



LIBRARY OF CONGRESS

Office of Business Enterprises
Duplication Services Section

THIS IS TO CERTIFY that the collections of the Library of Congress contain a journal entitled **MICROWAVE AND OPTICAL TECHNOLOGY LETTERS**, call number "TK 7876.M5235," and that the following pages— the binding cover page, title page from Volume 11/Number 2, February 5, 1996, publisher page, page 55 with Library of Congress Copyright stamp, and pages 66 through-69 - are a true and accurate representation from that work.

THIS IS TO CERTIFY FURTHER, that work is marked with a Library of Congress Copyright Office stamp dated January 29, 1996.

IN WITNESS WHEREOF, the seal of the Library of Congress is affixed hereto on July 18, 2018.

Deirdre Scott
Business Enterprises Officer
Office of Business Enterprises
Library of Congress



LIBRARY OF CONGRESS
0 033 225 113 2

MICROWAVE AND OPTICAL TECHNOLOGY LETTERS 11 1996

TK 7876
.M5235



MICROWAVE AND OPTICAL TECHNOLOGY LETTERS

VOLUME 11 / NUMBER 2

FEBRUARY 5 1996

The Resonant Frequency of Rectangular Microstrip Antenna Elements with Various Substrate Thicknesses, 55-59

M. Karu

Microstrip Notched-Sectorial Power Combiner with Improved Isolation, 59-61

S. P. Yeo, M. S. Leong, P. S. Kooi, T. S. Yeo, and X. D. Zhou

Gaussian-Mode Radius Polynomials for Modeling Doped Fiber Amplifiers and Lasers, 61-64

P. Mysliński and J. Christowski

Computing the Quality Factor of Resonators Using the Finite-Difference-Time-Domain Algorithms, 64-66

P. H. Hurm, Y. Shinoy, and R. Mitra

Experimental Investigations on the Impedance and Radiation Properties of a Three-Element Concentric Microstrip Square-Ring Antenna, 66-69

I. Nalla Mitra and S. K. Chowdhury

Radiation Behavior of Planar Double-Layer Dielectric Waveguides Combined with a Finite Metal-Strip Grating, 69-73

V. I. Kalinichev

Rayleigh Formula for Bim isotropic Mixtures, 73-75

A. Sihvola

Wire Antenna Array Analysis, 75-78

Ph. Gouret, A. Shanuba, C. Terret, and A. Skrivervik

The Mueller Scattering Matrix of Two Parallel Chiral Circular Cylinders, 78-83

Y. Wengyan

A Single-Layer Dual-Frequency Rectangular Microstrip Patch Antenna Using a Single Probe Feed, 83-84

J. Chen and K. Wong

An Experimental Study on the Electroacoustic Effect on the Radiation Efficiency of a Ferrite-Based Annular Ring Microstrip Antenna, 84-87

S. S. Pattnaik and S. Devi

Novel Design of Low-Loss Wide-Angle Symmetric Y-Branch Waveguides, 87-89

H. P. Chan, S. Y. Cheng, and P. S. Chung

Optical Implementation and Routing Technique for a SW-Banyan Network, 90-93

H. Peng, L. Liu, and F. Wang

Tapered Optical-Fiber Temperature Sensor, 93-95

P. Datta, I. Matias, C. Aramburu, A. Bakas, M. López-Arno, and J. M. Oñón

S-Parameter Extraction of Transistors Under Class-C Bias, 95-98

K. F. Tsang, G. B. Morgan, and P. C. L. Yip

Excitation of Magnetostatic Waves in Ferromagnetic Films by Various Sources, 99-102

E. O. Kamenevskii

On the Technology of Making Chiral and Bim isotropic Waveguides for Microwave Propagation, 103-107

E. O. Kamenevskii

Collective Scattering Effects of Trees Generated by Stochastic Lindenmayer Systems, 107-111

G. Zhang, L. Tsang, and Z. Chen



A WILEY-INTERSCIENCE PUBLICATION

John Wiley & Sons, Inc.

