0.5/2.5)^2 = 4\%, \qquad T = 96\%$$
$$T_t = (0.96)^6 \approx 78.3\%.$$

4.41 $T = \dfrac{I(y)}{I_0} = e^{-\alpha y}, \qquad T_1 = e^{-\alpha}, \qquad T = (T_1)^y.$
$$T_t = (1 - R)^{2N}(T_1)^d.$$

4.42 At $\theta_i = 0$, $R = R_\parallel = R_\perp = \left(\dfrac{n_t - n_i}{n_t + n_i}\right)^2. \qquad [4.67]$

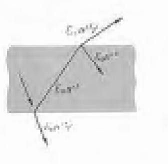
As $n_{ti} \rightarrow 1$, $n_t \rightarrow n_i$ and clearly $R \rightarrow 0$.
At $\theta_i = 0$,
$$T = T_\parallel = T_\perp \frac{4n_t n_i}{(n_t + n_i)^2}$$
and since $n_t \rightarrow n_i$, $\lim\limits_{n_{ti}\rightarrow 1} T = 4n_i^2/(2n_i)^2 = 1$.

From Problem 4.38, that is, Eqs. (4.100) and (4.101) and the fact that as $n_t \rightarrow n_i$ Snell's law says that $\theta_t \rightarrow \theta_i$, we have
$$\lim_{n_{ti}\rightarrow 1} T_\parallel = \frac{\sin^2 2\theta_i}{\sin^2 2\theta_i} = 1, \qquad \lim_{n_{ti}\rightarrow 1} T_\perp = 1.$$
From Eq. (4.43) and the fact that $R_\parallel = r_\parallel^2$ and $\theta_t \rightarrow \theta_i$, $\lim\limits_{n_{ti}\rightarrow 1} R_\parallel = 0$.

Similarly from Eq. (4.42) $\lim\limits_{n_{ti}\rightarrow 1} R_\perp = 0$.

4.44 For $\theta_i > \theta_c$, Eq. (4.70) can be written
$$r_\perp = \frac{\cos\theta_i - i(\sin^2\theta_i - n_{ti}^2)^{1/2}}{\cos\theta_i + i(\sin^2\theta_i - n_{ti}^2)^{1/2}}$$
$$r_\perp r_\perp^* = \frac{\cos^2\theta_i + \sin^2\theta_i - n_{ti}^2}{\cos^2\theta_i + \sin^2\theta_i - n_{ti}^2} = 1.$$
Similarly $r_\parallel r_\parallel^* = 1$.

4.45



$$t_{\parallel} = \frac{2 \sin \theta_2 \cos \theta_1}{\sin (\theta_1 + \theta_2) \cos (\theta_1 - \theta_2)}$$

$$t'_{\parallel} = \frac{2 \sin \theta_1 \cos \theta_2}{\sin (\theta_1 + \theta_2) \cos (\theta_2 - \theta_1)}$$

$$t_{\parallel} t'_{\parallel} = \frac{\sin 2\theta_1 \sin 2\theta_2}{\sin^2 (\theta_1 + \theta_2) \cos^2 (\theta_1 - \theta_2)}$$

$= T_{\parallel}$ from Eq. (4.100).

Similarly $t_{\perp} t'_{\perp} = T_{\perp}$

$$r_{\parallel}^2 = \left[\frac{\tan (\theta_1 - \theta_2)}{\tan (\theta_1 + \theta_2)}\right]^2 = \left[\frac{-\tan (\theta_2 - \theta_1)}{\tan (\theta_1 + \theta_2)}\right]^2$$

$$r_{\parallel}'^2 = \left[\frac{\tan (\theta_2 - \theta_1)}{\tan (\theta_1 + \theta_2)}\right]^2 = r_{\parallel}^2 = R_{\parallel}.$$

4.47 From Eq. (4.45)

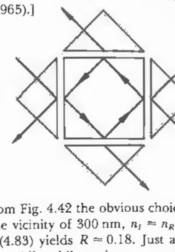
$$t'_{\parallel}(\theta'_p) t_{\parallel}(\theta_p) = \left[\frac{2 \sin \theta_p \cos \theta'_p}{\sin (\theta_p + \theta'_p) \cos (\theta'_p - \theta_p)}\right] \times \left[\frac{2 \sin \theta'_p \cos \theta_p}{\sin (\theta_p + \theta'_p) \cos (\theta_p - \theta'_p)}\right]$$

$$= \frac{\sin 2\theta'_p \sin 2\theta_p}{\cos^2 (\theta_p - \theta'_p)} \quad \text{since} \quad \theta_p + \theta'_p = 90°$$

$$= \frac{\sin^2 2\theta_p}{\cos^2 (\theta_p - \theta'_p)} \quad \text{since} \quad \sin 2\theta'_p = \sin 2\theta_p$$

$$= \frac{\sin^2 2\theta_p}{\cos^2 (2\theta_p - 90°)} = 1.$$

4.48 Gan be used as mixer to get various proportions of the two incident waves in the emitted beams. This could be done by adjusting gaps. [For some further remarks, see H. A. Daw and J. R. Izatt, *J. Opt. Soc. Am.* 55, 201 (1965).]



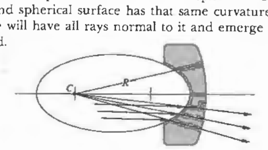
4.49 From Fig. 4.42 the obvious choice is silver. Note that in the vicinity of 300 nm, $n_I \approx n_R \approx 0.6$, in which case Eq. (4.83) yields $R \approx 0.18$. Just above 300 nm n_I increases rapidly, while n_R decreases quite strongly, with the result that $R \approx 1$ across the visible and then some.

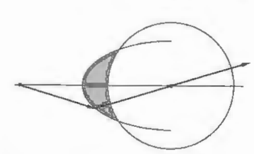
4.50 Light traverses the base of the prism as an evanescent wave, which propagates along the adjustable coupling gap. Energy moves into the dielectric film when the evanescent wave meets certain requirements. The film acts like a waveguide, which will support characteristic vibration configurations or modes. Each mode has associated with it a given speed and polarization. The evanescent wave will couple into the film when it matches a mode configuration.

CHAPTER 5

5.1 From (5.2), $\ell_o + \ell_i 3/2 =$ constant, $5 + (6)3/2 = 14$. Therefore $2\ell_o + 3\ell_i = 28$ when $\ell_o = 6$, $\ell_i = 5.3$, $\ell_o = 7$, $l_i = 4.66$. Note that the arcs centered on S and P have to intercept for physically meaningful values of ℓ_o and ℓ_i.

5.3 From Fig. 5.4(b) a plane wave impinging on a concave elliptical surface becomes spherical. If the second spherical surface has that same curvature, the wave will have all rays normal to it and emerge unaltered.





5.5 First surface: $\frac{n_1}{s_o} + \frac{n_2}{s_i} = \frac{n_2 - n_1}{R}$.

$$\frac{1}{1.2} + \frac{1.5}{s_i} = \frac{0.5}{0.1}.$$

$s_i = 0.36$ m (real image 0.36 m to the right of first vertex). Second surface $s_o = 0.20 - 0.36 = -0.16$ m (virtual object distance).

$$\frac{1.5}{-0.16} + \frac{1}{s_i} = \frac{-0.5}{-0.1}, \qquad s_i = 0.069.$$

Final image is real ($s_i > 0$), inverted ($M_T < 0$), and 6.9 cm to the right of the second vertex.

5.6 $s_o + s_i = s_o s_i / f$ to minimize $s_o + s_i$,

$$\frac{d}{ds_o}(s_o + s_i) = 0 = 1 + \frac{ds_i}{ds_o}$$

$$\text{or} \quad \frac{d}{ds_o}\left(\frac{s_o s_i}{f}\right) = \frac{s_i}{f} + \frac{s_o}{f}\frac{ds_i}{ds_o} = 0.$$

Thus $\frac{ds_i}{ds_o} = -1$ and $\frac{ds_i}{ds_o} = -\frac{s_i}{s_o}$, $\therefore s_i = s_o$.

The separation would be maximum if either were ∞, but both could not be. Hence, $s_i = s_o$ is the condition for a minima. From Gaussian equation, $s_o = s_i = 2f$.

5.7 From (5.8), $1/8 + 1.5/s_i = 0.5/{-20}$. At first surface, $s_i = -10$ cm. Virtual image 10 cm to left of first vertex. At second surface, object is *real* 15 cm from second vertex.

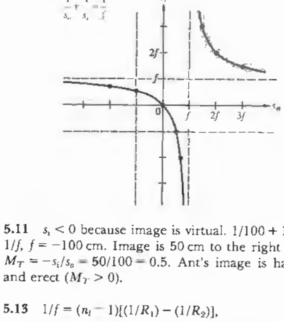
$$1.5/15 + 1/s_i = -0.5/10, \qquad s_i = -20/3 = -6.66 \text{ cm}.$$

Virtual, to left of second vertex.

5.9 $1/5 + 1/s_i = 1/10$, $s_i = -10$ cm virtual, $M_T = -s_i/s_o = 10/5 = 2$ erect. Image is 4 cm high. Or $-5(x_i) = 100$, $x_i = -20$, $M_T = -x_i/f = 20/10 = 2$.

5.10 $1/s_o + 1/s_i = 1/f$

s_o	0	f	∞	$2f$	$3f$	$-f$	$-2f$	$f/2$
s_i	0	∞	f	$2f$	$f3/2$	$f/2$	$f2/3$	$-f$



5.11 $s_i < 0$ because image is virtual. $1/100 + 1/{-50} = 1/f$, $f = -100$ cm. Image is 50 cm to the right as well. $M_T = -s_i/s_o = 50/100 = 0.5$. Ant's image is half-sized and erect ($M_T > 0$).

5.13 $1/f = (n_l - 1)[(1/R_1) - (1/R_2)]$,

$$= 0.5[(1/\infty) - (1/10)] = -0.5/10,$$

$$f = -20 \text{ cm}, \qquad \mathscr{D} = 1/f = -1/0.2 = -5 \text{ D}.$$

5.16

a) From the Gaussian lens equation

$$\frac{1}{15.0\text{ m}}+\frac{1}{s_i}=\frac{1}{3.00\text{ m}}$$

and $s_i = +3.75$ m.

b) Computing the magnification, we obtain

$$M_T=-\frac{s_i}{s_o}=-\frac{3.75\text{ m}}{15.0\text{ m}}=-0.25.$$

Because the image distance is positive, the image is *real*. Because the magnification is negative, the image is *inverted*, and because the absolute value of the magnification is less than one, the image is *minified*.

c) From the definition of magnification, it follows that

$$y_i = M_T y_o = (-0.25)(2.25\text{ m}) = -0.563\text{ m},$$

where the minus sign reflects the fact that the image is inverted.

d) Again from the Gaussian equation

$$\frac{1}{17.5\text{ m}}+\frac{1}{s_i}=\frac{1}{3.00\text{ m}}$$

and $s_i = +3.62$ m. The entire equine image is only 0.13 m long.

5.20 The first thing to find is the focal length in water, using the lensmaker's formula. Taking the ratio $f_w/f_a = f_w/(10\text{ cm}) = (n_g - 1)/[(n_g/n_w) - 1] = 0.56/0.17 = 3.24$; $f_w = 32$ cm. The Gaussian lens formula gives the image distance: $1/s_i + 1/100\text{ cm} = 1/32.4\text{ cm}$; $s_i = 48$ cm.

5.21 The image will be inverted if it's to be real, so the set must be upside down or else something more will be needed to flip the image; $M_T = -3 = -s_i/s_o$; $1/s_o + 1/3s_o = 1/0.60\text{ m}$; $s_o = 0.80$ m, hence $0.80\text{ m} + 3(0.80\text{ m}) = 3.2$ m.

