

RETRIEVABLE PACKERS

Notice: N728-04

Engineering Change Notice

Bill of Material Change -

Location: Navigation
Product Family: H99501
Product Description: 582-387 ISO - Frac Packer

DESCRIBE CHANGE BEING MADE
 Replaced Packing Element, Lower Cylinder, Drift Ring, and Upper Piston.

DESCRIBE REASON CHANGE IS BEING MADE
 Field specifications changed and now requires a smaller O.D. (5.820 vs. 5.910)

BILL OF MATERIAL CHANGES

Affected Assembly M/N	Item No.	Old M/N	Qty.	Item No.	New M/N	Qty.
H995015900	3	H036445701	1	3	H036445700	1
H995015900	8	H035521802	2	8	H036465100	2
H995015900	11	H036445901	1	11	H036445900	1
H995015900	25	H036034805	1	25	H035780505	1

DISPOSITION

Work in Progress: Manufacture/Rework To Latest
Plant Inventory -> Parts: Manufacture/Rework To Latest
Plant Inventory -> Assemblies: Manufacture/Rework To Latest
Field Inventory: Use As Is
Ass'y and Test Area -> Parts: Manufacture/Rework To Latest
Ass'y and Test Area -> Assemblies: Manufacture/Rework To Latest

ADDITIONAL INFORMATION

Tech Unit affected:
Assembly/TM Drawing:
Field Notificaton required:

ACCOUNTING INFORMATION

Cost Center / Internal Order No.:
 470310317

Account Number:
 501600 Scrap
 501550 In-House Rework
 689300 Outside Rework
 500900 Obsolete

WORKFLOW HISTORY

This ECN has not been released from Engineering yet.

Material	H995015900	582	Alt.	Usage
Reqd qty	MISC & SPCL	PROD, 581-387	4.5" BRL P 4.5	Valid 11/18/2004
Level no.	Item	Component no.	Base Quant	1.000 EA
	Description			Quant Un Ict Ex.
.1	0001	H036445800		1.000 EA L
.1	0002	HWG5180B0		20.000 EA L
.1	0003	H036445700		1.000 EA L
.1	0004	H034280400		2.000 EA L
.1	0005	H035676500		2.000 EA L
.1	0006	H035459702		2.000 EA L
.1	0007	H035459800		2.000 EA L
.1	0008	H036465100		2.000 EA L
.1	0009	H034394600		2.000 EA L
.1	0010	H036445600		1.000 EA L
.1	0011	H036445900		1.000 EA L
.1	0012	HWG6180BR		15.000 EA L
.1	0013	H035646600		8.000 EA L
.1	0014	H035462500		4.000 EA L
.1	0015	H035462500		2.000 EA L
.1	0016	H035466700		4.000 EA L
.1	0017	H035462600		2.000 EA L
.1	0018	H035462600		2.000 EA L
.1	0019	10067877		2.000 EA L
.1	0020	H035780605		1.000 EA L
.1	0021	H035786206		1.000 EA L
.1	0022	H035780800		1.000 EA L
.1	0023	H035782400		1.000 EA L
.1	0024	H035780200		1.000 EA L
.1	0025	H035780505		1.000 EA L
.1	0026	H036450300		1.000 EA L
.1	T001	H035943600		1.000 EA L
.1	T002	H035943500		0.000 EA L
.1	T003	H035943700		0.000 EA L

Material	H935015900	Alt.	Usage 1
Reqd qty	MISC & SPCCL PROD, 591-387 4.5" 8RL P 4.5	Base Quant	Valid 11/18/2004
Level no.	Item Component no.	Description	Quant Un Ict Ex.
.1	T004	FML CLAMSHL HSG F/7 PREM RMVBL PROD PKR	0.000 EA L
.1	T005	ASSY TL F/598 PREM RMVBL PROD PKR	0.000 EA L
.1	T006	SPEC TBLR, BULL PLG 4.5" 8RL B X.5"NPT	0.000 EA L
.1	T007	DRFT BARS 3.833"OD 42"LG NYL STANDARD PRESSURE TESTING	0.000 EA L

ENGINEERING JOB CONTROL CARD

Estimated Cost: \$ 179,579 <i>248,359</i>	Job No.: 4Z9-140
Estimated Hrs: 1,384 <i>1784</i>	Internal Order No.: 13005140
Planned Gate 3C Date: 03/05	Project Type: 3
Estimated Completion Date: 05/05	Revenue Class: R
Job Name: Iso Frac Packer for 7" Liner <i>System</i>	
<p>Job Instructions: Develop an 18 in. packing element for the open hole frac. system. Two designs will be developed per the attached Brainstorming Meeting Minutes. <i>Ball and sleeve development is also included in this job card</i></p> <ol style="list-style-type: none"> Maximum packer OD: 5.820" for up to 6.250" open hole desired; 5.820" for 6.00 in. open hole and 5.910" for 6.250" open hole acceptable Designed to deploy in 6.500" ID open hole Minimum ID: 3.875" Operating temperature of 100°F-250°F Differential pressure rating of 10,000 psi desired; 8,500 psi acceptable Torque rating through mandrel: 15,000 ft-lbf Burst & collapse rating of 10,000 psi Non-NACE service Setting pressure: 4,000 psi Desirable to have pistons below element; acceptable to have pistons above the element Maximum packer cost: \$4,000 <i>12. Test balls to 8,500 psi; acceptable, 10,000psi desired @ 250°F</i> See attached test plan for acceptance criteria <p><i>packer</i></p>	
<p>Milestone Dates:</p> <p>Prototype Chassis Available to Order: 1/24/05</p> <p>Commence Prototype Testing: 2/1/05</p> <p>First Packer Acceptance Test: 2/22/05</p> <p>Test Plan Completion: 3/31/05</p> <p>Estimated Ship Date: Week of 4/4/05</p>	
Written By: Gus Weinig	Date Written: 12/21/2004
Assigned To: Gary Anderson	Manager Assigned To: Gus Weinig
Cost Center: 470310317	Date Job Closed:
Approved By: (Engineering Director)	Approved By: (District Manager or designee)

Design Team

Name	Department	Core/Peripheral
Gary Anderson	Packer Engineering	Core
Craig Whitley	Region Manager	Core
Greg Badke	Wellbore Construction Engineering	Peripheral
Erick Peterson	Region Engineer	Peripheral

(Form: JOB CARD)

18. Use an atmospheric chamber continuously energize the element
19. Place a piston between the elements and cover it with rubber
20. Use a steel accordion with variable waves
21. Use a rubber accordion with variable waves
22. Make the center element thinner to reduce friction loss
23. Use a solid core ECP with a secondary setting piston
24. Undercut the element along its length

Each idea was reviewed and several were eliminated. The following two ideas were candidates for future development:

- Use an expandable element similar to the new Big Bore Permanent packers
- Use a solid core ECP with a secondary setting piston

After the review, each person voted for the three best designs. The results were:

Six votes for:

- Set the element system from both ends
- Six votes for: Taper the ID of the element and fill the void with Teflon, steel, another durometer rubber, or a flexible filler
- Six votes for: Use an MPAS sleeve under the element

Four votes for:

- Add multiple grooves with varying lengths and diameters

Three votes for:

- Mold varying thicknesses of continuous strand matting into the element

Two votes for:

- Use multiple elements with spacer rings between, but cover the spacers with a thin sheet of rubber
- Two votes for: Extend a long sleeve under the element and shear pin it to the gage rings
- Two votes for: Vary the durometer with each element, such as 70-80-90

4. Add another 500 psi and hold for 15 minutes
5. Continue applying pressure in 500 psi increments until failure

Brainstorming Meeting Minutes Iso Frac Packer Packing Element System

Meeting Date: December 7th, 2004

Attendees: Doug Murray, Chuck Pleasants, Jim Doane, Mike Evans, Cliff Mills, Hector Mireles, Gary Anderson, Greg Badke, Amy Farrar

Purpose: Choose three packing element concepts to pursue for the Iso Frac packer. The following constraints were placed on the designs:

- Compatible with the threaded backup rings off the 7" Premier packer
- Able to hold 10,000 psi water at 250°F in 6.250 in. ID casing
- Element Length: 18 in. continuous (run-in position)
- Maximum Element OD: 5.780 in.
- Mandrel OD: 5.525 in.
- Gage Ring OD: 5.890 in.
- Setting Force: 45,000 lbs.

The meeting began with a review of the constraints and a brief description of the application. It was agreed that the main challenge was to transfer enough force through the element to set the upper threaded backup ring and set the element in sequence to reduce voids and gaps.

Each person at the table presented a design. The following list was generated after several rounds of ideas.

1. Set the element system from both ends
2. Add multiple grooves with varying lengths and diameters
3. Use multiple elements with spacer rings between, but cover the spacers with a sheet of rubber
4. Use two, 6 in. elements with a 6 in. metal spacer covered with rubber
5. Extend a long sleeve under the element and shear pin it to the gage rings
6. Push the element over a metal or Teflon cone
7. Taper the ID of the element and fill the void with Teflon, steel, another durometer rubber, or a flexible filler
8. Use an MPAS sleeve under the element
9. Use an MPAS sleeve on the OD of the element
10. Make the backup rings out of wire mesh
11. Use an expandable element similar to the new Big Bore Permanent packers
12. Push through a long ZXP element
13. Use a double-piston with a tapered element
14. Shear pin spacers together or to an intermediate mandrel
15. Vary the durometer with each element, such as 70-80-90
16. Mold varying thicknesses of continuous strand matting into the element
17. Design a multiple-ramped ZXP element on a helix (similar to a Fishing spear)

Iso Frac Packer Test Plan

Test 1: Simulates loads on lower packer

Casing ID: 6.250"
Elastomer: Nitrile

Setting Temperature: 250°F
Test Medium: Water

Acceptance Criteria: Able to maintain the hold pressure with the Sprague pump.

