PTO/AIA/15 (03-13)

Approved for use through 01/31/2014. OMB 0651-0032

U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE

Under the Paperwork Reduction Act of 1995 no persons are required to re UTILITY	Attorney Docket No		
PATENT APPLICATION	First Named Invento	r WEI-YU	J CHEN
TRANSMITTAL	Title	IMAGE CAPTURIN TERMINAL	IG LENS SYSTEM, IMAGING DEVICE AND MOBILE
(Only for new nonprovisional applications under 37 CFR 1.53(b))	Express Mail Label I	lo.)
APPLICATION ELEMENTS See MPEP chapter 600 concerning utility patent application contents.	ADDRESS TC	:	mmissioner for Patents P.O. Box 1450 candria, VA 22313-1450
1. Fee Transmittal Form (PTO/SB/17 or equivalent)	ACCOMP	ANYING APP	PLICATION PAPERS
2. Applicant asserts small entity status. See 37 CFR 1.27	10. Assignmen (cover shee	Papers & document(s))	
3. Applicant certifies micro entity status. See 37 CFR 1.29. Applicant must attach form PTO/SB/15A or B or equivalent.		lame of Assignee	
Applicant must attach form PTO/SB/15A or B or equivalent. 4. ✓ Specification [Total Pages 56]] Both the claims and abstract must start on a new page. (See MPEP § 608.01(a) for information on the preferred arrangement) 5. ✓ Drawing(s) (35 U.S.C. 113) [Total Sheets 23]] 6. Inventor's Oath or Declaration [Total Pages 1]] (including substitute statements under 37 CFR 1.64 and assignments serving as an oath or declaration under 37 CFR 1.63(e)) a. ✓ Newly executed (original or copy) b. △ A copy from a prior application (37 CFR 1.63(d)) 7. ✓ Application Data Sheet * See note below. See 37 CFR 1.76 (PTO/AIA/14 or equivalent) 8. CD-ROM or CD-R in duplicate, large table, or Computer Program (Appendix) △ Landscape Table on CD 9. Nucleotide and/or Amino Acid Sequence Submission (if applicable, items a. – c. are required) a. △ Computer Readable Form (CRF) b. △ Specification Sequence Listing on: i. △ i. △ CD-ROM or CD-R (2 copies); or ii. ○	(when there 12. English Tra (if applicable 13. Informatio (PTO/SB/08. Co 14. Preliminary 15. Return Rec (MPEP § 503 16. Certified Ca (if foreign pr 17. Nonpublica	a Disclosure State or PTO-1449) bies of citations at Amendment eipt Postcard (Should be specifico opy of Priority Do pority is claimed) tion Request .C. 122(b)(2)(B)(i). A	ement ttached ally itemized)
c. Statements verifying identity of above copies			
 *Note: (1) Benefit claims under 37 CFR 1.78 and foreign priority claims (2) For applications filed under 35 U.S.C. 111, the application n assignee, person to whom the inventor is under an obligation interest in the matter. See 37 CFR 1.46(b). 	nust contain an ADS s on to assign, or perso	ecifying the appli who otherwise s	icant if the applicant is an
	NDENCE ADDRESS		
The address associated with Customer Number: 24728		OR	Correspondence address below
Name Address			
City State		Zip Code	
Country Telephone		Email	
signature /Tim Tingkang Xia/	Da	te	December 13, 2013
Name (Print/Type) Tim Tingkang Xia This collection of information is required by 37 CFR 1.53(b). The information is requ	(A	tomey/rigent/	45,242

This collection of information is required by 37 CFR 1.53(b). The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.11 and 1.14. This collection is estimated to take 12 minutes to complete, including gathering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete his form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

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PTO/SB/17 (03-13)

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FFF		NSN	ΊΙΤΤΑ		Applic	ation Num				
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Applicant asser	ts small ent	ity status. 9	See 37 CFR 1		-	lamed Inve		/EI-YU CHE		
Applicant certif		•				Examiner Name			.11	
Form PTO/SB/15A or B or equivalent must either be enclosed or have			Art Ur							
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✔ Deposit Accoun	it Deposit A	ccount Nur	mber: 50-3	537	D	eposit Acco	unt Name:	Morris, Mannin	g & Martin, L	LP
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✓ Charge f	ee(s) indica	ted below			Charg	e fee(s) ind	icated belov	<i>»,</i> except for	the filing f	ee
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WARNING: Informa			become pub	olic. Credit ca	ard informatio	on should n	ot be incluc	led on this fo	rm. Provid	e credit card
information and aut	horization c	on PTO-203	8.							
FEE CALCULATION										
1. BASIC FILING, SE			-			small entit	-	-	-	
Application Type	F <u>U (\$)</u>	ILING FEES <u>S (\$)</u>	<u>M (\$)</u>	s <u>u(\$)</u>	EARCH FEES <u>S (\$)</u>	<u>M (\$)</u>	EXA U (\$)	MINATION F		Fees Paid (\$
Utility	280	<u>3 (3)</u> 140*	70	<u>600</u>	<u>3 (5)</u> 300	150	720	<u>s (\$)</u> 360	<u>M (\$)</u> 180	1600
Design	180	90	45	120	60	30	460	230	115	
Plant	180	90	45	380	190	95	580	290	145	
Reissue	280	140	70	600	300	150	2,160	1,080	540	
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gathering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. **SEND** TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

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Application Data Sheet 37 CFR 1.76		Attorney Docket Number	14970-94702	
		Application Number		
Title of Invention	itle of Invention IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL			
The application data sheet is part of the provisional or nonprovisional application for which it is being submitted. The following form contains the				

bibliographic data arranged in a format specified by the United States Patent and Trademark Office as outlined in 37 CFR 1.76. This document may be completed electronically and submitted to the Office in electronic format using the Electronic Filing System (EFS) or the document may be printed and included in a paper filed application.

Secrecy Order 37 CFR 5.2

Portions or all of the application associated with this Application Data Sheet may fall under a Secrecy Order pursuant to 37 CFR 5.2 (Paper filers only. Applications that fall under Secrecy Order may not be filed electronically.)

Inventor Information:

Inventor 1 Remove									
Legal I	Legal Name								
Prefix	Give	en Name		Middle Nam	е		Family	/ Name	Suffix
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Resid	lence	Information ((Select One) 🔘	US Residency	۲	Non US R	esidency	Active US Military Service	e
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	1			I				1	
Mailing	Addr	ess of Invent	tor:						
Addre	ss 1		No.11, Jingke Rd	., Nantun Distric	t				
Addre	ss 2								
City		Taichung				State/Pro	vince		
Postal	l Code	5	408		Cou	intry i	TW		
	All Inventors Must Be Listed - Additional Inventor Information blocks may be generated within this form by selecting the Add button.								

Correspondence Information:

Enter either Customer Number or complete the Correspondence Information section below. For further information see 37 CFR 1.33(a).				
An Address is being provided for the correspondence Information of this application.				
Customer Number	24728			
Email Address	mmmipdocket@system.foundationip.com	Add Email	Remove Email	

Application Information:

Title of the Invention	IMAGE CAPTURIN	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL			
Attorney Docket Number	14970-94702	14970-94702 Small Entity Status Claimed			
Application Type	Nonprovisional	Nonprovisional			
Subject Matter	Utility	Utility			
Total Number of Drawing Sheets (if any)		23	Suggested Figure for Publication (if any)	1A	

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Application Da	ta Sheet 37 CFR 1.76	Attorney Docket Number	14970-94702
		Application Number	
Title of Invention	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL		

Publication Information:

Request Early Publication (Fee required at time of Request 37 CFR 1.219)
 Request Not to Publish. I hereby request that the attached application not be published under

35 U.S.C. 122(b) and certify that the invention disclosed in the attached application has not and will not be the subject of an application filed in another country, or under a multilateral international agreement, that requires publication at eighteen months after filing.

Representative Information:

Representative information should be provided for all practitioners having a power of attorney in the application. Providing this information in the Application Data Sheet does not constitute a power of attorney in the application (see 37 CFR 1.32). Either enter Customer Number or complete the Representative Name section below. If both sections are completed the customer Number will be used for the Representative Information during processing.

Please Select One:	Oustomer Number	O US Patent Practitioner	Limited Recognition (37 CFR 11.9)
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Application Da	ta Shoot 37 CED 1 76	Attorney Docket Number	14970-94702		
Application Data Sheet 37 CFR 1.76		Application Number			
Title of Invention	IMAGE CAPTURING LENS S	SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL			

Statement under 37 CFR 1.55 or 1.78 for AIA (First Inventor to File) Transition Applications

This application (1) claims priority to or the benefit of an application filed before March 16, 2013 and (2) also contains, or contained at any time, a claim to a claimed invention that has an effective filing date on or after March 16, 2013.

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Application Data Sheet 37 CFR 1.76			Application Nu	mber		
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IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL

RELATED APPLICATIONS

5 This application claims priority to Taiwan Application Serial Number 102139029, filed October 29, 2013, which is incorporated by reference herein in its entirety.

BACKGROUND

10 Technical Field

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The present disclosure relates to an image capturing lens system. More particularly, the present disclosure relates to a compact image capturing lens system applicable to a mobile terminal.

15 Description of Related Art

In recent years, with the popularity of mobile terminals having camera functionalities, the demand of miniaturized optical systems has been increasing. As the advanced semiconductor manufacturing technologies have allowed the pixel size of sensors to be reduced and compact optical systems have gradually

20 evolved toward the field of higher megapixels, there is an increasing demand for compact optical systems featuring better image quality.

A conventional compact optical system in a portable electronic product typically utilizes a three-element lens structure. Due to the popularity of mobile products with high-end specifications, such as smart phones, tablet personal computers, wearable apparatus and other high-end mobile terminals, the

requirements for high resolution and image quality of present compact optical systems increase significantly. However, the conventional optical systems cannot satisfy these requirements of the compact optical systems.

Another conventional compact optical system provides a four-element lens structure. However, it is hard to make a good balance between obtaining a large field of view and a short total track length. Furthermore, it is also not favorable for the resolving power and illumination in a peripheral region of an image; therefore, it cannot satisfy the requirements of the compact optical systems featuring better image quality.

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SUMMARY

According to one aspect of the present disclosure, an image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The first lens element has refractive power. The second lens element with 15 positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with refractive power has a concave image-side surface in a paraxial region thereof, wherein 20 both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive power. When an axial distance between an object-side surface of the first lens element and the 25

image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, a focal length of the second lens element is f2, and a focal length of the third lens element is f3, the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and

f2/f3 < -0.65.

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10 According to another aspect of the present disclosure, an image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The first lens element has refractive power. The second lens element with positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power 15 has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with refractive power has a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens 20 element has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive power. When an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal 25

length of the image capturing lens system is f, a focal length of the fourth lens element is f4, and a focal length of the third lens element is f3, the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and

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-2.0 < f/f3 < -0.95.

According to still another aspect of the present disclosure, an image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens 10 element. The first lens element has refractive power. The second lens element with positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with 15 refractive power has a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive 20 power. When an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens

element is f4, and an f-number of the image capturing lens system is Fno, the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

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|f/f4| < 1.20; and

1.40 < Fno ≤ 2.25.

According to yet another aspect of the present disclosure, an imaging device includes the image capturing lens system according to the aforementioned aspect and an image sensor, wherein the image sensor is located on an image plane of the image capturing lens system.

According to still yet another aspect of the present disclosure, a mobile terminal includes the imaging device according to the aforementioned aspect.

BRIEF DESCRIPTION OF THE DRAWINGS

15 The disclosure can be more fully understood by reading the following detailed description of the embodiments, with reference made to the accompanying drawings as follows:

Fig. 1A is a schematic view of an imaging device according to the 1st embodiment of the present disclosure;

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Fig. 1B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 1st embodiment;

Fig. 2A is a schematic view of an imaging device according to the 2nd embodiment of the present disclosure;

Fig. 2B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 2nd embodiment;

Fig. 3A is a schematic view of an imaging device according to the 3rd embodiment of the present disclosure;

Fig. 3B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 3rd embodiment;

Fig. 4A is a schematic view of an imaging device according to the 4th embodiment of the present disclosure;

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Fig. 4B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 4th embodiment;

Fig. 5A is a schematic view of an imaging device according to the 5th embodiment of the present disclosure;

Fig. 5B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 5th embodiment;

Fig. 6A is a schematic view of an imaging device according to the 6th embodiment of the present disclosure;

Fig. 6B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 6th embodiment;

Fig. 7A is a schematic view of an imaging device according to the 7th embodiment of the present disclosure;

Fig. 7B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 7th embodiment;

Fig. 8A is a schematic view of an imaging device according to the 8th embodiment of the present disclosure;

Fig. 8B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 8th embodiment;

Fig. 9A is a schematic view of an imaging device according to the 9th embodiment of the present disclosure;

Fig. 9B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 9th embodiment;

5 Fig. 10A is a schematic view of an imaging device according to the 10th embodiment of the present disclosure;

Fig. 10B shows spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 10th embodiment;

Fig. 11A shows a smart phone with an imaging device of the present disclosure installed therein;

Fig. 11B shows a tablet personal computer with an imaging device of the present disclosure installed therein; and

Fig. 11C shows a wearable device with an imaging device of the present disclosure installed therein.

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DETAILED DESCRIPTION

An image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The image capturing lens system has a total of four lens elements with refractive power.

The first lens element can have positive refractive power, so that it provides the image capturing lens system with the positive refractive power as it needs to be so as to reduce the total track length of the image capturing lens system. The first lens element can have a convex object-side surface in a

paraxial region thereof, so that it is favorable for further reducing the total track length.

The second lens element has positive refractive power, so that it is favorable for the second lens element adjusting the light gathering ability of the first lens element. The second lens element has a convex image-side surface in a paraxial region thereof, so that it is favorable for correcting the astigmatism of the image capturing lens system.

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The third lens element has negative refractive power, so that it is favorable for correcting the aberration of the image capturing lens system. The third lens element has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof, so that it is favorable for correcting the astigmatism of the image capturing lens system.

The fourth lens element can have a convex object-side surface in a paraxial region thereof and has a concave image-side surface in a paraxial region thereof. Furthermore, the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof. Therefore, it is favorable for correcting the astigmatism and aberration of the off-axis.

When an axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied: 0.5 mm < Td < 3.2 mm. Therefore, it is favorable for keeping the image capturing lens system compact. Preferably, the following condition is satisfied: 0.8 mm < Td < 2.5 mm.

When the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and half of a maximal field of view of the image capturing lens system is HFOV, the

following condition is satisfied: 1.0 mm < Td/tan(HFOV) < 3.75 mm. Therefore, it is favorable for obtaining a large field of view and short total track length for the image capturing lens system. Preferably, the following condition is satisfied: 1.2 mm < Td/tan(HFOV) < 2.75 mm.

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When a focal length of the image capturing lens system is f, and a focal length of the fourth lens element is f4, the following condition is satisfied: |f/f4| < 1.20. Therefore, it is favorable for the principal point of the image capturing lens system being positioned away from the image plane so as to reduce the total track length and keep the image capturing lens system compact.

When a focal length of the second lens element is f2, and a focal length of the third lens element is f3, the following condition is satisfied: f2/f3 < -0.65. Therefore, it is favorable for balancing the refractive powers of the second lens element and the third lens element so as to correct the aberration and reduce the photosensitivity. Preferably, the following condition is satisfied: f2/f3 < -0.75.

When the focal length of the image capturing lens system is f, and the focal length of the third lens element is f3, the following condition is satisfied: -2.0 < f/f3 < -0.95. Therefore, the third lens element serves as a correcting lens for balancing and correcting the aberrations of the image capturing lens system so as to obtain better image quality.

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When an f-number of the image capturing lens system is Fno, and the following condition is satisfied: $1.40 < Fno \le 2.25$. Therefore, it is favorable for improving the illumination in a peripheral region of the image capturing lens system.

When the focal length of the image capturing lens system is f, and a focal length of the first lens element is f1, the following condition is satisfied: -0.25 <f/f1 < 0.75. Therefore, the first lens element will have a more proper refractive power so as to avoid excess photosensitivity. Preferably, the following condition is satisfied: 0.25 < f/f1 < 0.75.

When a curvature radius of the object-side surface of the second lens element is R3, and a curvature radius of the image-side surface of the second lens element is R4, the following condition is satisfied: 0.5 < (R3+R4)/(R3-R4) <2.5. Therefore, it is favorable for further correcting the aberration of the image

10 capturing lens system.

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When the focal length of the image capturing lens system is f, and the following condition is satisfied: 0.5 mm < f < 2.0 mm. Therefore, it is favorable for providing a proper total track length.

When a sum of the central thicknesses of the first lens element, the second lens element, the third lens element, and the fourth lens element is ΣCT , 15 and the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, the following condition is satisfied: $0.80 < \Sigma CT/Td < 0.95$. Therefore, it is favorable for assembling the lens elements of the image capturing lens system so as to reduce the photosensitivity.

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When an Abbe number of the first lens element is V1, and the following condition is satisfied: 45 < V1. Therefore, it is favorable for correcting the chromatic aberration of the image capturing lens system.

When a central thickness of the second lens element is CT2, a central thickness of the first lens element is CT1, a central thickness of the third lens 25

element is CT3, and a central thickness of the fourth lens element is CT4, the following condition is satisfied: 0.65 < CT2/(CT1+CT3+CT4) < 2.0. Therefore, the thickness of each lens element is favorable for manufacturing and assembling the lens elements.

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When a maximal field of view of the image capturing lens system is FOV, and the following condition is satisfied: 80 degrees < FOV < 110 degrees. Therefore, it is favorable for obtaining enough field of view.

According to the image capturing lens system of the present disclosure, the lens elements thereof can be made of glass or plastic material. When the lens elements are made of glass material, the distribution of the refractive power of the image capturing lens system may be more flexible to design. When the lens elements are made of plastic material, the manufacturing cost can be effectively reduced. Furthermore, surfaces of each lens element can be arranged to be aspheric, since the aspheric surface of the lens element is easy to form a shape other than spherical surface so as to have more controllable variables for eliminating the aberration thereof, and to further decrease the required number of the lens elements. Therefore, the total track length of the image capturing lens system can also be reduced.

According to the image capturing lens system of the present disclosure, each of an object-side surface in a paraxial region thereof and an image-side surface has a paraxial region and an off-axis region. The paraxial region refers to the region of the surface where light rays travel close to the optical axis, and the off-axis region refers to the region of the surface where light rays travel away from the optical axis. Particularly, when the lens element has a convex

surface, it indicates that the surface is convex in the paraxial region thereof;

when the lens element has a concave surface, it indicates that the surface is concave in the paraxial region thereof.

According to the image capturing lens system of the present disclosure, the image capturing lens system can include at least one stop, such as an aperture stop, a glare stop or a field stop. Said glare stop or said field stop is for eliminating the stray light and thereby improving the image resolution thereof.

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According to the image capturing lens system of the present disclosure, an aperture stop can be configured as a front stop or a middle stop. A front stop disposed between an imaged object and the first lens element can provide a longer distance between an exit pupil of the image capturing lens system and the image plane and thereby improves the image-sensing efficiency of an image sensor. A middle stop disposed between the first lens element and the image plane is favorable for enlarging the field of view of the image capturing lens system and thereby provides a wider field of view for the same.

The present image capturing lens system can be optionally applied to moving focus optical systems. According to the image capturing lens system of the present disclosure, the image capturing lens system is featured with good correction ability and high image quality, and can be applied to 3D 20 (three-dimensional) image capturing applications, in products such as digital cameras, mobile devices, digital tablets, wearable devices and other mobile terminals.

According to the present disclosure, an imaging device is provided. The imaging device includes the image capturing lens system according to the aforementioned image capturing lens system of the present disclosure, and an

image sensor, wherein the image sensor is disposed on an image plane of the aforementioned image capturing lens system. As a result, it is favorable for reducing the total track length of the image capturing lens system while obtaining large field of view. Furthermore, it is also favorable for improving the resolving power and illumination so as to achieve the best image quality. Preferably, the imaging device can further include a barrel member, a holding member or a combination thereof.

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According to the present disclosure, a mobile terminal is provided, wherein the mobile terminal includes the aforementioned imaging device. The imaging device includes the image capturing lens system according to the aforementioned image capturing lens system of the present disclosure, and the image sensor, wherein the image sensor is disposed on an image plane of the aforementioned image capturing lens system. As a result, it is favorable for reducing the total track length of the image capturing lens system while obtaining large field of view. Furthermore, it is also favorable for improving the resolving power and illumination so as to achieve the best image quality.

In Fig. 11A, Fig. 11B and Fig. 11C, an imaging device 1101 may be installed in but not limited to a mobile terminal, including a smart phone 1110, a tablet personal computer 1120 or a wearable device 1130. The three exemplary figures of different kinds of mobile terminal are only exemplary for showing the imaging device of present disclosure installing in a mobile terminal and is not limited thereto. Preferably, the mobile terminal can further include but not limited to display, control unit, random access memory unit (RAM) a read only memory unit (ROM) or a combination thereof.

According to the above description of the present disclosure, the following 1st – 10th specific embodiments are provided for further explanation.

1st Embodiment

5 Fig. 1A is a schematic view of an imaging device according to the 1st embodiment of the present disclosure. Fig. 1B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 1st embodiment.

In Fig. 1A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 170. The image capturing lens system includes, in order from an object side to an image side, a first lens element 110, an aperture stop 100, a second lens element 120, a third lens element 130, a fourth lens element 140, an IR-cut filter 150 and an image plane 160, wherein the image capturing lens system has a total of four lens elements (110-140) with refractive power.

The first lens element 110 with positive refractive power has a convex object-side surface 111 in a paraxial region thereof and a concave image-side surface 112 in a paraxial region thereof, which are both aspheric, and the first lens element 110 is made of plastic material.

The second lens element 120 with positive refractive power has a convex object-side surface 121 in a paraxial region thereof and a convex image-side surface 122 in a paraxial region thereof, which are both aspheric, and the second lens element 120 is made of plastic material.

The third lens element 130 with negative refractive power has a concave object-side surface 131 in a paraxial region thereof and a convex image-side

surface 132 in a paraxial region thereof, which are both aspheric, and the third lens element 130 is made of plastic material.

The fourth lens element 140 with positive refractive power has a convex object-side surface 141 in a paraxial region thereof and a concave image-side surface 142 in a paraxial region thereof, which are both aspheric, and the fourth lens element 140 is made of plastic material. Furthermore, the image-side surface 142 of the fourth lens element 140 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 150 is made of glass and located between the fourth lens element 140 and the image plane 160, and will not affect the focal length of the image capturing lens system. The image sensor 170 is disposed on the image plane 160 of the image capturing lens system.

The equation of the aspheric surface profiles of the aforementioned lens elements of the 1st embodiment is expressed as follows:

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$$X(Y) = (Y^{2}/R)/(1 + sqrt(1 - (1 + k) \times (Y/R)^{2})) + \sum_{i} (Ai) \times (Y^{i})$$

, where,

X is the relative distance between a point on the aspheric surface spaced at a distance Y from the optical axis and the tangential plane at the aspheric surface vertex on the optical axis;

Y is the vertical distance from the point on the aspheric surface to the optical axis;

R is the curvature radius;

k is the conic coefficient; and

25 Ai is the i-th aspheric coefficient.

In the image capturing lens system of the imaging device according to the 1st embodiment, when a focal length of the image capturing lens system is f, an f-number of the image capturing lens system is Fno, and half of a maximal field of view of the image capturing lens system is HFOV, these parameters

In the image capturing lens system of the imaging device according to the 1st embodiment, when an Abbe number of the first lens element 110 is V1, the following condition is satisfied: V1 = 21.4.

have the following values: f = 1.17 mm; Fno = 2.20; and HFOV = 46.7 degrees.

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In the image capturing lens system according to the 1st embodiment, when a central thickness of the second lens element 120 is CT2, a central thickness of the first lens element 110 is CT1, a central thickness of the third lens element 130 is CT3, and a central thickness of the fourth lens element 140 is CT4, the following condition is satisfied: CT2/(CT1+CT3+CT4) = 0.69.

- In the image capturing lens system according to the 1st embodiment, when a curvature radius of the object-side surface 121 of the second lens element 120 is R3, and a curvature radius of the image-side surface 122 of the second lens element 120 is R4, the following condition is satisfied: (R3+R4)/(R3-R4) = 0.85.
- In the image capturing lens system of the imaging device according to the 1st embodiment, when the focal length of the image capturing lens system is f, and a focal length of the first lens element 110 is f1, the following condition is satisfied: f/f1 = 0.12.

In the image capturing lens system of the imaging device according to the 1st embodiment, when a focal length of the second lens element 120 is f2,

and a focal length of the third lens element 130 is f3, the following condition is satisfied: f2/f3 = -0.77.

In the image capturing lens system of the imaging device according to the 1st embodiment, when the focal length of the image capturing lens system is f, and a focal length of the fourth lens element 140 is f4, the following condition is satisfied: |f/f4| = 0.77.

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In the image capturing lens system of the imaging device according to the 1st embodiment, when the focal length of the image capturing lens system is f, and the focal length of the third lens element 130 is f3, the following condition is satisfied: f/f3 = -1.10.

In the image capturing lens system according to the 1st embodiment, when an axial distance between the object-side surface 111 of the first lens element 110 and the image-side surface 142 of the fourth lens element 140 is Td, the following condition is satisfied: Td = 1.850 mm.

In the image capturing lens system according to the 1st embodiment, when a sum of the central thicknesses of the first lens element 110, the second lens element 120, the third lens element 130, and the fourth lens element 140 is Σ CT, and the axial distance between the object-side surface 111 of the first lens element 110 and the image-side surface 142 of the fourth lens element 140 is

Td, the following condition is satisfied: $\Sigma CT/Td = 0.89$.

In the image capturing lens system according to the 1st embodiment, when the axial distance between the object-side surface 111 of the first lens element 110 and the image-side surface 142 of the fourth lens element 140 is Td, and half of the maximal field of view of the image capturing lens system is HFOV, the following condition is satisfied: Td/tan(HFOV) = 1.74 mm.

In the image capturing lens system of the imaging device according to the 1st embodiment, when a maximal field of view of the image capturing lens system is FOV, the following condition is satisfied: FOV = 93.4 degrees.

The detailed optical data of the 1st embodiment are shown in Table 1 and the aspheric surface data are shown in Table 2 below.

TABLE 1								
Embodiment 1								
f = 1.17 mm, Fno = 2.20, HFOV = 46.7 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Pla	ano	Infinity				
1	Lens 1	1.666	ASP	0.256	Plastic	1.650	21.4	9.56
2		2.139	ASP	0.031				
3	Ape. Stop	Pla	ano	0.019				
4	Lens 2	5.712	ASP	0.671	Plastic	1.544	55.9	0.82
5		-0.464	ASP	0.130				
6	Lens 3	-0.228	ASP	0.230	Plastic	1.634	23.8	-1.06
7		-0.480	ASP	0.030				
8	Lens 4	0.679	ASP	0.483	Plastic	1.535	55.7	1.52
9		3.062	ASP	0.300				
10	10 IR-cut filter Plano			0.145	Glass	1.517	64.2	-
11		Pla	ano	0.204				
12	Image	Pla	ano	-				
lote: Refere	ence wavelen	gth is 587	.6 nm (d-l	ine).			•	

	TABLE 2								
	Aspheric Coefficients								
Surface #	1	2	4	5					
k =	1.2237E+00	1.7244E+01	9.0000E+01	-6.9311E-01					
A4 =	3.1416E-01	1.1703E+00	-4.1498E-01	-6.9345E-01					
A6 =	-1.0010E+00	-2.0080E+01	3.6416E+00	1.3202E+00					
A8 =	4.5872E+01	5.2569E+02	4.3035E+01	1.0955E+01					
A10 =	-5.9339E+02	-3.0044E+03	-7.4996E+03	-3.8285E+02					
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0040E+03					
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04					
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04					
Surface #	6	7	8	9					

k =	-9.8477E-01	-3.2669E+00	-6.1619E-01	-1.4636E+01
A4 =	3.5682E+00	-1.8915E+00	-1.2870E+00	1.2883E+00
A6 =	-3.7958E+00	8.7075E+00	3.1244E+00	-3.7603E+00
A8 =	-1.1135E+02	-3.6761E+01	-9.1933E+00	5.9040E+00
A10 =	1.5862E+03	1.7257E+02	1.7146E+01	-5.8521E+00
A12 =	-8.7685E+03	-4.8146E+02	-1.9850E+01	3.5356E+00
A14 =	2.3054E+04	6.7728E+02	1.2752E+01	-1.1759E+00
A16 =	-2.3557E+04	-3.6747E+02	-3.5165E+00	1.6169E-01

In Table 1, the curvature radius, the thickness and the focal length are shown in millimeters (mm). Surface numbers 0-12 represent the surfaces sequentially arranged from the object-side to the image-side along the optical axis. In Table 2, k represents the conic coefficient of the equation of the aspheric surface profiles. A1-A16 represent the aspheric coefficients ranging from the 1st order to the 16th order. The tables presented below for each embodiment are the corresponding schematic parameter and aberration curves, and the definitions of the tables are the same as Table 1 and Table 2 of the 1st embodiment. Therefore, an explanation in this regard will not be provided again.

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2nd Embodiment

Fig. 2A is a schematic view of an imaging device according to the 2nd embodiment of the present disclosure. Fig. 2B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 2nd embodiment.

In Fig. 2A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 20 270. The image capturing lens system includes, in order from an object side to an image side, a first lens element 210, an aperture stop 200, a second lens element 220, a third lens element 230, a fourth lens element 240, an IR-cut filter 250 and an image plane 260, wherein the image capturing lens system has a total of four lens elements (210-240) with refractive power.

The first lens element 210 with positive refractive power has a convex object-side surface 211 in a paraxial region thereof and a concave image-side surface 212 in a paraxial region thereof, which are both aspheric, and the first lens element 210 is made of plastic material.

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The second lens element 220 with positive refractive power has a convex object-side surface 221 in a paraxial region thereof and a convex image-side surface 222 in a paraxial region thereof, which are both aspheric, and the second lens element 220 is made of plastic material.

The third lens element 230 with negative refractive power has a concave object-side surface 231 in a paraxial region thereof and a convex image-side surface 232 in a paraxial region thereof, which are both aspheric, and the third lens element 230 is made of plastic material.

The fourth lens element 240 with positive refractive power has a convex object-side surface 241 in a paraxial region thereof and a concave image-side surface 242 in a paraxial region thereof, which are both aspheric, and the fourth lens element 240 is made of plastic material. Furthermore, the image-side surface 242 of the fourth lens element 240 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 250 is made of glass and located between the fourth lens element 240 and the image plane 260, and will not affect the focal length of the

image capturing lens system. The image sensor 270 is disposed on the image plane 260 of the image capturing lens system.

The detailed optical data of the 2nd embodiment are shown in Table 3 and the aspheric surface data are shown in Table 4 below.

	TABLE 3								
Embodiment 2									
	f = 1.23 mm, Fno = 2.45, HFOV = 45.6 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ano	Infinity					
1	Lens 1	1.728	ASP	0.217	Plastic	1.640	22.0	1207.16	
2		1.647	ASP	0.041					
3	Ape. Stop	Pla	no	0.020					
4	Lens 2	2.201	ASP	0.685	Plastic	1.544	55.9	0.78	
5		-0.465	ASP	0.138					
6	Lens 3	-0.213	ASP	0.222	Plastic	1.634	23.8	-0.90	
7		-0.479	ASP	0.030					
8	Lens 4	0.691	ASP	0.430	Plastic	1.535	55.7	1.40	
9		7.112	ASP	0.300					
10	IR-cut filter	no	0.300	Glass	1.517	64.2	-		
11		Pla	ano	0.171					
12	Image	Pla	ino	-					
Note: Refere	ence wavelen	gth is 587	.6 nm (d-l	ine).					

	TABLE 4								
Aspheric Coefficients									
Surface #	1	2	4	5					
k =	-7.8611E-01	2.2256E+01	4.4287E+01	-6.8249E-01					
A4 =	2.7433E-01	3.5449E-01	-1.1581E+00	-5.9944E-01					
A6 =	-1.5466E+00	-2.9377E+01	8.9406E-01	3.6061E-01					
A8 =	4.7455E+01	6.4129E+02	4.1870E+01	1.6896E+01					
A10 =	-6.0092E+02	-3.8207E+03	-7.3180E+03	-3.8194E+02					
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0043E+03					
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04					
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04					
Surface #	6	7	8	9					
k =	-1.0107E+00	-3.0532E+00	-7.4231E-01	2.2155E+01					
A4 =	3.8803E+00	-1.7079E+00	-1.1152E+00	1.6267E+00					
A6 =	-4.2860E+00	8.7245E+00	2.9613E+00	-4.5228E+00					
A8 =	-1.1314E+02	-3.7291E+01	-9.2058E+00	6.4630E+00					

A10 =	1.5859E+03	1.7181E+02	1.7048E+01	-5.8730E+00
A12 =	-8.7686E+03	-4.8143E+02	-1.9563E+01	3.4083E+00
A14 =	2.3054E+04	6.7878E+02	1.3110E+01	-1.1920E+00
A16 =	-2.3557E+04	-3.6776E+02	-4.1607E+00	1.9105E-01

In the 2nd embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 2nd embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 3 and Table 4 as the following values and satisfy the following conditions:

2nd Embodiment							
f [mm]	1.23	f2/f3	-0.87				
Fno	2.45	f/f4	0.88				
HFOV [deg.]	45.6	f/f3	-1.37				
V1	22.0	Td [mm]	1.783				
CT2/(CT1+CT3+CT4)	0.79	ΣCT/Td	0.87				
(R3+R4)/(R3-R4)	0.65	Td/tan(HFOV) [mm]	1.75				
f/f1	0.00	FOV [deg.]	91.2				

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3rd Embodiment

Fig. 3A is a schematic view of an imaging device according to the 3rd embodiment of the present disclosure. Fig. 3B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 3rd embodiment.

In Fig. 3A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

370. The image capturing lens system includes, in order from an object side to an image side, a first lens element 310, an aperture stop 300, a second lens element 320, a third lens element 330, a fourth lens element 340, an IR-cut filter 350 and an image plane 360, wherein the image capturing lens system has a total of four lens elements (310-340) with refractive power.

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The first lens element 310 with positive refractive power has a convex object-side surface 311 in a paraxial region thereof and a concave image-side surface 312 in a paraxial region thereof, which are both aspheric, and the first lens element 310 is made of plastic material.

- The second lens element 320 with positive refractive power has a concave object-side surface 321 in a paraxial region thereof and a convex image-side surface 322 in a paraxial region thereof, which are both aspheric, and the second lens element 320 is made of plastic material.
- The third lens element 330 with negative refractive power has a concave object-side surface 331 in a paraxial region thereof and a convex image-side surface 332 in a paraxial region thereof, which are both aspheric, and the third lens element 330 is made of plastic material.

The fourth lens element 340 with positive refractive power has a convex object-side surface 341 in a paraxial region thereof and a concave image-side surface 342 in a paraxial region thereof, which are both aspheric, and the fourth lens element 340 is made of plastic material. Furthermore, the image-side surface 342 of the fourth lens element 340 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 350 is made of glass and located between the fourth lens element 340 and the image plane 360, and will not affect the focal length of the

image capturing lens system. The image sensor 370 is disposed on the image plane 360 of the image capturing lens system.

The detailed optical data of the 3rd embodiment are shown in Table 5 and the aspheric surface data are shown in Table 6 below.

TABLE 5								
Embodiment 3								
f = 1.66 mm, Fno = 2.15, HFOV = 46.8 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Pla	ino	Infinity				
1	Lens 1	1.333	ASP	0.286	Plastic	1.544	55.9	2.50
2		59.851	ASP	0.005				
3	Ape. Stop	Pla	ino	0.195				
4	Lens 2	-1.920	ASP	0.409	Plastic	1.544	55.9	1.60
5		-0.644	ASP	0.156				
6	Lens 3	-0.263	ASP	0.200	Plastic	1.650	21.4	-1.49
7		-0.470	ASP	0.030				
8	Lens 4	0.677	ASP	0.363	Plastic	1.535	55.7	2.33
9		1.206	ASP	0.400				
10	IR-cut filter	Pla	ino	0.175	Glass	1.517	64.2	-
11		Pla	ino	0.431				
12 Image Plano -								
Note: Reference wavelength is 587.6 nm (d-line).								
The effective	e radius of Su	irface 1 is	0.510 mm	۱.				

	TABLE 6								
	Aspheric Coefficients								
Surface #	1	2	4	5					
k =	-2.4704E+00	9.0000E+01	5.8947E+00	-3.7972E-01					
A4 =	-3.4848E-02	-3.8775E-01	-9.3075E-01	-3.3741E-01					
A6 =	-4.4471E-01	-2.8417E+00	3.6516E+00	9.2277E-01					
A8 =	-4.9925E-01	1.8185E+01	-4.0769E+01	-3.9461E+00					
A10 =	-1.2166E+01	-2.0954E+01	-4.4351E+00	-1.9037E+01					
A12 =	3.9114E+01	-1.4998E+03	1.2130E+03	4.9148E+01					
A14 =	-1.7950E+02	1.2389E+04	-4.4615E+03	1.0076E+02					
A16 =	3.3572E+02	-2.9058E+04	6.2425E+03	8.0489E+01					
Surface #	6	7	8	9					
k =	-1.1491E+00	-2.3808E+00	-1.7649E+00	-1.0689E+01					
A4 =	4.2079E+00	2.1562E-01	-6.9591E-01	9.1971E-01					
A6 =	-2.8310E+01	-4.4239E+00	1.2041E+00	-3.0958E+00					

A8 =	1.2287E+02	1.8790E+01	-2.9023E+00	4.8713E+00
A10 =	-3.9035E+02	-4.1840E+01	4.4195E+00	-4.6279E+00
A12 =	8.5064E+02	5.5883E+01	-3.7857E+00	2.6418E+00
A14 =	-9.7331E+02	-4.0255E+01	1.6532E+00	-8.3581E-01
A16 =	4.7213E+02	1.4428E+01	-2.8192E-01	1.1204E-01

In the 3rd embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 3rd embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 5 and Table 6 as the following values and satisfy the following conditions:

3rd Embodiment					
f [mm]	1.66	f2/f3	-1.07		
Fno	2.15	f/f4	0.71		
HFOV [deg.]	46.8	f/f3	-1.11		
V1	55.9	Td [mm]	1.644		
CT2/(CT1+CT3+CT4)	0.48	ΣCT/Td	0.77		
(R3+R4)/(R3-R4)	2.01	Td/tan(HFOV) [mm]	1.54		
f/f1	0.66	FOV [deg.]	93.6		

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4th Embodiment

Fig. 4A is a schematic view of an imaging device according to the 4th embodiment of the present disclosure. Fig. 4B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 4th embodiment.

In Fig. 4A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 470. The image capturing lens system includes, in order from an object side to an image side, a first lens element 410, an aperture stop 400, a second lens element 420, a third lens element 430, a fourth lens element 440, an IR-cut filter 450 and an image plane 460, wherein the image capturing lens system has a total of four lens elements (410-440) with refractive power.

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The first lens element 410 with negative refractive power has a convex object-side surface 411 in a paraxial region thereof and a concave image-side surface 412 in a paraxial region thereof, which are both aspheric, and the first lens element 410 is made of plastic material.

The second lens element 420 with positive refractive power has a convex object-side surface 421 in a paraxial region thereof and a convex image-side surface 422 in a paraxial region thereof, which are both aspheric, and the second lens element 420 is made of plastic material.

The third lens element 430 with negative refractive power has a concave object-side surface 431 in a paraxial region thereof and a convex image-side surface 432 in a paraxial region thereof, which are both aspheric, and the third lens element 430 is made of plastic material.

The fourth lens element 440 with positive refractive power has a convex object-side surface 441 in a paraxial region thereof and a concave image-side surface 442 in a paraxial region thereof, which are both aspheric, and the fourth lens element 440 is made of plastic material. Furthermore, the image-side surface 442 of the fourth lens element 440 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 450 is made of glass and located between the fourth lens element 440 and the image plane 460, and will not affect the focal length of the

image capturing lens system. The image sensor 470 is disposed on the image plane 460 of the image capturing lens system.

The detailed optical data of the 4th embodiment are shown in Table 7 and the aspheric surface data are shown in Table 8 below.

TABLE 7								
Embodiment 4								
f = 1.15 mm, Fno = 2.22, HFOV = 48.5 deg.								
Surface #		Curvature Radius		Thickness	Material	Index	Abbe #	Focal Length
0	Object	Pla	ano	Infinity				
1	Lens 1	1.999	ASP	0.200	Plastic	1.544	55.9	-46.83
2		1.789	ASP	0.021				
3	Ape. Stop	Plano		0.037				
4	Lens 2	1.606	ASP	0.471	Plastic	1.544	55.9	0.81
5		-0.543	ASP	0.184				
6	Lens 3	-0.207	ASP	0.209	Plastic	1.634	23.8	-1.22
7		-0.393	ASP	0.030				
8	Lens 4	0.747	ASP	0.319	Plastic	1.535	55.7	1.62
9		4.607	ASP	0.300				
10	IR-cut filter	Plano		0.300	Glass	1.517	64.2	-
11		Plano		0.130				
12	Image	Plano		-				
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).							

TABLE 8						
	Aspheric Coefficients					
Surface #	1	2	4	5		
k =	-2.2996E+01	3.4247E+01	9.8701E+00	-4.2975E-01		
A4 =	-2.1353E-01	-2.0670E+00	-2.2221E+00	-6.3795E-01		
A6 =	-3.6880E+00	-3.6063E+01	-8.7081E+00	-6.5092E+00		
A8 =	5.2789E+01	6.9201E+02	1.4888E+02	4.6114E+01		
A10 =	-6.4083E+02	-4.8238E+03	-8.2602E+03	-4.7532E+02		
A12 =	4.0983E+03	-1.6432E+05	1.3290E+05	3.0044E+03		
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0679E+04		
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3828E+04		
Surface #	6	7	8	9		
k =	-1.0439E+00	-2.0056E+00	-6.4024E-01	-3.3636E+00		
A4 =	4.2327E+00	-9.7476E-01	-8.3147E-01	1.0958E+00		
A6 =	-3.4551E+00	1.0236E+01	2.1761E+00	-1.7086E+00		
A8 =	-1.0303E+02	-3.7610E+01	-4.8336E+00	1.3575E+00		

A10 =	1.5970E+03	1.6620E+02	5.0397E+00	-2.6285E+00
A12 =	-8.9315E+03	-4.9093E+02	-4.1411E+00	4.3863E+00
A14 =	2.3054E+04	6.8046E+02	3.4069E+00	-3.3963E+00
A16 =	-2.3558E+04	-3.4010E+02	-1.6576E+00	9.5967E-01

In the 4th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 4th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 7 and Table 8 as the following values and satisfy the following conditions:

4th Embodiment					
f [mm]	1.15	f2/f3	-0.66		
Fno	2.22	f/f4	0.71		
HFOV [deg.]	48.5	f/f3	-0.94		
V1	55.9	Td [mm]	1.471		
CT2/(CT1+CT3+CT4)	0.65	ΣCT/Td	0.82		
(R3+R4)/(R3-R4)	0.49	Td/tan(HFOV) [mm]	1.30		
f/f1	-0.02	FOV [deg.]	97.0		

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5th Embodiment

Fig. 5A is a schematic view of an imaging device according to the 5th embodiment of the present disclosure. Fig. 5B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 5th embodiment.

