

*Formulas for
Stress and Strain* FIFTH EDITION

RAYMOND J. ROARK

WARREN C. YOUNG

McGraw-Hill Book Company

*New York St. Louis San Francisco Auckland Bogotá
Düsseldorf Johannesburg London Madrid Mexico
Montreal New Delhi Panama Paris São Paulo
Singapore Sydney Tokyo Toronto*

Dynacraft BSC, Inc.

Exhibit 1012

Dynacraft v. Mattel

IPR2018-00042

Library of Congress Cataloging in Publication Data

Roark, Raymond Jefferson, 1890-1966.

Formulas for stress and strain.

Includes bibliographical references and indexes.

1. Strength of materials—Tables, calculations, etc. 2. Strains and stresses—Tables, calculations, etc. I. Young, Warren Clarence, date, joint author. II. Title.

TA407.2.R6 1975 624'.176'0212 75-26612

ISBN 0-07-053031-9

Copyright © 1975, 1965 by McGraw-Hill, Inc. All rights reserved.
Copyright, 1938, 1943, 1954 by McGraw-Hill, Inc. All Rights Reserved.
Printed in the United States of America. No part of this publication may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording, or otherwise, without the prior written permission of the publisher.

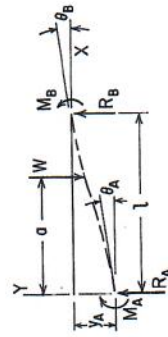
890 KPKP 84321

The editors for this book were Tyler G. Hicks and Ross Kepler, the designer was Naomi Auerbach, and the production supervisor was George Oechsner. It was set in Baskerville by York Graphic Services. It was printed and bound by The Kingsport Press.

TABLE 3 Shear, moment, slope, and deflection formulas for beams

NOTATION: W = load (pounds); w = unit load (pounds per linear inch); M_o = applied couple (inch-pounds); θ_o = externally created concentrated angular displacement (radians); Δ_o = externally created concentrated lateral displacement (inches); T_1 and T_2 = temperatures on the top and bottom surfaces, respectively (degrees). R_A and R_B are the vertical end reactions at the left and right, respectively, and are positive upward. M_A and M_B are the reaction end moments at the left and right, respectively. All moments are positive when producing compression on the upper portion of the beam cross section. The transverse shear force V is positive when acting upward on the left end of a portion of the beam. All applied loads, couples, and displacements are positive as shown. All forces are in pounds, all moments in inch-pounds, all deflections and beam dimensions in inches, all slopes in radians, and all temperatures in degrees. All deflections are positive upward, and all slopes are positive when up and to the right. E is the modulus of elasticity of the beam material, and I is the area moment of inertia about the centroidal axis of the beam cross section. γ is the temperature coefficient of expansion (inches per inch per degree)

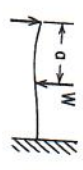



1. Concentrated intermediate load



$$\begin{aligned} \text{Transverse shear} &= V = R_A - W\langle x - a \rangle^0 \\ \text{Bending moment} &= M = M_A + R_A x - W\langle x - a \rangle \\ \text{Slope} &= \theta = \theta_A + \frac{M_A x}{EI} + \frac{R_A x^2}{2EI} - \frac{W}{2EI} \langle x - a \rangle^2 \\ \text{Deflection} &= y = \gamma_A + \theta_A x + \frac{M_A x^3}{6EI} + \frac{R_A x^3}{6EI} - \frac{W}{6EI} \langle x - a \rangle^3 \end{aligned}$$

(Note: see page 94 for a definition of the term $\langle x - a \rangle^n$.)

| End restraints, reference no. | Boundary values | Selected maximum values of moments and deformations |
|---|--|---|
| 1a. Left end free, right end fixed (cantilever) | $R_A = 0$ $M_A = 0$ $\theta_A = \frac{W(l-a)^2}{2EI}$ $\gamma_A = \frac{-W}{6EI}(2l^3 - 3l^2a + a^3)$ $R_B = W$ $M_B = -W(l-a)$ $\theta_B = 0$ $\gamma_B = 0$ | Max $M = M_B$; max possible value = $-Wl$ when $a = 0$ Max $\theta = \theta_A$; max possible value = $\frac{Wl^2}{2EI}$ when $a = 0$ Max $y = \gamma_A$; max possible value = $-\frac{Wl^3}{3EI}$ when $a = 0$ |

