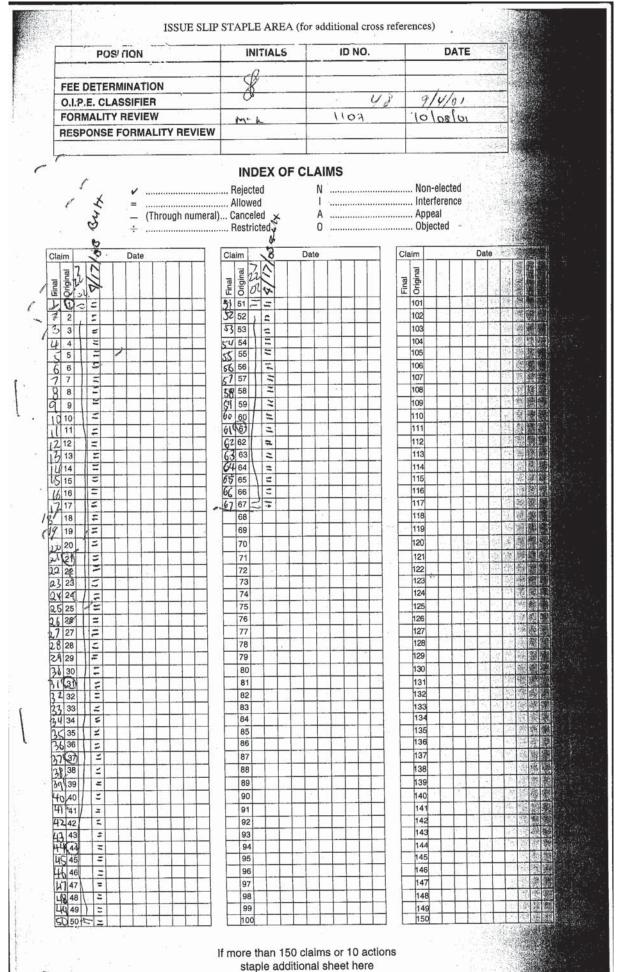
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# ABSTRACT OF THE DISCLOSURE

This invention provides a novel wavelength-separating-routing (WSR) apparatus that uses a diffraction grating to separate a multi-wavelength optical signal by wavelength into multiple spectral channels, which are then focused onto an array of corresponding channel micromirrors. The channel micromirrors are individually controllable and continuously pivotable to reflect the spectral channels into selected output ports. As such, the inventive WSR apparatus is capable of routing the spectral channels on a channel-by-channel basis and coupling any spectral channel into any one of the output ports. The WSR apparatus of the present invention may be further equipped with servo-control and spectral power-management capabilities, thereby maintaining the coupling efficiencies of the spectral channels into the output ports at desired values. The WSR apparatus of the present invention can be used to construct a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs) for WDM optical networking applications.

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### PATENT APPLICATION

# 5 RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES

## INVENTOR

#### Jeffrey P. Wilde

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# CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims priority of U.S. Provisional Patent Application No. 60/277,217, filed 19 March 2001, which is incorporated herein by reference.

# FIELD OF THE INVENTION

This invention relates generally to optical communication systems. More specifically, it relates to a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs) for wavelength division multiplexed optical networking applications.

#### BACKGROUND

As fiber-optic communication networks rapidly spread into every walk of modern life, there is a growing demand for optical components and subsystems that enable the fiber-optic communications networks to be increasingly scalable, versatile, robust, and cost-effective.

25 Contemporary fiber-optic communications networks commonly employ wavelength division multiplexing (WDM), for it allows multiple information (or data) channels to be simultaneously transmitted on a single optical fiber by using different wavelengths and thereby significantly enhances the information bandwidth of the fiber. The prevalence of WDM technology has made optical add-drop multiplexers indispensable building blocks of 30 modern fiber-optic communication networks. An optical add-drop multiplexer (OADM)

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serves to selectively remove (or drop) one or more wavelengths from a multiplicity of wavelengths on an optical fiber, hence taking away one or more data channels from the traffic stream on the fiber. It further adds one or more wavelengths back onto the fiber, thereby inserting new data channels in the same stream of traffic. As such, an OADM makes it possible to launch and retrieve multiple data channels (each characterized by a distinct wavelength) onto and from an optical fiber respectively, without disrupting the overall traffic flow along the fiber. Indeed, careful placement of the OADMs can dramatically improve an optical communication network's flexibility and robustness, while providing significant cost advantages.

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Conventional OADMs in the art typically employ multiplexers/demultiplexers (e.g., waveguide grating routers or arrayed-waveguide gratings), tunable filters, optical switches, and optical circulators in a parallel or serial architecture to accomplish the add and drop functions. In the parallel architecture, as exemplified in U.S. Patent 5,974,207, a demultiplexer (e.g., a waveguide grating router) first separates a multi-wavelength signal into its constituent spectral components. A wavelength switching/routing means (e.g., a combination of optical switches and optical circulators) then serves to drop selective wavelengths and add others. Finally, a multiplexer combines the remaining (i.e., the passthrough) wavelengths into an output multi-wavelength optical signal. In the serial architecture, as exemplified in U.S. Patent 6,205,269, tunable filters (e.g., Bragg fiber gratings) in combination with optical circulators are used to separate the drop wavelengths from the pass-through wavelengths and subsequently launch the add channels into the passthrough path. And if multiple wavelengths are to be added and dropped, additional multiplexers and demultiplexers are required to demultiplex the drop wavelengths and multiplex the add wavelengths, respectively. Irrespective of the underlying architecture, the OADMs currently in the art are characteristically high in cost, and prone to significant optical loss accumulation. Moreover, the designs of these OADMs are such that it is inherently difficult to reconfigure them in a dynamic fashion.

U.S. Patent 6,204,946 to Askyuk et al. discloses an OADM that makes use of free-space optics in a parallel construction. In this case, a multi-wavelength optical signal emerging from an input port is incident onto a ruled diffraction grating. The constituent spectral channels thus separated are then focused by a focusing lens onto a linear array of binary micromachined mirrors. Each micromirror is configured to operate between two discrete states, such that it either retroreflects its corresponding spectral channel back into the input port as a pass-through channel, or directs its spectral channel to an output port as a drop channel. As such, the pass-through signal (i.e., the combined pass-through channels) shares the same input port as the input signal. An optical circulator is therefore coupled to the input port, to provide necessary routing of these two signals. Likewise, the drop channels share the

10 output port with the add channels. An additional optical circulator is thereby coupled to the output port, from which the drop channels exit and the add channels are introduced into the output port. The add channels are subsequently combined with the pass-through signal by way of the diffraction grating and the binary micromirrors.

Although the aforementioned OADM disclosed by Askyuk et al. has the advantage of performing wavelength separating and routing in free space and thereby incurring less optical loss, it suffers a number of limitations. First, it requires that the pass-through signal share the same port/fiber as the input signal. An optical circulator therefore has to be implemented, to provide necessary routing of these two signals. Likewise, all the add and drop channels enter and leave the OADM through the same output port, hence the need for another optical circulator. Moreover, additional means must be provided to multiplex the add channels before entering the system and to demultiplex the drop channels after exiting the system. This additional multiplexing/demultiplexing requirement adds more cost and complexity that

can restrict the versatility of the OADM thus-constructed. Second, the optical circulators 25 implemented in this OADM for various routing purposes introduce additional optical losses, which can accumulate to a substantial amount. Third, the constituent optical components must be in a precise alignment, in order for the system to achieve its intended purpose. There are, however, no provisions provided for maintaining the requisite alignment; and no mechanisms implemented for overcoming degradation in the alignment owing to

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environmental effects such as thermal and mechanical disturbances over the course of operation.

U.S. Patent 5,906,133 to Tomlinson discloses an OADM that makes use of a design similar to that of Aksyuk et al. There are input, output, drop and add ports implemented in this case. By positioning the four ports in a specific arrangement, each micromirror, notwithstanding switchable between two discrete positions, either reflects its corresponding channel (coming from the input port) to the output port, or concomitantly reflects its channel to the drop port and an incident add channel to the output port. As such, this OADM is able to perform both

10 the add and drop functions without involving additional optical components (such as optical circulators used in the system of Aksyuk et al.). However, because a single drop port is designated for all the drop channels and a single add port is designated for all the add channels, the add channels would have to be multiplexed before entering the add port and the drop channels likewise need to be demutiplxed upon exiting from the drop port. Moreover, as in the case of Askyuk et al., there are no provisions provided for maintaining requisite optical alignment in the system, and no mechanisms implemented for combating degradation in the alignment due to environmental effects over the course of operation.

As such, the prevailing drawbacks suffered by the OADMs currently in the art are summarized as follows:

- The wavelength routing is intrinsically static, rendering it difficult to dynamically reconfigure these OADMs.
- Add and/or drop channels often need to be multiplexed and/or demultiplexed, thereby imposing additional complexity and cost.
- 25 3) Stringent fabrication tolerance and painstaking optical alignment are required. Moreover, the optical alignment is not actively maintained, rendering it susceptible to environmental effects such as thermal and mechanical disturbances over the course of operation.

In an optical communication network, OADMs are typically in a ring or cascaded configuration. In order to mitigate the interference amongst OADMs, which often

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adversely affects the overall performance of the network, it is essential that the power levels of spectral channels entering and exiting each OADM be managed in a systematic way, for instance, by introducing power (or gain) equalization at each stage. Such a power equalization capability is also needed for compensating for nonuniform gain caused by optical amplifiers (e.g., erbium doped fiber amplifiers) in the network. There lacks, however, a systematic and dynamic management of the power levels of various spectral channels in these OADMs.

5) The inherent high cost and heavy optical loss further impede the wide application of these OADMs.

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In view of the foregoing, there is an urgent need in the art for optical add-drop multiplexers that overcome the aforementioned shortcomings in a simple, effective, and economical construction.

#### SUMMARY

The present invention provides a wavelength-separating-routing (WSR) apparatus and method which employ an array of fiber collimators serving as an input port and a plurality of output ports; a wavelength-separator; a beam-focuser; and an array of channel micromirrors.

In operation, a multi-wavelength optical signal emerges from the input port. The wavelengthseparator separates the multi-wavelength optical signal into multiple spectral channels, each characterized by a distinct center wavelength and associated bandwidth. The beam-focuser focuses the spectral channels into corresponding spectral spots. The channel micromirrors are positioned such that each channel micromirror receives one of the spectral channels. The

25 channel micromirrors are individually controllable and movable, e.g., continuously pivotable (or rotatable), so as to reflect the spectral channels into selected ones of the output ports. As such, each channel micromirror is assigned to a specific spectral channel, hence the name "channel micromirror". And each output port may receive any number of the reflected spectral channels.

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A distinct feature of the channel micromirrors in the present invention, in contrast to those used in the prior art, is that the motion, e.g., pivoting (or rotation), of each channel micromirror is under analog control such that its pivoting angle can be continuously adjusted. This enables each channel micromirror to scan its corresponding spectral channel across all possible output ports and thereby direct the spectral channel to any desired output port.

In the WSR apparatus of the present invention, the wavelength-separator may be provided by a ruled diffraction grating, a holographic diffraction grating, an echelle grating, a curved diffraction grating, a dispersing prism, or other wavelength-separating means known in the art. The beam-focuser may be a single lens, an assembly of lenses, or other beam-focusing means known in the art. The channel micromirrors may be provided by silicon micromachined mirrors, reflective ribbons (or membranes), or other types of beam-deflecting means known in the art. And each channel micromirror may be pivotable about one or two axes. The fiber collimators serving as the input and output ports may be arranged in a onedimensional or two-dimensional array. In the latter case, the channel micromirrors must be pivotable biaxially.

The WSR apparatus of the present invention may further comprise an array of collimatoralignment mirrors, in optical communication with the wavelength-separator and the fiber collimators, for adjusting the alignment of the input multi-wavelength signal and directing the spectral channels into the selected output ports by way of angular control of the collimated beams. Each collimator-alignment mirror may be rotatable about one or two axes. The collimator-alignment mirrors may be arranged in a one-dimensional or two-dimensional array. First and second arrays of imaging lenses may additionally be optically interposed between the collimator-alignment mirrors and the fiber collimators in a telecentric arrangement, thereby "imaging" the collimator-alignment mirrors onto the corresponding fiber collimators to ensure an optimal alignment.

The WSR apparatus of the present invention may further include a servo-control assembly, in communication with the channel micromirrors and the output ports. The servo-control

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assembly serves to monitor the power levels of the spectral channels coupled into the output ports and further provide control of the channel micromirrors on an individual basis, so as to maintain a predetermined coupling efficiency of each spectral channel in one of the output ports. As such, the servo-control assembly provides dynamic control of the coupling of the spectral channels into the respective output ports and actively manages the power levels of the spectral channels coupled into the output ports. (If the WSR apparatus includes an array of collimator-alignment mirrors as described above, the servo-control assembly may additionally provide dynamic control of the collimator-alignment mirrors.) Moreover, the utilization of such a servo-control assembly effectively relaxes the requisite fabrication tolerances and the precision of optical alignment during assembly of a WSR apparatus of the present invention, and further enables the system to correct for shift in optical alignment over the course of operation. A WSR apparatus incorporating a servo-control assembly thus described is termed a WSR-S apparatus, thereinafter in the present invention.

Accordingly, the WSR-S (or WSR) apparatus of the present invention may be used to construct a variety of optical devices, including a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs), as exemplified in the following embodiments.

One embodiment of an OADM of the present invention comprises an aforementioned WSR-S (or WSR) apparatus and an optical combiner. The output ports of the WSR-S apparatus include a pass-through port and one or more drop ports, each carrying any number of the spectral channels. The optical combiner is coupled to the pass-through port, serving to combine the pass-through channels with one or more add spectral channels. The combined optical signal constitutes an output signal of the system. The optical combiner may be an  $N \times 1$  ( $N \ge 2$ ) broadband fiber-optic coupler, for instance, which also serves the purpose of multiplexing a multiplicity of add spectral channels to be coupled into the system.

In another embodiment of an OADM of the present invention, a first WSR-S (or WSR) apparatus is cascaded with a second WSR-S (or WSR) apparatus. The output ports of the first WSR-S (or WSR) apparatus include a pass-through port and one or more drop ports.

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The second WSR-S (or WSR) apparatus includes a plurality of input ports and an exiting port. The configuration is such that the pass-through channels from the first WSR-S apparatus and one or more add channels are directed into the input ports of the second WSR-S apparatus, and consequently multiplexed into an output multi-wavelength optical signal directed into the exiting port of the second WSR-S apparatus. That is to say that in this embodiment, one WSR-S apparatus (e.g., the first one) effectively performs a dynamic drop function, whereas the other WSR-S apparatus (e.g., the second one) carries out a dynamic add function. And there are essentially no fundamental restrictions on the wavelengths that can be added or dropped, other than those imposed by the overall communication system. Moreover, the underlying OADM architecture thus presented is intrinsically scalable and can be readily extended to any number of the WSR-S (or WSR) systems, if so desired for performing intricate add and drop functions in a network environment.

Those skilled in the art will recognize that the aforementioned embodiments provide only two of many embodiments of a dynamically reconfigurable OADM according to the present invention. Various changes, substitutions, and alternations can be made herein, without departing from the principles and the scope of the invention. Accordingly, a skilled artisan can design an OADM in accordance with the present invention, to best suit a given application.

All in all, the OADMs of the present invention provide many advantages over the prior art devices, notably:

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By advantageously employing an array of channel micromirrors that are individually and continuously controllable, an OADM of the present invention is capable of routing the spectral channels on a channel-by-channel basis and directing any spectral channel into any one of the output ports. As such, its underlying operation is dynamically reconfigurable, and its underlying architecture is intrinsically scalable to a large number of channel counts.

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- 2) The add and drop spectral channels need not be multiplexed and demultiplexed before entering and after leaving the OADM respectively. And there are not fundamental restrictions on the wavelengths to be added or dropped.
- 3) The coupling of the spectral channels into the output ports is dynamically controlled by a servo-control assembly, rendering the OADM less susceptible to environmental effects (such as thermal and mechanical disturbances) and therefore more robust in performance. By maintaining an optimal optical alignment, the optical losses incurred by the spectral channels are also significantly reduced.
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The power levels of the spectral channels coupled into the output ports can be dynamically managed according to demand, or maintained at desired values (e.g., equalized at a predetermined value) by way of the servo-control assembly. This spectral power-management capability as an integral part of the OADM will be particularly desirable in WDM optical networking applications.

The use of free-space optics provides a simple, low loss, and cost-effective construction. Moreover, the utilization of the servo-control assembly effectively relaxes the requisite fabrication tolerances and the precision of optical alignment during initial assembly, enabling the OADM to be simpler and more adaptable in structure, lower in cost and optical loss.

The underlying OADM architecture allows a multiplicity of the OADMs according to the present invention to be readily assembled (e.g., cascaded) for WDM optical networking applications.

The novel features of this invention, as well as the invention itself, will be best understood from the following drawings and detailed description.

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#### BRIEF DESCRIPTION OF THE FIGURES

- FIGS. 1A-1D show a first embodiment of a wavelength-separating-routing (WSR) apparatus according to the present invention, and the modeling results demonstrating the performance of the WSR apparatus;
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FIGS. 2A-2C depict second and third embodiments of a WSR apparatus according to the present invention;

FIG. 3 shows a fourth embodiment of a WSR apparatus according to the present invention;

- FIGS. **4A-4B** show schematic illustrations of two embodiments of a WSR-S apparatus comprising a WSR apparatus and a servo-control assembly, according to the present invention;
- 5 FIG. 5 depicts an exemplary embodiment of an optical add-drop multiplexer (OADM) according to the present invention; and

FIG. 6 shows an alternative embodiment of an OADM according to the present invention.

#### DETAILED DESCRIPTION

10 In this specification and appending claims, a "spectral channel" is characterized by a distinct center wavelength and associated bandwidth. Each spectral channel may carry a unique information signal, as in WDM optical networking applications.

FIG. 1A depicts a first embodiment of a wavelength-separating-routing (WSR) apparatus according to the present invention. By way of example to illustrate the general principles and the topological structure of a wavelength-separating-routing (WSR) apparatus of the present invention, the WSR apparatus 100 comprises multiple input/output ports which may be in the form of an array of fiber collimators 110, providing an input port 110-1 and a plurality of output ports 110-2 through 110-N (N  $\geq$  3); a wavelength-separator which in one form may be a diffraction grating 101; a beam-focuser in the form of a focusing lens 102; and an array of channel micromirrors 103.

In operation, a multi-wavelength optical signal emerges from the input port 110-1. The diffraction grating 101 angularly separates the multi-wavelength optical signal into multiple spectral channels, which are in turn focused by the focusing lens 102 into a spatial array of distinct spectral spots (not shown in FIG. 1A) in a one-to-one correspondence. The channel micromirrors 103 are positioned in accordance with the spatial array formed by the spectral spots, such that each channel micromirror receives one of the spectral channels. The channel micromirrors 103 are individually controllable and movable, e.g., pivotable (or rotatable) under analog (or continuous) control, such that, upon reflection, the spectral channels are directed into selected ones of the output ports 110-2 through 110-N by way of the focusing

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lens 102 and the diffraction grating 101. As such, each channel micromirror is assigned to a specific spectral channel, hence the name "channel micromirror". Each output port may receive any number of the reflected spectral channels.

5 For purposes of illustration and clarity, only a selective few (e.g., three) of the spectral channels, along with the input multi-wavelength optical signal, are graphically illustrated in FIG. 1A and the following figures. It should be noted, however, that there can be any number of the spectral channels in a WSR apparatus of the present invention (so long as the number of spectral channels does not exceed the number of channel mirrors employed in the system).

It should also be noted that the optical beams representing the spectral channels shown in FIG. **1A** and the following figures are provided for illustrative purpose only. That is, their sizes and shapes may not be drawn according to scale. For instance, the input beam and the corresponding diffracted beams generally have different cross-sectional shapes, so long as the angle of incidence upon the diffraction grating is not equal to the angle of diffraction, as is known to those skilled in the art.

In the embodiment of FIG. 1A, it is preferable that the diffraction grating 101 and the channel micromirrors 103 are placed respectively at the first and second (i.e., the front and back) focal points (on the opposing sides) of the focusing lens 102. Such a telecentric arrangement allows the chief rays of the focused beams to be parallel to each other and generally parallel to the optical axis. In this application, the telecentric configuration further allows the reflected spectral channels to be efficiently coupled into the respective output ports, thereby minimizing various translational walk-off effects that may otherwise arise. Moreover, the input multi-wavelength optical signal is preferably collimated and circular in cross-section. The corresponding spectral channels diffracted from the diffraction grating 101 are generally effected in the

elliptical in cross-section; they may be of the same size as the input beam in one dimension and elongated in the other dimension.

It is known that the diffraction efficiency of a diffraction grating is generally polarizationdependent. That is, the diffraction efficiency of a grating in a standard mounting

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configuration may be considerably higher for P-polarization that is perpendicular to the groove lines on the grating than for S-polarization that is orthogonal to P-polarization, especially as the number of groove lines (per unit length) increases. To mitigate such polarization-sensitive effects, a quarter-wave plate 104 may be optically interposed between the diffraction grating 101 and the channel micromirrors 103, and preferably placed between the diffraction grating 101 and the focusing lens 102 as is shown in FIG. 1A. In this way, each spectral channel experiences a total of approximately 90-degree rotation in polarization upon traversing the quarter-wave plate 104 twice. (That is, if a beam of light has P-polarization when first encountering the diffraction grating, it would have predominantly (if not all) S-polarization upon the second encountering, and vice versa.) This ensures that all the spectral channels incur nearly the same amount of round-trip polarization dependent loss.

In the WSR apparatus 100 of FIG. 1A, the diffraction grating 101, by way of example, is oriented such that the focused spots of the spectral channels fall onto the channel micromirrors 103 in a horizontal array, as illustrated in FIG. 1B.

Depicted in FIG. 1B is a close-up view of the channel micromirrors 103 shown in the embodiment of FIG. 1A. By way of example, the channel micromirrors 103 are arranged in a one-dimensional array along the x-axis (i.e., the horizontal direction in the figure), so as to receive the focused spots of the spatially separated spectral channels in a one-to-one correspondence. (As in the case of FIG. 1A, only three spectral channels are illustrated, each represented by a converging beam.) Let the reflective surface of each channel micromirror lie in the x-y plane as defined in the figure and be movable, e.g., pivotable (or deflectable) about the x-axis in an analog (or continuous) manner. Each spectral channel, upon reflection, is deflected in the y-direction (e.g., downward) relative to its incident direction, so to be directed into one of the output ports 110-2 through 110-N shown in FIG. 1A.

As described above, a unique feature of the present invention is that the motion of each channel micromirror is individually and continuously controllable, such that its position, e.g., pivoting angle, can be continuously adjusted. This enables each channel micromirror to scan

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its corresponding spectral channel across all possible output ports and thereby direct the spectral channel to any desired output port. To illustrate this capability, FIG. 1C shows a plot of coupling efficiency as a function of a channel micromirror's pivoting angle  $\theta$ , provided by a ray-tracing model of a WSR apparatus in the embodiment of FIG. 1A. As used herein, the coupling efficiency for a spectral channel is defined as the ratio of the amount of optical power coupled into the fiber core in an output port to the total amount of optical power incident upon the entrance surface of the fiber (associated with the fiber collimator serving as the output port). In the ray-tracing model, the input optical signal is incident upon a diffraction grating with 700 lines per millimeter at a grazing angle of 85 degrees, where the grating is blazed to optimize the diffraction efficiency for the "-1" order. The focusing lens has a focal length of 100 mm. Each output port is provided by a quarter-pitch GRIN lens (2 mm in diameter) coupled to an optical fiber (see FIG. 1D). As displayed in FIG. 1C, the coupling efficiency varies with the pivoting angle  $\theta$ , and it requires about a 0.2-degree change in  $\theta$  for the coupling efficiency to become practically negligible in this exemplary case. As such, each spectral channel may practically acquire any coupling efficiency value by way of controlling the pivoting angle of its corresponding channel micromirror. This is also to say that variable optical attenuation at the granularity of a single wavelength can be obtained in a WSR apparatus of the present invention. FIG. 1D provides ray-tracing illustrations of two extreme points on the coupling efficiency vs. 0 curve of FIG. 1C: on-axis coupling corresponding to  $\theta = 0$ , where the coupling efficiency is maximum; and off-axis coupling corresponding to  $\theta = 0.2$  degrees, where the representative collimated beam (representing an exemplary spectral channel) undergoes a significant translational walk-off and renders the coupling efficiency practically negligible. All in all, the exemplary modeling results thus described demonstrate the unique capabilities of the WSR apparatus of the present invention.

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FIG. 1A provides one of many embodiments of a WSR apparatus according to the present invention. In general, the wavelength-separator is a wavelength-separating means that may be a ruled diffraction grating, a holographic diffraction grating, an echelle grating, a dispersing prism, or other types of spectral-separating means known in the art. The beamfocuser may be a focusing lens, an assembly of lenses, or other beam-focusing means known

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in the art. The focusing function may also be accomplished by using a curved diffraction grating as the wavelength-separator. The channel micromirrors may be provided by silicon micromachined mirrors, reflective ribbons (or membranes), or other types of beam-deflecting elements known in the art. And each micromirror may be pivoted about one or two axes.