In Fig. 5A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 570. The image capturing lens system includes, in order from an object side to an image side, a first lens element 510, an aperture stop 500, a second lens element 520, a third lens element 530, a fourth lens element 540, an IR-cut filter 550 and an image plane 560, wherein the image capturing lens system has a total of four lens elements (510-540) with refractive power.

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The first lens element 510 with negative refractive power has a convex object-side surface 511 in a paraxial region thereof and a concave image-side surface 512 in a paraxial region thereof, which are both aspheric, and the first lens element 510 is made of glass material.

The second lens element 520 with positive refractive power has a convex object-side surface 521 in a paraxial region thereof and a convex image-side surface 522 in a paraxial region thereof, which are both aspheric, and the second lens element 520 is made of glass material.

The third lens element 530 with negative refractive power has a concave object-side surface 531 in a paraxial region thereof and a convex image-side surface 532 in a paraxial region thereof, which are both aspheric, and the third lens element 530 is made of plastic material.

The fourth lens element 540 with positive refractive power has a convex object-side surface 541 in a paraxial region thereof and a concave image-side surface 542 in a paraxial region thereof, which are both aspheric, and the fourth lens element 540 is made of plastic material. Furthermore, the image-side surface 542 of the fourth lens element 540 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 550 is made of glass and located between the fourth lens element 540 and the image plane 560, and will not affect the focal length of the

image capturing lens system. The image sensor 570 is disposed on the image plane 560 of the image capturing lens system.

The detailed optical data of the 5th embodiment are shown in Table 9 and the aspheric surface data are shown in Table 10 below.

	TABLE 9								
	Embodiment 5								
	f = 2.24 mm, Fno = 2.51, HFOV = 44.2 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ano	Infinity					
1	Lens 1	1.367	ASP	0.300	Glass	2.144	17.8	-13.68	
2		1.110	ASP	0.144					
3	Ape. Stop	Pla	Plano						
4	Lens 2	3.909	ASP	1.483	Glass	1.525	70.3	1.60	
5		-0.932	ASP	0.325					
6	Lens 3	-0.341	ASP	0.277	Plastic	1.639	23.5	-1.72	
7		-0.651	ASP	0.030					
8	Lens 4	0.897	ASP	0.606	Plastic	1.565	57.0	2.00	
9		3.302	ASP	0.800					
10	IR-cut filter	Pla	no	0.300	Glass	1.517	64.2	-	
11		Pla	Plano						
12	Image	Plano		-					
Note: Refere	ence wavelen	gth is 587	.6 nm (d-li	ine).					

	TABLE 10							
	Aspheric Coefficients							
Surface #	1	2	4	5				
k =	1.1992E+00	1.9195E+00	2.1734E+01	-7.2786E-01				
A4 =	5.8324E-02	1.2422E-01	-9.9032E-02	-1.2252E-01				
A6 =	-1.4402E-01	-5.2189E-01	5.9983E+00	5.2990E-01				
A8 =	1.0028E+00	4.2713E+00	-1.1966E+02	-3.0301E+00				
A10 =	-4.0021E+00	1.8016E+01	1.4083E+03	7.9248E+00				
A12 =	8.9035E+00	-4.2193E+02	-9.4428E+03	-1.0795E+01				
A14 =	-9.8479E+00	2.2697E+03	3.3923E+04	6.3429E+00				
A16 =	3.0263E+00	-4.1004E+03	-5.0610E+04	-8.0066E-01				
Surface #	6	7	8	9				
k =	-9.8774E-01	-3.1767E+00	-8.3817E-01	-2.4331E+01				
A4 =	2.5606E+00	-1.2881E-01	-4.2259E-01	3.5717E-01				
A6 =	-7.9740E+00	-6.6170E-01	4.3675E-01	-4.5759E-01				
A8 =	1.4853E+01	1.1888E+00	-4.6275E-01	2.9937E-01				

A10 =	-1.1480E+01	-4.2607E-01	3.1380E-01	-1.1921E-01
A12 =	-4.4740E+00	-5.1720E-01	-1.2912E-01	2.8364E-02
A14 =	1.2594E+01	5.0722E-01	2.9275E-02	-3.7104E-03
A16 =	-5.4160E+00	-1.2485E-01	-2.8533E-03	2.0238E-04

In the 5th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 5th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 9 and Table 10 as the following values and satisfy the following conditions:

5th Embodiment						
f [mm]	2.24	f2/f3	-0.93			
Fno	2.51	f/f4	1.12			
HFOV [deg.]	44.2	f/f3	-1.30			
V1	17.8	Td [mm]	3.150			
CT2/(CT1+CT3+CT4)	1.25	ΣCT/Td	0.85			
(R3+R4)/(R3-R4)	0.61	Td/tan(HFOV) [mm]	3.24			
f/f1	-0.16	FOV [deg.]	88.4			

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6th Embodiment

Fig. 6A is a schematic view of an imaging device according to the 6th embodiment of the present disclosure. Fig. 6B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the

15 imaging device according to the 6th embodiment.

In Fig. 6A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 670. The image capturing lens system includes, in order from an object side to an image side, a first lens element 610, an aperture stop 600, a second lens element 620, a third lens element 630, a fourth lens element 640, an IR-cut filter 650 and an image plane 660, wherein the image capturing lens system has a total of four lens elements (610-640) with refractive power.

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The first lens element 610 with positive refractive power has a convex object-side surface 611 in a paraxial region thereof and a convex image-side surface 612 in a paraxial region thereof, which are both aspheric, and the first lens element 610 is made of plastic material.

- The second lens element 620 with positive refractive power has a concave object-side surface 621 in a paraxial region thereof and a convex image-side surface 622 in a paraxial region thereof, which are both aspheric, and the second lens element 620 is made of plastic material.
- The third lens element 630 with negative refractive power has a concave object-side surface 631 in a paraxial region thereof and a convex image-side surface 632 in a paraxial region thereof, which are both aspheric, and the third lens element 630 is made of plastic material.

The fourth lens element 640 with positive refractive power has a convex object-side surface 641 in a paraxial region thereof and a concave image-side surface 642 in a paraxial region thereof, which are both aspheric, and the fourth lens element 640 is made of plastic material. Furthermore, the image-side surface 642 of the fourth lens element 640 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 650 is made of glass and located between the fourth lens element 640 and the image plane 660, and will not affect the focal length of the

image capturing lens system. The image sensor 670 is disposed on the image plane 660 of the image capturing lens system.

The detailed optical data of the 6th embodiment are shown in Table 11 and the aspheric surface data are shown in Table 12 below.

	TABLE 11								
	Embodiment 6								
	f = 1.27 mm, Fno = 2.10, HFOV = 44.4 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ino	Infinity					
1	Lens 1	2.393	ASP	0.280	Plastic	1.544	55.9	3.85	
2		-16.057	ASP	0.017					
3	Ape. Stop	Pla	Plano						
4	Lens 2	-30.373	ASP	0.755	Plastic	1.544	55.9	0.87	
5		-0.468	ASP	0.121					
6	Lens 3	-0.246	ASP	0.240	Plastic	1.639	23.5	-0.90	
7		-0.594	ASP	0.030					
8	Lens 4	0.639	ASP	0.522	Plastic	1.530	55.8	1.47	
9		2.521	ASP	0.400					
10	IR-cut filter	Pla	no	0.175	Glass	1.517	64.2	-	
11		Plano		0.073					
12	Image	Plano		-					
Note: Refere	ence wavelen	gth is 587	.6 nm (d-l	ine).					

	TABLE 12							
	Aspheric Coefficients							
Surface #	1	2	4	5				
k =	1.7241E+00	-8.9754E+01	-9.0000E+01	-7.5923E-01				
A4 =	2.1410E-01	1.4516E+00	1.5168E-01	-5.4982E-01				
A6 =	-2.3810E-01	-1.0826E+01	4.8929E+00	2.0791E+00				
A8 =	2.3555E+01	1.9495E+02	-3.2116E+01	8.2787E-01				
A10 =	-2.5034E+02	-5.1780E+02	-2.6801E+03	-1.4893E+02				
A12 =	1.4357E+03	-5.7593E+04	4.6579E+04	1.0534E+03				
A14 =	-4.2381E+03	9.2351E+05	-3.3256E+05	-3.0936E+03				
A16 =	4.9589E+03	-4.2045E+06	9.0327E+05	3.3098E+03				
Surface #	6	7	8	9				
k =	-9.9704E-01	-3.7851E+00	-7.3474E-01	-2.0751E+00				
A4 =	2.9255E+00	-1.3600E+00	-1.2133E+00	1.8260E+00				
A6 =	-2.4852E+00	5.5927E+00	3.0817E+00	-5.9653E+00				
A8 =	-5.7718E+01	-1.8755E+01	-1.0034E+01	9.6816E+00				

A10 =	6.7135E+02	7.3016E+01	1.9498E+01	-9.2466E+00
A12 =	-3.0733E+03	-1.6937E+02	-2.1549E+01	5.1894E+00
A14 =	6.6780E+03	1.9522E+02	1.2590E+01	-1.5760E+00
A16 =	-5.6393E+03	-8.6932E+01	-3.0510E+00	1.9769E-01

In the 6th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 6th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 11 and Table 12 as the following values and satisfy the following conditions:

6th Embodiment						
f [mm]	1.27	f2/f3	-0.97			
Fno	2.10	f/f4	0.86			
HFOV [deg.]	44.4	f/f3	-1.41			
V1	55.9	Td [mm]	2.009			
CT2/(CT1+CT3+CT4)	0.72	ΣCT/Td	0.89			
(R3+R4)/(R3-R4)	1.03	Td/tan(HFOV) [mm]	2.05			
f/f1	0.33	FOV [deg.]	88.8			

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7th Embodiment

Fig. 7A is a schematic view of an imaging device according to the 7th embodiment of the present disclosure. Fig. 7B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the

15 imaging device according to the 7th embodiment.

In Fig. 7A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 770. The image capturing lens system includes, in order from an object side to an image side, an aperture stop 700, a first lens element 710, a second lens element 720, a third lens element 730, a fourth lens element 740, an IR-cut filter 750 and an image plane 760, wherein the image capturing lens system has a total of four lens elements (710-740) with refractive power.

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The first lens element 710 with positive refractive power has a convex object-side surface 711 in a paraxial region thereof and a concave image-side surface 712 in a paraxial region thereof, which are both aspheric, and the first lens element 710 is made of plastic material.

- The second lens element 720 with positive refractive power has a concave object-side surface 721 in a paraxial region thereof and a convex image-side surface 722 in a paraxial region thereof, which are both aspheric, and the second lens element 720 is made of plastic material.
- The third lens element 730 with negative refractive power has a concave object-side surface 731 in a paraxial region thereof and a convex image-side surface 732 in a paraxial region thereof, which are both aspheric, and the third lens element 730 is made of plastic material.

The fourth lens element 740 with positive refractive power has a convex object-side surface 741 in a paraxial region thereof and a concave image-side surface 742 in a paraxial region thereof, which are both aspheric, and the fourth lens element 740 is made of plastic material. Furthermore, the image-side surface 742 of the fourth lens element 740 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 750 is made of glass and located between the fourth lens element 740 and the image plane 760, and will not affect the focal length of

the image capturing lens system. The image sensor 770 is disposed on the image plane 760 of the image capturing lens system.

The detailed optical data of the 7th embodiment are shown in Table 13 and the aspheric surface data are shown in Table 14 below.

	TABLE 13									
Embodiment 7										
	f = 1.57 mm, Fno = 2.05, HFOV = 48.5 deg.									
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length		
0	Object	Pla	ano	Infinity						
1	Ape. Stop	Pla	ano	-0.052						
2	Lens 1	1.142	ASP	0.279	Plastic	1.544	55.9	2.84		
3		4.008	ASP	0.159						
4	Lens 2	-4.075	ASP	0.614	Plastic	1.544	55.9	1.24		
5		-0.608	ASP	0.142						
6	Lens 3	-0.255	ASP	0.230	Plastic	1.634	23.8	-1.37		
7		-0.487	ASP	0.030						
8	Lens 4	0.636	ASP	0.414	Plastic	1.535	55.7	2.35		
9		0.998	ASP	0.500						
10	IR-cut filter	Pla	ino	0.175	Glass	1.517	64.2	-		
11		Pla	ano	0.141						
12	Image	Plano		-						
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).									

	TABLE 14							
	Aspheric Coefficients							
Surface #	2	3	4	5				
k =	-5.4318E-01	6.9324E+01	6.0179E+01	-4.8138E-01				
A4 =	1.1275E-01	-3.4138E-01	-6.6571E-01	-8.5384E-02				
A6 =	-1.4350E+00	-2.7321E+00	4.9846E-01	-6.6518E-01				
A8 =	6.0529E+00	2.0740E+01	-4.5807E+00	-2.1554E-01				
A10 =	4.7148E+01	-7.0776E+01	-1.7027E+02	-7.9977E+00				
A12 =	-1.4571E+02	-1.4998E+03	1.2130E+03	2.5638E+01				
A14 =	-3.8164E+03	1.2389E+04	-4.4615E+03	-4.3167E+01				
A16 =	1.5882E+04	-2.9058E+04	6.2425E+03	7.2938E+01				
Surface #	6	7	8	9				
k =	-1.1103E+00	-3.0258E+00	-9.3042E-01	-5.1455E+00				
A4 =	5.4423E+00	4.5345E-01	-7.7223E-01	7.0200E-01				
A6 =	-3.5666E+01	-4.9768E+00	9.4468E-01	-1.5850E+00				
A8 =	1.3446E+02	1.9752E+01	-1.3669E+00	1.7028E+00				

A10 =	-2.5131E+02	-4.2912E+01	1.1409E+00	-1.1082E+00
A12 =	-7.3665E+01	5.3544E+01	-5.2307E-01	4.3302E-01
A14 =	1.1117E+03	-3.5702E+01	1.2365E-01	-9.2838E-02
A16 =	-1.2600E+03	1.0063E+01	-1.1645E-02	8.3092E-03

In the 7th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 7th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 13 and Table 14 as the following values and satisfy the following conditions:

7th Embodiment						
f [mm]	1.57	f2/f3	-0.91			
Fno	2.05	f/f4	0.67			
HFOV [deg.]	48.5	f/f3	-1.15			
V1	55.9	Td [mm]	1.868			
CT2/(CT1+CT3+CT4)	0.67	ΣCT/Td	0.82			
(R3+R4)/(R3-R4)	1.35	Td/tan(HFOV) [mm]	1.65			
f/f1	0.55	FOV [deg.]	97.0			

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8th Embodiment

Fig. 8A is a schematic view of an imaging device according to the 8th embodiment of the present disclosure. Fig. 8B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the

15 imaging device according to the 8th embodiment.

In Fig. 8A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor

870. The image capturing lens system includes, in order from an object side to an image side, a first lens element 810, an aperture stop 800, a second lens element 820, a third lens element 830, a fourth lens element 840, an IR-cut filter 850 and an image plane 860, wherein the image capturing lens system has a total of four lens elements (810-840) with refractive power.

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The first lens element 810 with positive refractive power has a convex object-side surface 811 in a paraxial region thereof and a concave image-side surface 812 in a paraxial region thereof, which are both aspheric, and the first lens element 810 is made of plastic material.

- The second lens element 820 with positive refractive power has a concave object-side surface 821 in a paraxial region thereof and a convex image-side surface 822 in a paraxial region thereof, which are both aspheric, and the second lens element 820 is made of plastic material.
- The third lens element 830 with negative refractive power has a concave object-side surface 831 in a paraxial region thereof and a convex image-side surface 832 in a paraxial region thereof, which are both aspheric, and the third lens element 830 is made of plastic material.

The fourth lens element 840 with positive refractive power has a convex object-side surface 841 in a paraxial region thereof and a concave image-side surface 842 in a paraxial region thereof, which are both aspheric, and the fourth lens element 840 is made of plastic material. Furthermore, the image-side surface 842 of the fourth lens element 840 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 850 is made of glass and located between the fourth lens element 840 and the image plane 860, and will not affect the focal length of

the image capturing lens system. The image sensor 870 is disposed on the image plane 860 of the image capturing lens system.

The detailed optical data of the 8th embodiment are shown in Table 15 and the aspheric surface data are shown in Table 16 below.

TABLE 15									
	Embodiment 8								
	f = 1.68 mm, Fno = 2.10, HFOV = 46.0 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ino	Infinity					
1	Lens 1	1.787	ASP	0.278	Plastic	1.544	55.9	3.81	
2		12.133	ASP	0.022					
3	Ape. Stop	Pla	ino	0.145					
4	Lens 2	-3.839	ASP	0.668	Plastic	1.544	55.9	1.38	
5		-0.668	ASP	0.194					
6	Lens 3	-0.273	ASP	0.230	Plastic	1.639	23.5	-1.18	
7		-0.569	ASP	0.030					
8	Lens 4	0.784	ASP	0.496	Plastic	1.530	55.8	1.65	
9		5.992	ASP	0.400					
10	IR-cut filter	Pla	ino	0.175	Glass	1.517	64.2	-	
11		Pla	ino	0.472					
12	Image	Plano		-					
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								

	TABLE 16							
	Aspheric Coefficients							
Surface #	1	2	4	5				
k =	-1.3232E+00	5.3151E+01	5.1693E+01	-5.9308E-01				
A4 =	1.6281E-02	-1.2122E-02	-2.5602E-01	-1.1508E-01				
A6 =	1.5823E-01	-1.1940E+00	-1.0332E+00	-6.8787E-01				
A8 =	5.9941E-01	1.2093E+01	1.0464E+01	-9.7964E-02				
A10 =	-1.3812E+01	-2.0003E+01	-1.9940E+02	-6.2734E+00				
A12 =	4.5317E+01	-1.4998E+03	1.2130E+03	2.8529E+01				
A14 =	-4.4460E+01	1.2389E+04	-4.4615E+03	-4.4589E+01				
A16 =	-4.7734E+01	-2.9058E+04	6.2425E+03	2.7908E+01				
Surface #	6	7	8	9				
k =	-1.0578E+00	-3.0032E+00	-8.6121E-01	5.6610E+00				
A4 =	4.0391E+00	9.4553E-02	-6.6716E-01	7.7788E-01				
A6 =	-2.6571E+01	-4.4170E+00	1.1395E+00	-1.2944E+00				
A8 =	1.2417E+02	1.9085E+01	-1.7698E+00	1.0967E+00				

A10 =	-3.9394E+02	-4.1568E+01	1.6239E+00	-5.7605E-01
A12 =	8.2748E+02	5.5376E+01	-8.6944E-01	1.8609E-01
A14 =	-9.7331E+02	-4.1902E+01	2.5418E-01	-3.3617E-02
A16 =	4.7213E+02	1.3653E+01	-3.1838E-02	2.5144E-03

In the 8th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 8th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 15 and Table 16 as the following values and satisfy the following conditions:

8th Embodiment						
f [mm]	1.68	f2/f3	-1.17			
Fno	2.10	f/f4	1.02			
HFOV [deg.]	46.0	f/f3	-1.42			
V1	55.9	Td [mm]	2.063			
CT2/(CT1+CT3+CT4)	0.67	ΣCT/Td	0.81			
(R3+R4)/(R3-R4)	1.42	Td/tan(HFOV) [mm]	1.99			
f/f1	0.44	FOV [deg.]	92.0			

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9th Embodiment

Fig. 9A is a schematic view of an imaging device according to the 9th embodiment of the present disclosure. Fig. 9B shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 9th embodiment.

In Fig. 9A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 970. The image capturing lens system includes, in order from an object side to an image side, a first lens element 910, an aperture stop 900, a second lens element 920, a third lens element 930, a fourth lens element 940, an IR-cut filter 950 and an image plane 960, wherein the image capturing lens system has a total of four lens elements (910-940) with refractive power.

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The first lens element 910 with positive refractive power has a convex object-side surface 911 in a paraxial region thereof and a convex image-side surface 912 in a paraxial region thereof, which are both aspheric, and the first lens element 910 is made of plastic material.

The second lens element 920 with positive refractive power has a convex object-side surface 921 in a paraxial region thereof and a convex image-side surface 922 in a paraxial region thereof, which are both aspheric, and the second lens element 920 is made of plastic material.

The third lens element 930 with negative refractive power has a concave object-side surface 931 in a paraxial region thereof and a convex image-side surface 932 in a paraxial region thereof, which are both aspheric, and the third lens element 930 is made of plastic material.

The fourth lens element 940 with positive refractive power has a convex object-side surface 941 in a paraxial region thereof and a concave image-side surface 942 in a paraxial region thereof, which are both aspheric, and the fourth lens element 940 is made of plastic material. Furthermore, the image-side surface 942 of the fourth lens element 940 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 950 is made of glass and located between the fourth lens element 940 and the image plane 960, and will not affect the focal length of

the image capturing lens system. The image sensor 970 is disposed on the image plane 960 of the image capturing lens system.

The detailed optical data of the 9th embodiment are shown in Table 17 and the aspheric surface data are shown in Table 18 below.

TABLE 17									
	Embodiment 9								
	f = 0.92 mm, Fno = 2.45, HFOV = 43.9 deg.								
Surface #		Curvature	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ino	Infinity					
1	Lens 1	100.000	ASP	0.205	Plastic	1.633	23.4	13.12	
2		-9.046	ASP	0.017					
3	Ape. Stop	Pla	ino	0.024					
4	Lens 2	1.695	ASP	0.475	Plastic	1.544	55.9	0.54	
5		-0.319	ASP	0.100					
6	Lens 3	-0.148	ASP	0.160	Plastic	1.634	23.8	-0.65	
7		-0.329	ASP	0.030					
8	Lens 4	0.595	ASP	0.239	Plastic	1.530	55.8	1.28	
9		4.109	ASP	0.300					
10	IR-cut filter	Pla	ino	0.145	Glass	1.517	64.2	-	
11		Pla	Plano						
12	Image	Pla	Plano						
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								

	TABLE 18							
	Aspheric Coefficients							
Surface #	1	2	4	5				
k =	-9.0000E+01	9.0000E+01	3.3243E+01	-6.6437E-01				
A4 =	2.5656E-01	2.4894E+00	-1.9077E+00	-1.5093E+00				
A6 =	-1.0613E+00	-9.5530E+01	-1.3506E+01	4.3096E+00				
A8 =	1.6769E+02	3.0126E+03	1.0928E+01	1.6065E+02				
A10 =	-3.7307E+03	-2.3016E+04	-4.4021E+04	-2.9203E+03				
A12 =	3.9786E+04	-1.5960E+06	1.2908E+06	2.9181E+04				
A14 =	-2.1485E+05	4.6819E+07	-1.6860E+07	-1.5683E+05				
A16 =	4.5990E+05	-3.8994E+08	8.3772E+07	3.0696E+05				
Surface #	6	7	8	9				
k =	-1.0921E+00	-2.4247E+00	-6.0015E-01	3.3921E+01				
A4 =	8.8579E+00	-1.7457E+00	-1.8642E+00	3.4965E+00				
A6 =	-9.7201E+00	2.7059E+01	4.2816E+00	-1.7965E+01				
A8 =	-4.6210E+02	-1.6609E+02	-3.6842E+01	3.3243E+01				

A10 =	1.0079E+04	1.0699E+03	9.4802E+01	-3.1178E+01
A12 =	-8.5169E+04	-4.7330E+03	-1.9140E+02	1.8452E+01
A14 =	3.3855E+05	1.0605E+04	3.6755E+02	-3.7397E+01
A16 =	-5.2300E+05	-7.7191E+03	-9.3365E+02	3.7762E+01

In the 9th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 9th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 17 and Table 18 as the following values and satisfy the following conditions:

9th Embodiment						
f [mm]	0.92	f2/f3	-0.83			
Fno	2.45	f/f4	0.72			
HFOV [deg.]	43.9	f/f3	-1.42			
V1	23.4	Td [mm]	1.250			
CT2/(CT1+CT3+CT4)	0.79	ΣCT/Td	0.86			
(R3+R4)/(R3-R4)	0.68	Td/tan(HFOV) [mm]	1.30			
f/f1	0.07	FOV [deg.]	87.8			

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10th Embodiment

Fig. 10A is a schematic view of an imaging device according to the 10th embodiment of the present disclosure. Fig. 10B shows, in order from left to 15 right, spherical aberration curves, astigmatic field curves and a distortion curve of the imaging device according to the 10th embodiment.

In Fig. 10A, the imaging device includes the image capturing lens system (not otherwise herein labeled) of the present disclosure and an image sensor 1070. The image capturing lens system includes, in order from an object side to an image side, an aperture stop 1000, a first lens element 1010, a second lens element 1020, a third lens element 1030, a fourth lens element 1040, an IR-cut filter 1050 and an image plane 1060, wherein the image capturing lens system has a total of four lens elements (1010-1040) with refractive power.

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The first lens element 1010 with positive refractive power has a convex object-side surface 1011 in a paraxial region thereof and a concave image-side surface 1012 in a paraxial region thereof, which are both aspheric, and the first lens element 1010 is made of plastic material.

The second lens element 1020 with positive refractive power has a concave object-side surface 1021 in a paraxial region thereof and a convex image-side surface 1022 in a paraxial region thereof, which are both aspheric, and the second lens element 1020 is made of plastic material.

The third lens element 1030 with negative refractive power has a concave object-side surface 1031 in a paraxial region thereof and a convex image-side surface 1032 in a paraxial region thereof, which are both aspheric, and the third lens element 1030 is made of plastic material.

The fourth lens element 1040 with positive refractive power has a convex object-side surface 1041 in a paraxial region thereof and a concave image-side surface 1042 in a paraxial region thereof, which are both aspheric, and the fourth lens element 1040 is made of plastic material. Furthermore, the image-side surface 1042 of the fourth lens element 1040 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 1050 is made of glass and located between the fourth lens element 1040 and the image plane 1060, and will not affect the focal length

of the image capturing lens system. The image sensor 1070 is disposed on the image plane 1060 of the image capturing lens system.

The detailed optical data of the 10th embodiment are shown in Table 19 and the aspheric surface data are shown in Table 20 below.

TABLE 19									
	Embodiment 10								
	f = 1.80 mm, Fno = 2.12, HFOV = 47.2 deg.								
Surface #		Curvatur	e Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Pla	ano	Infinity					
1	Ape. Stop	Pla	ano	-0.060					
2	Lens 1	1.246	ASP	0.289	Plastic	1.544	55.9	2.97	
3		5.018	ASP	0.191					
4	Lens 2	-3.749	ASP	0.593	Plastic	1.544	55.9	1.57	
5		-0.733	ASP	0.156					
6	Lens 3	-0.288	ASP	0.248	Plastic	1.634	23.8	-1.33	
7		-0.584	ASP	0.030					
8	Lens 4	0.704	ASP	0.601	Plastic	1.535	55.7	2.05	
9		1.382	ASP	0.500					
10	IR-cut filter	Pla	ino	0.210	Glass	1.517	64.2	-	
11		Pla	ano	0.198					
12	Image	Pla	ino	-					
Note: Refere	Note: Reference wavelength is 587.6 nm (d-line).								
The effective	The effective radius of Surface 9 is 1.676 mm.								

	TABLE 20							
	Aspheric Coefficients							
Surface #	2	3	4	5				
k =	-5.0585E-01	9.0000E+01	3.6143E+01	-3.9805E-01				
A4 =	8.6099E-02	-2.2970E-01	-4.8540E-01	-1.5034E-01				
A6 =	-9.1382E-01	-1.8900E+00	2.7508E-01	-5.1276E-01				
A8 =	1.9706E+00	1.1233E+01	-2.0152E+00	-1.5742E-01				
A10 =	1.9492E+01	-3.0654E+01	-6.3534E+01	-3.0117E+00				
A12 =	-3.5519E+01	-4.4967E+02	3.6120E+02	7.3424E+00				
A14 =	-8.0910E+02	2.9681E+03	-1.0702E+03	-1.0241E+01				
A16 =	2.4600E+03	-5.5960E+03	1.2022E+03	1.7746E+01				
Surface #	6	7	8	9				
k =	-1.1070E+00	-2.9894E+00	-9.3316E-01	-5.2865E+00				
A3 =			-1.4739E-01	5.0831E-01				
A4 =	4.3809E+00	4.3352E-01	-3.5412E+00	2.6512E+00				

		2.4672E-02	
		2.4012E-02	1.3099E-01
6437E+01	-3.7903E+00	1.0303E+01	-3.1255E+01
		3.7082E-02	2.0652E-01
1296E+01	1.0965E+01	-3.1616E+01	1.1148E+02
		-2.2687E-03	-9.0797E-01
5853E+02	-1.4675E+01	6.3626E+01	-2.2327E+02
		-2.3794E-03	3.6058E-01
3141E+00	7.7310E+00	-7.5604E+01	2.6201E+02
		8.0966E-03	1.7201E-01
3963E+02	1.2159E+00	4.7652E+01	-1.7041E+02
		-5.5857E-02	1.0396E-01
9976E+02	-1.8447E+00	-1.2153E+01	4.7523E+01
	1296E+01 5853E+02 3141E+00 3963E+02	1296E+01 1.0965E+01 5853E+02 -1.4675E+01 3141E+00 7.7310E+00 3963E+02 1.2159E+00	3.7082E-02 1296E+01 1.0965E+01 -3.1616E+01 -2.2687E-03 5853E+02 -1.4675E+01 6.3626E+01 -2.3794E-03 3141E+00 7.7310E+00 -7.5604E+01 8.0966E-03 3963E+02 1.2159E+00 4.7652E+01 -5.5857E-02

In the 10th embodiment, the equation of the aspheric surface profiles of the aforementioned lens elements is the same as the equation of the 1st embodiment. Also, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 10th embodiment, so an explanation in this regard will not be provided again.

Moreover, these parameters can be calculated from Table 19 and Table 20 as the following values and satisfy the following conditions:

10th Embodiment					
f [mm]	1.80	f2/f3	-1.18		
Fno	2.12	f/f4	0.88		
HFOV [deg.]	47.2	f/f3	-1.35		
V1	55.9	Td [mm]	2.108		
CT2/(CT1+CT3+CT4)	0.52	ΣCT/Td	0.82		
(R3+R4)/(R3-R4)	1.49	Td/tan(HFOV) [mm]	1.95		
f/f1	0.61	FOV [deg.]	94.4		

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The foregoing description, for purpose of explanation, has been described with reference to specific embodiments. It is to be noted that

TABLES 1-20 show different data of the different embodiments; however, the data of the different embodiments are obtained from experiments. The embodiments were chosen and described in order to best explain the principles of the disclosure and its practical applications, to thereby enable others skilled

- ⁵ in the art to best utilize the disclosure and various embodiments with various modifications as are suited to the particular use contemplated. The embodiments depicted above and the appended drawings are exemplary and are not intended to be exhaustive or to limit the scope of the present disclosure to the precise forms disclosed. Many modifications and variations are possible
- 10 in view of the above teachings.

CLAIMS

WHAT IS CLAIMED IS:

1. An image capturing lens system comprising, in order from an object side to an image side:

a first lens element having refractive power;

a second lens element with positive refractive power having a convex image-side surface in a paraxial region thereof;

a third lens element with negative refractive power having a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof; and

a fourth lens element with refractive power having a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof;

wherein the image capturing lens system has a total of four lens elements with refractive power, an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, a focal length of the second lens element is f2, a focal length of the third lens element is f3, and the following conditions are satisfied:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td/tan(HFOV) < 3.75 mm;

|f/f4| < 1.20; and f2/f3 < -0.65.

2. The image capturing lens system of claim 1, wherein the fourth lens element has the object-side surface being convex in a paraxial region thereof.

3. The image capturing lens system of claim 2, wherein the focal length of the image capturing lens system is f, a focal length of the first lens element is f1, and the following condition is satisfied:

-0.25 < f/f1 < 0.75.

4. The image capturing lens system of claim 2, wherein the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied:

0.8 mm < Td < 2.5 mm.

5. The image capturing lens system of claim 2, wherein an f-number of the image capturing lens system is Fno, and the following condition is satisfied:

1.40 < Fno ≤ 2.25.

6. The image capturing lens system of claim 2, wherein a curvature radius of the object-side surface of the second lens element is R3, a curvature radius of the image-side surface of the second lens element is R4, and the following condition is satisfied:

0.5 < (R3+R4)/(R3-R4) < 2.5.

7. The image capturing lens system of claim 2, wherein the focal length of the image capturing lens system is f, and the following condition is satisfied: 0.5 mm < f < 2.0 mm.

8. The image capturing lens system of claim 1, wherein the first lens element has a convex object-side surface in a paraxial region thereof.

9. The image capturing lens system of claim 8, wherein the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of the maximal field of view of the image capturing lens system is HFOV, and the following condition is satisfied:

1.2 mm < Td/tan(HFOV) < 2.75 mm.

10. The image capturing lens system of claim 8, wherein a sum of the central thicknesses of the first lens element, the second lens element, the third lens element, and the fourth lens element is Σ CT, the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied:

0.80 < ΣCT/Td < 0.95.

11. The image capturing lens system of claim 8, wherein an Abbe number of the first lens element is V1, and the following condition is satisfied:

45 < V1.

12. The image capturing lens system of claim 8, wherein a central thickness of the second lens element is CT2, a central thickness of the first lens element is CT1, a central thickness of the third lens element is CT3, a central thickness of the fourth lens element is CT4, and the following condition is satisfied:

0.65 < CT2/(CT1+CT3+CT4) < 2.0.

13. An imaging device, comprising:the image capturing lens system of claim 1; and an image sensor.

14. A mobile terminal, comprising:the imaging device of claim 13.

15. An image capturing lens system comprising, in order from an object side to an image side:

a first lens element having refractive power;

a second lens element with positive refractive power having a convex image-side surface in a paraxial region thereof;

a third lens element with negative refractive power having a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof; and a fourth lens element with refractive power having a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof;

wherein the image capturing lens system has a total of four lens elements with refractive power, an axial distance between an object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, a focal length of the third lens element is f3, and the following conditions are satisfied:

0.5 mm < Td < 3.2 mm; 1.0 mm < Td/tan(HFOV) < 3.75 mm; |f/f4| < 1.20; and -2.0 < f/f3 < -0.95.

16. The image capturing lens system of claim 15, wherein an Abbe number of the first lens element is V1, and the following condition is satisfied:

45 < V1.

17. The image capturing lens system of claim 15, wherein the focal length of the image capturing lens system is f, a focal length of the first lens element is f1, and the following condition is satisfied:

-0.25 < f/f1 < 0.75.

18. The image capturing lens system of claim 15, wherein a maximal field of view of the image capturing lens system is FOV, and the following condition is satisfied:

80 degrees < FOV < 110 degrees.

19. The image capturing lens system of claim 15, wherein the axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, and the following condition is satisfied:

0.8 mm < Td < 2.5 mm.

20. The image capturing lens system of claim 15, wherein a focal length of the second lens element is f2, the focal length of the third lens element is f3, and the following condition is satisfied:

f2/f3 < -0.75.

21. An image capturing lens system comprising, in order from an object side to an image side:

a first lens element having refractive power;

a second lens element with positive refractive power having a convex image-side surface in a paraxial region thereof;

a third lens element with negative refractive power having a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof; and a fourth lens element with refractive power having a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface of the fourth lens element are aspheric, and the image-side surface of the fourth lens element has at least one convex shape in an off-axis region thereof;

wherein the image capturing lens system has a total of four lens elements with refractive power, an axial distance between the object-side surface of the first lens element and the image-side surface of the fourth lens element is Td, half of a maximal field of view of the image capturing lens system is HFOV, a focal length of the image capturing lens system is f, a focal length of the fourth lens element is f4, an f-number of the image capturing lens system is Fno, and the following conditions are satisfied:

0.5 mm < Td < 3.2 mm; 1.0 mm < Td/tan(HFOV) < 3.75 mm; |f/f4| < 1.20; and 1.40 < Fno ≤ 2.25.

22. The image capturing lens system of claim 21, wherein a focal length of the second lens element is f2, a focal length of the third lens element is f3, and the following condition is satisfied:

f2/f3 < -0.65.

23. The image capturing lens system of claim 21, wherein an Abbe number of the first lens element is V1, and the following condition is satisfied:

45 < V1.

24. The image capturing lens system of claim 21, wherein the first lens element has positive refractive power, the focal length of the image capturing lens system is f, a focal length of the first lens element is f1, and the following condition is satisfied:

0.25 < f/f1 < 0.75.

25. The image capturing lens system of claim 21, wherein a maximal field of view of the image capturing lens system is FOV, and the following condition is satisfied:

80 degrees < FOV < 110 degrees.

26. The image capturing lens system of claim 21, wherein a central thickness of the second lens element is CT2, a central thickness of the first lens element is CT1, a central thickness of the third lens element is CT3, a central thickness of the fourth lens element is CT4, and the following condition is satisfied:

0.65 < CT2/(CT1+CT3+CT4) < 2.0.

ABSTRACT OF THE DISCLOSURE

An image capturing lens system includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element and a fourth lens element. The first lens element has refractive power. The second lens element with positive refractive power has a convex image-side surface in a paraxial region thereof. The third lens element with negative refractive power has a concave object-side surface in a paraxial region thereof and a convex image-side surface in a paraxial region thereof. The fourth lens element with refractive power has a concave image-side surface in a paraxial region thereof, wherein both of an object-side surface and the image-side surface thereof are aspheric, and the image-side surface thereof has at least one convex shape in an off-axis region thereof. The image capturing lens system has a total of four lens elements with refractive power.