Steps:

1. Heat fixture to 250°F
2. Set with 4,000 psi
3. Pressure below element with 8,500 psi and hold for 30 minutes
4. Cool down to 100°F with 8,500 psi below and hold for 30 minutes
5. Reverse to top at 100°F and hold 8,500 psi for 30 minutes
6. Reverse pressure to below and repeat steps 3 and 5 at 10,000 psi

Test 2: Simulates loads on upper packers

Casing ID: 6.250"
Elastomer: Nitrile

Setting Temperature: 250°F
Test Medium: Water

Acceptance Criteria: Able to maintain the hold pressure with the Sprague pump.

Steps:

1. Heat fixture to 250°F
2. Set with 8,500 psi
3. Cool to 100°F
4. Pressure below element with 8,500 psi and hold for 30 minutes
5. Reverse to top at 100°F and hold 8,500 psi for 30 minutes
6. Reverse pressure to below and repeat steps 4 and 5 at 10,000 psi

Test 3: Determine pressure rating in larger ID hole with pressure from below

Casing ID: 6.500"
Elastomer: Nitrile

Setting Temperature: 250°F
Test Medium: Water

Acceptance Criteria: Able to maintain the hold pressure with the Sprague pump.

Steps:

1. Set with 4,000 psi
2. Pressure below element with 4,000 psi and hold for 15 minutes
3. Add another 500 psi and hold for 15 minutes
4. Continue applying pressure in 500 psi increments until failure

Test 4: Determine pressure rating in larger ID hole with pressure from above

Casing ID: 6.500"
Elastomer: Nitrile

Setting Temperature: 250°F
Test Medium: Water

Acceptance Criteria: Able to maintain the hold pressure with the Sprague pump.

Steps:

1. Set with 4,000 psi
2. Pressure below element with 1,000 psi less than the failure pressure from test #3
3. Reverse pressure to above at 4,000 psi and hold for 15 minutes

PROJECT PLAN

JOB NUMBER: 4Z9-140

Hourly Rate: \$71.95

Project Steps	Hours Reqd	Prototype Expenses	Completion Date	Comments	Reqd Steps	Documentation Verified
<u>FEASIBILITY</u>						
Identify Technological Obstacles						
Marketing Feasibility						
Manufacturing Feasibility						
Conceptual Layout/Sketch						
Preliminary Calculations						
<u>PROJECT DEFINITION</u>						
JOB CONTROL CARD	8				Yes	
Form Design Team						
Project Schedule	8					
Pre-design						
<u>CONCEPTUAL DEVELOPMENT</u>						
Conceptual Layout/Sketch						
Patent Disclosure						
Preliminary Calculations						
Conceptual Testing						
Conceptual Design Review						
<u>DESIGN</u>						
DESIGN LAYOUT	160 200				Yes	
Preliminary Calculations	60 80				Yes	
Manufacturing Feasibility						
Cost Estimate	60					
DESIGN REVIEW	16				Yes	
<u>DESIGN DOCUMENTATION</u>						
DETAIL & ASSY DRAWINGS	160 200				Yes	
CHECK LAYOUT	80 100				Yes	
FINAL DESIGN CALCULATIONS	40 60				Yes	
ANALYSIS VERIFICATION						
Tolerance Study	40					
Mfg/VA Review						
<u>MANUFACTURE/ASSEMBLY</u>						
MANUFACTURE PRODUCT	16				Yes	
ASSEMBLE PRODUCT	16				Yes	
Mfg/Assy Evaluation						
First Article Inspection						
Assy Instruction Draft						
<u>TEST</u>						
TESTING	800	740	100,000		Yes	
TEST REPORT	80	40			Yes	
<u>DOCUMENTATION</u>						
Verify Standard Cost						
Update Drawings/Calculations						
Pre-design Details/Assys						
<u>FIELD EVALUATION</u>						
Interim Field Runs						
Interim Tech Unit						

PROJECT PLAN

Project Steps	Hours Reqd	Prototype Expenses	Completion Date	Comments	Reqd Steps	Documentation Verified
<u>PROJECT WRAP-UP</u>						
Release for Production						
TECH UNIT	40					
CLOSE JOB CONTROL FILE	40				Yes	

PROJECT TOTAL - HOURS	1,384
PROJECT TOTAL - PROTOTYPE	\$80,000
TOTAL ENGR EXPENSE	\$179,579

ENGINEERING JOB EST. ATTACHED: _____ YES

IF FOR SOME REASON, MANDATORY PHASES OR STEPS DO NOT APPLY, APPROVAL MUST BE GIVEN BY AN ENGINEERING MANAGER TO OMIT. PROOF OF APPROVAL MUST BE INSERTED INTO THE ENGINEERING JOB CONTROL FILE DOCUMENTING THE REASON FOR DISCREPANCY

PROJ. PLAN PREPARED BY: _____ DATE: _____

PROJ. PLAN APPROVED BY: _____ DATE: _____
(Manager)

PROJ. PLAN APPROVED BY: _____ DATE: _____
(Engineering Director)

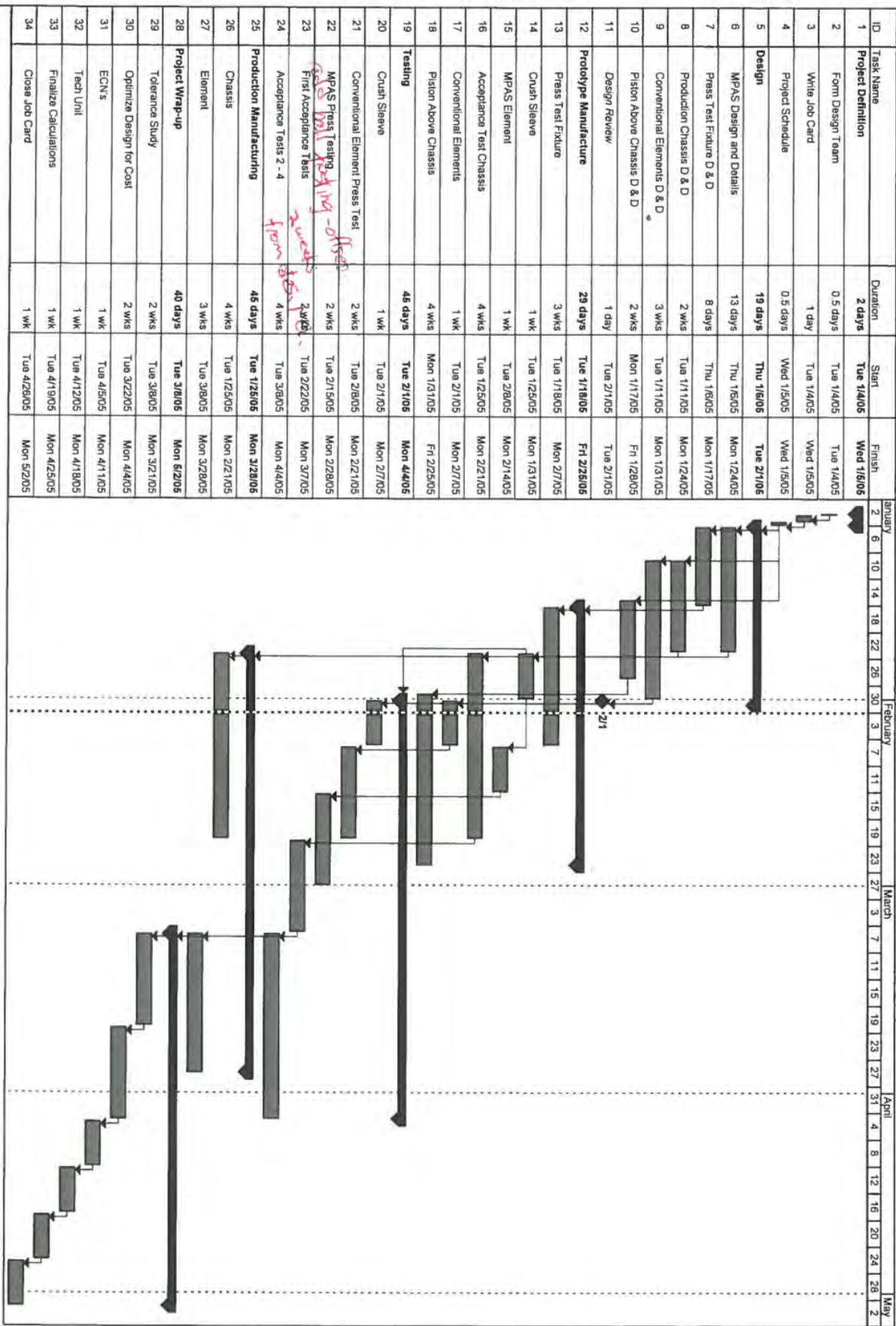
Outputs Verified: _____ DATE: _____
(District Manager or designee)

JOB CLOSURE APPROVED: _____ DATE: _____
(Engineering Director)

(DOCUMENTATION OF MANDATORY STEPS MUST BE VERIFIED BY APPROVERS AT JOB CLOSURE)

FORM: PROJ PLAN (02/02)
Ref: Eng Unit 201

Iso Frac Packer 18 in. Element Design



Project: New Dual
Date: Thu 2/3/05

Task Progress

Milestone Summary

Task Legend: Rolled Up Task, Rolled Up Milestone, Split, External Tasks, Project Summary

Submitted By: Erick Peterson		Date Submitted: 11/5/2004	Requested Reply Date:
Location: Oklahoma City		Phone: (405) 842-4005	Requested Ship Date: 12/6/2004
Is this request for an SAP Quote ?			Reference SAP Quote #

Request Type-make a selection in both boxes:

Action: Order Orders Only: Reference PO or STO

Type: New Material Number Number to Reinstate

Number of New Products covered by this Opportunity: See Attachment for additional item requirements

Which items in the attachment require action for this Opportunity

Actions Requested (check all that apply)

SAP Material Number Delivery Sales Price:

Special QA-Include Attachment with Requirements Standard Cost Transfer Price

SAP Order Acknowledgement--Orders only--Non-SAP Districts only

Extend to Operations District Plant-Include all SAP data for District:

District Plant # Profit Center Sales/Rental

Storage location Pur.Group

Other Requirements, Please Describe:

PROJECT DESCRIPTION

Project / Well Name: Customer:

Estimated Total Project Value

Project Summary:

Brief Well Description

Drill Pipe / Tubing? <input type="button" value="v"/>	Casing / Liner? <input type="button" value="v"/>	Open Hole Diameter: <input &="" 4"="" 6-1="" type="text" value="6"/>
Size: <input type="text"/>	Size: <input type="text" value="4-1/2"/>	Temperature Range: <input type="text" value="250F"/>
Grade: <input type="text"/>	Grade: <input type="text" value="P-110"/>	Pressure Range: <input type="text" value="8500psi"/>
Weight: <input type="text"/>	Weight: <input type="text" value="11.60 & 13.50"/>	

Operations Approval Use Only:

Originator: Recommended: Approved:

Tool Description

Max O.D. 5.820 / Min I.D. 3.844 (blanking dimension for 4-1/2" 13.5 ppf Atlas-Bradford ST-L thread)

100°F - 250°F temperature rating, Open hole range 6.00 to 6.25, Non-NACE service

Baker Equivalent Threads Acceptable?