| | | |
|--|--|--|
| <p>1c. Left end simply supported, right end fixed</p>  | $R_A = \frac{W}{2l^3}(l-a)^2(2l+a) \quad M_A = 0$ $\theta_A = \frac{-Wa}{4EI}(l-a)^2 \quad \gamma_A = 0$ $R_B = \frac{Wa}{2l^3}(3l^2-a^2) \quad \theta_B = 0$ $M_B = \frac{-Wa}{2l^2}(l^2-a^2) \quad \gamma_B = 0$ | <p>Max $M = M_B = \frac{Wl^2}{2l^3}(l-a)^2(2l+a)$ at $x = a$; max possible value = 0.174Wl when $a = 0.366l$</p> <p>Max $-M = M_A$; max possible value = -0.1924Wl when $a = 0.5773l$</p> <p>Max $y = \frac{-Wa}{6EI}(l-a)^2\left(\frac{a}{2l+a}\right)^{1/2}$ at $x = l\left(\frac{a}{2l+a}\right)^{1/2}$ when $a > 0.414l$</p> <p>Max $y = \frac{-Wa(l^2-a^2)^{3/2}}{3EI(3l^2-a^2)^2}$ at $x = \frac{l(l^2+a^2)}{3l^2-a^2}$ when $a < 0.414l$; max possible $y = -0.0098 \frac{Wl^3}{EI}$ when $x = a = 0.414l$</p> |
| <p>1d. Left end fixed, right end fixed</p>  | $R_A = \frac{W}{l^3}(l-a)^3(l+2a)$ $M_A = \frac{-Wa}{l^2}(l-a)^2$ $\theta_A = 0 \quad \gamma_A = 0$ $R_B = \frac{Wl^2}{l^3}(3l-2a)$ $M_B = \frac{-Wa^2}{l^2}(l-a)$ $\theta_B = 0 \quad \gamma_B = 0$ | <p>Max $+M = \frac{2Wa^2}{l^3}(l-a)^2$ at $x = a$; max possible value = $\frac{Wl}{8}$ when $a = \frac{l}{2}$</p> <p>Max $-M = M_A$ if $a < \frac{l}{2}$; max possible value = -0.1481Wl when $a = \frac{l}{3}$</p> <p>Max $y = \frac{-2Wl(l-a)^2a^3}{3EI(l+2a)^2}$ at $x = \frac{2al}{l+2a}$ if $a > \frac{l}{2}$; max possible value = $\frac{-Wl^3}{192EI}$ when $x = a = \frac{l}{2}$</p> |
| <p>1e. Left end simply supported, right end simply supported</p>  | $R_A = \frac{W}{l}(l-a) \quad M_A = 0$ $\theta_A = \frac{-Wa}{6EI}(2l-a)(l-a) \quad \gamma_A = 0$ $R_B = \frac{W}{l} \quad M_B = 0$ $\theta_B = \frac{Wa}{6EI}(l^2-a^2) \quad \gamma_B = 0$ | <p>Max $M = R_a a$ at $x = a$; max possible value = $\frac{Wl}{4}$ when $a = \frac{l}{2}$</p> <p>Max $y = \frac{-Wa}{3EI}\left(\frac{l^2-a^2}{3}\right)^{3/2}$ at $x = l - \left(\frac{l^2-a^2}{3}\right)^{1/2}$ when $a < \frac{l}{2}$; max possible value = $\frac{-Wl^3}{48EI}$ at $x = \frac{l}{2}$ when $a = \frac{l}{2}$</p> <p>Max $\theta = \theta_A$ when $a < \frac{l}{2}$; max possible value = $-\frac{0.0642}{EI} \frac{Wl^2}{EI}$ when $a = 0.433l$</p> |
| <p>1f. Left end guided, right end simply supported</p>  | $R_A = 0 \quad M_A = W(l-a) \quad \theta_A = 0$ $\gamma_A = \frac{-W(l-a)}{6EI}(2l^2+2al-a^2)$ $R_B = W \quad M_B = 0$ $\theta_B = \frac{W}{2EI}(l^2-a^2) \quad \gamma_B = 0$ | <p>Max $M = M_A$ for $0 < x < a$; max possible value = Wl when $a = 0$</p> <p>Max $\theta = \theta_B$; max possible value = $\frac{Wl^2}{2EI}$ when $a = 0$</p> <p>Max $y = \gamma_A$; max possible value = $\frac{-Wl^3}{3EI}$ when $a = 0$</p> |