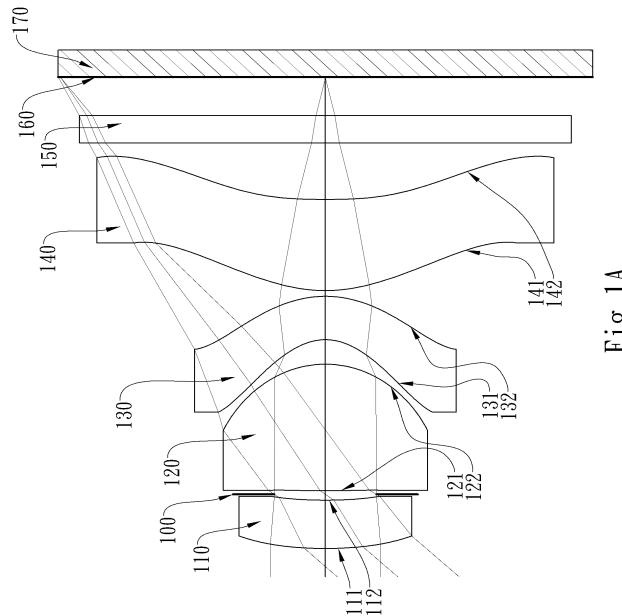
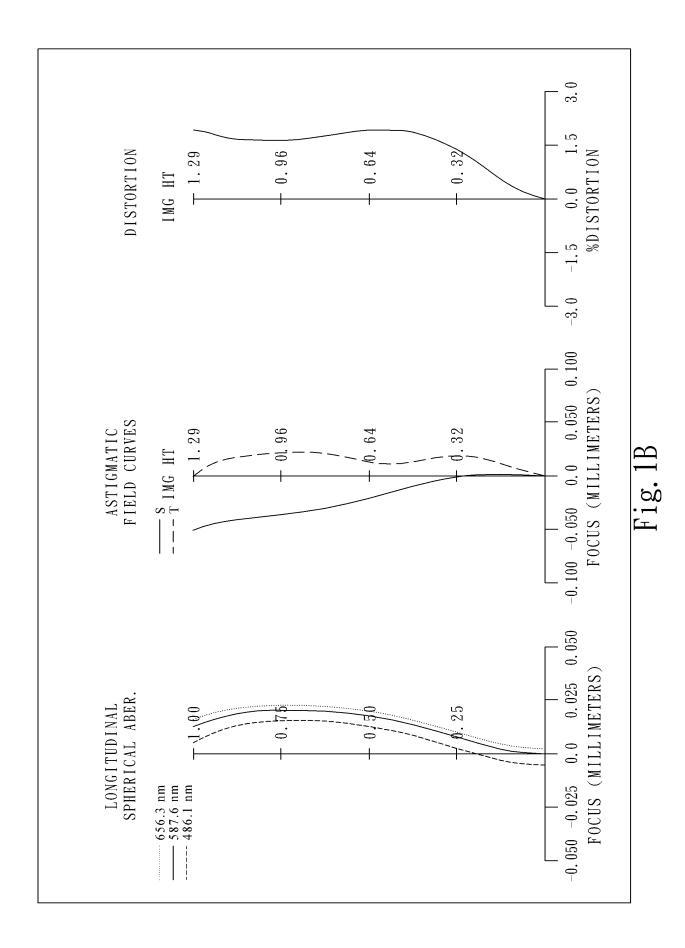


Fig. 1A



AOET, Ex. 1002 Page 66

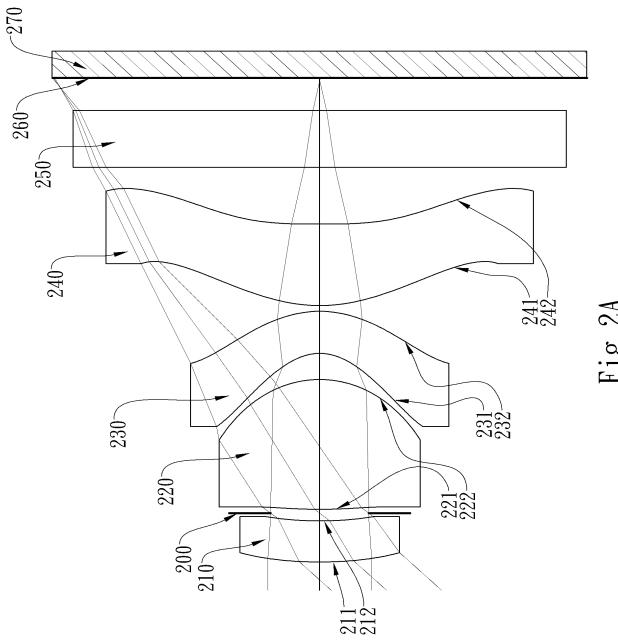
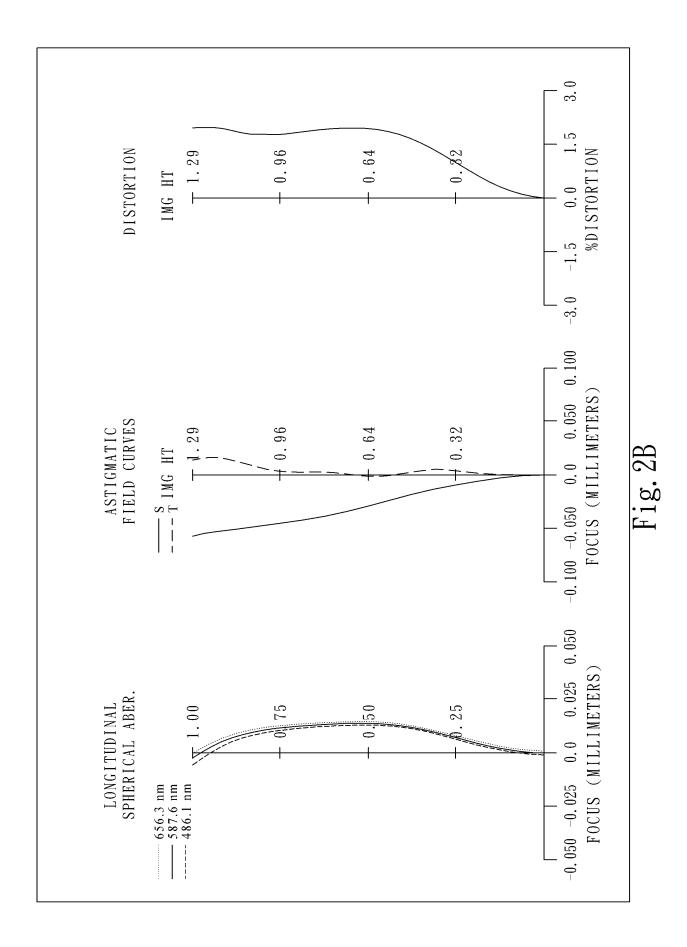
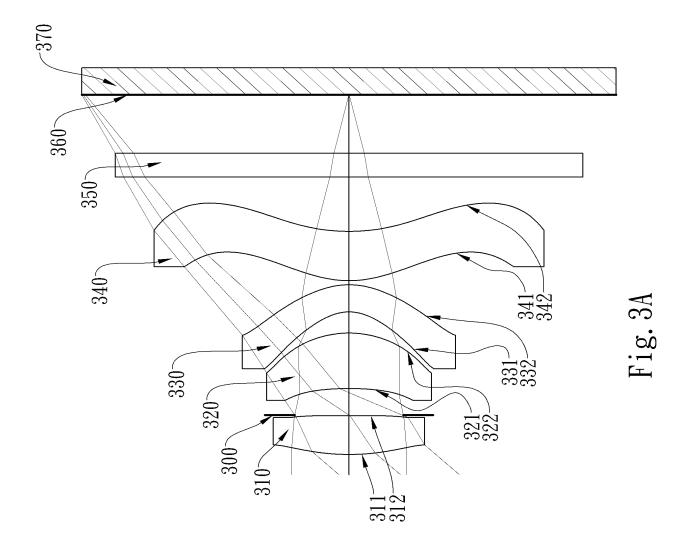
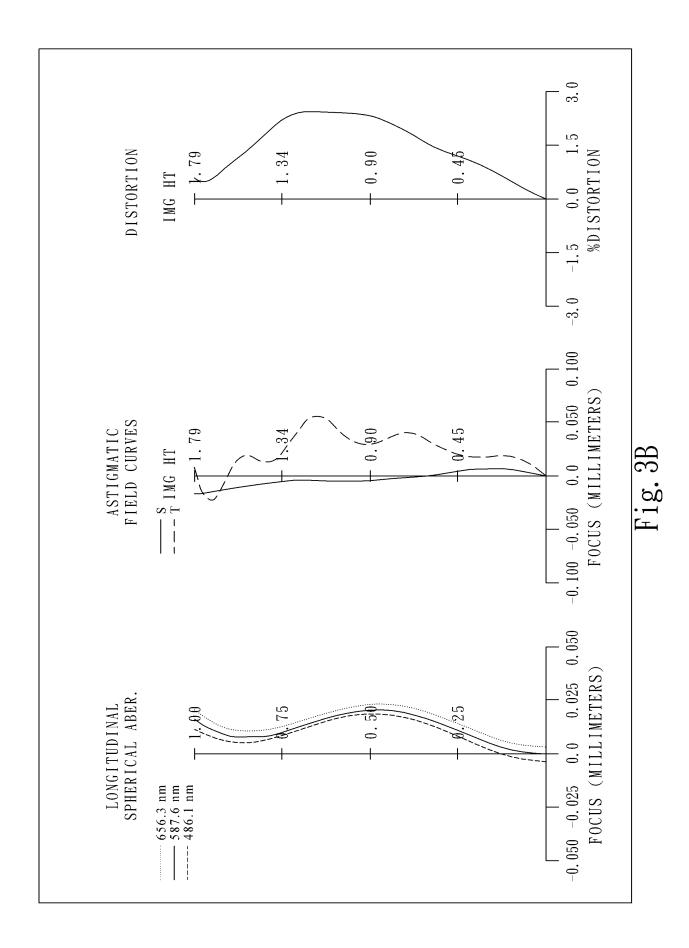


Fig.2A

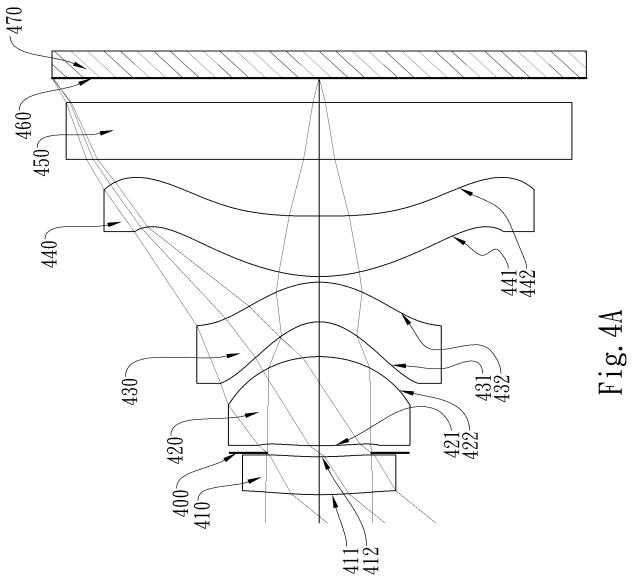


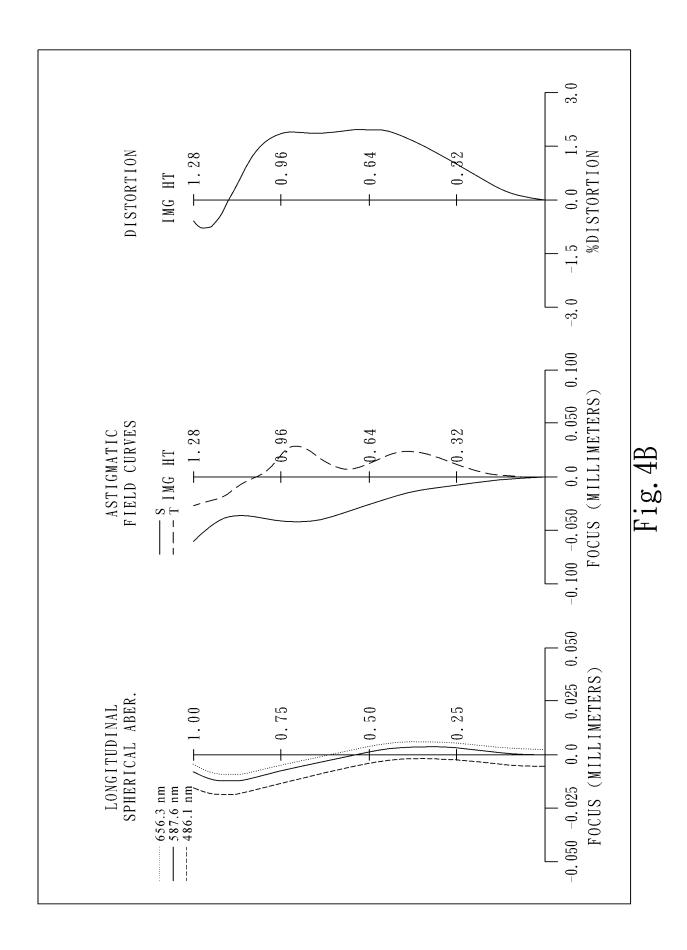
AOET, Ex. 1002 Page 68



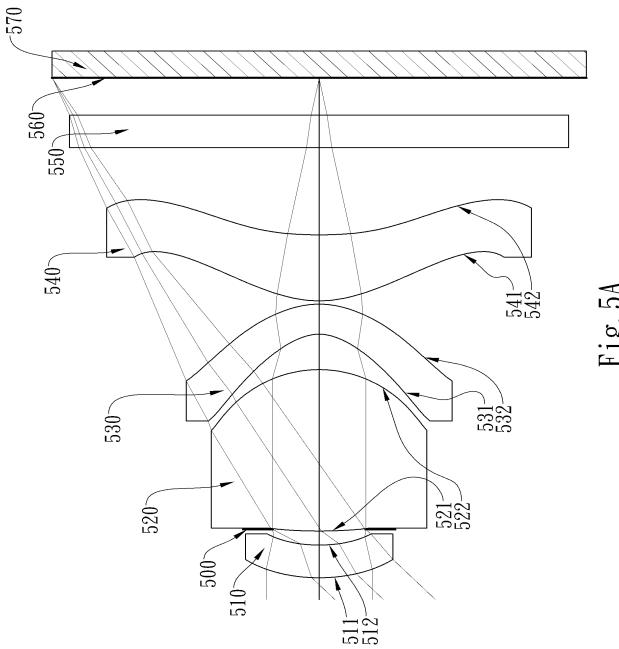


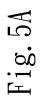
AOET, Ex. 1002 Page 70

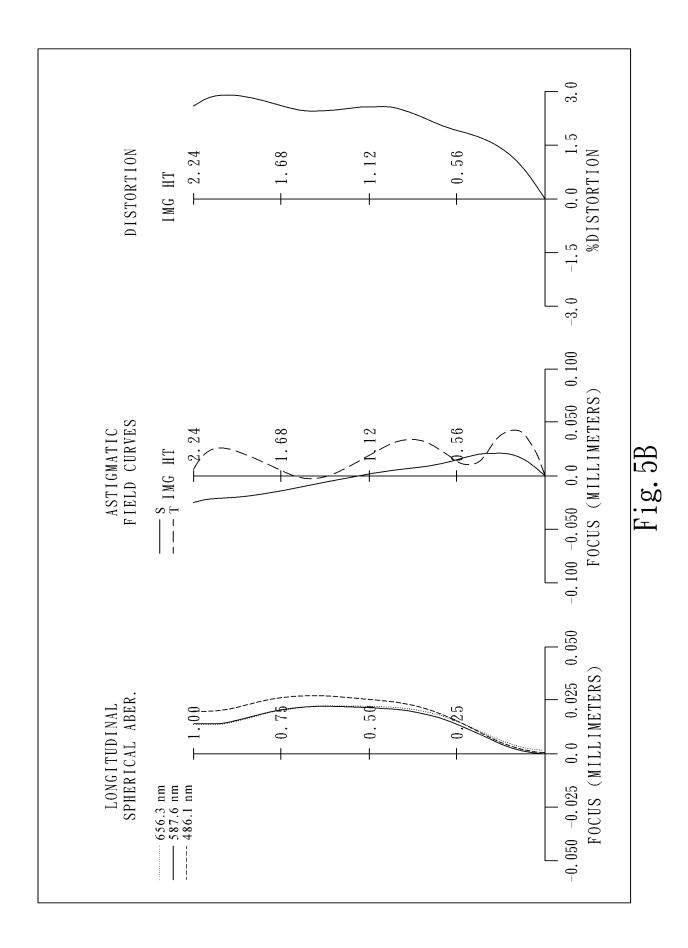


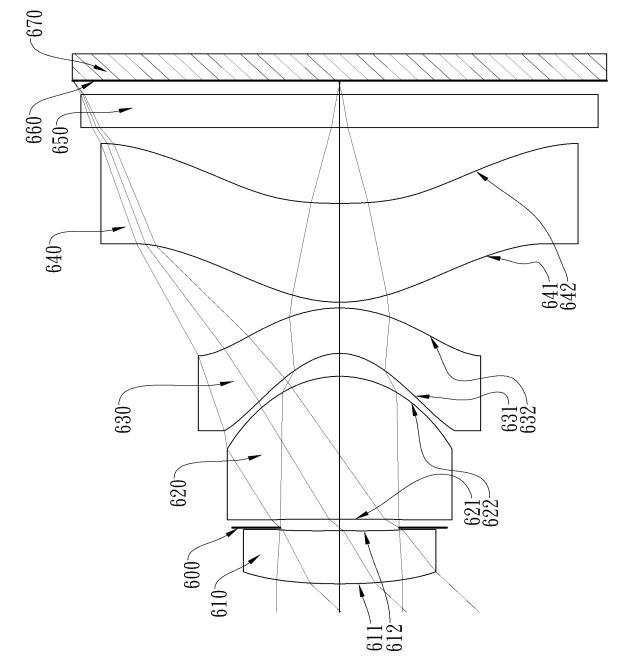


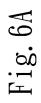
AOET, Ex. 1002 Page 72

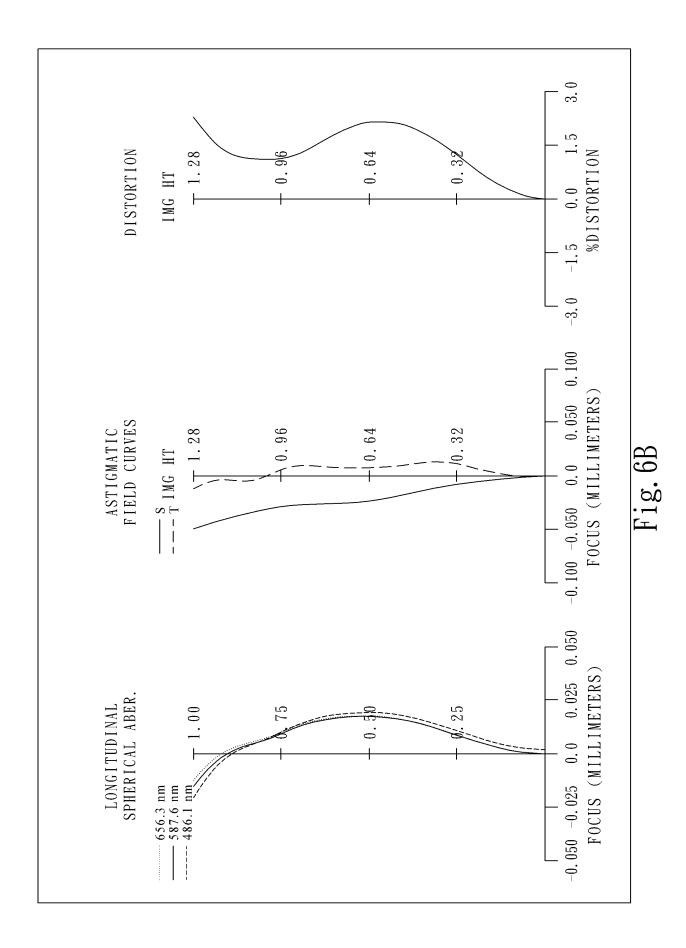


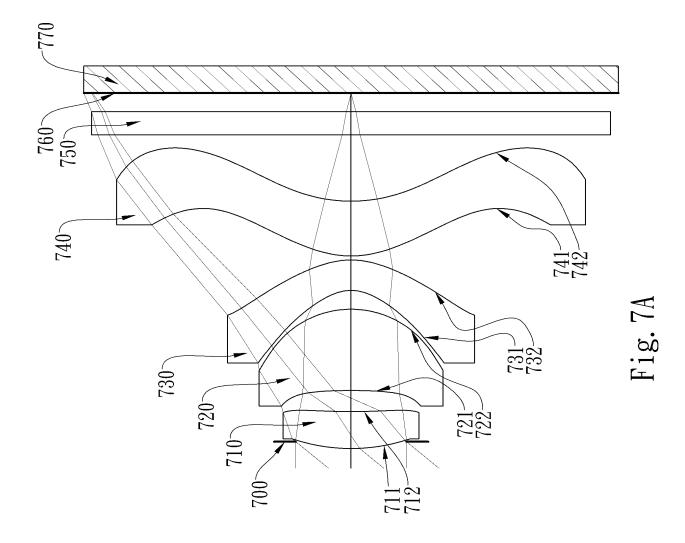


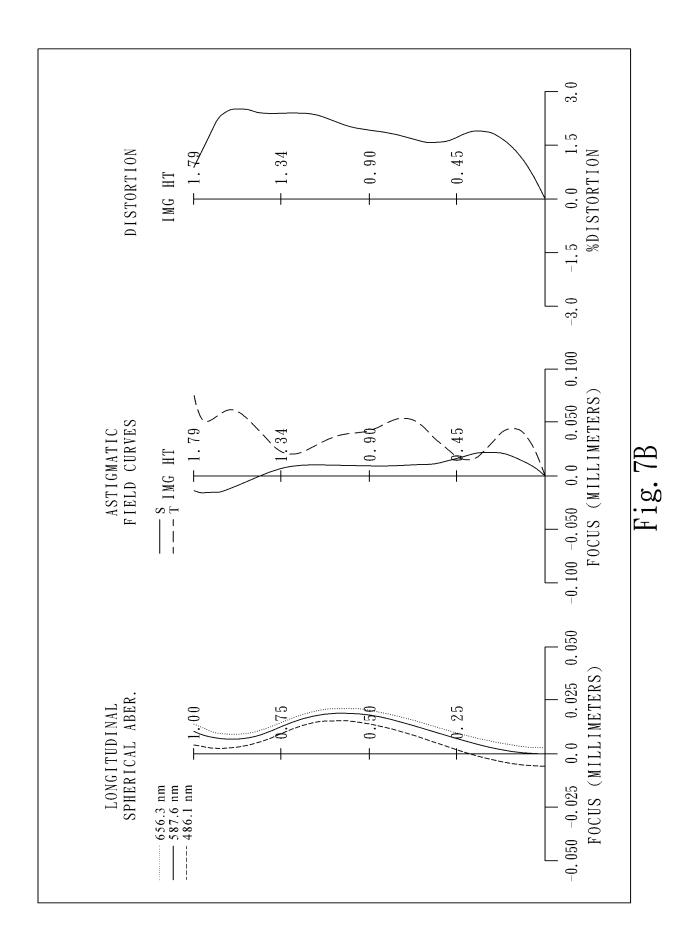


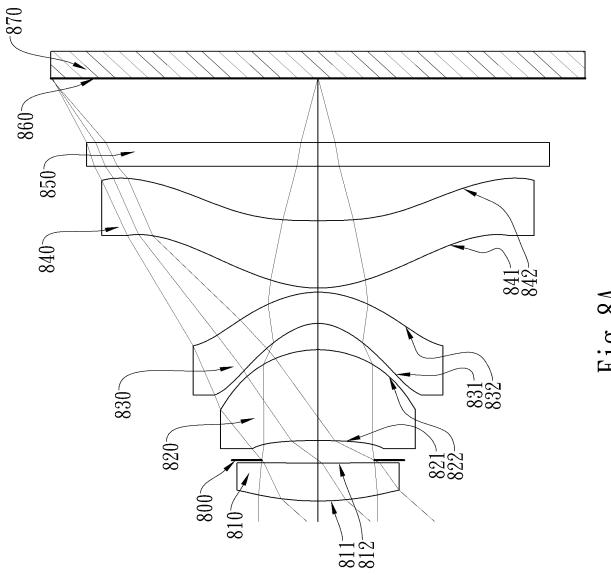


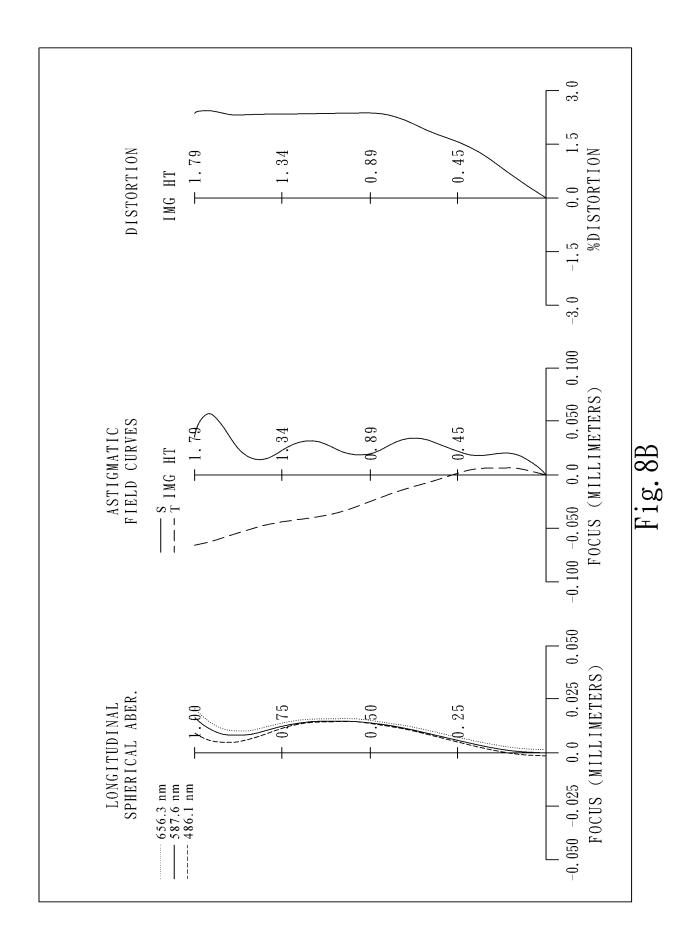












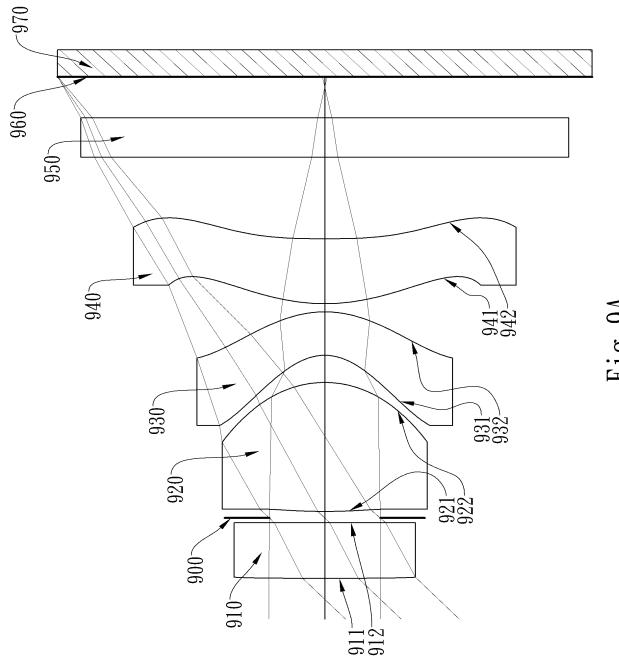
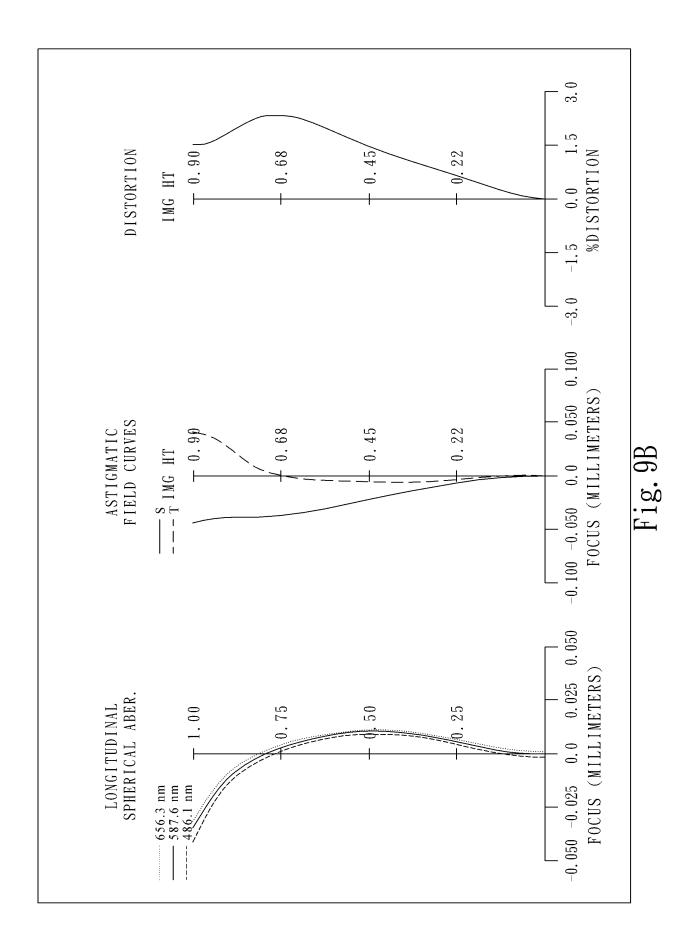
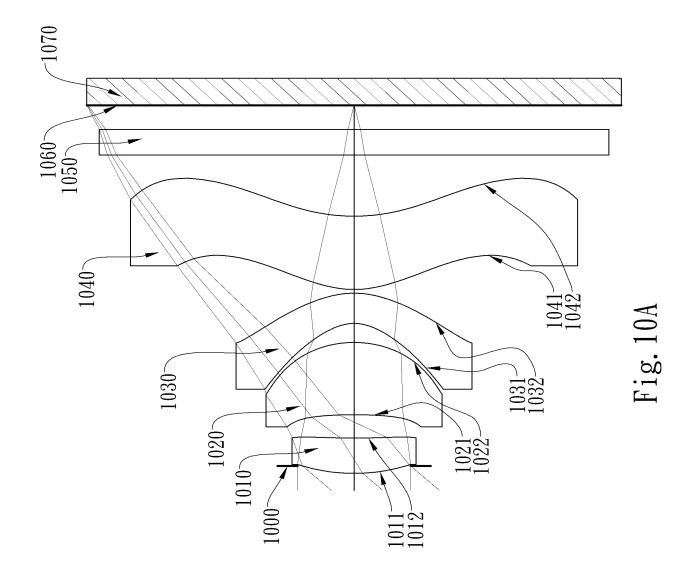
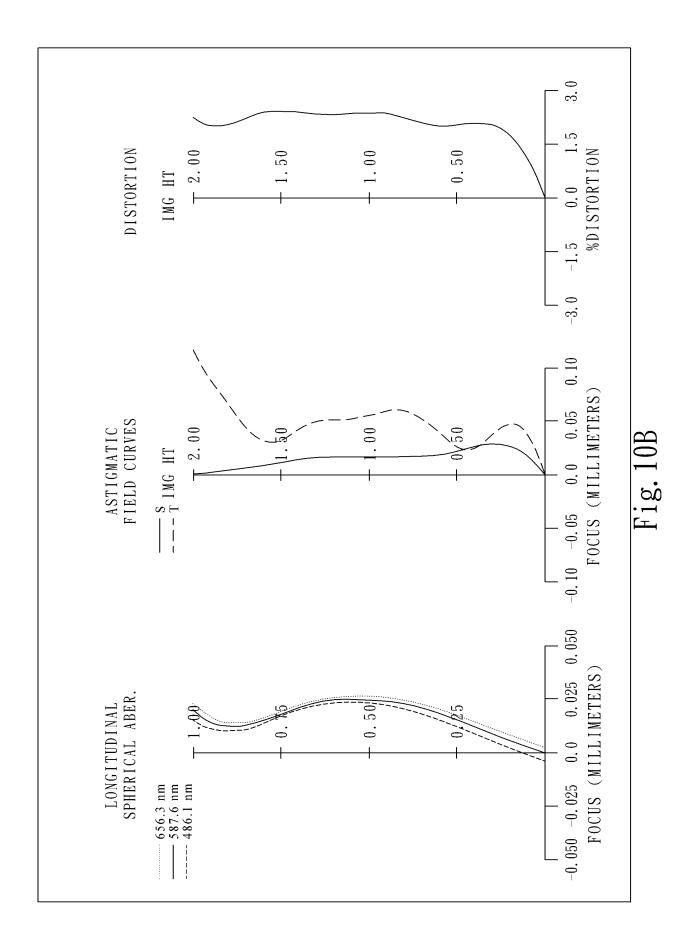


Fig.9A







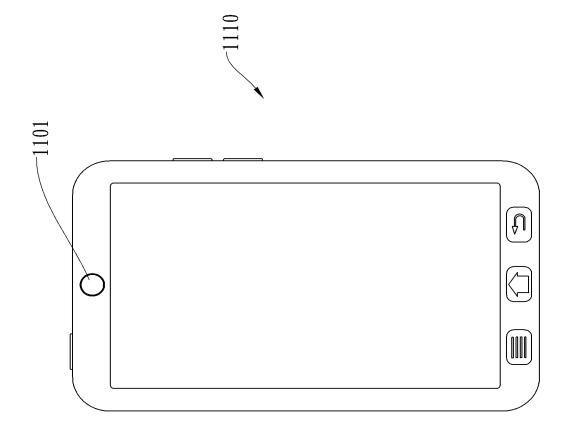
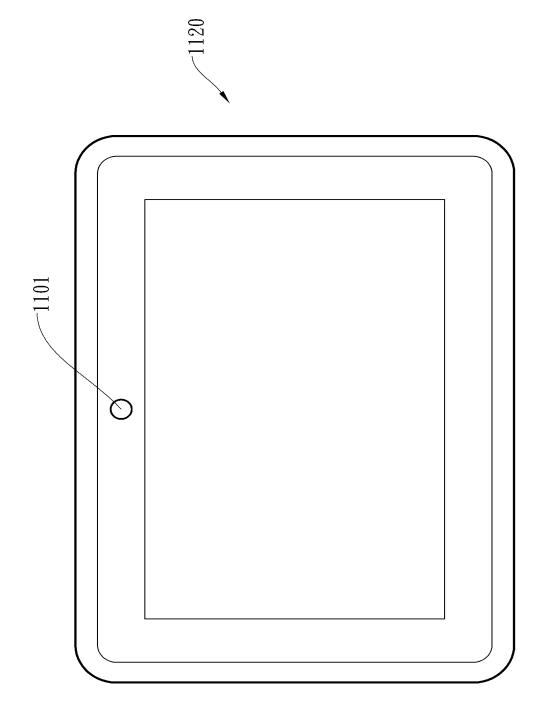
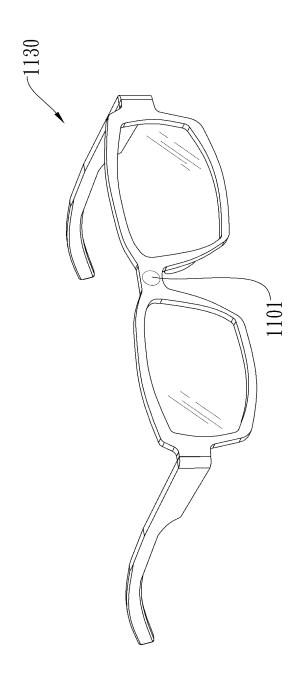


Fig. 11A





TRANSMITTAL FOR POWER OF ATTORNEY TO ONE OR MORE REGISTERED PRACTITIONERS

<u>NOTE</u>: This form is to be submitted with the Power of Attorney by Applicant form (PTO/AIA/82B or equivalent) to identify the application to which the Power of Attorney is directed, in accordance with 37 CFR 1.5. If the Power of Attorney by Applicant form is not accompanied by this transmittal form or an equivalent, the Power of Attorney will not be recognized in the application.

Application Number					
Filing Date		December 13, 2013			
First Named Inv	entor	WEI-YU CHEN			
Title		IMAGE CAPTURING LENS SYSTEM, IM	IAGING DEV	ICE AND MOBILE TERMINAL	
Art Unit					
Examiner Name)				
Attorney Docket	Number	14970-94702			
	SIGNA	URE of Applicant or Patent Practitioner			
Signature	/Tim Tingk	ang Xia/	Date	December 13, 2013	
Name	Tim Ting	kang Xia	Telephone	4044953678	
Registration Number	45242				
NOTE: This form must be signed in accordance with 37 CFR 1.33. See 37 CFR 1.4(d) for signature requirements and certifications.					
■ *Total of <u>1</u>	*Total of forms are submitted.				

This collection of information is required by 37 CFR 1.31, 1.32 and 1.33. The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.11 and 1.14. This collection is estimated to take 3 minutes to complete, including gathering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

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I hereby app transact all in the attact OR	point Practitioner(s) associ business in the United Star hed transmittal letter (form	ated with the following C res Patent and Tradems PTO/AiA/82A or equiva below as mi/out attorn	tustomar Number Int Office connect lent): 247	r as my/ou led therowi 28 , and lo tra	attorney(s) c ih for the app nsact all busi	r agent(s), and to lication raterence
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PTO/AIA/01 (06-12) Approved for use through 01/31/2014. OMB 0651-0032 U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE

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DECLARATION (37 CFR 1.63) FOR UTILITY OR DESIGN APPLICATION USING AN APPLICATION DATA SHEET (37 CFR 1.76)

Title of	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL					
Invention						
As the belo	w named inventor, I hereby declare that:					
This declar is directed						
	United States application or PCT international application number					
	filed on					
The above-	identified application was made or authorized to be made by me.					
I believe that	at I am the original inventor or an original joint inventor of a claimed invention in the application.					
	mowledge that any willful false statement made in this declaration is punishable under 18 U.S.C. 1001 aprisonment of not more than five (5) years, or both.					
	WARNING:					
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LEGAL N	AME OF INVENTOR					
Inventor: Signature	Chen, Wei-Yu Date (Optional): 21 St Nov 2013					
	lication data sheet (PTO/AIA/14 or equivalent), including naming the entire inventive entity, must accompany this form. onal PTO/SB/AIA01 form for each additional inventor.					
by the USPTO I complete, includ comments on the Patent and Trace	of information is required by 35 U.S.C. 115 and 37 CFR 1.63. The information is required to obtain or retain a benefit by the public which is to file (and o process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.11 and 1.14. This collection is estimated to take 1 minute to ting gathering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any se amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. semark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO S. SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.					

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Electronic Patent Application Fee Transmittal						
Application Number:						
Filing Date:						
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERM			D MOBILE TERMINAL		
First Named Inventor/Applicant Name:	WE	EI-YU CHEN				
Filer:	Tin	n Tingkang Xia/Deb	by Yew			
Attorney Docket Number:	149	970-94702				
Filed as Large Entity						
Utility under 35 USC 111(a) Filing Fees						
Description		Fee Code	Quantity	Amount	Sub-Total in USD(\$)	
Basic Filing:						
Utility application filing		1011	1	280	280	
Utility Search Fee		1111	1	600	600	
Utility Examination Fee		1311	1	720	720	
Pages:						
Claims:						
Claims in Excess of 20		1202	6	80	480	
Miscellaneous-Filing:						
Petition:						
				AOET	Ex 1002	

Description	Fee Code	Quantity	Amount	Sub-Total in USD(\$)
Patent-Appeals-and-Interference:				
Post-Allowance-and-Post-Issuance:				
Extension-of-Time:				
Miscellaneous:				
	Tot	al in USD	(\$)	2080

Electronic A	Electronic Acknowledgement Receipt					
EFS ID:	17655791					
Application Number:	14105811					
International Application Number:						
Confirmation Number:	5836					
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL					
First Named Inventor/Applicant Name:	WEI-YU CHEN					
Customer Number:	24728					
Filer:	Tim Tingkang Xia/Debby Yew					
Filer Authorized By:	Tim Tingkang Xia					
Attorney Docket Number:	14970-94702					
Receipt Date:	13-DEC-2013					
Filing Date:						
Time Stamp:	14:55:47					
Application Type:	Utility under 35 USC 111(a)					

Payment information:

Submitted with Payment	yes			
Payment Type	Deposit Account			
Payment was successfully received in RAM	\$2080			
RAM confirmation Number	1437			
Deposit Account	503537			
Authorized User				
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Charge any Additional Fees required under 37 C.F.R. Section 1.17 (Patent application and reexamination processing fees)				
	AOET, Ex. 1002			

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File Listing	:				
Document Number	Document Description	File Name	File Size(Bytes)/ Message Digest	Multi Part /.zip	Pages (if appl.)
1		14070047007	191208		1
1	Transmittal of New Application	1497094702Trans.pdf	c911943ffb92207dc234e0ab91fe63eb9832 931f	no	I
Warnings:	·		· · · · · ·	-	
Information:			1		
2	Fee Worksheet (SB06)	1497094702FeeTrans.pdf	169762	no	1
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Information:			1		
3	Application Data Sheet	1497094702ADS.pdf	1505518	no	6
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Information:					
4		1497094702Spec.pdf	296526	yes	56
			832ad976d3e8915629b09063f87e1e98258 4299f		
	Multip	art Description/PDF files in	.zip description		
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	Specificati	on	1	2	17
	Claims		48	5	55
	Abstract	t	56	<u>.</u>	56
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Information:					
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5	drawings	1497 0547 02D1awings.pdi	c0565e7bd2ed4bfa2dbfc4191ecf76326662 d2e0	110	25
Warnings:					
Information:					
6	Power of Attorney	1497094702POA.pdf	374075	no	2
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Warnings:					
Information:				ET. Ex. 10	

7	Oath or Declaration filed	1497094702Dec.pdf	442888	no	1		
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8	Fee Worksheet (SB06)	fee-info.pdf	ce80c93b35e126b657e711b774b52e7114 277f93	no			
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		Total Files Size (in bytes)	36	36789			
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If a new application is being filed and the application includes the necessary components for a filing date (see 37 CFR 1.53(b)-(d) and MPEP 506), a Filing Receipt (37 CFR 1.54) will be issued in due course and the date shown on this Acknowledgement Receipt will establish the filing date of the application.

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If a timely submission to enter the national stage of an international application is compliant with the conditions of 35 U.S.C. 371 and other applicable requirements a Form PCT/DO/EO/903 indicating acceptance of the application as a national stage submission under 35 U.S.C. 371 will be issued in addition to the Filing Receipt, in due course.

New International Application Filed with the USPTO as a Receiving Office

If a new international application is being filed and the international application includes the necessary components for an international filing date (see PCT Article 11 and MPEP 1810), a Notification of the International Application Number and of the International Filing Date (Form PCT/RO/105) will be issued in due course, subject to prescriptions concerning national security, and the date shown on this Acknowledgement Receipt will establish the international filing date of the application.

PATENT APPLICATION FEE DETERMINATION RECORD Substitute for Form PTO-875								Application or Docket Number 14/105,811			
APPLICATION AS FILED - PART I (Column 1) (Column 2) SMALL ENTITY						OR	OTHER THAN OR SMALL ENTITY				
	FOR	NUMBE	R FILE	D NUMBE	R EXTRA		RATE(\$)	FEE(\$)		RATE(\$)	FEE(\$)
	SIC FEE FR 1.16(a), (b), or (c))	N	/A	1	J/A		N/A]	N/A	280
	ARCH FEE FR 1.16(k), (i), or (m))	N	/A	Ν	J/A		N/A		1	N/A	600
	MINATION FEE FR 1.16(o), (p), or (q)	N	/A	Ν	N/A		N/A		1	N/A	720
TOT	AL CLAIMS	26	minus	20= *	6				OR	× 80 =	480
IND	EPENDENT CLAI FR 1.16(h))	^{MS} 3	minus	3 = *					1	× 420 =	0.00
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		CATION AS A			1		I		1		
		(Column 1)		(Column 2)	(Column 3)		SMALL	ENTITY	OR	OTHER THAN SMALL ENTITY	
NT A		CLAIMS REMAINING AFTER AMENDMENT		HIGHEST NUMBER PREVIOUSLY PAID FOR	PRESENT EXTRA		RATE(\$)	ADDITIONAL FEE(\$)		RATE(\$)	ADDITIONAL FEE(\$)
ΜË	Total (37 CFR 1.16(i))	*	Minus	**	=	x	=		OR	x =	
AMENDMENT	Independent (37 CFR 1.16(h))	*	Minus	***	=	x	=		OR	x =	
AM	Application Size F	ee (37 CFR 1.16(s))			1						
	FIRST PRESENT	ATION OF MULTIPL	E DEPEN	DENT CLAIM (37 C	CFR 1.16(j))				OR		
							TOTAL ADD'L FEE		OR	TOTAL ADD'L FEE	
		(Column 1)		(Column 2)	(Column 3)	. —			•		
NT B		CLAIMS REMAINING AFTER AMENDMENT		HIGHEST NUMBER PREVIOUSLY PAID FOR	PRESENT EXTRA		RATE(\$)	ADDITIONAL FEE(\$)		RATE(\$)	ADDITIONAL FEE(\$)
ΜË	Total (37 CFR 1.16(i))	*	Minus	**	=	×	=		OR	x =	
AMENDMENT	Independent (37 CFR 1.16(h))	*	Minus	***	=	x	=		OR	x =	
AM		ee (37 CFR 1.16(s))							1		
	FIRST PRESENT	ATION OF MULTIPL	E DEPEN	DENT CLAIM (37 C	CFR 1.16(j))				OR		
							TOTAL ADD'L FEE		OR	TOTAL ADD'L FEE	
*	 If the entry in co If the "Highest N If the "Highest Num The "Highest Num 	Jumber Previous	ly Paid Fo Paid For"	or" IN THIS SPA IN THIS SPACE is	CE is less thar s less than 3, er	n 20, e nter "3"	nter "20". '.	in column 1.			

	United State	<u>s Patent</u>	and Tradema	ARK OFFICE UNITED STATES DI United States Pater Address: COMMISSIONE P.O. Box 1450 Alexandria, Virginia www.uspto.gov	nt and Trademark O CR FOR PATENTS	
APPLICATION NUMBER	FILING or 371(c) DATE	GRP ART UNIT	FIL FEE REC'D	ATTY.DOCKET.NO	TOT CLAIMS	IND CLAIMS
14/105,811	12/13/2013	2872	2080	14970-94702	26	3
				COI	NFIRMATION	NO. 5836
24728				FILING RECE	EIPT	
MORRIS MAN	NING MARTIN	I LLP				
1600 ATLANT	A FINANCIAL (CENTER		*0000	00000065866426	
ATLANTA GA	30326					

Date Mailed: 01/08/2014

Receipt is acknowledged of this non-provisional patent application. The application will be taken up for examination in due course. Applicant will be notified as to the results of the examination. Any correspondence concerning the application must include the following identification information: the U.S. APPLICATION NUMBER, FILING DATE, NAME OF APPLICANT, and TITLE OF INVENTION. Fees transmitted by check or draft are subject to collection. Please verify the accuracy of the data presented on this receipt. If an error is noted on this Filing Receipt, please submit a written request for a Filing Receipt Correction. Please provide a copy of this Filing Receipt with the changes noted thereon. If you received a "Notice to File Missing Parts" for this application, please submit any corrections to this Filing Receipt with your reply to the Notice. When the USPTO processes the reply to the Notice, the USPTO will generate another Filing Receipt incorporating the requested corrections

Inventor(s)

WEI-YU CHEN, Taichung, TAIWAN;

Applicant(s)

LARGAN PRECISION CO., LTD., Taichung, TAIWAN Assignment For Published Patent Application

LARGAN PRECISION CO., LTD., Taichung, TAIWAN

Power of Attorney: The patent practitioners associated with Customer Number 24728

Domestic Applications for which benefit is claimed - None. A proper domestic benefit claim must be provided in an Application Data Sheet in order to constitute a claim for domestic benefit. See 37 CFR 1.76 and 1.78.