Threads up: <input 13.50="" flush="" joint"="" type="text" value="4-1/2"/>	Threads down: <input 13.50="" flush="" joint"="" type="text" value="4-1/2"/>
Thread Size: <input type="button" value="v"/>	Thread Size: <input type="button" value="v"/>
Thread Weight: <input type="text"/>	Thread Weight: <input type="text"/>
Tool O.D. Max.: <input type="text"/>	Tool I.D. Max.: <input type="text"/>
Elastomer: <input type="text"/>	Material: <input type="text"/>
Tool I.D. Min.: <input type="text"/>	

Similar to Material Number: Order/Quote Quantity:

The Difference:

Plant Use Only

Weight: <input type="text"/>	Volume: <input type="text"/>	I.D./O.D./Length: <input type="text"/>
Opportunity Profile # <input type="text"/>	Delivery ARO: <input type="text"/>	
PDM Project Type <input type="text"/>	Cost Each: <input type="text"/>	
SAP Material #: <input type="text"/>	Price Each: <input type="text"/>	<input type="button" value="v"/>

Test: try 8,500 then 10Ks)

Open Hole Pin Point Frac System

Greg Backe
- layout

Information Provided By: _____
 Original Date: 10/15/04 Revision Date: _____
 Size & Model/Name: Open Hole Pin Point Frac System Rev. Level: _____

ITEM	DESCRIPTION	REV LEVEL	PREFERRED SPECIFICATIONS	MINIMUM ACCEPTABLE SPECIFICATIONS
1	General			
1.1	Model / Name		Open Hole Pin Point Frac System	
1.2	Maximum OD		5.75 inch <i>Can have w/ 5.875</i>	
1.3	Minimum ID		3.80 inch	
1.4	Anchor		Anchor on packer is preferred	
1.5	Stabilizer OD (if required)		5.81 inch	
1.6	Wellbore Fluid		Water based mud / completion brine	
1.7	Seal Longevity		Need to seal only during frac job	
1.8	Dog Leg		Need to pass through 159/100 ft doglegs	
2	Performance			
2.1	Burst Rating of System		12,410 psi <i>3,500 psi setting P</i>	10,690 psi (equivalent to 4.5 11.60# P-110)
2.2	Collapse Rating of System		(not required to exceed maximum frac pressures)	10,000 psi (equivalent to 4.5 13.50# P-110)
2.3	Setting ID			
2.3.1	Gauged Hole			6.00 to 6.25 inch
2.3.2	Oval Hole			N/A
2.4	Bottom hole operating temperature		275 F	250 F
2.5	Differential Pressures			
2.5.1	In gauged hole after set		10,000 psi	8,000 psi
2.5.2	In oval hole after set		N/A	N/A
2.6	Torqued Connections		15,000 ft-lbs <i>16,250 act.</i>	10,000 ft-lbs
3	Basic Type Materials			
3.1	Elastomers		Compatible with bottom hole temperature, pressures and temperature	
3.1	Material		Non Corrosion Resistant Alloy (Non CRA)	
4	Market / Economic Factors			
4.1	Target Factory Cost of seal device		\$5,000 US	
4.2	Target Factory Cost of frac sleeve		\$2,500 US (already designed by Eric Peterson)	
4.2	EOQ		10	
4.3	Time to Market		End of November 2004	

PLM Approval: _____

Date: _____

PED Approval: _____

Date: _____

Document Printed: October 21, 2004

Project for		Company	Date		
Matt Rees		Petro-Canada	Aug.10/03		
Drawn by		Description	Type of Packer		
Shaw		14-21-48-22W5	High Rate Acid Frac		
Depth	Drawing		OO(mm)	ID(mm)	Length
		177.8mm Casing 47.16Kg/m L-80 set at 3995m			-2.20
		Picked up for tubing compression			6.67
		KBD			0.23
		Hanger			0.30
		Pin to pin hanger cross over			8.26
		4 PH-6 pups lengths-1.25, 1.71, 2.33, 2.97			3932.77
		114.3mm 23.10 kg/m PH-6 Hydril premium connection tubing 407 Jts			0.34
		114.30mm PH-6 Hydril 403 Box 88.90mm EUE Pin L-80 X-Over Sub			
3945.19		7" 3.5" PL on-off tool with LH release c/w Otis 'X' Profile w/ 69.85mm ID (API Modified)	149.23	69.85	0.68
3945.77		177.8mm x 88.9mm EUE Plus-6 mechanical retrievable double grip 10K packer c/w P-110 mandrel RH set and release and emergency shear safety release (API Modified)	149.23	72.00	2.44
3945.77		88.9mm EUE High Pressure 10K sealed Tubing swivel c/w HSN Elastomer (API Modified)			0.31
		P-110 Material			9.60
		88.90mm EUE 13.84 kg/m L-80 Tubing c/w Bevelled Collars			0.44
3958.12		88.90mm EUE Profile Nipple Otis Original 'XN' w/ 69.85mm Seal Bore ID & 66.93mm NoGo ID (API Modified) P-110 Landing Nipple to be Halliburton original		66.93	2.46
		88.90mm EUE 13.84 kg/m L-80 Tubing c/w Regular Collars			116.02
4073.58		177.8mm x 88.9mm RockSeal II packer with HPHT packing element - hydraulic set shear release Heavy Wall P-110 Mandrel (Approximate setting pressure 15.5mpa)	146.05	69.85	1.27
		Rockseal centralizer P-110 Material			2.75
		88.90mm EUE 13.84 kg/m P-110 Tubing c/w Bevelled Collars	147.62		0.28
4147.11		Ball activated frac port assembly P-110 Material			71.96
		2 1/2" ball for 2 1/4" Seat			0.85
		88.90mm EUE 13.84 kg/m P-110 Tubing c/w Bevelled Collars			57.16
4189.42		Rockseal centralizer P-110 Material			41.48
		177.8mm x 88.9mm RockSeal II packer with HPHT packing element - hydraulic set shear release Heavy Wall P-110 Mandrel Material (Approximate setting pressure 15.5mpa)	146.05	69.85	1.27
		Rockseal centralizer P-110 Material	147.62		0.28
4248.44		88.90mm EUE 13.84 kg/m P-110 Tubing c/w Bevelled Collars			67.47
		Ball activated frac port assembly P-110 Material			50.80
		2 1/4" ball for 2" Seat			0.55
4280.85		88.90mm EUE 13.84 kg/m P-110 Tubing c/w Bevelled Collars			31.86
		Ball activated frac port assembly P-110 Material			44.45
		2" Ball for 1 3/4" Seat			0.55
		88.90mm EUE 13.84 kg/m P-110 Tubing c/w Bevelled Collars			41.11
4322.79		Rockseal centralizer P-110 Material	147.62		0.28
		177.8mm x 88.9mm RockSeal II packer with HPHT packing element - hydraulic set shear release Heavy Wall P-110 Mandrel Material (Approximate setting pressure 14mpa)	146.05	69.85	1.27
		Rockseal centralizer P-110 Material	147.62		0.28
4381.07		88.90mm EUE 13.84 kg/m L-80 Tubing c/w Regular Collars			56.73
		Ball activated frac port assembly P-110 Material			38.10
		1 3/4" Ball for 1 1/2" Seat			0.55
		88.90mm EUE 13.84 kg/m L-80 Tubing c/w Regular Collars			67.40
4449.3		Rockseal centralizer P-110 Material	147.62		0.28
		177.8mm x 88.9mm RockSeal II packer with HPHT packing element - hydraulic set shear release Heavy Wall P-110 Mandrel Material (Approximate setting pressure 14mpa)	146.05	69.85	1.27
		Rockseal centralizer P-110 Material	147.62		0.28
4489.32		88.90mm EUE 13.84 kg/m L-80 Tubing c/w Regular Collars			38.47
		High Pressure P-110 Internal Hydraulic Activated Frac Port Tool (Opening Pressure 27MPa) P-110 Material			69.85
		88.90mm EUE 13.84 kg/m L-80 Tubing c/w Regular Collars			67.76
4547.59		Rockseal centralizer P-110 Material	147.62		0.28
		7" x 3 1/2" 177.8mm x 88.9mm RockSeal II packer with HPHT packing element - hydraulic set shear release Heavy Wall P-110 Mandrel Material (Approximate setting pressure 14mpa)	146.05	69.85	1.27
		Rockseal centralizer P-110 Material	147.62		0.28
4559.06		88.90mm EUE Reverse Frac Port Tool P-110 Material (Hydraulic Closing Circulating Sleeve) (1 1/2" Ball for 1 1/4" Ball Seat) Set to close at 6-8 MPA			0.45
4560.00		Rockseal centralizer P-110 Material	147.62		0.28
		88.9mm EUE P-110 Material Bull Plug			0.21
		152.40mm Open Hole			

Contains Confidential Information. Red Deer 403-340-0735. Competitor Equivalent. Woody Randall. Bruce Bond 203-7587. 10-27 Final

Open Hole Pin Point Frac System

Information Provided By: _____ Revision Date: _____
 Original Date: 10/15/04
 Size & Model/Name: Open Hole Pin Point Frac System

injection sealing after movement on LWS/LWSB tomorrow
setting @ 2,000 psi, 772 centralization
tomorrow