5.22

$$\frac{1}{f}=(n_{lm}-1)\left(\frac{1}{R_1}-\frac{1}{R_2}\right),$$

$$\frac{1}{f_w}=\frac{(n_{lm}-1)}{(n_l-1)}\frac{1}{f_a}=\frac{1.5/1.33-1}{1.5-1}\frac{1}{f_a}=\frac{0.125}{0.5}\frac{1}{f_a},$$

$$f_w = 4f_a$$

5.24 $1/f = 1/f_1 + 1/f_2$, $1/50 = 1/f_1 - 1/50$, $f_1 = 25$ cm. If R_{11} and R_{12}, and R_{21} and R_{22} are the radii of the first and second lenses,

$$1/f_1 = (n_l - 1)(1/R_{11} - 1/R_{12}), \qquad 1/25 = 0.5(2/R_{11}),$$

$$R_{11} = -R_{12} = -R_{21} = 25\text{ cm},$$

$$1/f_2 = (n_l - 1)(1/R_{21} - 1/R_{22}),$$

$$-1/50 = 0.55(1/-25 - 1/R_{22}),$$

$$R_{22} = -275\text{ cm}.$$

5.25

$$M_{T_1} = -s_{i1}/s_{o1} = -f_1/(s_{o1} - f_1)$$

$$M_{T_2} = -s_{i2}/s_{o2} = -s_{i2}/(d - s_{i1})$$

$$M_T = f_1 s_{i2}/(s_{o1} - f_1)(d - s_{i1}).$$

From (5.30), on substituting for s_{i1}, we have

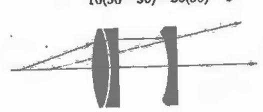
$$M_T = \frac{f_1 s_{i2}}{(s_{o1} - f_1)d - s_{o1}f_1}.$$

5.26 First lens $1/s_{i1} = 1/30 - 1/30 = 0$, $s_{i1} = \infty$. Second lens $1/s_{i2} = 1/(-20) - 1/(-\infty)$, the object for the second lens is to the right at ∞, that is, $s_{o2} = -\infty$. $s_{i2} = -20$ cm, virtual, 10 cm to the left of first lens.

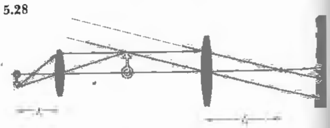
$$M_T = (-\infty/30)(+20/-\infty) = \frac{2}{3}$$

or from (5.34)

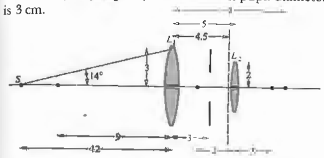
$$M_T = \frac{30(-20)}{10(30-30)-30(30)} = \frac{2}{3}.$$



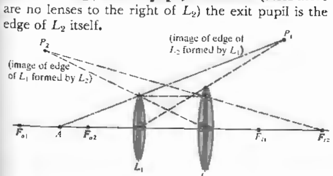
5.28



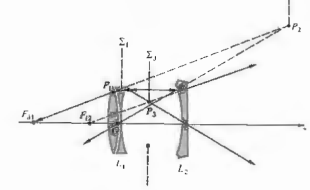
5.30 The angle subtended by L_1 at S is $\tan^{-1} 3/12 = 14°$. To find the image of the diaphragm in L_1 we use Eq. (5.23): $x_o x_i = f^2$, $(-6)(x_i) = 81$, $x_i = -13.5$ cm, so that the image is 4.5 cm behind L_1. The magnification is $-x_i/f = 13.5/9 = 1.5$, and thus the image (of the edge) of the hole is $(0.5)(1.5) = 0.75$ cm in radius. Hence the angle subtended at S is $\tan^{-1} 0.75/16.5 = 2.6°$. The image of L_2 in L_1 is obtained from $(-4)(x_i) = 81$, $x_i = -20.2$ cm, in other words, the image is 11.2 cm to the right of L_1. $M_T = 20.2/9 = 2.2$; hence the edge of L_2 is imaged 4.4 cm above the axis. Thus its subtended angle at S is $\tan^{-1} 4.4/(12 + 11.2)$ or 9.8°. Accordingly, the diaphragm is the A.S., and the entrace pupil (its image in L_1) has a diameter of 1.5 cm at 4.5 cm behind L_1. The image of the diaphragm in L_2 is the exit pupil. Consequently, $\frac{1}{2} + 1/s_i = \frac{1}{3}$ and $s_i = -6$, that is, 6 cm in front of L_2. $M_T = \frac{6}{2} = 3$, so that the exit pupil diameter is 3 cm.



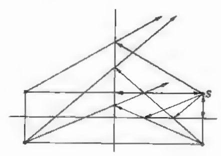
5.31 Either the margin of L_1 or L_2 will be the A.S.; thus, since no lenses are to the left of L_1, either its periphery or P_1 corresponds to the entrance pupil. Beyond (to the left of) point A, L_1 subtends the smallest angle and is the entrance pupil; nearer in (to the right of A), P_1 marks the edge of the entrance pupil. In the former case P_2 is the exit pupil; in the latter (since there are no lenses to the right of L_2) the exit pupil is the edge of L_2 itself.



5.32 The A.S. is either the edge of L_1 or L_2. Thus the entrance pupil is either marked by P_1 or P_2. Beyond F_{o1}, P_1 subtends the smaller angle; thus Σ_1 locates the A.S. The image of the A.S. in the lenses to its right, L_2, locates P_3 as the exit pupil.



5.33



5.35 $1/s_o + 1/s_i = -2/R$. Let $R \to \infty$: $1/s_o + 1/s_i = 0$, $s_o = -s_i$, and $M_T = +1$. Image is virtual, same size, and erect.

5.36 From Eq. (5.49), $1/100 + 1/s_i = -2/80$, and so $s_i = -28.5$ cm. Virtual ($s_i < 0$), erect ($M_T > 0$), and minified. (Check with Table 5.5.)

5.38 Image on screen must be real ∴ s_i is +

$$\frac{1}{25}+\frac{1}{100}=-\frac{2}{R}, \qquad \frac{5}{100}=-\frac{2}{R}, \qquad R=-40\text{ cm}.$$

5.39 The image is erect and minified. That implies (Table 5.5) a convex spherical mirror.

5.40 No—although she might be looking at you.

5.41 The mirror is parallel to the plane of the painting, and so the girl's image should be directly behind her and not off to the right.

5.43 To be magnified and erect the mirror must be concave, and the image virtual; $M_T = 2.0 = s_i/(0.015\text{ m})$, $s_i = -0.03$ m, and hence $1/f = 1/0.015\text{ m} + 1/{-0.03}\text{ m}$; $f = 0.03$ m and $f = -R/2$; $R = -0.06$ m.

5.44 $M_T = y_i/y_o = -s_i/s_o$, using Eq. (5.50), $s_i = fs_o/(s_o - f)$, and since $f = -R/2$, $M_T = -f/(s_o - f) = -(-R/2)/(s_o + R/2) = R/(2s_o + R)$.

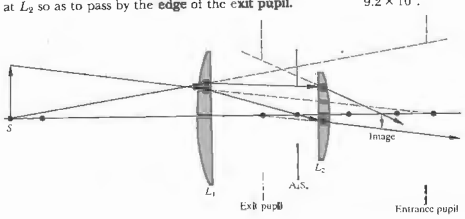
5.47 $M_T = -s_i/25\text{ cm} = -0.064$; $s_i = 1.6$ cm. $1/25\text{ cm} + 1/1.6\text{ cm} = -2/R$, $R = -3.0$ cm.

5.51 $f = -R/2 = 30$ cm, $1/20 + 1/s_i = 1/30$, $1/s_i = 1/30 - 1/20$.

$$s_i = -60\text{ cm},\ M_T = -s_i/s_o = 60/20 = 3.$$

Image is virtual ($s_i < 0$), erect ($M_T > 0$), located 60 cm behind mirror, and 9 inches tall.

5.53 Draw the chief ray from the tip to L_1 such that when extended it passes through the center of the entrance pupil. From there it goes through the center of the A.S., and then it bends at L_2 so as to extend through the center of the exit pupil. A marginal ray from S extends to the edge of the entrance pupil, bends at L_1 so it just misses the edge of A.S., and then bends at L_2 so as to pass by the edge of the exit pupil.



5.54

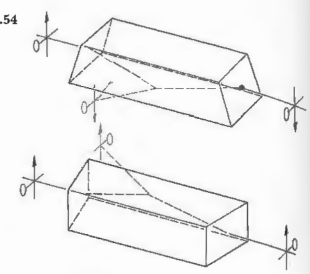


Image rotated through 180°.

5.55 From Eq. (5.64)

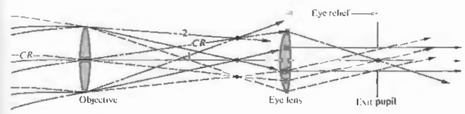
$$\text{NA} = (2.624 - 2.310)^{1/2} = 0.550,$$

$$\theta_{max} = \sin^{-1} 0.550 = 33°22'.$$

Maximum acceptance angle is $2\theta_{max} = 66°44'$. A ray at 45° would quickly leak out of the fiber; in other words, very little energy fails to escape, even at the first reflection.

5.56 Considering Eq. (5.65) (p. 174), $\log 0.5 = -0.30 = -\alpha L/10$, and so $L = 15$ km.

5.57 From Eq. (5.64) (p. 171) NA = 0.232 and $N_m = 9.2 \times 10^2$.



5.59 $M_T = -f/x_o = -1/x_o\mathscr{D}$. For the human eye $\mathscr{D} \approx 58.6$ diopters.

$$x_o = 230{,}000 \times 1.61 = 371 \times 10^3\text{ km}$$

$$M_T = -1/3.71 \times 10^6(58.6) = 4.6 \times 10^{-11}$$

$$y_i = 2160 \times 1.61 \times 10^3 \times 4.6 \times 10^{-11} = 0.16\text{ mm}.$$

5.61 $1/20 + 1/s_{io} = 1/4$, $s_{io} = 5$ m.

$$1/0.3 + 1/s_{ie} = 1/0.6,\quad s_{ie} = -0.6\text{ m}.$$

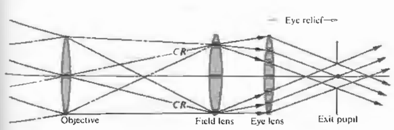
$$M_{To} = -5/10 = -0.5$$

$$M_{Te} = -(-0.6)/0.5 = +1.2$$

$$M_{To}M_{Te} = -0.6.$$

5.64 Ray 1 in the figure above misses the eye-lens, and there is, therefore, a decrease in the energy arriving at the corresponding image point. This is vignetting.

5.65 Rays that would have missed the eye-lens in the previous problem are made to pass through it by the field-lens. Note how the field-lens bends the chief rays a bit so that they cross the optical axis slightly closer to the eye-lens, thereby moving the exit pupil and shortening the eye relief. (For more on the subject, see *Modern Optical Engineering*, by Smith.)



5.69 $$\mathscr{D}_l = \frac{\mathscr{D}_c}{1 + \mathscr{D}_c d} = \frac{3.2D}{1 + (3.2D)(0.017\text{ m})} = +3.03D$$

or to two figures $+3.0D$. $f_l = 0.330$ m, and so the far point is $0.330\text{ m} - 0.017\text{ m} = 0.313$ m behind the eye lens. For the contact lens $f_c = 1/3.2 = 0.313$ m. Hence the far point at 0.31 m is the same for both, as it indeed must be.

5.71

a) The intermediate image-distance is obtained from the lens formula applied to the objective;

$$\frac{1}{27\text{ mm}} + \frac{1}{s_i} = \frac{1}{25\text{ mm}}$$

and $s_i = 3.38 \times 10^2$ mm. This is the distance from the objective to the intermediate image, to which must be added the focal length of the eyepiece to get the lens separation; $3.38 \times 10^2\text{ mm} + 25\text{ mm} = 3.6 \times 10^2$ mm.

b) $M_{To} = -s_i/s_o = -3.38 \times 10^2\text{ mm}/27\text{ mm} = -12.5\times$, while the eyepiece has a magnification of $d_o\mathscr{D} = (254\text{ mm})(1/25\text{ mm}) = 10.2\times$. Thus the total magnification is MP $= (-12.5)(10.2) = -1.3 \times 10^2$; the minus sign just means the image is inverted.

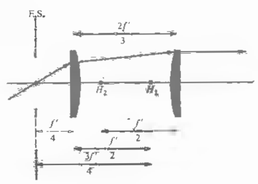
CHAPTER 6

6.2 From Eq. (6.8),

$$1/f = 1/f' + 1/f' - d/f'f' = 2/f' - 2/3f', \qquad f = 3f'/4.$$

From Eq. (6.9), $\overline{H_{11}H_1} = (3f'/4)(2f'/3)/f' = f'/2$.