Foreign Applications (You may be eligible to benefit from the **Patent Prosecution Highway** program at the USPTO. Please see <u>http://www.uspto.gov</u> for more information.) TAIWAN 102139029 10/29/2013

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IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL

Preliminary Class

Title

359

Statement under 37 CFR 1.55 or 1.78 for AIA (First Inventor to File) Transition Applications: No

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NOTICE OF ACCEPTANCE OF POWER OF ATTORNEY

This is in response to the Power of Attorney filed 12/13/2013.

The Power of Attorney in this application is accepted. Correspondence in this application will be mailed to the above address as provided by 37 CFR 1.33.

/hnguyen/

Office of Data Management, Application Assistance Unit (571) 272-4000, or (571) 272-4200, or 1-888-786-0101

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茲證明所附文件,係本局存檔中原申請案的副本,正確無訛, 其申請資料如下 :

This is to certify that annexed is a true copy from the records of this office of the application as originally filed which is identified hereunder :

西元 2013 年 10 月 29 日 申 請 日 Oct. 29, 2013 **Application Date** 申 號 : 102139029 請 案 Application No. 申 人 : 大立光電股份有限公司 請 Applicant(s) 人 : 陳緯彧 發 明 Inventor(s) 長 局

Director General 王美花

西元 <u>2013</u> 年 <u>11</u> 月 <u>11</u> 日 Nov. 11, 2013



發明摘要

※ 申請案號: ※ 申請日:

※IPC 分類:

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5 【發明名稱】(中文/英文)

影像拾取系統透鏡組、取像裝置及可攜裝置/ Image Capturing Lens System, Imaging Device and Mobile Terminal

10 【中文】

本發明提供一種影像拾取系統透鏡組,由物側至像側依序包 含:一具屈折力的第一透鏡;一具正屈折力的第二透鏡,其像側面 於近光軸處為凸面;一具負屈折力的第三透鏡,其物側面於近光軸 處為凹面,其像側面於近光軸處為凸面;及一具屈折力的第四透 鏡,其像側面於近光軸處為凹面,其物側面及像側面皆為非球面, 且其像側面於離軸處具有至少一凸面。藉由上述結構,在滿足特定 條件下,可有利於具備大視角及縮短系統總長度,並提升周邊解像 力和照度。

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【英文】



This invention provides an image capturing lens system comprising from object-side to image-side: a first lens element with refractive power; a positive second lens element having a convex image-side surface in a paraxial region; a negative third lens element having a concave object-side surface in a paraxial region and a convex image-side surface in a paraxial region; and a fourth lens element with refractive power having a concave image-side surface in a paraxial region, both of the object-side and image-side surfaces being aspheric, and the image-side surface has at least a convex shape at an off-axis region thereof. When particular relations are satisfied with the aforesaid structure configuration, wide field of view can be obtained, the total track length can be favorably reduced and the resolution for peripheral image and illumination can be improved.

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【代表圖】

【本案指定代表圖】:第(一A)圖。 【本代表圖之符號簡單說明】:

5	光圈	100	•	
	第一透鏡	110		
	物側面	111	像側面	112
	第二透鏡	120		1
	物側面	121	像側面	122
10	第三透鏡	130		
	物側面	131	像側面	132
	第四透鏡	140		
	物側面	141	像側面	142
	紅外線濾除濾光元件		150	
15 [·]	成像面	160		•
	電子感光元件	- 170	•	

【本案若有化學式時,請揭示最能顯示發明特徵的化學式】:

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無

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發明專利說明書

(本說明督格式、順序,請勿任意更勁)

【發明名稱】(中文/英文)

影像拾取系統透鏡組、取像裝置及可攜裝置/ Image Capturing Lens System, Imaging Device and Mobile Terminal

【技術領域】

本發明係關於一種影像拾取系統透鏡組,特別是關於一種應 10 用於可攜式電子產品的影像拾取系統透鏡組。

【先前技術】

> 隨著個人電子產品逐漸輕薄化,電子產品內部各零組件被要求具有更小的尺寸。攝影鏡頭的尺寸在這個趨勢下同樣面臨著小型化的要求。除了小型化的要求之外,因為半導體製程技術的進步使得感光元件的畫素面積縮小,攝影鏡頭逐漸往高畫素領域發展,因此,對成像品質的要求也日益增加。

傳統搭載於可攜式電子產品上的小型化光學系統,多採用三 片式透鏡結構為主,但由於智慧型手機(Smart Phone)、平板電腦 (Tablet PC)與可穿戴式設備(Wearable Apparatus)等高規格可攜裝 置(Mobile Terminal)的盛行,使得攝影鏡頭在畫素與成像品質上 的迅速攀升,習知的三片式攝影鏡頭已無法滿足更高階的攝影需 求。

領域中亦提出四片式透鏡組,期能提供更優異的成像品質。 然而,習用四片式透鏡組往往未能在大視角及鏡頭總長度之間取 得良好的平衡,且對於周邊影像的解像力與照度也不甚理想,尚 未能滿足領域中所要求的高階成像品質。

因此,領域中急需一種在滿足小型化的條件下,具有良好之

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周邊解像力與照度的攝影鏡頭。

【發明內容】

本發明提供一種影像拾取系統透鏡組,由物側至像側依序包 含:一具屈折力的第一透鏡;一具正屈折力的第二透鏡,其像側 5 面於近光軸處為凸面;一具負屈折力的第三透鏡,其物側面於近 光軸處為凹面,其像側面於近光軸處為凸面;及一具屈折力的第 四透鏡,其像側面於近光軸處為凹面,其物側面及像側面皆為非 球面,且其像側面於離軸處具有至少一凸面;其中,該影像拾取 系統透鏡組中具有屈折力的透鏡為四片;其中,該第一透鏡物側 10 面至該第四透鏡像側面於光軸上的距離為 Td·該影像拾取系統透 鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組的焦距 為 f,該第四透鏡的焦距為 f4,該第二透鏡的焦距為 f2,該第三 透鏡的焦距為 f3, 係滿足下列關係式: 0.5 mm < Td < 3.2 mm; 1.0 mm < Td / tan(HFOV) < 3.75 mm; |f / f4| < 1.20; 及 f2 / f3 < 15 -0.65 •

另一方面,本發明提供一種影像拾取系統透鏡組,由物側至 像側依序包含:一具屈折力的第一透鏡;一具正屈折力的第二透 鏡,其像側面於近光軸處為凸面;一具負屈折力的第三透鏡,其 物側面於近光軸處為凹面,其像側面於近光軸處為凸面;及一具 屈折力的第四透鏡,其像側面於近光軸處為凹面,其物側面及像 側面皆為非球面,且其像側面於離軸處具有至少一凸面;其中, 該影像拾取系統透鏡組中具有屈折力的透鏡為四片;其中,該第 一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td·該影像 拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透 鏡組的焦距為 f,該第四透鏡的焦距為 f4,該第三透鏡的焦距為 f3, 係滿足下列關係式: 0.5 mm < Td < 3.2 mm; 1.0 mm < Td / tan(HFOV) < 3.75 mm; |f / f4| < 1.20; 及-2.0 < f / f3 < -0.95。

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又一方面,本發明提供一種影像拾取系統透鏡組,由物側至 像側依序包含:一具屈折力的第一透鏡;一具正屈折力的第二透 鏡,其像側面於近光軸處為凸面;一具負屈折力的第三透鏡,其 物側面於近光軸處為凹面,其像側面於近光軸處為凸面;及一具 屈折力的第四透鏡,其像側面於近光軸處為凹面,其物側面及像 側面皆為非球面,且其像側面於避軸處具有至少一凸面;其中, 該影像拾取系統透鏡組中具有屈折力的透鏡為四片;其中,該第 一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像 拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透 鏡組的焦距為 f,該第四透鏡的焦距為 f4,該影像拾取系統透鏡 組的光圈值為 Fno, 係滿足下列關係式:0.5 mm < Td < 3.2 mm; 1.0 mm < Td / tan(HFOV) < 3.75 mm; |f / f4| < 1.20;及 1.40 < Fno ≤ 2.25 。

再一方面,本發明提供一種取像裝置,包含如前述的影像拾15 取系統透鏡組及一電子感光元件。

更一方面,本發明提供一種可攜裝置,包含如前述的取像裝置。

當 Td 滿足上述條件時,有利於維持系統的小型化。

當 Td / tan(HFOV)滿足上述條件時,有助於使該影像拾取系 20 統透鏡組同時具備大視角及短總長的特性。

當|f / f4|滿足上述條件時,可使系統的主點更遠離成像面, 有利於缩短系統的光學總長度,以維持鏡頭的小型化。

當 f2 / f3 滿足上述條件時,該第二透鏡與該第三透鏡的屈折 力配置較為平衡,可有助於像差的修正與敏感度的降低。

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當 f / f3 滿足上述條件時,該第三透鏡的作用如同補正透鏡, 其功能為平衡及修正系統所產生的各項像差,進而可使系統獲得 更高的成像品質。

當 Fno 滿足上述條件時,有助於提升系統的周邊照度。

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【圖式簡單說明】

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第一 A 圖係本發明第一窗施例的取像裝置示意圖。 第一 B 圖係本發明第一寶施例的像差曲線圖。 第二 A 圖係本發明第二實施例的取像裝置示意圖。 第二 B 圖係本發明第二實施例的像差曲線圖。 第三 A 圖係本發明第三實施例的取像裝置示意圖。 第三 B 圖係本發明第三實施例的像差曲線圖。 第四 A 圖係本發明第四實施例的取像裝置示意圖。 第四 B 圖係本發明第四實施例的像差曲線圖。 第五 A 圖係本發明第五實施例的取像裝置示意圖。 第五 B 圖係本發明第五實施例的像差曲線圖。 第六 A 圖係本發明第六實施例的取像裝置示意圖。 第六 B 圖係本發明第六實施例的像差曲線圖。 第七 A 圖係本發明第七實施例的取像裝置示意圖。 第七B圖係本發明第七實施例的像差曲線圖。 第八 A 圖係本發明第八實施例的取像裝置示意圖。 第八 B 圖係本發明第八實施例的像差曲線圖。 第九 A 圖係本發明第九實施例的取像裝置示意圖。 第九 B 圖係本發明第九實施例的像差曲線圖。 第十 A 圖係本發明第十寶施例的取像裝置示意圖。 第十 B 圖係本發明第十實施例的像差曲線圖。 第十一 A 圖係示意裝設有本發明之取像裝置的智慧型手機。 第十一 B 圖係示意裝設有本發明之取像裝置的平板電腦。 第十一 C 圖係示意裝設有本發明之取像裝置的可穿戴式設

25 備。

【實施方式】

本發明提供一種影像拾取系統透鏡組,由物側至像側依序包 含具屈折力的第一透鏡、第二透鏡、第三透鏡、及第四透鏡。

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該第一透鏡可具有正屈折力,可提供系統所需的正屈折力, 有助於缩短系統的總長度。該第一透鏡物側面可為凸面,可有效 加強缩短光學總長度的功效。

該第二透鏡具正屈折力,有助於利用第二透鏡調和第一透鏡 的匯聚能力。該第二透鏡的像側面於近光軸處為凸面,有助於修 正系統的像散。

該第三透鏡具負屈折力,有助於系統的像差修正。該第三透 鏡物側面近光軸處為凹面,其像側面近光軸處為凸面,可有助於 修正系統的像散。

該第四透鏡物側面近光軸處可為凸面,其像側面近光軸處為 凹面,且其像側面於離軸處具有至少一凸面,有助於修正系統非 點收差(Astigmatism),並可有效修正離軸像差。

該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,當影像拾取系統透鏡組滿足下列關係式:0.5 mm < Td < 3.2 mm 時,有利於維持系統的小型化;較佳地,滿足下列關係式: 0.8 mm < Td < 2.5 mm。

該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,當影像 拾取系統透鏡組滿足下列關係式:1.0 mm < Td / tan(HFOV) < 3.75 mm 時,有助於使該影像拾取系統透鏡組同時具備大視角及 短總長的特性;較佳地,滿足下列關係式:1.2 mm < Td / tan(HFOV) < 2.75 mm。

該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,當影像拾取系統透鏡組滿足下列關係式: |f/f4| < 1.20 時, 可使系統的主點更遠離成像面,有利於縮短系統的光學總長度, 以維持鏡頭的小型化。

該第二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,當影像拾 取系統透鏡組滿足下列關係式:f2/f3<-0.65時,該第二透鏡與 該第三透鏡的屈折力配置較為平衡,可有助於像差的修正與敏感

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度的降低;較佳地,滿足下列關係式:f2/f3 < -0.75。

該影像拾取系統透鏡組的焦距為 f,該第三透鏡的焦距為 f3,當影像拾取系統透鏡組滿足下列關係式:-2.0 < f / f3 < -0.95 時,該第三透鏡的作用如同補正透鏡,其功能為平衡及修正系統 所產生的各項像差,進而可使系統獲得更高的成像品質。

該影像拾取系統透鏡組的光圈值為 Fno,當影像拾取系統透鏡組滿足下列關係式:1.40 < Fno ≤ 2.25 時,有助於提升系統的 周邊照度。

該影像拾取系統透鏡組的焦距為 f,該第一透鏡的焦距為 f1,
a影像拾取系統透鏡組滿足下列關係式:-0.25 < f / f1 < 0.75 時,
該第一透鏡的屈折力較為合適,避免敏感度過高;較佳地,滿足下列關係式:0.25 < f / f1 < 0.75。

該第二透鏡物側面的曲率半徑為 R3,該第二透鏡像側面的曲率半徑為 R4。當影像拾取系統透鏡組滿足下列關係式:0.5
(R3+R4)/(R3-R4) < 2.5 時,有助於加強像差的修正。

該影像拾取系統透鏡組的焦距為 f,當影像拾取系統透鏡組滿 足下列關係式: 0.5 mm < f < 2.0 mm 時,有助於提供適當的光學 總長度。

該第一透鏡、該第二透鏡、該第三透鏡、及該第四透鏡於光
 軸上之厚度的總合為ΣCT,該第一透鏡物側面至該第四透鏡像側
 面於光軸上的距離為 Td,當影像拾取系統透鏡組滿足下列關係
 式:0.80 < ΣCT / Td < 0.95 時,有利於該影像拾取系統透鏡組的
 組裝,並降低敏感度。

該第一透鏡的色散係數為 V1,當影像拾取系統透鏡組滿足下25 列關係式: 45 < V1 時,可有效修正系統色差。

該第二透鏡於光軸上的厚度為 CT2,該第一透鏡於光軸上的 厚度為 CT1,該第三透鏡於光軸上的厚度為 CT3,該第四透鏡於 光軸上的厚度為 CT4,當影像拾取系統透鏡組滿足下列關係式: 0.65 < CT2 / (CT1+CT3+CT4) < 2.0 時,各透鏡的厚度較為合適,

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有助於鏡片的製作及組裝。

該影像拾取系統透鏡組的最大視角為 FOV,當影像拾取系統 透鏡組滿足下列關係式:80度 < FOV < 110度時,有利於取得 足夠的視場角。

本發明的影像拾取系統透鏡組中,透鏡的材質可為玻璃或塑 膠,若透鏡的材質為玻璃,則可以增加該影像拾取系統透鏡組屈 折力配置的自由度,若透鏡材質為塑膠,則可以有效降低生產成 本。此外,可於鏡面上設置非球面(ASP),非球面可以容易製作 成球面以外的形狀,獲得較多的控制變數,用以消減像差,進而 缩减透鏡使用的數目,因此可以有效降低本發明的影像拾取系統 透鏡組的總長度。

本發明的影像拾取系統透鏡組中,可至少設置一光闌,如孔 徑光闌(Aperture Stop)、耀光光闌(Glare Stop)或視場光闌(Field Stop)等。

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本發明影像拾取系統透鏡組中,光圈配置可為前置或中置, 其中前置光圈意即光圈設置於被攝物與第一透鏡間,中置光圈則 表示光圈設置於第一透鏡與成像面間,前置光圈可使影像拾取系 統透鏡組的出射瞳(Exit Pupil)與成像面產生較長的距離,使之具 有遠心(Telecentric)效果,可增加電子感光元件如 CCD 或 CMOS 接收影像的效率;中置光圈則有助於擴大系統的視場角,使影像 拾取系統透鏡組具有廣角鏡頭之優勢。

本發明影像拾取系統透鏡組中,就以具有屈折力的透鏡而 言,若透鏡表面係為凸面且未界定該凸面位置時,則表示該透鏡 表面於近光軸處為凸面;若透鏡表面係為凹面且未界定該凹面位 置時,則表示該透鏡表面於近光軸處為凹面。

本發明的影像拾取系統透鏡組更可視需求應用於變焦的光 學系統中,並兼具優良像差修正與良好成像品質的特色可多方面 應用於 3D(三维)影像擷取、數位相機、行動裝置、數位平板與可 穿戴式設備等可攜裝置中。

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本發明更提供一種取像裝置,其包含前述影像拾取系統 透鏡組以及電子感光元件,其中該電子感光元件設置於該影 像拾取系統透鏡組的成像面,因此取像裝置可藉由影像拾取系 統透鏡組的系統設計,有利於縮短大視角的系統總長,並提升周 邊解像力與照度,進而達到最佳成像效果。較佳地,該取像裝置 可進一步包含鏡筒(Barrel Member)、支持裝置(Holder Member)或 其組合。

請參第十一 A 圖、第十一 B 圖、第十一 C 圖,該取像裝置 (1101)可搭載於可攜裝置,其包括,但不限於:智慧型手機(1110)、 70 平板電腦(1120)、或可穿戴式設備(1130)。前揭可攜裝置僅是示範 性地說明本發明之取像裝置的實際運用例子,並非限制本發明之 取像裝置的運用範圍。較佳地,該可攜裝置可進一步包含控制單 元(Control Unit)、顯示單元(Display)、儲存單元(ROM)、暫儲存單 元(RAM)或其組合。

本發明的取像裝置及影像拾取系統透鏡組將藉由以下具體 實施例配合所附圖式予以詳細說明。

《第一實施例》

本發明第一實施例請參閱第一 A 圖,第一實施例的像差曲線 請參閱第一 B 圖。第一實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(170),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(110),其材質為塑膠,其物側面 (111)於近光軸處為凸面,其像側面(112)於近光軸處為凹面,且其 兩面皆為非球面;

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一具正屈折力的第二透鏡(120),其材質為塑膠,其物側面 (121)於近光軸處為凸面,其像側面(122)於近光軸處為凸面,且 其兩面皆為非球面;

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一具負屈折力的第三透鏡(130),其材質為塑膠,其物側面 (131)於近光軸處為凹面,其像側面(132)於近光軸處為凸面,且 其兩面皆為非球面;及

一具正屈折力的第四透鏡(140),其材質為塑膠,其物側面 (141)於近光軸處為凸面,其像側面(142)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(142)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(100),置於該 第一透鏡(110)與該第二透鏡(120)間;另包含有一紅外線濾除濾光 元件(IR-cut filter)(150)置於該第四透鏡(140)與一成像面(160) 間,其材質為玻璃且不影響焦距。

其中,該電子感光元件(170)設置於該成像面(160)上。

第一實施例詳細的光學數據如表一所示,其非球面數據如表 二所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義 為最大視角的一半。

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		Wije	爱			· · ·		
			(第一節	了施例)				
		<u>f = 1.J7 m</u>	m <u>, Fno = 2,</u>	20. HFOV =	= 46.7 deg.	_		
表面#		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限	1			
1	第一透鏡	1.666	ASP	0.256	塑膠	1.650	21.4	9.56
2		2.139	ASP	0.031				
3	光圈	平面		0.019				
4	第二透鏡	5.712	ASP	0.671	塑膠	1.544	55.9	0.82
5		-0.464	ASP	0.130				
6	第三透鏡	-0.228	ASP	0.230	塑膠	1.634	23.8	-1.06
7		-0.480	ASP	0.030				
8	第四透鏡	0.679	ASP	0.483	塑膠	1.535	55.7	1.52
9		3.062	ASP	0.300				
10	红外缐滬除	平面		0.145	玻璃	1.517	64.2	-
11	泡光 片	平面		0.204		Γ		
12	成像面	平面		-				
注:参考	波長為 d-line	587.6 nm						

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		表二	•	
		非球面係數		
表面#	1	2	4	5
k ==	1.2237E+00	1.7244E+01	9.0000E+01	-6.9311E-01
A4 =	3.1416E-01	1.1703E+00	-4.1498E-01	-6.9345E-01
A6 =	-1.0010E+00	-2.0080E+01	3.6416E+00	1.3202E+00
A8 =	4.5872E+01	5.2569E+02	4.3035E+01	1.0955E+01
A10 =	-5.9339E+02	-3.0044E+03	-7.4996E+03	-3.8285E+02
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0040E+03
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04
表面 #	6	7	8	9
k =	-9.8477E-01	-3.2669E+00	-6.1619E-01	-1.4636E+01
A4 =	3.5682E+00	-1.8915E+00	-1.2870E+00	1.2883E+00
A6 =	-3.7958E+00	8.7075E+00	3.1244E+00	-3.7603E+00
A8 =	-1.1135E+02	-3.6761E+01	-9.1933E+00	5.9040E+00
A10 =	1.5862E+03	1.7257E+02	1.7146E+01	-5.8521E+00
A12 =	-8.7685E+03	-4.8146E+02	-1.9850E+01	3.5356E+00
A14 =	2.3054E+04	6.7728E+02	1.2752E+01	-1.1759E+00
A16 =	-2.3557E+04	-3.6747E+02	-3.5165E+00	1.6169E-01

上述的非球面曲線的方程式表示如下:

$$X(Y)=(Y^2/R)/(1+sqrt(1-(1+k)*(Y/R)^2))+\sum (Ai)*(Y')$$

其中:

X:非球面上距離光軸為Y的點,其與相切於非球面光軸上 頂點之切面的相對距離;

Y:非球面曲線上的點與光軸的垂直距離;

R:曲率半徑;

k: 錐面係數;

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Ai:第i階非球面係數。

影像拾取系統透鏡組的焦距為 f,影像拾取系統透鏡組的光圈 值為 Fno,影像拾取系統透鏡組中最大視角的一半為 HFOV,其 數值為:f=1.17(毫米), Fno=2.20, HFOV=46.7(度)。

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該第一透鏡(110)的色散係數為 V1,其關係式為: V1 = 21.4。

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該第二透鏡(120)於光軸上的厚度為 CT2,該第一透鏡(110)於 光軸上的厚度為 CT1,該第三透鏡(130)於光軸上的厚度為 CT3, 該第四透鏡(140)於光軸上的厚度為 CT4,其關係式為: CT2 / (CT1+CT3+CT4) = 0.69。

該第二透鏡物側面(121)的曲率半徑為 R3,該第二透鏡像側面 (122)的曲率半徑為 R4,其關係式為:(R3+R4)/(R3-R4)=0.85。

該影像拾取系統透鏡組的焦距為 f,該第一透鏡(110)的焦距為 f1,其關係式為: f/f1 = 0.12。

該第二透鏡(120)的焦距為 f2,該第三透鏡(130)的焦距為 f3,
 10 其關係式為: f2 / f3 = -0.77。

該影像拾取系統透鏡組的焦距為 f,該第四透鏡(140)的焦距為 f4,其關係式為: |f/f4| = 0.77。

該影像拾取系統透鏡組的焦距為 f,該第三透鏡(130)的焦距為 f,其關係式為: f/f3 = -1.10。

該第一透鏡物側面(111)至該第四透鏡像側面(142)於光軸上 的距離為 Td,其關係式為: Td = 1.850(毫米)。

該第一透鏡(110)、該第二透鏡(120)、該第三透鏡(130)、及該
第四透鏡(140)於光軸上之厚度的總合為∑CT,該第一透鏡物側面
(111)至該第四透鏡像側面(142)於光軸上的距離為 Td,其關係式為:∑CT/Td = 0.89。

該第一透鏡物側面(111)至該第四透鏡像側面(142)於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,其關係式為:Td/tan(HFOV) = 1.74(毫米)。

該影像拾取系統透鏡組的最大視角為 FOV,其關係式為:FOV25 = 93.4(度)。

《第二實施例》

本發明第二實施例請參閱第二 A 圖,第二實施例的像差曲線 請參閱第二 B 圖。第二實施例的取像裝置包含影像拾取系統透鏡

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AOET, Ex. 1002 Page 115 i. S 組與一電子感光元件(270),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(210),其材質為塑膠,其物側面 (211)於近光軸處為凸面,其像側面(212)於近光軸處為凹面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(220),其材質為塑膠,其物側面 (221)於近光軸處為凸面,其像側面(222)於近光軸處為凸面,且 其兩面皆為非球面;

一具負屈折力的第三透鏡(230),其材質為塑膠,其物側面
 (231)於近光軸處為凹面,其像側面(232)於近光軸處為凸面,且
 其兩面皆為非球面;及

一具正屈折力的第四透鏡(240),其材質為塑膠,其物側面 (241)於近光軸處為凸面,其像側面(242)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(242)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(200),置於該 第一透鏡(210)與該第二透鏡(220)間;另包含有一紅外線濾除濾 光元件(250)置於該第四透鏡(240)與一成像面(260)間,其材質為 玻璃且不影響焦距。

其中,該電子感光元件(270)設置於該成像面(260)上。

第二實施例詳細的光學數據如表三所示,其非球面數據如表 四所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義 為最大視角的一半。

			农	Ξ				
			(第二)	雪施例)				· .
	•	<u>f = 1.23 r</u>	<u>nm, Fno = 2.</u>	45 <u>, HFOV</u> =	= 45.6 deg.		·	
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.728	ASP	0.217	塑膠	1.640	22.0	1207.16
2		1.647	ASP	0.041				
3	光圈	平面		0.020	1			

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4	第二透鏡	2.201	ASP	0.685	磁磁	1.544	55.9	0.78
5		-0.465	ASP	0.138		· · .		
6	第三透鏡	-0.213	ASP	0.222	塑膠	1.634	23.8	-0.90
7		-0.479	ASP	0.030				
8	第四透鏡	0.691	ASP	0.430	塑膠	1.535	55.7	1.40
9		7.112	ASP	0.300	·			
10	紅外線濾除	平面		0.300	玻璃	1.517	64.2	-
11	泡光片 🗌	平面		0.171				
12	成像面	平面		-				1

		表四		_					
	非球面係數								
表面 #	1	2	4	5					
k =	-7.8611E-01	2.2256E+01	4.4287E+01	-6.8249E-01					
A4 =	2.7433E-01	3.5449E-01	-1.1581E+00	-5.9944E-01					
A6 =	-1.5466E+00	-2.9377E+01	8.9406E-01	3.6061E-01					
A8 =	4.7455E+01	6.4129E+02	4.1870E+01	1.6896E+01					
A10 =	-6.0092E+02	-3.8207E+03	-7.3180E+03	-3.8194E+02					
A12 =	4.0961E+03	-1.6432E+05	1.3290E+05	3.0043E+03					
A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0680E+04					
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3826E+04					
表面 #	6	7	8	9					
k =	-1.0107E+00	-3.0532E+00	-7.4231E-01	2.2155E+01					
A4 =	3.8803E+00	-1.7079E+00	-1.1152E+00	1.6267E+00					
A6 =	-4.2860E÷00	8.7245E+00	2.9613E+00	-4.5228E+00					
A8 =	-1.1314E+02	-3.7291E+01	-9.2058E+00	6.4630E+00					
A10 =	1.5859E+03	1.7181E+02	1.7048E+01	-5.8730E+00					
A12 =	-8.7686E+03	-4.8143E+02	-1.9563E+01	3.4083E+00					
A14 =	2.3054E+04	6.7878E+02	1.3110E+01	-1.1920E+00					
A16 =	-2.3557E+04	-3.6776E+02	-4.1607E+00	1.9105E-01					

第二實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表五中所列。

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	表五		
	第二質加		
f (mm)	1.23	12/13	-0.87
Fno	2.45	£7f4	0.88
HFOV [deg.]	45.6	f/B	-1.37

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V1	22.0	Td (mm)	1.783
CT2/(CT1+CT3+CT4)	0.79	ECT/Td	0.87
(R3+R4)/(R3-R4)	0.65	Td/tan(HFOV) [mm]	1.75
f/f1	0.00	FOV [deg.]	91.2

《第三實施例》

本發明第三實施例請參閱第三 A 圖,第三實施例的像差曲線 請參閱第三 B 圖。第三實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(370),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(310),其材質為塑膠,其物側面 (311)於近光軸處為凸面,其像側面(312)於近光軸處為凹面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(320),其材質為塑膠,其物側面 (321)於近光軸處為凹面,其像側面(322)於近光軸處為凸面,且 其兩面皆為非球面;

一具負屈折力的第三透鏡(330),其材質為塑膠,其物側面 (331)於近光軸處為凹面,其像側面(332)於近光軸處為凸面,且 其兩面皆為非球面;及

一具正屈折力的第四透鏡(340),其材質為塑膠,其物側面 (341)於近光軸處為凸面,其像側面(342)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(342)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(300),置於該 20 第一透鏡(310)與該第二透鏡(320)間;另包含有一紅外線濾除濾 光元件(350)置於該第四透鏡(340)與一成像面(360)間,其材質為 玻璃且不影響焦距。

其中,該電子感光元件(370)設置於該成像面(360)上。

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第三實施例詳細的光學數據如表六所示,其非球面數據如表 25 七所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義 為最大視角的一半。

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			表	 穴				
			(第三)	實施例)			<u> </u>	<u> </u>
		<u>f = 1.66 m</u>	m, Fno = 2.	15, HFOV =	= 46.8 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面	•	無限	1			•
1	第一透鏡	1.333	ASP	0.286	塑膠	1.544	55.9	2.50
2		59.851	ASP	0.005				
3	光圈	平面		0.195				
4	第二透鏡	-1.920	ASP	0.409	塑膠	1.544	55.9	1.60
5		-0.644	ASP	0.156				
6	第三透鏡	-0.263	ASP	0.200	塑膠	1.650	21.4	-1.49
7		-0.470	ASP	0.030				
8	第四透鏡	0.677	ASP	0.363	塑膠	1.535	55.7	2.33
9		1.206	ASP	0.400				
10	紅外線滬除	平面		0.175	玻璃	1.517	64.2	•
11	過 光片	平面		0.431				
12	成像面	平面		-				
主:参考	波長為 d-line	587.6 nm						
	第1面有效-	半徑為 0.510 mm						

		表七						
	非球面係數							
表面 #	1	2	4	5				
k =	-2.4704E+00	9.0000E+01	5.8947E+00	-3.7972E-01				
A4 =	-3.4848E-02	-3.8775E-01	-9.3075E-01	-3.3741E-01				
A6 =	-4.4471E-01	-2.8417E+00	3.6516E+00	9.2277E-01				
A8 =	-4.9925E-01	1.8185E+01	-4.0769E+01	-3.9461E+00				
A10 =	-1.2166E+01	-2.0954E+01	-4.4351E+00	-1.9037E+01				
A12 =	3.9114E+01	-1.4998E+03	1.2130E+03	4.9148E+01				
A14 =	-1.7950E+02	1.2389E+04	-4.4615E+03	1.0076E+02				
A16 =	3.3572E+02	-2.9058E+04	6.2425E+03	8.0489E+01				
表面 #	6	7	8	9				
k =	-1.1491E+00	-2.3808E+00	-1.7649E+00	-1.0689E+01				
A4 =	4.2079E+00	2.1562E-01	-6.9591E-01	9.1971E-01				
A6 =	-2.8310E+01	-4.4239E+00	1.2041E+00	-3.0958E+00				
A8 =	1.2287E+02	1.8790E+01	-2.9023E÷00	4.8713E+00				
A10 =	-3.9035E+02	-4.1840E+01	4.4195E+00	-4.6279E+00				
A12 =	8.5064E+02	5.5883E+01	-3.7857E+00	2.6418E+00				
A14 =	-9.7331E+02	-4.0255E+01	1.6532E+00	-8.3581E-01				
A16 =	4.7213E+02	1.4428E+01	-2.8192E-01	1.1204E-01				

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第三實施例非球面曲線方程式的表示如同第一實施例的形 式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表八中所列。

	퀷	 長八	
	第三	窗施例	
f (mm)	1.66	f2/f3	-1.07
Fno	2.15	f/f4	0.71
HFOV [deg.]	46.8	f/f3	-1.11
V1	55.9	Td (mm)	1.644
CT2/(CT1+CT3+CT4)	0.48	ΣCT/Td	0.77
(R3+R4)/(R3-R4)	2.01	Td/tan(HFOV) [mm]	1.54
វវា	0.66	FOV [deg.]	93.6

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《第四實施例》

本發明第四實施例請參閱第四 A 圖,第四實施例的像差曲線 請參閱第四 B 圖。第四實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(470),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具負屈折力的第一透鏡(410),其材質為塑膠,其物側面 (411)於近光軸處為凸面,其像側面(412)於近光軸處為凹面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(420),其材質為塑膠,其物側面
 (421)於近光軸處為凸面,其像側面(422)於近光軸處為凸面,且
 其兩面皆為非球面;

一具負屈折力的第三透鏡(430),其材質為塑膠,其物側面 (431)於近光軸處為凹面,其像側面(432)於近光軸處為凸面,且 其兩面皆為非球面;及

一具正屈折力的第四透鏡(440),其材質為塑膠,其物側面 (441)於近光軸處為凸面,其像側面(442)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(442)於離軸處具有至少一凸面;

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其中,該影像拾取系統透鏡組另設置有一光圈(400),置於該 第一透鏡(410)與該第二透鏡(420)間;另包含有一紅外線濾除濾 光元件(450)置於該第四透鏡(440)與一成像面(460)間,其材質為 玻璃且不影響焦距。

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其中,該電子感光元件(470)設置於該成像面(460)上。

第四實施例詳細的光學數據如表九所示,其非球面數據如表 十所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義 為最大視角的一半。

			农	·九				
			(第四)	茸施例)				
		<u>f = 1.15 n</u>	<u>ım, Fno = 2</u> ,	22, HFOV =	<u>- 48.5 deg.</u>		· · · ·	
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.999	ASP	0.200	塑膠	1.544	55.9	-46.83
2		• 1.789	ASP	0.021				
3	光圈	平面		0.037				
4	第二透鏡	1.606	ASP	0.471	塑膠	,1.544	55.9	0.81
5		-0.543	ASP	0.184	1			
6	第三透鏡	-0.207	ASP	0.209	塑膠	1.634	23.8	-1.22
7		-0.393	ASP	0.030				
8	第四透鏡	0.747	ASP	0.319	塑膠	1.535	55.7	1.62
9		4.607	ASP	0.300				
10	紅外線濾除	平面		0.300	玻璃	1.517	64.2	-
11	减光片	平面		0.130				
12	成像面	平面		-	<u> </u>			
E:参考	波長為 d-line	587.6 nm		·	•	•		

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	丧于 · · · · · · · · · · · · · · · · · · ·							
		非球面係數	·····	<u></u>				
表面 #	1	2	4	5				
k =	-2.2996E+01	3.4247E+01	9.8701E+00	-4.2975E-01				
A4 =	-2.1353E-01	-2.0670E+00	-2.2221E+00	-6.3795E-01				
A6 =	-3.6880E+00	-3.6063E+01	-8.7081E+00	-6.5092E+00				
A8 =	5.2789E+01	6.9201E+02	1.4888E÷02	4.6114E+01				
A10 =	-6.4083E+02	-4.8238E+03	-8.2602E+03	-4.7532E+02				
A12 =	4.0983E+03	-1.6432E+05	1.3290E+05	3.0044E+03				

A14 =	-1.4631E+04	3.1882E+06	-1.1481E+06	-1.0679E+04
A16 =	2.0715E+04	-1.7563E+07	3.7732E+06	1.3828E+04
表面 #	6	7	8	9
k =	-1.0439E+00	-2.0056E+00	-6.4024E-01	-3.3636E+00
A4 =	4.2327E+00	-9.7476E-01	-8.3147E-01	1.0958E+00
A6 =	-3.4551E+00	1.0236E+01	2.1761E+00	-1.7086E+00
A8 =	-1.0303E+02	-3.7610E+01	-4.8336E+00	1.3575E+00
A10 =	1.5970E+03	1.6620E+02	5.0397E+00	-2.6285E+00
A12 =	-8.9315E+03	-4.9093E+02	-4.1411E+00	4.3863E+00
A14 =	2.3054E+04	6.8046E+02	3.4069E+00	-3.3963E+00
A16 =	-2.3558E+04	-3.4010E+02	-1.6576E+00	9.5967E-01

第四實施例非球面曲線方程式的表示如同第一實施例的形 式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表十一中所列。

	表	+							
	第四實施例								
f [mm]	1.15	f2/f3	-0.66						
Fno	2.22	€/f4	0.71						
HFOV [deg.]	48.5	f/f3	-0.94						
V1	55.9	Td (mm)	1.471						
CT2/(CT1+CT3+CT4)	0.65	DCT/Td	0.82						
(R3+R4)/(R3-R4)	0.49	Td/tan(HFOV) [mm]	1.30						
<i>បី</i> ព	-0.02	FOV [deg.]	97.0						

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《第五實施例》

本發明第五實施例請參閱第五 A 圖,第五實施例的像差曲線 請參閱第五 B 圖。第五實施例的取像裝置包含該影像拾取系統透 鏡組與一電子感光元件(570),該影像拾取系統透鏡組主要由四片 具屈折力的透鏡構成,由物側至像側依序包含:

一具負屈折力的第一透鏡(510),其材質為玻璃,其物側面 (511)於近光軸處為凸面,其像側面(512)於近光軸處為凹面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(520),其材質為玻璃,其物側面(521)於近光軸處為凸面,其像側面(522)於近光軸處為凸面,且

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其兩面皆為非球面;

一具負屈折力的第三透鏡(530),其材質為塑膠,其物側面 (531)於近光軸處為凹面,其像側面(532)於近光軸處為凸面,且 其兩面皆為非球面;及

一具正屈折力的第四透鏡(540),其材質為塑膠,其物側面 (541)於近光軸處為凸面,其像側面(542)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(542)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(500),置於該 第一透鏡(510)與該第二透鏡(520)間;另包含有一紅外線濾除濾 光元件(550)置於該第四透鏡(540)與一成像面(560)間,其材質為 玻璃且不影響焦距。

其中,該電子感光元件(570)設置於該成像面(560)上。

第五實施例詳細的光學數據如表十二所示,其非球面數據如 表十三所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義為最大視角的一半。

			表一	+=				
			(第五)	寶施例)				
	· · ·	<u>f = 2.24</u>	mm, Fno = 2.	51 <u>, HFOV</u> =	= 44.2 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限		ł		
1	第一透鏡	1.367	ASP	0.300	玻璃	2.144	17.8	-13.68
2		1.110	ASP	0.144				
3	光圈	平面	平面					
4	第二透鏡	3.909	ASP	1.483	玻璃	1.525	70.3	1.60
5		-0.932	ASP	0.325				
6	第三透鏡	-0.341	ASP	0.277	塑膠	1.639	23.5	-1.72
7		-0.651	ASP	0.030				
8	第四透鏡	0.897	ASP	0.606	塑膠	1.565	57.0	2.00
9		3.302	ASP	0.800		1		
10	红外缐滤除			0.300	玻璃	1.517	64.2	-
11	遼光 片	平面		0.342				
12	成像面			•				
E:参考	波長為 d-line	587.6 nm			1 <u>. </u>	.4		

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		表十三								
	非球面係數									
表面 #		2	4.	5						
k =	1.1992E+00	1.9195E+00	2.1734E+01	-7.2786E-01						
A4 =	5.8324E-02	1.2422E-01	-9.9032E-02	-1.2252E-01						
A6 =	-1.4402E-01	-5.2189E-01	5.9983E+00	5.2990E-01						
A8 =	1.0028E+00	4.2713E+00	-1.1966E+02	-3.0301E+00						
A10 =	-4.0021E+00	1.8016E+01	1.4083E+03	7.9248E+00						
A12 =	8.9035E+00	-4.2193E+02	-9.4428E+03	-1.0795E+01						
A14 =	-9.8479E+00	2.2697E+03	3.3923E+04	6.3429E+00						
A16 =	3.0263E+00	-4.1004E+03	-5.0610E+04	-8.0066E-01						
表面 #	. 6	7	8	9 .						
k =	-9.8774E-01	-3.1767E+00	-8.3817E-01	-2.4331E+01						
·A4 =	2.5606E+00	-1.2881E-01	-4.2259E-01	3.5717E-01						
A6 =	-7.9740E+00	-6.6170E-01	4.3675E-01	-4.5759E-01						
A8 =	1.4853E+01	1.1888E+00	-4.6275E-01	2.9937E-01						
A10 =	-1.1480E+01	-4.2607E-01	3.1380E-01	-1.1921E-01						
A12 =	-4.4740E+00	-5.1720E-01	-1.2912E-01	2.8364E-02						
A14 =	1.2594E+01	5.0722E-01	2.9275E-02	-3.7104E-03						
A16 =	-5.4160E+00	-1.2485E-01	-2.8533E-03	2.0238E-04						

第五實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表十四中所列。

	表	十四	
	第五	實施例	
f [mm]	2.24	f2/f3	-0.93
Fno	2.51	 f/f4 	1.12
HFOV [deg.]	44.2	ťß	-1.30
VI	17.8	Td [mm]	3.150
CT2/(CT1+CT3+CT4)	1.25	ΣCT/Td	0.85
(R3+R4)/(R3-R4)	0.61	Td/tan(HFOV) [mm]	3.24
f/fi	-0.16	FOV [deg.]	88.4

《第六實施例》

本發明第六實施例請參閱第六 A 圖,第六實施例的像差曲線 請參閱第六 B 圖。第六實施例的取像裝置包含影像拾取系統透鏡

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組與一電子感光元件(670),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(610),其材質為塑膠,其物側面 (611)於近光軸處為凸面,其像側面(612)於近光軸處為凸面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(620),其材質為塑膠,其物側面 (621)於近光軸處為凹面,其像側面(622)於近光軸處為凸面,且 其兩面皆為非球面;

一具負屈折力的第三透鏡(630),其材質為塑膠,其物側面
 (631)於近光軸處為凹面,其像側面(632)於近光軸處為凸面,且
 其兩面皆為非球面;及

一具正屈折力的第四透鏡(640),其材質為塑膠,其物側面 (641)於近光軸處為凸面,其像側面(642)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(642)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(600),置於該 第一透鏡(610)與該第二透鏡(620)間;另包含有一紅外線濾除濾 光元件(650)置於該第四透鏡(640)與一成像面(660)間,其材質為 玻璃且不影響焦距。

其中,該電子感光元件(670)設置於該成像面(660)上。

第六實施例詳細的光學數據如表十五所示,其非球面數據如 表十六所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV 定義為最大視角的一半。

			表-	F五				
		· · ·	(第六)	訂施例)				
		<u>f = 1.27 m</u>	<u>m, Fno = 2.</u>	10, HFOV =	= 44.4 deg.	_		
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面	•	無限	_			
1	第一透鏡	2.393	ASP	0.280	塑膠	1.544	55.9	3.85
2		-16.057	ASP	0.017				
3	光圈	平面		0.044				