- 5 What is important is that the pivoting (or rotational) motion of each channel micromirror be individually controllable in an analog manner, whereby the pivoting angle can be continuously adjusted so as to enable the channel micromirror to scan a spectral channel across all possible output ports. The underlying fabrication techniques for micromachined mirrors and associated actuation mechanisms are well documented in the art, see U.S. Patent
- 10 5,629,790 for example. Moreover, a fiber collimator is typically in the form of a collimating lens (such as a GRIN lens) and a ferrule-mounted fiber packaged together in a mechanically rigid stainless steel (or glass) tube. The fiber collimators serving as the input and output ports may be arranged in a one-dimensional array, a two-dimensional array, or other desired spatial pattern. For instance, they may be conveniently mounted in a linear array along a V-groove F 15 TU fabricated on a substrate made of silicon, plastic, or ceramic, as commonly practiced in the art. It should be noted, however, that the input port and the output ports need not necessarily be in close spatial proximity with each other, such as in an array configuration (although a close packing would reduce the rotational range required for each channel micromirror). Those skilled in the art will know how to design a WSR apparatus according to the present () 20 invention, to best suit a given application.

A WSR apparatus of the present invention may further comprise an array of collimatoralignment mirrors, for adjusting the alignment of the input multi-wavelength optical signal and facilitating the coupling of the spectral channels into the respective output ports, as shown in FIGS. 2A-2B and 3.

Depicted in FIG. 2A is a second embodiment of a WSR apparatus according to the present invention. By way of example, WSR apparatus 200 is built upon and hence shares a number of the elements used in the embodiment of FIG. 1A, as identified by those labeled with identical numerals. Moreover, a one-dimensional array 220 of collimator-alignment mirrors

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220-1 through 220-N is optically interposed between the diffraction grating 101 and the fiber collimator array 110. The collimator-alignment mirror 220-1 is designated to correspond with the input port 110-1, for adjusting the alignment of the input multi-wavelength optical signal and therefore ensuring that the spectral channels impinge onto the corresponding channel micromirrors. The collimator-alignment mirrors 220-2 through 220-N are designated to the output ports 110-2 through 110-N in a one-to-one correspondence, serving to provide angular control of the collimated beams of the reflected spectral channels and thereby facilitating the coupling of the spectral channels into the respective output ports according to desired coupling efficiencies. Each collimator-alignment mirror may be rotatable about one axis, or two axes.

The embodiment of FIG. 2A is attractive in applications where the fiber collimators (serving as the input and output ports) are desired to be placed in close proximity to the collimatoralignment mirror array 220. To best facilitate the coupling of the spectral channels into the output ports, arrays of imaging lenses may be implemented between the collimator-alignment mirror array 220 and the fiber collimator array 110, as depicted in FIG. 2B. By way of example, WSR apparatus 250 of FIG. 2B is built upon and hence shares many of the elements used in the embodiment of FIG. 2A, as identified by those labeled with identical numerals. Additionally, first and second arrays 260, 270 of imaging lenses are placed in a 4-f telecentric arrangement with respect to the collimator-alignment mirror array 220 and the fiber collimator alignment mirror array 220 and the fiber collimator array 110. The dashed box 280 shown in FIG. 2C provides a top view of such a telecentric arrangement. In this case, the imaging lenses in the first and second arrays 260, 270 all have the same focal length f. The collimator-alignment mirrors 220-1 through 220-N are placed at the respective first (or front) focal points of the imaging lenses in the first array

25 260. Likewise, the fiber collimators 110-1 through 110-N are placed at the respective second (or back) focal points of the imaging lenses in the second array 270. And the separation between the first and second arrays 260, 270 of imaging lenses is 2f. In this way, the collimator-alignment mirrors 220-1 through 220-N are effectively imaged onto the respective entrance surfaces (i.e., the front focal planes) of the GRIN lenses in the corresponding fiber collimators 110-1 through 110-N. Such a telecentric imaging system substantially eliminates

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translational walk-off of the collimated beams at the output ports that may otherwise occur as the mirror angles change.

FIG. 3 shows a fourth embodiment of a WSR apparatus according to the present invention. 5 By way of example, WSR apparatus 300 is built upon and hence shares a number of the elements used in the embodiment of FIG. 2B, as identified by those labeled with identical numerals. In this case, the one-dimensional fiber collimator array 110 of FIG. 2B is replaced by a two-dimensional array 350 of fiber collimators, providing for an input-port and a plurality of output ports. Accordingly, the one-dimensional collimator-alignment mirror 10 array 220 of FIG. 2B is replaced by a two-dimensional array 320 of collimator-alignment mirrors, and first and second one-dimensional arrays 260, 270 of imaging lenses of FIG. 2B are likewise replaced by first and second two-dimensional arrays 360, 370 of imagining lenses respectively. As in the case of the embodiment of FIG. 2B, the first and second twodimensional arrays 360, 370 of imaging lenses are placed in a 4-f telecentric arrangement with respect to the two-dimensional collimator-alignment mirror array 320 and the twodimensional fiber collimator array 350. The channel micromirrors 103 must be pivotable biaxially in this case (in order to direct its corresponding spectral channel to any one of the output ports). As such, the WSR apparatus 300 is equipped to support a greater number of the output ports.

In addition to facilitating the coupling of the spectral channels into the respective output ports as described above, the collimator-alignment mirrors in the above embodiments also serve to compensate for misalignment (e.g., due to fabrication and assembly errors) in the fiber collimators that provide for the input and output ports. For instance, relative misalignment between the fiber cores and their respective collimating lenses in the fiber collimators can lead to pointing errors in the collimated beams, which may be corrected for by the collimatoralignment mirrors. For these reasons, the collimator-alignment mirrors are preferably rotatable about two axes. They may be silicon micromachined mirrors, for fast rotational speeds. They may also be other types of mirrors or beam-deflecting elements known in the

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To optimize the coupling of the spectral channels into the output ports and further maintain the optimal optical alignment against environmental effects such as temperature variations and mechanical instabilities over the course of operation, a WSR apparatus of the present invention may incorporate a servo-control assembly, for providing dynamic control of the coupling of the spectral channels into the respective output ports on a channel-by-channel A WSR apparatus incorporating a servo-control assembly is termed a WSR-S basis. apparatus, thereinafter in this specification.

10 FIG. 4A depicts a schematic illustration of a first embodiment of a WSR-S apparatus according to the present invention. The WSR-S apparatus 400 comprises a WSR apparatus 410 and a servo-control assembly 440. The WSR 410 may be in the embodiment of FIG. 1A, or any other embodiment in accordance with the present invention. The servo-control assembly 440 includes a spectral monitor 460, for monitoring the power levels of the spectral channels coupled into the output ports 420-1 through 420-N of the WSR apparatus 410. By 15 way of example, the spectral monitor 460 is coupled to the output ports 420-1 through 420-N by way of fiber-optic couplers 420-1-C through 420-N-C, wherein each fiber-optic coupler serves to tap off a predetermined fraction of the optical signal in the corresponding output The servo-control assembly 440 further includes a processing unit 470, in port. 门 20 communication with the spectral monitor 460 and the channel micromirrors 430 of the WSR ĥd apparatus 410. The processing unit 470 uses the power measurements from the spectral monitor 460 to provide feedback control of the channel micromirrors 430 on an individual basis, so as to maintain a desired coupling efficiency for each spectral channel into a selected output port. As such, the servo-control assembly 440 provides dynamic control of the 25 coupling of the spectral channels into the respective output ports on a channel-by-channel basis and thereby manages the power levels of the spectral channels coupled into the output ports. The power levels of the spectral channels in the output ports may be dynamically managed according to demand, or maintained at desired values (e.g., equalized at a predetermined value) in the present invention. Such a spectral power-management capability 30 is essential in WDM optical networking applications, as discussed above.

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FIG. 4B depicts a schematic illustration of a second embodiment of a WSR-S apparatus according to the present invention. The WSR-S apparatus 450 comprises a WSR apparatus 480 and a servo-control assembly 490. In addition to the channel micromirrors 430 (and other elements identified by the same numerals as those used in FIG. 4A), the WSR apparatus 480 further includes a plurality of collimator-alignment mirrors 485, and may be configured. according to the embodiment of FIG. 2A, 2B, 3, or any other embodiment in accordance with the present invention. By way of example, the servo-control assembly 490 includes the spectral monitor 460 as described in the embodiment of FIG. 4A, and a processing unit 495. In this case, the processing unit 495 is in communication with the channel micromirrors 430 and the collimator-alignment mirrors 485 of the WSR apparatus 480, as well as the spectral monitor 460. The processing unit 495 uses the power measurements from the spectral monitor 460 to provide dynamic control of the channel micromirrors 430 along with the collimator-alignment mirrors 485, so to maintain the coupling efficiencies of the spectral channels into the output ports at desired values.

In the embodiment of FIG. 4A or 4B, the spectral monitor 460 may be one of spectral power monitoring devices known in the art that is capable of detecting the power levels of spectral components in a multi-wavelength optical signal. Such devices are typically in the form of a wavelength-separating means (e.g., a diffraction grating) that spatially separates a multiwavelength optical signal by wavelength into constituent spectral components, and one or more optical sensors (e.g., an array of photodiodes) that are configured such to detect the power levels of these spectral components. The processing unit 470 in FIG. 4A (or the processing unit 495 in FIG. 4B) typically includes electrical circuits and signal processing 25 programs for processing the power measurements received from the spectral monitor 460 and generating appropriate control signals to be applied to the channel micromirrors 430 (and the collimator-alignment mirrors 485 in the case of FIG. 4B), so to maintain the coupling efficiencies of the spectral channels into the output ports at desired values. The electronic circuitry and the associated signal processing algorithm/software for such processing unit in a 30 servo-control system are known in the art. A skilled artisan will know how to implement a

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suitable spectral monitor along with an appropriate processing unit to provide a servo-control assembly in a WSP-S apparatus according to the present invention, for a given application.

The incorporation of a servo-control assembly provides additional advantages of effectively relaxing the requisite fabrication tolerances and the precision of optical alignment during initial assembly of a WSR apparatus of the present invention, and further enabling the system to correct for shift in the alignment over the course of operation. By maintaining an optimal optical alignment, the optical losses incurred by the spectral channels are also significantly reduced. As such, the WSR-S apparatus thus constructed is simpler and more adaptable in structure, more robust in performance, and lower in cost and optical loss. Accordingly, the WSR-S (or WSR) apparatus of the present invention may be used to construct a variety of optical devices and utilized in many applications.

For instance, by directing the spectral channels into the output ports in a one-channel-per-port fashion and coupling the output ports of a WSR-S (or WSR) apparatus to an array of optical sensors (e.g., photodiodes), or a single optical sensor that is capable of scanning across the output ports, a dynamic and versatile spectral power monitor (or channel analyzer) is provided, which would be highly desired in WDM optical networking applications. Moreover, a novel class of optical add-drop multiplexers (OADMs) may be built upon the WSR-S (or WSR) apparatus of the present invention, as exemplified in the following embodiments.

FIG. 5 depicts an exemplary embodiment of an optical add-drop multiplexer (OADM) according to the present invention. By way of example, OADM 500 comprises a WSR-S (or WSR) apparatus 510 and an optical combiner 550. An input port 520 of the WSR-S apparatus 510 transmits a multi-wavelength optical signal. The constituent spectral channels are subsequently separated and routed into a plurality of output ports, including a pass-through port 530 and one or more drop ports 540-1 through 540-N (N  $\geq$  1). The pass-through port 530 may receive any number of the spectral channels (i.e., the pass-through spectral channels). Each drop port may also receive any number of the spectral channels (i.e., the

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drop spectral channels). The pass-through port 530 is optically coupled to the optical combiner 550, which serves to combine the pass-through spectral channels with one or more add spectral channels provided by one or more add ports 560-1 through 560-M ( $M \ge 1$ ). The combined optical signal is then routed into an existing port 570, providing an output multi-wavelength optical signal.

In the above embodiment, the optical combiner 550 may be a K×1 (K  $\ge$  2) broadband fiberoptic coupler, wherein there are K input-ends and one output-end. The pass-through spectral channels and the add spectral channels are fed into the K input-ends (e.g., in a one-to-one correspondence) and the combined optical signal exits from the output-end of the K×1 fiberoptic coupler as the output multi-wavelength optical signal of the system. Such a multipleinput coupler also serves the purpose of multiplexing a multiplicity of add spectral channels to be coupled into the OADM 500. If the power levels of the spectral channels in the output multi-wavelength optical signal are desired to be actively managed, such as being equalized at a predetermined value, two spectral monitors may be utilized. As a way of example, the first spectral monitor may receive optical signals tapped off from the pass-through port 530 and the drop ports 540-1 through 540-N (e.g., by way of fiber-optic couplers as depicted in FIG. 4A or 4B). The second spectral monitor receives optical signals tapped off from the exiting port 570. A servo-control system may be constructed accordingly for monitoring and controlling the pass-through, drop and add spectral channels. As such, the embodiment of FIG. 5 provides a versatile optical add-drop multiplexer in a simple and low-cost assembly, while providing multiple physically separate drop/add ports in a dynamically reconfigurable fashion.

FIG. 6 depicts an alternative embodiment of an optical add-drop multiplexer (OADM) according to the present invention. By way of example, OADM 600 comprises a first WSR-S apparatus 610 optically coupled to a second WSR-S apparatus 650. Each WSR-S apparatus may be in the embodiment of FIG. 4A or 4B. (A WSR apparatus of the embodiment of FIG. 1A, 2A, 2B, or 3 may be alternatively implemented.) The first WSR-S apparatus 610 includes an input port 620, a pass-through port 630, and one or more drop ports 640-1

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through 640-N (N  $\geq$  1). The pass-through spectral channels from the pass-through port 630 are further coupled to the second WSR-S apparatus 650, along with one or more add spectral channels emerging from add ports 660-1 through 660-M (M  $\geq$  1). In this exemplary case, the pass-through port 630 and the add ports 660-1 through 660-M constitute the input ports for the second WSR-S apparatus 650. By way of its constituent wavelength-separator (e.g., a diffraction grating) and channel micromirrors (not shown in FIG. 6), the second WSR-S apparatus 650 serves to multiplex the pass-through spectral channels and the add spectral channels, and route the multiplexed optical signal into an exiting port 770 to provide an output signal of the system.

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In the embodiment of FIG. 6, one WSR-S apparatus (e.g., the first WSR-S apparatus 610) effectively performs dynamic drop function, whereas the other WSR-S apparatus (e.g., the second WSR-S apparatus 650) carries out dynamic add function. And there are essentially no fundamental restrictions on the wavelengths that can be added or dropped (other than those imposed by the overall communication system). Moreover, the underlying OADM architecture thus presented is intrinsically scalable and can be readily extended to any number of cascaded WSR-S (or WSR) systems, if so desired for performing intricate add and drop functions. Additionally, the OADM of FIG. 6 may be operated in reverse direction, by using the input ports as the output ports, the drop ports as the add ports, and vice versa.

Those skilled in the art will recognize that the aforementioned embodiments provide only two of many embodiments of a dynamically reconfigurable OADM according to the present invention. Those skilled in the art will also appreciate that various changes, substitutions, and alternations can be made herein without departing from the principles and the scope of the invention as defined in the appended claims. Accordingly, a skilled artisan can design an OADM in accordance with the principles of the present invention, to best suit a given application.

Although the present invention and its advantages have been described in detail, it should be understood that various changes, substitutions, and alternations can be made herein without

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departing from the principles and the scope of the invention. Accordingly, the scope of the present invention should be determined by the following claims and their legal equivalents.

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# CLAIMS

What is claimed is:

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13 4 |4 1. A wavelength-separating-routing apparatus, comprising:

- a) multiple fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- a wavelength-separator, for separating said multi-wavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots; and
  - d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously controllable to reflect said spectral channels into selected ones of said output ports.
- The wavelength-separating-routing apparatus of claim 1 further comprising a servocontrol assembly, in communication with said channel micromirrors and said output ports, for providing control of said channel micromirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.
- 3. The wavelength-separating-routing apparatus of claim 2 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors.
- 4. The wavelength-separating-routing apparatus of claim 3 wherein said servo-control assembly maintains said power levels at a predetermined value.

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5. The wavelength-separating-routing apparatus of claim 1 further comprising an array of collimator-alignment mirrors, in optical communication with said wavelength-separator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

6. The wavelength-separating-routing apparatus of claim 5 wherein each collimatoralignment mirror is rotatable about one axis.

The wavelength-separating-routing apparatus of claim 5 wherein each collimatoralignment mirror is rotatable about two axes.

 The wavelength-separating-routing apparatus of claim 5 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimatoralignment mirrors and said fiber collimators.

 The wavelength-separating-routing apparatus of claim 1 wherein each channel micromirror is continuously pivotable about one axis.

The wavelength-separating-routing apparatus of claim 1 wherein each channel
 micromirror is pivotable about two axes.

 The wavelength-separating-routing apparatus of claim 10 wherein said fiber collimators are arranged in a two-dimensional array.

1 12. The wavelength-separating-routing apparatus of claim 1 wherein each channel
 micromirror is a silicon micromachined mirror.

1 13. The wavelength-separating-routing apparatus of claim 1 wherein said fiber
 2 collimators are arranged in a one-dimensional array.

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	1	14.	The wavelength-separating-routing apparatus of claim 1 wherein said beam-focuser
	2		comprises a focusing lens having first and second focal points.
	3		
	1	15.	The wavelength-separating-routing apparatus of claim 14 wherein said wavelength-
	2		separator and said channel micromirrors are placed respectively at said first and
	3		second focal points of said focusing lens.
	4		
	1	16.	The wavelength-separating-routing apparatus of claim 1 wherein said beam-focuser
	2		comprises an assembly of lenses.
	3		
	1	17.	The wavelength-separating-routing apparatus of claim 1 wherein said wavelength-
ប្រ	2		separator comprises an element selected from the group consisting of ruled diffraction
	3		gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings,
	4		and dispersing prisms.
сП я	5		
0	1	18.	The wavelength-separating-routing apparatus of claim 1 further comprising a quarter-
ΓIJ	2		wave plate optically interposed between said wavelength-separator and said channel
	3		micromirrors.
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	1	19.	The wavelength-separating-routing apparatus of claim 1 wherein each output port
	2		carries a single one of said spectral channels.
	3		
	1	20.	The wavelength-separating-routing apparatus of claim 19 further comprising one or
	2		more optical sensors, optically coupled to said output ports.
	3		
	1	21.	A servo-based optical apparatus comprising:
	2		a) multiple fiber collimators, providing an input port for a multi-wavelength
	3		optical signal and a plurality of output ports;
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	4		b) a wavelength-separator, for separating said multi-wavelength optical signal
	5		from said input port into multiple spectral channels;
	6 7		<ul> <li>a beam-focuser, for focusing said spectral channels into corresponding spectral spots;</li> </ul>
	8		d) a spatial array of channel micromirrors positioned such that each channel
	9		micromirror receives one of said spectral channels, said channel micromirrors
	10		being individually controllable to reflect said spectral channels into selected
	11		ones of said output ports; and
	12		e) a servo-control assembly, in communication with said channel micromirrors
	13		and said output ports, for maintaining a predetermined coupling of each
	14		reflected spectral channel into one of said output ports.
00	15		fontotion spectrul chainer into one of suid output ports.
	1	22.	The servo-based optical apparatus of claim 21 wherein said servo-control assembly
	2		comprises a spectral monitor for monitoring power levels of said spectral channels
	3		coupled into said output ports, and a processing unit responsive to said power levels
())	4		for providing control of said channel micromirrors.
а (3)	5		
co ru	1	23.	The servo-based optical apparatus of claim 22 wherein said servo-control assembly
ų	2		maintains said power levels at a predetermined value.
ALL ALL	3		
	1	24.	The servo-based optical apparatus of claim 21 further comprising an array of
	2		collimator-alignment mirrors, in optical communication with said wavelength-
	3		separator and said fiber collimators, for adjusting an alignment of said multi-
4	4		wavelength optical signal from said input port and directing said reflected spectral
	5		channels into said output ports.
	6		್ಷ ಕೊಂಡಿ ತ
	1	25.	The servo-based optical apparatus of claim 24 further comprising first and second
	2		arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment
	3		mirrors and said fiber collimators.
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	1	26.	The servo-based optical apparatus of claim 24 wherein each collimator-alignment
	2		mirror is rotatable about at least one axis.
	2		
6	1	27.	The servo-based optical apparatus of claim 21 wherein each channel micromirror is
	2	27.	continuously pivotable about at least one axis.
	3		
	1	28.	The servo-based optical apparatus of claim 21 wherein each channel micromirror is a
	2		silicon micromachined mirror.
	3		
00	1	29.	The servo-based optical apparatus of claim 21 wherein said wavelength-separator
	2		comprises an element selected from the group consisting of ruled diffraction gratings,
	3		holographic diffraction gratings, echelle gratings, curved diffraction gratings, and
ъD.	4	0	dispersing prisms.
	5		
E Tunt	• 1	30.	The servo-based optical apparatus of claim 21 wherein said beam-focuser comprises
ţ'n	2		one or more lenses.
ь С	3		
CO FU	1	31.	An optical apparatus comprising:
LU	2	2 .	a) an array of fiber collimators, providing an input port for a multi-wavelength
		3	optical signal and a plurality of output ports;
		4 8	b) a wavelength-separator, for separating said multi-wavelength optical signal
	4	5 <b>3</b>	from said input port into multiple spectral channels;
		6 (	c) a beam-focuser, for focusing said spectral channels into corresponding
		7	spectral spots;
		8	d) a spatial array of channel micromirrors positioned such that each channel
		9	micromirror receives one of said spectral channels, said channel micromirrors
	1	10	being individually controllable to reflect said spectral channels into selected
		11	ones of said output ports; and

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a one-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

32. The optical apparatus of claim 31 further comprising a servo-control assembly, in communication with said channel micromirrors, said collimator-alignment mirrors, and said output ports, for providing control of said channel micromirrors along with said collimator-alignment mirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

The optical apparatus of claim 32 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors and said collimator-alignment mirrors.

34. The optical apparatus of claim 31 wherein each channel micromirror is continuously pivotable about at least one axis.

35. The optical apparatus of claim 31 wherein each collimator-alignment mirror is rotatable about at least one axis.

36. The optical apparatus of claim 31 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

37. An optical apparatus comprising:

an array of fiber collimators, providing an input port for a multi-wavelength
 optical signal and a plurality of output ports;

b) a wavelength-separator, for separating said multi-wavelength optical signal from said input port into multiple spectral channels;

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a beam-focuser, for focusing said spectral channels into corresponding spectral spots;

a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually controllable to reflect said spectral channels into selected ones of said output ports; and

a two-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

The optical apparatus of claim 37 further comprising a servo-control assembly, in communication with said channel micromirrors, said collimator-alignment mirrors, and said output ports, for providing control of said channel micromirrors along with said collimator-alignment mirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

The optical apparatus of claim 38 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors and said collimator-alignment mirrors.

40. The optical apparatus of claim 37 wherein each collimator-alignment mirror is rotatable about at least one axis.

41. The optical apparatus of claim 37 wherein each channel micromirror is continuously pivotable about at least one axis.

42. The optical apparatus of claim 41 wherein each channel micromirrors is pivotable about two axes, and wherein said fiber collimators are arranged in a two-dimensional array.

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	1	43.	The optical apparatus of claim 37 further comprising first and second arrays of
	2	e - 3	imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors
	3		and said fiber collimators.
	4	(6)	
5	1	44.	An optical system comprising a wavelength-separating-routing apparatus, wherein
	2		said wavelength-separating-routing apparatus includes:
	3	2	a) an array of fiber collimators, providing an input port for a multi-wavelength
	4		optical signal and a plurality of output ports including a pass-through port and
	5		one or more drop ports;
505	6		b) a wavelength-separator, for separating said multi-wavelength optical signal
	7		from said input port into multiple spectral channels;
10	8		c) a beam-focuser, for focusing said spectral channels into corresponding
304 <u>-</u>	9		spectral spots; and
-F FU	10		d) a spatial array of channel micromirrors positioned such that each channel
ſN	11		micromirror receives one of said spectral channels, said channel micromirrors
	12		being individually and continuously pivotable to reflect said spectral channels
io ru	13		into selected ones of said output ports, whereby said pass-through port
5	14		receives a subset of said spectral channels.
	15		A
	1	45.	The optical system of claim 44 further comprising a servo-control assembly, in
	2		communication with said channel micromirrors and said output ports, for providing
	3		control of said channel micromirrors and thereby maintaining a predetermined
	4		coupling of each reflected spectral channel into one of said output ports.
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	1	46.	The optical system of claim 45 wherein said servo-control assembly comprises a
	2		spectral monitor for monitoring power levels of said spectral channels coupled into
	3		said output ports, and a processing unit responsive to said power levels for providing
	4		control of said channel micromirrors.
	5		

- 47. The optical system of claim 44 further comprising an array of collimator-alignment mirrors, in optical communication with said wavelength-separator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.
- The optical system of claim 47 further comprising first and second arrays of imaging 48. lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.
- 49. The optical system of claim 47 wherein each collimator-alignment mirror is rotatable about at least one axis.
- 50. The optical system of claim 44 wherein each channel micromirror is pivotable about at least one axis.