NEW YORK • CHICHESTER • BRISBANE • TORONTO • SINGAPORE

ISSN 0895-2477

MOJL 11(2) 55-111 (1996)



MICROWAVE AND OPTICAL TECHNOLOGY LETTERS

VOLUME 11 / NUMBER 2 FEBRUARY 5 1996

EDITOR
Kal Chang

Texas A&M University
College Station
Texas

EDITORIAL BOARD

K. K. Agarwal, E-Systems, USA
J. Archer, CSIRO, Australia

I. J. Bahl, IIT, USA

P. Bernardi, University of Rome, Italy

K. B. Bhasin, NASA Lewis Research Center, USA

K. J. Button, MIT National Magnet Labs, USA

H. J. Caulfield, Alabama A & M University, USA

J. Chrostowski, National Research Council, Canada

R. A. Cryan, University of Northumbria, UK

A. A. de Salles, CETUC-PUC, Brazil

U. Efron, Hughes Research Labs, USA

M. Ettenberg, David Sarnoff Research Center, USA

H. R. Fetterman, UCLA, USA

L. Figueroa, Boeing Co., USA

T. K. Findakly, Hoechst Celanese Corp., USA

T. T. Fong, Hughes Aircraft Co., USA

N. N. Pomin, Moscow Technical University, Russia

V. Fouad Hanna, CNET PAB / STS, France

P. B. Gallion, ENST, France

F. Gardiol, École Polytechnique Federal, Switzerland

H. Ghafouri-Shiraz, University of Birmingham, England

J. Goel, TRW, USA

P. F. Goldsmith, Cornell University, USA

K. C. Gupta, University of Colorado, USA

G. I. Haddad, University of Michigan, USA

R. C. Hansen, Consultant, USA

A. Hardy, Tel Aviv University, Israel

P. R. Herzfeld, Drexel University, USA

W. J. R. Hofer, University of Victoria, Canada

M. Horno, University of Sevilla, Spain

H. C. Huang, Shanghai Science Technology University, China

C. Jackson, TRW, USA

R. Jansen, Industrial Microwave and RF Techniques Inc., Germany

S. Kawakami, Tohoku University, Japan

M. A. Karim, University of Dayton, USA

E. L. Kollberg, Chalmers University of Technology, Sweden

J. A. Kong, MIT, USA

Y. Konishi, Uniden Corporation, Japan

S. K. Koul, Indian Institute of Technology, India

H. J. Kuno, Hughes Aircraft Co., USA

C. H. Lee, University of Maryland, USA

J. N. Lee, Naval Research Labs, USA

R. Q. Lee, NASA Lewis Research Center, USA

S. W. Lee, University of Illinois, USA

T. Li, Bell Telephone Labs, USA

C. Lin, Bell Communication Research, USA

J. C. Lin, University of Illinois, USA

W. Lin, Chengdu Institute of Radio Engineering, China

H. Ling, University of Texas, USA

I. V. Lindell, Helsinki University of Technology, Helsinki, Finland

Y. T. Lo, University of Illinois, USA

J. M. McMahon, Naval Research Labs, USA

K. A. Michalski, Texas A & M University, USA

T. Midford, Hughes Aircraft Co., USA

J. W. Mink, North Carolina State University, USA

Y. Naito, Tokyo Institute of Technology, Japan

R. Nevels, Texas A & M University, USA

A. I. Nosich, National Academy Science, Ukraine

J. Ojeda-Castaneda, Instituto Nacional de Astrofísica, México

K. Peterman, Technical University, Berlin, Germany

J. Ra, KAIST, Korea

A. Rosen, David Sarnoff Research Center, USA

G. Salmer, Université des Sciences et Techniques de Lille-Flandres-Artois, France

F. K. Scherwing, US Army CECOM, USA

A. K. Sharma, TRW, USA

L. C. Shen, University of Houston, USA

D. W. Smith, British Telecom Research Labs, England

B. E. Spielman, Washington University in St. Louis, USA

C. Sun, California Polytechnic State University, USA

H. F. Taylor, Texas A & M University, USA

C. S. Tsai, University of California at Irvine, USA

H. G. Tseng, Texas Instruments, USA

J. B. Y. Tsui, Wright-Patterson AFB, USA

O. Wada, Fujitsu Labs, Japan

R. W. Wang, Academia Sinica, China

A. G. Williamson, University of Auckland, New Zealand

J. C. Wiltee, Georgia Technology Research Institute, USA

J. Wu, National Taiwan University, Taiwan

E. Yamashita, University of Electro-Communications, Japan

S. K. Yeo, Optech, USA

H. W. Yen, Hughes Research Labs, USA

F. T. S. Yu, Pennsylvania State University, USA

Microwave and Optical Technology Letters (ISSN: 0895-2477) is published monthly except semi-monthly in February, April, June, August, October, and December, three volumes per year by John Wiley & Sons, Inc., 605 Third Avenue, New York, NY 10158.