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4	第二透鏡	-30.373	ASP	0.755	塑膠	1.544	55.9	0.87
5		-0.468	ASP	0.121				<u> </u>
6	第三透鏡	-0.246	ASP	0.240	塑膠	1.639	23.5	-0.90
7		-0.594	ASP	0.030				
8	第四透鏡	0.639	ASP	0.522	塑膠	1.530	55.8	1.47
9		2.521	ASP	0.400				
10	紅外線濾除	平面		0.175	玻璃	1.517	64.2	-
11	1 濾光片	平面		0.073				
12	成像面	平面		-				<u> </u>

	非球面係數									
	. 1	2	4	5						
k =	1.7241E+00	-8.9754E+01	-9.0000E+01	-7.5923E-01						
A4 =	2.1410E-01	1.4516E+00	1.5168E-01	-5.4982E-01						
A6 =	-2.3810E-01	-1.0826E+01	4.8929E+00	2.0791E+00						
A8 =	2.3555E+01	1.9495E+02	-3.2116E+01	8.2787E-01						
A10 =	-2.5034E+02	-5.1780E+02	-2.6801E+03	-1.4893E+02						
A12 =	1.4357E+03	-5.7593E+04	4.6579E+04	1.0534E+03						
A14 =	-4.2381E+03	9.2351E+05	-3.3256E+05	-3.0936E+03						
A16 =	4.9589E+03	-4.2045E+06	9.0327E+05	3.3098E+03						
表面 #	6	7	8	9						
<u>k</u> =	-9.9704E-01	-3.7851E+00	-7.3474E-01	-2.0751E+00						
A4 =	2.9255E+00	-1.3600E+00	-1.2133E+00	1.8260E+00						
A6 =	-2.4852E+00	5.5927E+00	3.0817E+00	-5.9653E+00						
A8 =	-5.7718E+01	-1.8755E+01	-1.0034E+01	9.6816E+00						
A10 =	6.7135E+02	7.3016E+01	1.9498E+01	-9.2466E+00						
A12 =	-3.0733E+03	-1.6937E+02	-2.1549E+01	5.1894E+00						
A14 =	6.6780E+03	1.9522E+02	1.2590E+01	-1.5760E+00						
A16 =	-5.6393E+03	-8.6932E+01	-3.0510E+00	1.9769E-01						

第六實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表十七中所列。

	表十十	-	
	第六實族		
f (mm)	1.27	f2/f3	-0.97
Fno	2.10	f/f4	0.86
HFOV [deg.]	44.4	f/f3	-1.41

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VI	55.9	Td [mm]	2.009
CT2/(CT1+CT3+CT4)	0.72	ΣCT/Td	0.89
(R3+R4)/(R3-R4)	1.03	Td/tan(HFOV) [mm]	2.05
ชก	0.33	FOV [deg.]	88.8

《第七實施例》

本發明第七實施例請參閱第七 A 圖,第一實施例的像差曲線 請參閱第七 B 圖。第七實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(770),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(710),其材質為塑膠,其物側面 (711)於近光軸處為凸面,其像側面(712)於近光軸處為凹面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(720),其材質為塑膠,其物側面 (721)於近光軸處為凹面,其像側面(722)於近光軸處為凸面,且 其兩面皆為非球面;

一具負屈折力的第三透鏡(730),其材質為塑膠,其物側面
 (731)於近光軸處為凹面,其像側面(732)於近光軸處為凸面,且
 15 其兩面皆為非球面;及

一具正屈折力的第四透鏡(740),其材質為塑膠,其物側面 (741)於近光軸處為凸面,其像側面(742)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(742)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(700),置於一 被攝物與該第一透鏡(710)間;另包含有一紅外線濾除濾光元件 (750)置於該第四透鏡(740)與一成像面(760)間,其材質為玻璃且 不影響焦距。

其中,該電子感光元件(770)設置於該成像面(760)上。

第七實施例詳細的光學數據如表十八所示,其非球面數據如
 25 表十九所示,其中曲率半徑、厚度及焦距的單位為毫米,HFOV
 定義為最大視角的一半。

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	·····		表	十八				
	····		(第七	實施例)				
		<u>f = 1.57</u>	<u>mm, Fno = 2</u>	.05, HFOV =	= 48.5 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	光圈	平面		-0.052			1	
2	第一透鏡	1.142	ASP	0.279	塑膠	1.544	55.9	2.84
3		4.008	ASP	0.159				
4	第二透鏡	-4.075	ASP	0.614	塑膠	1.544	55.9	1.24
5		-0.608	ASP	0.142			1	
6	第三透鏡	-0.255	ASP	0.230	塑膠	1.634	23.8	-1.37
7		-0.487	ASP	0.030				
8	第四透鏡	0.636	ASP	0.414	塑膠	1.535	55.7	2.35
9		0.998	ASP	0.500				
10	紅外線濾除	平面		0.175	玻璃	1.517	64.2	-
11	濾光片	平面		0.141				
12	成像面	平面		•				

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	非球面係數									
表面 #	2	3	4	5						
k =	-5.4318E-01	6.9324E+01	6.0179E+01	-4.8138E-01						
A4 =	- 1.1275E-01	-3.4138E-01	-6.6571E-01	-8.5384E-02						
A6 =	-1.4350E+00	-2.7321E+00	4.9846E-01	-6.6518E-01						
A8 =	6.0529E+00	2.0740E+01	-4.5807E+00	-2.1554E-01						
A10 =	4.7148E+01	-7.0776E+01	-1.7027E+02	-7.9977E+00						
A12 =	-1.4571E+02	-1.4998E+03	1.2130E+03	2.5638E+01						
A14 =	-3.8164E+03	1.2389E+04	-4.4615E+03	-4.3167E+01						
A16 =	1.5882E+04	-2.9058E+04	6.2425E+03	7.2938E+01						
表面 #	6	7	8	9						
k =	-1.1103E+00	-3.0258E+00	-9.3042E-01	-5.1455E+00						
A4 =	5.4423E+00	4.5345E-01	-7.7223E-01	7.0200E-01						
A6 =	-3.5666E+01	-4.9768E÷00	9.4468E-01	-1.5850E+00						
A8 =	1.3446E+02	1.9752E+01	-1.3669E+00	1.7028E+00						
A10 =	-2.5131E+02	-4.2912E+01	1.1409E+00	-1.1082E+00						
A12 =	-7.3665E+01	5.3544E+01	-5.2307E-01	4.3302E-01						
A14 =	1.1117E+03	-3.5702E+01	1.2365E-01	-9.2838E-02						
A16 =	-1.2600E+03	1.0063E+01	-1.1645E-02	8.3092E-03						

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第七實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表二十中所列。

	表	二十							
	第七實施例								
f [mm]	1.57	f2/f3	-0.91						
Fno	2.05	£7f4	0.67						
HFOV [deg.]	48.5	វាល	-1.15						
V1	55.9	Td [mm]	1.868						
CT2/(CT1+CT3+CT4)	0.67	SCT/Td	0.82						
(R3+R4)/(R3-R4)	1.35	Td/tan(HFOV) [mm]	1.65						
1/fi	0.55	FOV [deg.]	97.0						

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《第八實施例》

本發明第八實施例請參閱第八 A 圖,第八實施例的像差曲線 請參閱第八 B 圖。第八實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(870),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(810),其材質為塑膠,其物側面 (811)於近光軸處為凸面,其像側面(812)於近光軸處為凹面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(820),其材質為塑膠,其物側面
 (821)於近光軸處為凹面,其像側面(822)於近光軸處為凸面,且
 其兩面皆為非球面;

一具負屈折力的第三透鏡(830),其材質為塑膠,其物側面 (831)於近光軸處為凹面,其像側面(832)於近光軸處為凸面,且 其兩面皆為非球面;及

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一具正屈折力的第四透鏡(840),其材質為塑膠,其物側面 (841)於近光軸處為凸面,其像側面(842)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(842)於離軸處具有至少一凸面;

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其中,該影像拾取系統透鏡組另設置有一光圈(800),置於該 第一透鏡(810)與該第二透鏡(820)間;另包含有一紅外線濾除濾 光元件(850)置於該第四透鏡(840)與一成像面(860)間,其材質為 玻璃且不影響焦距。

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其中,該電子感光元件(870)設置於該成像面(860)上。

第八實施例詳細的光學數據如表二十一所示,其非球面數據 如表二十二所示,其中曲率半徑、厚度及焦距的單位為毫米, HFOV 定義為最大視角的一半。

			表 二	-+-				
			(第八)	實施例)				
		<u>f = 1.68</u>	<u>mm, Fno = 2</u>	.10, HFOV :	= 46.0 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	1.787 ·	ASP	0.278	塑膠	1.544	55.9	3.81
2		12.133	ASP	0.022				
3	光圈	平面		0.145	1			
4	第二透鏡	-3.839	ASP	0.668	塑膠	1.544	55.9	1.38
5		-0.668	ASP	0.194				
6	第三透鏡	-0.273	ASP	0.230	塑膠	1.639	23.5	-1.18
7		-0.569	ASP	0.030	1			
8	第四透鏡	0.784	ASP	0.496	塑膠	1.530	55.8	1.65
9		5.992	ASP	0.400				
10	紅外線濾除	平面		0.175	玻璃	1.517	64.2	-
11	濾光 片	平面		0.472		· · · · ·	1	
12	成像面	平面		-	1	İ	1	

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	·····································								
		非球面係數							
表面 #)	2	4	5					
k =	-1.3232E+00	5.3151E+01	5.1693E+01	-5.9308E-01					
A4 =	1.6281E-02	-1.2122E-02	-2.5602E-01	-1.1508E-01					
A6 =	1.5823E-01	-1.1940E+00	-1.0332E+00	-6.8787E-01					
A8 =	5.9941E-01	1.2093E+01	1.0464E+01	-9.7964E-02					
A10 =	-1.3812E+01	-2.0003E+01	-1.9940E+02	-6.2734E+00					
A12 =	4.5317E+01	-1.4998E+03	1.2130E+03	2.8529E+01					

		•		
A14 =	-4.4460E+01	1.2389E+04	-4.4615E+03	-4.4589E+01
A16 =	-4.7734E+01	-2.9058E+04	6.2425E+03	2.7908E+01
表面#	6	7	8	9
k =	-1.0578E+00	-3.0032E+00	-8.6121E-01	5.6610E+00
A4 =	4.0391E+00	9.4553E-02	-6.6716E-01	7.7788E-01
A6 =	-2.6571E+01	-4.4170E+00	1.1395E+00	-1.2944E+00
A8 =	1.2417E+02	1.9085E+01	-1.7698E+00	1.0967E÷00
A10 =	-3.9394E+02	-4.1568E+01	1.6239E+00	-5.7605E-01
A12 =	8.2748E+02	5.5376E+01	-8.6944E-01	1.8609E-01
A14 =	-9.7331E+02	-4.1902E+01	2.5418E-01	-3.3617E-02
A16 =	4.7213E+02	1.3653E+01	-3.1838E-02	2.5144E-03

第八實施例非球面曲線方程式的表示如同第一實施例的形式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表二十三中所列。

表二十三									
	第八實施例								
f [mm]	1.68	f2/f3	-1.17						
Fno	2.10	Ø/f4	1.02						
HFOV [deg.]	46.0	f/f3	-1.42						
VI	55.9	Td [mm]	2.063						
CT2/(CT1+CT3+CT4)	0.67	ECT/Td	0.81						
(R3+R4)/(R3-R4)	1.42	Td/tan(HFOV) [mm]	1.99						
ថ្មព	0.44	FOV [deg.]	92.0						

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《第九實施例》

本發明第九實施例請參閱第九 A 圖,第九實施例的像差曲線 請參閱第九 B 圖。第一實施例的取像裝置包含影像拾取系統透鏡 組與一電子感光元件(970),該影像拾取系統透鏡組主要由四片具 屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(910),其材質為塑膠,其物側面 (911)於近光軸處為凸面,其像側面(912)於近光軸處為凸面,且其 兩面皆為非球面;

一具正屈折力的第二透鏡(920),其材質為塑膠,其物側面15 (921)於近光軸處為凸面,其像側面(922)於近光軸處為凸面,且

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其兩面皆為非球面;

一具負屈折力的第三透鏡(930),其材質為塑膠,其物側面 (931)於近光軸處為凹面,其像側面(932)於近光軸處為凸面,且 其兩面皆為非球面;及

一具正屈折力的第四透鏡(940),其材質為塑膠,其物側面 (941)於近光軸處為凸面,其像側面(942)於近光軸處為凹面,其 兩面皆為非球面,且其像側面(942)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(900),置於該 第一透鏡(910)與該第二透鏡(920)間;另包含有一紅外線濾除濾 光元件(950)置於該第四透鏡(940)與一成像面(960)間,其材質為 玻璃且不影響焦距。

其中,該電子感光元件(970)設置於該成像面(960)上。

第九實施例詳細的光學數據如表二十四所示,其非球面數據 如表二十五所示,其中曲率半徑、厚度及焦距的單位為毫米, HFOV 定義為最大視角的一半。

			表二	十四				
			(第九)	實施例)				
	T	<u>f = 0.92</u>	mm, Fno = 2.	<u>45, HFOV -</u>	= 43.9 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限				
1	第一透鏡	100.000	ASP	0.205	塑膠	1.633	23.4	13.12
2		-9.046	ASP	0.017				
3	光圈	平面		0.024				
4	第二透鏡	1.695	ASP	0.475	塑膠	1.544	55.9	0.54
5		-0.319	ASP	0.100				
6	第三透鏡	-0.148	ASP	0.160	塑膠	1.634	23.8	-0.65
7	•	-0.329	ASP	0.030			1	
8	第四透鏡	0.595	ASP	0.239	塑膠	1.530	55.8	1.28
9		4.109	ASP	0.300				
10	紅外線濾除	平面		0.145	玻璃	1.517	64.2	-
11	濾光片	平面		0.151				
12	成像面	平面		-			†	

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		表二十五		
		非球面係數		
表面 #	1	2	4	5
k =	-9.0000E+01	9.0000E+01	3.3243E+01	-6.6437E-01
A4 =	2.5656E-01	2.4894E+00	-1.9077E+00	-1.5093E+00
A6 =	-1.0613E+00	-9.5530E+01	-1.3506E+01	4.3096E+00
A8 =	1.6769E+02	3.0126E+03	1.0928E+01	1.6065E+02
A10 =	-3.7307E+03	-2.3016E+04	-4.4021E+04	-2.9203E+03
A12 =	3.9786E+04	-1.5960E+06	1.2908E+06	2.9181E+04
A14 =	-2.1485E+05	4.6819E+07	-1.6860E+07	-1.5683E+05
A16 =	4.5990E+05	-3.8994E+08	8.3772E+07	3.0696E+05
表面 #	6	7	8	9
k =	-1.0921E+00	-2.4247E+00	-6.0015E-01	3.3921E+01
A4 =	8.8579E+00	-1.7457E+00	-1.8642E+00	3.4965E+00
A6 =	-9.7201E+00	2.7059E+01	4.2816E+00	-1.7965E+01
A8 =	-4.6210E+02	-1.6609E+02	-3.6842E+01	3.3243E+01
A10 =	1.0079E+04	1.0699E+03	9.4802E+01	-3.1178E+01
A12 =	-8.5169E+04	-4.7330E+03	-1.9140E+02	1.8452E+01
A14 =	3.3855E+05	1.0605E+04	3.6755E+02	-3.7397E+01
A16 =	-5.2300E+05	-7.7191E+03	-9.3365E+02	3.7762E+01

第九實施例非球面曲線方程式的表示如同第一實施例的形 式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表二十六中所列。

	表二	二十六					
	第九	第九寶施例					
f [mm]	0.92	f2/f3	-0.83				
Fno	2.45	 f/f4 	0.72				
HFOV [deg.]	43.9	f/f3	-1.42				
V1	23.4	Td (mm)	1.250				
CT2/(CT1+CT3+CT4)	0.79	ΣCT/Td	0.86				
(R3+R4)/(R3-R4)	0.68	Td/tan(HFOV) [mm]	1.30				
ศก	0.07	FOV [deg.]	87.8				

《第十實施例》

本發明第十實施例請參閱第十 A 圖,第十實施例的像差曲線 請參閱第十 B 圖。第一實施例的取像裝置包含影像拾取系統透鏡

組與一電子感光元件(1070),該影像拾取系統透鏡組主要由四片 具屈折力的透鏡構成,由物側至像側依序包含:

一具正屈折力的第一透鏡(1010),其材質為塑膠,其物側面 (1011)於近光軸處為凸面,其像側面(1012)於近光軸處為凹面,且 其兩面皆為非球面;

一具正屈折力的第二透鏡(1020),其材質為塑膠,其物側面 (1021)於近光軸處為凹面,其像側面(1022)於近光軸處為凸面, 且其兩面皆為非球面;

一具負屈折力的第三透鏡(1030),其材質為塑膠,其物側面 (1031)於近光軸處為凹面,其像側面(1032)於近光軸處為凸面, 且其兩面皆為非球面;及

一具正屈折力的第四透鏡(1040),其材質為塑膠,其物側面 (1041)於近光軸處為凸面,其像側面(1042)於近光軸處為凹面, 其兩面皆為非球面,且其像側面(1042)於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組另設置有一光圈(1000),置於 一被攝物與該第一透鏡(1010)間;另包含有一紅外線濾除濾光元 件(1050)置於該第四透鏡(1040)與一成像面(1060)間,其材質為玻 璃且不影響焦距。

其中,該電子感光元件(1070)設置於該成像面(1060)上。

第十實施例詳細的光學數據如表二十七所示,其非球面數據 如表二十八所示,其中曲率半徑、厚度及焦距的單位為毫米, HFOV 定義為最大視角的一半。

			表二	:++			¥	
			(第十)	實施例)		<u></u>		
		<u>f = 1.80</u>	mm, Fno = 2	.12, HFOV =	• 47.2 deg.			
表面 #		曲率半徑		厚度	材質	折射率	色散係數	焦距
0	被攝物	平面		無限		<u></u>		
1	光圈	平面		-0.060				
2	第一透鏡	1.246	ASP	0.289	塑膠	1.544	55.9	2.97
3		5.018	ASP	0.191		1		····

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. 4	第二透鏡	-3.749	ASP	0.593	塑膠	1.544	55.9	1.57
5		-0.733	ASP	0.156				•
6	第三透鏡	-0.288	ASP	0.248	塑膠	1.634	23.8	-1.33
7		-0.584	ASP	0.030				
8	第四透鏡	0.704	ASP	0.601	塑膠	1.535	55.7	2.05
9		1.382	ASP	0.500				
10	红外缐遮除	· 平面		0.210	玻璃	1.517	64.2	-
н	泡光片 🗌	平面		0.198				[
12	成像面	平面		-				[
庄: 参考	序波長為 d-line 5	87.6 nm		•			*	•
<u>a</u>	第9面有效半	徑為 1.676 mm		· · ·				
**	······································	the second s						

		表二十八		
		非球面係數		
表面 #	2	3	4	5
k =	-5.0585E-01	9.0000E+01	3.6143E+01 ·	-3.9805E-01
A4 =	8.6099E-02	-2.2970E-01	-4.8540E-01	-1.5034E-01
A6 =	-9.1382E-01	-1.8900E+00	2.7508E-01	-5.1276E-01
A8 =	1.9706E+00	1.1233E+01	-2.0152E+00	-1.5742E-01
A10 =	1.9492E+01	-3.0654E+01	-6.3534E+01	-3.0117E+00
A12 =	-3.5519E+01	-4.4967E+02	3.6120E+02	7.3424E+00
A14 =	-8.0910E+02	2.9681E+03	-1.0702E+03	-1.0241E+01
A16 =	2.4600E+03	-5.5960E+03	1.2022E+03	1.7746E+01
表面 #	6	7	8	9
k = .	-1.1070E+00	-2.9894E+00	-9.3316E-01	-5.2865E+00
A3 =			-1.4739E-01	5.0831E-01
A4 =	4.3809E+00	4.3352E-01	-3.5412E+00	2.6512E+00
A5 =			2.4672E-02	1.3099E-01
A6 =	-2.6437E+01	-3.7903E+00	1.0303E+01	-3.1255E+01
A7 =			3.7082E-02	2.0652E-01
A8 =	9.1296E+01	1.0965E+01	-3.1616E+01	1.1148E+02
A9 =			-2.2687E-03	-9.0797E-01
A10 =	-1.5853E+02	-1.4675E+01	6.3626E+01	-2.2327E+02
A11 =			-2.3794E-03	3.6058E-01
A12 =	8.3141E+00	7.7310E+00 .	-7.5604E+01	2.6201E+02
A13 =			8.0966E-03	1.7201E-01
A14 =	3.8963E+02	1.2159E+00	4.7652E+01	-1.7041E+02
A15 =			-5.5857E-02	1.0396E-01
A16 =	-3.9976E+02	-1.8447E+00	-1.2153E+01	4.7523E÷01

第十實施例非球面曲線方程式的表示如同第一實施例的形

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式。此外,各個關係式的參數係如同第一實施例所闡釋,惟各個 關係式的數值係如表二十六中所列。

	表二	二十九 二十九	
	第十	實施例	
f (mm)	1.80	f2/f3	-1.18
Fno	2.12	£/f4	0.88
HFOV [deg.]	47.2	Øf3	-1.35
V1 .	55.9	Td [mm]	2.108
CT2/(CT1+CT3+CT4)	0.52	ΣCT/Td	0.82
(R3+R4)/(R3-R4)	1.49	Td/tan(HFOV) [mm]	1.95
67f1	0.61	FOV [deg.]	94.4

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表一至表二十九所示為本發明的影像拾取系統透鏡組實 施例的不同數值變化表,然本發明各個實施例的數值變化皆屬 實驗所得,即使使用不同數值,相同結構的產品仍應屬於本發 明的保護範疇,故以上的說明所描述的及圖式僅做為例示性, 非用以限制本發明的申請專利範圍。

10 【符號說明】

光圈 100 • 200 • 300 • 400 • 500 • 600 • 700 • 800 • 900 • 1000 第一透鏡 110 . 210 . 310 . 410 . 510 . 610 . 710 . 810 . 910 . 1010 15 物側面 111、211、311、411、511、611、711、811、911、 1011 像側面 $112 \cdot 212 \cdot 312 \cdot 412 \cdot 512 \cdot 612 \cdot 712 \cdot 812 \cdot 912 \cdot$ 1012 第二透鏡 $120 \cdot 220 \cdot 320 \cdot 420 \cdot 520 \cdot 620 \cdot 720 \cdot 820 \cdot 920 \cdot .$ 20 1020 物側面 121 \ 221 \ 321 \ 421 \ 521 \ 621 \ 721 \ 821 \ 921 \

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像側面 122、222、322、422、522、622、722、822、922、 1022

第三透鏡 130、230、330、430、530、630、730、830、930、 5 1030

物側面 131、231、331、431、531、631、731、831、931、 1031

像側面 132、322、332、432、532、632、732、832、932、 1032

10 第四透鏡 140、240、340、440、540、640、740、840、940、 1040

物側面 141、241、341、441、541、641、741、841、941、 1041

像側面 142、422、342、442、542、642、742、842、942、 15 1042

紅外線濾除濾光元件 150、250、350、450、550、650、 750、850、950、1050

成像面 160、260、360、460、560、660、760、860、960、 1060

20 電子感光元件 170、270、370、470、570、670、770、870、 970、1070

取像裝置 1101
智慧型手機 1110
平板電腦 1120
可穿戴式設備 1130

影像拾取系統透鏡組的焦距為f

第一透鏡的焦距為 fl

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第二透鏡的焦距為 f2

第三透鏡的焦距為 f3

第四透鏡的焦距為 f4

第一透鏡的色散係數為 V1

- 第一透鏡物側面至第四透鏡像側面於光軸上的距離為 Td
 - 第一透鏡於光軸上的厚度為 CT1
 - 第二透鏡於光軸上的厚度為 CT2
 - 第三透鏡於光軸上的厚度為 CT3
 - 第四透鏡於光軸上的厚度為 CT4
- 10 第一透鏡、第二透鏡、第三透鏡、及第四透鏡於光軸上的厚度 的總和為ΣCT

第二透鏡物側面的曲率半徑為 R3

第二透鏡像側面的曲率半徑為 R4

影像拾取系統透鏡組的光圈值為 Fno

15 影像拾取系統透鏡組的最大視角為 FOV 影像拾取系統透鏡組中最大視角的一半為 HFOV

【生物材料寄存】

國內寄存資訊【請依寄存機構、日期、號碼順序註記】

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國外寄存資訊【請依寄存國家、機構、日期、號碼順序註記】

無

無

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申請專利範圍

1. 一種影像拾取系統透鏡組, 由物側至像側依序包含:

一具屈折力的第一透镜;

一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;

一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其 像側面於近光軸處為凸面;及

一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物 側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;

其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離 為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影 像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該第二透 鏡的焦距為 f2,該第三透鏡的焦距為 f3,係滿足下列關係式:

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0.5 mm < Td < 3.2 mm ;

- 1.0 mm < Td / tan(HFOV) < 3.75 mm;

|f / f4| < 1.20;及

 $f2 / f3 < -0.65 \circ$

2. 如申請專利範圍第 1 項所述的影像拾取系統透鏡組,其中該第
 20 四透鏡的物側面於近光軸處為凸面。

3. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的焦距為 f,該第一透鏡的焦距為 fl,係滿足下列關係式:

-0.25 < f / f1 < 0.75 •

25 4. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,其中該第 一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,係滿 足下列關係式:

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0.8 mm < Td < 2.5 mm

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5. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的光圈值為 Fno,係滿足下列關係式:

 $1.4 \leq Fno \leq 2.25$ •

 6. 如申請專利範圍第 2 項所述的影像拾取系統透鏡組,該第二透
 鏡物側面的曲率半徑為 R3,該第二透鏡像側面的曲率半徑為 R4,係滿足下列關係式:

0.5 < (R3+R4) / (R3-R4) < 2.5

 如申請專利範圍第2項所述的影像拾取系統透鏡組,其中該影 像拾取系統透鏡組的焦距為f,係滿足下列關係式:

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0.5 mm < f < 2.0 mm

- 如申請專利範圍第1項所述的影像拾取系統透鏡組,其中該第 一透鏡物側面於近光軸處為凸面。
- 9. 如申請專利範圍第 8 項所述的影像拾取系統透鏡組,其中該第 一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影
- 15 像拾取系統透鏡組中最大視角的一半為 HFOV, 係滿足下列關 係式:

 $1.2 \text{ mm} < \text{Td} / \text{tan}(\text{HFOV}) < 2.75 \text{ mm} \cdot$

- 10.如申請專利範圍第 8 項所述的影像拾取系統透鏡組,其中該第 一透鏡、該第二透鏡、該第三透鏡、及該第四透鏡於光軸上之
- 20 厚度的總合為∑CT,該第一透鏡物側面至該第四透鏡像側面於 光軸上的距離為 Td,係滿足下列關係式:

 $0.80 < \sum CT / Td < 0.95$ •

11.如申請專利範圍第8項所述的影像拾取系統透鏡組,其中該第 一透鏡的色散係數為V1,係滿足下列關係式:

25 45 < V1 •

12.如申請專利範圍第 8 項所述的影像拾取系統透鏡組,其中該第 二透鏡於光軸上的厚度為 CT2,該第一透鏡於光軸上的厚度為 CT1,該第三透鏡於光軸上的厚度為 CT3,該第四透鏡於光軸上

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的厚度為 CT4, 係滿足下列關係式:

 $0.65 < CT2 / (CT1+CT3+CT4) < 2.0 \circ$

- 13.一種取像裝置,包含如申請專利範圍第1項所述的影像拾取系 統透鏡組及一電子感光元件。
- 5 14.一種可攜裝置,包含如申請專利範圍第 13 項所述的取像裝置。 15.一種影像拾取系統透鏡組,由物側至像側依序包含:

- 一具屈折力的第一透鏡;

一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;

一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其10 像側面於近光軸處為凸面;及

一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物 側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;

其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離 15 為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影 像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該第三透 鏡的焦距為 f3,係滿足下列關係式:

0.5 mm < Td < 3.2 mm;

1.0 mm < Td / tan(HFOV) < 3.75 mm;

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|f / f4| < 1.20;及

-2.0 < f / f3 < -0.95 •

16.如申請專利範圍第15項所述的影像拾取系統透鏡組,其中該第 一透鏡的色散係數為 V1,係滿足下列關係式:

45 < V1 •

25 17.如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的焦距為 f,該第一透鏡的焦距為 fl,係滿足下列關係式:

3

-0.25 < f / f1 < 0.75 •

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18. 如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的最大視角為 FOV, 係滿足下列關係式:

80 度 < FOV < 110 度。

19.如申請專利範圍第15項所述的影像拾取系統透鏡組,其中該第 一透鏡物側面至該第四透鏡像側面於光軸上的距離為Td,係滿 足下列關係式:

0.8 mm < Td < 2.5 mm

20. 如申請專利範圍第 15 項所述的影像拾取系統透鏡組,其中該第

二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,係滿足下列關係10 式:

f2 / f3 < -0.75 •

21.一種影像拾取系統透鏡組,由物側至像側依序包含:

一具屈折力的第一透鏡:

一具正屈折力的第二透鏡,其像側面於近光軸處為凸面;

一具負屈折力的第三透鏡,其物側面於近光軸處為凹面,其 像側面於近光軸處為凸面;及

一具屈折力的第四透鏡,其像側面於近光軸處為凹面,其物 側面及像側面皆為非球面,且其像側面於離軸處具有至少一凸面;

其中,該影像拾取系統透鏡組中具有屈折力的透鏡為四片;

其中,該第一透鏡物側面至該第四透鏡像側面於光軸上的距離為 Td,該影像拾取系統透鏡組中最大視角的一半為 HFOV,該影像拾取系統透鏡組的焦距為 f,該第四透鏡的焦距為 f4,該影像拾取系統透鏡組的光圈值為 Fno,係滿足下列關係式:

0.5 mm < Td < 3.2 mm;

25

20

15

5

1.0 mm < Td / tan(HFOV) < 3.75 mm;

|f / f4| < 1.20;及

 $1.40 < Fno \leq 2.25$ •

22.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第

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二透鏡的焦距為 f2,該第三透鏡的焦距為 f3,係滿足下列關係 式:

f2 / f3 < -0.65 •

23.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第 一透鏡的色散係數為 V1,係滿足下列關係式:

45 < V1 •

5

10

24.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第 一透鏡具正屈折力,該影像拾取系統透鏡組的焦距為 f,該第一 透鏡的焦距為 f1,係滿足下列關係式:

0.25 < f / f1 < 0.75 •

25.如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該影像拾取系統透鏡組的最大視角為 FOV,係滿足下列關係式:

80度 < FOV < 110度。

26. 如申請專利範圍第 21 項所述的影像拾取系統透鏡組,其中該第

5

15 二透鏡於光軸上的厚度為 CT2,該第一透鏡於光軸上的厚度為 CT1,該第三透鏡於光軸上的厚度為 CT3,該第四透鏡於光軸上 的厚度為 CT4,係滿足下列關係式:

0.65 < CT2 / (CT1+CT3+CT4) < 2.0 •

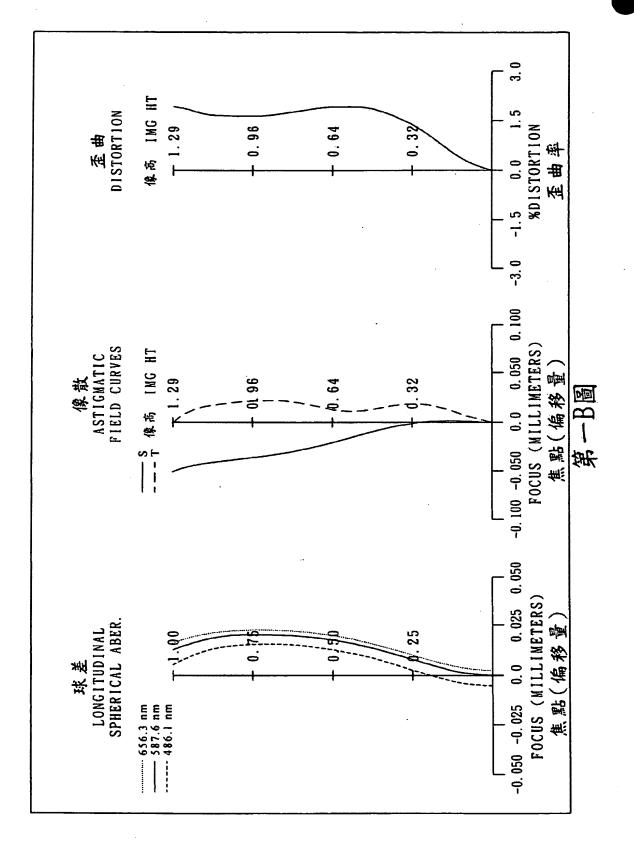
申請案號:102139029

AOET, Ex. 1002 Page 143 (.) S

圖式 170 160-150-140 第一A圖 130-33 120-121-100 110

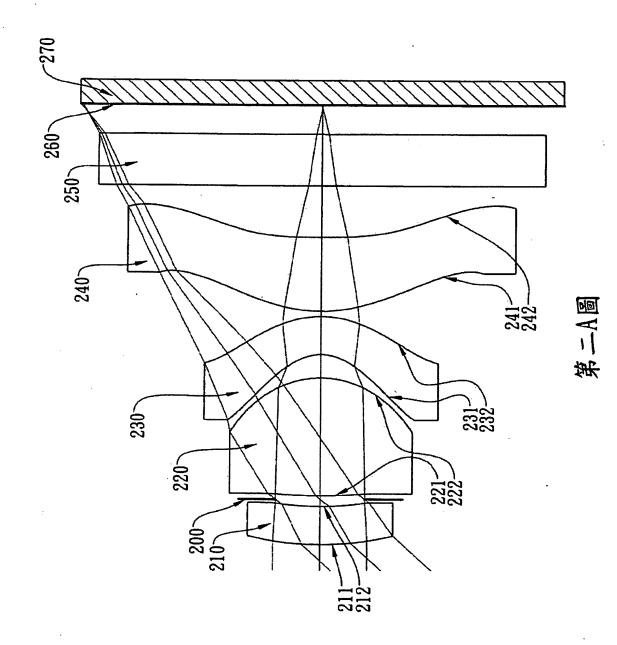
申請案號:102139029

AOET, Ex. 1002 Page 144



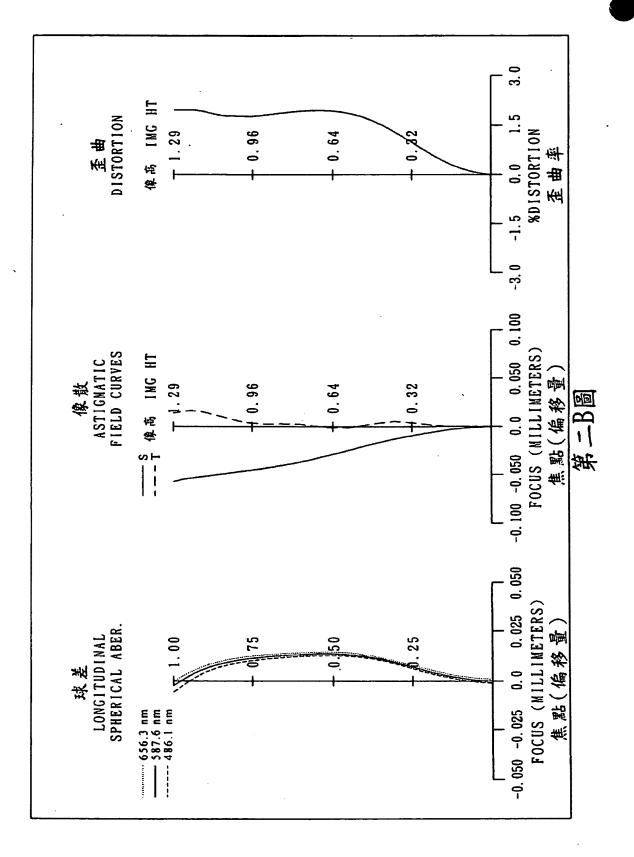
申請案號:102139029

AOET, Ex. 1002 Page 145 :-:-



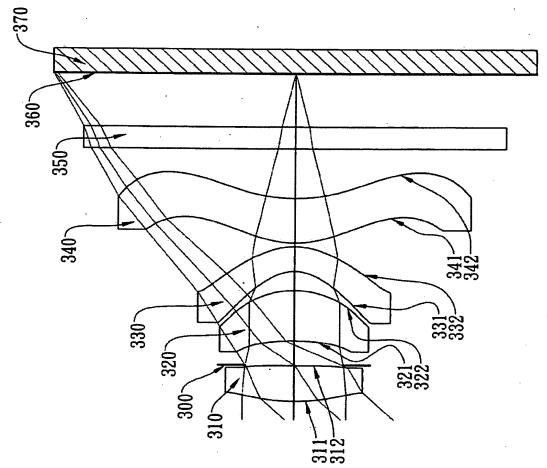
AOET, Ex. 1002 Page 146

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申請案號: 102139029

AOET, Ex. 1002 Page 147

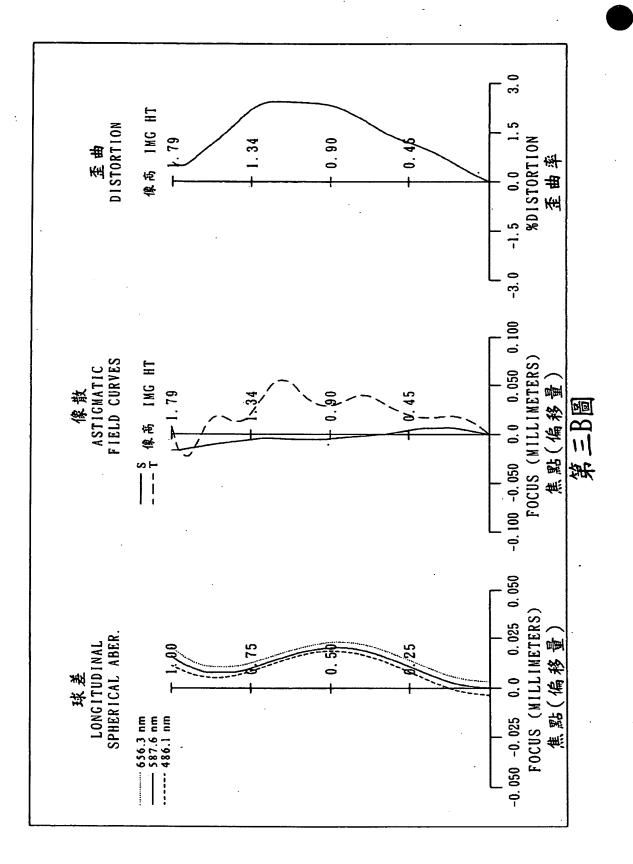


第三A圖

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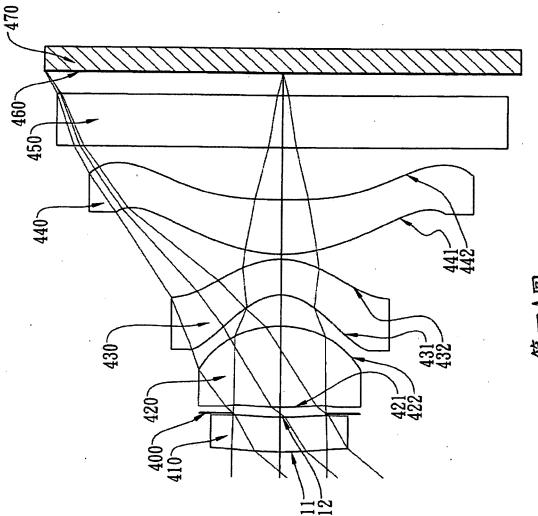
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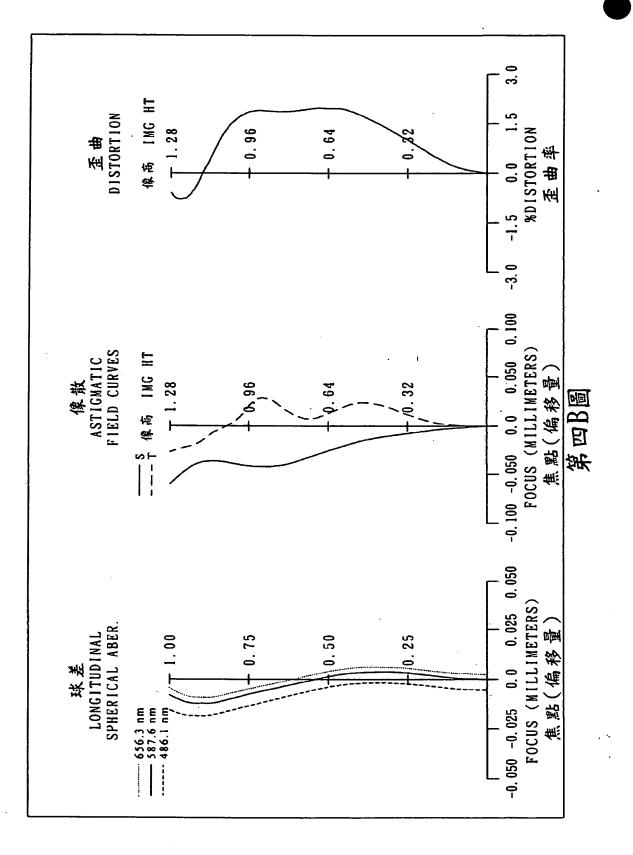


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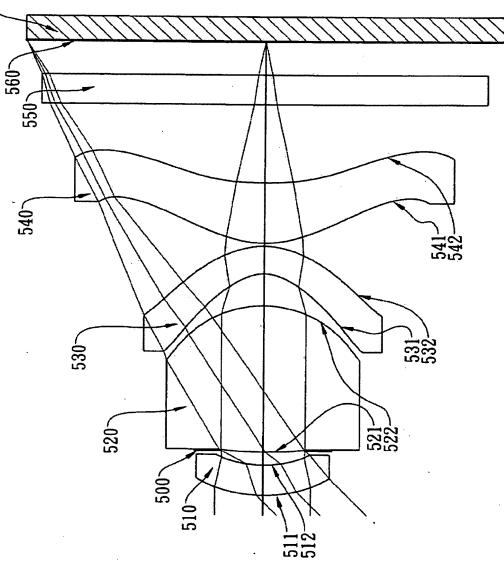


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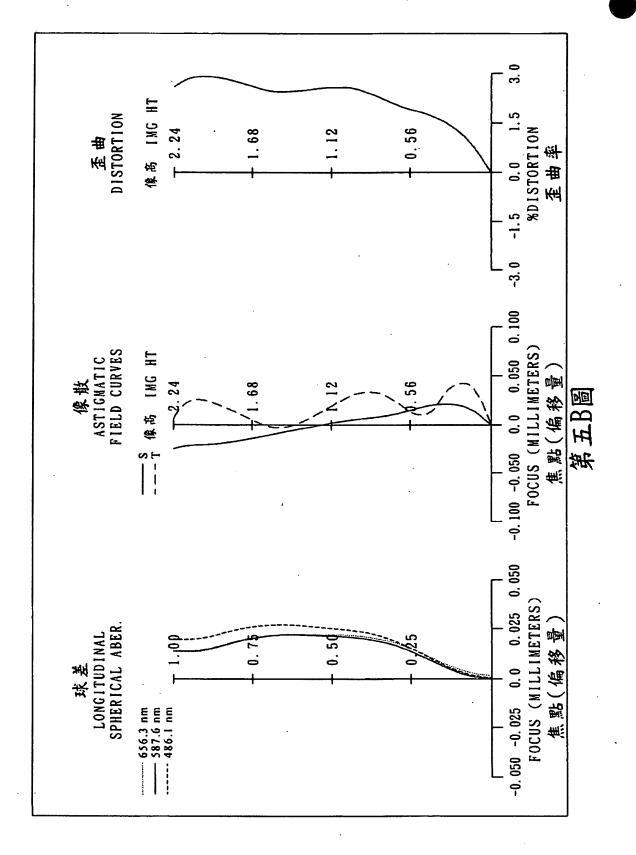