ITEM	DESCRIPTION	REV LEVEL	PREFERRED SPECIFICATIONS	MINIMUM ACCEPTABLE SPECIFICATIONS
1	General			
1.1	Model / Name		Open Hole Pin Point Frac System	
1.2	Maximum OD		5.75 inch	
1.3	Minimum ID		3.80 inch	
1.4	Anchor		Anchor on packer is preferred	5.81 inch
1.5	Stabilizer OD (if required)			Water based mud / completion brine
1.6	Wellbore Fluid			Need to seal only during frac job
1.7	Seal Longevity			Need to pass through 15#/100 ft doglegs <i>Chuck will check</i>
1.8	Dog Leg			
2	Performance			
2.1	Burst Rating of System		12,410 psi <i>west Texas</i> (equivalent to 4.5 13.50# P-110)	10,690 psi (equivalent to 4.5 11.60# P-110)
2.2	Collapse Rating of System		(not required to exceed maximum frac pressures)	10,000 psi
2.3	Setting ID			
2.3.1	Gauged Hole		6.00 to 6.25 inch	
2.3.2	Oval Hole			N/A
2.4	Bottom hole operating temperature		275 F	250 F
2.5	Differential Pressures			
2.5.1	In gauged hole after set		10,000 psi	8,000 psi
2.5.2	In oval hole after set		N/A	N/A
2.6	Torqued Connections		16,500' <i>good to 5</i> 15,000 ft-lbs <i>Gay will check</i>	10,000 ft-lbs
3	Basic Type Materials			
3.1	Elastomers		Compatible with bottom hole temperature, pressures and temperature	
3.1	Material		Non Corrosion Resistant Alloy (Non CRA)	
4	Market / Economic Factors			
4.1	Target Factory Cost of seal device			\$5,000 US
4.2	Target Factory Cost of frac sleeve			\$2,500 US (already designed by Eric Peterson)
4.2	EOQ			10
4.3	Time to Market			End of November 2004

PLM Approval: _____

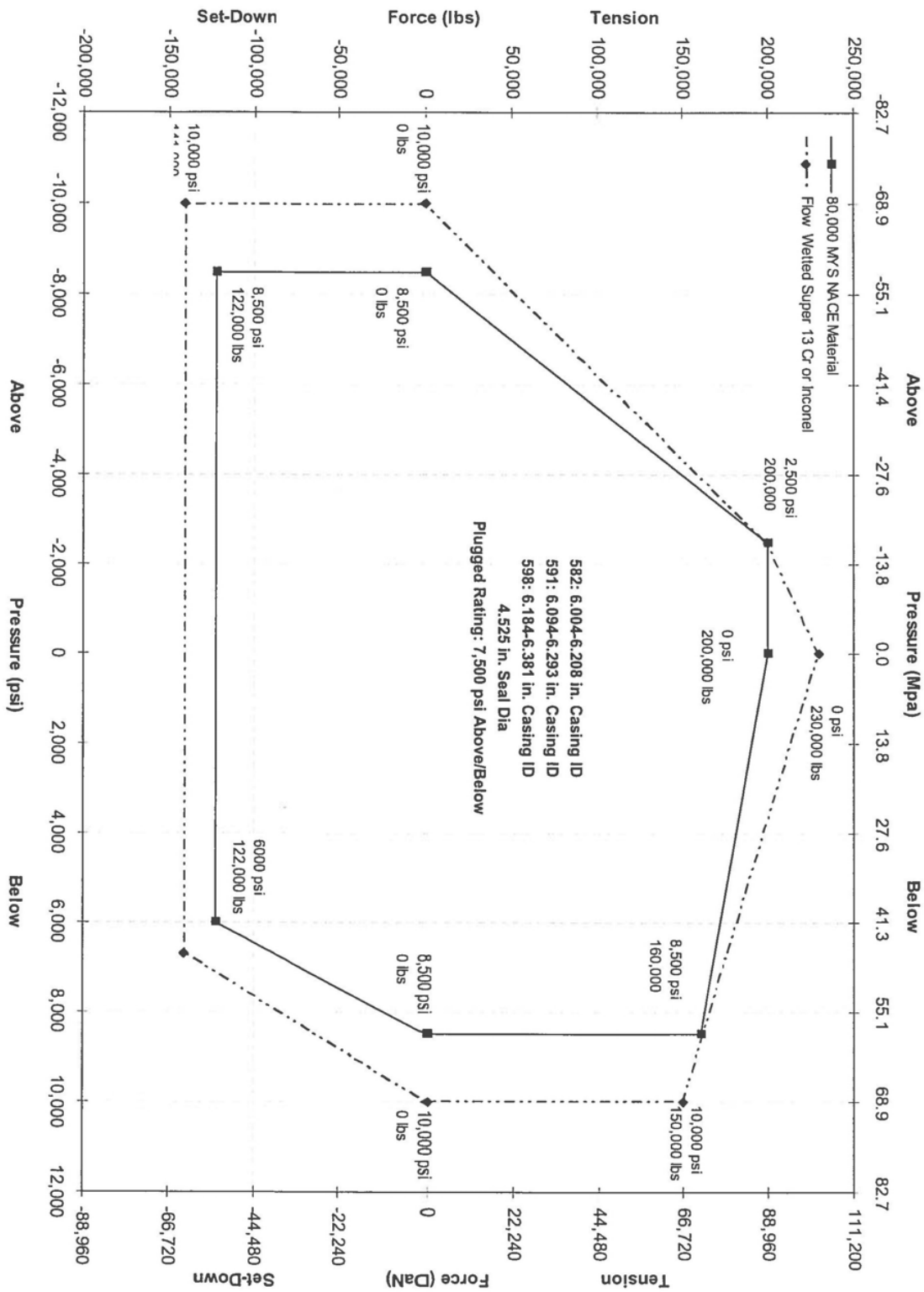
Date: _____

PED Approval: _____

Date: _____

Add a torque shoulder
Add Burst, collapse, Piston Areas, Torque

582/591/598-387 Cut Release Premier Packer



Unit No. 10244
 1-21-04
 Page 24 of 24
 Rev. B

Premier™ Cut Release Removable Production
 Packer, Size 7" x 4-1/2"

ESN: 8, Rev. 51G

Spreadsheet Prepared By: Eddie Hixson

Spreadsheet Checked By: Kurt Hickey

Spreadsheet Approved By: Steve Shirk

Date Approved: 6-11-92

COMBINED STRESS ANALYSIS

Page 1 of 2

Calc. Prepared By: GLA

Date Prepared: 10/21/04

Calc. Approved By:

Date Approved:

Ref: 357-806-00

SECTION OD: 5.790

SECTION ID: 5.179

REF: BMS- A098

COMPONENT NAME: Cylinder

WORKING TEMPERATURE: 275°F

TEST TEMPERATURE: 275°F

D/=
19.0

YIELD STR: 106,000 PSI

YIELD STR: 106,000 PSI

Major Dia. of "piston" area ++

Minor Dia. of "piston" area

STRESS CALCULATED AT OD or ID

TOTAL TENSILE LOAD lbs

RADIAL STRESS THICK psi

TANGENTIAL STRESS THICK psi

AXIAL STRESS psi

EQUIVALENT STRESS THICK psi

REFERENCE SAFETY FACTOR

per case

1.08

1.10

1.04

1.06

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

1.00

CASE	YIELD STRENGTH AT TEMP	APPLIED INTERNAL PRESSURE	APPLIED EXTERNAL PRESSURE	Applied Tensile Load	Major Dia. of "piston" area ++	Minor Dia. of "piston" area	STRESS CALCULATED AT OD or ID	TOTAL TENSILE LOAD	RADIAL STRESS THICK	TANGENTIAL STRESS THICK	AXIAL STRESS	EQUIVALENT STRESS THICK	REFERENCE SAFETY FACTOR
UNIT	psi	psi	psi	lbs	in	in	(OD or ID)	lbs	psi	psi	psi	psi	per case
A	110,000	10,690	0	0	0.000	0.000	ID	0	-10,690	96,254	0	102,020	1.08
B	110,000	0	10,000	0	0.000	0.000	ID	0	0	-100,041	0	100,041	1.10
C	106,000	10,690	0	0	0.000	0.000	ID	0	-10,690	96,254	0	102,020	1.04
D	106,000	0	10,000	0	0.000	0.000	ID	0	0	-100,041	0	100,041	1.06
E	110,000	11,526	0	0	0.000	0.000	ID	0	-11,526	103,783	0	110,000	1.00
F	110,000	0	10,995	0	0.000	0.000	ID	0	0	-110,000	0	110,000	1.00
G	106,000	11,107	0	0	0.000	0.000	ID	0	-11,107	100,009	0	106,000	1.00
H	106,000	0	10,596	0	0.000	0.000	ID	0	0	-106,000	0	106,000	1.00
	0	0	0	0	0.000	0.000	ID	0	0	0	0	0	N/A

As = Cross Sectional area of component = 5.264in²
++ Use negative sign for compressive load

EQUATIONS

Thick Section Analysis Description	Symbol	Equation	Where:
Tangential Stress (Pi & Po)	S _t	$S_t = ((P_i \cdot r_i^2) - (P_o \cdot r_o^2) - (r_i^2 \cdot r_o^2 \cdot (P_o - P_i) / r^2)) / (r_o^2 - r_i^2)$	Po=External Pressure Pi=Internal Pressure ri=inside radius ro=outside radius
Radial Stress (Pi & Po)	S _r	$S_r = ((P_i \cdot r_i^2) - (P_o \cdot r_o^2) + (r_i^2 \cdot r_o^2 \cdot (P_o - P_i) / r^2)) / (r_o^2 - r_i^2)$	r=radius at which stresses are to be calculated D=Diameter which pressure creating load is applied ID=Inside Diameter of cross section being analyzed OD=Outside Diameter of cross section being analyzed
Axial Stress	S _z	$S_z = (P_i \cdot P_o) \cdot D^2 / (OD^2 \cdot ID^2)$	
Equivalent Stress	Seq	$Seq = (((S_r - S_t)^2 + (S_t - S_z)^2 + (S_z - S_r)^2) / 2)^{1/2}$	

* For description of loading cases, see SSOPM unit D001-2, section 6.0
 Definitions, assumptions, derivations, and references are as per:
 API Specification 5C3, "Bulletin on Formulas and Calculations for Casing, Tubing, Drill Pipe and Line Pipe Properties", 5th Edition, July 1989, p. 5-14 & 16-17.
 Shigley, J. and Mischke C.: "Mechanical Engineering Design", 5th Edition, McGraw-Hill, New York, 1989, p. 58-60.
 Roark, R. and Young, W.: "Formulas for Stress and Strain", 5th Edition, McGraw-Hill, New York, 1975, p. 446.
 Bednar, Henry H.: "Pressure Vessel Design Handbook", Van Nostrand Reinhold Co. Inc., New York, 1981, p. 39.