51. The optical system of claim 44 wherein each channel micromirror is a silicon micromachined mirror.

52. The optical system of claim 44 wherein said beam-focuser comprises a focusing lens having first and second focal points, and wherein said wavelength-separator and said channel micromirrors are placed respectively at said first and second focal points.

53. The optical system of claim 44 wherein said wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

54. The optical system of claim 44 further comprising a quarter-wave plate optically interposed between said wavelength-separator and said channel micromirrors.

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	1	55.	The optical system of claim 44 further comprising an auxiliary wavelength-
	2		separating-routing apparatus, including:
	3		a) multiple auxiliary fiber collimators, providing a plurality of auxiliary input
	4		ports and an exiting port;
	5		b) an auxiliary wavelength-separator;
	6		c) an auxiliary beam-focuser; and
	7		d) a spatial array of auxiliary channel micromirrors;
	8		wherein said subset of said spectral channels in said pass-through port and one or
	9		more add spectral channels are directed into said auxiliary input ports, and
	10	×.	multiplexed into an output optical signal directed into said exiting port by way of
	11		said auxiliary wavelength-separator, said auxiliary beam-focuser and said
0	12		auxiliary channel micromirrors.
50	13		
10 LJ	1	56.	The optical system of claim 55 wherein said auxiliary channel micromirrors are
Ta Ca	2		individually pivotable.
ru	3		
ព្រា	1	57.	The optical system of claim 55 wherein each auxiliary channel micromirror is
C) (0)	2		pivotable continuously about at least one axis.
ru	3		
	1	58.	The optical system of claim 55 wherein each auxiliary channel micromirror is a
¥.ah	2		silicon micromachined mirror.
	3		
	1	59.	The optical system of claim 55 wherein said auxiliary wavelength-separator comprises
	2		an element selected from the group consisting of ruled diffraction gratings,
	3		holographic diffraction gratings, echelle gratings, curved diffraction gratings, and
	4		dispersing prisms.
	5		
	1	60.	The optical system of claim 55 wherein said pass-through port constitutes one of said
	2	1920-092	auxiliary input ports.
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	1	61.	A method of performing dynamic wavelength separating and routing, comprising:
	2		a) receiving a multi-wavelength optical signal from an input port;
	3		b) separating said multi-wavelength optical signal into multiple spectral channels;
	4		c) focusing said spectral channels onto a spatial array of corresponding beam-
	5		deflecting elements, whereby each beam-deflecting element receives one of
	6		said spectral channels; and
	7		d) dynamically and continuously controlling said beam-deflecting elements,
	8		thereby directing said spectral channels into a plurality of output ports.
	9		
	1	62.	The method of claim 61 further comprising the step of providing feedback control of
	2		said beam-deflecting elements, thereby maintaining a predetermining coupling of each
5	3		spectral channel directed into one of said output ports.
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	1	63.	The method of claim 62 further comprising the step of maintaining power levels of
	2		said spectral channels directed into said output ports at a predetermining value.
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	1	64.	The method of claim 61 wherein each spectral channel is directed into a separate
) 0	2		output port.
	3		
5	1	65.	The method of claim 61 wherein a subset of said spectral channels is directed into one
di,	2		of said output ports, thereby providing one or more pass-through spectral channels.
	3		
	- 1	66.	The method of claim 65 further comprising the step of multiplexing said pass-through
	2	- 47	spectral channels with one or more add spectral channels, so as to provide an output
	3		optical signal.
	4		
	1	67.	The method of claim 61 wherein said beam-deflecting elements comprise an array of
	2		silicon micromachined mirrors.
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## DECLARATION AND POWER OF ATTORNEY

#### DECLARATION:

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As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe, I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled **RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES:** 

X is attached hereto.

- was filed as United States Application
- Serial No. \_\_\_\_\_ on and was amended on

(if applicable).

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to the examination of this application in accordance with Title 37, Code of Federal Regulations, §1.56(a).

I hereby claim foreign priority benefits under Title 35, United States Code, §119 of any foreign application(s) for patent or inventor's certificate or of any PCT international application(s) designating at least one country other than the United States of America listed below and have also identified below any foreign application(s) for patent or inventor's certificate or any PCT international application(s) designating at least one country other than the United States of America filed below any foreign application at least one country other than the United States of America filed by me on the same subject matter having a filing date before that of the application(s) on which priority is claimed:

PRIOR FOREIGN/PCT APPLICATION(S) AND ANY PRIORITY CLAIMS UNDER 35 U.S.C. 119:

Country (If PCT, indicate PCT)	Application Number	Date Filed	Priority Claimed (Yes/No)

I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) or PCT international application(s) designating the United States of America that is/are listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in that/those prior application(s) in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, §1.56(a) which occurred between the filing date of the prior application(s) and the national or PCT international filing date of this application:

U.S. AP	PLICATIONS	STATUS (check one)			
UMBER	U.	S. FILING DATE	PATENTED	PENDING	ABANDONED
	3/19/200	1		X	3
18406620					Ω.
CATIONS	DESIGNAT	ING THE U.S.			
PCT FIL	ING DATE	U.S. SERIAL NUMBERS ASSIGNED (if any)			
	25/7				
		3/19/200	UMBER U.S. FILING DATE 3/19/2001 CATIONS DESIGNATING THE U.S. PCT FILING DATE U.S. SERIAL NUMBERS	UMBER     U.S. FILING DATE     PATENTED       3/19/2001     3/19/2001       CATIONS DESIGNATING THE U.S.       PCT FILING DATE     U.S. SERIAL       NUMBERS	IUMBER     U.S. FILING DATE     PATENTED     PENDING       3/19/2001     X       CATIONS DESIGNATING THE U.S.     Image: Comparison of the c

#### POWER OF ATTORNEY:

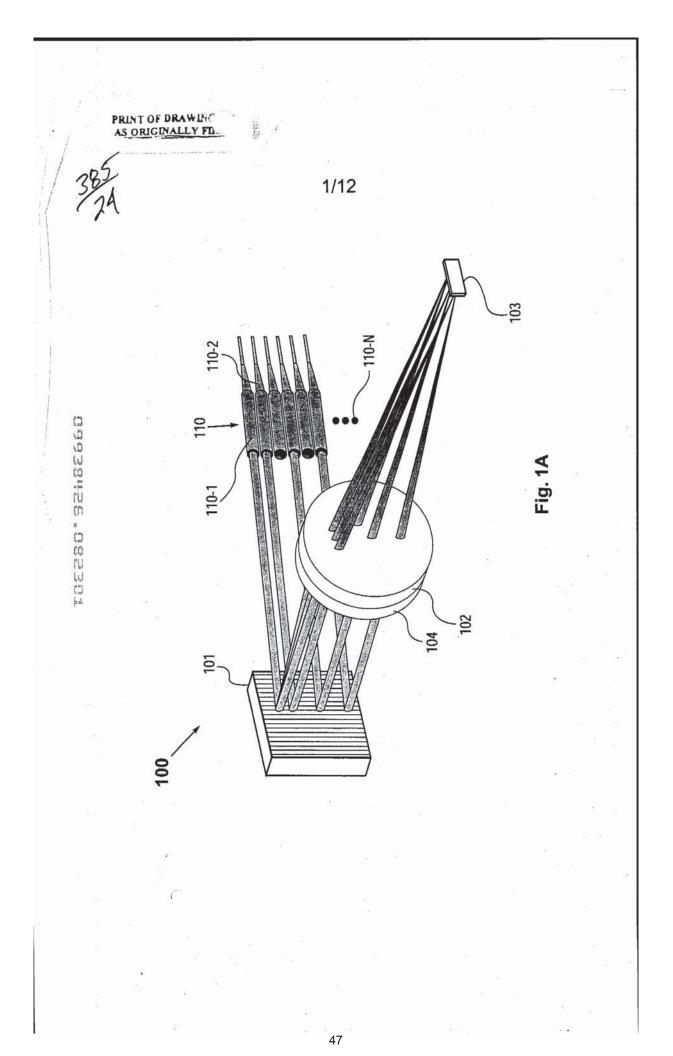
As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) with full power of substitution to act exclusively to prosecute this application and transact all business in the Patent and Trademark Office connected there with: Barry N. Young (Reg. No. 27,744); Timothy W. Lohse (Reg. No. 35,255); Stephen E. Reiter (Reg. No. 31,192); Steven R. Sprinkle (Reg. No. 40,825); Terrance A. Meador (Reg. No. 30,298); Ramsey R. Stewart (Reg. No. 38,322); June M. Learn (Reg. No. 31,238); John Oskorep (Reg. No. 41,234); Timothy N. Ellis (Reg. No. 41,734); William G. Goldman (Reg. No. 42,590); Sheila Kirschenbaum (Reg. No. 44,835); Travis L. Dodd (Reg. No. 42,491); Charles D. Gavrilovich, Jr. (Reg. No. 41,031); Gerald W. Maliszewski (Reg. No. 38054); Hayward A. Verdun (Reg. No. 43,223); Armando Pastrana, Jr. (Reg. No. 44,997); Richard M. Goldman (Reg. No. 25,585); Lisa A. Haile (Reg. No. 38,347); Sal Lim (Reg. No. 45,706); Joseph R. Baker, Jr. (Reg. No. 40,900); Richard J. Imbra (Reg. No. 37,643); Mark L. Berrier (Reg. No. 35,066); Mark M. Takahashi (Reg. No. 38,631); James P. Cleary (Reg. No. 45,843); Karl A. Limbach (Reg. No. 18689); Gerald T. Sekimura (Reg. No. 30,103); Kyla L. Harriel (Reg. No. 41,816); Eric N. Hoover (Reg. No. 37,355); George C. Limbach (Reg. No. 19,305); Ronald L. Yin (Reg. No. 27,607); Alan A. Limbach (Reg. No. 39,749); Edward B. Weller (Reg. No. 37,468); Jian Ma (Reg. No. 48,088) David Alberti (Reg. No. 43,465)

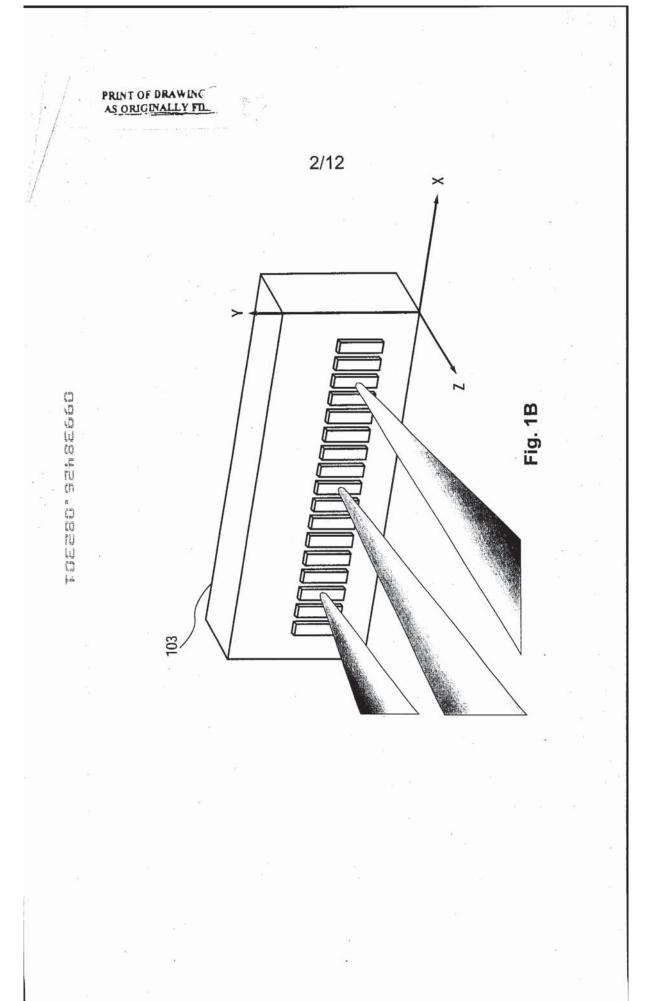
All correspondence should be addressed to:

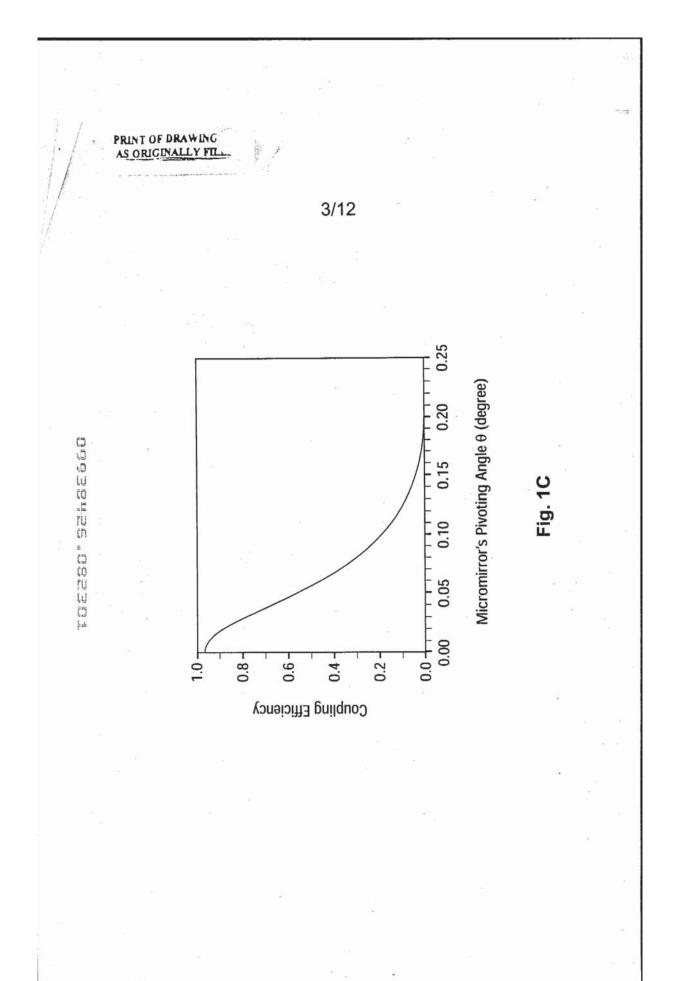
Patent Department GRAY CARY WARE & FREIDENRICH LLP 1755 Embarcadero Road Palo Alto, CA 94303

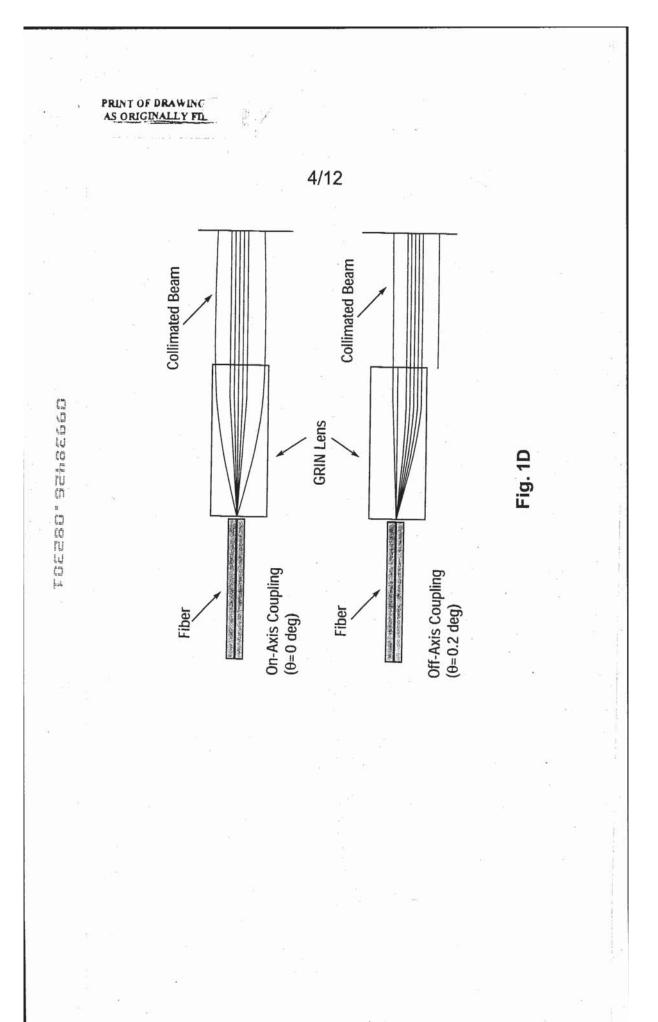
All telephone calls should be directed to Barry N. Young, telephone number (650) 320-7439.

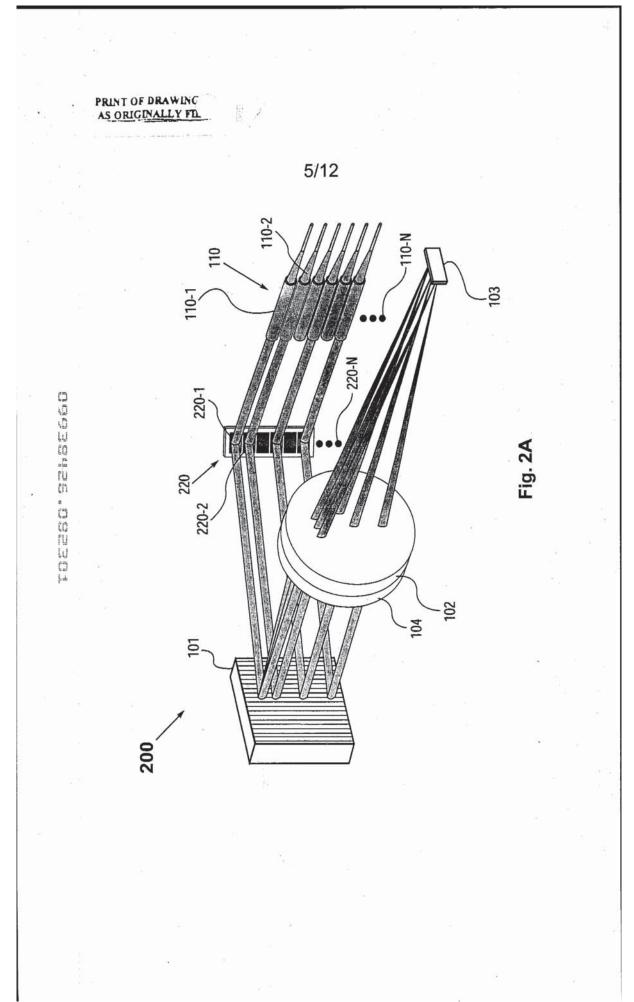
Inventor's Full Name:	Jeffrey P. Wilde	
Inventor's Signature:	all Blue	
Date:	(18-23-0)	
Residence: (City, State and/or country)	Los Gatos, CA	
Citizenship:	US	
Post Office Address:	18555 Mountain View Avenue Los Gatos, CA 95033	