第五A圖

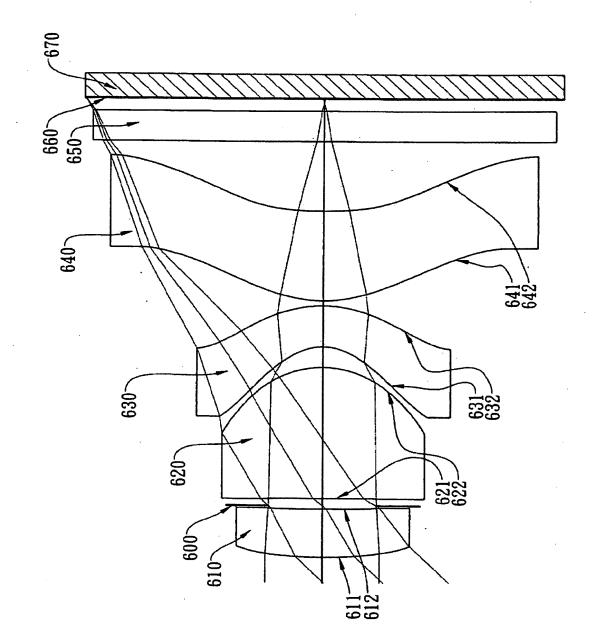
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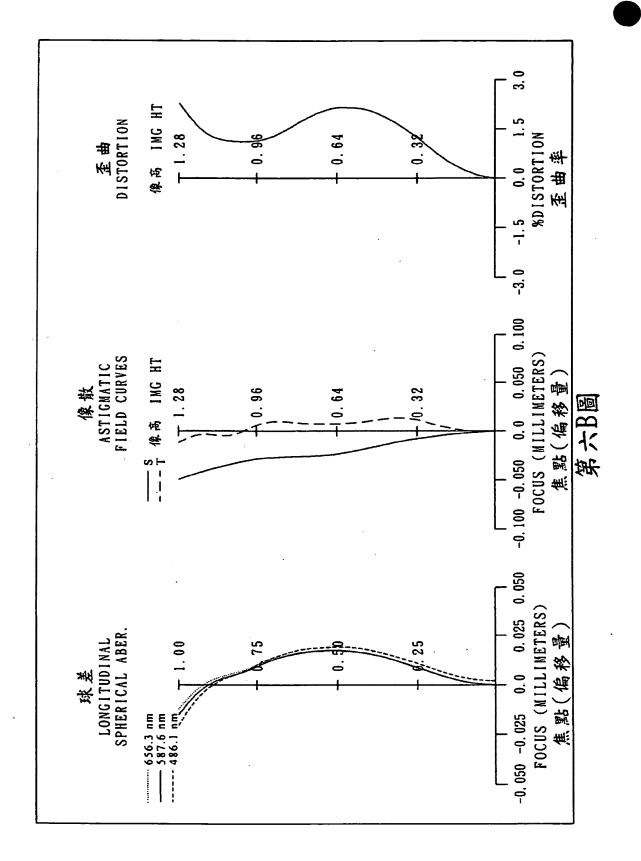
第六A圖

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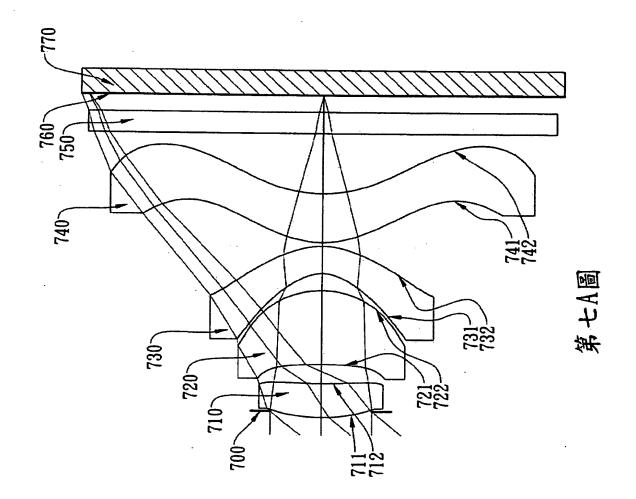
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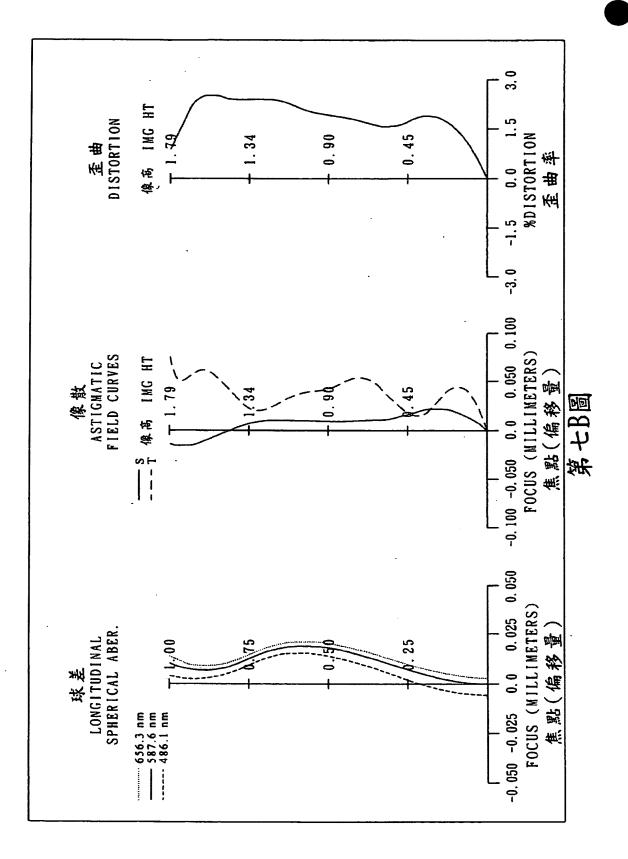
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申請案號:102139029

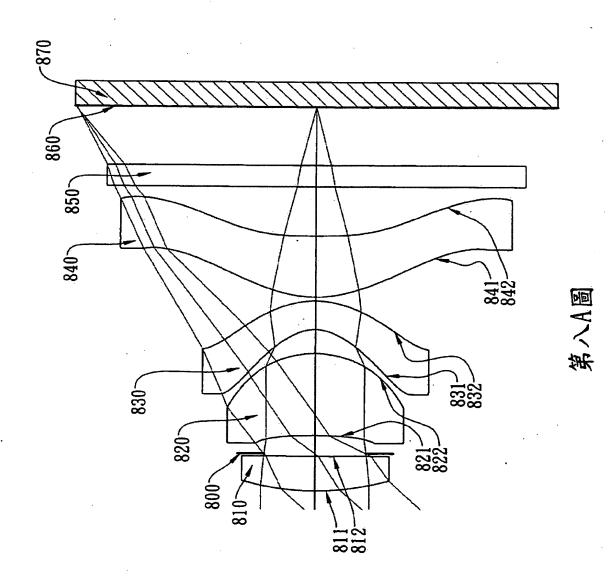
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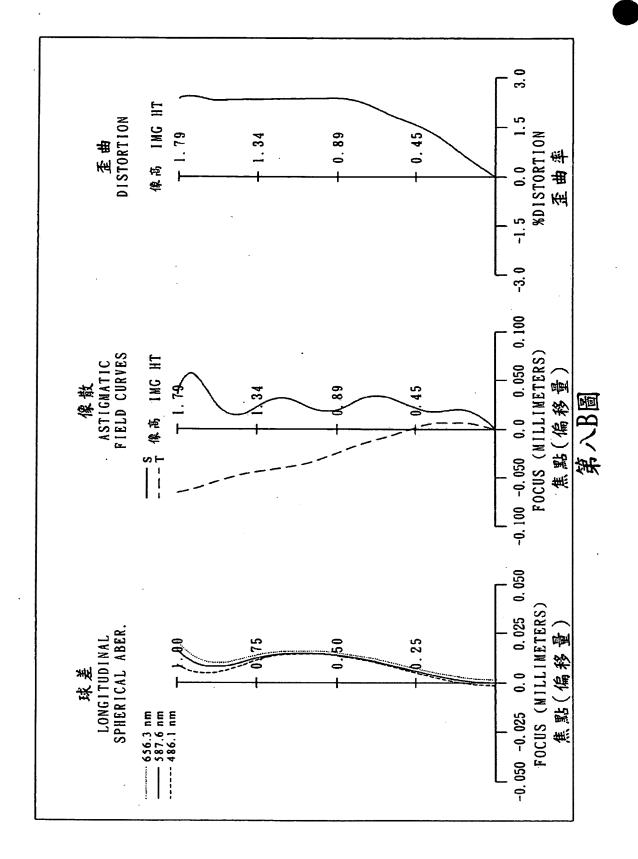


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AOET, Ex. 1002 Page 159 8. N 6

-970 -096 950 940 941 942 930~ 931-932-920 921-922--006 910 911⁻ 912⁻

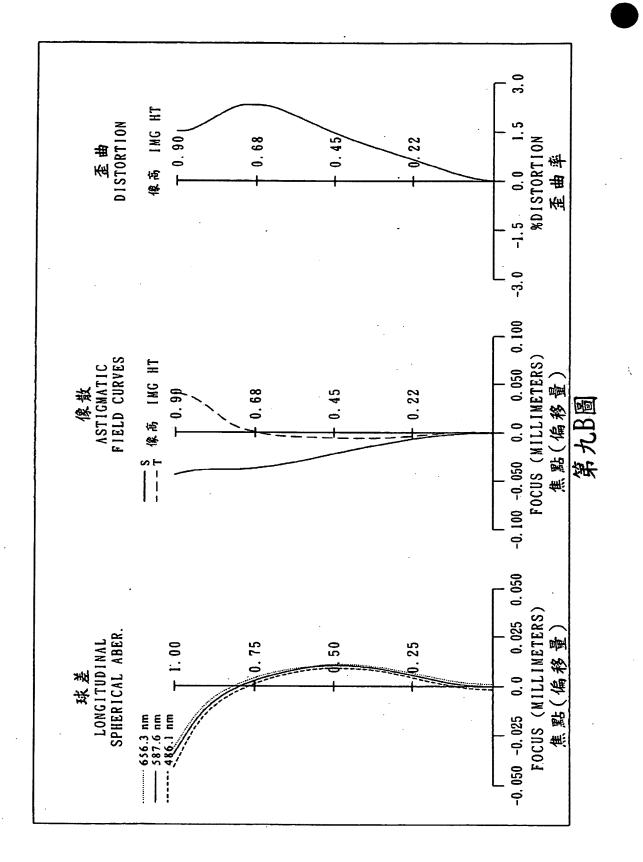
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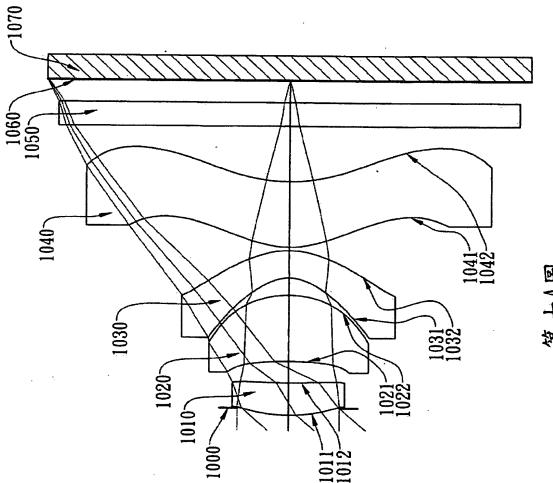
第九A圖

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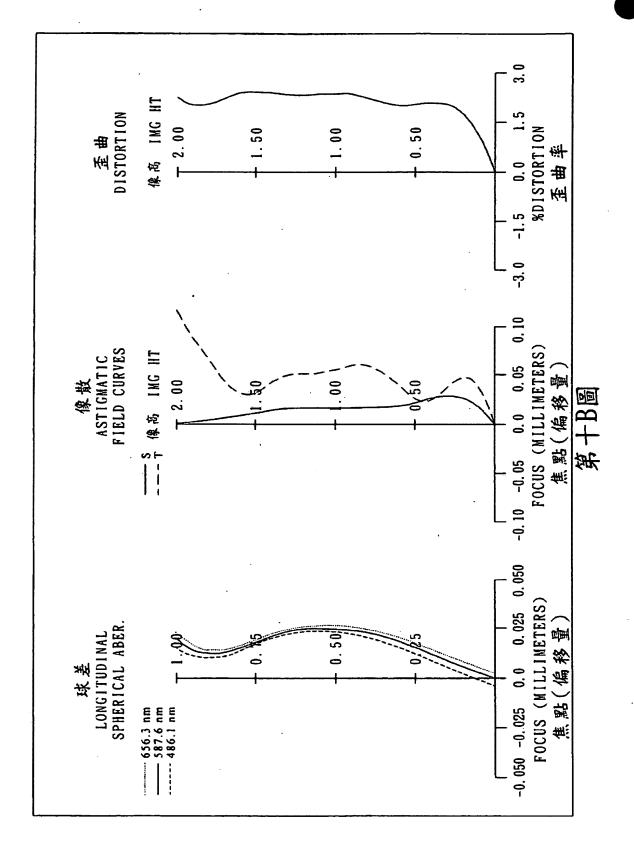


第十A圖

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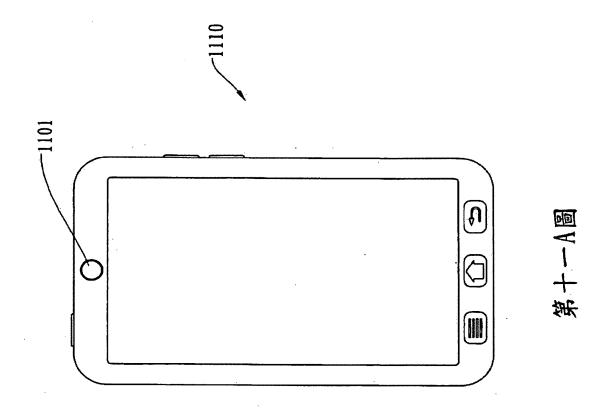
AOET, Ex. 1002 Page 162

申請案號:102139029

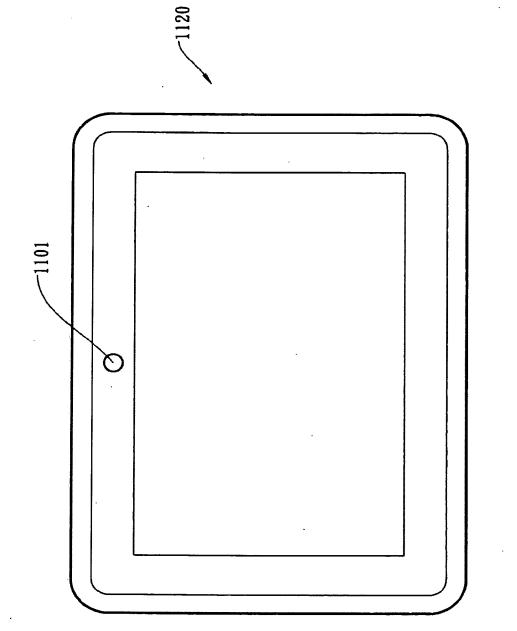


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AOET, Ex. 1002 Page 164

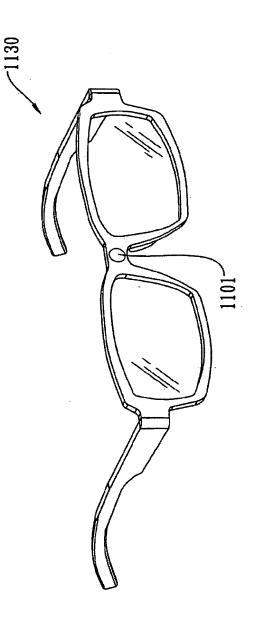


第十一B圖

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申請案號:102139029

AOET, Ex. 1002 Page 166 S

23/23

	S/N: 14/105	,811		PATENT
0	PAP		Cont	firmation No. 5836
		IN THE UNITED STATES PATE	NT AND TRADEMARK O	FFICE
STEW & T	RADE MANDENCANT:	Wei-Yu Chen	Examiner:	Unassigned
	Serial No.:	14/105,811	Group Art Unit:	Unassigned
	Filed:	December 13, 2013	Docket No.:	14970-94702
	Title:	IMAGE CAPTURING LENS SYS TERMINAL	TEM, IMAGING DEVICE A	AND MOBILE
•				

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Certified Copy of Priority Document Taiwan Patent Application 102139029, filed October 29, 2013 (66 pages)

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MORRIS, MANNING & MARTIN, LLP 1600 Atlanta Financial Center 3343 Peachtree Road NE Atlanta, Georgia 30326 404.495.3678 Customer No. 24728

By: Xia

Name: Tim Tingkang Xia Reg. No.: 45,242 TTX

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MORRIS, MANNING & MARTIN, L.L.P. 1600 Atlanta Financial Center 3343 Peachtree Road, N.E. Atlanta, Georgia 30326 404-495-3678 Direct Customer No. 24728

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January 6, 2014

claims priority is hereby submitted as the priority document.

If there are any questions regarding this matter, please call the undersigned at 404-495-3678.

The certified copy of Taiwan Patent Application No. 102139029, from which this application

Respectfully submitted,

MORRIS, MANNING & MARTIN, LLP

Tim Tingkang Xia Reg. No. 45,242 Attorney for the Assignee and Applicants on Record

January 6, 2014

CUSTOMER NO. 24728

Applicant: Serial No.:	Wei-Yu Chen	Examiner:	Unassigned
Serial No.:	14/105,811	Group Art Unit:	Unassigned
Filed:	December 13, 2013	Docket No.:	14970-94702
Title:	IMAGE CAPTURING LENS SYSTEM, IM TERMIAL	AGING DEVICE AND	MOBILE

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SUBMISSION OF PRIORITY DOCUMENT

Name: Tim Tingkang Xia

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S/N: 14/105,811

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APPLICATION NUMBER	PATENT NUMBER	GROUP ART UNIT	FILE WRAPPER LOCATION
14/105,811		2872	

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Application Number		14105811
Filing Date		2013-12-13
First Named Inventor	WEI-Y	/U CHEN
Art Unit		2872
Examiner Name		
Attorney Docket Number		14970-94702

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Examiner Initial*	Cite No	Patent Number	Kind Code ¹	Issue Dat	te	Name of Patentee or Applicant of cited Document		Pages,Columns,Lines where Relevant Passages or Releva Figures Appear		
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	Application Number		14105811	
	Filing Date		2013-12-13	
INFORMATION DISCLOSURE	First Named Inventor WEI-1		YU CHEN	
(Not for submission under 37 CFR 1.99)	Art Unit		2872	
	Examiner Name			
	Attorney Docket Numb	er	14970-94702	

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Standard S ⁻ ⁴ Kind of do	T.3). ³ F cument	[:] or Japa by the a	O Patent Documents at <u>www.USPTO.GOV</u> or MPEP 901.04. ² Enter office that issued the documer anese patent documents, the indication of the year of the reign of the Emperor must precede the seri appropriate symbols as indicated on the document under WIPO Standard ST.16 if possible. ⁵ Applic n is attached.	ial number of the patent doc	ument.

	Application Number	14105811	
	Filing Date	2013-12-13	
INFORMATION DISCLOSURE	First Named Inventor W	YU CHEN	
STATEMENT BY APPLICANT (Not for submission under 37 CFR 1.99)	Art Unit	2872	
	Examiner Name		
	Attorney Docket Number	14970-94702	

CERTIFICATION STATEMENT

Please see 37 CFR 1.97 and 1.98 to make the appropriate selection(s):

That each item of information contained in the information disclosure statement was first cited in any communication from a foreign patent office in a counterpart foreign application not more than three months prior to the filing of the information disclosure statement. See 37 CFR 1.97(e)(1).

OR

That no item of information contained in the information disclosure statement was cited in a communication from a foreign patent office in a counterpart foreign application, and, to the knowledge of the person signing the certification after making reasonable inquiry, no item of information contained in the information disclosure statement was known to any individual designated in 37 CFR 1.56(c) more than three months prior to the filing of the information disclosure statement. See 37 CFR 1.97(e)(2).

See attached certification statement.

The fee set forth in 37 CFR 1.17 (p) has been submitted herewith.

X A certification statement is not submitted herewith.

SIGNATURE

A signature of the applicant or representative is required in accordance with CFR 1.33, 10.18. Please see CFR 1.4(d) for the form of the signature.

Signature	/Tim Tingkang Xia/	Date (YYYY-MM-DD)	2014-12-01
Name/Print	Tim Tingkang Xia	Registration Number	45242

This collection of information is required by 37 CFR 1.97 and 1.98. The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 1 hour to complete, including gathering, preparing and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. **SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450**.

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- 7. A record from this system of records may be disclosed, as a routine use, to the Administrator, General Services, or his/her designee, during an inspection of records conducted by GSA as part of that agency's responsibility to recommend improvements in records management practices and programs, under authority of 44 U.S.C. 2904 and 2906. Such disclosure shall be made in accordance with the GSA regulations governing inspection of records for this purpose, and any other relevant (i.e., GSA or Commerce) directive. Such disclosure shall not be used to make determinations about individuals.
- 8. A record from this system of records may be disclosed, as a routine use, to the public after either publication of the application pursuant to 35 U.S.C. 122(b) or issuance of a patent pursuant to 35 U.S.C. 151. Further, a record may be disclosed, subject to the limitations of 37 CFR 1.14, as a routine use, to the public if the record was filed in an application which became abandoned or in which the proceedings were terminated and which application is referenced by either a published application, an application open to public inspections or an issued patent.
- 9. A record from this system of records may be disclosed, as a routine use, to a Federal, State, or local law enforcement agency, if the USPTO becomes aware of a violation or potential violation of law or regulation.

English Translation of Abstract of JP2014-178623

This invention provides a wide-angle lens system 10 from an object-side to an image-side in order including a first lens element 11 with negative refractive power, a second lens element 12 with positive refractive power, a third lens element 13 with negative refractive power and a fourth lens element 14 with positive refractive power. The first lens element 11 has negative refractive power and a concave surface and the second lens element 12 has positive refractive power and convex surfaces such that a total track length of the lens system with more than 65-degree view of angle is controlled within about 5mm. An image surface 14b of the fourth lens element 14 is provided with inflection points so as to control a direction of the light coming from the wide-angle lens system 10.

(11)特許出願公與番号

0.2公開特許公報(A)

(19)日本国特許厅(JP)

特開2014-178623 (P2014-178623A)

(43) 公開日 平成28年9月25日(2014.9.25)

(\$1) Int.Cl.		F L		チーマコード(参考)
GO28 13/00	(2006.01)	GO2B	13/00	2H087
GO28 13/18	(2008.01)	GO2B	13/18	

審査譜本 未譜家 歸求項の数 7 OL (全 3) 頁)

(21) 出题普号 (22) 出题日	特顏2013-53900 (P2013-53990) 平成25年3月15日 (2013. 3. 15)	(71)出颜人	000005810 日立マクセル株式会社 大阪府茨木市丑賞一丁目1番88号
		(74)代理人	100090170 弁理士 演訳 憲郎
		70代理人	99-38 1. 09195 weep 100142619
		0.0.0000	弁理士 河合 徽
		(74)代理人	100163316
			<u> 奔曜士</u> (河口)伸子
		(72)発明者	杉山一餐
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			マクセル株式会社内
		(72)発明者	上海縣 隆
			大阪府茨木市丑寅一丁目1番88号 日立
			マクセル体式会社内
			最終質に続く

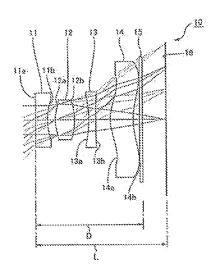
(64) (発明の名称) 広角レンズおよび摄像装置

(57)【要約】

【課題】レンズ系の全長を短く抑え、結像面に対する主 光線入射角度を小さく抑制できる広角レンズを提供する こと。

【解決手段】広角レンズ10は、物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ1 1、正のパワーを有する第2レンズ12、負のパワーを 有する第3レンズ13、および正のパワーを有する第4 レンズ14からなる。第1レンズ11に凹形状を備える 負のパワーのレンズを配置し、第2レンズ12に凸形状 を備える正のパワーを有するレンズを配置したので、6 5°以上の頭角を備えるレンズ系の全長を5mm程度に 抑えることができる。第4レンズ14の像劇レンズ面1 4bは、変曲点を有しているので、広角レンズ10から の射出光線の方向を制御できる。

【選択図】図1



【特許請求の範囲】

【請求項1】

物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ、正のパワ ーを有する第2レンズ、負のパワーを有する第3レンズおよび正のパワーを有する第4レ ンズからなり、

前記第1レンズの像側レンズ面は、凹形状を備え、

前記第2レンズの物体側レンズ面は、凸形状を備え、

前記第4レンズの像側レンズ面は、変曲点を備える非球菌であり、光軸を含む中央部分 が凹形状をしており、

前記館4レンズの像棚レンズ面を含む少なくとも2つのレンズ面が非球面とされている ¹⁰ ことを特徴とする広角レンズ。

【需求項2】

請意項主において、

レンズ系全体の焦点距離を「、前記第2レンズの焦点距離を「2としたときに、以下の 条件式(1)を満たすことを特徴とする広角レンズ。

 $0.4 \leq 12/1 \leq 0.7 + (1)$

【請求項3】

請求項1または2において、

前記第3レンズの焦点距離を13としたときに、以下の条件式(2)を満たすことを特徴とする広角レンズ。
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 $-1 \leq f 2/f 3 \leq -0.25 \cdot (2)$

【諸求項4】

請求項1ないし3のうちのいずれかの項において、

 $1, 0 \leq 0 / t \leq 2, 0 - (3)$

【請求項5】

諸求項1ないしょのうちのいずれかの項において、

前記第1レンズの無点距離をf1としたときに、以下の条件式(4)を満たすことを特 ³⁰ 微とする広角レンズ。

 $-3.0 \leq f_1/f_1 \leq -0.5 + (4)$

【請求項6】

請求項1ないし5のうちのいずれかの項において、

画角が65°以上であることを特徴とする広角レンズ。

【請求項7】

請求項1ないし6のうちのいずれかの項に記載の広角レンズと、

前記広角レンズの焦点位留に配置された撮像素子と、を有することを特徴とする撮像装 ***

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(発明の詳細な説明)

【技術分野】

[0001]

本発明は、4枚のレンズからなる小型の広角レンズおよび当該広角レンズを搭載する撮 像装置に関する。

【背景技術】

(0002]

携帯電話などの情報端末や小型のデジタルカメラに搭載される撮像レンズは特許文献1 に記載されている。開文献の撮影レンズは物体側から像側に向かって順に配置された、正 のパワーを備える第1レンズ、負のパワーを備える第2レンズ、正のパワーを備える第3 レンズ、像側が凸のメニスカス形状の第4レンズ、および、像側レンズ面が変曲点を備え

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(3)

る非球面形状とされた第5レンズを備えている。両文献の撮像レンズの最大画角は60° である。 【先行技術文献】 【特許文献】 【特許文献1】特開2009-14947号公報 【発明の概要】 【発明の概要】 【発明が解決しようとする課題】 【0004】

宿報端末や小型のデジタルカメラなどの機器に搭載される撮像レンズにおいては、使い ¹⁰ 勝手を考慮して画角を広くする場合がある。すなわち、これらの小型の機器においては、 標準画角の撮像レンズを、60°以上の画角の広角レンズに置き換えることが要求される 場合がある。

[0005]

ここで、標準レンズを広角レンズに置き換えるためには、広角レンズのレンズ系の全長 (第1レンズの物体側レンズ面の物体側の端から結像固までの距離)を短く抑え、広角レ ンズを標準レンズの配置スペースに設置可能としなければならない。また、これらの機器 において、操像レンズの焦点位置に配置される撮像業子には、そのセンサ面に斜めから入 射する光に対して感度が低下する特性を有するものがあるので、センサ面(撮像レンズの 結像面)に対する主光線入射角度を小さく抑制して、画質の劣化を抑制しなければならな い。

[0006]

さらに、情報端末や小型のデジタルカメラなどの機器に搭載される撮像レンズには、軽 量化や製造コストの抑制が求められている。かかる要求に対応するためには、撮像レンズ を構成しているレンズの複数を減少させることが黛ましい。

[0007]

このような点に鑑みて、本発明の課題は、レンズ系の全長を短く抑え、結像面に対する 主光線入射角度を小さく抑制できる4枚のレンズから構成された広角レンズを提供することにある。また、このような広角レンズを搭載する撮像装置を提供することにある。 【課題を解決するための手段】

[0008]

上記課題を解決するために、本発明の広角レンズは、

物体機から像側に向かって順に配置された、負のパワーを有する第1レンズ、正のパワ ーを有する第2レンズ、負のパワーを有する第3レンズおよび正のパワーを有する第4レ ンズからなり。

前記第1レンズの像側レンズ面は、凹形状を備え、

前記第2レンズの物体側レンズ面は、凸形状を備え、

前記第4レンズの像棚レンズ面は、変曲点を備える非球面であり、光軸を含む中央部分 が凹形状をしており、

前記第4レンズの像側レンズ面を含む少なくとも2つのレンズ面が非球面とされている⁴⁰ ことを特徴とする。

[0009]

本発明によれば、第1レンズに凹形状を備える負のパワーのレンズを配置し、第2レン ズに凸形状を備える正のパワーを有するレンズを配置したので、レンズ系の全長を抑えた 広角レンズを構成できる。また、第4レンズの像側レンズ面を、変曲点を備える非球面と したので、広角レンズからの射出光線の方向を制御することが容易となり、結像面に入射 する主光線入射角度を小さく抑制することができる。さらに、第4レンズの像側レンズ面 を含む少なくとも2つのレンズ面が非球面とされているので、広角レンズを明るく構成す ることが容易である。これに加えて、4枚のレンズから広角レンズを構成したので、5枚 以上のレンズを備える摄像レンズと比較して、軽量化や製造コストの抑制を図ることが容

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易である。なお、広角レンズとは、一般的に、画角が60°以上の撮像レンズをいう。主 光線入射角度とは、結像面へ入射する光線と光軸が交差する角度である。

[0010]

本発明において、レンズ系全体の焦点距離を1、前記第2レンズの焦点距離を12とし たときに、以下の条件式(1)を満たすことが認ましい。

 $0.4 \leq f 2 / f \leq 0.7 + (1)$

[0011]

条件式(1)はレンズ系の全長の抑制を容易にするものであり、条件式(1)の上環値 を上回ると、レンズ系の全長の増大を招く。条件式(1)の下限値を下回ると、バックフ オーカスを確保することが困難となる。

[0012]

本発明において、前記第3レンズの焦点距離を13としたときに、以下の条件式(2) を満たすことが望ましい。

 $-1 \leq f_2 / f_3 \leq -0, 25 \cdots (2)$

[0013]

条件式(2)は軸上の色収差を抑制するものである。すなわち、軸上の色収差は隣接配 置した正のパワーを有する第2レンズ12、負のパワーを有する第3レンズ13によって 抑制することが可能であるが、第2レンズのパワーと第3レンズのパワーのパランスによ って、条件式(2)の上限値を上回ると色収差の補正が不足となり、条件式(2)の下限 値を下回ると色収差に過剰補正が生じる。

(0014)

本発明において、前記第1レンズの物体側レンズ面の物体側の端から第4レンズの像側 レンズ面の像側の端までの距離(レンズ系のレンズ厚)をDとしたときに、以下の条件式 (3)を満たすことが望ましい。

 $1.0 \leq D/I \leq 2.0 + (3)$

[0015]

条件式(3)はパックフォーカスを確保しながらレンズ系の全長を抑制することを容易 にするものである。条件式(3)の上限値を上回るとパックフォーカスを確保することが 困難となる。条件式(3)の下跟値を下回ると、各レンズの間の距離が短くなり、各レン ズの配置に無理が生じやすい。すなわち、各レンズの中心厚やコパ厚によって、各レンズ の配置が困難となる場合が発生する。

[0016]

本発明において、前記第1レンズの焦点距離をf1としたときに、以下の条件式(4) を満たすことが望ましい。

 $-30 \leq f 1/f \leq -0.5 \cdot \cdot (4)$

[0017]

条件式(4)は画角の確保を容易にするものである。条件式(4)の上開催を上囲ると 第1レンズのパワーがレンズ系の中で大きくなりすぎて、金長の増大を招く。また、第1 レンズのパワーがレンズ系の中で大きくなりすぎて、像面湾曲の補正が困難となる。条件 式(2)の下限値を下回ると、第1レンズのパワーの低下により画角の確保が難しくなる

[0018]

本発明において、画角は65°以上とすることができる。すなわち、標準レンズよりも 広い画角を備えるものとすることができる。

[0019]

次に、本発明の撮像装置は、上記の広角レンズと、前記広角レンズの焦点位置に配置された撮像業子とを有することを特徴とする。

[0050]

本発明によれば、広角レンズのレンズ系の全長が短く抑えられている。従って、爆爆装 置を小さく構成できる。また、広角レンズが明るく、結像面に対する主光線入射角度が小 50

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さく抑制されている。従って、撮像レンズの焦点位器に配置される撮像業子がそのセンサ 語に斜めから入射する光に対して感度が低下する特性を有するものであっても、画質の劣 化を抑制することができる。さらに、4枚のレンズから広角レンズを構成したので、5枚 以上のレンズを備える撮像レンズを搭載する場合と比較して、撮像装置の軽量化や製造コ ストの抑制を図ることが容易である。

【発明の効果】

[0021]

本発明によれば、レンズ系の全長を短く抑え、結像面に対する主光線入射角度を小さく 抑制した明るい広角レンズを4枚のレンズから構成できる。

【図面の簡単な説明】

[0022]

【図1】本発明を適用した実施例1の広角レンズの構成図である。

【図2】図1の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【図3】本発明を適用した実施例2の広角レンズの構成図である。

【図4】図3の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【図5】本発明を適用した実施例3の広角レンズの構成図である。

【図6】図5の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【図7】本発明を適用した実施例4の広角レンズの構成図である。

【図8】図7の広角レンズの縦収差図、横収差図、像面湾曲図、重曲収差図である。

【図9】本発明を適用した実施例5の広角レンズの構成図である。

【図10】図9の広角レンズの縦収差図、横収差図、像面湾曲図、歪曲収差図である。

【図11】広角レンズを搭載する撮像装置の説明図である。

【発明を実施するための形態】

[0023]

以下に図面を参照して、本発明を適用した広角レンズを説明する。

[0024]

(実施例1)

図1は実施例1の広角レンズの光線図である。図1に示すように、広角レンズ10は、 物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ11、正のパ ワーを有する第2レンズ12、負のパワーを有する第3レンズ13、および正のパワーを 有する第4レンズ14からなる。第1レンズ11と第2レンズ12の間には絞り(不闘示)が配置されている。第4レンズ14の像側にはカパーガラス15が配置されている。結 像面16はカパーガラス15と関係を開けた位置にある。

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第1レンズ11は、物体側レンズ面11aおよび像側レンズ面11bのそれぞれが非球面とされている。物体側レンズ面11aは凸形状を備えており、像側レンズ面11bは凹形状を備えている。物体側レンズ面11aは、凸形状をしているレンズ面部分の曲率半径が大きく、平面形状に近い。

[0026]

第2レンズ12は、物体側レンズ面12aおよび像側レンズ面12bのそれぞれが非球 40 面とされている。物体側レンズ面12aおよび像側レンズ面12bは、それぞれ凸形状を 備えている。

[0027]

第3レンズ13は、物体側レンズ面13aおよび像側レンズ面13bのそれぞれが非球 面とされている。物体側レンズ面13aおよび像側レンズ面13bは、それぞれ凹形状を 備えている。

[0028]

第4レンズ14は、物体側レンズ面14aおよび像側レンズ面14bのそれぞれが非球 面とされている。物体側レンズ面14aは光軸を含む中央部分に凸形状を備えている。像 側レンズ面14bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。

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従って、像側レンズ面14bは変曲点から内環側に向かって物体側に湾曲しており、変曲

広角レンズ10の開口数をFno、、半面角をω、および、レンズ系の全長(第1レン

点から外周側に向かって物体側に湾曲している。

[0029]

ズ11の物体側レンズ面11cの物体側の端から結像面16までの距離)をし、レンズ系 のレンズ潭(第1レンズ11の物体側レンズ面118の物体側の端から第4レンズ14の 像棚レンズ菌14bの像棚の端までの距離)をDとすると、これらの値は以下のとおりで ある。 Fno. = 2. 8 w≈85.8° L = 4.281 mm D = 3.212 mm[0030] また、金レンズ系の焦点距離をす、第1レンズ11の焦点距離を「1、第2レンズ12 の焦点距離を12、第3レンズ13の焦点距離を13、第4レンズ14の焦点距離を14 とすると、これらの値は以下のとおりである。 f=2.564 $f_1 = -3.390$ f2=1.490 f3 =-- 3. 241 $f_4 = 4$, 561 [0031]ここで、本例の広角レンズ10は、以下の条件式(1)~(4)を満たす。 $0.4 \leq f2/f \leq 0.7 \cdot (1)$ $-1 \leq f 2 / f 3 = \leq -0.25 \cdot \cdot (2)$ $1. 0 \leq D/f \leq 2. 0 \cdots (3)$ $-30 \leq f_1/f_5 = -0.5 \cdot \cdot (4)$ [0032] すなわち、f2/f=0、581であり、f2/f3=−0,460であり、D/f= 1.253であり、11/1=-1.322である。 [0033] 広角レンズ10は条件式(1)を満たすので、レンズ系の全曼を抑制し、パックフォー カスを確保することが容易である。すなわち、条件式(1)の上限値を上回ると、全長の 増大を招く。条件式(1)の下環値を下回ると、バックフォーカスを確保することが困難 となる。 [0034]広角レンズ10は条件式(2)を満たすので、軸上の色収差が抑制される。すなわち、 軸上の色収差は隣接配置した正のパワーを有する第2レンズ12、負のパワーを有する第 3 レンズ13によって抑制することが可能となっているが、第2 レンズ12のパワーと第 3レンズ13のパワーのバランスによって、条件式(2)の上環値を上囲ると色収差の補 正が不足となり、条件式(2)の下限値を下回ると色収差に過剰補正が生じる。 [0035] 広角レンズ10は条件式(3)を満たすので、パックフォーカスを確保しながらレンズ 系の全長を抑制することが容易である。すなわち、条件式(3)の上限値を上回るとパッ クフォーカスを確保することが困難となる。条件式(3)の下環値を下回ると、各レンズ の間の距離が短くなるので、各レンズの中心厚やコパ厚によって、各レンズの配置が困難 となる場合が発生する。 [0036] 広角レンズ10は条件式(4)を満たすので、画角の確保が容易である。すなわち、条

件式(4)の上限値を上回ると第1レンズ11のパワーがレンズ系の中で大きくなりすぎ 50

AOET, Ex. 1002 Page 180 て、レンズ系の全長の増大を招く。また、条件式(4)の上限値を上回ると第1レンズ1 1のパワーがレンズ系の中で大きくなりすぎて、像面湾曲の補正が困難となる。一方、条 件式(2)の下限値を下回ると、第1レンズ11のパワーの低下により画角の確保が難し くなる。

[0037]

また、広角レンズ10は、以下の条件式(5)、(6)を満たす。

 $-1.4 \leq 13/1 \leq -0.6 \cdot \cdot (5)$

 $1. 3 \leq L/I \leq 2. 5 \cdot \cdot (6)$

[0038]

すなわち、f3/f=−1、264であり、L/f=1.679である。 【0039】

広角レンズ10は条件式(5)を満たすので、色収差を良好に補正できる。すなわち、 条件式(5)の上環値を上回ると色収差の補正が過剰となり、下限値を下回ると色収差の 補正に不足が生じる。

[0040]

さらに、広角レンズ10は条件式(6)を満たすので、パックフォーカスを確保しなが らレンズ系の全長を抑制することがより容易となる。すなわち、条件式(6)の上環線を 上回るとパックフォーカスを確保することが困難となる。条件式(6)の下環線を下回る と、各レンズの間の距離が短くなるので、各レンズの中心厚やコバ厚によって、各レンズ の配置が困難となる場合が発生する。

[0041]

以下の表1Aは広角レンズ10の各レンズ面のレンズデータを示す。表1Aでは物体側 から数えた機器で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非 球面である。なお、9面および10面はカバーガラス15のガラス面であり、11面は結 像面16である。曲率半径および開陽の単位はミリメートルである。

[0042]

【轰1A】

面番	曲率半径	RIG.	Nd(屈振率)	Vd(アッベ数)	材料
1	18.988	0.400	1,53116	56.0	樹脂
2	1.639	0.259			
3	1.306	0.627	1.53116	58.0	樹脂
4	~1.693	0.477			
5	-2,153	0.228	1.83494	24.0	樹脂
6	61.884	0.479			
7	1.220	0,744	1.53118	56.0	
8	1.929	0.210			
9	infinity	0.100	1.51680	64.2	光学ガラス
10	infinity	0.781			Į
11	infinity	-0.022			1

[0043]

次に、表1B、表1Cは非球面とされたレンズ面の非球面形状を規定するための非球面 係数を示す。表1B、表1Cにおいても物体側から数えた順番で各レンズ面を特定してい る。 30

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【表18】

{	業1面	第2面	第3 面	第4前	<u>38500</u>	第6面
K	0.00000 E+00	1,96845 E+00	-3.24341 E+00	0.00000 E+00	-4.91958 E+01	3.84487 E+03
A4	-6,70903 E-02	~1,23090 E-01	1.05137 E-01	2.08266 E01	-4,45527 E-02	2.10240 E-02
A6	1,43040 E-02	1.93268 E-01	2.60961 E-01	-7.07806 E-01	0.00000 E+00	0.00000 E+00
AS	0.000000 5400	0.00000 E+00	-5.44654 E-01	1.00543 E+00	-1.05324 E-01	5.55869 E-02
A10	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.000000 E+0.0	0.00000 E+00	0.00000 E+00
A12	0,00000 E+00	0.00000 E+00	0.000000 E+00	0.00000 E+00	0.00000 E+00	0.000000E+00
A14	0,00000 E+00	0.00000 E+00	0,00000 E+00	0.000000 E+00	0.00000 E+00	0.000000E+00
AIS	0.00000 E+00	0.00000 E+00	0.000000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00