From Eq. (6.10), $\overline{H_{22}H_2} = -(3f'/4)(2f'/3)/f' = -f'/2$.



6.3 From Eq. (6.2), $1/f = 0$ when $-(1/R_1 - 1/R_2) = (n_l - 1)d/n_lR_1R_2$. Thus $d = n_l(R_1 - R_2)/(n_l - 1)$.

6.4 $1/f = 0.5[1/6 - 1/10 + 0.5(3)/1.5(6)10]$

$$= 0.5[10/60 - 6/60 + 1/60];\ f = +24;$$

$$h_1 = -24(0.5)(3)/10(1.5) = -2.4,$$

$$h_2 = -24(0.5)(3)/6(1.5) = -4.$$

6.5 $f = \frac{1}{2}nR/(n-1);\ h_1 = +R,\ h_2 = -R.$

6.9 $f = 29.6 + 0.4 = 30$ cm; $s_o = 49.8 + 0.2 = 50$ cm; $1/50 + 1/s_i = 1/30$ cm. $s_i = 75$ cm from H_2 and 74.6 cm from the back face.

6.11 From Eq. (6.2),

$$1/f = \tfrac{1}{2}[(1/4.0) - (1/-15) + \tfrac{1}{2}(4.0)/(3/2)(4.0)(-15)]$$

$$= 0.147 \quad \text{and} \quad f = 6.8 \text{ cm}.$$

$h_1 = -(6.8)\frac{1}{2}(4.0)/(-15)(3/2) = +0.60$ cm, while $h_2 = -2.3$. To find the image $1/(100.6) + 1/s_i = 1/(6.8)$; $s_i = 7.3$ cm or 5 cm from the back face of the lens.

6.16 $h_1 = n_{i1}(1 - a_{11})/-a_{12} = (\mathscr{D}_2 d_{21}/n_{t1})f$

$$= -(n_{t1} - 1)d_{21}f/R_2 n_{t1},$$

from Eq. (5.64) where $n_{t1} = n_t$;

$$h_2 = n_{t2}(a_{22} - 1)/-a_{12}$$

$$= -(\mathscr{D}_1 d_{21}/n_{t1})f \text{ from Eq. (5.70)},$$

$$= -(n_{t1} - 1)d_{21}f/R_1 n_{t1}.$$

6.17 $\mathscr{A} = \mathscr{R}_2\mathscr{T}_{21}\mathscr{R}_1$, but for the planar surface

$$\mathscr{R}_2 = \begin{bmatrix} 1 & -\mathscr{D}_2 \\ 0 & 1 \end{bmatrix}$$

and $\mathscr{D}_2 = (n_{t1} - 1)/-R_2$ but $R_2 = \infty$

$$\mathscr{R}_2 = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

which is the unit matrix, hence $\mathscr{A} = \mathscr{T}_{21}\mathscr{R}_1$.

6.18 $\mathscr{D}_1 = (1.5 - 1)/0.5 = 1$

and $\mathscr{D}_2 = (1.5 - 1)/-(-0.25) = 2$

$$\mathscr{A} = \begin{bmatrix} 1 - 2(0.3)/1.5 & -1 + 2(1)(0.3)/(1.5 - 2) \\ 0.3/1.5 & -1(0.3)/1.5 + 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0.6 & -2.6 \\ 0.2 & 0.8 \end{bmatrix}$$

$$|\mathscr{A}| = 0.6(0.8) - (0.2)(-2.6) = 0.48 + 0.52 = 1.$$

6.22 See E. Slayter, *Optical Methods in Biology*. $\overline{PC}/\overline{CA} = (n_1/n_2)R/R = n_1/n_2$, while $\overline{CA}/\overline{P'C} = n_1/n_2$. Therefore triangles ACP and ACP' are similar; using the sine law

$$\frac{\sin \measuredangle PAC}{\overline{PC}} = \frac{\sin \measuredangle APC}{\overline{CA}}$$

or

$$n_2 \sin \measuredangle PAC = n_1 \sin \measuredangle APC,$$

but $\theta_i = \measuredangle PAC$, thus $\theta_t = \measuredangle APC = \measuredangle P'AC$, and the refracted ray appears to come from P'.

6.23 From Eq. (5.6), let $\cos\varphi = 1 - \varphi^2/2$; then

$$\ell_o = [R^2 + (s_o + R)^2 - 2R(s_o + R) + R(s_o + R)\varphi^2]^{1/2},$$

$$\ell_o^{-1} = [s_o^2 + R(s_o + R)\varphi^2]^{-1/2},$$

$$\ell_i^{-1} = [s_i^2 - R(s_i - R)\varphi^2]^{-1/2},$$

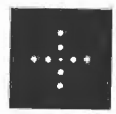
where the first two terms of the binomial series are used,

$$\ell_o^{-1} \approx s_o^{-1} - (s_o + R)h^2/2s_o^3R \quad \text{where } \varphi \approx h/R,$$

$$\ell_i^{-1} \approx s_i^{-1} + (s_i - R)h^2/2s_i^3R.$$

Substituting into Eq. (5.5) leads to Eq. (6.40).

6.24



CHAPTER 7

7.1 $E_0^2 = 36 + 64 + 2 \cdot 6 \cdot 8 \cos \pi/2 = 100, \quad E_0 = 10;$

$$\tan\alpha = \tfrac{8}{6}, \quad \alpha = 53.1° = 0.93 \text{ rad}.$$

$$E = 10 \sin(120\pi t + 0.93).$$

7.5 $\dfrac{1 \text{ m}}{500 \text{ nm}} = 0.2 \times 10^7 = 2{,}000{,}000$ waves.

$$\text{In the glass } \frac{\mathbf{0.05}}{\boldsymbol{\lambda_0/n}} = \frac{\mathbf{0.05(1.5)}}{\mathbf{500\ nm}} = 1.5 \times 10^5;$$

$$\text{in air } \frac{0.95}{\lambda_0} = 0.19 \times 10^7;$$

total 2,050,000 waves.
OPD = [(1.5)(0.05) + (1)(0.95)] − (1)(1)
OPD = 1.025 − 1.000 = 0.025 m

$$\frac{\Lambda}{\lambda_0} = \frac{\mathbf{0.025}}{\mathbf{500\ nm}} = 5 \times 10^4 \text{ waves}.$$

7.8 $E = E_1 + E_2 = E_{01}\{\sin[\omega t - k(x + \Delta x)]$

$$+ \sin(\omega t - kx)\}.$$

Since $\sin\beta + \sin\gamma = 2\sin\frac{1}{2}(\beta + \gamma)\cos\frac{1}{2}(\beta - \gamma)$,

$$E = 2E_{01}\cos\frac{k\,\Delta x}{2}\sin\left[\omega t - k\left(x + \frac{\Delta x}{2}\right)\right].$$

7.9 $E = E_0 \,\text{Re}\,[e^{i(kx+\omega t)} - e^{i(kx-\omega t)}]$

$$= E_0\,\text{Re}\,[e^{ikx}(e^{i\omega t} - e^{-i\omega t})]$$

$$= E_0\,\text{Re}\,[e^{ikx}2i \sin\omega t]$$

$$= E_0\,\text{Re}\,[2i\cos kx \sin\omega t - 2\sin kx \sin\omega t]$$

and $E = -2E_0 \sin kx \sin\omega t$. Standing wave with node at $x = 0$.

7.10 $\dfrac{\partial E}{\partial x} = -\dfrac{\partial B}{\partial t}.$

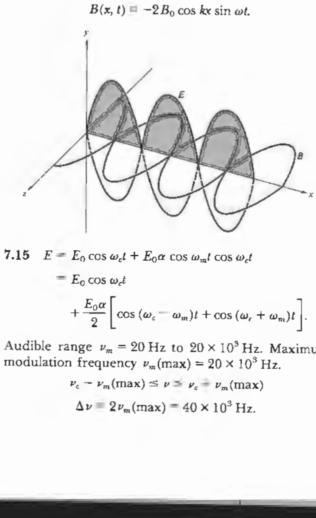
Integrate to get

$$B(x,t) = -\int \frac{\partial E}{\partial x}\,dt = -2E_0 k \cos kx \int \cos\omega t\,dt$$

$$= -\frac{2E_0 k}{\omega}\cos kx \sin\omega t.$$

But $E_0k/\omega = E_0/c = B_0$; thus

$$B(x,t) = -2B_0 \cos kx \sin\omega t.$$



7.15 $E = E_0 \cos\omega_c t + E_0\alpha \cos\omega_m t \cos\omega_c t$

$$= E_0 \cos\omega_c t + \frac{E_0\alpha}{2}\left[\cos(\omega_c - \omega_m)t + \cos(\omega_c + \omega_m)t\right].$$

Audible range $\nu_m = 20$ Hz to 20×10^3 Hz. Maximum modulation frequency $\nu_m(\text{max}) = 20 \times 10^3$ Hz.

$$\nu_c - \nu_m(\text{max}) \leq \nu \leq \nu_c + \nu_m(\text{max})$$

$$\Delta\nu = 2\nu_m(\text{max}) = 40 \times 10^3 \text{ Hz}.$$

7.16 $v = \omega/k = ak, \qquad v_g = d\omega/dk = 2ak = 2v.$

7.17

$$v = \sqrt{\frac{g\lambda}{2\pi}} = \sqrt{g/k}$$

$$v_g = v + k\frac{dv}{dk} \qquad [7.38]$$

$$\frac{dv}{dk} = -\frac{1}{2k}\sqrt{\frac{g}{k}} = -\frac{v}{2k}$$

$$v_g = v/2.$$

7.19 $v_g = v + k\dfrac{dv}{dk}$ and $\dfrac{dv}{dk} = \dfrac{dv}{d\omega}\dfrac{d\omega}{dk} = v_g\dfrac{dv}{d\omega}.$

Since $v = c/n$, $\dfrac{dv}{d\omega} = \dfrac{dv}{dn}\dfrac{dn}{d\omega} = -\dfrac{c}{n^2}\dfrac{dn}{d\omega}$

$$v_g = v - \frac{v_g ck}{n^2}\frac{dn}{d\omega} = \frac{v}{1 + (ck/n^2)(dn/d\omega)} = \frac{c}{n + \omega(dn/d\omega)}.$$

7.22

$$\omega \gg \omega_i, \qquad n^2 = 1 - \frac{Nq_e^2}{\omega^2\epsilon_0 m_e}\sum f_i = 1 - \frac{Nq_e^2}{\omega^2\epsilon_0 m_e}.$$

Using the binomial expansion, we have

$$(1 - x)^{1/2} \approx 1 - \frac{1}{2}x \quad \text{for } x \ll 1.$$

$$n = 1 - Nq_e^2/\omega^2\epsilon_0 m_e 2, \qquad dn/d\omega = Nq_e^2/\epsilon_0 m_e\omega^3$$

$$v_g = \frac{c}{n + \omega(dn/d\omega)}$$

$$= \frac{c}{1 - Nq_e^2/\omega^2\epsilon_0 m_e 2 + Nq_e^2/\epsilon_0 m_e\omega^2}$$

$$= \frac{c}{1 + Nq_e^2/\epsilon_0 m_e\omega^2 2}$$

and $v_g < c$,

$$v = c/n = \frac{c}{1 - Nq_e^2/\epsilon_0 m_e\omega^2 2}.$$

Binomial expansion

$$(1 - x)^{-1} \approx 1 + x, \qquad x \ll 1$$

$$v = c[1 + Nq_e^2/\epsilon_0 m_e\omega^2 2]; \qquad vv_g = c^2.$$

7.24 $\displaystyle\int_0^\lambda \sin akx \sin bkx\, dx$

$$= \frac{1}{2k}\left[\int_0^\lambda \cos[(a-b)kx]k\,dx - \int_0^\lambda \cos[(a+b)kx]\,k\,dx\right]$$

$$= \frac{1}{2k}\frac{\sin(a-b)kx}{a-b}\Bigg|_0^\lambda - \frac{1}{2k}\frac{\sin(a+b)kx}{a+b}\Bigg|_0^\lambda$$

$$= 0 \quad \text{if } a \neq b.$$

Whereas if $a = b$,

$$\int_0^\lambda \sin^2 akx\,dx = \frac{1}{2k}\int_0^\lambda (1 + \cos 2akx)\,k\,dx = \frac{\lambda}{2},$$

The other integrals are similar.