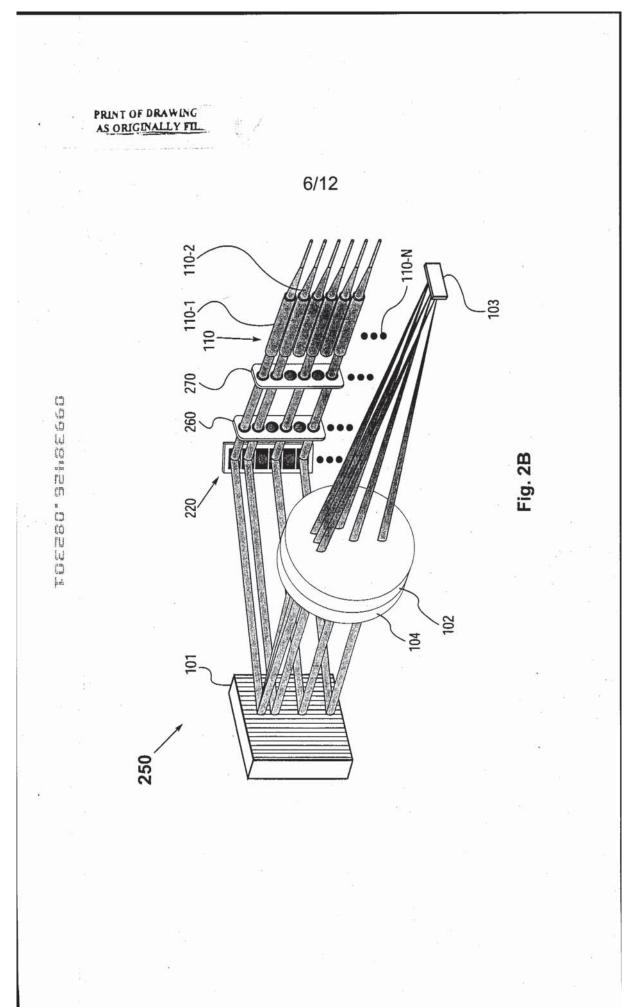


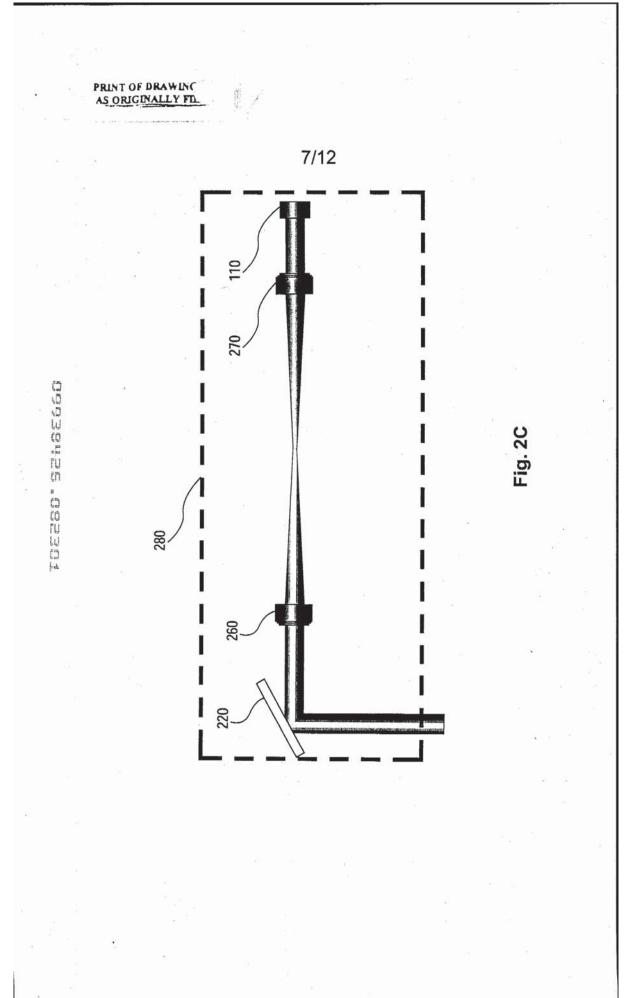


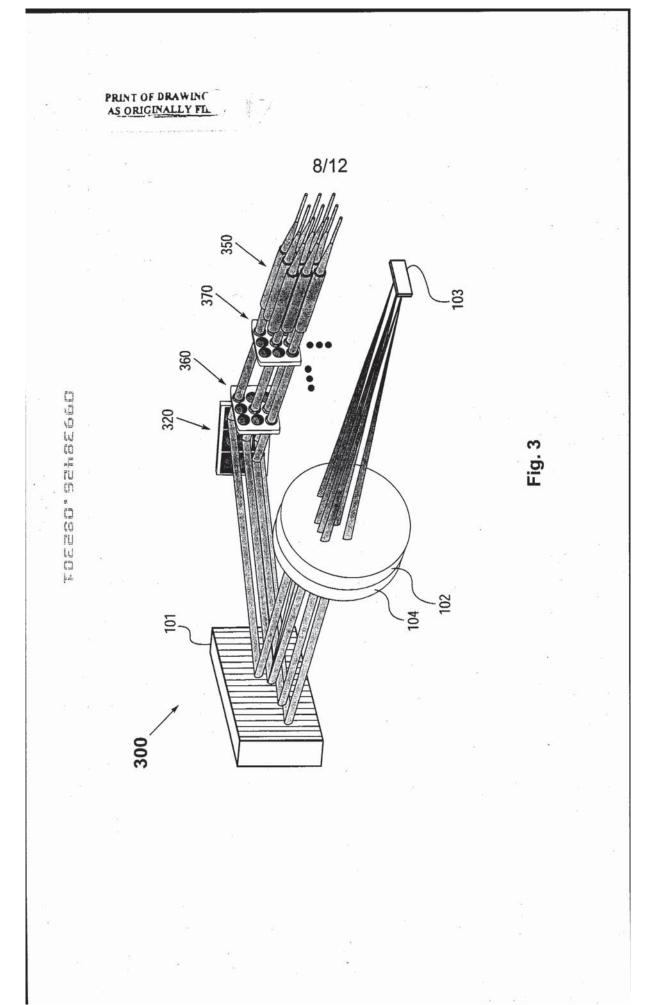












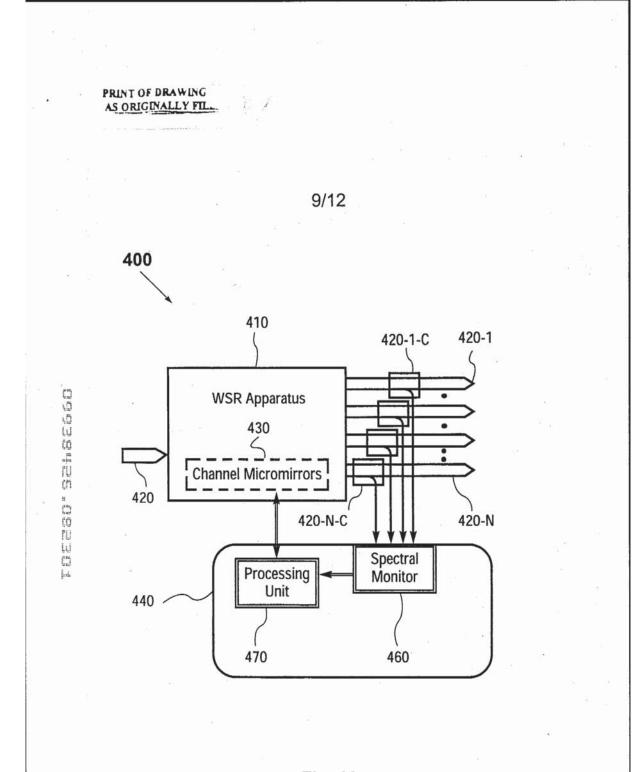
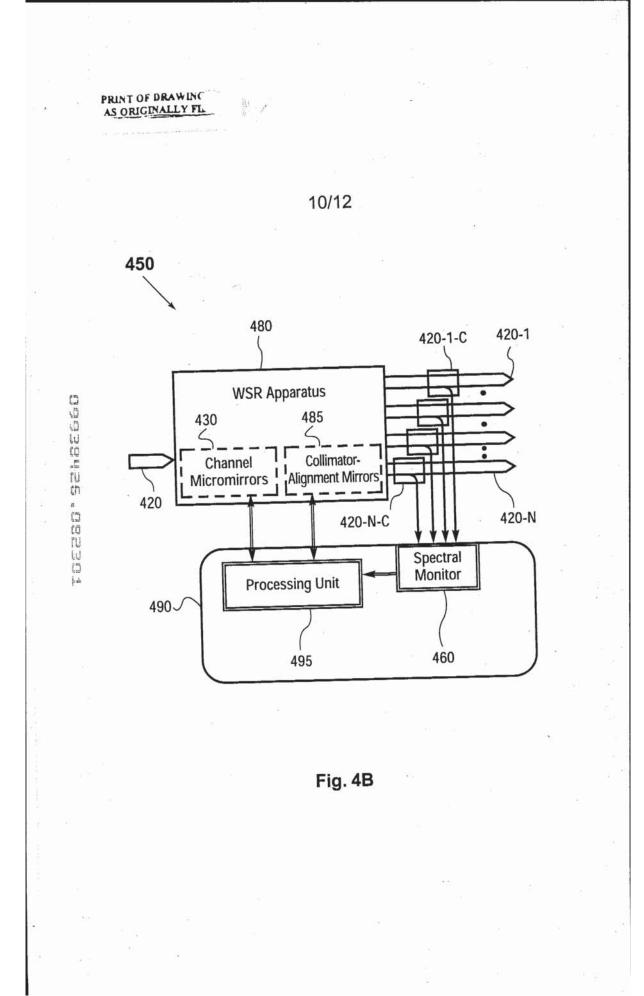
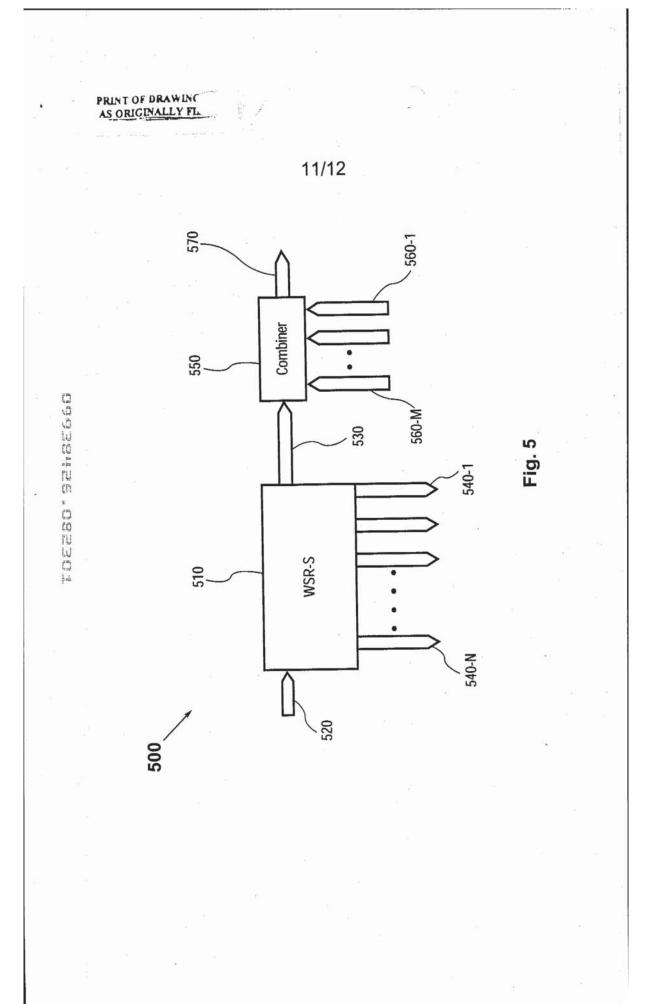
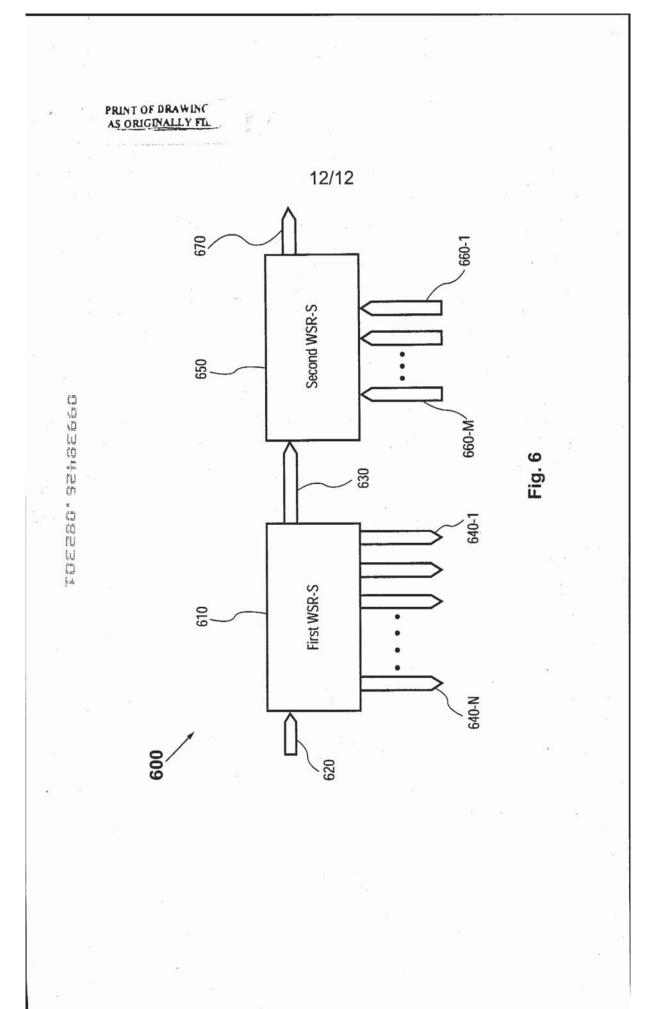


Fig. 4A







	Application No.	Applicant(s)	/*
10 ×	Application No.		
Notice of Allowability	09/938,426	WILDE, JEFFREY P.	
······································	Examiner	Art Unit	
4	Hung N Ngo	2874	
The MAILING DATE of this communication a All claims being allowable, PROSECUTION ON THE MERITS herewith (or previously mailed), a Notice of Allowance (PTOL NOTICE OF ALLOWABILITY IS NOT A GRANT OF PATEN of the Office or upon petition by the applicant. See 37 CFR 1	S IS (OR REMAINS) CL -85) or other appropriate IT RIGHTS. This applica	OSED in this application. If not included communication will be mailed in due co	urse. THIS
. This communication is responsive to			3
The allowed claim(s) is/are <u>1-67</u> .		124	
The drawings filed on 23 August 2001 are accepted by	y the Examiner.		
. Acknowledgment is made of a claim for foreign priority		a)-(d) or (f).	
a) All b) Some* c) None of the:			
1. Certified copies of the priority documents	have been received.		
2. Certified copies of the priority documents	have been received in A	oplication No.	
3. Copies of the certified copies of the priorit			n from the
International Bureau (PCT Rule 17.2(a			
* Certified copies not received:	<i>))</i> .		
<ul> <li>Acknowledgment is made of a claim for domestic prior</li> </ul>	ity under 25 U.S.C. & 110		34 120
(a) The translation of the foreign language provision			
<ul> <li>Acknowledgment is made of a claim for domestic prior</li> </ul>			.,
	ity under 55 0.5.0. 33 1		
Applicant has THREE MONTHS FROM THE "MAILING DAT below. Failure to timely comply will result in ABANDONMEN 7.  A SUBSTITUTE OATH OR DECLARATION must be s	T of this application. TH submitted. Note the attact	IS THREE-MONTH PERIOD IS NOT EX	TENDABLE
NFORMAL PATENT APPLICATION (PTO-152) which gives	reason(s) why the oath o	or declaration is deficiént.	
B. CORRECTED DRAWINGS must be submitted.			
(a) [] including changes required by the Notice of Draft	sperson's Patent Drawin	g Review ( PTO-948) attached	
1) 🛄 hereto or 2) 🔲 to Paper No		· · · · · · · · · · · · · · · · · · ·	
(b) including changes required by the proposed draw	ing correction filed	which has been approved by the Exa	miner
(c) including changes required by the attached Exam			
Identifying Indicla such as the application number (see 37 C of each sheet. The drawings should be filed as a separate p	FR 1.84(c)) should be writ aper with a transmittal let	ten on the drawings in the top margin (not ter addressed to the Official Draftsperson.	the back)
DEPOSIT OF and/or INFORMATION about the d attached Examiner's comment regarding REQUIREMENT FC	eposit of BIOLOGICA OR THE DEPOSIT OF BI	_ MATERIAL must be submitted. Not OLOGICAL MATERIAL.	e the
Attachment(s)			
Notice of References Cited (PTO-892)	2 1	Notice of Informal Patent Application (PT	0-152)
<ul> <li>Notice of Draftperson's Patent Drawing Review (PTO-94)</li> <li>Information Disclosure Statements (PTO-1449), Paper N</li> <li>Examiner's Comment Regarding Requirement for Depos of Biological Material</li> </ul>	8) 4[] I lo 6[] E	nterview Summary (PTO-413), Paper No Examiner's Amendment/Comment Examiner's Statement of Reasons for Alk	) ·
		Primary Examiner Art Unit: 2874	$(\cdot)$

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					Application/C 09/938,426	ontrol No.	Applicant(s)/F Reexaminatio WILDE, JEFF	ion	
,		Notice of References	s Cited		Examiner Art Unit Hung N Ngo 2874		Art Unit 2874	Page 1 of 1	
				U.S. PAT	PATENT DOCUMENTS				
*	1	Document Number Country Code-Number-Kind Code	Date MM-YYYY		a 4	Name	and the second second	Classification	
+	A	US-6,263,135	07-2001	Wade, R	obert Kent			359/130	
+	в	US-6,289,155	09-2001	Wade, R	obert Kent			385/33	
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\*A copy of this reference is not being furnished with this Office action. (See MPEP § 707.05(a).) Dates in MM-YYYY format are publication dates. Classifications may be US or foreign.

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APPLICATION NO.	FILING DATE	FIRST N	AMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.
09/938,426	08/23/2001	Jef	frey P. Wilde	210393-991101	2587
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B. If the status is changed, pay the PUBLICATION FEE (if required) and twice the amount of the ISSUE FEE shown above and notify the United States Patent and Trademark Office of the change in status, or	B. If applicant claimed SMALL ENTITY status before, or is now claiming SMALL ENTITY status, check the box below and enclose the PUBLICATION FEE and 1/2 the ISSUE FEE shown above.
	<ul> <li>Applicant claims SMALL ENTITY status. See 37 CFR 1.27.</li> </ul>

II. PART B - FEE(S) TRANSMITTAL should be completed and returned to the United States Patent and Trademark Office (USPTO) with your ISSUE FEE and PUBLICATION FEE (if required). Even if the fee(s) have already been paid, Part B - Fee(s) Transmittal should be completed and returned. If you are charging the fee(s) to your deposit account, section "4b" of Part B - Fee(s) Transmittal should be completed and an extra copy of the form should be submitted.

III. All communications regarding this application must give the application number. Please direct all communications prior to issuance to Box ISSUE FEE unless advised to the contrary.

IMPORTANT REMINDER: Utility patents issuing on applications filed on or after Dec. 12, 1980 may require payment of maintenance fees. It is patentee's responsibility to ensure timely payment of maintenance fees when due.

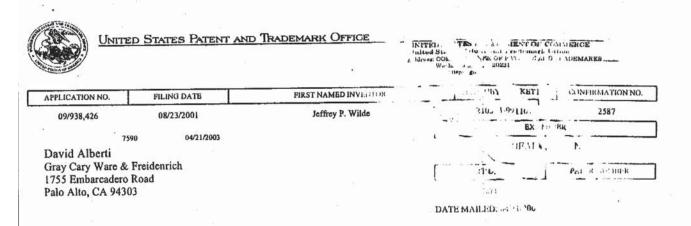
# PART B - FEE(S) TRANSMITTAL

Complete and send this form, together with applicable fee(s), to: Mail Box ISSUE FEE Commissioner for Patents Washington, D.C. 20231 Fax (703)746-4000

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David Alberti				formal drawing,	must have its own certificate of ma	ailing or transmission.
Gray Cary Ware &	Freidenrich				Certificate of Mailing or Transp	mission
1755 Embarcadero				I hereby certify	that this Fee(s) Transmittal is I	being deposited with the
Palo Alto, CA 9430				envelope addres transmitted to th	that this Fec(s) Transmittal is l solal Service with sufficient postag sed to the Box Issue Fee address the USPTO, on the date indicated be	above, or being facsimile
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obtain or retain a benefit application. Confidentiali estimated to take 12 minu completed application for suggestions for reducing Patent and Trademark Of NOT SEND FEES OI Commissioner for Patente	ation is required by 37 CF by the public which is to ty is governed by 35 U.S.C. ites to complete, including rm to the USPTO. Time of the amount of time you this burden, should be set fice, U.S. Department of C & COMPLETED FORM , Washington, DC 20231.	in file (and by the USP) , 122 and 37 CFR 1.14, gathering, preparing, a will vary depending u a require to complete at to the Chief Informa Commerce, Washington S TO THIS ADDRI	To to process) an . This collection is and submitting the pon the individual this form and/or ation Officer, U.S. a, D.C. 20231. DO ESS. SEND TO:		* * * *	ыйсы Itt Ю
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TRANSMIT THIS FORM WITH FEE(S) U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE

PTOL-85 (REV. 04-02) Approved for use through 01/31/2004. OMB 0651-0033



# Determination of Patent Term Adjustment under 35 U.S.C. 154 (b) (application filed on or after May 29, 2000)

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The patent term adjustment to date is 0 days. If the issue fee is paid on the date that is three months after the mailing date of this notice and the patent issues on the Tuesday before the date that is 28 weeks (six and a half months) after the mailing date of this notice, the term adjustment will be 0 days.

If a continued prosecution application (CPA) was filed in the above-identified application, the filing date that determines patent term adjustment is the filing date of the most recent CPA.

Applicant will be able to obtain more detailed information by accessing the Patent Application Information Retrieval (PAIR) system. (http://pair.uspto.gov)

Any questions regarding the patent term extension or adjustment determination should be directed to the Office of Patent Legal Administration at (703)305-1383.

Page 3 of 4

		Uni	UNITED STATES DEPARTMENT OF COMMERCE United States Patent and Trademark Office Addrew: COMMISSIONER OF PATENTS AND TRADEMARKS Washington, D.C. 20221 www.uspla.gov				
APPLICATION NO.	FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.			
09/938,426	08/23/2001	Jeffrey P. Wilde	210393-991101	2587			
75	90 04/21/2003		EXAMIN	ER			
David Alberti			HEALY, B	RIAN			
Gray Cary Ware & 1755 Embarcadero			ART UNIT	PAPER NUMBER			
Palo Alto, CA 9430 UNITED STATES	)3		2874 DATE MAILED: 04/21/2003				

#### Notice of Fee Increase on January 1, 2003

If a reply to a "Notice of Allowance and Fee(s) Due" is filed in the Office on or after January 1, 2003, then the amount due will be higher than that set forth in the "Notice of Allowance and Fee(s) Due" since there will be an increase in fees effective on January 1, 2003. <u>See Revision of Patent and Trademark Fees for Fiscal Year 2003</u>; Final Rule, 67 Fed. Reg. 70847, 70849 (November 27, 2002).

The current fee schedule is accessible from: http://www.uspto.gov/main/howtofees.htm.

If the issue fee paid is the amount shown on the "Notice of Allowance and Fee(s) Due," but not the correct amount in view of the fee increase, a "Notice to Pay Balance of Issue Fee" will be mailed to applicant. In order to avoid processing delays associated with mailing of a "Notice to Pay Balance of Issue Fee," if the response to the Notice of Allowance and Fee(s) due form is to be filed on or after January 1, 2003 (or mailed with a certificate of mailing on or after January 1, 2003), the issue fee paid should be the fee that is required at the time the fee is paid. If the issue fee was previously paid, and the response to the "Notice of Allowance and Fee(s) Due" includes a request to apply a previously-paid issue fee to the issue fee now due, then the difference between the issue fee amount at the time the response is filed and the previously paid issue fee should be paid. See Manual of Patent Examining Procedure, Section 1308.01 (Eighth Edition, August 2001).

Questions relating to issue and publication fee payments should be directed to the Customer Service Center of the Office of Patent Publication at (703) 305-8283.

Page 4 of 4

PTOL-85 (REV. 04-02) Approved for use through 01/31/2004.

Attorney D et No. 2102393-991101

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### IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Applicant: Wilde

Serial No. 09/938,426

## Group Art Unit: 2874

Filed: August 23, 2001

Examiner: Garland, Steven R

## Title: RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES

I hereby certify that this correspondence is being deposited with the United States Postal Service with sufficient postage as FIRST CLASS MAIL in an envelope addressed to: Commissioner of Patents and Trademarks, Washington, D.C. 20231, BOX RCE on October 8, 2002.

Date: October 8, 2002

Signature an C. Pingue

### REQUEST FOR CONTINUED EXAMINATION PURSUANT TO 37 C.F.R. §1.114

Assistant Commissioner for Patents Washington, D.C. 20231

Dear Sir/Madam:

Applicant hereby requests, pursuant to 37 C.F.R. §1.114, continued examination of the above-identified application for consideration of the references listed on the Information Disclosure Statement being submitted herewith on PTO form 1499. Copies of those references are enclosed.

One of the references, i.e., U.S. Patent No. 6,204,946 of Aksyuk et al., was used to reject claims in co-pending, related U.S. application serial number 10/005,714. This reference and all other references contained in the Information Disclosure Statement were cited and discussed in the specification of the present application. However, out of an abundance of caution, Applicant is nevertheless submitting these references in the form of an Information Disclosure Statement, and respectfully requests that the Examiner consider them in this application. Applicant's

# Attorney D et No. 2102393-991101

submission of these references should not be construed, however, as an admission that they ar from analogous arts or material. Applicant specifically reserves the right to argue that any on these references are not material at a later date should the need arise.

Applicant encloses herewith a check in the amount of \$370.00 to cover the fee set forth in 37 C.F.R. §1.17(e). Applicant hereby authorizes the commissioner to charge any other fees required to the PTO Deposit Account Number 07-1896.

If the Examiner has any questions, the Examiner is invited to contact Applicant's attorney at the following address or telephone number:

David Alberti c/o Patent Department GRAY CARY WARE & FREIDENRICH LLP 1755 Embarcadero Road Palo Alto, CA 94303 Telephone: (650) 833-2052

Respectfully submitted,

Dated: October \_ & , 2002

Gray Cary\EM\7123922.1 2102393-991101

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David Alberti Reg. No. 43,465

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OTPE 4			Based on PTO/SB/30 (10-01)
REQUES	T	Application Number	JJ/938,426
GI 15 200L OF REGUES		Filing Date	August 23, 2001
	NATION (RCE)	First Named Inventor	Jeffrey Wilde
TRANSMIT	TAL	Group Art Unit	2874
Subsection (b) of 35 U.S.C. § 132, ef provides for continued examination application filed on or after	on of an utility or plant	Examiner Name	Garland, Steven
See The American Inventors Protect	tion Act of 1999 (AIPA).	Attorney Docket Number	2102393-991101
consider filing a continued prosecuti	e on May 29, 2000. If the above- on application (CPA) under 37 C.I	F.R. § 1.53(d) (PTO/SB/29) instea	tified application. r to May 29, 2000, applicant may wish to d of a RCE to be eligible for the patent term n Practice, Final Rule, 65 Fed. Reg. 50092 11, 2000), which established RCE practice.
1. Submission required under 37 C.F	.R. § 1.114		01
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I. Consider the amendr (Any unentered amend	nent(s)/reply under 37 C.F.F Iment(s) referred to above wil	k, § 1.116 previously filed of I be entered).	
	nts in the Appeal Brief or Re		
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b. 🛛 Enclosed			
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il. Affidavit(s)/Declaration			
iii. Information Disclosu			No .
iv. [_] Other			
2. Miscellaneous		24 10	3 A C
a. Suspension of action on t	he above-identified applicat	ion is requested under 37 C	.F.R. § 1.103(c) for a period of
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TRANSMIT		Filing Date	August 23, 2001			
FORM		First Named Inventor	leffrey P Wilde			
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		Examiner	Healy, Brian			
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Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450, DO NOT ADDRESS SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

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 Date
 July 16, 2003

 This collection of information is required by 37 CFR 1.17 and 1.27. The information is required to obtain or retain a benefit by the public which is to file (and by the USPTO to process) an application. Condentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 12 minutes to complete including gethering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark. Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.
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Initial Class Su cla	Translation	
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Name (Print/Type) David L. Alberti	nna-T	(Attorney		4	3,465		Telephone	650-833	3-2052
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FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO
08/23/2001	Jeffrey P. Wilde	210393-991101	2587
12/04/2002			
		EXAM	INER
& Freidenrich o Road		NGO, HUN	IG NHAT
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	08/23/2001 12/04/2002 & Freidenrich	08/23/2001 Jeffrey P. Wilde 12/04/2002 & Freidenrich ro Road	FILING DATE     FIRST NAMED INVENTOR     ATTORNEY DOCKET NO.       08/23/2001     Jeffrey P. Wilde     210393-991101       12/04/2002     EXAMI       & Freidenrich     NGO, HUN       vo Road     NGO, HUN

Please find below and/or attached an Office communication concerning this application or proceeding.