Copyright © 1996 John Wiley & Sons, Inc. All rights reserved. No part of this publication may be reproduced in any form or by any means, except as permitted under section 107 or 108 of the 1976 United States Copyright Act, without either the prior written permission of the publisher, or authorization through the Copyright Clearance Center, 222 Rosewood Drive, Danvers, MA 01923, (508) 750-8400, fax (508) 750-4470. Second-class postage paid at New York, NY, and at additional mailing offices.

This consent does not extend to other kinds of copying, such as copying for general distribution, for advertising or promotional purposes, for creating new collective works, or for resale. Such permission requests and other permission inquiries should be addressed to the publisher.

Aims and Scope

Microwave and Optical Technology Letters provides quick publication (3 to 6 month turnaround) of the most recent findings and achievements in high frequency technology, from RF to optical spectrum. The journal publishes original short papers and letters on theoretical, applied, and system results in the following areas:

RF, Microwave, and Millimeter Waves

Antennas and Propagation

Submillimeter-Wave and Infrared Technology

Optics

All papers are subject to peer review before publication.

Subscription price (Volumes 11 - 13, 1996): \$558.00 in US, \$738.00 in

Canada and Mexico, \$837.00 outside North America. All subscriptions outside US will be sent by air. Subscriptions at the personal rate are available only to individuals. Payment must be made in US dollars drawn on a US bank. Claims for undelivered copies will be accepted only after the following issue has been received. Please enclose a copy of the mailing label. Missing copies will be supplied when losses have been sustained in transit and where reserve stock permits. Please allow four weeks for processing a change of address. For subscription inquiries, please call 212-850-6645 or e-mail: SUBINFO@jwiley.com.

Advertising Sales: Inquiries concerning advertising should be forwarded to Roberta Frederick, Advertising Sales, John Wiley & Sons, 605 Third Ave., New York, NY 10158; (212) 850-8832. Advertising Sales, European Contact: Michael Levermore, Advertising Manager, John Wiley & Sons, Ltd., Baffins Lane, Chichester, Sussex PO19 1UD, England

Reprints: reprint sales and inquiries should be directed to the customer service dept., John Wiley & Sons, Inc., 605 Third Ave., New York, NY 10158. Telephone (212) 850-8776.

Postmaster: Send address changes to Susan Malawski, Director, Subscription Fulfillment and Distribution, Microwave and Optical Technology Letters, Subscription Department, John Wiley & Sons, Inc., 605 Third Ave., New York, NY 10158, (212) 850-6645.

Manuscripts should be submitted to the Editor, Professor Kal Chang, Electrical Engineering Department, Texas A & M University, College Station, Texas 77843-3128. Telephone (409) 845-5425.

Other correspondence should be addressed to: Microwave and Optical Technology Letters, Publisher, Interscience Division, Professional, Reference, & Trade Group, John Wiley & Sons, Inc., 605 Third Ave., New York, NY 10158.

This journal is printed on acid-free paper

THE RESONANT FREQUENCY OF RECTANGULAR MICROSTRIP ANTENNA ELEMENTS WITH VARIOUS SUBSTRATE THICKNESSES

Mehmet Kara

Weapons Systems Division
Aeronautical & Maritime Research Laboratory
Defence Science and Technology Organisation
P.O. Box 1500
Salisbury SA 5108, Australia



KEY TERMS

Resonant frequency, various substrate, patch antenna, microstrip

ABSTRACT

Formulas based on transmission-line, cavity, and magnetic-wall models to determine the resonant frequencies of a rectangular microstrip antenna element have been studied and their validity assessed. Their variations were experimentally verified by analyzing a set of newly designed antenna elements with substrates satisfying the criteria $h \leq 0.0815\lambda_0$ for $2.22 \leq \epsilon_r \leq 10.2$, where λ_0 is the free-space wavelength, h the thickness, and ϵ_r the relative permittivity of the dielectric substrate. © 1996 John Wiley & Sons, Inc.

1. INTRODUCTION

The resonant frequency of microstrip antenna elements must be determined accurately, as they have narrow bandwidth and can only operate effectively in the vicinity of the resonant frequency.

Factors for determining the frequency at which resonance occurs include

- The voltage standing-wave ratio (VSWR), referred to the input terminals of the antenna, is at a minimum. This corresponds to a minimum in the magnitude of the reflection coefficient.
- The input impedance, referred to the input terminals, is real ($Z_{in} = R_{in}$), which means the input impedance has no reactive part. Generally, this point is very close to the frequency where the resistance reaches a maximum. Therefore the resonant frequency may also be defined as the point at which the resistance reaches a maximum, independent of the value of reactance.