7.25 Even function, therefore $B_m = 0$.

$$A_0 = \frac{2}{\lambda}\int_{-\lambda/a}^{\lambda/a} dx = \frac{2}{\lambda}\left(\frac{\lambda}{a} + \frac{\lambda}{a}\right) = \frac{4}{a},$$

$$A_m = \frac{2}{\lambda}\int_{-\lambda/a}^{\lambda/a} (1)\cos mkx\,dx$$

$$= \frac{2}{mk\lambda}\sin mkx\Bigg]_{-\lambda/a}^{\lambda/a},$$

$$A_m = \frac{2}{m\pi}\sin\frac{m2\pi}{a}.$$

7.26

$$f'(x) = \frac{1}{\pi}\int_0^a E_0 L\frac{\sin kL/2}{kL/2}\cos kx\,dk$$

$$= \frac{E_0 L}{\pi 2}\int_0^b \frac{\sin(kL/2 + kx)}{kL/2}dk$$

$$+ \frac{E_0 L}{\pi 2}\int_0^b \frac{\sin(kL/2 - kx)}{kL/2}dk.$$

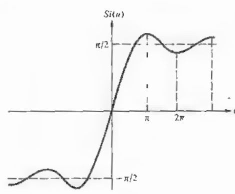
Let $kL/2 = w$, $(L/2)\,dk = dw$, $kx = wx'$.

$$f'(x) = \frac{E_0}{\pi}\int_0^b \frac{\sin(w + wx')}{w}dw + \frac{E_0}{\pi}\int_0^b \frac{\sin(w - wx')}{w}dw$$

where $b = aL/2$. Let $w + wx' = t$, $dw/w = dt/t$. $0 \le w \le b$ and $0 \le t \le (x'+1)b$. Let $w - wx' = -t$ in other integral $0 \le w \le b$ and $0 \le t \le (x'-1)b$.

$$f'(x) = \frac{E_0}{\pi}\int_0^{(x'+1)b}\frac{\sin t}{t}dt - \frac{E_0}{\pi}\int_0^{(x'-1)b}\frac{\sin t}{t}dt$$

$$f'(x) = \frac{E_0}{\pi}\text{Si}[b(x'+1)] - \frac{E_0}{\pi}\text{Si}[b(x'-1)], \qquad x' = 2x/L.$$



7.27 By analogy with Eq. (7.61),

$$A(\omega) = \frac{\Delta t}{2}E_0\,\text{sinc}\,(\omega_p - \omega)\frac{\Delta t}{2}.$$

From Table 1 (p. 624) sinc $(\pi/2) = 63.7\%$. Not quite 50% actually,

$$\text{sinc}\left(\frac{\pi}{1.65}\right) = 49.8\%.$$

$$\left|(\omega_p - \omega)\frac{\Delta t}{2}\right| < \frac{\pi}{2} \quad\text{or}\quad -\frac{\pi}{\Delta t} < (\omega_p - \omega) < \frac{\pi}{\Delta t};$$

thus appreciable values of $A(\omega)$ lie in a range $\Delta\omega \sim 2\pi/\Delta t$ and $\Delta\nu\,\Delta t \sim 1$. Irradiance is proportional to $A^2(\omega)$, and $[\text{sinc}\,(\pi/2)]^2 = 40.6\%$.

7.28 $\Delta x_c = c\,\Delta t_c$, $\Delta x_c \sim c/\Delta\nu$. But $\Delta\omega/\Delta k_0 = \bar{\omega}/\bar{k}_0 = c$; thus $|\Delta\nu/\Delta\lambda_0| = \bar{\nu}/\bar{\lambda}_0$,

$$\Delta x_c \sim \frac{c\bar{\lambda}_0}{\Delta\lambda_0\bar{\nu}}, \qquad \Delta x_c \sim \bar{\lambda}_0^2/\Delta\lambda_0.$$

Or try using the uncertainty principle:

$$\Delta x \sim \frac{h}{\Delta p} \quad \text{where } p = h/\lambda \text{ and } \Delta\lambda_0 \ll \bar{\lambda}_0.$$

7.29 $\Delta x_c = c\,\Delta t_c = 3 \times 10^8$ m/s 10^{-8} s $= 3$ m.

$\Delta\lambda_0 \sim \lambda_0^2/\Delta x_c = (500 \times 10^{-9}\text{ m})^2/3$ m,

$\Delta\lambda_0 \sim 8.3 \times 10^{-14}$ m $= 8.3 \times 10^{-5}$ nm,

$\Delta\lambda_0/\bar{\lambda}_0 = \Delta\nu/\bar{\nu} = 8.3 \times 10^{-5}/500 = 1.6 \times 10^{-7}$

~ 1 part in 10^7.

7.30 $\Delta\nu = 54 \times 10^3$ Hz;

$$\Delta\nu/\bar{\nu} = \frac{(54 \times 10^3)(10{,}600 \times 10^{-9}\text{ m})}{(3 \times 10^8\text{ m/s})}$$

$$= 1.91 \times 10^{-9}.$$

$$\Delta x_c = c\Delta t_c \sim c/\Delta\nu,$$

$$\Delta x_c \sim \frac{(3 \times 10^8\text{ m/s})}{(54 \times 10^3\text{ Hz})} = 5.55 \times 10^3\text{ m}.$$

7.32 $\Delta x_c = c\,\Delta t_c = 3 \times 10^8 \times 10^{-10} = 3 \times 10^{-2}$ m,

$\Delta\nu \sim 1/\Delta t_c = 10^{10}$ Hz,

$\Delta\lambda_0 = \bar{\lambda}_0^2/\Delta x_c$ (see Problem 7.28)

$= (632.8\text{ nm})^2/3 \times 10^{-2}\text{ m} = 0.013$ nm.

$\Delta\nu = 10^{15}$ Hz, $\Delta x_c = c \times 10^{-15} = 300$ nm,

$\Delta\lambda_0 \sim \bar{\lambda}_0^2/\Delta x_c = 1334.78$ nm.

CHAPTER 8

8.1

a) $\mathbf{E} = \hat{\imath}E_0\cos(kz - \omega t) + \hat{\jmath}E_0\cos(kz - \omega t + \pi)$. Equal amplitudes, E_y lags E_x by π. Therefore $\mathscr{P}$-state at 135° or −45°.

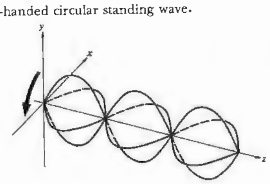
b) $\mathbf{E} = \hat{\imath}E_0\cos(kz - \omega t - \pi/2) + \hat{\jmath}E_0\cos(kz - \omega t + \pi/2)$. Equal amplitudes, E_y lags E_x by π. Therefore same as (a).

c) E_x leads E_y by $\pi/4$. They have equal amplitudes. Therefore it is an ellipse tilted at +45° and is left-handed.

d) E_y leads E_x by $\pi/2$. They have equal amplitudes. Therefore it is an $\mathscr{R}$-state.

8.2 $\mathbf{E}_x = \hat{\imath} \cos \omega t, \qquad \mathbf{E}_y = \hat{\jmath} \sin \omega t.$

Left-handed circular standing wave.



8.3 $\mathbf{E}_{\mathscr{R}} = \hat{\imath} E_0 \cos (kz - \omega t) + \hat{\jmath} E_0 \sin (kz - \omega t)$

$$\mathbf{E}_{\mathscr{L}} = \hat{\imath} E_0' \cos (kz - \omega t) - \hat{\jmath} E_0' \sin (kz - \omega t)$$

$$\mathbf{E} = \mathbf{E}_{\mathscr{R}} + \mathbf{E}_{\mathscr{L}} = \hat{\imath}(E_0 + E_0') \cos (kz - \omega t) + \hat{\jmath}(E_0 - E_0') \sin (kz - \omega t).$$

Let $E_0 + E_0' = E_{0x}''$ and $E_0 - E_0' = E_{0y}''$; then $\mathbf{E} = \hat{\imath} E_{0x}'' \cos (kz - \omega t) + \hat{\jmath} E_{0y}'' \sin (kz - \omega t)$. From Eqs. (8.11) and (8.12) it is clear that we have an ellipse where $\varepsilon = -\pi/2$ and $\alpha = 0$.

8.4 $E_{0y} = E_0 \cos 25°;\ E_{0z} = E_0 \sin 25°;$

$$\mathbf{E}(x, t) = (0.91\hat{\jmath} + 0.42\hat{\mathbf{k}}) E_0 \cos (kx - \omega t + \tfrac{1}{2}\pi)$$

8.6 $\mathbf{E} = E_0[\hat{\jmath} \sin (kx - \omega t) - \hat{\mathbf{k}} \cos (kx - \omega t)]$

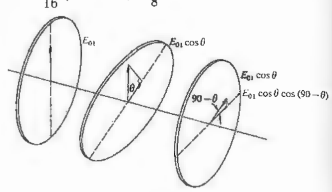
8.7 In natural light each filter passes 32% of the incident beam. Half of the incoming flux density is in the form of a $\mathscr{P}$-state parallel to the extinction axis, and effectively none of this emerges. Thus, 64% of the light parallel to the transmission axis is transmitted. In the present problem $32\% I_i$ enters the second filter, and $64\% (32\% I_i) = 21\% I_i$ leaves it.

8.11 From the figure (upper right), it follows that

$$I = \tfrac{1}{2} E_{01}^2 \sin^2 \theta \cos^2 \theta = \frac{E_{01}^2}{8} (1 - \cos 2\theta)(1 + \cos 2\theta)$$

$$= \frac{E_{01}^2}{8} (1 - \cos^2 2\theta) = \frac{E_{01}^2}{8} [1 - (\tfrac{1}{2} \cos 4\theta + \tfrac{1}{2})]$$

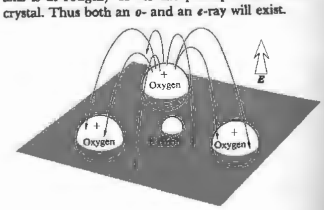
$$= \frac{E_{01}^2}{16} (1 - \cos 4\theta) = \frac{I_1}{8} (1 - \cos 4\theta); \qquad \theta = \omega t.$$



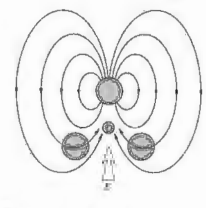
8.12 No. The crystal performs as if it were two oppositely oriented specimens in series. Two similarly oriented crystals in series would behave like one thick specimen and thus separate the *o*- and *e*-rays even more.

8.14 Light scattered from the paper passes through the polaroids and becomes linearly polarized. Light from the upper left filter has its **E**-field parallel to the principal section (which is diagonal across the second and fourth quadrants) and is therefore an *e*-ray. Notice how the letters *P* and *T* are shifted downward in an *extraordinary* fashion. The lower right filter passes an *o*-ray so that the letter *C* is undeviated. Note that the ordinary image is closer to the blunt corner.

8.15 (a) and (c) are two aspects of the previous problem. (b) shows double refraction because the polaroid's axis is at roughly 45° to the principal section of the crystal. Thus both an *o*- and an *e*-ray will exist.



8.16 When **E** is perpendicular to the CO_3 plane the polarization will be less than when it is parallel. In the former case, the field of each polarized oxygen atom tends to reduce the polarization of its neighbors. In other words, the induced field, as shown in the figure, is down while **E** is up. When **E** is in the carbonate plane two dipoles reinforce the third and vice versa. A reduced polarizability leads to a lower dielectric constant, a lower refractive index, and a higher speed. Thus $v_\parallel > v_\perp$.