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	Office Action Summary	Exa	miner	Art Unit	
		Hur	ng N Ngo	2874	
Period fo	The MAILING DATE of this commu r Reply	nication appears	on the cover sheet	with the corresponden	ce address
THE N - Exter after - If the - If NO - Failur - Any n	ORTENED STATUTORY PERIOD F MAILING DATE OF THIS COMMUN usions of time may be available under the provision: SIX (6) MONTHS from the mailing date of this comm period for reply specified above is less than thirty (i period for reply is specified above, the maximum s re to reply within the set or extended period for repl eply received by the Office later than three months id patent term adjustment. See 37 CFR 1.704(b).	ICATION. s of 37 CFR 1.136(a). I munication. 30) days, a reply within tatutory period will appl y will, by statute, cause	In no event, however, may the statutory minimum of it y and will expire SIX (6) M the application to become	a reply be timely filed hirty (30) days will be consider ONTHS from the mailing date of ABANDONED (35 U.S.C. § 13	of this communication. 33).
1)[[]	Responsive to communication(s) f	iled on			
2a)	This action is FINAL.	2b) This act	tion is non-final.	2(	
3)	Since this application is in conditio closed in accordance with the prac on of Claims	n for allowance	except for formal n		
	Claim(s) <u>1-67</u> is/are pending in the	application		i.	
	4a) Of the above claim(s) is/a		om consideration		
	Claim(s) is/are allowed.				
	Claim(s) <u>1,21,31,37 and 61</u> is/are re	eiected.		3 <del>3</del>	
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9)[] -	The specification is objected to by th	e Examiner.			
10)[] 1	The drawing(s) filed on is/are	a) accepted o	r b) objected to b	y the Examiner.	
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	The oath or declaration is objected to	o by the Examin	er.		a ()
Priority u	nder 35 U.S.C. §§ 119 and 120				
13)	Acknowledgment is made of a claim	n for foreign prio	rity under 35 U.S.C	C.§ 119(a)-(d) or (f).	
a)[	All b) Some * c) None of:				
	1. Certified copies of the priority				
	2. Certified copies of the priority				
	<ol> <li>Copies of the certified copies application from the Internee the attached detailed Office action</li> </ol>	national Bureau	(PCT Rule 17.2(a)	).	ional Stage
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Application/Control Number: 09/938,426 Art Unit: 2874

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Page 2

The following is a quotation of the appropriate paragraph. of 35 U.S.C. 102 that the rejections under this section made in the Ot conaction: "and to a patent unless form the L ratent granted on an ap cation f A person shall be entry the application patient of Circum Eiternation of application (e) the invention was described in ... - (A) at ection 371( -) of this United States before the invention thereon, by another who has fulfilled the requirements of p. title before the invention thereof by the applicant for pair

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1910. Piliontic The changes made to 35 U.S.C. 102(e) by the American ... \ct Aliun of 1999 (AIPA) do not apply to the examination of this application as the  $a_{\rm F}$ being examined was not (1) filed on or after November 29, 2000, or (2) volue 11 Jm published under 35 U.S.C. 122(b). Therefore, this application is examined under the U.S.C. 102(e) prior to the amendment by the AIPA (pre-AIPA 35 U.S.C. 102(e)).

Claims 1, 21, 31, 37 and 61 are rejected under 35 U.S.C. 102(e) as beau; 2. anticipated by Aksyul et al (6,204,946). Aksyul et al discloses a polarizaton rotating unit

(56) and a wavelength separator (12).

Claims 2-20, 22-30, 32-36, 38-43, 45-60 and 62-67 are objected to as being 3. dependent upon a rejected base claim, but would be allowable if rewritten in independent form including all of the limitations of the base claim and any intervening claims.

Any inquiry concerning this communication or earlier communications from the examiner should be directed to Hung N Ngo whose telephone number is (703) 308-0297. The examiner can normally be reached on M-F (8:30-5:00).

If attempts to reach the examiner by telephone are unsuccessful, the examiner's supervisor, Rodney Bovernick can be reached on 703-308-4819. The fax phone

Application/Control Number: 09/938,426 Art Unit: 2874

numbers for the organization where this application or proceeding is assigned are 703-308-7724 for regular communications and 703-308-7724 for After Final communications.

Any inquiry of a general nature or relating to the status of this application or proceeding should be directed to the receptionist whose telephone number is 703-308-0956.

Hung 🕅 Ngo

Primary Examiner Art Unit 2874

hn November 27, 2002

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#### ATTORNEY DOCKET NO. 2102393-991101

**GROUP NO.: 2587** 

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

DEC 1 6 2002

APPLICANTS:

SERIAL NO.: 09/938,426

Jeffrey P. Wilde

FILING DATE: August 23, 2001

TITLE:

Reconfigurable Optical Add-Drop Multiplexers With Servo Control And Dynamic Spectral Power Management Capabilities

#### INFORMATION DISCLOSURE STATEMENT

Assistant Commissioner for Patents Box DD Washington, D.C. 20231

Dear Sir:

In accordance with the provisions of 37 C.F.R. § 1.97, Applicants hereby make of record the references listed on the accompanying Form PTO-1449 for consideration by the Examiner in connection with the examination of the above-identified patent application. Copies of the references are enclosed.

## REMARKS

In accordance with the provisions of 37 C.F.R, § 1.97, this statement is being filed (CHECK ONE).

- [X] (1) within three (3) months of the Filing Date or before the mailing date of a First
   Office Action on the merits; or
- [ ] (2) after the period defined in (1) but before the mailing date of a Final Rejection or Notice of Allowance, and
  - [ ] the requisite Statement is below, **OR**
  - [] the requisite fee under Rule 1.17(p), namely \$180.00, is included herein, or
- [ ] (3) after the mailing date of a Final Rejection or Notice of Allowance but before the payment of the Issued Fee, AND
  - [ ] Applicant hereby Petitions the Commissioner to accept and consider the attached Information Disclosure Statement, **AND**
  - ] the requisite Statement is below, AND

#### ATTORNEY DOCKET NO. 2102393-991101

[ ] the requisite petition fee due under Rule 1.17(i), namely \$130.00 is included herein.

It is respectfully requested that each of the references shown on the attached Form PTO-1449 be made of record in this application.

### STATEMENT

As required under §1.97(e), Applicants, through the undersigned, hereby state either that [check the appropriate space]:

[E]ach item of information contained in the Information Disclosure Statement was cited in a communication from a foreign patent office in a counterpart foreign application **not more than** three months prior to the filing date of the Information Disclosure Statement; or

[N]o item of information contained in the Information Disclosure Statement was cited in a communication from a foreign patent office in a counterpart foreign application, and to the knowledge of the person signing this Statement after making reasonable inquiry, no item of information contained in the Information Disclosure Statement was known to **any** individual designated in §1.56(c) **more than** three months prior to the filing of the Information Disclosure Statement.

## FEE AUTHORIZATION

Should any fee associated with the submission of this paper not be attached hereto as a check, the Commissioner is authorized to charge the missing fee to our Deposit Account No. 07-1896. Any overpayments should be credited to said Deposit Account.

Respectfully submitted,

David Alberti Reg. No. 43,465 Attorney for Assignee

Date: December 6, 2002

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**GRAY CARY WARE & FREIDENRICH** 1755 Embarcadero Road Palo Alto, CA 94303-3340 Telephone No.: 650-320-7400 Facsimile No.: 650-320-7401

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Substitute for form 1449A/PTO

## INFORMATION DISCLOSURE STATEMENT BY APPLICANT

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Filing Date	August 23, 2001	
First Named Inventor	Jeffrey P. Wilde	
Group Art Unit	2587	
Examiner Name	Garland, Steven	
Attorney Docket Number	2102393-991101	

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	Group Art Unit	2874
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			Attorneys for Applicant(s	5)	
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Attorney Docket Number 2102393-991101 0 3 2003 IN THE UNITED STATES PATENT AND TRADEMARK OFF TECHNOLOGY CENTER 2800 M. Baunson 2/6/2 RADENAN Applicant: Wilde Serial No. 09/938,426 Group Art Unit: 2874 Filed: August 23, 2001 Examiner: Ngo, Hung Nhat Title: RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES I hereby certify that this correspondence is being deposited with the United States Postal Service with sufficient postage as FIRST CLASS MAIL in an envelope addressed to: Com-missioner of Patents and Trademarks, Washington, D.C. 20231, on: Signature AMENDMENT AND RESPONSE TO OFFICE ACTION Commissioner of Patents and Trademarks Washington, DC 20231 Sir/Madam: Applicant responds to the outstanding Office Action mailed on December 4, 2002 as follows: IN THE CLAIMS: Please amend claims 31 and 37 as follows (a marked up versions of these claims are attached hereto as Appendix A): Claim 31 (amended, clean version) An optical apparatus comprising: a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports; 1 Gray Cary\EM\7132730.1 2102393-991101

- b) a wavelength-separator, for separating said multi-wavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously controllable to reflect said spectral channels into selected ones of said output ports; and
- e) a one-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

#### Claim 37 (amended, clean version)

An optical apparatus comprising:

- a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multi-wavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously controllable to reflect said spectral channels into selected ones of said output ports; and
- e) a two-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

#### REMARKS

The Examiner rejected claims 1, 21, 31, 37 and 61 under 35 U.S.C. §102(e) as being anticipated by United States Patent No. 6,204,946 of Aksyuk et al. ("Aksyuk"). While the Examiner did not specifically indicate that claim 44 was rejected (or on what grounds it was rejected), the Examiner did not state that claim 44 was allowable. Thus, Applicant will treat the claim as rejected based on Aksyuk for the purposes of this office action. Claims 2-20, 22-30, 32-36, 38-43, 45-60 and 62-67 were determined to be allowable if rewritten independent form. Claims 31 and 37 have been amended to clarify that each micromirror in the array is continuously controllable. For the reasons stated below, Applicant asserts that all of claims 1-67 are allowable in the present form over Aksyuk.

As discussed more fully and completely below, Aksyuk does not teach an optical method or apparatus including all of the elements of Applicant's claimed inventions. Particularly, Aksyuk does not teach an optical method or apparatus, which uses an array of micromirrors (or beam deflecting elements) that are individually and continuously controllable to reflect a plurality of spectral channels into a plurality of output ports, as recited in claims 1, 31, 37, 44 and 61. Furthermore, Aksyuk does not teach the use of a servo-control assembly in communication with the micromirrors for maintaining a predetermined coupling, as recited in claim 21. Therefore, Aksyuk can neither anticipate nor render obvious any of claims 1, 21, 31, 37, 44 and 61.

#### Claims 1, 31, 37, 44 and 61

Aksyuk does not disclose nor suggest the novel optical apparatus of independent claims 1, 31, 37, 44 and 61. Independent claims 1, 31, 37, and 44 each require an optical (or wavelength-separating-routing) apparatus or system having an input port, a plurality of output ports (which may include a pass-through port and one or more drop ports) and an array of micromirrors that are individually and continuously controllable to reflect a plurality of spectral channels into selected output ports.

First, Aksyuk does not teach an apparatus that includes an input port and a plurality of output ports (e.g., drop and pass-through ports). In contrast, Aksyuk teaches that the pass-through wavelengths are reflected back into the input port and input fiber rather than to a

separate port and fiber. As discussed in column 3, line 51 - column 4, line 5 of Aksyuk, the WDM switch 10 operates to reflect the pass-through signals back to the input port 16, while the reflected drop signals are all sent to a single second port 26. Thus, in order to implement an add/drop multiplexer, circulators are required at the input and output ports of the claimed WDM switch 10. (See Aksyuk Figure 3, column 4, lines 6 - 48).

Moreover, Aksyuk does not disclose an array of micromirrors that are continuously controllable. Rather, the micromirrors of Aksyuk operate in a "binary" or discrete manner. That is each micromirror is configured to be positionable between two discrete states, such that it either retroreflects its corresponding wavelength back into the input port as a pass-through channel, or directs its wavelength to a single output port as a drop channel. (Aksyuk at column 3, lines 30 - 40). As a result, the pass-through channels share the same input port as the input signal, and the drop channels share the same output port as the add channels, thereby requiring optical circulators to be coupled to both ports in order to provide an add/drop multiplexer application.

Applicant describes these fundamental limitations of Aksyuk on page 3 of the pending application:

... Each micromirror [of Aksyuk] is configured to operate between two discrete states, such that it either retroreflects its corresponding spectral channel back into the input port as a pass-through channel, or directs its spectral channel to an output port as a drop channel. As such, the pass-through signal (i.e., the combined pass-through channels) shares the same input port as the input signal. An optical circulator is therefore coupled to the input port, to provide necessary routing of these two signals. Likewise, the drop channels share the output port with the add channels. An additional optical circulator is thereby coupled to the output port, from which the drop channels exit and the add channels are introduced into the output port. The add channels are subsequently combined with the pass-through signal by way of the diffraction grating and the binary micromirrors.

Although the aforementioned OADM disclosed by Aksyuk et al. has the advantage of performing wavelength separating and routing in free space and thereby incurring less optical loss, it suffers a number of limitations. First, it requires that the pass-through signal share the same port/fiber as the input signal. An optical circulator therefore has to be implemented, to provide necessary routing of these two signals. Likewise, all the add and drop channels enter and leave the OADM through the same output port, hence the need for another optical circulator. Moreover, additional means must be provided to multiplex the add channels before entering the system and to demultiplex the drop channels after exiting the system. This additional multiplexing/demultiplexing requirement adds more cost and complexity that can

restrict the versatility of the OADM thus-constructed. Second, the optical circulators implemented in this OADM for various routing purposes introduce additional optical losses, which can accumulate to a substantial amount.

Applicant also describes the advantages of the claimed optical apparatus, including multiple output ports and micromirrors that are continuously controllable to direct the spectral channels into selected output ports, in the pending application. As explained by Applicant on pages 12 and 13 of the pending application, "a unique feature of the present invention is that the motion of each channel micromirror is individually and continuously controllable, such that its position, e.g., pivoting angle, can be continuously adjusted. This enables each channel micromirror to scan its corresponding spectral channel across all possible output ports and thereby direct the spectral channel to any desired output port." By reflecting all of the pass-through wavelengths as well as the dropped wavelengths to separate fibers from the input fiber, the claimed devices do not reuse the same optical fiber used to input the WDM signal. This avoids the necessity for circulators for combining or separating the multiple wavelengths on a single input and output port as does the claimed devices. Therefore, the claimed devices have the advantage of being significantly less complicated than the devices disclosed in the Aksyuk patent.

Further advantages of Applicant's novel, claimed configuration are described on pages 8 and 9 of the pending application:

- By advantageously employing an array of channel micromirrors that are individually and continuously controllable, an OADM of the present invention is capable of routing the spectral channels on a channel-by-channel basis and directing any spectral channel into any one of the output ports. As such, its underlying operation is dynamically reconfigurable, and its underlying architecture is intrinsically scalable to a large number of channel counts.
- 2) The add and drop spectral channels need not be multiplexed and demultiplexed before entering and after leaving the OADM respectively. And there are not fundamental restrictions on the wavelengths to be added or dropped.

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In summary, Aksyuk entirely fails to disclose or suggest multiple elements of claims 1, 31, 37 and 44 (e.g., an input and multiple output ports and an array of micromirrors that are individually and continuously controllable to reflect a plurality of spectral channels into selected output ports). For at least these reasons, claims 1, 31, 37 and 44, are patentable over Aksyuk.

Claim 61 recites a method for performing dynamic wavelength separating and routing. Like claims 1, 31, 37 and 44, claim 61 requires the use of a separate input port and a plurality of output ports, and beam-deflecting elements that are dynamically and continuously controlled to direct a plurality of spectral channels into a plurality of output ports. As set forth above, Aksyuk does not disclose or suggest the use of a separate input port and a plurality of output ports, or continuously controllable beam deflecting elements. For at least these reasons, claim 61 is allowable over the prior art of record.

#### Claim 21

Claim 21 recites a servo-based optical apparatus including an input port, a plurality of output ports, a micromirror array and a "servo-control assembly, in communication with the micromirrors and said output ports, for maintaining a predetermined coupling for each reflected spectral channel into one of said output ports." The servo-control assembly is shown for example in Figure 4A and is described on pages 17 and 18 of the pending application. The servo-control assembly allows the power levels of the spectral channels coupled into the output ports to be dynamically managed. Aksyuk neither discloses or suggests any type of servo-control assembly whatsoever. Because this element is completely missing from Aksyuk, Aksyuk can neither anticipate nor render obvious any of claim 21.

#### CONCLUSIONS

Applicant's invention is both novel and nonobvious over the prior art for the reasons set forth above. None of the prior art of record, either alone or in combination, teaches each and every element of Applicant's claimed invention.

For all of these reasons, Applicant respectfully asserts that claims 1-67 are in condition for allowance. The Examiner's early reconsideration is respectfully requested. If

the Examiner has any questions, the Examiner is invited to contact Applicant's attorney at the following address or telephone number:

David Alberti c/o Patent Department GRAY CARY WARE & FREIDENRICH LLP 1755 Embarcadero Road Palo Alto, CA 94303 Telephone: (650) 833-2052

Respectfully submitted,

David Alberti

Reg. No. 43,465

Dated: January 24, 2003

#### Appendix A

## Claim 31 (amended, marked up version)

An optical apparatus comprising:

- f) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- g) a wavelength-separator, for separating said multi-wavelength optical signal from said input port into multiple spectral channels;
- h) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually <u>and continuously</u> controllable to reflect said spectral channels into selected ones of said output ports; and
- j) a one-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

#### Claim 37 (amended, marked-up version)

An optical apparatus comprising:

- f) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- g) a wavelength-separator, for separating said multi-wavelength optical signal from said input port into multiple spectral channels;
- h) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;

 a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually <u>and continuously</u> controllable to reflect said spectral channels into selected ones of said output ports; and

 a two-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

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	Brian M. Healy	2874	Page 1 of 1

#### **U.S. PATENT DOCUMENTS**

*		Document Number Country Code-Number-Kind Code	Date MM-YYYY	Name	Classification
*	A	US-6,222,954	04-2001	Riza, Nabeel Agha	385/18
*	в	US-6,205,269	03-2001	Morton, Paul A.	385/24
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۲	v	U.S. Patent Application Publication No. 2003/0043471A1 (BELSER ET. AL.), 03/06/2003.
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U.S. Patent and Trademark Office PTO-892 (Rev. 01-2001)

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09/938,426	08/23/2001	Jeffrey	P. Wilde	210393-991101	2587
APPI N TYPE	SMALL ENTITY	ISSUE FEE	PUBLICATION FEE	TOTAL FEE(S) DUE	DATE DUE
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APPLICATION NO.	FILING DATE		FIRST NAMED INVENTOR		ATTORNEY DOCKET NO.	CONFIRMATION NO	
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#### Determination of Patent Term Adjustment under 35 U.S.C. 154 (b) (application filed on or after May 29, 2000)

The patent term adjustment to date is 0 days. If the issue fee is paid on the date that is three months after the mailing date of this notice and the patent issues on the Tuesday before the date that is 28 weeks (six and a half months) after the mailing date of this notice, the term adjustment will be 0 days.

If a continued prosecution application (CPA) was filed in the above-identified application, the filing date that determines patent term adjustment is the filing date of the most recent CPA.

Applicant will be able to obtain more detailed information by accessing the Patent Application Information Retrieval (PAIR) system. (http://pair.uspto.gov)

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#### Notice of Fee Increase on October 1, 2002

If a reply to a "Notice of Allowance and Fee(s) Due" is filed in the Office on or after October 1, 2002, then the amount due may be higher than that set forth in the "Notice of Allowance and Fee(s) Due" since there will be an increase in fees effective on October 1, 2002. See Revision of Patent and Trademark Fees for Fiscal Year 2003; Notice of Proposed Rulemaking, 67 Fed. Reg. 30634, 30636 (May 7, 2002). Although a change to the amount of the publication fee is not currently proposed for October 2002, if the issue fee or publication fee is to be paid on or after October 1, 2002, applicant should check the USPTO web site for the current fees before submitting the payment. The USPTO Internet address for the fee schedule is: http://www.uspto.gov/main/howtofees.htm.

If the issue fee paid is the amount shown on the "Notice of Allowance and Fee(s) Due," but not the correct amount in view of the fee increase, a "Notice to Pay Balance of Issue Fee" will be mailed to applicant. In order to avoid processing delays associated with mailing of a "Notice to Pay Balance of Issue Fee," if the response to the Notice of Allowance and Fee(s) due form is to be filed on or after October 1, 2002 (or mailed with a certificate of mailing on or after October 1, 2002), the issue fee paid should be the fee that is required at the time the fee is paid. If the issue fee was previously paid, and the response to the "Notice of Allowance and Fee(s) Due" includes a request to apply a previously-paid issue fee to the issue fee now due, then the difference between the issue fee amount at the time the response is filed and the previously paid issue fee should be paid. See Manual of Patent Examining Procedure, Section 1308.01 (Eighth Edition, August 2001).

Effective October 1, 2002, 37 CFR 1.18 is proposed to be revised to change the patent issue fees as set forth below. As stated above, the final fees may be a different amount, and applicant should check the web site given above when paying the fee.