【表10】

	第7面	第8節
K	-5.35406 E+00	0.00000 E+00
A4	-6.29015E-02	-1.28252 E-01
A6	-2.28756 E-03	3.60116 E02
A8	-8.15992 E-03	-3.97193E-02
A10	3.30573 E-04	3.02334 E-02
A12	7.78451 E-03	-1.38145 E-02
A14	-4.09359 E-03	3.33327 E-03
A16	4.32061 E-04	~3.35E-04

[0044]

なお、レンズ面に採用する非球面形状は、Yをサグ量、cを曲率半径の逆数、Kを円錐 係数、hを光線高さ、4次、6次、8次、10次、12次、14次、16次の非球面係数 をそれぞれA4、A6、A8、A10、A12、A14、A16とすると、次式により表 わされる。

[0045]

【数1】

$$Y(h) = \frac{ch^{*}}{1 + \sqrt{1 - (K+1)c^{2}h^{2}}} + A_{4}h^{4} + A_{6}h^{6} + A_{8}h^{8} + A_{10}h^{10} + A_{12}h^{12} + A_{14}h^{14} + A_{16}h^{16}$$
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[0046]

(作用効果)

図2(a)~(d)は広角レンズ10の縦収差図、横収差図、像面湾曲図、蛋曲収差図 である。図2(a)の縦収差図では、横軸は光線が光軸しと交わる位置を示し、縦軸は光 線がレンズ系に入射する高さを示している。図2(b)の横収差図では横軸は入射腫底標 を示し、縦軸は収差量を示す。図2(a)、(b)では、波長の異なる複数の可視光線に ついてのシミュレーション結果を示してある。図2(c)の像面湾曲図では横軸は光軸方 向の距離を示し、縦軸は像の高さを示す。図2(c)において、Sはサジタル面における 像面濱曲収差を示し、Tはタンジェンシャル面における像面湾曲収差を示す。図2(d) の瓷曲収差図では横軸は像の歪み量を示し、縦軸は像の高さを示す。

[0047]

図2(a)に示すように、広角レンズ10によれば、軸上の色収差が良好に補正されて いる。また、図2(b)に示すように、色の滲みが抑制される。さらに、図2(c)、(d)に示すように、像面満曲が良好に補正されている。従って、広角レンズ10が高解像 度となる。

[0048]

また、広角レンズ10では、第1レンズ11に凹形状を備える負のパワーのレンズを配 置し、第2レンズ12に凸形状を備える正のパワーを有するレンズを配置したので、65 *以上の副角を備えるレンズ系の全長を4.3mm以下に抑えることができる。さらに、 第4レンズ14の像側レンズ面14bを、変曲点を備える非球面としたので、広角レンズ -10

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10からの射出光線の方向を制御することが容易となり、結像面16に入射する主光線入 射角度を小さく抑制することができる。また、本例では、苔レンズのレンズ面を非球面と したので、広角レンズ10が明るく構成される。さらに、4枚のレンズから広角レンズ1 0を構成したので、5枚以上のレンズを備える撮像レンズと比較して、軽量化や製造コス トの抑制を図ることが容易である。

[0049]

(実施例2)

図3は実施例2の広角レンズの光線図である。図3に示すように、広角レンズ20は、 物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ21、正のパ ワーを有する第2レンズ22、負のパワーを有する第3レンズ23、および正のパワーを 有する第4レンズ24からなる。第1レンズ21と第2レンズ22の間には絞り(不認示)が配置されている。第4レンズ24の像側にはカバーガラス25が配置されている。結 像面25はカバーガラス25と開端を開けた位置にある。

[0050]

第1レンズ21は、物体側レンズ面21aおよび像側レンズ面21bのそれぞれが非球 面とされている。物体側レンズ面21aは凸形状を備えており、像側レンズ面21bは凹 形状を備えている。物体側レンズ面21aは、凸形状をしているレンズ面部分の曲率半径 が大きく、平面形状に近い。

[0051]

第2レンズ22は、物体側レンズ面22aおよび像側レンズ面22bのそれぞれが非球 ²⁰ 面とされている。物体側レンズ面22aおよび像側レンズ面22bは、それぞれ凸形状を 備えている。

[0052]

第3レンズ23は、物体側レンズ面23aおよび像側レンズ面23bのそれぞれが非球 面とされている。物体側レンズ面23aおよび像側レンズ面23bは、それぞれ凹形状を 備えている。

[0053]

第4レンズ24は、物体側レンズ面24aおよび像側レンズ面24bのそれぞれが非球 面とされている。物体側レンズ面24aは光軸を含む中央部分に凸形状を備えている。像 側レンズ面24bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。 従って、像側レンズ面24bは変曲点から内周側に向かって物体側に湾曲しており、変曲 点から外周側に向かって物体側に湾曲している。

[0054]

広角レンズ20の第口数をFno、、半面角をω、および、レンズ系の全長(第1レン ズ21の物体側レンズ面21aの物体側の端から結像面26までの距離)をL、レンズ系 のレンズ厚(第1レンズ21の物体側レンズ面21aの物体側の端から第4レンズ24の 像側レンズ面24bの像側の端までの距離)をDとすると、これらの値は以下のとおりで ある。

Pno. = 2.8 $\omega = 85.8^{\circ}$ L = 4.983mmD = 3.935mm

[0055]

また、全レンズ系の無点距離を「、第1レンズ21の焦点距離を「1、第2レンズ22 の焦点距離を「2、第3レンズ23の焦点距離を「3、第4レンズ24の焦点距離を「4 とすると、これらの値は以下のとおりである。

 $f = 2 \cdot 5 \cdot 6 \cdot 3$ $f = -6 \cdot 9 \cdot 7 \cdot 2$ $f = 2 = 1 \cdot 5 \cdot 2 \cdot 9$ $f = -2 \cdot 4 \cdot 7 \cdot 9$

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(10)

f 4 = 7.890[0056] ここで、本例の広角レンズ20は、以下の条件式(1)~(4)を満たす。 $0, 4 \leq f Z / f = 0, 596 \leq 0.7 \cdot (1)$ $-1 \le f 2 / f 3 = -0.617 \le -0.25 * (2)$ $1.0 \le D/f = 1.535 \le 2.0$ (3) $-30 \le f_1/f = -2, 720 \le -0, 5 \rightarrow (4)$ 100571 広海レンズ20は、条件式(1)~(4)を満たすので、65°以上の画角を確保しな 10 がら、レンズ系の全長を抑制し、パックフォーカスを確保することが容易である。また、 軸上の色収差を抑制することができる。 [0058] また、広角レンズ20は、以下の条件式(5)、(6)を満たす。 $-1.4 \leq 13/1 = -0.967 \leq -0.6 + (5)$ $1.3 \leq L/(-1.944) \leq 2.5 + (6)$ [0059]

広角レンズ20は条件式(5)、(6)を満たすので、色収差を良好に補正できる。また、結像面26に入射する主光線入射角度を小さくできる。さらに、バックフォーカスを 確保しながらレンズ系の会長を抑制することが容易である。

[0060]

以下の表2Aは広角レンズ20の各レンズ面のレンズデータを示す。表2Aでは物体側 から数えた順番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非 球面である。なお、9面および10面はカバーガラス25のガラス面であり、11面は結 像面26である。曲率半径および間隔の単位はミリメートルである。

【0061】 【表2A】

M *	曲率半径	RE RE	Nd(屈折率)	Vd(77%)	材料
1	18.988	0.400	1.53116	56.0	樹脂
2	3.087	1.087		<u>.</u>	
3	1.218	0.529	1.53116	56.0	樹脂
4	-2.093	0.215			
5	-2.030	0.383	1.6349.4	24.0	樹脂
6	7.868	0.601			
7	1.498	0.739	1.53116	56.0	樹脂
8	1.928	0.210			
9	infinity	0.100	1.51680	64.2	光学ガラス
10	infinity	0.762			
1 11	infinity	-0.024	1)	¥

[0062]

次に、表2B、表2Cは非球面とされたレンズ面の非球面形状を規定するための非球面 40 係数を示す。表2B、表2Cにおいても物体側から数えた順番で各レンズ面を特定してい る。

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【表 2 B】

{	1111 1111	第2面	¥3)	第4面	<u> </u>	97.6 mi
K	0.00000 E+00		-2.99208 E+00	2.54698 E+00	-4.48502 E+01	0.00000 E+00
A4	5.78055 E-03		7.81867 E02	1.02286 E01	-7.96020 E-02	2.08047 E-01
AS	-1.09778 E-02	-4,44309 E-02	3.32598 E-02	-5.30883 E-01	0.00000 E+08	0.00000 E+00
AS	0.00000 E+00	0.000000 E+00	-7.00411 E-01	6.21259E-01	-2.22084E-01	8.71866 E-02
A10	0.00000 E+00	0.00000 E+00	~3,91407 E-01	-1.87758E+00	<u>-3.06686 E-01</u>	
A12	0.00000 E+00	······	0,00000 E+00	0.00000 E+00	0.00000 E+00	(
A14	0.00000 E+00		0.000000 E+00	0.00000 E+00	0.00000 E+00	
AIS	0.00000 E+00	0,00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00

【表 2 C】

	黨7面	<u> </u>
K	-6.38920 E+00	8.00000 E+00
A4	-1.11271 E-01	-1.63845E-01
Aß	3.08045 E-02	4.93248E-02
A8	-3.76929 E-03	<u>-3.99351 E-02</u>
A10	-3.21888 E-03	3.00214 E02
A12	5.97323 E-03	-1.39517E-02
A14	-4.16558 E-03	<u>3.30562 E03</u>
A18	9.01603 E-04	3.20E04

 $(0,1)_{i\in \mathbb{N}} \in \mathbb{N}$

[0063]

(作用効果)

照4(a)~(d)は広角レンズ20の縦収差図、横収差図、像面湾曲図、亜曲収差図 である。図4(a)に示すように、広角レンズ20によれば、軸上の色収差が良好に補正 されている。また、図4(b)に示すように、色の滲みが抑制される。さらに、図4(c))、(d)に示すように、像面湾曲が良好に補正されている。従って、広角レンズ20が 高解像度となる。

[0064]

また、広角レンズ20では、第1レンズ21に凹形状を備える負のパワーのレンズを配置し、第2レンズ22に凸形状を備える正のパワーを有するレンズを配置したので、65 30 * 以上の画角を備えるレンズ系の全長を5mm以下に抑えることができる。さらに、第4 レンズ24の像側レンズ菌24bを、変曲点を備える非球菌としたので、広角レンズ20 からの射出光線の方向を制御することが容易となり、結像菌26に入射する主光線入射角 度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面とした ので、広角レンズ20が明るく構成される。さらに、4枚のレンズから広角レンズを構成 したので、5枚以上のレンズを備える撮像レンズと比較して、軽量化や製造コストの抑制 を図ることが容易である。

[0065]

(実施例3)

図5は実施例3の広角レンズの光線図である。図5に示すように、広角レンズ30は、 40 物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ31、正のパ ワーを有する第2レンズ32、魚のパワーを有する第3レンズ33、および正のパワーを 有する第4レンズ34からなる。第1レンズ31と第2レンズ32の間には絞り(不図示)が配置されている。第4レンズ34の像側にはカバーガラス35が配置されている。結 像面36はカバーガラス35と開端を開けた位置にある。

[0086]

第1レンズ31は、物体側レンズ面31aおよび像側レンズ面31bのそれぞれが非球面とされている。物体側レンズ面31aは凸形状を備えており、像側レンズ面31bは凹形状を備えている。物体側レンズ面31aは、凸形状をしているレンズ面部分の曲率半径が大きく、平面形状に近い。

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(12)

[0087]

第2レンズ32は、物体側レンズ面32aおよび像側レンズ面32bのそれぞれが非球 面とされている。物体側レンズ面32aおよび像側レンズ面32bは、それぞれ凸形状を 備えている。

[0068]

第3レンズ33は、物体側レンズ面33aおよび像側レンズ面33bのそれぞれが非球 面とされている。物体側レンズ面33aは凹形状を備えており、像側レンズ面33bは凸 形状を備えている。

[0059]

第4レンズ34は、物体側レンズ面34aおよび像側レンズ面34bのそれぞれが非球¹⁰ 面とされている。物体側レンズ面34aは光軸を含む中央部分に凸形状を備えている。像 側レンズ面34bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。 従って、像側レンズ面34bは変曲点から内角側に向かって物体側に湾曲しており、変曲 点から外周側に向かって物体側に湾曲している。

[0070]

広角レンズ30の開口数をFno.、半面角をm、および、レンズ系の全長(第1レン ズ31の物体側レンズ面31aの物体側の端から結像面36までの距離)をL、レンズ系 のレンズ厚(第1レンズ31の物体側レンズ面31aの物体側の端から第4レンズ34の 像側レンズ面34bの像側の端までの距離)をDとすると、これらの値は以下のとおりで ある。

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P n o. = 2.8 $w = 85.8^{\circ}$ L = 3.838 mm D = 2.783 mm[0071]

また、全レンズ系の焦点距離をf、第1レンズ31の焦点距離をf1、第2レンズ32 の焦点距離をf2、第3レンズ33の焦点距離をf3、第4レンズ34の焦点距離をf4 とすると、これらの値は以下のとおりである。

f = 2.563

f 1 == -- 4. 824

f 2 == 1. 3 4 0

f = -2.259

f 4 == 4, 190

[0072]

ことで、本例の広角レンズ30は、以下の条件式(1)~(4)を満たす。 0、4≤ f2/f=0、523 ≤0.7 · (1) -1≤ f2/f3=-0.593 ≤-0.25 · (2) 1、0≤ D/f=1.086 ≤2.0 · (3) -30≤ f1/f=-1.882 ≤-0.5 · (4) [0073]

広角レンズ30は、条件式(1)~(4)を満たすので、65°以上の顕角を確保しな がら、レンズ系の全長を抑制し、パックフォーカスを確保することが容易である。また、 軸上の色収差を抑制することができる。

[0074]

また、広角レンズ30は、以下の条件式(5)、(6)を満たす。
-1、4≤ f3/f=-0、881 ≤-0、6 ・ (5)
1、3≤ L/f=1、498 ≤2.5 ・ (6)
[0075]

広角レンズ30は条件式(5)、(6)を満たすので、色収差を良好に補正できる。また、結像面36に入射する主光線入射角度を小さくできる。さらに、パックフォーカスを 50

確保しながらレンズ系の全長を抑制することが容易である。

[0076]

以下の表3Aは広角レンズ30の各レンズ面のレンズデータを示す。表3Aでは物体側 から数えた順番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非 球面である。なお、9面および10面はカパーガラス35のガラス面であり、11面は結 像面36である。曲率半径および間隔の単位はミリメートルである。

100771

【表 3 A】

<u>in 7</u>	曲率半径		Nd(圖新率)	Vd(アッベ数)	材料
1	150,000	0,400	1,53116	56.0	樹脂
2	2.527	0.068			
3	0.974	0,479	1.53116	56.0	樹膽
4	-2.225	0.289			
5	-0.878	0.322	1.6349.4	24.0	樹皺
8	-1.512	0.301			
7	1.218	0.923	1.5311.6	56.0	樹脂
8	1.971	0.210			
9	infinity	0.100	1.51680	64.2	<u>光学ガラス</u>
10	infinity	0.773	<u></u>		Į
11	infinity	-0.028	}		Į

[0078]

次に、表3B、表3Cは非球面とされたレンズ面の非球面形状を規定するための非球面 係数を示す。表3B、表3Cにおいても物体側から数えた顕示で各レンズ面を特定してい る。

【表38】

[家日面	第2面	第3页	第4面	第5面	第6面
K	0,00000 E+00	3.50577 E+00	-3.83881 E+00	5,33536 E+00	-4.54098 E+00	***************************************
A4	-1.74521E-02	-3.32642 E-01	5,90588 E-02	8.27775 E-02	<u>-4.37925 E-01</u>	1.43565 E-01
As	-1.70578 E-01	-1.70011 E-01	8.54666 E-02	-2.36439 E-01	**************************************	human human has a second s
AS	0.00000 E+00	0.00000 E+00	-5.37071 E-01	~1.38356 E+00	1.01643 E+00	6.87456 E-01
A10	0.00000 E+00	0.00000 E+00	~3.10124 E+00	9.66727E-01	1.18549 E+00	<u>-1.66451E-01</u>
A12	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00
A14	0,00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+08	0.00000 E+00
A16	0,00000 E+00	0.000000 E+0.0	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.000000E+001

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【表3C】

	第7面	<u> </u>
K	-7.24393 E+00	0.000000 E+00
<u>A4</u>	-1.40591 8-01	-1.80857 E-01
A6	4.71327 E-02	6.52796 E-02
A8	-5.32562 E-03	-4.48510 E-02
A10	~5.36876 E~03	2.97256E-02
A12	5.96681E-03	-1.34959 E-02
A14	~4.45794E-03	3.25636 E-03
A18	1.08896 E-03	-3.236-04

[0079]

(作用効果)

図6(a)~(d)は広角レンズ30の縦収差図、横収差図、像面湾曲図、歪曲収差図 である。図6(a)に示すように、広角レンズ30によれば、軸上の色収差が良好に補正 されている。また、図6(b)に示すように、色の滲みが抑制される。さらに、図6(c))、(d)に示すように、像面湾曲が良好に補正されている。従って、広角レンズ30が

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高解像度となる。

[0080]

また、広角レンズ30では、第1レンズ31に凹形状を備える負のパワーのレンズを配 置し、第2レンズ32に凸形状を備える正のパワーを有するレンズを配置したので、65 *以上の画角を備えるレンズ系の全長を4mm以下に抑えることができる。さらに、第4 レンズ34の像側レンズ面34bを、変曲点を備える非球面としたので、広角レンズ30 からの射出光線の方向を制御することが容易となり、結像面36に入射する主光線入射角 度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面とした ので、広角レンズ30が明るく構成される。さらに、4枚のレンズから広角レンズ10を 構成したので、5枚以上のレンズを備える撮像レンズと比較して、軽量化や製造コストの 抑制を図ることが容易である。

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【0081】 (実施例4)

図7は実施例4の広角レンズの光線図である。図7に示すように、広角レンズ40は、 物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ41、正のパ ワーを有する第2レンズ42、負のパワーを有する第3レンズ43、および正のパワーを 有する第4レンズ44からなる。第1レンズ41と第2レンズ42の間には絞り(不図示)が配置されている。第4レンズ44の像側にはカバーガラス45が配置されている。結 像面46はカバーガラス45と問題を開けた位置にある。

[0082]

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第1レンズ41は、物体側レンズ面41aおよび像側レンズ面41bのそれぞれが非球 面とされている。物体側レンズ面41aは凸形状を備えており、像側レンズ面41bは凹 形状を備えている。物体側レンズ面41aは、凸形状をしているレンズ面部分の曲率半径 が大きく、平面形状に近い。

[0 0 8 3]

第2レンズ42は、物体側レンズ面42aおよび像側レンズ面42bのそれぞれが非球 面とされている。物体側レンズ面42aおよび像側レンズ面42bは、それぞれ凸形状を 備えている。

[0084]

第3レンズ43は、物体側レンズ面43aおよび像側レンズ面43bのそれぞれが非球 30 面とされている。物体側レンズ面43aは凹形状を備えており、像側レンズ面43bは凸 形状を備えている。

[0085]

第4レンズ44は、物体側レンズ面44aおよび像側レンズ面44bのそれぞれが非球 固とされている。物体側レンズ面44aは光軸を含む中央部分に凸形状を備えている。像 側レンズ面44bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。 従って、像側レンズ面44bは変曲点から内周期に向かって物体側に湾曲しており、変曲 点から外周側に向かって物体側に湾曲している。

[0086]

広角レンズ40の開口数をFno、、半面角をω、および、レンズ系の全長(第1レン ⁴⁰ ズ41の物体側レンズ面41aの物体側の端から結像面46までの距離)をし、レンズ系 のレンズ厚(第1レンズ41の物体側レンズ面41aの物体側の端から第4レンズ44の 像側レンズ面44bの像側の端までの距離)をDとすると、これらの値は以下のとおりで ある。

P n o. = 2.8 $m = 85.8^{\circ}$ L = 3.932 mm D = 2.895 mm[0087]

また、金レンズ系の焦点距離をす、第1レンズ41の焦点距離をす1、第2レンズ42 50

の焦点距離を12、第3レンズ43の焦点距離を13、第4レンズ44の焦点距離を14 とすると、これらの値は以下のとおりである。 f=2. 563 f1 = -14.458 $f_2 = 1.595$ $f_3 = -2.032$ f4 = 3, 607[0088] ここで、本例の広角レンズ40は、以下の条件式(1)~(4)を満たす。 10 $0, 4 \le f 2 / f = 0, 6 2 2 \le 0, 7 + (1)$ $-1 \leq \{2 \neq 1 \ 3 = -0, 7 \ 8 \ 5 \leq -0, 2 \ 5 \ \cdot \ (2)$ 1. $0 \le D/t = 1.129 \le 2.0 + (3)$ $-30 \leq f1/f=-5.640 \leq -0.5 \cdot (4)$ [0089] 広角レンズ40は、条件式(1)~(4)を満たすので。65°以上の画角を確保しな から、レンズ系の全長を抑制し、パックフォーカスを確保することが容易である。また、 軸上の色収差を抑制することができる。 [0090] また。広角レンズ40は、以下の条件式(5)、(8)を溺たす。 20 $-1: 4 \leq 13/1 = -0.793 \leq -0.6 + (5)$ 1. $3 \leq L/f = 1, 534 \leq 2.5 + (6)$ [0091] 広角レンズ40は条件式(5)、(6)を備たすので、色収差を良好に補正できる。ま た、結像面46に入射する主光線入射角度を小さくできる。さらに、パックフォーカスを 確保しながらレンズ系の全長を抑制することが容易である。 [0092]

以下の表4Aは広角レンズ40の各レンズ面のレンズデータを示す。表4Aでは物体側 から数えた順番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非 球面である。なお、9面および10面はカバーガラス45のガラス面であり、11面は結 像面46である。曲率半径および関際の単位はミリメートルである。 【0093】

[æ4Å]

面番	曲率半径	關聯	Nd(照拆率)	Vd(アッベ数)	材料
1	150.000	0,400	1,53116	56.0	樹脂
2	7.327	0.099		<u>}</u>	
3	1,413	0,558	1.53116	56.0	樹脂
4	-1.848	0,338			
5	-0.578	0.361	1,63494	24.0	
6	-1.285	0.146			
7	1.147	0.995	1.5311.6	56.0	樹脂
8	1.985	0.210	<u> </u>		
9	infinity	0.100	1.5168.0	64.2	光学ガラス
10	<u>infinity</u>	0.753	<u>.</u>		
11	infinity	-0.026		\$	<u> </u>

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[0094]

次に、表4B、表4Cは非球面とされたレンズ面の非球面形状を規定するための非球面 係数を示す。表4B、表4Cにおいても物体側から数えた順番で各レンズ面を特定してい る。 【表48]

[第1面	第2面	<u> </u>	\$\$4 1 31	<u> </u>	<u> </u>
X	0.00000 E+00	9.96692 E+01	~4.55267E+00	5.20287 E+00	-3.51020 E+00	0.00000 E+00
A4	-2.50623 E-03	-3.83857 E-02	3.83770 E-02	-1.33640 E-01	~5.16180E-01	1.22505 E-01
Aß	~8.07761 E-02	-6.22535 E-02	-1.17843 E-01	7.52591 E02	0.00000 E+00	0.00000 E+00
A8	0.00000 E+00	-3.63324 E-01	~7.96090E-01	-1.60850 E+00	8,70251 E-01	6.90508 E-01
AIQ	0.000000 E+00	0.00000 E+00	~4.16550 E+00	5.85779 E-01	8.59858 E-01	<u>-3.11595E-01</u>
A12	0.00000 E+00	0.00000 E+00	8.20707 E+00	1.85436 E+00	-3.35128E-01	-4.39279E-02
A14	0.000000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.000000 E+00
A18	0.00000 E+00	0.000000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00

【表40】

	% 7 m	\$8.8M
K	~8.11925 E+00	0.00000 E+00
A4	-1.95885 E-01	-1.93101 E-01
A6	1.03146E-01	7.12000 E-02
AS	-3.81144 E-02	-4.41820 E-02
A10	2.84718 - 03	2.85423 E-02
A12	6.32241 E-03	-1.35319 E-02
A14	-6.95948 E-03	3.43603 E03
A18	1.89193 E-03	-3.56E-04

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(作用効果)

図8(a)~(d)は広角レンズ40の縦収差図、横収差図、像面薄曲図、歪曲収差図 である。図8(a)に示すように、広角レンズ40によれば、軸上の色収差が良好に補正 されている。また、図8(b)に示すように、色の滲みが抑制される。さらに、図8(c)、(d)に示すように、像面湾曲が良好に補正されている。従って、広角レンズ40が 高解像度となる。

[0096]

また、広角レンズ40では、第1レンズ41に四形状を備える負のパワーのレンズを配 置し、第2レンズ42に凸形状を備える正のパワーを有するレンズを配置したので、65 ・以上の画角を備えるレンズ系の全長を4、0mm以下に抑えることができる。さらに、 第4レンズ44の像側レンズ面44bを、変曲点を備える非球面としたので、広角レンズ 40からの射出光線の方向を制御することが容易となり、結像面46に入射する主光線入 射角度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面と したので、広角レンズ40が明るく構成される。さらに、4枚のレンズから広角レンズを 構成したので、5枚以上のレンズを備える撮像レンズと比較して、経量化や製造コストの 抑制を図ることが容易である。

[0097]

(実施例5)

図9は実施例5の広角レンズの光線圏である。図9に示すように、広角レンズ50は、 40 物体側から像側に向かって順に配置された、負のパワーを有する第1レンズ51、正のパ ワーを有する第2レンズ52、黄のパワーを有する第3レンズ53。および正のパワーを 有する第4レンズち4からなる。第1レンズ51と第2レンズ52の間には絞り(不図示)が配置されている。第4レンズ54の像側にはカバーガラス55が配置されている。結 像面56はカバーガラス55と開陽を開けた位置にある。

[0098]

第1レンズ51は、物体側レンズ面51aおよび像側レンズ面51bのそれぞれが非球 部とされている。物体側レンズ面51aは凸形状を備えており、像側レンズ面51bは凹 形状を備えている。物体側レンズ面51aは、凸形状をしているレンズ面部分の曲率半径 が大きく、平面形状に近い。

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[0099]

第2レンズ52は、物体側レンズ面52aおよび像側レンズ面52bのそれぞれが非球 面とされている。物体側レンズ面52aおよび像側レンズ面52bは、それぞれ凸形状を 備えている。

[0100]

第3レンズ53は、物体側レンズ面53aおよび像側レンズ面53bのそれぞれが非球 面とされている。物体側レンズ面53aは凹形状を備えており、像側レンズ面53bは凸 形状を備えている。

[0101]

第4レンズ54は、物体側レンズ面54aおよび像側レンズ面54bのそれぞれが非球¹⁰ 面とされている。物体側レンズ面54aは光軸を含む中央部分に凸形状を備えている。像 側レンズ面54bは、変曲点を有しており、光軸を含む中央部分に凹形状を備えている。 従って、像側レンズ面54bは変曲点から内周側に向かって物体側に湾曲しており、変曲 点から外周側に向かって物体側に湾曲している。

[0102]

広角レンズ50の開口数をFno、、半面角をω、および、レンズ系の全長(第1レンズ51の物体側レンズ面51aの物体側の端から結像面56までの距離)をL、レンズ系のレンズ厚(第1レンズ51の物体側レンズ面51aの物体側の端から第4レンズ54の像側レンズ面54bの像側の端までの距離)をDとすると、これらの値は以下のとおりである。

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Fno. = 2.8 $\omega = 85.7^{\circ}$ L = 4.107mm D = 3.031mm [0103]

また、金レンズ系の焦点距離を「、第1レンズ51の焦点距離を「1、第2レンズ52 の焦点距離を「2、第3レンズ53の焦点距離を「3、第4レンズ54の焦点距離を「4 とすると、これらの値は以下のとおりである。

8=2.563

f1 = -62.580

f2 = 1.715

f3 = -1.832

f 4 = 3.091

[0104]

ここで、本例の広角レンズ50は、以下の条件式(1)~(4)を満たす。 0、4≤ f2/f=0、669 ≤0、7 ・・(1) -1≤ f2/f3=-0、936 ≤-0、25 ・・(2) 1、0≤ D/f=1、182 ≤2、0 ・・(3) -30≤ f1/f=-24、417 ≤-0、5 ・・(4) [0105] 広角レンズ50は、条件式(1)~(4)を満たすので、65°以上の顯角を

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広角レンズ50は、条件式(1)~(4)を満たすので、65°以上の画角を確保しな がら、レンズ系の金長を抑制し、バックフォーカスを確保することが容易である。また、 軸上の色収差を抑制することができる。

[0106]

また、広角レンズ50は、以下の条件式(5)、(6)を満たす。 -1.4≦ f3/f=-0.715 ≦-0.6 ・・(5) 1.3≦ L/f=1.602 ≦2.5 ・・(6)

[0107]

広角レンズ50は条件式(5)、(6)を満たすので、色収差を良好に補正できる。また、結像面56に入射する主光線入射角度を小さくできる。さらに、パックフォーカスを 50

確保しながちレンズ系の全長を抑制することが容易である。

[0108]

以下の表5Aは広角レンズ50の各レンズ面のレンズデータを示す。表5Aでは物体側 から数えた順番で各レンズ面を特定している。本例では、各レンズの全てのレンズ面が非 球面である。なお、9面および10面はカバーガラス55のガラス面であり、11面は結 像面56である。曲率半径および開端の単位はミリメートルである。

[0109]

【表 5 A】

m #	曲率半径	間隔	Nd(屈折率)	Vd(アッベ数)	材料
1	150.000	0.400	1,53116	56.0	樹膽
2	27.279	0.298			<u></u>
3	1.796	0.549	1.53116	56.0	樹脂
4	-1.687	0.352	Į	<u>.</u>	
5	-0.536	0.331	1.6349.4	24.0	樹脂
6	-1.225	0.109			
7	1.053	0.992	1.53116	56.0	樹脂
8	1.960	0.210			
9	infinity	0.100	1.51680	64.2	<u> 光学ガラス</u>
10	infinity	0,791			<u></u>
11	infinity	-0.025			<u> </u>

[0110]

次に、表5B。表5Cは非球面とされたレンズ面の非球面形状を規定するための非球面 係数を示す。表5B、表5Cにおいても物体側から数えた順番で各レンズ面を特定してい る。

【表 5 B】

[第1面	第2面	第 3函	<u>%4</u> m	<u> 第5</u> 11	第6面
K	0.00000 E+00	1.68169 E+03	-7.82206 E-01	4.95063 E+00	~3.52793 E+00	0.00000 E+00
A4	1,35856 E-01	4.80109 E-01	1.56539 E01	-1.62437 E-01	-7.43230 E-01	1.06681 E-01
A6	-2.24346 E-02	-6.34433 E-01	-2.72463 E-02	4.51584E-01	0.00000 E+00	8.00000 E+08
A8	0,00000 E+00	1.41506 E+00	-7.42170E-01	-1.63061E+00	9.47084 E-01	7.11233 E-01
A10	0,00000 E+00	0.000000 E+00	~3,96390 E+00	-7.77874 E-02	7.17913 E01	-3.14780 E-01
A12	0.00000 E+00	0.00000 E+00	7.84072 E+00	2.79289 E+00	-3.48348 E+00	-6.16063E-02
A14	0.00000 E+00	0,000000 E+00	0.000000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00
A16	0.00000 E+00	0.000000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00	0.00000 E+00

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【麦5 C】

	第7面	第8而
ĸ	~8.73455 E+00	0.000000 E+00
A4	-1.85191 E-01	-1.98948 E-01
Aß	9.59854 E-02	7.50201 E-02
A8	-3.21706 E-02	~4.53006 E-02
A10	2.48962 E-03	2.82001 E02
A12	6.31466 E-03	-1.34263 E-02
A14	-7.56292 E-03	3,48357 E-03
A16	2.27749 E-03	-3.70E-04

[0111]

(作用効果)

図10(a)~(d)は広角レンズ50の縦収差図、横収差図、像面湾曲図、歪曲収差 図である。図10(a)に示すように、広角レンズ50によれば、軸上の色収差が良好に 補正されている。また、図10(b)に示すように、色の滲みが抑制される。さらに、図 10(c)、(d)に示すように、像面湾曲が良好に補正されている。従って、広角レン

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ズ50が高解像度となる。

[0112]

また、広角レンズ50では、第1レンズ51に凹形状を備える負のパワーのレンズを配 置し、第2レンズ52に凸形状を備える正のパワーを有するレンズを配置したので、65 *以上の画角を備えるレンズ系の全長を4.1mm程度に抑えることができる。さらに、 第4レンズ54の像側レンズ面54bを、変曲点を備える非球面としたので、広角レンズ 50からの射出光線の方向を制御することが容易となり、結像面56に入射する主光線入 射角度を小さく抑制することができる。また、本例では、各レンズのレンズ面を非球面と したので、広角レンズ50が明るく構成される。さらに、4枚のレンズから広角レンズを 構成したので、5枚以上のレンズを備える撮像レンズと比較して、軽量化や製造コストの 抑制を図ることが容易である。

(0113)

(摄像装置)

図11は本発明の広角レンズ10を搭載する撮像装置100の説明図である。図11に 示すように、撮像装置100は広角レンズ10の結像面16(焦点位置)にセンサ面10 1aを配置した撮像素子101を備えるものである。撮像素子101は、CCDセンサ或 いはCMOSセンサである。

[0114]

本例によれば、広角レンズ10のレンズ系の全長しが短いので、撮像装置100を小型 化することができる。さらに、広角レンズ10から撮像素子101に入射する主光線入射 角度が小さく抑えられるので、撮像装置100における画質の劣化を抑制できる。すなわ ち、これらの撮像素子101ではセンサ面101aに斜めから入射する光に対して感度が 低下する特性を有するので、主光線入射角度が大きくなると画質の劣化を招いてしまうが 、本例の広角レンズ10によれば結像面に対する主光線入射角度を小さくすることができ るので、センサ面への光線の入射角度に起因する画質の劣化を抑制できる。また、広角レ ンズ10の解像度が高いので、撮像素子101として画素数の多い撮像素子101を採用 することにより、撮像装置100を高解像度のものとすることができる。なお、撮像装置 100には、広角レンズ20~50を広角レンズ10と同様に搭載することができ、この 場合にも同様の効果を得ることができる。

[0115]

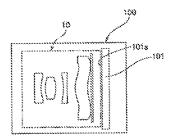
なお、上記の例では、全てのレンズ面が非球面とされているが、第4レンズの像側レン ズ面を含む少なくとも2つのレンズ面を非球面とすれば、広角レンズを明るく構成するこ とが容易となる。

【符号の説明】 【0116】 10、20、30、40、50、、広角レンズ 11、21、31、41、51、、第1レンズ 12、22、32、42、52、、第2レンズ 13、23、33、43、53、、第3レンズ 14、24、34、44、54、、第4レンズ 14b、24b、34b、44b、54b、、第4レンズ 14b、24b、34b、44b、54b、、第4レンズ 15、25、35、45、55、、カバーガラス 15、26、36、46、56、、結像面 100、、機像装置 101、、、撮像業子のセンサ面 D、、、レンズ系のレンズ厚 L、、、レンズ系の全長

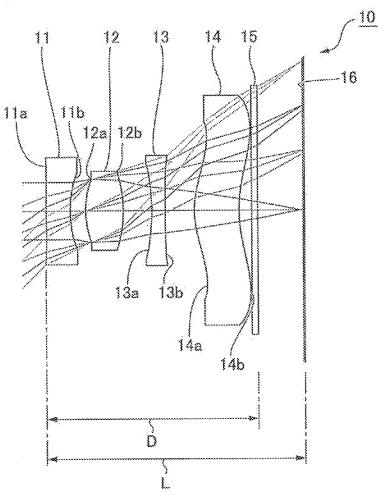
-28

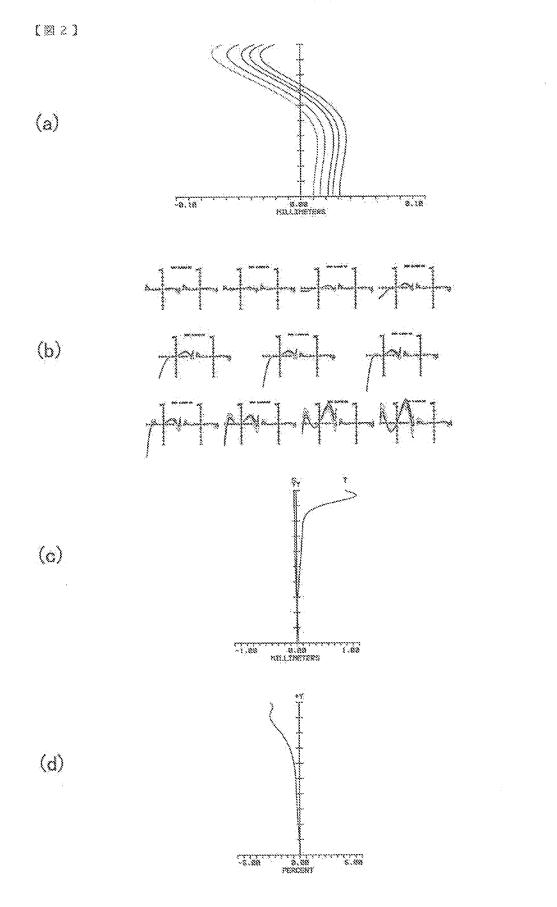
10

[図11]

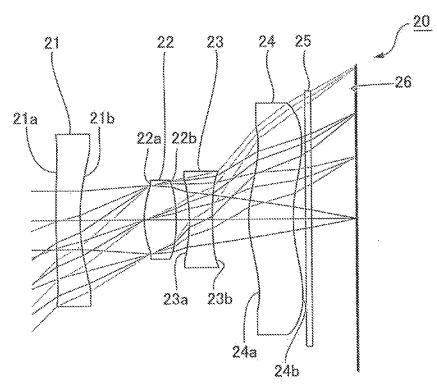






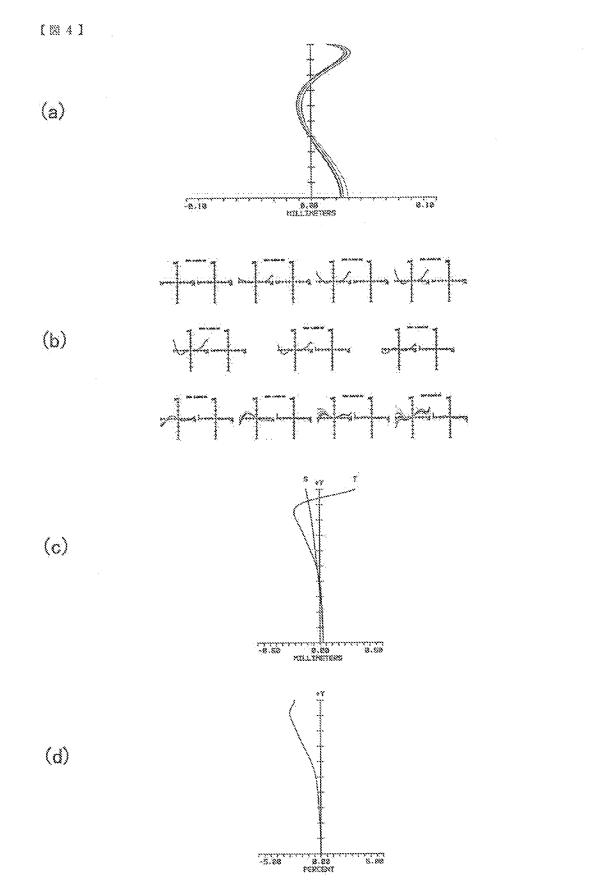


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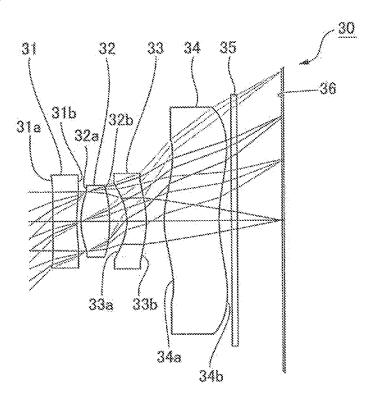


AOET, Ex. 1002 Page 197

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[85]



27.73



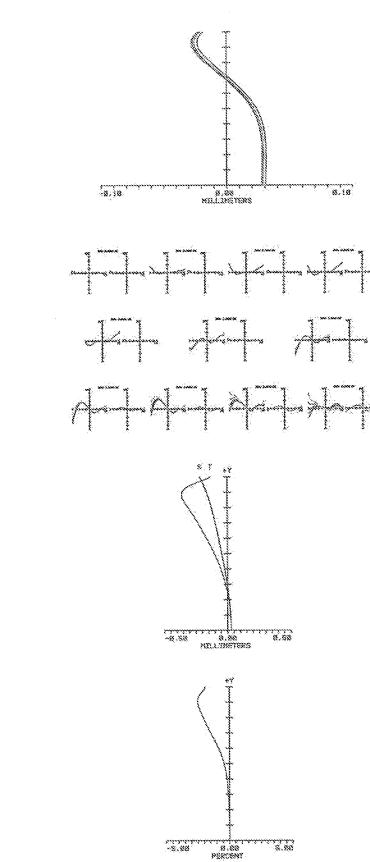
(a)

(b)

(c)

(d)

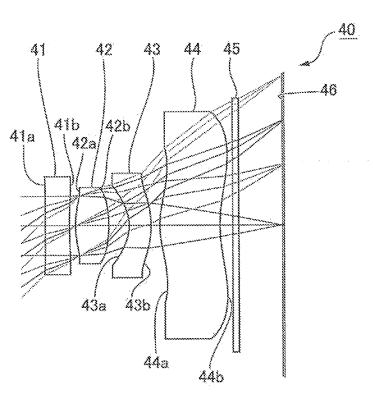
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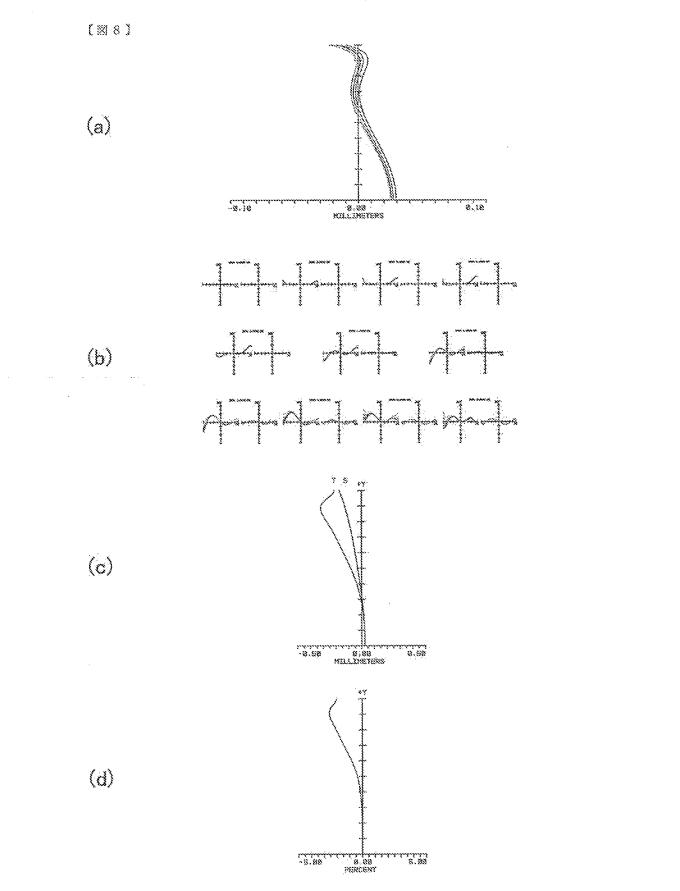


AOET, Ex. 1002 Page 200

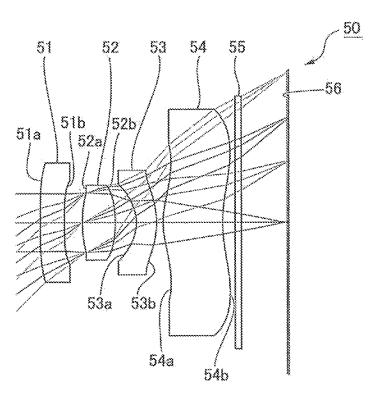
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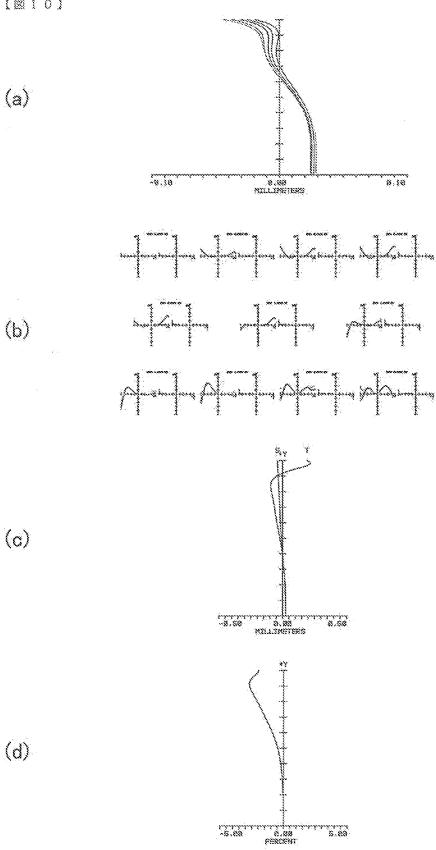




[🖾 9]



(M10)



AOET, Ex. 1002 Page 204

 $\varphi_{1}, \varphi_{2}, \dots, \varphi_{n-1}$

フロントページの続き

ドターム(参考) 28087 KAO1 LAO1 PAD4 PA17 PB04 QAO2 QAO6 QA17 QA21 QA26 QA32 QA42 QA45 RA04 RA05 RA12 RA13 RA32 RA42 RA44 **BA01**

Electronic A	cknowledgement Receipt
EFS ID:	20824379
Application Number:	14105811
International Application Number:	
Confirmation Number:	5836
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL
First Named Inventor/Applicant Name:	WEI-YU CHEN
Customer Number:	24728
Filer:	Tim Tingkang Xia/Chenae Byrd
Filer Authorized By:	Tim Tingkang Xia
Attorney Docket Number:	14970-94702
Receipt Date:	01-DEC-2014
Filing Date:	13-DEC-2013
Time Stamp:	12:35:20
Application Type:	Utility under 35 USC 111(a)

Payment information:

Submitted wit	th Payment	no	no				
File Listing	g:						
Document Number	Document Description	File Name	File Size(Bytes)/ Message Digest	Multi Part /.zip	Pages (if appl.)		
1	Information Disclosure Statement (IDS)	1497094702IDS.pdf	612323	no	4		
, ,	Form (SB08)	1497 0947 02105.pdf	63520b4aa164287e65ef6d12ce3a54d601d d4935	110	т		
Warnings:							
Information:			AO	ET, Ex. 10	02		

Information					
Warnings:					
2	Foreign Reference	1497094702JP2014178623.pdf		no	32
			4629754		

Total Files Size (in byte	s): 5242077
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This Acknowledgement Receipt evidences receipt on the noted date by the USPTO of the indicated documents, characterized by the applicant, and including page counts, where applicable. It serves as evidence of receipt similar to a Post Card, as described in MPEP 503.