This article is primarily concerned with antenna elements that are matched to their transmission-line feeds. In this case, the frequency at which the input impedance is real is equal to the frequency at which the VSWR is at a minimum.

Several methods have been proposed and used to determine performance properties of microstrip antenna elements [1-17]. These methods have different levels of complexity, require vastly different computational efforts, and can generally be divided into two groups: simple analytical methods and rigorous numerical methods. Simple analytical methods can give a good intuitive explanation of antenna radiation properties. Exact mathematical formulations in rigorous methods involve extensive numerical procedures, resulting in round-off errors, and may also need final experimental adjustments to the theoretical results. They are also time consuming and not easily included in a computer-aided-design system. Basically, there is no clear-cut rule as to which one of these is the best to use; the first guideline would be the thickness of the substrate.

Based on this observation, simplified analytical methods are used in this work. Formulas based on transmission-line, cavity, and magnetic-wall models to determine the resonant frequencies of a rectangular microstrip antenna element have been investigated. Their respective regions of validity in theory and applicability for a given antenna element have also been established. For the above-specified range of substrates, a transmission line model has been verified and successfully used to calculate the resonant frequencies of rectangular microstrip antenna elements without involving complicated, time-consuming, and difficult numerical methods. These results are then compared with specified design frequencies.

2. ANALYSIS

The configuration of a probe-fed rectangular microstrip antenna element is shown in Figure 1. The transmission-line [1-4], the cavity [5-10], and the magnetic-wall models [11] have been used for calculating the resonant frequencies, and there have been variations compared with measurements.

The basic formulas for computing the resonant frequencies are given in the following sections.

2.1. Formulas Based on the Transmission-Line Model. To calculate the resonant frequency of a rectangular microstrip antenna element, the antenna is regarded as two parallel radiating slots [3] with dimensions W and h having constant field aperture distributions and separated by the element length L of approximately half the wavelength in the dielectric.

In reality the electric field at the open end of the patch is distorted by an abrupt termination at the edges, resulting in fringing electric fields. This fringing effect is incorporated into the formula for the resonant frequency.

A formula for the resonant frequencies of rectangular antenna elements with thin substrates was given by Bahl [2] and Derneryd [4] as

$$f_r = \frac{c_0}{2(L + 2\Delta W)\sqrt{\epsilon_e(W)}} \quad (1)$$

where c_0 is the velocity of electromagnetic waves in free space and $\epsilon_e(W)$ is the effective dielectric constant, which is obtained from [18]

$$\epsilon_e(W) = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2\sqrt{1 + 10h/W}}; \quad (2)$$

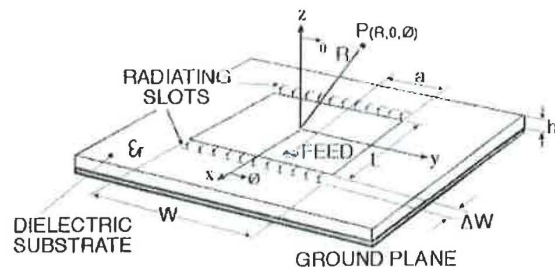


Figure 1 Configuration of a rectangular microstrip antenna element with dimensional parameters

Explore Litigation Insights

Docket Alarm provides insights to develop a more informed litigation strategy and the peace of mind of knowing you're on top of things.

Real-Time Litigation Alerts



Keep your litigation team up-to-date with **real-time alerts** and advanced team management tools built for the enterprise, all while greatly reducing PACER spend.

Our comprehensive service means we can handle Federal, State, and Administrative courts across the country.

Advanced Docket Research



With over 230 million records, Docket Alarm's cloud-native docket research platform finds what other services can't. Coverage includes Federal, State, plus PTAB, TTAB, ITC and NLRB decisions, all in one place.

Identify arguments that have been successful in the past with full text, pinpoint searching. Link to case law cited within any court document via Fastcase.

Analytics At Your Fingertips



Learn what happened the last time a particular judge, opposing counsel or company faced cases similar to yours.

Advanced out-of-the-box PTAB and TTAB analytics are always at your fingertips.

API

Docket Alarm offers a powerful API (application programming interface) to developers that want to integrate case filings into their apps.

LAW FIRMS

Build custom dashboards for your attorneys and clients with live data direct from the court.

Automate many repetitive legal tasks like conflict checks, document management, and marketing.

FINANCIAL INSTITUTIONS

Litigation and bankruptcy checks for companies and debtors.

E-DISCOVERY AND LEGAL VENDORS

Sync your system to PACER to automate legal marketing.