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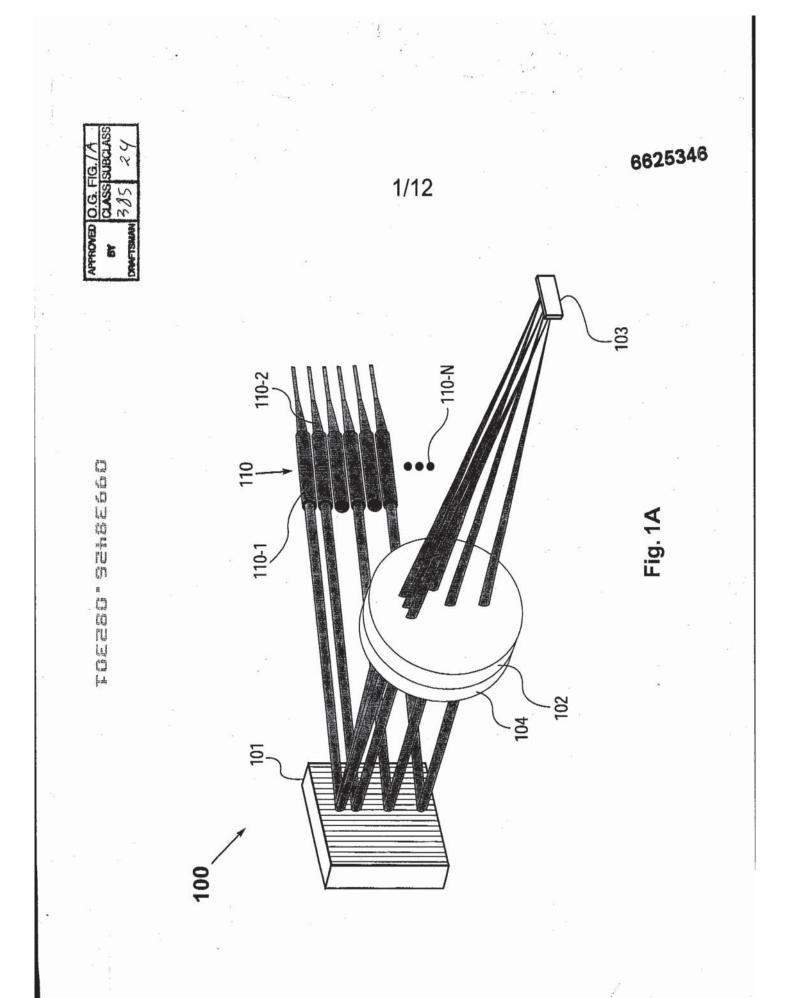
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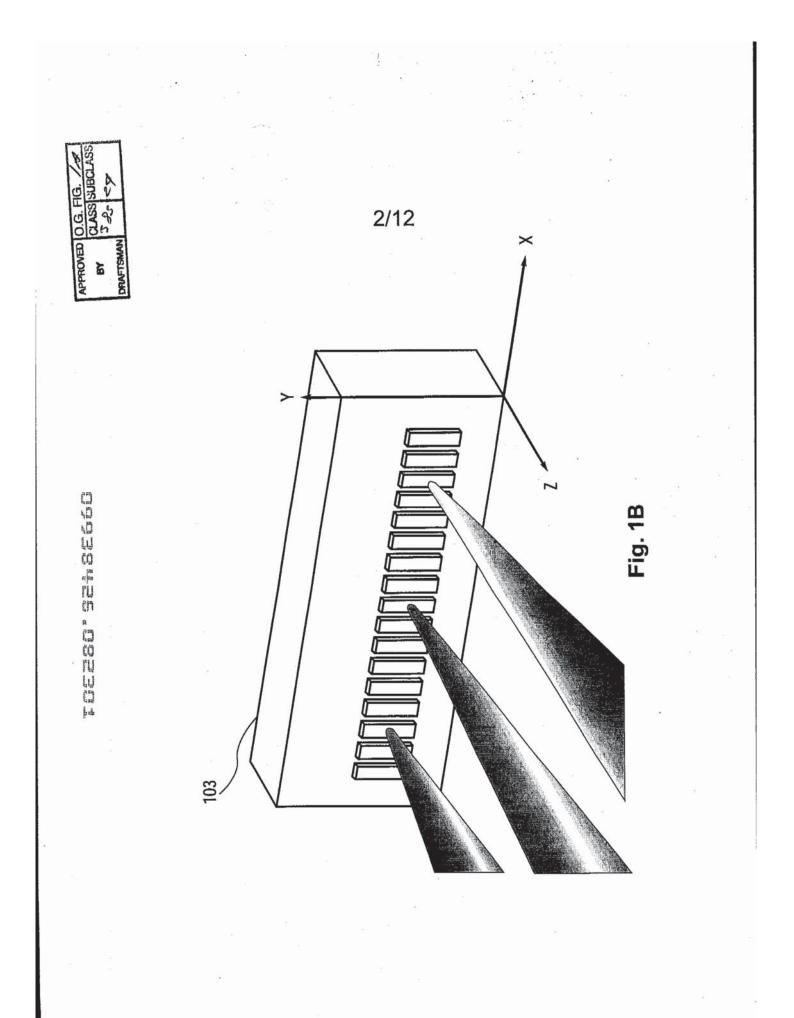
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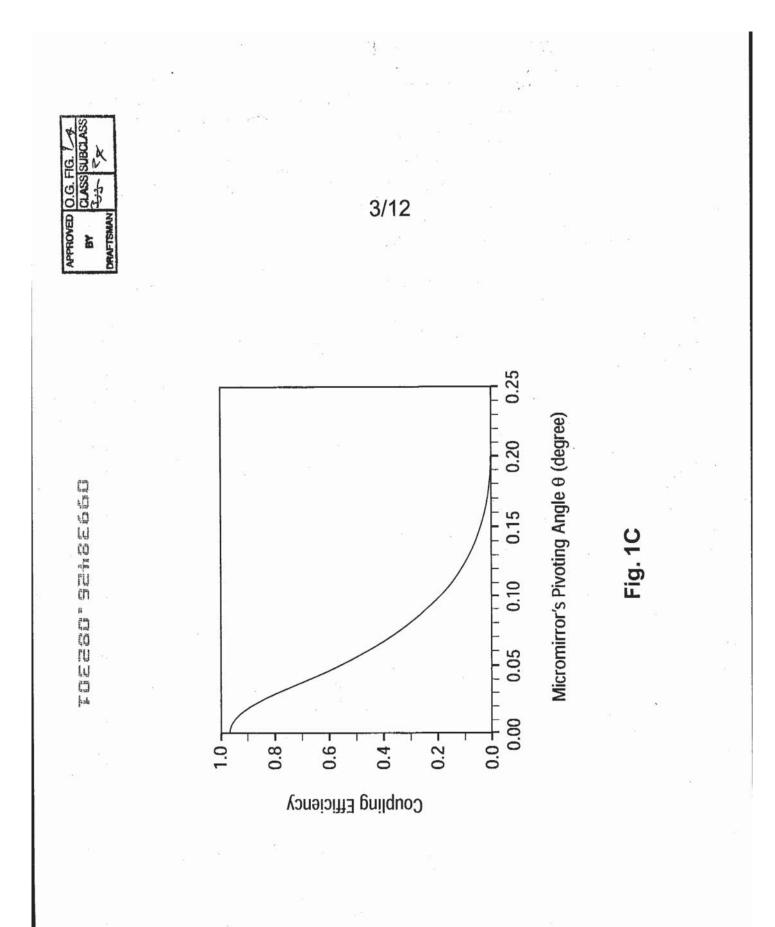
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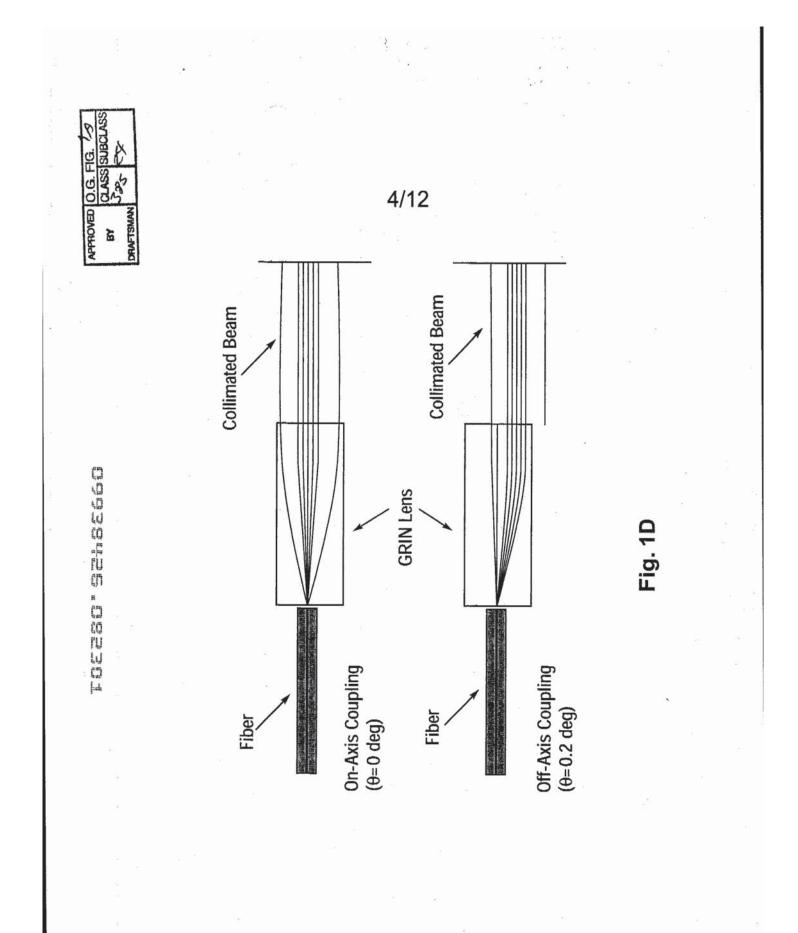
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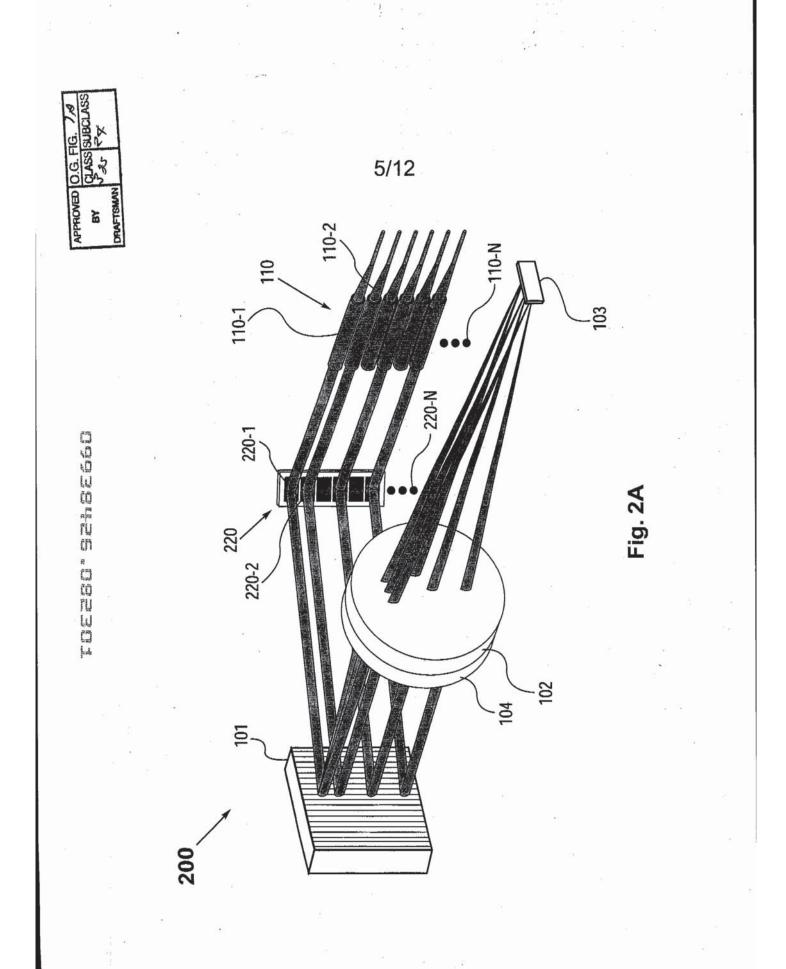
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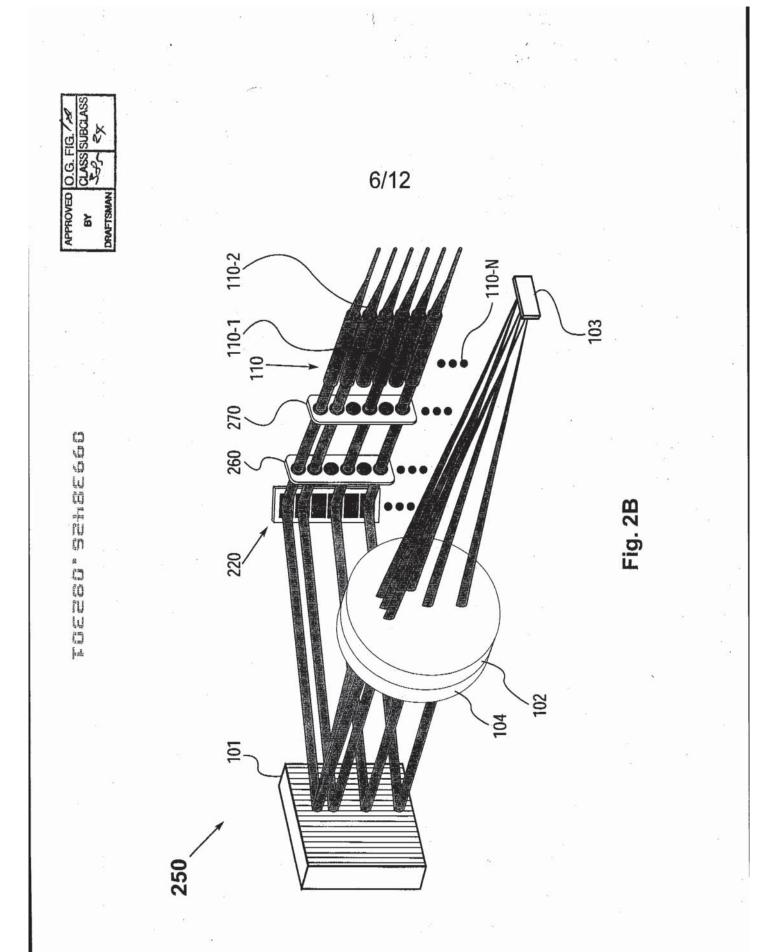


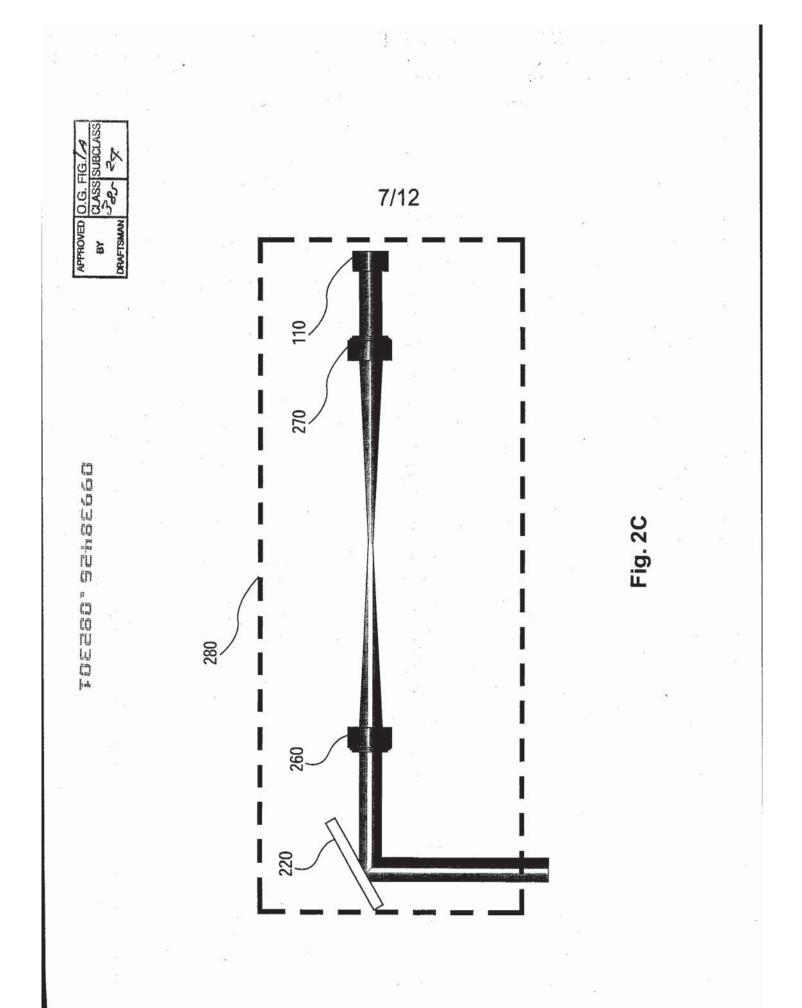


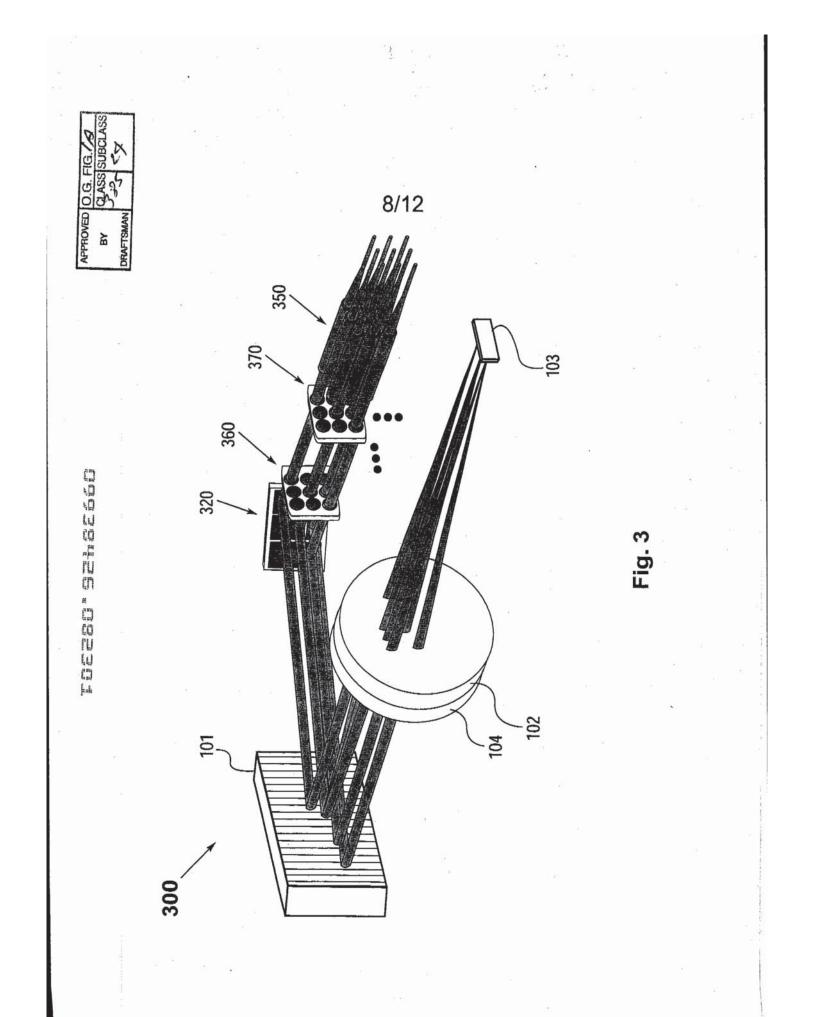












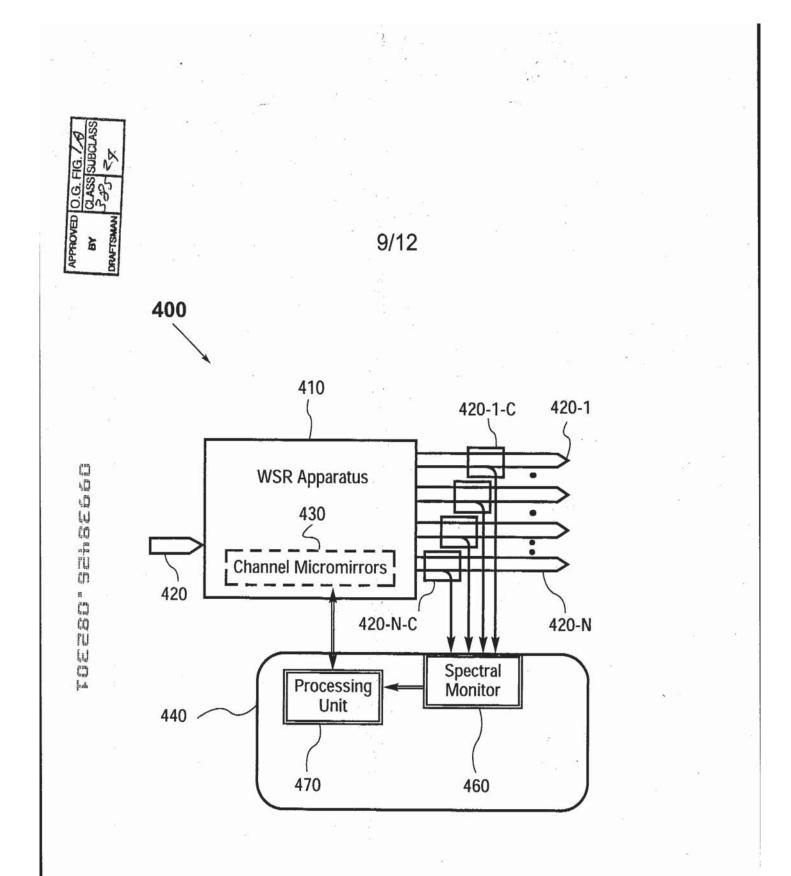
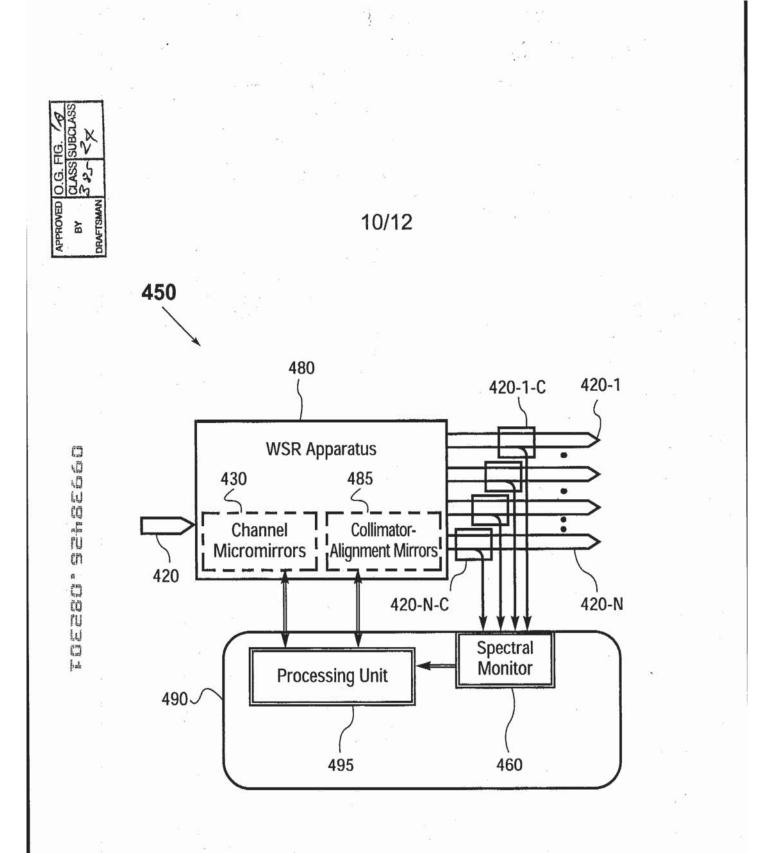
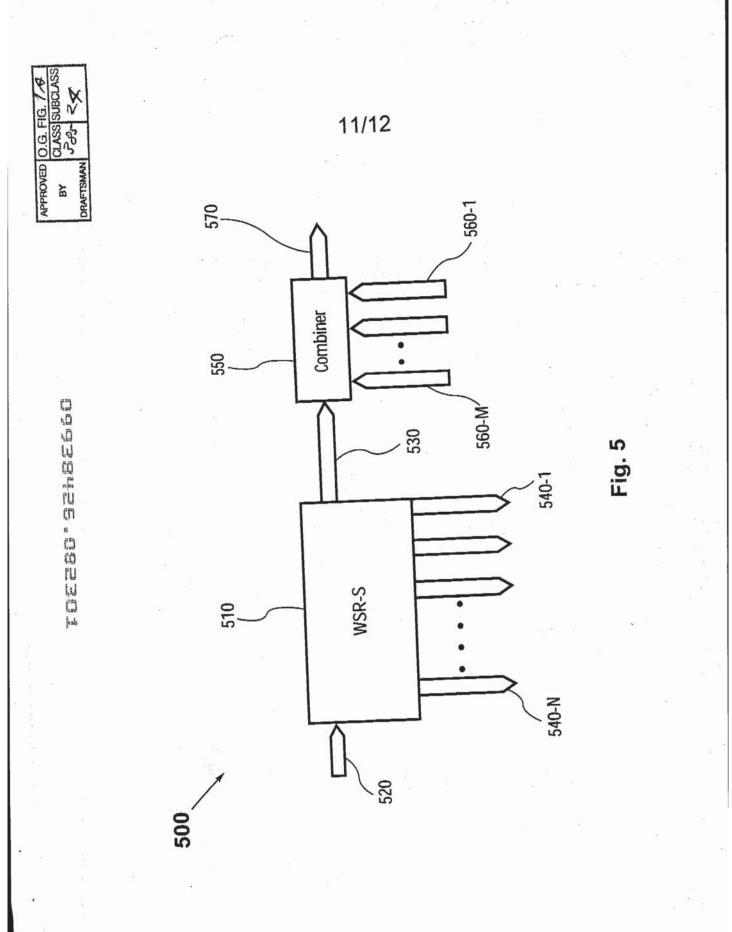
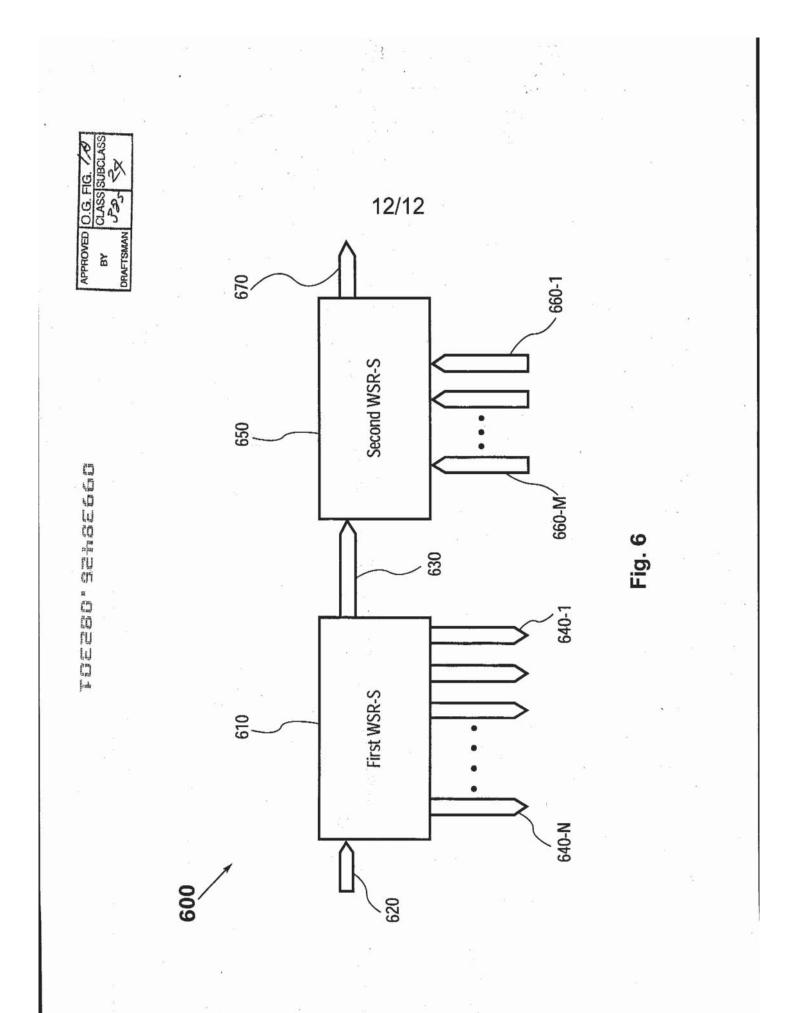


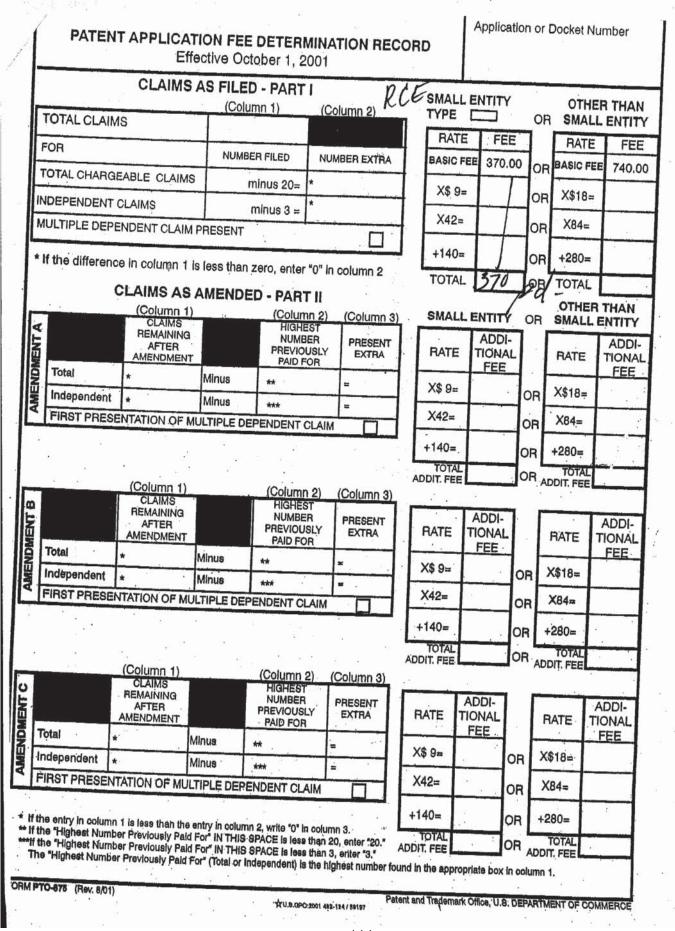
Fig. 4A



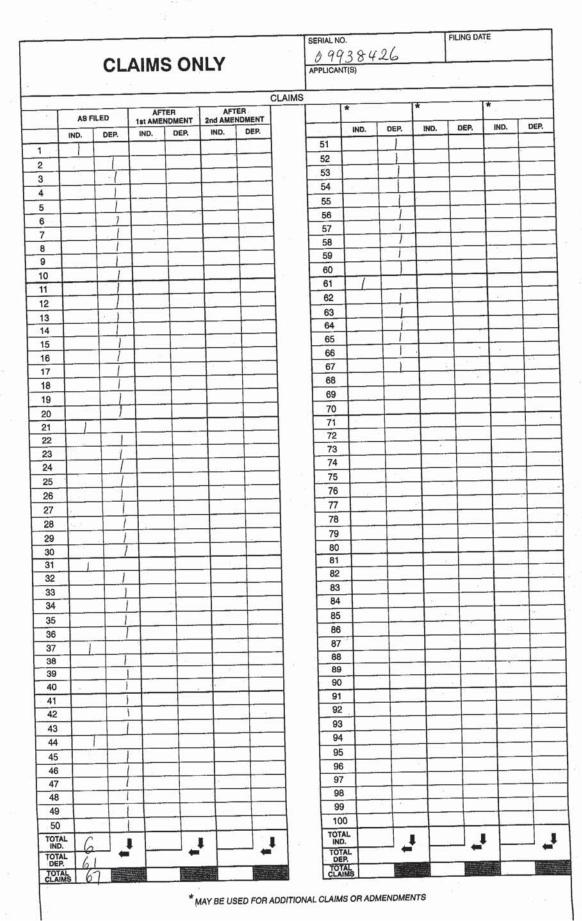
# Fig. 4B







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# (19) United States

# (12) Patent Application Publication Wilde (10) Pub. No.: US 2002/0131687 A1 (43) Pub. Date: Sep. 19, 2002

(54) RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES

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- (21) Appl. No.: 09/938,426
- (22) Filed: Aug. 23, 2001

### Related U.S. Application Data

(60) Provisional application No. 60/277,217, filed on Mar. 19, 2001.