8.20 $n_o = 1.6584,\ n_e = 1.4864$. Snell's law:

$$\sin \theta_i = n_o \sin \theta_{to} = 0.766$$

$$\sin \theta_i = n_e \sin \theta_{te} = 0.766$$

$$\sin \theta_{to} \approx 0.463, \qquad \theta_{to} \approx 27°35';$$

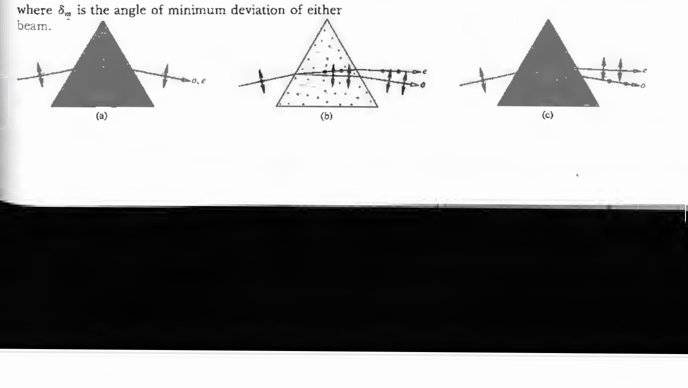
$$\sin \theta_{te} \approx 0.516, \qquad \theta_{te} \approx 31°4';$$

$$\Delta\theta \approx 3°29'.$$

8.22 Calcite $n_o > n_e$. Two spectra will be visible when (b) or (c) is used in a spectrometer. The indices are computed in the usual way, using

$$n = \frac{\sin \frac{1}{2}(\alpha + \delta_m)}{\sin \frac{1}{2}\alpha},$$

where δ_m is the angle of minimum deviation of either beam.

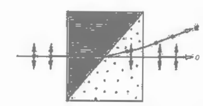


(a) (b) (c)

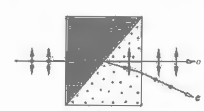
8.23 E_x leads E_y by $\pi/2$. They were initially in phase and $E_x > E_y$. Therefore the wave is left-handed, elliptical, and horizontal.

8.24 $\sin \theta_c = \dfrac{n_{\text{balsam}}}{n_0} = \dfrac{1.55}{1.658} = 0.935; \qquad \theta_c \sim 69°.$

8.26



(a) Calcite



(b) Quartz

c) Undesired energy in the form of one of the $\mathscr{P}$-states can be disposed of without local heating problems.

d) The Rochon transmits an undeviated beam (the *o*-ray), which is therefore achromatic as well.

8.31

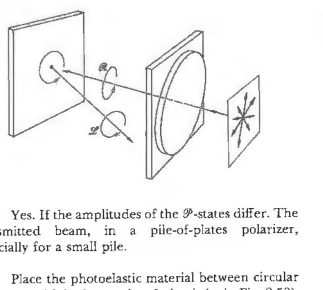
$$\Delta\varphi = \frac{2\pi}{\lambda_0} d\, \Delta n$$

but $\Delta\varphi = (1/4)(2\pi)$ because of the fringe shift. Therefore $\Delta\varphi = \pi/2$ and

$$\frac{\pi}{2} = \frac{2\pi d\, (0.005)}{589.3 \times 10^{-9}}$$

$$d = \frac{589.3 \times 10^{-9}}{2(10^{-2})} = 2.94 \times 10^{-5}\ \text{m}.$$

8.32 The $\mathscr{R}$-state incident on the glass screen drives the electrons in circular orbits, and they reradiate reflected circular light whose **E**-field rotates in the same direction as that of the incoming beam. But the propagation direction has been reversed on reflection, so that although the incident light is in an $\mathscr{R}$-state, the reflected light is left-handed. It will therefore be completely absorbed by the right-circular polarizer. This is illustrated in the figure below.



8.33 Yes. If the amplitudes of the $\mathscr{P}$-states differ. The transmitted beam, in a pile-of-plates polarizer, especially for a small pile.

8.35 Place the photoelastic material between circular polarizers with both retarders facing it (as in Fig. 8.52). Under circular illumination no orientation of the stress axes is preferred over any other, and they will thus all be indistinguishable. Only the birefringence will have an effect, and so the isochromatics will be visible. If the two polarizers are different, that is, one an $\mathscr{R}$, the other an $\mathscr{L}$, regions where Δn leads to $\Delta\varphi = \pi$ will appear bright. If they are the same, such regions appear dark.

8.37 $V_{\lambda/2} = \lambda_0/2n_0^3 r_{63}$ [8.44]

$$= 550 \times 10^{-9}/2(1.58)^3 5.5 \times 10^{-12}$$

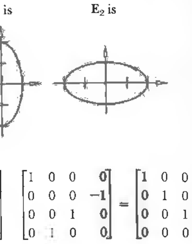
$$= 10^5/2(3.94) = 12.7\text{ kV}.$$

8.38 $\mathbf{E}_1 \cdot \mathbf{E}_2^* = 0, \quad \mathbf{E}_2 = \begin{bmatrix} e_{21} \\ e_{22} \end{bmatrix}$

$$\mathbf{E}_1 \cdot \mathbf{E}_2^* = (1)(e_{21})^* + (-2i)(e_{22})^* = 0$$

$$\mathbf{E}_2 = \begin{bmatrix} 2 \\ i \end{bmatrix}$$

$\mathbf{E}_1$ is $\mathbf{E}_2$ is



8.44

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$

8.46

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix}$$

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ -1 \end{bmatrix}$$

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ -1 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix}$$

8.47

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \end{bmatrix} \frac{1}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 1 & 0 \end{bmatrix}$$

$$\frac{1}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\frac{1}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\frac{1}{2} \begin{bmatrix} 1 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\frac{1}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ -1 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\frac{1}{2} \begin{bmatrix} 1 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \\ -1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

8.49

$$\begin{bmatrix} te^{i\varphi} & 0 \\ 0 & te^{i\varphi} \end{bmatrix},$$

where a phase increment of φ is introduced into both components as a result of traversing the plate.

$$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \qquad \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}.$$

8.50

$$\begin{bmatrix} t^2 & 0 & 0 & 0 \\ 0 & t^2 & 0 & 0 \\ 0 & 0 & t^2 & 0 \\ 0 & 0 & 0 & t^2 \end{bmatrix} \qquad \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

8.51 $V = \dfrac{I_p}{I_p + I_u} = \dfrac{(\mathcal{S}_1^2 + \mathcal{S}_2^2 + \mathcal{S}_3^2)^{1/2}}{\mathcal{S}_0}$

$$I_p = (\mathcal{S}_1^2 + \mathcal{S}_2^2 + \mathcal{S}_3^2)^{1/2}; \qquad I - I_p = I_u.$$

$$\mathcal{S}_0 - (\mathcal{S}_1^2 + \mathcal{S}_2^2 + \mathcal{S}_3^2)^{1/2} = I_u$$

$$\begin{bmatrix} 4 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 5 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$5 - (0 + 0 + 1)^{1/2} = I_u.$$

CHAPTER 9

9.1 $\mathbf{E}_1 \cdot \mathbf{E}_2 = \frac{1}{2}(\boldsymbol{E}_1 e^{-i\omega t} + \boldsymbol{E}_1^* e^{i\omega t}) \cdot \frac{1}{2}(\boldsymbol{E}_2 e^{-i\omega t} + \boldsymbol{E}_2^* e^{i\omega t})$,

where $\operatorname{Re}(z) = \frac{1}{2}(z + z^*)$.

$$\mathbf{E}_1 \cdot \mathbf{E}_2 = \tfrac{1}{4}[\boldsymbol{E}_1 \cdot \boldsymbol{E}_2 e^{-2i\omega t} + \boldsymbol{E}_1^* \cdot \boldsymbol{E}_2^* e^{2i\omega t} + \boldsymbol{E}_1 \cdot \boldsymbol{E}_2^* + \boldsymbol{E}_1^* \cdot \boldsymbol{E}_2].$$

The last two terms are time independent, while

$$\langle \boldsymbol{E}_1 \cdot \boldsymbol{E}_2 e^{-2i\omega t} \rangle \to 0 \quad \text{and} \quad \langle \mathbf{E}_1^* \cdot \mathbf{E}_2^* e^{2i\omega t} \rangle \to 0$$

because of the $1/T\omega$ coefficient. Thus

$$I_{12} = 2\langle \mathbf{E}_1 \cdot \mathbf{E}_2 \rangle = \tfrac{1}{2}(\boldsymbol{E}_1 \cdot \boldsymbol{E}_2^* + \boldsymbol{E}_1^* \cdot \boldsymbol{E}_2).$$

9.2 The largest value of $(r_1 - r_2)$ is equal to a. Thus if $\varepsilon_1 = \varepsilon_2$, $\delta = k(r_1 - r_2)$ varies from 0 to ka. If $a \gg \lambda$, $\cos\delta$ and therefore I_{12} will have a great many maxima and minima and therefore average to zero over a large region of space. In contrast, if $a \ll \lambda$, δ varies only slightly from 0 to $ka \ll 2\pi$. Hence I_{12} does not average to zero, and from Eq. (9.17), I deviates little from $4I_0$. The two sources effectively behave as a single source of double the original strength.

9.3 A bulb at S would produce fringes. We can imagine it as made up of a very large number of incoherent point sources. Each of these would generate an independent pattern, all of which would then overlap. Bulbs at S_1 and S_2 would be incoherent and could not generate detectable fringes.

9.5

a) $(r_1 - r_2) = \pm\frac{1}{2}\lambda$, hence $a \sin\theta_1 = \pm\frac{1}{2}\lambda$ and $\theta_1 = \pm\frac{1}{2}\lambda/a = \pm\frac{1}{2}(632.8 \times 10^{-9}\text{ m})/(0.200 \times 10^{-3}\text{ m}) = \pm 1.58 \times 10^{-3}$ rad, or since $y_1 = s\theta_1 = (1.00\text{ m})\ (\pm 1.58 \times 10^{-3}\text{ rad}) = \pm 1.58$ mm.

b) $y_5 = s5\lambda/a = (1.00\text{ m})5(632.8 \times 10^{-9})/(0.200 \times 10^{-3}\text{ m}) = 1.582 \times 10^{-2}$ m.

c) Since the fringes vary as cosine-squared and the answer to (a) is half a fringe width, the answer to (b) is 10 times larger.

9.13 $r_2^2 = a^2 + r_1^2 - 2ar_1 \cos(90 - \theta)$. The contribution to $\cos \delta/2$ from the third term in the Maclaurin expansion will be negligible if

$$\frac{k}{2}\left(\frac{a^2}{2r_1}\cos^2\theta\right) \ll \pi/2;$$

therefore $r_1 \gg a^2/\lambda$.

9.14 $E = \frac{1}{2}mv^2$; $v = 0.42 \times 10^6$ m/s;

$\lambda = h/mv = 1.73 \times 10^{-9}$; $\Delta y = s\lambda/a = 3.46$ mm.

9.18 $\Delta y = s\lambda_0/2d\alpha(n - n')$.

9.19 $\Delta y = (s/a)\lambda$, $a = 10^{-2}$ cm, $a/2 = 5 \times 10^{-3}$ cm.

9.20 $\delta = k(r_1 - r_2) + \pi$ (Lloyd's mirror)

$\delta = k\{a/2 \sin\alpha - [\sin(90 - 2\alpha)]a/2 \sin\alpha\} + \pi$

$\delta = ka(1 - \cos 2\alpha)/2 \sin\alpha + \pi$,

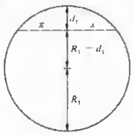
maximum occurs for

$\delta = 2\pi$ when $\sin\alpha(\lambda/a) = (1 - \cos 2\alpha) = 2\sin^2\alpha$.

First maximum $\alpha = \sin^{-1}(\lambda/2a)$.

9.22 Here $1.00 < 1.34 > 1.00$, hence from Eq. (9.36) with $m = 0$, $d = (0 + \frac{1}{2})(633\text{ nm})/2(1.34) = 118$ nm.

9.25 Eq. (9.37) $m = 2n_f d/\lambda_0 = 10{,}000$. A minimum, therefore central dark region.



9.26 The fringes are generally a series of fine jagged bands, which are fixed with respect to the glass.

9.27 $x^2 = d_1[(R_1 - d_1) + R_1] = 2R_1 d_1 - d_1^2$.

Similarly $x^2 = 2R_2 d_2 - d_2^2$.

$$d = d_1 - d_2 = \frac{x^2}{2}\left[\frac{1}{R_1} - \frac{1}{R_2}\right], \qquad d = m\frac{\lambda_f}{2}.$$

As $R_2 \to \infty$, x_m approaches Eq. (9.43).