ESN-8, Rev. 51G
 Spreadsheet Prepared By: Eddie Hixson
 Spreadsheet Checked By: Kurt Hickey
 Spreadsheet Approved By: Steve Shirk
 Date Approved: 6-11-92

COMBINED STRESS ANALYSIS

COMPONENT NAME: Upper Mandrel
 WORKING TEMPERATURE: 275°F
 TEST TEMPERATURE: 275°F

YIELD STR: 106,000 PSI
 YIELD STR: 106,000 PSI
 SECTION OD: 4.412
 SECTION ID: 3.900
 REF: BMS- A098

Job Number: None
 Reference: Ref. 358-503-00
 Date Approved: Calc. Approved By: GLA
 Date Approved: 10/21/04

CASE * AT TEMP	YIELD STRENGTH	APPLIED INTERNAL PRESSURE	APPLIED EXTERNAL PRESSURE	Applied Tensile Load	Major Dia. of "piston" area ++		Minor Dia. of "piston" area		STRESS CALCULATED AT OD or ID	TOTAL TENSILE LOAD	RADIAL STRESS THICK	TANGENTIAL STRESS THICK	AXIAL STRESS	EQUIVALENT STRESS THICK	REFERENCE SAFETY FACTOR
					lbs	in	in	(OD or ID)							
A	110,000	10,690	0	0	0.000	0.000	0.000	0.000	ID	0	-10,690	87,102	0	92,909	1.18
B	110,000	0	10,000	0	0.000	0.000	0.000	0.000	ID	0	0	-91,480	0	91,480	1.20
C	106,000	10,690	0	0	0.000	0.000	0.000	0.000	ID	0	-10,690	87,102	0	92,909	1.14
D	106,000	0	10,000	0	0.000	0.000	0.000	0.000	ID	0	0	-91,480	0	91,480	1.16
E	110,000	12,656	0	0	0.000	0.000	0.000	0.000	ID	0	-12,656	103,124	0	110,000	1.00
F	110,000	0	12,025	0	0.000	0.000	0.000	0.000	ID	0	0	-110,000	0	110,000	1.00
G	106,000	12,196	0	0	0.000	0.000	0.000	0.000	ID	-12,196	99,374	-106,000	0	106,000	1.00
H	106,000	0	11,587	0	0.000	0.000	0.000	0.000	ID	0	0	-106,000	0	106,000	1.00
Safety Factor (worst case, Seq):															1.00

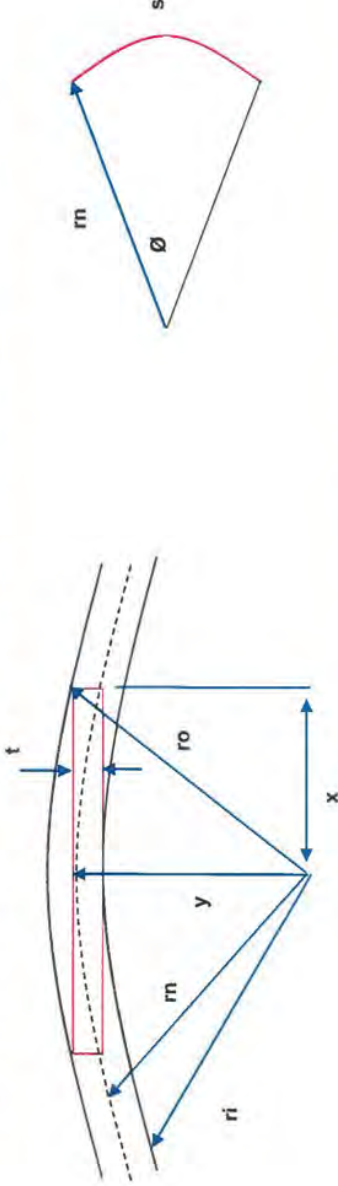
As = Cross Sectional area of component = 3.342in²
 ++ Use negative sign for compressive load

EQUATIONS

Thick Section Analysis Description	Symbol	Equation	Where:
Tangential Stress (Pi & Po)	St	$St = ((Pi \cdot r_i^2 - Po \cdot r_o^2) / (r_i^2 - r_o^2)) / (r_i^2)$	Po=External Pressure Pi=Internal Pressure ri=inside radius ro=outside radius
Radial Stress (Pi & Po)	Sr	$Sr = ((Pi \cdot r_i^2 - Po \cdot r_o^2) / (r_i^2 - r_o^2)) / (r_i^2 - r_o^2)$	r=radius at which stresses are to be calculated D=Diameter which pressure creating load is applied ID=Inside Diameter of cross section being analyzed OD=Outside Diameter of cross section being analyzed
Axial Stress	Sz	$Sz = (Pi \cdot Po) \cdot D^2 / (OD^2 \cdot ID^3)$	
Equivalent Stress	Seq	$Seq = (((Sr - Sz)^2 + (St - Sz)^2 + (Sz - Sr)^2) / 2)^{1/2}$	

* For description of loading cases, see SSQPM unit D001-2, section 6.0
 Definitions, assumptions, derivations, and references are as per:
 API Specification SC3, "Bulletin on Formulas and Calculations for Casing, Tubing, Drill Pipe and Line Pipe Properties", 5th Edition, July 1989, p. 5-14 & 16-17.
 Shigley, J. and Mischke C.: "Mechanical Engineering Design", 5th Edition, McGraw-Hill, New York, 1989, p. 58-60.
 Roark, R. and Young, W.: "Formulas for Stress and Strain", 5th Edition, McGraw-Hill, New York, 1975, p. 446.
 Bednar, Henry H.: "Pressure Vessel Design Handbook", Van Nostrand Reinhold Co., Inc., New York, 1981, p. 39.

MAX TOOL LENGTH - ASSUMES TOOL OD CONSISTENT THROUGHOUT LENGTH



Comments: Open Hole Pin Point Frac System, 6.00-6.25 open hole ID

Case Number	INPUT INFORMATION				rr, nom wellbore radius of curvature		ro (in)	ri (in)	y (in)	x (in)	Tool Lgh (2*x) (in)
	s, Arc Lgh (ft)	Ø, Angle (degrees)	t, Max Tool OD, (in)	Csg ID min. (in)	(ft)	(in)					
1	100.00	15.00	5.875	6.000	381.97	4,583.66	4,586.66	4,580.66	4,586.54	33.88	67.72
2	100.00	15.00	5.875	6.250	381.97	4,583.66	4,586.79	4,580.54	4,586.41	58.65	117.30
3	100.00	15.00	5.750	6.000	381.97	4,583.66	4,586.66	4,580.66	4,586.41	47.89	95.78
4	100.00	15.00	5.750	6.250	381.97	4,583.66	4,586.79	4,580.54	4,586.29	67.72	135.45
5					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
11					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
12					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
13					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15					#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

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Open Hole Pin Point Frac System

Information Provided By: Eric Peterson Revision Date: 10/15/04
 Original Date: 10/15/04 Rev. Level: 1
 Size & Model/Name: Open Hole Pin Point Frac System

*H 64629 - Inverted Lock Set
 1 reversal*

ITEM	DESCRIPTION	REV LEVEL	PREFERRED SPECIFICATIONS	MINIMUM ACCEPTABLE SPECIFICATIONS
1	General			
1.1	Model / Name		Open Hole Pin Point Frac System	
1.2	Maximum OD		5.75 inch	5 7/8 max, 6" 1/6.25 hole
1.3	Minimum ID		3.80 inch	3.0 min
1.4	Anchor		Anchor on packer is preferred	
1.5	Stabilizer OD (if required)		5.81 inch	
1.6	Wellbore Fluid		Water based mud / completion brine	
1.7	Seal Longevity		Need to seal only during frac job	
1.8	Dog Leg		Need to pass through 15"/100 ft doglegs	
2	Performance			
2.1	Burst Rating of System		12,410 psi (equivalent to 4.5 13.50# P-110)	10,690 psi (equivalent to 4.5 11.60# P-110)
2.2	Collapse Rating of System		(not required to exceed maximum frac pressures)	10,000 psi
2.3	Setting ID			
2.3.1	Gauged Hole		6.00 to 6.25 inch	
2.3.2	Oval Hole		N/A	
2.4	Bottom hole operating temperature		275 F	250 F
2.5	Differential Pressures			
2.5.1	In gauged hole after set		10,000 psi	8,000 psi
2.5.2	In oval hole after set		N/A	N/A
2.6	Torqued Connections		15,000 ft-lbs	10,000 ft-lbs
3	Basic Type Materials			
3.1	Elastomers		Compatible with bottom hole temperature, pressures and temperature	
3.1	Material		Non Corrosion Resistant Alloy (Non CRA)	
4	Market / Economic Factors			
4.1	Target Factory Cost of seal device			\$5,000 US
4.2	Target Factory Cost of frac sleeve		(already designed by Eric Peterson)	\$2,500 US
4.2	EOQ			10
4.3	Time to Market			End of November 2004

*fracturing @ 10ksi but
 bottom hole is 8ksi
 Craig Whittier suggested
 Premier
 - length would be nice*

*off-the-shelf as much as possible
 4 1/2 needed*

PLM Approval: _____ Date: _____
 PED Approval: _____ Date: _____
 Document Printed: October 19, 2004

Radoil, Inc.