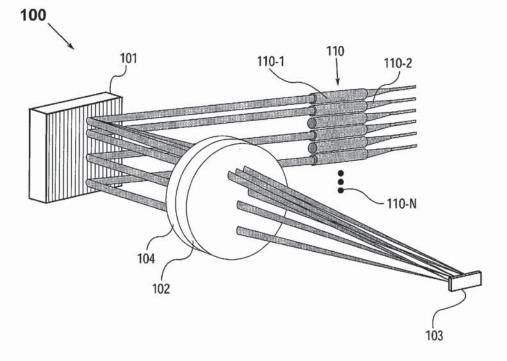
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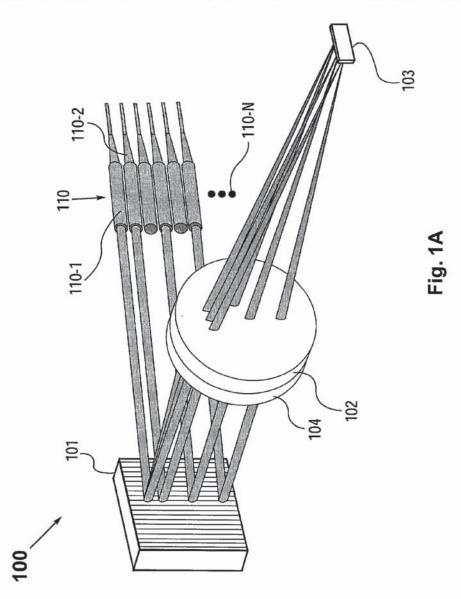
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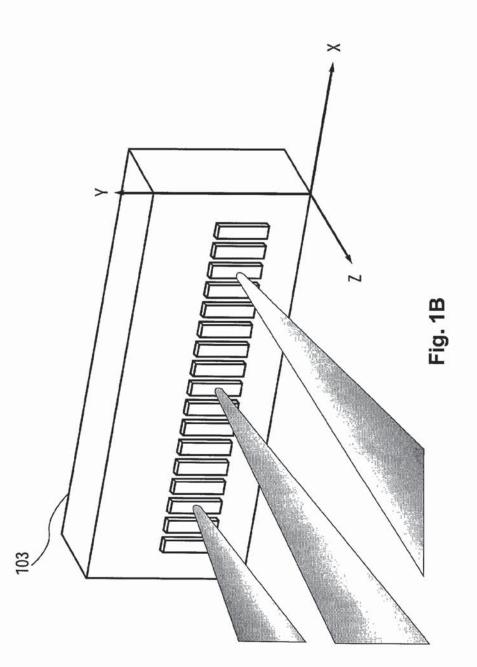
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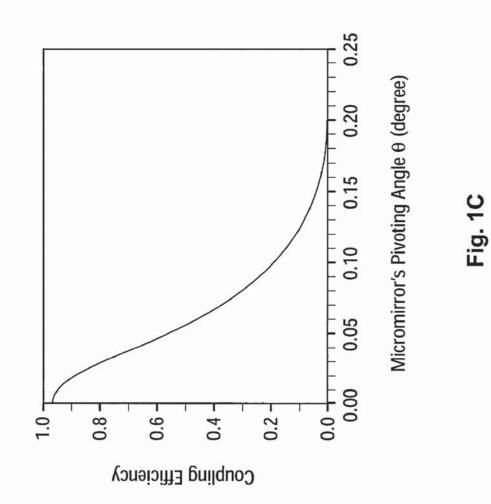
# (57) ABSTRACT

This invention provides a novel wavelength-separatingrouting (WSR) apparatus that uses a diffraction grating to separate a multi-wavelength optical signal by wavelength into multiple spectral channels, which are then focused onto an array of corresponding channel micromirrors. The channel micromirrors are individually controllable and continuously pivotable to reflect the spectral channels into selected output ports. As such, the inventive WSR apparatus is capable of routing the spectral channels on a channel-bychannel basis and coupling any spectral channel into any one of the output ports. The WSR apparatus of the present invention may be further equipped with servo-control and spectral power-management capabilities, thereby maintaining the coupling efficiencies of the spectral channels into the output ports at desired values. The WSR apparatus of the present invention can be used to construct a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs) for WDM optical networking applications.

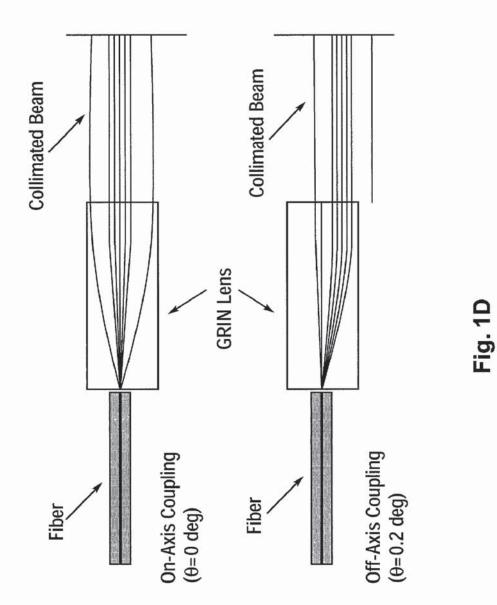


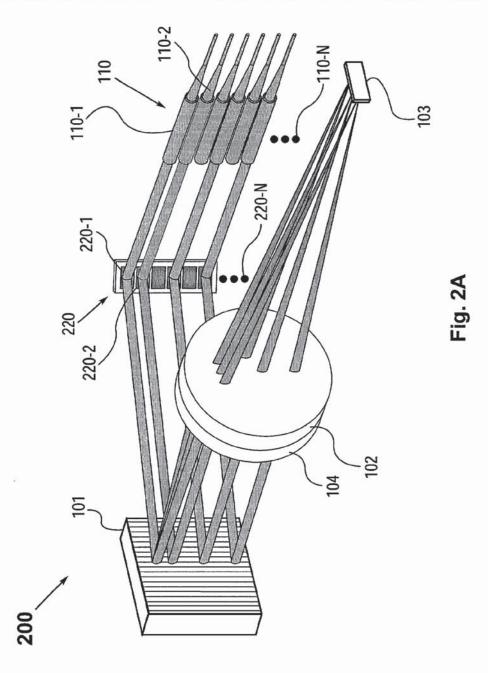


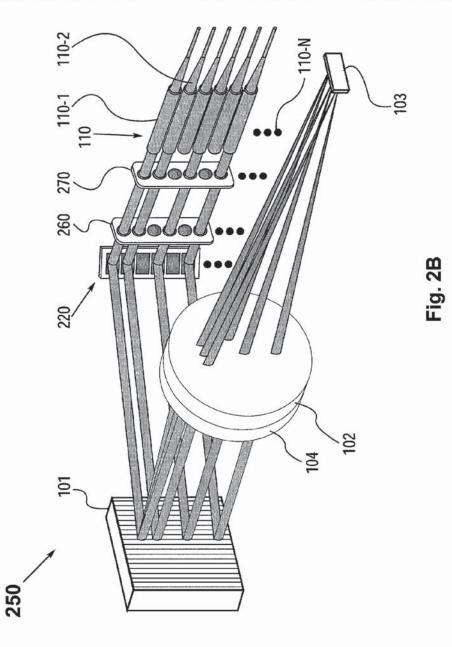


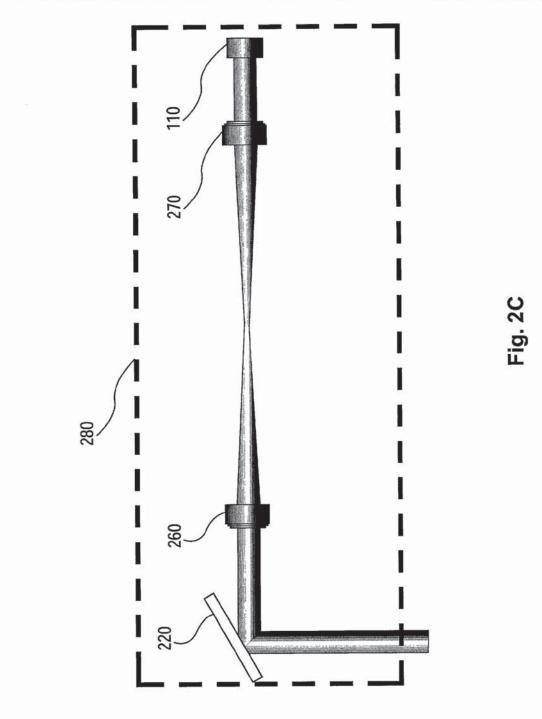


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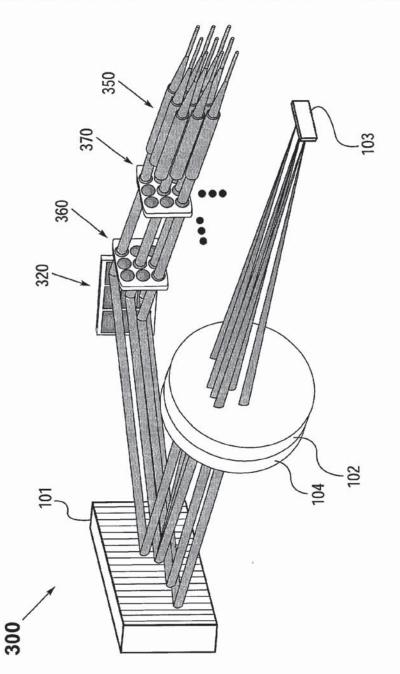


Fig. 3

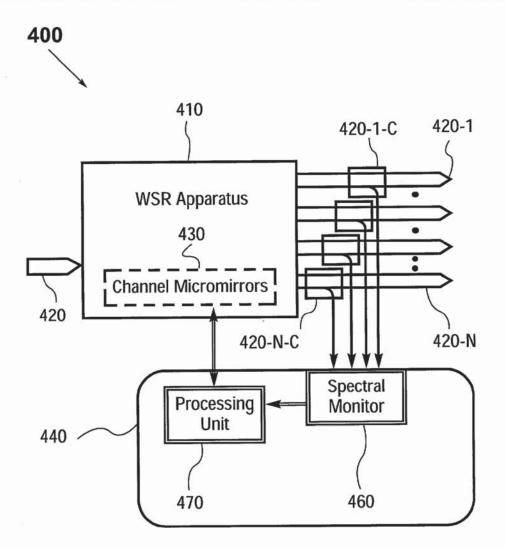


Fig. 4A

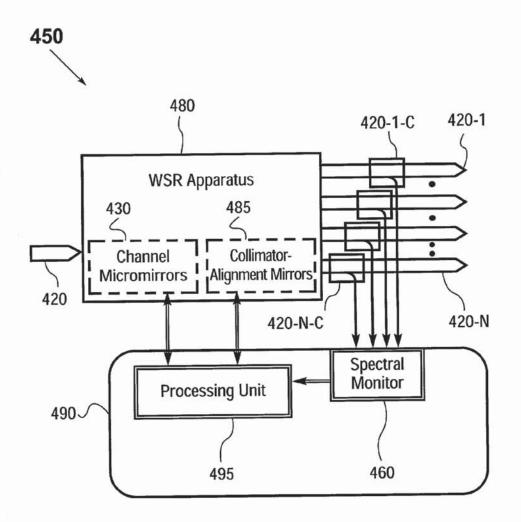
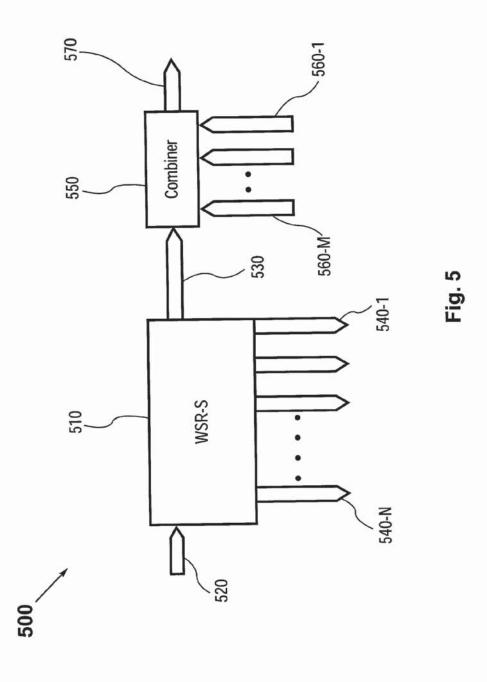


Fig. 4B



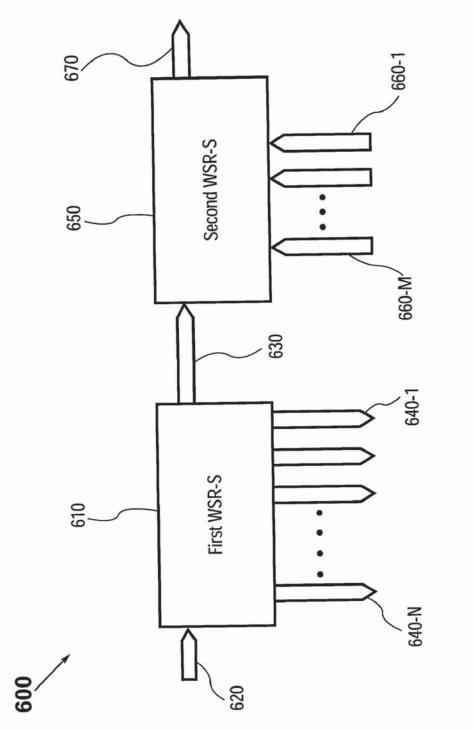


Fig. 6

### RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES

1

### CROSS REFERENCE TO RELATED APPLICATIONS

**[0001]** This application claims priority of U.S. Provisional Patent Application No. 60/277,217, filed Mar. 19, 2001, which is incorporated herein by reference.

### FIELD OF THE INVENTION

[0002] This invention relates generally to optical communication systems. More specifically, it relates to a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs) for wavelength division multiplexed optical networking applications.

### BACKGROUND

**[0003]** As fiber-optic communication networks rapidly spread into every walk of modem life, there is a growing demand for optical components and subsystems that enable the fiber-optic communications networks to be increasingly scalable, versatile, robust, and cost-effective.

[0004] Contemporary fiber-optic communications networks commonly employ wavelength division multiplexing (WDM), for it allows multiple information (or data) channels to be simultaneously transmitted on a single optical fiber by using different wavelengths and thereby significantly enhances the information bandwidth of the fiber. The prevalence of WDM technology has made optical add-drop multiplexers indispensable building blocks of modem fiberoptic communication networks. An optical add-drop multiplexer (OADM) serves to selectively remove (or drop) one or more wavelengths from a multiplicity of wavelengths on an optical fiber, hence taking away one or more data channels from the traffic stream on the fiber. It further adds one or more wavelengths back onto the fiber, thereby inserting new data channels in the same stream of traffic. As such, an OADM makes it possible to launch and retrieve multiple data channels (each characterized by a distinct wavelength) onto and from an optical fiber respectively, without disrupting the overall traffic flow along the fiber. Indeed, careful placement of the OADMs can dramatically improve an optical communication network's flexibility and robustness, while providing significant cost advantages.

[0005] Conventional OADMs in the art typically employ multiplexers/demultiplexers (e.g, waveguide grating routers or arrayed-waveguide gratings), tunable filters, optical switches, and optical circulators in a parallel or serial architecture to accomplish the add and drop functions. In the parallel architecture, as exemplified in U.S. Pat. No. 5,974, 207, a demultiplexer (e.g., a waveguide grating router) first separates a multi-wavelength signal into its constituent spectral components. A wavelength switching/routing means (e.g., a combination of optical switches and optical circulators) then serves to drop selective wavelengths and add others. Finally, a multiplexer combines the remaining (i.e., the pass-through) wavelengths into an output multiwavelength optical signal. In the serial architecture, as exemplified in U.S. Pat. No. 6,205,269, tunable filters (e.g., Bragg fiber gratings) in combination with optical circulators are used to separate the drop wavelengths from the passthrough wavelengths and subsequently launch the add channels into the pass-through path. And if multiple wavelengths are to be added and dropped, additional multiplexers and demultiplexers are required to demultiplex the drop wavelengths and multiplex the add wavelengths, respectively. Irrespective of the underlying architecture, the OADMs currently in the art are characteristically high in cost, and prone to significant optical loss accumulation. Moreover, the designs of these OADMs are such that it is inherently difficult to reconfigure them in a dynamic fashion.

[0006] U.S. Pat. No. 6,204,946 to Askyuk et al. discloses an OADM that makes use of free-space optics in a parallel construction. In this case, a multi-wavelength optical signal emerging from an input port is incident onto a ruled diffraction grating. The constituent spectral channels thus separated are then focused by a focusing lens onto a linear array of binary micromachined mirrors. Each micromirror is configured to operate between two discrete states, such that it either retroreflects its corresponding spectral channel back into the input port as a pass-through channel, or directs its spectral channel to an output port as a drop channel. As such, the pass-through signal (i.e., the combined pass-through channels) shares the same input port as the input signal. An optical circulator is therefore coupled to the input port, to provide necessary routing of these two signals. Likewise, the drop channels share the output port with the add channels. An additional optical circulator is thereby coupled to the output port, from which the drop channels exit and the add channels are introduced into the output port. The add channels are subsequently combined with the pass-through signal by way of the diffraction grating and the binary micromirrors.

[0007] Although the aforementioned OADM disclosed by Askyuk et al. has the advantage of performing wavelength separating and routing in free space and thereby incurring less optical loss, it suffers a number of limitations. First, it requires that the pass-through signal share the same port/ fiber as the input signal. An optical circulator therefore has to be implemented, to provide necessary routing of these two signals. Likewise, all the add and drop channels enter and leave the OADM through the same output port, hence the need for another optical circulator. Moreover, additional means must be provided to multiplex the add channels before entering the system and to demultiplex the drop channels after exiting the system. This additional multiplexing/demultiplexing requirement adds more cost and complexity that can restrict the versatility of the OADM thusconstructed. Second, the optical circulators implemented in this OADM for various routing purposes introduce additional optical losses, which can accumulate to a substantial amount. Third, the constituent optical components must be in a precise alignment, in order for the system to achieve its intended purpose. There are, however, no provisions provided for maintaining the requisite alignment; and no mechanisms implemented for overcoming degradation in the alignment owing to environmental effects such as thermal and mechanical disturbances over the course of operation.

[0008] U.S. Pat. No. 5,906,133 to Tomlinson discloses an OADM that makes use of a design similar to that of Aksyuk et al. There are input, output, drop and add ports implemented in this case. By positioning the four ports in a

specific arrangement, each micromirror, notwithstanding switchable between two discrete positions, either reflects its corresponding channel (coming from the input port) to the output port, or concomitantly reflects its channel to the drop port and an incident add channel to the output port. As such, this OADM is able to perform both the add and drop functions without involving additional optical components (such as optical circulators used in the system of Aksyuk et al.). However, because a single drop port is designated for all the drop channels and a single add port is designated for all the add channels, the add channels would have to be multiplexed before entering the add port and the drop channels likewise need to be demutiplxed upon exiting from the drop port. Moreover, as in the case of Askyuk et al., there are no provisions provided for maintaining requisite optical alignment in the system, and no mechanisms implemented for combating degradation in the alignment due to environmental effects over the course of operation.

**[0009]** As such, the prevailing drawbacks suffered by the OADMs currently in the art are summarized as follows:

- [0010] 1) The wavelength routing is intrinsically static, rendering it difficult to dynamically reconfigure these OADMs.
- [0011] 2) Add and/or drop channels often need to be multiplexed and/or demultiplexed, thereby imposing additional complexity and cost.
- [0012] 3) Stringent fabrication tolerance and painstaking optical alignment are required. Moreover, the optical alignment is not actively maintained, rendering it susceptible to environmental effects such as thermal and mechanical disturbances over the course of operation.
- [0013] 4) In an optical communication network, OADMs are typically in a ring or cascaded configuration. In order to mitigate the interference amongst OADMs, which often adversely affects the overall performance of the network, it is essential that the power levels of spectral channels entering and exiting each OADM be managed in a systematic way, for instance, by introducing power (or gain) equalization at each stage. Such a power equalization capability is also needed for compensating for non-uniform gain caused by optical amplifiers (e.g., erbium doped fiber amplifiers) in the network. There lacks, however, a systematic and dynamic management of the power levels of various spectral channels in these OADMs.
- [0014] 5) The inherent high cost and heavy optical loss further impede the wide application of these OADMs.

**[0015]** In view of the foregoing, there is an urgent need in the art for optical add-drop multiplexers that overcome the aforementioned shortcomings in a simple, effective, and economical construction.

#### SUMMARY

**[0016]** The present invention provides a wavelength-separating-routing (WSR) apparatus and method which employ an array of fiber collimators serving as an input port and a plurality of output ports; a wavelength-separator; a beamfocuser; and an array of channel micromirrors.

[0017] In operation, a multi-wavelength optical signal emerges from the input port. The wavelength-separator separates the multi-wavelength optical signal into multiple spectral channels, each characterized by a distinct center wavelength and associated bandwidth. The beam-focuser focuses the spectral channels into corresponding spectral spots. The channel micromirrors are positioned such that each channel micromirror receives one of the spectral channels. The channel micromirrors are individually controllable and movable, e.g., continuously pivotable (or rotatable), so as to reflect the spectral channels into selected ones of the output ports. As such, each channel micromirror is assigned to a specific spectral channel, hence the name "channel micromirror". And each output port may receive any number of the reflected spectral channels.

**[0018]** A distinct feature of the channel micromirrors in the present invention, in contrast to those used in the prior art, is that the motion, e.g., pivoting (or rotation), of each channel micromirror is under analog control such that its pivoting angle can be continuously adjusted. This enables each channel micromirror to scan its corresponding spectral channel across all possible output ports and thereby direct the spectral channel to any desired output port.

[0019] In the WSR apparatus of the present invention, the wavelength-separator may be provided by a ruled diffraction grating, a holographic diffraction grating, an echelle grating, a curved diffraction grating, a dispersing prism, or other wavelength-separating means known in the art. The beam-focuser may be a single lens, an assembly of lenses, or other beam-focusing means known in the art. The channel micro-mirrors may be provided by silicon micromachined mirrors, reflective ribbons (or membranes), or other types of beam-deflecting means known in the art. And each channel micro-mirror may be pivotable about one or two axes. The fiber collimators serving as the input and output ports may be arranged in a one-dimensional or two-dimensional array. In the latter case, the channel micromirrors must be pivotable biaxially.