New Applications Under 35 U.S.C. 111

If a new application is being filed and the application includes the necessary components for a filing date (see 37 CFR 1.53(b)-(d) and MPEP 506), a Filing Receipt (37 CFR 1.54) will be issued in due course and the date shown on this Acknowledgement Receipt will establish the filing date of the application.

National Stage of an International Application under 35 U.S.C. 371

If a timely submission to enter the national stage of an international application is compliant with the conditions of 35 U.S.C. 371 and other applicable requirements a Form PCT/DO/EO/903 indicating acceptance of the application as a national stage submission under 35 U.S.C. 371 will be issued in addition to the Filing Receipt, in due course.

New International Application Filed with the USPTO as a Receiving Office

If a new international application is being filed and the international application includes the necessary components for an international filing date (see PCT Article 11 and MPEP 1810), a Notification of the International Application Number and of the International Filing Date (Form PCT/RO/105) will be issued in due course, subject to prescriptions concerning national security, and the date shown on this Acknowledgement Receipt will establish the international filing date of the application. UNITED STATES PATENT AND TRADEMARK OFFICE



UNITED STATES DEPARTMENT OF COMMERCE United States Patent and Trademark Office Address: COMMISSIONER FOR PATENTS P.O. Box 1450 Alexandria, Virginia 22313-1450 www.uspto.gov

NOTICE OF ALLOWANCE AND FEE(S) DUE

24728 7590 01/27/2015 MORRIS MANNING MARTIN LLP IP Department 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER ATLANTA, GA 30326 EXAMINER DINH, JACK ART UNIT PAPER NUMBER

2872

DATE MAILED: 01/27/2015

APPLICATION NO.	FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.
14/105,811	12/13/2013	WEI-YU CHEN	14970-94702	5836

TITLE OF INVENTION: IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL

APPLN. TYPE	ENTITY STATUS	ISSUE FEE DUE	PUBLICATION FEE DUE	PREV. PAID ISSUE FEE	TOTAL FEE(S) DUE	DATE DUE
nonprovisional	UNDISCOUNTED	\$960	\$0	\$O	\$960	04/27/2015

THE APPLICATION IDENTIFIED ABOVE HAS BEEN EXAMINED AND IS ALLOWED FOR ISSUANCE AS A PATENT. <u>PROSECUTION ON THE MERITS IS CLOSED</u>. THIS NOTICE OF ALLOWANCE IS NOT A GRANT OF PATENT RIGHTS. THIS APPLICATION IS SUBJECT TO WITHDRAWAL FROM ISSUE AT THE INITIATIVE OF THE OFFICE OR UPON PETITION BY THE APPLICANT. SEE 37 CFR 1.313 AND MPEP 1308.

THE ISSUE FEE AND PUBLICATION FEE (IF REQUIRED) MUST BE PAID WITHIN <u>THREE MONTHS</u> FROM THE MAILING DATE OF THIS NOTICE OR THIS APPLICATION SHALL BE REGARDED AS ABANDONED. <u>THIS STATUTORY PERIOD CANNOT BE EXTENDED</u>. SEE 35 U.S.C. 151. THE ISSUE FEE DUE INDICATED ABOVE DOES NOT REFLECT A CREDIT FOR ANY PREVIOUSLY PAID ISSUE FEE IN THIS APPLICATION. IF AN ISSUE FEE HAS PREVIOUSLY BEEN PAID IN THIS APPLICATION (AS SHOWN ABOVE), THE RETURN OF PART B OF THIS FORM WILL BE CONSIDERED A REQUEST TO REAPPLY THE PREVIOUSLY PAID ISSUE FEE TOWARD THE ISSUE FEE NOW DUE.

HOW TO REPLY TO THIS NOTICE:

I. Review the ENTITY STATUS shown above. If the ENTITY STATUS is shown as SMALL or MICRO, verify whether entitlement to that entity status still applies.

If the ENTITY STATUS is the same as shown above, pay the TOTAL FEE(S) DUE shown above.

If the ENTITY STATUS is changed from that shown above, on PART B - FEE(S) TRANSMITTAL, complete section number 5 titled "Change in Entity Status (from status indicated above)".

For purposes of this notice, small entity fees are 1/2 the amount of undiscounted fees, and micro entity fees are 1/2 the amount of small entity fees.

II. PART B - FEE(S) TRANSMITTAL, or its equivalent, must be completed and returned to the United States Patent and Trademark Office (USPTO) with your ISSUE FEE and PUBLICATION FEE (if required). If you are charging the fee(s) to your deposit account, section "4b" of Part B - Fee(s) Transmittal should be completed and an extra copy of the form should be submitted. If an equivalent of Part B is filed, a request to reapply a previously paid issue fee must be clearly made, and delays in processing may occur due to the difficulty in recognizing the paper as an equivalent of Part B.

III. All communications regarding this application must give the application number. Please direct all communications prior to issuance to Mail Stop ISSUE FEE unless advised to the contrary.

IMPORTANT REMINDER: Utility patents issuing on applications filed on or after Dec. 12, 1980 may require payment of maintenance fees. It is patentee's responsibility to ensure timely payment of maintenance fees when due.

PART B - FEE(S) TRANSMITTAL

Complete and send this form, together with applicable fee(s), to: <u>Mail</u> Mail Stop ISSUE FEE **Commissioner for Patents** P.O. Box 1450 Alexandria, Virginia 22313-1450

or <u>Fax</u> (571)-273-2885

INSTRUCTIONS: This form should be used for transmitting the ISSUE FEE and PUBLICATION FEE (if required). Blocks 1 through 5 should be completed where appropriate. All further correspondence including the Patent, advance orders and notification of maintenance fees will be mailed to the current correspondence address as indicated unless corrected below or directed otherwise in Block 1, by (a) specifying a new correspondence address; and/or (b) indicating a separate "FEE ADDRESS" for maintenance fee notifications.

CURRENT CORRESPONDENCE ADDRESS (Note: Use Block 1 for any change of address)

24728 7590 01/27/2015 MORRIS MANNING MARTIN LLP **IP** Department 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER **ATLANTA, GA 30326**

Note: A certificate of mailing can only be used for domestic mailings of the Fee(s) Transmittal. This certificate cannot be used for any other accompanying papers. Each additional paper, such as an assignment or formal drawing, must have its own certificate of mailing or transmission.

Certificate of Mailing or Transmission I hereby certify that this Fee(s) Transmittal is being deposited with the United States Postal Service with sufficient postage for first class mail in an envelope addressed to the Mail Stop ISSUE FEE address above, or being facsimile transmitted to the USPTO (571) 273-2885, on the date indicated below.

(Depo	sitor's name)
	(Signature)
	(Date)

APPLICATION NO.	FILING DATE		FIRST NAMED INVENTOR		ATTORNEY DOCKET NO. CONFIRMA		
14/105,811	12/13/2013		WEI-YU CHEN		14970-94702	5836	
TITLE OF INVENTION	: IMAGE CAPTURING	LENS SYSTEM, IMAG	ING DEVICE AND MOB	ILE TERMINAL			
		· · · · · · · · · · · · · · · · · · ·	·				
APPLN. TYPE	ENTITY STATUS	ISSUE FEE DUE	PUBLICATION FEE DUE		FEE TOTAL FEE(S) DUE	DATE DUE	
nonprovisional	UNDISCOUNTED	\$960	\$0	\$0	\$960	04/27/2015	
EXAM	IINER	ART UNIT	CLASS-SUBCLASS				
DINH,	JACK	2872	359-779000				
1. Change of correspond	ence address or indicatio	n of "Fee Address" (37	2. For printing on the p	atent front page, list			
CFR 1.363). Change of correspondence address (or Change of Correspondence Address form PTO/SB/122) attached.			(1) The names of up to or agents OR, alternativ	3 registered patent	attorneys 1		
					member a 2		
Tee Address" indication (or "Fee Address" Indication form PTO/SB/47; Rev 03-02 or more recent) attached. Use of a Customer			(2) The name of a single registered attorney or a 2 registered patent attor	gent) and the name rnevs or agents. If n	s of up to o name is 3		
Number is required.	2 of more recent) utuen	cu. ese or a customer	listed, no name will be	printed.	5 5		
			THE PATENT (print or typ	<i>,</i>			
PLEASE NOTE: Un recordation as set fort	less an assignee is ident h in 37 CFR 3.11. Com	ified below, no assignee pletion of this form is NO	data will appear on the pa T a substitute for filing an a	atent. If an assigne assignment.	e is identified below, the d	ocument has been filed for	
(A) NAME OF ASSI			(B) RESIDENCE: (CITY				
			_	_		_	
Please check the appropr	iate assignee category or	categories (will not be pr	rinted on the patent):	Individual 🖵 Cor	poration or other private gr	oup entity 🔲 Government	
4a. The following fee(s)	are submitted:	41	D. Payment of Fee(s): (Plea	se first reapply any	y previously paid issue fee	shown above)	
Issue Fee			A check is enclosed.				
	No small entity discount j		Payment by credit car			Gologowa and dita and	
Advance Order - #	t of Copies		The director is hereby authorized to charge the required fee(s), any deficiency, or credits any overpayment, to Deposit Account Number (enclose an extra copy of this form).				
5. Change in Entity Sta	tus (from status indicate	d above)					
	ng micro entity status. Se		NOTE: Absent a valid ce	rtification of Micro	Entity Status (see forms PT	O/SB/15A and 15B), issue	
					Entity Status (see forms PT ot be accepted at the risk of		
	g small entity status. See		to be a notification of loss	s of entitlement to m	er micro entity status, check iicro entity status.	ing this box will be taken	
Applicant changin	g to regular undiscounte	d fee status.	<u>NOTE:</u> Checking this boy entity status, as applicable		a notification of loss of ent	tlement to small or micro	
NOTE: This form must b	e signed in accordance v	with 37 CFR 1.31 and 1.33	3. See 37 CFR 1.4 for signa	ature requirements a	nd certifications.		
Authorized Signature				Date			
Typed or printed name				Registration No)		
			Page 2 of 3		AOET, I	Ex. 1002	
			1 age 2 01 5		,	2n = 200	

PTOL-85 Part B (10-13) Approved for use through 10/31/2013.

OMB 0651-0033

U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE

UNITED STATES PATENT AND TRADEMARK OFFICE United States Patent and Trademark Office Address: COMMISSIONER FOR PATENTS P.O. Box 1450 Alexandria, Virginia 22313-1450 www.uspto.gov							
APPLICATION NO.	FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.			
14/105,811	12/13/2013	WEI-YU CHEN	14970-94702	5836			
24728 75	90 01/27/2015		EXAM	IINER			
	ING MARTIN LLP		DINH,	JACK			
IP Department 3343 PEACHTRE	E ROAD, NE		ART UNIT	PAPER NUMBER			
	FINANCIAL CENTER	2872					
ATLANTA, GA 30	<i>J</i> 320		DATE MAILED: 01/27/201	5			

Determination of Patent Term Adjustment under 35 U.S.C. 154 (b)

(Applications filed on or after May 29, 2000)

The Office has discontinued providing a Patent Term Adjustment (PTA) calculation with the Notice of Allowance.

Section 1(h)(2) of the AIA Technical Corrections Act amended 35 U.S.C. 154(b)(3)(B)(i) to eliminate the requirement that the Office provide a patent term adjustment determination with the notice of allowance. See Revisions to Patent Term Adjustment, 78 Fed. Reg. 19416, 19417 (Apr. 1, 2013). Therefore, the Office is no longer providing an initial patent term adjustment determination with the notice of allowance. The Office will continue to provide a patent term adjustment determination with the Issue Notification Letter that is mailed to applicant approximately three weeks prior to the issue date of the patent, and will include the patent term adjustment on the patent. Any request for reconsideration of the patent term adjustment determination (or reinstatement of patent term adjustment) should follow the process outlined in 37 CFR 1.705.

Any questions regarding the Patent Term Extension or Adjustment determination should be directed to the Office of Patent Legal Administration at (571)-272-7702. Questions relating to issue and publication fee payments should be directed to the Customer Service Center of the Office of Patent Publication at 1-(888)-786-0101 or (571)-272-4200.

OMB Clearance and PRA Burden Statement for PTOL-85 Part B

The Paperwork Reduction Act (PRA) of 1995 requires Federal agencies to obtain Office of Management and Budget approval before requesting most types of information from the public. When OMB approves an agency request to collect information from the public, OMB (i) provides a valid OMB Control Number and expiration date for the agency to display on the instrument that will be used to collect the information and (ii) requires the agency to inform the public about the OMB Control Number's legal significance in accordance with 5 CFR 1320.5(b).

The information collected by PTOL-85 Part B is required by 37 CFR 1.311. The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 12 minutes to complete, including gathering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, Virginia 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, Virginia 22313-1450. Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

Privacy Act Statement

The Privacy Act of 1974 (P.L. 93-579) requires that you be given certain information in connection with your submission of the attached form related to a patent application or patent. Accordingly, pursuant to the requirements of the Act, please be advised that: (1) the general authority for the collection of this information is 35 U.S.C. 2(b)(2); (2) furnishing of the information solicited is voluntary; and (3) the principal purpose for which the information is used by the U.S. Patent and Trademark Office is to process and/or examine your submission related to a patent application or patent. If you do not furnish the requested information, the U.S. Patent and Trademark Office may not be able to process and/or examine your submission, which may result in termination of proceedings or abandonment of the application or expiration of the patent.

The information provided by you in this form will be subject to the following routine uses:

- 1. The information on this form will be treated confidentially to the extent allowed under the Freedom of Information Act (5 U.S.C. 552) and the Privacy Act (5 U.S.C 552a). Records from this system of records may be disclosed to the Department of Justice to determine whether disclosure of these records is required by the Freedom of Information Act.
- 2. A record from this system of records may be disclosed, as a routine use, in the course of presenting evidence to a court, magistrate, or administrative tribunal, including disclosures to opposing counsel in the course of settlement negotiations.
- 3. A record in this system of records may be disclosed, as a routine use, to a Member of Congress submitting a request involving an individual, to whom the record pertains, when the individual has requested assistance from the Member with respect to the subject matter of the record.
- 4. A record in this system of records may be disclosed, as a routine use, to a contractor of the Agency having need for the information in order to perform a contract. Recipients of information shall be required to comply with the requirements of the Privacy Act of 1974, as amended, pursuant to 5 U.S.C. 552a(m).
- 5. A record related to an International Application filed under the Patent Cooperation Treaty in this system of records may be disclosed, as a routine use, to the International Bureau of the World Intellectual Property Organization, pursuant to the Patent Cooperation Treaty.
- 6. A record in this system of records may be disclosed, as a routine use, to another federal agency for purposes of National Security review (35 U.S.C. 181) and for review pursuant to the Atomic Energy Act (42 U.S.C. 218(c)).
- 7. A record from this system of records may be disclosed, as a routine use, to the Administrator, General Services, or his/her designee, during an inspection of records conducted by GSA as part of that agency's responsibility to recommend improvements in records management practices and programs, under authority of 44 U.S.C. 2904 and 2906. Such disclosure shall be made in accordance with the GSA regulations governing inspection of records for this purpose, and any other relevant (i.e., GSA or Commerce) directive. Such disclosure shall not be used to make determinations about individuals.
- 8. A record from this system of records may be disclosed, as a routine use, to the public after either publication of the application pursuant to 35 U.S.C. 122(b) or issuance of a patent pursuant to 35 U.S.C. 151. Further, a record may be disclosed, subject to the limitations of 37 CFR 1.14, as a routine use, to the public if the record was filed in an application which became abandoned or in which the proceedings were terminated and which application is referenced by either a published application, an application open to public inspection or an issued patent.
- 9. A record from this system of records may be disclosed, as a routine use, to a Federal, State, or local law enforcement agency, if the USPTO becomes aware of a violation or potential violation of law or regulation. AOET, Ex. 1002

	Application No. 14/105,811		Applicant(s) CHEN, WEI-YU			
Notice of Allowability	Examiner	Art Unit	AIA (First Inventor to			
······································	JACK DINH	2872	File) Status Yes			
The MAILING DATE of this communication app All claims being allowable, PROSECUTION ON THE MERITS IS herewith (or previously mailed), a Notice of Allowance (PTOL-85 NOTICE OF ALLOWABILITY IS NOT A GRANT OF PATENT F of the Office or upon petition by the applicant. See 37 CFR 1.31	6 (OR REMAINS) CLOSED in) or other appropriate communities RIGHTS. This application is set to the set of t	n this application. If no unication will be mailed	it included I in due course. THIS			
1. X This communication is responsive to the communication fill	ed on 12/01/14.					
A declaration(s)/affidavit(s) under 37 CFR 1.130(b) wa	s/were filed on <u> </u>					
2. An election was made by the applicant in response to a response to a requirement and election have been incorporated into this a		during the interview o	n; the restriction			
 3. A The allowed claim(s) is/are <u>1-26</u>. As a result of the allowed Highway program at a participating intellectual property off <u>http://www.uspto.gov/patents/init_events/pph/index.jsp</u> or s 	ice for the corresponding ap	plication. For more info				
4. Acknowledgment is made of a claim for foreign priority und	er 35 U.S.C. § 119(a)-(d) or	(f).				
a) ⊠ All b) □ Some *c) □ None of the:						
1. Certified copies of the priority documents hav	e been received.					
2. Certified copies of the priority documents hav		on No				
3. 🔲 Copies of the certified copies of the priority do	ocuments have been receive	d in this national stage	application from the			
International Bureau (PCT Rule 17.2(a)).						
* Certified copies not received:						
Applicant has THREE MONTHS FROM THE "MAILING DATE" noted below. Failure to timely comply will result in ABANDON THIS THREE-MONTH PERIOD IS NOT EXTENDABLE.	MENT of this application.	a reply complying wit	h the requirements			
5. CORRECTED DRAWINGS (as "replacement sheets") mus	st be submitted.					
including changes required by the attached Examiner Paper No./Mail Date	's Amendment / Comment or	in the Office action of				
Identifying indicia such as the application number (see 37 CFR each sheet. Replacement sheet(s) should be labeled as such in			(not the back) of			
6. DEPOSIT OF and/or INFORMATION about the deposit of attached Examiner's comment regarding REQUIREMENT F			the			
Attachment(s)						
1. I Notice of References Cited (PTO-892)	5. 🗌 Examiner's	Amendment/Comme	nt			
2. Information Disclosure Statements (PTO/SB/08), Paper No./Mail Date 20141201	6. 🛛 Examiner's	Statement of Reason	s for Allowance			
 3. Examiner's Comment Regarding Requirement for Deposit of Biological Material 	7. 🗌 Other	·				
4. ☐ Interview Summary (PTO-413), Paper No./Mail Date						
/JACK DINH/						
Primary Examiner, Art Unit 2872						
LLS. Patent and Trademark Office						

REASONS FOR ALLOWANCE

 Claims 1-26 are allowed. The following is an examiner's statement of reasons for allowance. Regarding claims 1, 15 and 21, the prior art fails to satisfy the conditions as claimed.

2. The prior art taken either singly or in combination fails to anticipate or fairly suggest the limitations of the independent claims, in such a manner that a rejection under 35 USC 102 or 103 would be improper. Any comments considered necessary by applicant must be submitted no later than the payment of the issue fee and, to avoid processing delays, should preferably accompany the issue fee. Such submissions should be clearly labeled "Comments on Statement of Reasons for Allowance."

Other Information/Remarks

3. Any inquiry concerning this communication or earlier communications from the examiner should be directed to JACK DINH whose telephone number is (571)272-2327. The examiner can normally be reached on M-F (7:30 AM - 4:00 PM).

If attempts to reach the examiner by telephone are unsuccessful, the examiner's supervisor, Thomas K. Pham can be reached on 571-272-3689. The fax phone number for the organization where this application or proceeding is assigned is 571-273-8300.

Application/Control Number: 14/105,811 Art Unit: 2872

Information regarding the status of an application may be obtained from the Patent Application Information Retrieval (PAIR) system. Status information for published applications may be obtained from either Private PAIR or Public PAIR. Status information for unpublished applications is available through Private PAIR only. For more information about the PAIR system, see http://pair-direct.uspto.gov. Should you have questions on access to the Private PAIR system, contact the Electronic Business Center (EBC) at 866-217-9197 (toll-free). If you would like assistance from a USPTO Customer Service Representative or access to the automated information system, call 800-786-9199 (IN USA OR CANADA) or 571-272-1000.

/Jack Dinh/ Primary Examiner, Art Unit 2872 01/12/15

Application/Control No. Ap				Appli Reexa	Applicant(s)/Patent Under Reexamination										
Index of Claims				14105811				CHEN	CHEN, WEI-YU						
				Examiner				Art U	Art Unit						
					JACK DINH										
				II											
✓ Rejected -					Cancelled N Non-El			lected		Δ	A Appeal				
										· • • •					
= A	= Allowed		÷	F	Restricted		Ι	Interference			0	Objected			
☐ Claims renumbered in the same order as presented by					s presented by a	applica	ant		CPA T.D.).	🗌 R.1.47		
CLA	MIM							DATE							
Final	Original	01/12/2	2015												
1	1	=													
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Part of Paper No.: 20150112

EAST Search History

EAST Search History (Prior Art)

Ref #	Hits	Search Query	DBs	Default Operator	Plurals	Time Stamp
L1	0	"14105811"	US-PGPUB; USPAT	OR	OFF	2015/01/12 06:50
L2	1	("8842379").PN.	USPAT; USOCR	OR	OFF	2015/01/12 07:09
L3	2	"20100165485"	US-PGPUB; USPAT	OR	OFF	2015/01/12 07:12
L4	10323	lens\$2 same (first) same (second near6 positive) same (third near6 negative) same (fourth)	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L5	396	(359/771).CCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L6	308	(359/772).CCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L7	186	(359/779).CCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L8	284	(359/781).CCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:15
L9	1059	(359/771,772,779,781).OOLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:16
L10	265	L9 and L4	US-PGPUB; USPAT;	OR	OFF	2015/01/12 07:16

AOET, Ex. 1002

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			USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB			
L11	636	lens\$2 same (first) same ((second near6 positive) with convex with image) same ((third near6 negative) with concave with object with convex with image) same (fourth with concave with image)	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18
L12	889	(359/715).COLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18
L13	1714	(359/715,771,772,779,781).CCLS.	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18
L14	86	L11 and L13	US-PGPUB; USPAT; USOCR; FPRS; EPO; JPO; DERWENT; IBM_TDB	OR	OFF	2015/01/12 07:18

EAST Search History (Interference)

Ref #	Hits	Search Query	DBs	Default Operator	Plurals	Time Stamp
L15		(lens\$2 and (first) and ((second near6 positive) with convex with image) and ((third near6 negative) with concave with object with convex with image) and (fourth with concave with image)).clm.	PGPUB;	OR	1 .	2015/01/12 07:30
L16		(lens\$2 and (first) and ((second near6 positive) with convex with image) and ((third near6 negative) with concave with object with convex with image) and (fourth with concave with image) and Td and HFOV).clm.	PGPUB;	OR	OFF	2015/01/12 07:30

1/ 12/ 2015 7:31:07 AM C:\ Users\ jdinh\ Documents\ EAST\ Workspaces\ Case 14105811.wsp

	Application/Control No.	Applicant(s)/Patent Under Reexamination
Search Notes	14105811	CHEN, WEI-YU
	Examiner	Art Unit
	JACK DINH	2872

CPC- SEARCHED		
Symbol	Date	Examiner

CPC COMBINATION SETS - SEARCHED				
Symbol	Date	Examiner		

US CLASSIFICATION SEARCHED							
Class Subclass Date Examiner							
359	771,772,779,781,715	01/12/15	JD				

SEARCH NOTES					
Search Notes	Date	Examiner			
Search EAST and NPL.	01/12/15	JD			

INTERFERENCE SEARCH							
US Class/ CPC Symbol	US Subclass / CPC Group	Date	Examiner				
See search history.		01/12/15	JD				



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BIB DATA SHEET

CONFIRMATION NO. 5836

	SERIAL NUMBER FILING OF			CLASS	GR	OUP ART	UNIT	ATTORNEY DOCKET NO.	
14/105,81	1	12/13/2013		359		2872		14970-94702	
		RULE							
APPLICANTS LARGAN	-	SION CO., LTD., Taich	nung, T A	NWAN, Assigne	e (wit	th 37 CFF	R 1.172	Interes	st);
INVENTORS WEI-YU CHEN, Taichung, TAIWAN;									
** CONTINUING	G DATA	/ *******	*						
		TIONS ************************************	******						
** IF REQUIRE 01/02/201		EIGN FILING LICENS	E GRAN	NTED **					
Foreign Priority claime 35 USC 119(a-d) cond		Yes No Yes No Met af Allowa	fter	STATE OR COUNTRY		IEETS WINGS	TOT CLAI		INDEPENDENT CLAIMS
	JACK DIN Examiner's	H/		TAIWAN		23 26		6	3
IP Depart 3343 PEA 1600 ATL ATLANTA UNITED S	ADDRESS MORRIS MANNING MARTIN LLP IP Department 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER ATLANTA, GA 30326 UNITED STATES								
TITLE									
IMAGE C	APTUR	ING LENS SYSTEM, I	MAGIN	G DEVICE AND) MOE		MINAL		
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		for following				🖵 1.18 F	Fees (Iss	sue)	
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	Application/Control No.	Applicant(s)/Patent Under Reexamination
Issue Classification	14105811	CHEN, WEI-YU
	Examiner	Art Unit
	JACK DINH	2872

Symbol				Туре			
G02B	13		004	F	2013-01-01		
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Symbol	Туре	Set	Ranking	Version				

NONE		Total Claims Allowed:	
(Assistant Examiner)	(Date)	2	6
/JACK DINH/ Primary Examiner.Art Unit 2872	01/12/2015	O.G. Print Claim(s)	O.G. Print Figure
(Primary Examiner)	(Date)	1	1A
U.S. Patent and Trademark Office		Pa	rt of Paper No. 20150112

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Page 220

	Application/Control No.	Applicant(s)/Patent Under Reexamination
Issue Classification	14105811	CHEN, WEI-YU
	Examiner	Art Unit
	JACK DINH	2872

	US OR	RIGINAL CL	ASSIFIC	ATION						INTERNATIONAL	CLA	SSI	FIC	ATI	ON
	CLASS			SUBCLASS			CLAIMED NON-CLAIMED							CLAIMED	
359			779			G	0	2	В	9 / 34 (2006.0)					
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CLASS	SUE	BCLASS (ONE	SUBCLAS	S PER BLO	CK)										
359	781	715													

NONE		Total Claims Allowed:		
(Assistant Examiner)	(Date)	26		
/JACK DINH/ Primary Examiner.Art Unit 2872	01/12/2015	O.G. Print Claim(s)	O.G. Print Figure	
(Primary Examiner)	(Date)	1	1A	

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Part of Paper No. 20150112

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Page 221

	Application/Control No.	Applicant(s)/Patent Under Reexamination
Issue Classification	14105811	CHEN, WEI-YU
	Examiner	Art Unit
	JACK DINH	2872

	Claims renumbered in the same order as presented by applicant				r as prese	ented by a	applicant		CP] T.D.	۵] R.1.	47	
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NONE		Total Claims Allowed:		
(Assistant Examiner)	(Date)	26		
/JACK DINH/ Primary Examiner.Art Unit 2872	01/12/2015	O.G. Print Claim(s)	O.G. Print Figure	
(Primary Examiner)	(Date)	1	1A	
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Page 222

Doc description: Information Disclosure Statement (IDS) Filed

14105811 - GAL :: 2872

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INFORMATION DISCLOSURE STATEMENT BY APPLICANT (Not for submission under 37 CFR 1.99)

Application Number		14105811
Filing Date		2013-12-13
First Named Inventor	WEI-1	/U CHEN
Art Unit		2872
Examiner Name		
Attorney Docket Number		14970-94702

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Examiner Initial*	Cite No	Pa	atent Number	Kind Code ¹	Issue D)ate	Name of Patentee or Applicant of cited Document		Pages,Columns,Lines when Relevant Passages or Relev Figures Appear		
	1	88	42379	B2	2014-09	9-23	Largan Precision Co., Ltd.				
If you wisl	h to ao	dd ac	lditional U.S. Pate	nt citatio	n inform	ation pl	ease click the	Add button.		Add	
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	1		20100165485	A1	2010-07	/-01	Milestone Co., Ltd.				
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Examiner Initial*	Cite No		eign Document nber³	Country Code ²		Kind Code⁴	Publication Date	Name of Patentee Applicant of cited Document	e or	Pages,Columns,Lines where Relevant Passages or Relevant Figures Appear	T 5
	1	201	4-178623	JP			2014-09-25	Hitachi Maxell, Ltd.			×
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14105811 - GAU: 2872 Receipt date: 12/01/2014 Application Number 14105811 Filing Date 2013-12-13 **INFORMATION DISCLOSURE** First Named Inventor WEI-YU CHEN STATEMENT BY APPLICANT 2872 Art Unit (Not for submission under 37 CFR 1.99) **Examiner Name** Attorney Docket Number 14970-94702

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If you wish to	add ad	ditional non-patent literatu	re document citation information p	lease click the Add I	outton Add	<u> </u>
			EXAMINER SIGNATURE			
Examiner Sig	gnature	/Jack Dinh/		Date Considered	01/12/2015	
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Standard ST.3).	³ For Jap ent by the	anese patent documents, the in- appropriate symbols as indicate	<u>SPTO.GOV</u> or MPEP 901.04. ² Enter offic dication of the year of the reign of the Empe d on the document under WIPO Standard s	eror must precede the set	rial number of the patent doo	cument.

Receipt date: 12/01/2014 14105811 - GAU: 2872 Application Number 14105811 Filing Date 2013-12-13 INFORMATION DISCLOSURE First Named Inventor WEI-YU CHEN STATEMENT BY APPLICANT 2872 Art Unit (Not for submission under 37 CFR 1.99) Examiner Name Attorney Docket Number 14970-94702

CERTIFICATION STATEMENT

Please see 37 CFR 1.97 and 1.98 to make the appropriate selection(s):

That each item of information contained in the information disclosure statement was first cited in any communication from a foreign patent office in a counterpart foreign application not more than three months prior to the filing of the information disclosure statement. See 37 CFR 1.97(e)(1).

OR

That no item of information contained in the information disclosure statement was cited in a communication from a foreign patent office in a counterpart foreign application, and, to the knowledge of the person signing the certification after making reasonable inquiry, no item of information contained in the information disclosure statement was known to any individual designated in 37 CFR 1.56(c) more than three months prior to the filing of the information disclosure statement. See 37 CFR 1.97(e)(2).

See attached certification statement.

The fee set forth in 37 CFR 1.17 (p) has been submitted herewith.

X A certification statement is not submitted herewith.

SIGNATURE

A signature of the applicant or representative is required in accordance with CFR 1.33, 10.18. Please see CFR 1.4(d) for the form of the signature.

Signature	/Tim Tingkang Xia/	Date (YYYY-MM-DD)	2014-12-01
Name/Print	Tim Tingkang Xia	Registration Number	45242

This collection of information is required by 37 CFR 1.97 and 1.98. The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 1 hour to complete, including gathering, preparing and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. **SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450**.

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The information provided by you in this form will be subject to the following routine uses:

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- 3. A record in this system of records may be disclosed, as a routine use, to a Member of Congress submitting a request involving an individual, to whom the record pertains, when the individual has requested assistance from the Member with respect to the subject matter of the record.
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- 7. A record from this system of records may be disclosed, as a routine use, to the Administrator, General Services, or his/her designee, during an inspection of records conducted by GSA as part of that agency's responsibility to recommend improvements in records management practices and programs, under authority of 44 U.S.C. 2904 and 2906. Such disclosure shall be made in accordance with the GSA regulations governing inspection of records for this purpose, and any other relevant (i.e., GSA or Commerce) directive. Such disclosure shall not be used to make determinations about individuals.
- 8. A record from this system of records may be disclosed, as a routine use, to the public after either publication of the application pursuant to 35 U.S.C. 122(b) or issuance of a patent pursuant to 35 U.S.C. 151. Further, a record may be disclosed, subject to the limitations of 37 CFR 1.14, as a routine use, to the public if the record was filed in an application which became abandoned or in which the proceedings were terminated and which application is referenced by either a published application, an application open to public inspections or an issued patent.
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(Depositor's name)
(Signature)
(Date)

APPLICATION NO.	FILING DATE		FIRST NAMED INVENTOR		TORNEY DOCKET NO.	CONFIRMATION NO.		
14/105,811	12/13/2013	•	WEI-YU CHEN		14970-94702	5836		
TITLE OF INVENTION	N: IMAGE CAPTURING	LENS SYSTEM, IMAC	FING DEVICE AND MOB	ILE TERMINAL				
APPLN. TYPE	ENTITY STATUS	ISSUE FEE DUE	PUBLICATION FEE DUE	PREV. PAID ISSUE FR	EE TOTAL FEE(S) DUE	DATE DUE		
nonprovisional	UNDISCOUNTED	\$960	\$0	\$0	\$960	04/27/2015		
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DINH	, JACK	2872	359-779000	•				
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_			(2) The name of a single registered attorney or a 2 registered patent atto	le firm (having as a me agent) and the names of	$\frac{2 \text{ IIM IINC}}{2 \text{ of up to}}$	KANG XIA, ESQ		
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(A) NAME OF ASSI			(B) RESIDENCE: (CITY					
LARGAN PREC	ISION CO., LTD.		TAICHUNG, TW					
Please check the appropriate	riate assignee category or	r categories (will not be p	rinted on the patent):	Individual 🖾 Corpo	pration or other private gro	oup entity 🔲 Government		
4a. The following fee(s)	are submitted:	4	b. Payment of Fee(s): (Ple a	ise first reapply any p	oreviously paid issue fee	shown above)		
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Applicant certifyi	ng micro entity status. Se	ee 37 CFR 1.29	<u>NOTE:</u> Absent a valid ce fee payment in the micro	rtification of Micro En entity amount will not	tity Status (see forms PT be accepted at the risk of	D/SB/15A and 15B), issue application abandonment.		
Applicant assertin	ng small entity status. See	e 37 CFR 1.27	<u>NOTE:</u> If the application was previously under micro entity status, checking this box will be taken to be a notification of loss of entitlement to micro entity status.					
Applicant changing to regular undiscounted fee status.			<u>NOTE:</u> Checking this box will be taken to be a notification of loss of entitlement to small or micro entity status, as applicable.					
NOTE: This form must	be signed in accordance v	with 37 CFR 1.31 and 1.3	3. See 37 CFR 1.4 for signa	ature requirements and	certifications.			
Authorized Signature	e <u>/Tim Tingkang Xia/</u>	,		Date FEBRU	ARY 5, 2015			
	ne TIM TINGKANC			Registration No.	,			
Typed or printed nam				Registration No.				
			Page 2 of 3		AOET, I			
PTOL-85 Part B (10-13)) Approved for use throug	gh 10/31/2013.	OMB 0651-0033 U	J.S. Patent and Tradem	hark Office; U.S. DEPAR	Page 227		

PTOL-85 Part B (10-13) Approved for use through 10/31/2013.

Electronic Patent Application Fee Transmittal								
Application Number:	14105811							
Filing Date:	13-	13-Dec-2013						
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMIN) MOBILE TERMINAL			
First Named Inventor/Applicant Name:	WEI-YU CHEN							
Filer:	Tim Tingkang Xia/Michelle Ellis							
Attorney Docket Number:	149	970-94702						
Filed as Large Entity								
Filing Fees for Utility under 35 USC 111(a)								
Description		Fee Code	Quantity	Amount	Sub-Total in USD(\$)			
Basic Filing:								
Pages:								
Claims:								
Miscellaneous-Filing:								
Petition:								
Patent-Appeals-and-Interference:								
Post-Allowance-and-Post-Issuance:								
Utility Appl Issue Fee		1501	1	960	960			

Description	Fee Code	Quantity	Amount	Sub-Total in USD(\$)
Extension-of-Time:				
Miscellaneous:				
	Tot	al in USD	(\$)	960

Electronic Ac	cknowledgement Receipt
EFS ID:	21413714
Application Number:	14105811
International Application Number:	
Confirmation Number:	5836
Title of Invention:	IMAGE CAPTURING LENS SYSTEM, IMAGING DEVICE AND MOBILE TERMINAL
First Named Inventor/Applicant Name:	WEI-YU CHEN
Customer Number:	24728
Filer:	Tim Tingkang Xia/Michelle Ellis
Filer Authorized By:	Tim Tingkang Xia
Attorney Docket Number:	14970-94702
Receipt Date:	05-FEB-2015
Filing Date:	13-DEC-2013
Time Stamp:	16:13:28
Application Type:	Utility under 35 USC 111(a)

Payment information:

Submitted with Payment	yes					
Payment Type	Deposit Account					
Payment was successfully received in RAM	\$960					
RAM confirmation Number	2937					
Deposit Account	503537					
Authorized User						
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1	Issue Fee Payment (PTO-85B)	1497094702IFTrans.pdf	1099156	no	1
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INFORMATION DISCLOSURE
STATEMENT BY APPLICANT
(Not for submission under 37 CFR 1.99)Application Number14105811First Named Inventor2013-12-13First Named InventorWEI-YU CHENArt Unit2872Examiner Name(hence (a) endiedAttorney Docket Number(hence (a) endied14970-94702

<u>Change(s)</u> applied

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APPLICATION NO.	ISSUE DATE	PATENT NO.	ATTORNEY DOCKET NO.	CONFIRMATION NO.
14/105,811	03/24/2015	8988796	14970-94702	5836

24728 7590 03/04/2015 MORRIS MANNING MARTIN LLP IP Department 3343 PEACHTREE ROAD, NE 1600 ATLANTA FINANCIAL CENTER

ATLANTA, GA 30326

ISSUE NOTIFICATION

The projected patent number and issue date are specified above.

Determination of Patent Term Adjustment under 35 U.S.C. 154 (b)

(application filed on or after May 29, 2000)

The Patent Term Adjustment is 0 day(s). Any patent to issue from the above-identified application will include an indication of the adjustment on the front page.

If a Continued Prosecution Application (CPA) was filed in the above-identified application, the filing date that determines Patent Term Adjustment is the filing date of the most recent CPA.

Applicant will be able to obtain more detailed information by accessing the Patent Application Information Retrieval (PAIR) WEB site (http://pair.uspto.gov).

Any questions regarding the Patent Term Extension or Adjustment determination should be directed to the Office of Patent Legal Administration at (571)-272-7702. Questions relating to issue and publication fee payments should be directed to the Application Assistance Unit (AAU) of the Office of Data Management (ODM) at (571)-272-4200.

APPLICANT(s) (Please see PAIR WEB site http://pair.uspto.gov for additional applicants):

LARGAN PRECISION CO., LTD., Taichung, TAIWAN, Assignee (with 37 CFR 1.172 Interest); WEI-YU CHEN, Taichung, TAIWAN;

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IR103 (Rev. 10/09)