9.29 $\Delta x = \lambda_f/2\alpha$, $\alpha = \lambda_0/2n_f\,\Delta x$,

$\alpha = 5 \times 10^{-5}$ rad $= 10.2$ seconds.

9.31 A motion of $\lambda/2$ causes a single fringe pair to shift past, hence $92\ \lambda/2 = 2.53 \times 10^{-5}$ m and $\lambda = 550$ nm.

9.35 $E_t^2 = E_t E_t^* = E_0^2(tt')^2/(1 - r^2 e^{-i\delta})(1 - r^2 e^{+i\delta})$

$I_t = I_i(tt')^2/(1 - r^2 e^{-i\delta} - r^2 e^{i\delta} + r^4)$.

9.36

a) $R = 0.80 \therefore F = 4R/(1 - R)^2 = 80$

b) $\gamma = 4\sin^{-1} 1/\sqrt{F} = 0.448$

c) $\mathscr{F} = 2\pi/0.448$

d) $C = 1 + F$

9.37
$$\frac{2}{1 + F(\Delta\delta/4)^2} = 0.81\left[1 + \frac{1}{1 + F(\Delta\delta/2)^2}\right]$$

$$F^2(\Delta\delta)^4 - 15.5F(\Delta\delta)^2 - 30 = 0.$$

9.38 $I = I_{max}\cos^2\delta/2$

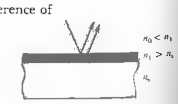
$I = I_{max}/2$ when $\delta = \pi/2 \quad \therefore \gamma = \pi$.

Separation between maxima is 2π.

$$\mathscr{F} = 2\pi/\gamma = 2.$$

9.40 At near normal incidence ($\theta_i \approx 0$) Fig. 4.23(e) indicates that the relative phase shift between an internally and externally reflected beam is π rad. That means a total relative phase difference of

$$\frac{2\pi}{\lambda_f}[2(\lambda_f/4)] + \pi.$$



or 2π. The waves are in phase and interfere constructively.

9.41 $n_0 = 1$ $n_s = n_g$ $n_1 = \sqrt{n_g}$

$\sqrt{1.54} = 1.24$

$$d = \frac{1}{4}\lambda_f = \frac{1}{4}\frac{\lambda_0}{n_1} = \frac{1}{4}\frac{540}{1.24}\text{ nm}.$$

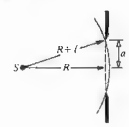
No relative phase shift between two waves.

9.42 The refracted wave will traverse the film twice, and there will be no relative phase shift on reflection. Hence

$$d = \lambda_0/4n_f = (550\text{ nm})/4(1.38) = 99.6\text{ nm}.$$

CHAPTER 10

10.1 $(R + \ell)^2 = R^2 + a^2$; therefore $R = (a^2 - \ell^2)/2\ell \approx a^2/2\ell$, $\ell R = a^2/2$, so for $\lambda \gg \ell$, $\lambda R \gg a^2/2 \therefore R = (1 \times 10^{-3})^2 10/2\lambda = 10$ m.



10.2 $E_0/2 = R\sin(\delta/2)$

$E = 2R\sin(N\delta/2)$ chord length

$E = [E_0\sin(N\delta/2)]/\sin(\delta/2)$

$I = E^2$.

10.4 $d\sin\theta_m = m\lambda$, $\quad \theta = N\delta/2 = \pi$

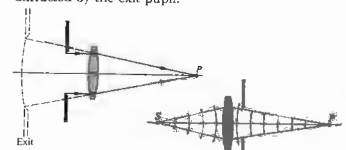
$7\sin\theta = (1)(0.21)$ $\quad \delta = 2\pi/N$

$= kd\sin\theta$

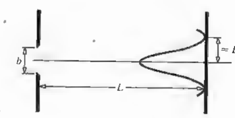
$\sin\theta = 0.03$ $\quad \sin\theta = 0.0009$

$\theta = 1.7°$ $\quad \theta = 3$ min.

10.5 Converging spherical wave in image space is diffracted by the exit pupil.



10.6



$\beta = \pm\pi$

$\sin\theta = \pm\lambda/b$

$\theta \approx \pm\lambda/b$

$L\theta \approx \pm L\lambda/b$

$L\theta \approx \pm f_2\lambda/b$.

10.9 $\lambda = (20\text{ cm})\sin 36.87° = 12$ cm.

10.10 $\alpha = \frac{ka}{2}\sin\theta$, $\quad \beta = \frac{kb}{2}\sin\theta$

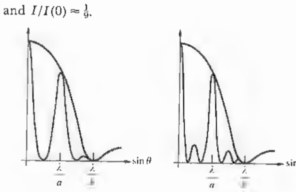
$a = mb$, $\alpha = m\beta$, $\alpha = m2\pi$

N = number of fringes $= \alpha/\pi = m2\pi/\pi = 2m$.

10.12 $\alpha = 3\pi/2N = \pi/2$ [10.34]

$$I(\theta) = \frac{I(0)}{N^2}\left(\frac{\sin\beta}{\beta}\right)^2 \qquad \text{from Eq. (10.35)}$$

and $I/I(0) \approx \frac{1}{9}$.



10.15 If the aperture is symmetrical about a line, the pattern will be symmetrical about a line parallel to it. Moreover, the pattern will be symmetrical about yet another line perpendicular to the aperture's symmetry axis. This follows from the fact that Fraunhofer patterns have a center of symmetry.

10.16

10.17 Three parallel short slits.

10.18 Two parallel short slits.

10.19 An equilateral triangular hole.

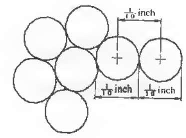
10.20 A cross-shaped hole.

10.21 The E-field of a rectangular hole.

10.23 From Eq. (10.58), $q_1 = 1.22(f/D)\lambda \approx \lambda$.

10.24

10.27 1 part in 1000. 3 yd ≈ 100 inches.



10.32 From Eq. (10.32), where $a = 1/(1000$ lines per cm$) = 0.001$ cm per line (center to center), $\sin\theta_m = 1(650 \times 10^{-9}\text{ m})/(0.001 \times 10^{-2}\text{ m}) = 6.5 \times 10^{-2}$ and $\theta_1 = 3.73°$.

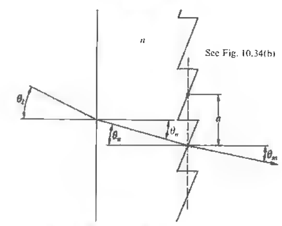
10.35 The largest value of m in Eq. (10.32) occurs when the sine function is equal to one, making the left side of the equation as large as possible, then $m = a/\lambda = (1/10 \times 10^5)/(3.0 \times 10^8\text{ m/s} \div 4.0 \times 10^{14}\text{ Hz}) = 1.3$, and only the first-order spectrum is visible.

10.37 $\sin\theta_i = n \sin\theta_n$

Optical path length difference $= m\lambda$

$a \sin\theta_m - na \sin\theta_n = m\lambda.$

$a(\sin\theta_m - \sin\theta_i) = m\lambda.$



10.38 $\mathcal{R} = mN = 10^6$, $N = 78 \times 10^3$

$\therefore m = 10^6/78 \times 10^3$.

$\Delta\lambda_{fsr} = \lambda/m = 500\text{ nm}/(10^6/78 \times 10^3) = 39\text{ nm}.$

$$\mathscr{R} = \mathscr{F}m = \mathscr{F}\frac{2n_f d}{\lambda} = 10^6 \qquad [9.76]$$

$$\Delta\lambda_{fsr} = \lambda^2/2n_f d = 0.0125\ \text{nm}. \qquad [9.78]$$

10.39 $\mathscr{R} = \lambda/\Delta\lambda = 5892.9/5.9 = 999$

$$N = \mathscr{R}/m = 333.$$

10.41 $y = L\lambda/d$

$$d = 12\times10^{-6}/12\times10^{-2} = 10^{-4}\ \text{m}.$$

10.43 $A = 2\pi\rho^2\int_0^{\varphi}\sin\varphi\, d\varphi = 2\pi\rho^2(1-\cos\varphi)$

$$\cos\varphi = [\rho^2 + (\rho+r_0)^2 - r_l^2]/2\rho(\rho+r_0)$$

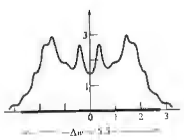
$$r_l = r_0 + l\lambda/2.$$

Area of first l zones

$$A = 2\pi\rho^2 - \pi\rho(2\rho^2 + 2\rho r_0 - l\lambda r_0 - l^2\lambda^2/4)/(\rho+r_0)$$

$$A_l = A - A_{l-1} = \frac{\lambda\pi\rho}{\rho+r_0}\left[r_0 + \frac{(2l-1)\lambda}{4}\right].$$

10.45



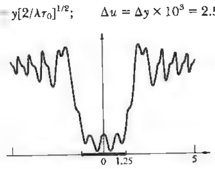
10.46 $I = \frac{I_0}{2}\{[\frac{1}{2} - \mathscr{C}(v_1)]^2 + [\frac{1}{2} - \mathscr{S}(v_1)]^2\}$

$$I = \frac{I_0}{2}\left(\frac{1}{\pi v_1}\right)^2\left[\sin^2\left(\frac{\pi v_1^2}{2}\right) + \cos^2\left(\frac{\pi v_1^2}{2}\right)\right]$$

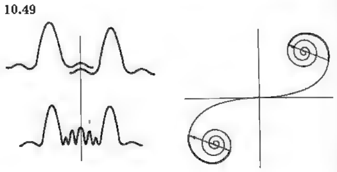
$$= \frac{I_0}{2}\left(\frac{1}{\pi v_1}\right)^2.$$

10.47 Fringes in both the clear and shadow region [(see M. P. Givens and W. L. Goffe, *Am. J. Phys.* **34**, 248 (1966)].

10.48 $u = y[2/\lambda r_0]^{1/2}$; $\quad \Delta u = \Delta y \times 10^3 = 2.5.$



10.49



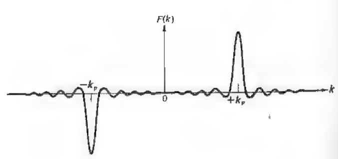
CHAPTER 11

11.1 $E_0 \sin k_p x = E_0(e^{ik_p x} - e^{-ik_p x})/2i$

$$F(k) = \frac{E_0}{2i}\left[\int_{-L}^{+L} e^{i(k+k_p)x}\, dx - \int_{-L}^{+L} e^{i(k-k_p)x}\, dx\right]$$

$$F(k) = -\frac{iE_0 \sin(k+k_p)L}{(k+k_p)} + \frac{iE_0\sin(k-k_p)L}{(k-k_p)}$$

$$F(k) = iE_0L[\text{sinc}\,(k-k_p)L - \text{sinc}(k+k_p)L].$$



11.3 $\cos^2\omega_p t = \frac{1}{2} + \frac{1}{2}\cos 2\omega_p t = \frac{1}{2} + \frac{e^{2i\omega_p t} + e^{-2i\omega_p t}}{4}.$

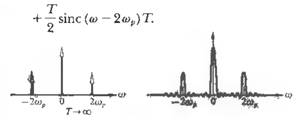
$$F(\omega) = \tfrac{1}{2}\int_{-T}^{+T} e^{i\omega t}\, dt + \tfrac{1}{4}\int e^{i(\omega+2\omega_p)t}\, dt + \tfrac{1}{4}\int e^{i(\omega-2\omega_p)t}\, dt$$

$$F(\omega) = \frac{1}{\omega}\sin\omega T + \frac{1}{2(\omega+2\omega_p)}\sin(\omega+2\omega_p)T$$

$$+ \frac{1}{2(\omega-2\omega_p)}\sin(\omega-2\omega_p)T$$

$$F(\omega) = T\,\text{sinc}\,\omega T + \frac{T}{2}\text{sinc}\,(\omega+2\omega_p)T$$

$$+ \frac{T}{2}\text{sinc}\,(\omega-2\omega_p)T.$$



11.6 $\mathscr{F}\{af(x) + bh(x)\} = aF(k) + bH(k)$

11.8 $F(k) = L\,\text{sinc}^2\, kL/2$ at $k = 0$, $F(0) = L$, and $F(\pm 2\pi/L) = 0$.