12251 FM 529, HOUSTON, TEXAS 77041 (713) 937-4494, FAX 937-4624, E-MAIL bbaugh@radoil.com

August 10, 2004

QUOTATION NO. 040802-01

Baker Oil tools
P.O. Box 3048
Houston, Texas 77243-3048

ATTENTION: John Fothergill, Manager - Cased Hole Market Development

Subject: DEVELOPMENT PROGRAM - 2 7/8" ISOLATION PACKER & PACKER ANCHOR

ITEM	QTY	DESCRIPTION	ITEM COSTS	TOTAL COSTS
1	1	ENGINEERING DESIGN - ANCHOR PACKER - 2 7/8" <ul style="list-style-type: none">* Collect design information, including:<ol style="list-style-type: none">1. 2 7/8" API Upset tubing thread2. 10,000 p.s.i. minimum burst pressure3. 80,000 lbs. minimum tensile load4. 50,000 lbs. minimum compressive load5. 4140 28-36 Roc C material specification6. 3.90" min I.D.7. 5.91" max. O.D.* Prepare Acad manufacturing detail drawings* Prepare Acad assembly drawing* Prepare design calculation package	\$3,200.00	\$3,200.00
2	1	PROTOTYPE MANUFACTURE - ANCHOR PACKER - 2 7/8" <ul style="list-style-type: none">* To be estimated based on actual drawings* Prototype testing will be as follows:<ol style="list-style-type: none">1. Mechanical functioning2. Internally pressure test to 10,000 p.s.i.3. Set in 6.50" I.D. pipe & pull to 80,000 lbs.	\$18,000.00	\$18,000.00
3	1	ENGINEERING DESIGN - FRAC PACKER - 2 7/8" <ul style="list-style-type: none">* Collect design information, including:<ol style="list-style-type: none">1. 2 7/8" API Upset tubing thread2. 10,000 p.s.i. minimum burst pressure3. 80,000 lbs. minimum tensile load4. 50,000 lbs. minimum compressive load5. 4140 28-36 Roc C material specification6. 3.90" min I.D.7. 5.91" max. O.D.* Prepare Acad manufacturing detail drawings* Prepare Acad assembly drawing* Prepare design calculation package	\$3,200.00	\$3,200.00
4	1	PROTOTYPE MANUFACTURE - FRAC PACKER - 2 7/8" <ul style="list-style-type: none">* To be estimated based on actual drawings* Prototype testing will be as follows:<ol style="list-style-type: none">1. Mechanical functioning2. Internally pressure test to 10,000 p.s.i.3. Set in 6.50" I.D. pipe & pull to 80,000 lbs.	\$18,000.00	\$18,000.00
1	1	ENGINEERING DESIGN - FRAC SLEEVE <ul style="list-style-type: none">* Collect design information, including:<ol style="list-style-type: none">1. 2 7/8" API Upset tubing thread	\$3,200.00	\$3,200.00

RESTRICTED - OUTSIDE ATTORNEYS' EYES ONLY - TECHNICAL
20 of 34

BH00363827

Ex. 2052
IPR2016-01496

- 2. 10,000 p.s.i. minimum burst pressure
- 3. 80,000 lbs. minimum tensile load (100,000 preferred)
- 4. 50,000 lbs. minimum compressive load (75,000 preferred)
- 5. 4140 28-36 Roc C material specification
- 6. 3.90" min I.D.
- 7. 5.91" max. O.D.
- * Prepare Acad design layouts
- * Prepare Acad manufacturing detail drawings
- * Prepare Acad assembly drawing
- * Prepare design calculation package

2	1 PROTOTYPE MANUFACTURE - FRAC SLEEVE	\$14,000.00	\$14,000.00
	* To be estimated based on actual drawings		
	* Prototype testing will be as follows:		
	* 1. Mechanical functioning		
	* 2. Internally pressure test to 12,500 p.s.i., 2 times		

TOTAL FOR THIS QUOTATION \$59,600.00

Notes:

- 1. Terms: Net 30 days
- 2. Delivery: Item 1 & 3 in 3 weeks, item 2 & 4 due 6 weeks after approval of item 1
- 3. Past due invoices will be subject to a charge of 1 1/2% per month
- 4. Quotation is valid for 90 days
- 5. Warranted to be free of manufacturing defects for one year

We appreciate the opportunity of providing this quotation.

Regards,

Benton F. Baugh, Ph.D., P.E.
President

**Iso-Frac System Component Project Specifications
for Quotation 7-23-04**

Tool	Reference Size	Tool-OD	Tool-ID	Heaviest Intermediate Casing Size	Production String or Liner Size	Gaged Hole Size	Qualifying Test ID Size
Packer	591-390	5.91"	3.90"	7" (32#)	4-1/2" (11.6-13.5#)	6-1/4"	6-1/2"
	770-490	7.70"	4.90"	8-5/8" (32#)	5-1/2" (14-20#)	7-7/8"	8-1/8"
	448-287	4.48"	2.87"	5-1/2" (23#)	3-1/2" (9.3#)	4-3/4"	5"
	375-238	3.75"	2.38"	4-1/2" (13.5#)	2-7/8" (6.50#)	3-7/8"	4-1/8"
Frac Sleeve	591-390	5.91"	3.90"	7" (32#)	4-1/2" (11.6-13.5#)	6-1/4"	
	770-490	7.70"	4.90"	8-5/8" (32#)	5-1/2" (14-20#)	7-7/8"	
	448-287	4.48"	2.87"	5-1/2" (23#)	3-1/2" (9.3#)	4-3/4"	
	375-238	3.75"	2.38"	4-1/2" (13.5#)	2-7/8" (6.50#)	3-7/8"	
Hyd Anchor Packer	591-275	5.91"	2.75"	7" (32#)	4-1/2" (11.6-13.5#)	6-1/4"	6-1/2"
	770-450	7.70"	4.50"	8-5/8" (32#)	5-1/2" (14-20#)	7-7/8"	8-1/8"
	448-200	4.48"	2.00"	5-1/2" (23#)	3-1/2" (9.3#)	4-3/4"	5"
	375-188	3.75"	1.88"	4-1/2" (13.5#)	2-7/8" (6.50#)	3-7/8"	4-1/8"

Materials	Differential Pressure Rating	Initiating Setting Pressure	Comments
Metallurgy	Elastomer		
Packer	110ky 4140 Nitrile 80D	3,500 psi	Setting psi target can adjust to meet ID requirement. Preset protection (interlock mechanism) must be engaged to the packer body and outer housing. Flow Area ≥ Tubular Slip Hardness HT 56rc to .030 depth in wickers
Frac Sleeve	110ky 4140 Non-Elastomeric	3,000 psi	
Hyd Anchor	110ky 4140 Nitrile 80D o'rings	2,500 psi	

All dimensional references are subject to change, to the extent OD remains at least .060 below drift of the restrictive Casing ID, and ID of packer and sleeves (assumes ball seat drilled out) is ≥ drift of its mating tubular's drift ID.

chassis only; sent 1-20-05

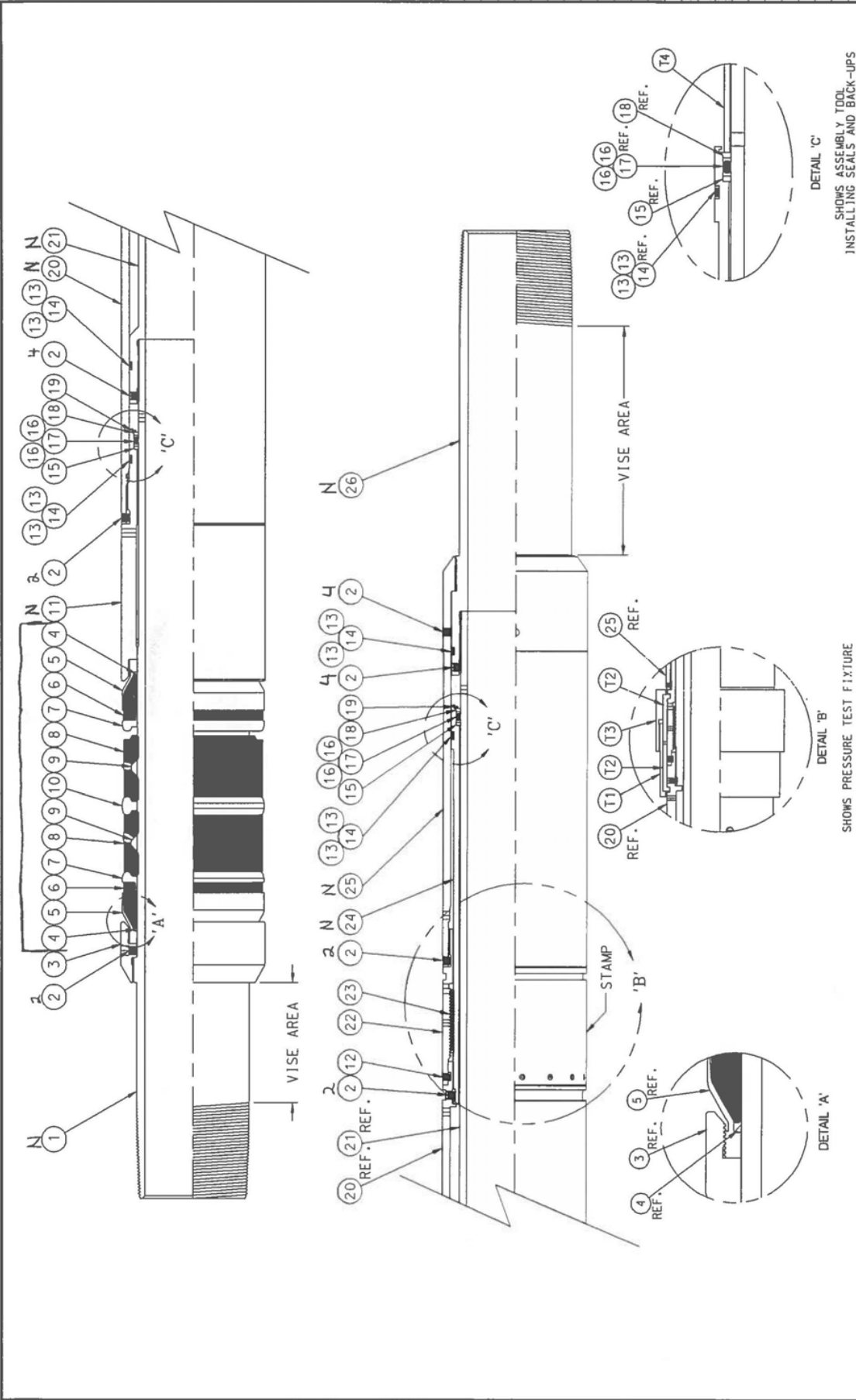
Parts List

582-387 Iso-Frac

w/ 4.5" 13.5 lb/ft Buttress Casing Thread, Box x Pin

ITEM	MATERIAL	DESCRIPTION	QTY
1	x H036474700	Upper Mandrel	1
2	x HWWG51B0B0	5/16-18x3.125 Set Screw	20
3	x H036445700	Drift Ring	1
4-10	TBD	Element System	1
11	H036474800	Upper Piston	1
12	x HWWGE180BR	1/4-20x5/16 Shear Screw	15
13	x H035646600	O-Ring Back Up	8
14	x HWWB249P40	O-Ring, Peroxide Nitrile 90 Duro	4
15	x H035462500	Upper Back-Up Retainer	2
16	x H035466700	O-Ring Back Up	4
17	x HWWB348P40	O-Ring, Peroxide Nitrile 90 Duro	2
18	x H035462600	Lower Back-Up Retainer	2
19	x 10067877	Spiral Retainer Ring	2
20	x H036474900	Upper Cylinder	1
21	x H036475000	Lower Mandrel	1
22	x H035780800	Body Lock Ring Housing	1
23	x H035782400	Body Lock Ring	1
24	x H036475100	Lower Piston	1
25	H036475200 H036477900	Lower Cylinder	1
26	x H036475300	Bottom Sub	1

NOT TO SCALE



MATERIAL: BMS		POLYMER/WELDING SPEC:		HEAT TREAT: BMS		COATING: BCS		REF DWG: 350-901-00		CATEGORY: 479		SUPERSEDES		DRAWING NO. 385					
		TOLERANCES FOR MACHINED SURFACES UNLESS OTHERWISE SPECIFIED										DATE 11-29-04		PAGE 1					
		.125 - .0005										PRODUCT FAMILY H99501		OF 5					
		.015 - .005										MATERIAL NO.		219-00					
		.005 - .002										DRAWN BY: RALPHILLIPS		CHECKED: DA					
		.002 - .001										APPROVED: GW							
		ALL ANGLES TO BE 25-50°										TITLE		SHOWS ASSEMBLY TOOL INSTALLING SEALS AND BACK-UPS					
		CHECK DIMENSIONS AT STAMPED PRODUCT NUMBER LOCATION										© 2004 BAKER OIL TOOLS DIVISION OF BAKER HUGHES INCORPORATED							
												BAKER HUGHES INCORPORATED							
												THIS DOCUMENT IS THE PROPERTY OF BAKER HUGHES INCORPORATED. IT IS CONFIDENTIAL AND NOT TO BE REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, ELECTRONIC OR MECHANICAL, INCLUDING PHOTOCOPYING, RECORDING, OR BY ANY INFORMATION STORAGE AND RETRIEVAL SYSTEM, WITHOUT THE WRITTEN CONSENT OF BAKER HUGHES INCORPORATED. THIS DOCUMENT IS SUBJECT TO THE TERMS AND CONDITIONS OF THE LICENSE AGREEMENT WHICH MAY BE APPLICABLE TO THIS DOCUMENT. IN ANY CASE, THIS DOCUMENT IS NOT TO BE REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, ELECTRONIC OR MECHANICAL, INCLUDING PHOTOCOPYING, RECORDING, OR BY ANY INFORMATION STORAGE AND RETRIEVAL SYSTEM, WITHOUT THE WRITTEN CONSENT OF BAKER HUGHES INCORPORATED.		Baker Oil Tools					
												GENERATED ON THE MicroStation CAD SYSTEM		ASM					
DATE		REV		BY		CHK		APP		DATE		REV		BY		CHK		APP	
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IsoFrac – Generation 1

- Generation 1
 - System Status (Testing and Development)?
 - Packer
 - Design Requirements – Hold 8,500 psi at 250F in 6.250 in. open hole
 - Packer Testing Results – Held 8,500 psi consistently, able to achieve 10,000 psi
 - Frac Sleeve
 - Design Requirements – Reference Job Card
 - Ball Testing Time Line and Results
 - Equipment Delivery
 - Status of Equipment
 - System Issues

PS&W
BAKER
HUGHES Baker Oil Tools

Packer Length = 76"
 Gage-to-Gage = 55"
 PE Length = 7 1/4"
 H995015910

IsoFrac – Generation 2

- Generation 2
 - System Status (Testing and Development)?
 - Packer
 - Design Requirements – Hold 8,500 psi at 250F in 6.250 in. open hole using an 18 in. element
 - Packer Testing Time Line and Results – Preliminary testing underway, initial packer testing March 1st
 - Delays or Roadblocks to Development – Setting sequence and force transfer of long element, centralization

PS&W
BAKER
HUGHES Baker Oil Tools

Packer Length = 104"
 Gage-to-Gage = 82"
 PE Length = 19"

IsoFrac – Generation 3

- Generation 3 Drivers
 - General Design Specifications
 - 10,000 PSI / 350F
 - Generation 2 System Chassis
 - Multiple Cycle Frac Sleeves
 - Additional Open Hole Sizes
 - Technical Road Blocks – Setting sequence and force transfer of long element at higher temperature, centralization, higher pressures

PS&W
BAKER
HUGHES Baker Oil Tools

Generation 3 Requirements

- MALT Area
 - Freestone Area:
 - 6 1/8" to 6 1/4" Hole ID
 - 10K / 320F
 - Horizontal – 4 to 5 Zones
 - Vernon/Bossier Area:
 - 6 1/8" to 6 1/4" Hole ID
 - 10K / 350 to 375F
 - Horizontal – 4 to 5 Zones
 - Haley Area:
 - 6 1/8" to 6 1/4" Hole ID
 - 10K / 280F
 - Vertical 7 to 9 Zones

EG&W
BAKER
HUGHES Baker Oil Tools

Market Drivers & Opportunities

- Competition:
 - Packers Plus
 - Proven System
- Opportunities
 - Mid Con
 - Generation 1 and Generation 2
 - 6 1/4" Open Hole, 8,500PSI, & 250F
 - MALT
 - Generation 3
 - 6 1/4" Open Hole, 10,000PSI, & 375F

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Iso Frac Packer Testing Update

Test #1: Simulate loads on lower packer

Casing ID: 6.250"
Elastomer: HNBR

Setting Temperature: 250°F
Test Medium: Water

Acceptance Criteria: Able to maintain the hold pressure with the Sprague pump.

Steps:

1. Heat fixture to 250°F
2. Set with 4,000 psi
3. Pressure below element with 5,000 psi and hold for 30 minutes
4. Cool down to 100°F with 5,000 psi below and hold for 30 minutes
5. Reverse to top at 100°F and hold 5,000 psi for 30 minutes
6. Heat back up to 250°F with 5,000 psi above and hold for 30 minutes
7. Reverse pressure to below and repeat steps 3-6 at 8,500 psi, then at 10,000 psi

Results: Passed 5,000 psi cycle. Passed with 8,500 psi below. Leaked when 8,500 psi was reversed to above at 100°F. Setting force was re-applied and the packer held 10,000 psi. There was a leak but 10 ksi was maintained with the Sprague pump. Packing element had evidence of trapped fluid between center elements.

Test #2: Repeat test #1 but start at 8,500 psi. Center elements were re-worked to eliminate trapped fluid problem.

Results: Passed with 8,500 psi below the element. Got to 8,500 psi above the element at 100°F (further than last test), and the crossover to the push/pull device zippered out. Packing element did not show evidence of trapped fluid between the center elements.

Next Test: Repeat test #2 with the test packer, which has stronger threads that connect to the push/pull device. Start test on Monday (12/20/04).

Written by: Gus Weinig 12/15/04

Opportunity Profile 8.0

Submitted By: Erick Peterson	Date Submitted: 11/5/2004	Requested Reply Date:	Requested Ship Date: 12/6/2004
Location: Oklahoma City	Phone: (405) 842-4005		
Is this request for an SAP Quote <input type="checkbox"/>		Reference SAP Quote #	

Request Type-make a selection in both boxes:

Action: Order	Orders Only: Reference PO or STO
Type: New Material Number	Number to Reinstat:

Number of New Products covered by this Opportunity: See Attachment for additional item requirements

Which items in the attachment require action for this Opportunity:

Actions Requested (check all that apply)

<input checked="" type="checkbox"/> SAP Material Number	<input checked="" type="checkbox"/> Delivery	Sales Price: <input type="text"/>
<input type="checkbox"/> Special QA-Include Attachment with Requirements	<input checked="" type="checkbox"/> Standard Cost	<input type="checkbox"/> Transfer Price
<input type="checkbox"/> SAP Order Acknowledgement---Orders only---Non-SAP Districts only		
<input checked="" type="checkbox"/> Extend to Operations District Plant-Include all SAP data for District:		

District Plant #: 0073	Profit Center: 170125400	Sales/Renta: <input type="text"/>
Storage location: <input type="text"/>	Pur.Group: <input type="text"/>	

Other Requirements, Please Describe:

PROJECT DESCRIPTION

Project / Well Name: 582-387 Open Hole Premier Packer	Customer: Multiple Customers
Estimated Total Project Value: \$500,000	

Project Summary:
 Manufacture 6 qty 582-387 Open Hole Premier Packers for use in the Iso-Frac horizontal frac isolation hookups

Brief Well Description

Drill Pipe / Tubing? <input type="text"/>	Casing / Liner? Liner <input type="text"/>	Open Hole Diameter: 6" & 6-1/4"
Size: <input type="text"/>	Size: 4-1/2"	Temperature Range: 250F
Grade: <input type="text"/>	Grade: P-110	Pressure Range: 8500psi
Weight: <input type="text"/>	Weight: 11.60 & 13.50	