11.15 $\int_{x=-\infty}^{x=+\infty} f(x)h(X-x)\, dx$

$$= -\int_{x'=+\infty}^{x'=-\infty} f(X-x')h(x')\, dx'$$

$$= \int_{-\infty}^{+\infty} h(x')f(X-x')\, dx'$$

where $x' = X - x$, $dx = -dx'$.

$$f \circledast h = h \circledast f$$

or

$$\mathscr{F}\{f\circledast h\} = \mathscr{F}\{f\}\cdot\mathscr{F}\{h\} = \mathscr{F}\{h\}\cdot\mathscr{F}\{f\} = \mathscr{F}\{h\circledast f\}.$$

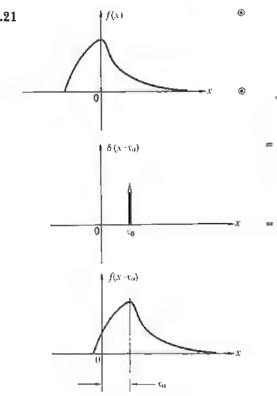
11.17 A point on the edge of $f(x, y)$, for example, at $(x = d, y = 0)$, is spread out into a square 2ℓ on a side centered on $X = d$. Thus it extends no farther than $X = d + \ell$, and so the convolution must be zero at $X = d + \ell$ and beyond.

11.19 $f(x - x_0)\circledast h(x) = \int_{-\infty}^{+\infty} f(x-x_0)h(X-x)\, dx,$

and setting $x - x_0 = \alpha$, this becomes

$$\int_{-\infty}^{+\infty} f(\alpha)h(X - \alpha - x_0)\, d\alpha = g(X - x_0)$$

11.21



11.24 We see that $f(x)$ is the convolution of a rect-function with two δ-functions, and from the convolution theorem,

$$F(k) = \mathscr{F}\{(\text{rect}\,(x)\circledast[\delta(x-a) + \delta(x+a)]\}$$

$$= \mathscr{F}\{\text{rect}\,(x)\}\cdot\mathscr{F}\{[\delta(x-a)+\delta(x+a)]\}$$

$$= a\,\text{sinc}\,\tfrac{1}{2}ka\cdot(e^{ika} + e^{-ika})$$

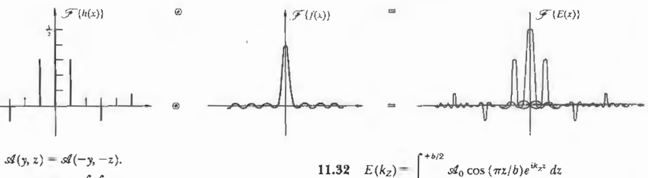
$$= a\,\text{sinc}\,(\tfrac{1}{2}ka)\cdot 2\cos ka.$$

11.25 $f(x)\circledast h(x)$

$$= [\delta(x+3) + \delta(x-2) + \delta(x-5)]\circledast h(x)$$

$$= h(x+3) + h(x-2) + h(x-5)$$

11.28



11.29 $\mathscr{A}(y, z) = \mathscr{A}(-y, -z)$.

$$E(Y, Z, t) \propto \iint \mathscr{A}(y, z) e^{i(k_Y y + k_Z z)}\, dy\, dz.$$

Change Y to $-Y$, Z to $-Z$, y to $-y$, z to $-z$, then k_Y goes to $-k_Y$ and k_Z to $-k_Z$.

$$E(-Y, -Z) \propto \iint \mathscr{A}(-y, -z) e^{i(k_Y y + k_Z z)}\, dy\, dz$$

$$\therefore E(-Y, -Z) = E(Y, Z).$$

11.30 From Eq. (11.63),

$$E(Y, Z) = \iint \mathscr{A}(y, z) e^{ik(Yy+Zz)/R}\, dy\, dz$$

$$E'(Y, Z) = \iint \mathscr{A}(\alpha y, \beta z) e^{ik(Yy+Zz)/R}\, dy\, dz;$$

now let $y' = \alpha y$ and $z' = \beta z$:

$$E'(Y, Z) = \frac{1}{\alpha\beta} \iint \mathscr{A}(y', z') e^{ik[(Y/\alpha)y' + (Z/\beta)z']}\, dy'\, dz'$$

or

$$E'(Y, Z) = \frac{1}{\alpha\beta} E(Y/\alpha, Z/\beta).$$

11.31

$$C_{ff} = \lim_{T\to\infty} \frac{1}{2T} \int_{-T}^{+T} A \sin(\omega t + \varepsilon) A \sin(\omega t - \omega\tau + \varepsilon)\, dt$$

$$= \lim_{T\to\infty} \frac{A^2}{2T} \int [\tfrac{1}{2}\cos(\omega\tau) - \tfrac{1}{2}\cos(2\omega t - \omega\tau + 2\varepsilon)]\, dt,$$

since $\cos\alpha - \cos\beta = -2\sin\frac{1}{2}(\alpha+\beta)\sin\frac{1}{2}(\alpha-\beta)$. Thus

$$C_{ff} = \frac{A^2}{2}\cos(\omega\tau).$$

11.32 $E(k_Z) = \int_{-b/2}^{+b/2} \mathscr{A}_0 \cos(\pi z/b) e^{ik_Z z}\, dz$

$$= \mathscr{A}_0 \int \cos\frac{\pi z}{b}\cos k_Z z\, dz$$

$$+ i\mathscr{A}_0 \int \cos\frac{\pi z}{b}\sin k_Z z\, dz$$

$$E(k_Z) = \mathscr{A}_0 \cos\frac{bk_Z}{2}\left[\frac{1}{\left(\frac{\pi}{b} - k_Z\right)} + \frac{1}{\left(\frac{\pi}{b} + k_Z\right)}\right].$$

CHAPTER 12

12.1 At low pressures, the intensity emitted from the lamp is low, the bandwidth is narrow, and the coherence length is large. The fringes will initially display a high contrast, although they'll be fairly faint. As the pressure builds, the coherence length will decrease, the contrast will drop off, and the fringes might even vanish entirely.

12.4 Each sine function in the signal produces a cosinusoidal autocorrelation function with its own wavelength and amplitude. All of these are in phase at the zero delay point corresponding to $\tau = 0$. Beyond that origin the cosines soon fall out of phase, producing a jumble where destructive interference is more likely. (The same sort of thing happens when, say, a square pulse is synthesized out of sinusoids—everywhere beyond the pulse all the contributions cancel.) As the number of components increases and the signal becomes more complex—resembling random noise—the autocorrelation narrows, ultimately becoming a δ-spike at $\tau = 0$.

12.6 The irradiance at Σ_0 arising from a point source is $4I_0\cos^2(\delta/2) = 2I_0(1 + \cos\delta)$.

For a differential source element of width dy at point S', y from the axis, the OPD to P at Y via the two slits is

$$\Lambda = (\overline{S'S_1} + \overline{S_1P}) - (\overline{S'S_2} + \overline{S_2P})$$

$$= (\overline{S'S_1} - \overline{S'S_2}) + (\overline{S_1P} - \overline{S_2P})$$

$$= ay/l + aY/s \text{ from Section 9.3.}$$

The contribution to the irradiance from dy is then

$$dI \propto (1 + \cos k\Lambda)\, dy$$

$$I \propto \int_{-b/2}^{+b/2} (1 + \cos k\Lambda)\, dy$$

$$I \propto b + \frac{d}{ka}\left[\sin\left(\frac{aY}{s} + \frac{ab}{2l}\right) - \sin\left(\frac{aY}{s} - \frac{ab}{2l}\right)\right]$$

$$I \propto b + \frac{d}{ka}[\sin(kaY/s)\cos(kab/2l)$$
$$+ \cos(kaY/s)\sin(kab/2l)$$
$$- \sin(kaY/s)\cos(kab/2l)$$
$$+ \cos(kaY/s)\sin(kab/2l)]$$

$$I \propto b + \frac{l2}{ka}\sin(kab/2l)\cos(kaY/s).$$

12.7

$$\mathscr{V} = \frac{I_{\max} - I_{\min}}{I_{\max} + I_{\min}}$$

$$I_{\max} = I_1 + I_2 + 2\sqrt{I_1 I_2}|\tilde{\gamma}_{12}|$$

$$I_{\min} = I_1 + I_2 - 2\sqrt{I_1 I_2}|\tilde{\gamma}_{12}|$$

$$\mathscr{V} = \frac{4\sqrt{I_1 I_2}|\tilde{\gamma}_{12}|}{2(I_1 + I_2)}.$$

12.8 When

$$S''S_1O' - S'S_1O' = \lambda/2, 3\lambda/2, 5\lambda/2, \ldots,$$

the irradiance due to S' is given by

$$I' = 4I_0\cos^2(\delta'/2) = 2I_0(1 + \cos\delta'),$$

while the irradiance due to S'' is

$$I'' = 4I_0\cos^2(\delta''/2) = 4I_0\cos^2(\delta' + \pi)/2$$
$$= 2I_0(1 - \cos\delta').$$

Hence $I' + I'' = 4I_0$.

12.10 $\theta = \frac{1}{2}° = 0.0087$ rad

$$h = 0.32\bar{\lambda}_0/\theta \text{ using } \bar{\lambda}_0 = 550 \text{ nm}$$

$$h = 0.32\,(550 \text{ nm})/0.0087$$

$$h = 2 \times 10^{-2} \text{ mm.}$$

12.11 $I_1(t) = \Delta I_1(t) + \langle I_1\rangle$;

hence

$$\langle I_1(t+\tau)I_2(t)\rangle$$
$$= \langle[\langle I_1\rangle + \Delta I_1(t+\tau)][\langle I_2\rangle + \Delta I_2(t)]\rangle,$$

since $\langle I_1\rangle$ is independent of time.

$$\langle I_1(t+\tau)I_2(t)\rangle = \langle I_1\rangle\langle I_2\rangle + \langle\Delta I_1(t+\tau)\Delta I_2(t)\rangle,$$

if we recall that $\langle\Delta I_1(t)\rangle = 0$. Eq. (12.34) follows by comparison with Eq. (12.32).

12.13 From Eq. (12.22), $\mathscr{V} = 2\sqrt{(10I)I}/(10I + I) = 2\sqrt{10}/11 = 0.57$.

12.15 Using the van Cittert–Zernike theorem, we can find $\tilde{\gamma}_{12}(0)$ from the diffraction pattern over the apertures, and that will yield the visibility on the observation plane: $\mathscr{V} = |\tilde{\gamma}_{12}(0)| = |\text{sinc}\,\beta|$. From Table 1, $\sin u/u = 0.85$ when $u = 0.97$, hence $\pi b y/l\lambda = 0.97$, and if $y = \overline{P_1P_2} = 0.50$ mm, then $b = 0.97(l\lambda/\pi y) = 0.97(1.5 \text{ m})(500 \times 10^{-9} \text{ m})/\pi(0.50 \times 10^{-3} \text{ m}) = 0.46$ mm.

12.18 From the van Cittert–Zernike theorem, the degree of coherence can be obtained from the Fourier transform of the source function, which itself is a series of δ-functions corresponding to a diffraction grating with spacing a, where $a\sin\theta_m = m\lambda$. The coherence function is therefore also a series of δ-functions. Hence the $\overline{P_1P_2}$, the slit separation d, must correspond to the location of the first-order diffraction fringe of the source if $\mathscr{V}$ is to be maximum. $a\theta_1 \approx \lambda$, and so $d \approx l\theta_1 \approx \lambda l/a = (500 \times 10^{-9} \text{ m})(2.0 \text{ m})/(500 \times 10^{-6} \text{ m}) = 2.0$ mm.