Operations Approval Use Only:

Originator: <input type="text"/>	Recommended: <input type="text"/>	Approved: <input type="text"/>
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Tool Description

o Max O.D. 5.820 / Min I.D. 3.844 (blanking dimension for 4-1/2" 13.5 ppf Atlas-Bradford ST-L thread)

o 100°F – 250°F temperature rating, Open hole range 6.00 to 6.25, Non-NACE service

Baker Equivalent Threads Acceptable

Threads up: 4-1/2" 13.50 Flush Joint	Threads down: 4-1/2" 13.50 Flush Joint
Thread Size: <input type="text"/>	Thread Size: <input type="text"/>
Thread Weight: <input type="text"/>	Thread Weight: <input type="text"/>
Tool O.D. Max.: <input type="text"/>	Tool I.D. Max.: <input type="text"/>
Elastomer: <input type="text"/>	Material: <input type="text"/>
Tool I.D. Min.: <input type="text"/>	

Similar to Material Number: Order/Quote Quantity:

The Difference:

Plant Use Only

Weight: <input type="text"/>	Volume: <input type="text"/>	I.D./O.D./Length: <input type="text"/>
Opportunity Profile #: <input type="text"/>	Delivery ARO: <input type="text"/>	
PDM Proejct Type: <input type="text"/>	Cost Each: <input type="text"/>	
SAP Material #: <input type="text"/>	Price Each: <input type="text"/>	<input type="text"/>

Iso-Frac Design and Testing

01/14/05

Requirement--design a packing element system with the following characteristics:

- Utilizes metal Back-up Rings similar to those of the 7" Premier packer
- Has at least 18 inches of uninterrupted rubber visible
- Withstand pressure differentials up to 8,500 psi with minimal leakage
- Must seal in open-hole of up to 6.25" ID, possibly more *6.500"*
work in

Technical Challenges:

- Transferring sufficient force through the long element to expand the uppermost metal Back-up Ring
- Controlling the expansion shape of the long Packing Element in such a way that it creates a seal without the aid of boost
- Storing sufficient energy in the packing element system with limited setting force to maintain a seal if temperature decreases

Methods of Controlling Packing Element Properties to Meet Technical Challenges (singularly or in combination):

- Rubber Durometer *BT*
- Geometrical Features (ID Grooves)
- Shaped Spacer Rings (*secondary*) *teflon*
- Impregnated materials (crush sleeve, fiberglass mesh, helical spring)

Design Evaluation and Verification:

- 1. Start with simplest design (closest to existing, most predictable designs).
- 2. Confirm desired shape of packing element system components with only setting force applied using one of the following methods:
 - o Set in slotted casing
 - o Set in transparent tube
 - o Set in casing and then retrieve
- Change existing design to improve shape of set packing element system components **OR** move to a different design, **OR** run a functional pressure test in a solid piece of casing *or use a piston above*

When Gary is done w/ FEA checks, talk to Jim Coakley about FEA

Design Review Minutes Iso-Frac Packing Element

IWO #: 13005140

Meeting Date: January 26, 2005

Meeting Location: BOT-Navigation

Attendees: Gary Anderson, Dale Cockrell, Jim Doane, Mike Evans, Frank Maenza, Hector Mireles, Gus Weinig

Minutes:

- Listed requirements: 18" Center Packing Element, 8,500 psi at 250°F, compatible with current Premier End Packing Elements and Threaded Back-up Ring system, March delivery.
 - Highlighted the anticipated challenges of developing a working system.
 - * - Gave a tentative test plan: Test prototype in transparent acrylic tube or slotted casing, evaluate, then repeat with another concept or move on to a functional test.
 - Introduced four concepts.
 - Opened question and answer session. ← answer these
- testb 1. Will an asymmetrical element seal from both sides? -Frank M.
 - no 2. Can we use two 9" elements? -Jim D.
 - testb 3. For concept #4, is the spacing between the spacers practical (i.e. 0.1" difference)? -Hector M.
 4. Does setting time matter? Is the setting sequence in our test environment realistic enough, or do we need to try to set it faster? -Dale C.
 5. Does the whole element have to contact the casing, i.e. could the spacers in concept #4 be a continuous piece as long as the element system seals in one spot? -Dale C.
 - testb 6. Do you have to get the fluid out if it becomes trapped in the element? Dale C.
 - no 7. Have we ever tried the glass fiber mesh? -Jim D.
 - note 8. Can the Upper Packing Element be wrapped in Kevlar? -Mike E.
 9. Do you have to seal with the center element [or every element]? -Frank M.
 - * testb → yes 10. Is it possible to test concept #4 by testing a series of conventional 80 hd. short elements without wrapping the OD to cover them up? -Mike E.
 - note designed → too long 11. Could we use petal metal back-ups to reduce the amount of force needed to set the back-up system? -Jim D.
 - ? 12. Could we wrap metal back-up rings into the rubber to control the setting? -Frank M.
 - * ← try a couple different lengths 13. What assumptions can we make of a good element design? What would we need to know to model the problem mathematically or with FEA? -Dale C.
 - * Jim together info 14. What is the critical buckling length of rubber? -Hector M.
 - no time 15. Are there other back-up options, i.e. garter springs? -Jim D.

Action Items:

1. For testing, contact Sean Calahan to find leads on sourcing clear acrylic tube.
-Gary A.

2. Research buckling calculations to determine a critical buckling length for the rubber element. -Jim D.
3. Design and order parts to test a "short" version of concept #4 on the existing test packer, with multiple elements but without the outer sheath. -Gary A.

Minutes written by Gary Anderson, Jan. 28, 2005

Questions to ask search software

- what is the buckling force of a cylindrical-shaped ^{elastomer} piece of rubber

~~what is~~

^{elastomer}

- what is calc. for ν or change with applied force

- what is the force/deflection curve for elastomers

Features vs. Cost – Premier Packer

Feature Removed	Benefit of Removal	Relative Cost	Survey Conclusions from PLM
Chemical Cut	Eliminate packing stack with backup retainers	Low	Yes (needed)
No Body Movement	Less complicated cones and cages, calibrated shear screws unnecessary	Medium	Yes, but AI feels they don't do much stacked
Large ID	Reduce number of pistons, use as-rolled or as-drilled material	Medium (High in conjunction with other changes)	Yes
Low Setting Pressure	Reduce number of pistons	Medium	No std is fine Yes, UKSI needed
Rotationally Locked Bottom Sub	Combine two parts into one	Low	No. How will this affect the interface with the LC Striker? —
High pressure and load ratings/gas tight rating/high temperature ratings	Less complicated cages (no staged release), same slips above and below, looser tolerances, larger setting piston, no element backups required, O-ring back-ups may be Teflon instead of PEEK	High needs to test w/gas to determine slip retrievability, but the gas test could leak I said 2-3 weeks feasibility to do design something (experienced persh)	7,500 psi with current loads ISO 14310 V1 acceptable 6Kst plugged — NO 300 F okay
Reliability	More cast parts	High → Med.	Yes ??
Locked upper slips	Less complicated parts	Low	Yes
Rotational lock	Less mill work	Medium → Low	Yes
Piston pre-set protection	Fewer parts and less complicated cylinder	Medium	Don't understand, what changes on the packer? Yes
Premium end connections	Less expensive Mandrel, Bottom Sub, and coupling	Medium	Yes
Easily retrievable	Fewer parts, shorter less complicated Mandrel	Medium	New Valve - cost ?? \$50/HR ✓ EQQ=5
Aflas available	No PEEK back-ups required for elements, less expensive elements	Low Med. to go to Nitrile	Need Removability
Box x pin	Eliminates coupling or Alt. Seal Bore	Medium	HNBR Pin x Pin okay

Debris Barrier
 want to plug through Benny w/ rolled elements
 *would need to quantify cost savings of non-staged slips to justify cost of testing

Parts List

582-387 Iso-Frac

w/ 4.5" 13.5 lb/ft Buttress Casing Thread, Pin x Pin

See Drawing No. 385-219-00

ITEM	MATERIAL	DESCRIPTION	QTY
1	H036474700	Upper Mandrel	1
2	HWWG51B0B0	5/16-18x3.125 Set Screw	20
3	H036445700	Drift Ring	1
4-10	TBD	Element System	1
11	H036474800	Upper Piston	1
12	HWWGE180BR	1/4-20x5/16 Shear Screw	15
13	H035646600	O-Ring Back Up	8
14	HWWB249P40	O-Ring, Peroxide Nitrile 90 Duro	4
15	H035462500	Upper Back-Up Retainer	2
16	H035466700	O-Ring Back Up	4
17	HWWB348P40	O-Ring, Peroxide Nitrile 90 Duro	2
18	H035462600	Lower Back-Up Retainer	2
19	10067877	Spiral Retainer Ring	2
20	H036474900	Upper Cylinder	1
21	H036475000	Lower Mandrel	1
22	H035780800	Body Lock Ring Housing	1
23	H035782400	Body Lock Ring	1
24	H036475100	Lower Piston	1
25	H036477900	Lower Cylinder	1
26	H036475300	Bottom Sub	1

Iso-Frac Packer Availability

	Packer OD	Packer ID	Hole ID	Initiation Pressure	Setting Pressure	Maximum Temperature	Maximum Torque	Maximum Pressure	Failure Mode
Size 582-387 High Pressure (Available)	5.820"	3.875"	6.250"	2,500 psi	4,000 psi	250°F	16,500 ft-lbs	10,000 psi	Packing Element
Size 582-387 Medium Duty (Available)	5.820"	3.875"	6.250"	2,500 psi	4,000 psi	250°F	12,000 ft-lbs	8,300 psi	Mandrel Tension
Size 365-237 (Not Available*)	3.650"	2.375"	4.000"	2,200 psi	3,500 psi	200°F	3,500 ft-lbs	8,500 psi	Mandrel Tension

* The size 365-237 Iso-Frac packer will be available 6 months after approval of the specifications