CHAPTER 13

13.1 $I_e = \sigma T^4$ *[13.1]*

$(22.8\ \mathrm{W\ cm^2})(10^4\ \mathrm{cm^2/m^2}) = (5.7 \times 10^{-8}\ \mathrm{W\ m^{-2}\ K^{-4}})T^4$

$$T = \left[\frac{22.8 \times 10^4}{5.7 \times 10^{-8}}\right]^{1/4} = 1.414 \times 10^3 = 1414\ \mathrm{K}.$$

13.3 $\nu = c/\lambda, \qquad d\nu = -c\, d\lambda/\lambda^2.$

Since $I_{e\lambda}$ and $I_{e\nu}$ are to be positive and since an increase in λ yields a decrease in ν, we write

$$I_{e\lambda}\, d\lambda = -I_{e\nu}\, d\nu$$

and

$$I_{e\nu} = -I_{e\lambda}\, d\lambda/d\nu = I_{e\lambda}\lambda^2/c.$$

13.4 $$\lambda = \frac{h}{mv} = \frac{6.63 \times 10^{-34}\ \mathrm{J\ s}}{(0.15\ \mathrm{kg})(25\ \mathrm{m/s})}.$$

Baseball: $$\lambda = \frac{6.63 \times 10^{-34}}{3.75} = 1.76 \times 10^{-34}\ \mathrm{m}$$

Hydrogen: $$\lambda = \frac{6.63 \times 10^{-34}}{(1.67 \times 10^{-27})(10^3)} = 3.96 \times 10^{-10}\ \mathrm{m}.$$

13.6 $$\lambda = \frac{c}{\nu} = \frac{hc}{h\nu} = \frac{(6.63 \times 10^{-34})(3 \times 10^8)}{(1.6 \times 10^{-19})h\nu[\text{in eV}]}$$

$$\lambda = \frac{12.39 \times 10^{-7}\ \mathrm{m}}{h\nu[\text{in eV}]} = \frac{12{,}390\ \text{Å}}{h\nu[\text{in eV}]}.$$

The usual mnemonic is

$$\lambda = \frac{12{,}345\ \text{Å}}{h\nu[\text{in eV}]}.$$

13.7 $\lambda(\min) = 300\ \mathrm{nm}$

$$h\nu = hc/\lambda$$

$$= \frac{(6.63 \times 10^{-34}\ \mathrm{J\ s})(3 \times 10^8\ \mathrm{m/s})}{300 \times 10^{-9}\ \mathrm{m}}$$

$$\mathscr{E} = 6.63 \times 10^{-19}\ \mathrm{J} = 4.14\ \mathrm{eV}.$$

13.9 $N h\nu = (1.4 \times 10^3\ \mathrm{W/m^2})(1\ \mathrm{m^2})(1\ \mathrm{s})$

$$N = \frac{1.4 \times 10^3(700 \times 10^{-9})}{(6.63 \times 10^{-34})(3 \times 10^8)} = \frac{980 \times 10^{20}}{19.89}$$

$$N = 49.4 \times 10^{20}.$$

13.10 $$h\nu = \frac{hc}{\lambda} = \frac{(6.63 \times 10^{-34})(3 \times 10^8)}{500 \times 10^{-9}}$$

$$= 3.98 \times 10^{-9}\ \mathrm{J}$$

$$h\nu = 2.5\ \mathrm{eV}.$$

$$\text{Energy per second} = \pi r^2 I = (3.14)(10^{-20})(10^{-10})$$

$$= 3.14 \times 10^{-30}\ \mathrm{J/s}$$

$$(T)(3.14 \times 10^{-30}\ \mathrm{J/s}) = 3.98 \times 10^{-19}\ \mathrm{J}$$

$$T = 1.27 \times 10^{11}\ \mathrm{s} \quad (1\ \mathrm{yr} = 3.154 \times 10^7\ \mathrm{s}),$$

$$T \sim 4000\ \text{years}$$

$$\lambda^2 = 25 \times 10^{-14}\ \mathrm{m^2}. \quad \lambda^2 I = 25 \times 10^{-24}\ \mathrm{J/s}$$

$$T = \frac{3.98 \times 10^{-19}}{2.5 \times 10^{-23}} = 1.59 \times 10^4\ \mathrm{s} \qquad (3.6 \times 10^3\ \mathrm{s/h})$$

$T = 4.4$ h (still impossible).

It would take twice as long if $h\nu = 5$ eV, which means (Problem 13.6)

$$\lambda = \frac{12345\ \text{Å}}{5} = 247\ \text{nm (ultraviolet).}$$

13.11 $$\nu_0 = \Phi_0/h = \frac{2.28(1.6 \times 10^{-19})}{6.63 \times 10^{-34}}$$ *[13.8]*

$$= 5.5 \times 10^{14}\ \mathrm{Hz} = 550\ \mathrm{THz}$$

$$\nu = c/\lambda = 3 \times 10^8/400 \times 10^{-9} = 750 \times 10^{12}\ \mathrm{Hz}.$$

$$\frac{mv_{\max}^2}{2} = h(\nu - \nu_0) = h200 \times 10^{12}$$ *[13.9]*

$$= 13.26 \times 10^{-20}\ \mathrm{J}.$$

13.13 The photon's gravitational potential energy $U = -GMm/R$, where m is photon mass but $m = h\nu/c^2$; thus

$$U = -GMh\nu/Rc^2.$$

Ergo $$\mathscr{E} = h\nu - GMh\nu/Rc^2 = h\nu\left(1 - \frac{GM}{c^2R}\right).$$

At the Earth $\mathscr{E} = h\nu_e$ and

$$\nu_e = \nu - \frac{GM}{c^2R}\nu.$$

Since $\Delta\nu = \nu - \nu_e$, $\Delta\nu = \dfrac{GM}{c^2R}\nu.$

13.14 $$\frac{\Delta\nu}{\nu} = \frac{(6.67 \times 10^{-11}\ \mathrm{Nm^2/kg^2})(1.99 \times 10^{30}\ \mathrm{kg})}{(3 \times 10^8\ \mathrm{m/s})^2(6.96 \times 10^8\ \mathrm{m})}$$

$$\frac{\Delta\nu}{\nu} = 2.12 \times 10^{-6}$$

$$\Delta\nu = \frac{2.12 \times 10^{-6}(3 \times 10^8)}{650 \times 10^{-9}} = 9.8 \times 10^8\ \mathrm{Hz}$$

or

$$\frac{\Delta\lambda}{\lambda} = \frac{\Delta\nu}{\nu} \quad \therefore \quad \Delta\lambda = \Delta\nu\,\lambda/\nu$$

$$\Delta\lambda = 2.12 \times 10^{-6}(650 \times 10^{-9})$$

$$\Delta\lambda = 13.8 \times 10^{-13} = 0.0014\ \mathrm{nm}.$$

13.15 $h\nu_f = h\nu_i - mgd$ *[13.13]*

$$\Delta\nu = -mgd/h = -\frac{h\nu}{c^2}\frac{gd}{h} = -gd\nu/c^2$$

$$\frac{\Delta\nu}{\nu} = -\frac{(9.8\ \mathrm{m/s^2})(20\ \mathrm{m})}{(3 \times 10^8\ \mathrm{m/s})^2} = -2.18 \times 10^{-15}.$$

13.16 $F = GMm/r^2 = GMm/R^2 \sec^2\theta$

$$F_\perp = F\cos\theta = GMm\cos\theta/R^2\sec^2\theta$$

$$dt = R\sec^2\theta\, d\theta/c.$$

$$p_\perp = \int F_\perp\, dt = \frac{GMm}{cR}\int_{-\pi/2}^{\pi/2}\cos\theta\, d\theta = 2GMm/cR.$$

$$\tan\varphi = p_\perp/p_\parallel = 2GM/c^2R \approx \varphi$$

$$\varphi = \frac{2(6.67 \times 10^{-11}\ \mathrm{Nm^2/kg^2})(1.99 \times 10^{30}\ \mathrm{kg})}{(3 \times 10^8\ \mathrm{m/s})^2(6.96 \times 10^8\ \mathrm{m})}$$

$\varphi = 24.5 \times 10^{-5}$ degrees $= 0.88$ seconds of arc.

13.18 $\frac{3}{2}kT = 6.17 \times 10^{-21}\ \mathrm{J} = 3.85 \times 10^{-2}\ \mathrm{eV}$

$$p = [2m_0(3kT/2)]^{1/2} = 4.55 \times 10^{-24}$$

$$\lambda = h/p = 1.45\ \text{Å}.$$

13.19 No—splitting a photon would result in two lower-frequency pieces, which we could presumably separate and detect.

13.21 $$\Pi = \frac{1000\ \mathrm{W}}{h\nu} = \frac{1000(10600 \times 10^{-9})}{6.63 \times 10^{-34}(3 \times 10^8)}$$

$$= 5.06 \times 10^{22}\ \text{photons/s}.$$

13.22

$$\mathscr{E} = \frac{p^2}{2m_0} + U, \quad h\nu = \frac{h^2}{\lambda^2 2m_0} + U, \quad \hbar\omega = \hbar^2k^2/2m_0 + U.$$

13.24 $\psi = C_1e^{-i(\omega t + kx)} + C_2e^{-i(\omega t - kx)}$

$$\frac{\partial\psi}{\partial t} = -i\omega\psi; \qquad \frac{\partial\psi}{\partial x} = -ikC_1e^{-i(\omega t + kx)} + ikC_2e^{-i(\omega t - kx)}$$

$$\frac{\partial^2\psi}{\partial x^2} = -k^2C_1e^{-i(\omega t + kx)} - k^2C_2e^{-i(\omega t - kx)} = -k^2\psi.$$

Using the dispersion relation of Problem 13.22, we obtain

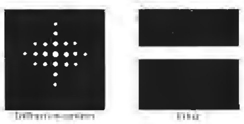
$$\hbar\omega\psi = \hbar^2k^2\psi/2m_0 + U\psi$$

$$i\hbar\frac{\partial\psi}{\partial t} = \frac{-\hbar^2}{2m_0}\frac{\partial^2\psi}{\partial x^2} + U\psi.$$

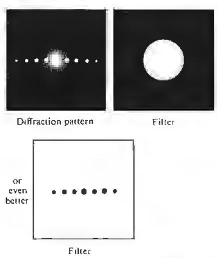
CHAPTER 14

14.1

14.2



14.3



14.5

14.6 From the geometry, $f_t\theta = f_i\Phi$: $k_O = k \sin\theta$ and $k_I = k \sin\Phi$, hence $\sin\theta \approx \theta \approx k_O\lambda/2\pi$ and $\sin\Phi \approx \Phi \approx k_I\lambda/2\pi$, therefore $\theta/\Phi = k_O/k_I$ and $k_I = k_O(\Phi/\theta) = k_O(f_t/f_i)$. When $f_i > f_t$ the image will be larger than the object, the spatial periods in the image will also be larger, and the spatial frequencies in the image will be smaller than in the object.

14.7 $a = (1/50)$ cm: $a \sin\theta = m\lambda$, $\sin\theta \approx \theta$, hence $\theta = (5000\ m)\lambda$, and the distance between orders on the transform plane is $f\theta = 5000\lambda f = 2.7$ mm.

14.9 Each point on the diffraction pattern corresponds to a single spatial frequency, and if we consider the diffracted wave to be made up of plane waves, it also corresponds to a single-plane wave direction. Such waves, by themselves, carry no information about the periodicity of the object and produce a more or less uniform image. The periodicity of the source arises in the image when the component plane waves interfere.

14.11 The relative field amplitudes are 1.00, 0.60, and 0.60; hence $E \propto 1 + 0.60 \cos(+ky') + 0.60 \cos(-ky') = 1 + 1.2 \cos ky'$. This is a cosine oscillating about a line equal to 1.0. It varies from +2.2 to −0.2. The square of this will correspond to the irradiance, and it will be a series of tall peaks with a relative height of $(2.2)^2$, between each pair of which there will be a short peak proportional to $(0.2)^2$; notice the similarity with Fig. 11.32.

14.12 $a \sin\theta = \lambda$, here $f\theta = 50\lambda f = 0.20$ cm; hence $\lambda = 0.20/50(100) = 400$ nm. The magnification is 1.0 when the focal lengths are equal, hence the spacing is again 50 wires/cm.

14.18 $I = \frac{1}{2}v\epsilon E_0^2 = \frac{n}{2}\left(\frac{\epsilon_0}{\mu_0}\right)^{1/2} E_0^2$, where $\mu \approx \mu_0$

$$E_0^2 = 2(\mu_0/\epsilon_0)^{1/2} I/n \qquad (\mu_0/\epsilon_0)^{1/2} = 376.730\ \Omega$$

$$E_0 = 27.4(I/n)^{1/2}.$$

14.20 The inherent motion of the medium would cause the speckle pattern to vanish.

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