**[0020]** The WSR apparatus of the present invention may further comprise an array of collimator-alignment mirrors, in optical communication with the wavelength-separator and the fiber collimators, for adjusting the alignment of the input multi-wavelength signal and directing the spectral channels into the selected output ports by way of angular control of the collimated beams. Each collimator-alignment mirror may be rotatable about one or two axes. The collimatoralignment mirrors may be arranged in a one-dimensional or two-dimensional array. First and second arrays of imaging lenses may additionally be optically interposed between the collimator-alignment mirrors and the fiber collimators in a telecentric arrangement, thereby "imaging" the collimatoralignment mirrors onto the corresponding fiber collimators to ensure an optimal alignment.

[0021] The WSR apparatus of the present invention may further include a servo-control assembly, in communication with the channel micromirrors and the output ports. The servo-control assembly serves to monitor the power levels of the spectral channels coupled into the output ports and further provide control of the channel micromirrors on an individual basis, so as to maintain a predetermined coupling efficiency of each spectral channel in one of the output ports. As such, the servo-control assembly provides dynamic control of the coupling of the spectral channels into the respective output ports and actively manages the power levels of the spectral channels coupled into the output ports. (If the WSR apparatus includes an array of collimator-alignment mirrors as described above, the servo-control assembly may additionally provide dynamic control of the collimatoralignment mirrors.) Moreover, the utilization of such a servo-control assembly effectively relaxes the requisite fabrication tolerances and the precision of optical alignment during assembly of a WSR apparatus of the present invention, and further enables the system to correct for shift in optical alignment over the course of operation. A WSR apparatus incorporating a servo-control assembly thus described is termed a WSR-S apparatus, thereinafter in the present invention.

**[0022]** Accordingly, the WSR-S (or WSR) apparatus of the present invention may be used to construct a variety of optical devices, including a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs), as exemplified in the following embodiments.

**[0023]** One embodiment of an OADM of the present invention comprises an aforementioned WSR-S (or WSR) apparatus and an optical combiner. The output ports of the WSR-S apparatus include a pass-through port and one or more drop ports, each carrying any number of the spectral channels. The optical combiner is coupled to the pass-through port, serving to combine the pass-through channels with one or more add spectral channels. The combined optical signal constitutes an output signal of the system. The optical combiner may be an N×1 (N $\geq$ 2) broadband fiber-optic coupler, for instance, which also serves the purpose of multiplexing a multiplicity of add spectral channels to be coupled into the system.

**[0024]** In another embodiment of an OADM of the present invention, a first WSR-S (or WSR) apparatus is cascaded with a second WSR-S (or WSR) apparatus. The output ports of the first WSR-S (or WSR) apparatus include a pass-through port and one or more drop ports.

[0025] The second WSR-S (or WSR) apparatus includes a plurality of input ports and an exiting port. The configuration is such that the pass-through channels from the first WSR-S apparatus and one or more add channels are directed into the input ports of the second WSR-S apparatus, and consequently multiplexed into an output multi-wavelength optical signal directed into the exiting port of the second WSR-S apparatus. That is to say that in this embodiment, one WSR-S apparatus (e.g., the first one) effectively performs a dynamic drop function, whereas the other WSR-S apparatus (e.g., the second one) carries out a dynamic add function. And there are essentially no fundamental restrictions on the wavelengths that can be added or dropped, other than those imposed by the overall communication system. Moreover, the underlying OADM architecture thus presented is intrinsically scalable and can be readily extended to any number of the WSR-S (or WSR) systems, if so desired for performing intricate add and drop functions in a network environment.

**[0026]** Those skilled in the art will recognize that the aforementioned embodiments provide only two of many embodiments of a dynamically reconfigurable OADM according to the present invention. Various changes, substitutions, and alternations can be made herein, without depart-

ing from the principles and the scope of the invention. Accordingly, a skilled artisan can design an OADM in accordance with the present invention, to best suit a given application.

**[0027]** All in all, the OADMs of the present invention provide many advantages over the prior art devices, notably:

- [0028] 1) By advantageously employing an array of channel micromirrors that are individually and continuously controllable, an OADM of the present invention is capable of routing the spectral channels on a channel-by-channel basis and directing any spectral channel into any one of the output ports. As such, its underlying operation is dynamically reconfigurable, and its underlying architecture is intrinsically scalable to a large number of channel counts.
- [0029] 2) The add and drop spectral channels need not be multiplexed and demultiplexed before entering and after leaving the OADM respectively. And there are not fundamental restrictions on the wavelengths to be added or dropped.
- **[0030]** 3) The coupling of the spectral channels into the output ports is dynamically controlled by a servo-control assembly, rendering the OADM less susceptible to environmental effects (such as thermal and mechanical disturbances) and therefore more robust in performance. By maintaining an optimal optical alignment, the optical losses incurred by the spectral channels are also significantly reduced.
- [0031] 4) The power levels of the spectral channels coupled into the output ports can be dynamically managed according to demand, or maintained at desired values (e.g., equalized at a predetermined value) by way of the servo-control assembly. This spectral power-management capability as an integral part of the OADM will be particularly desirable in WDM optical networking applications.
- [0032] 5) The use of free-space optics provides a simple, low loss, and cost-effective construction. Moreover, the utilization of the servo-control assembly effectively relaxes the requisite fabrication tolerances and the precision of optical alignment during initial assembly, enabling the OADM to be simpler and more adaptable in structure, lower in cost and optical loss.
- [0033] 6) The underlying OADM architecture allows a multiplicity of the OADMs according to the present invention to be readily assembled (e.g., cascaded) for WDM optical networking applications.

**[0034]** The novel features of this invention, as well as the invention itself, will be best understood from the following drawings and detailed description.

# BRIEF DESCRIPTION OF THE FIGURES

**[0035]** FIGS. 1A-1D show a first embodiment of a wavelength-separating-routing (WSR) apparatus according to the present invention, and the modeling results demonstrating the performance of the WSR apparatus;

**[0036]** FIGS. **2A-2**C depict second and third embodiments of a WSR apparatus according to the present invention;

**[0037] FIG. 3** shows a fourth embodiment of a WSR apparatus according to the present invention;

**[0038]** FIGS. **4A-4**B show schematic illustrations of two embodiments of a WSR-S apparatus comprising a WSR apparatus and a servo-control assembly, according to the present invention;

**[0039]** FIG. 5 depicts an exemplary embodiment of an optical add-drop multiplexer (OADM) according to the present invention; and

**[0040] FIG. 6** shows an alternative embodiment of an OADM according to the present invention.

### DETAILED DESCRIPTION

**[0041]** In this specification and appending claims, a "spectral channel" is characterized by a distinct center wavelength and associated bandwidth. Each spectral channel may carry a unique information signal, as in WDM optical networking applications.

[0042] FIG. 1A depicts a first embodiment of a wavelength-separating-routing (WSR) apparatus according to the present invention. By way of example to illustrate the general principles and the topological structure of a wavelength-separating-routing (WSR) apparatus of the present invention, the WSR apparatus 100 comprises multiple input/output ports which may be in the form of an array of fiber collimators 110, providing an input port 110-1 and a plurality of output ports 110-2 through 110-N (N $\geq$ 3); a wavelength-separator which in one form may be a diffraction grating 101; a beam-focuser in the form of a focusing lens 102; and an array of channel micromirrors 103.

[0043] In operation, a multi-wavelength optical signal emerges from the input port 110-1. The diffraction grating 101 angularly separates the multi-wavelength optical signal into multiple spectral channels, which are in turn focused by the focusing lens 102 into a spatial array of distinct spectral spots (not shown in FIG. 1A) in a one-to-one correspondence. The channel micromirrors 103 are positioned in accordance with the spatial array formed by the spectral spots, such that each channel micromirror receives one of the spectral channels. The channel micromirrors 103 are individually controllable and movable, e.g., pivotable (or rotatable) under analog (or continuous) control, such that, upon reflection, the spectral channels are directed into selected ones of the output ports 110-2 through 110-N by way of the focusing lens 102 and the diffraction grating 101. As such, each channel micromirror is assigned to a specific spectral channel, hence the name 37 channel micromirror 38. Each output port may receive any number of the reflected spectral channels.

[0044] For purposes of illustration and clarity, only a selective few (e.g., three) of the spectral channels, along with the input multi-wavelength optical signal, are graphically illustrated in FIG. 1A and the following figures. It should be noted, however, that there can be any number of the spectral channels in a WSR apparatus of the present invention (so long as the number of spectral channels does not exceed the number of channel mirrors employed in the system). It should also be noted that the optical beams representing the spectral channels shown in FIG. 1A and the following figures are provided for illustrative purpose only. That is, their sizes and shapes may not be drawn according

to scale. For instance, the input beam and the corresponding diffracted beams generally have different cross-sectional shapes, so long as the angle of incidence upon the diffraction grating is not equal to the angle of diffraction, as is known to those skilled in the art.

[0045] In the embodiment of FIG. 1A, it is preferable that the diffraction grating 101 and the channel micromirrors 103 are placed respectively at the first and second (i.e., the front and back) focal points (on the opposing sides) of the focusing lens 102. Such a telecentric arrangement allows the chief rays of the focused beams to be parallel to each other and generally parallel to the optical axis. In this application, the telecentric configuration further allows the reflected spectral channels to be efficiently coupled into the respective output ports, thereby minimizing various translational walkoff effects that may otherwise arise. Moreover, the input multi-wavelength optical signal is preferably collimated and circular in cross-section. The corresponding spectral channels diffracted from the diffraction grating 101 are generally elliptical in cross-section; they may be of the same size as the input beam in one dimension and elongated in the other dimension.

[0046] It is known that the diffraction efficiency of a diffraction grating is generally polarization-dependent. That is, the diffraction efficiency of a grating in a standard mounting configuration may be considerably higher for P-polarization that is perpendicular to the groove lines on the grating than for S-polarization that is orthogonal to P-polarization, especially as the number of groove lines (per unit length) increases. To mitigate such polarization-sensitive effects, a quarter-wave plate 104 may be optically interposed between the diffraction grating 101 and the channel micromirrors 103, and preferably placed between the diffraction grating 101 and the focusing lens 102 as is shown in FIG. 1A. In this way, each spectral channel experiences a total of approximately 90-degree rotation in polarization upon traversing the quarter-wave plate 104 twice. (That is, if a beam of light has P-polarization when first encountering the diffraction grating, it would have predominantly (if not all) S-polarization upon the second encountering, and vice versa.) This ensures that all the spectral channels incur nearly the same amount of round-trip polarization dependent loss.

[0047] In the WSR apparatus 100 of FIG. 1A, the diffraction grating 101, by way of example, is oriented such that the focused spots of the spectral channels fall onto the channel micromirrors 103 in a horizontal array, as illustrated in FIG. 1B.

[0048] Depicted in FIG. 1B is a close-up view of the channel micromirrors 103 shown in the embodiment of FIG. 1A. By way of example, the channel micromirrors 103 are arranged in a one-dimensional array along the x-axis (i.e., the horizontal direction in the figure), so as to receive the focused spots of the spatially separated spectral channels in a one-to-one correspondence. (As in the case of FIG. 1A, only three spectral channels are illustrated, each represented by a converging beam.) Let the reflective surface of each channel micromirror lie in the x-y plane as defined in the figure and be movable, e.g., pivotable (or deflectable) about the x-axis in an analog (or continuous) manner. Each spectral channel, upon reflection, is deflected in the y-direction

(e.g., downward) relative to its incident direction, so to be directed into one of the output ports 110-2 through 110-N shown in FIG. 1A.

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[0049] As described above, a unique feature of the present invention is that the motion of each channel micromirror is individually and continuously controllable, such that its position, e.g., pivoting angle, can be continuously adjusted. This enables each channel micromirror to scan its corresponding spectral channel across all possible output ports and thereby direct the spectral channel to any desired output port. To illustrate this capability, FIG. 1C shows a plot of coupling efficiency as a function of a channel micromirror's pivoting angle  $\theta$ , provided by a ray-tracing model of a WSR apparatus in the embodiment of FIG. 1A. As used herein, the coupling efficiency for a spectral channel is defined as the ratio of the amount of optical power coupled into the fiber core in an output port to the total amount of optical power incident upon the entrance surface of the fiber (associated with the fiber collimator serving as the output port). In the ray-tracing model, the input optical signal is incident upon a diffraction grating with 700 lines per millimeter at a grazing angle of 85 degrees, where the grating is blazed to optimize the diffraction efficiency for the "-1" order. The focusing lens has a focal length of 100 mm. Each output port is provided by a quarter-pitch GRIN lens (2 mm in diameter) coupled to an optical fiber (see FIG. 1D). As displayed in FIG. 1C, the coupling efficiency varies with the pivoting angle  $\theta$ , and it requires about a 0.2-degree change in  $\theta$  for the coupling efficiency to become practically negligible in this exemplary case. As such, each spectral channel may practically acquire any coupling efficiency value by way of controlling the pivoting angle of its corresponding channel micromirror. This is also to say that variable optical attenuation at the granularity of a single wavelength can be obtained in a WSR apparatus of the present invention. FIG. 1D provides ray-tracing illustrations of two extreme points on the coupling efficiency vs.  $\theta$  curve of FIG. 1C: on-axis coupling corresponding to  $\theta=0$ , where the coupling efficiency is maximum; and off-axis coupling corresponding to  $\theta$ =0.2 degrees, where the representative collimated beam (representing an exemplary spectral channel) undergoes a significant translational walk-off and renders the coupling efficiency practically negligible. All in all, the exemplary modeling results thus described demonstrate the unique capabilities of the WSR apparatus of the present invention.

[0050] FIG. 1A provides one of many embodiments of a WSR apparatus according to the present invention. In general, the wavelength-separator is a wavelength-separating means that may be a ruled diffraction grating, a holographic diffraction grating, an echelle grating, a dispersing prism, or other types of spectral-separating means known in the art. The beam-focuser may be a focusing lens, an assembly of lenses, or other beam-focusing means known in the art. The focusing function may also be accomplished by using a curved diffraction grating as the wavelength-separator. The channel micromirrors may be provided by silicon micromachined mirrors, reflective ribbons (or membranes), or other types of beam-deflecting elements known in the art. And each micromirror may be pivoted about one or two axes. What is important is that the pivoting (or rotational) motion of each channel micromirror be individually controllable in an analog manner, whereby the pivoting angle can be continuously adjusted so as to enable the channel micromirror to scan a spectral channel across all possible output ports.

The underlying fabrication techniques for micromachined mirrors and associated actuation mechanisms are well documented in the art, see U.S. Pat. No. 5,629,790 for example. Moreover, a fiber collimator is typically in the form of a collimating lens (such as a GRIN lens) and a ferrulemounted fiber packaged together in a mechanically rigid stainless steel (or glass) tube. The fiber collimators serving as the input and output ports may be arranged in a onedimensional array, a two-dimensional array, or other desired spatial pattern. For instance, they may be conveniently mounted in a linear array along a V-groove fabricated on a substrate made of silicon, plastic, or ceramic, as commonly practiced in the art. It should be noted, however, that the input port and the output ports need not necessarily be in close spatial proximity with each other, such as in an array configuration (although a close packing would reduce the rotational range required for each channel micromirror). Those skilled in the art will know how to design a WSR apparatus according to the present invention, to best suit a given application.

[0051] A WSR apparatus of the present invention may further comprise an array of collimator-alignment mirrors, for adjusting the alignment of the input multi-wavelength optical signal and facilitating the coupling of the spectral channels into the respective output ports, as shown in FIGS. 2A-2B and 3.

[0052] Depicted in FIG. 2A is a second embodiment of a WSR apparatus according to the present invention. By way of example, WSR apparatus 200 is built upon and hence shares a number of the elements used in the embodiment of FIG. 1A, as identified by those labeled with identical numerals. Moreover, a one-dimensional array 220 of collimator-alignment mirrors 220-1 through 220-N is optically interposed between the diffraction grating 101 and the fiber collimator array 110. The collimator-alignment mirror 220-1 is designated to correspond with the input port 110-1, for adjusting the alignment of the input multi-wavelength optical signal and therefore ensuring that the spectral channels impinge onto the corresponding channel micromirrors. The collimator-alignment mirrors 220-2 through 220-N are designated to the output ports 110-2 through 110-N in a oneto-one correspondence, serving to provide angular control of the collimated beams of the reflected spectral channels and thereby facilitating the coupling of the spectral channels into the respective output ports according to desired coupling efficiencies. Each collimator-alignment mirror may be rotatable about one axis, or two axes.

[0053] The embodiment of FIG. 2A is attractive in applications where the fiber collimators (serving as the input and output ports) are desired to be placed in close proximity to the collimator-alignment mirror array 220. To best facilitate the coupling of the spectral channels into the output ports, arrays of imaging lenses may be implemented between the collimator-alignment mirror array 220 and the fiber collimator array 110, as depicted in FIG. 2B. By way of example, WSR apparatus 250 of FIG. 2B is built upon and hence shares many of the elements used in the embodiment of FIG. 2A, as identified by those labeled with identical numerals. Additionally, first and second arrays 260, 270 of imaging lenses are placed in a 4-f telecentric arrangement with respect to the collimator-alignment mirror array 220 and the fiber collimator array 110. The dashed box 280 shown in FIG. 2C provides a top view of such a telecentric

arrangement. In this case, the imaging lenses in the first and second arrays 260, 270 all have the same focal length f. The collimator-alignment mirrors 220-1 through 220-N are placed at the respective first (or front) focal points of the imaging lenses in the first array 260. Likewise, the fiber collimators 110-1 through 110-N are placed at the respective second (or back) focal points of the imaging lenses in the second array 270. And the separation between the first and second arrays 260, 270 of imaging lenses is 2f. In this way, the collimator-alignment mirrors 220-1 through 220-N are effectively imaged onto the respective entrance surfaces (i.e., the front focal planes) of the GRIN lenses in the corresponding fiber collimators 110-1 through 110-N. Such a telecentric imaging system substantially eliminates translational walk-off of the collimated beams at the output ports that may otherwise occur as the mirror angles change.

[0054] FIG. 3 shows a fourth embodiment of a WSR apparatus according to the present invention. By way of example, WSR apparatus 300 is built upon and hence shares a number of the elements used in the embodiment of FIG. 2B, as identified by those labeled with identical numerals. In this case, the one-dimensional fiber collimator array 110 of FIG. 2B is replaced by a two-dimensional array 350 of fiber collimators, providing for an input-port and a plurality of output ports. Accordingly, the one-dimensional collimatoralignment mirror array 220 of FIG. 2B is replaced by a two-dimensional array 320 of collimator-alignment mirrors, and first and second one-dimensional arrays 260, 270 of imaging lenses of FIG. 2B are likewise replaced by first and second two-dimensional arrays 360, 370 of imagining lenses respectively. As in the case of the embodiment of FIG. 2B, the first and second two-dimensional arrays 360, 370 of imaging lenses are placed in a 4-f telecentric arrangement with respect to the two-dimensional collimator-alignment mirror array 320 and the two-dimensional fiber collimator array 350. The channel micromirrors 103 must be pivotable biaxially in this case (in order to direct its corresponding spectral channel to any one of the output ports). As such, the WSR apparatus 300 is equipped to support a greater number of the output ports.

[0055] In addition to facilitating the coupling of the spectral channels into the respective output ports as described above, the collimator-alignment mirrors in the above embodiments also serve to compensate for misalignment (e.g., due to fabrication and assembly errors) in the fiber collimators that provide for the input and output ports. For instance, relative misalignment between the fiber cores and their respective collimating lenses in the fiber collimators can lead to pointing errors in the collimator-alignment mirrors. For these reasons, the collimator-alignment mirrors are preferably rotatable about two axes. They may be silicon micromachined mirrors, for fast rotational speeds. They may also be other types of mirrors or beam-deflecting elements known in the art.

**[0056]** To optimize the coupling of the spectral channels into the output ports and further maintain the optimal optical alignment against environmental effects such as temperature variations and mechanical instabilities over the course of operation, a WSR apparatus of the present invention may incorporate a servo-control assembly, for providing dynamic control of the coupling of the spectral channels into the respective output ports on a channel-by-channel basis. A WSR apparatus incorporating a servo-control assembly is termed a WSR-S apparatus, thereinafter in this specification.

[0057] FIG. 4A depicts a schematic illustration of a first embodiment of a WSR-S apparatus according to the present invention. The WSR-S apparatus 400 comprises a WSR apparatus 410 and a servo-control assembly 440. The WSR 410 may be in the embodiment of FIG. 1A, or any other embodiment in accordance with the present invention. The servo-control assembly 440 includes a spectral monitor 460, for monitoring the power levels of the spectral channels coupled into the output ports 420-1 through 420-N of the WSR apparatus 410. By way of example, the spectral monitor 460 is coupled to the output ports 420-1 through 420-N by way of fiber-optic couplers 420-1-C through 420-N-C, wherein each fiber-optic coupler Has: serves to tap off a predetermined fraction of the optical signal in the corresponding output port. The servo-control assembly 440 further includes a processing unit 470, in communication with the spectral monitor 460 and the channel micromirrors 430 of the WSR apparatus 410. The processing unit 470 uses the power measurements from the spectral monitor 460 to provide feedback control of the channel micromirrors 430 on an individual basis, so as to maintain a desired coupling efficiency for each spectral channel into a selected output port. As such, the servo-control assembly 440 provides dynamic control of the coupling of the spectral channels into the respective output ports on a channel-by-channel basis and thereby manages the power levels of the spectral channels coupled into the output ports. The power levels of the spectral channels in the output ports may be dynamically managed according to demand, or maintained at desired values (e.g., equalized at a predetermined value) in the present invention. Such a spectral power-management capability is essential in WDM optical networking applications, as discussed above.

[0058] FIG. 4B depicts a schematic illustration of a second embodiment of a WSR-S apparatus according to the present invention. The WSR-S apparatus 450 comprises a WSR apparatus 480 and a servo-control assembly 490. In addition to the channel micromirrors 430 (and other elements identified by the same numerals as those used in FIG. 4A), the WSR apparatus 480 further includes a plurality of collimator-alignment mirrors 485, and may be configured according to the embodiment of FIG. 2A, 2B, 3, or any other embodiment in accordance with the present invention. By way of example, the servo-control assembly 490 includes the spectral monitor 460 as described in the embodiment of FIG. 4A, and a processing unit 495. In this case, the processing unit 495 is in communication with the channel micromirrors 430 and the collimator-alignment mirrors 485 of the WSR apparatus 480, as well as the spectral monitor 460. The processing unit 495 uses the power measurements from the spectral monitor 460 to provide dynamic control of the channel micromirrors 430 along with the collimatoralignment mirrors 485, so to maintain the coupling efficiencies of the spectral channels into the output ports at desired values.

**[0059]** In the embodiment of **FIG. 4A** or **4B**, the spectral monitor **460** may be one of spectral power monitoring devices known in the art that is capable of detecting the power levels of spectral components in a multi-wavelength optical signal. Such devices are typically in the form of a wavelength-separating means (e.g., a diffraction grating)

that spatially separates a multi-wavelength optical signal by wavelength into constituent spectral components, and one or more optical sensors (e.g., an array of photodiodes) that are configured such to detect the power levels of these spectral components. The processing unit 470 in FIG. 4A (or the processing unit 495 in FIG. 4B) typically includes electrical circuits and signal processing programs for processing the power measurements received from the spectral monitor 460 and generating appropriate control signals to be applied to the channel micromirrors 430 (and the collimator-alignment mirrors 485 in the case of FIG. 4B), so to maintain the coupling efficiencies of the spectral channels into the output ports at desired values. The electronic circuitry and the associated signal processing algorithm/software for such processing unit in a servo-control system are known in the art. A skilled artisan will know how to implement a suitable spectral monitor along with an appropriate processing unit to provide a servo-control assembly in a WSP-S apparatus according to the present invention, for a given application.

**[0060]** The incorporation of a servo-control assembly provides additional advantages of effectively relaxing the requisite fabrication tolerances and the precision of optical alignment during initial assembly of a WSR apparatus of the present invention, and further enabling the system to correct for shift in the alignment over the course of operation. By maintaining an optimal optical alignment, the optical losses incurred by the spectral channels are also significantly reduced. As such, the WSR-S apparatus thus constructed is simpler and more adaptable in structure, more robust in performance, and lower in cost and optical loss. Accordingly, the WSR-S (or WSR) apparatus of the present invention may be used to construct a variety of optical devices and utilized in many applications.

[0061] For instance, by directing the spectral channels into the output ports in a one-channel-per-port fashion and coupling the output ports of a WSR-S (or WSR) apparatus to an array of optical sensors (e.g., photodiodes), or a single optical sensor that is capable of scanning across the output ports, a dynamic and versatile spectral power monitor (or channel analyzer) is provided, which would be highly desired in WDM optical networking applications. Moreover, a novel class of optical add-drop multiplexers (OADMs) may be built upon the WSR-S (or WSR) apparatus of the present invention, as exemplified in the following embodiments.

[0062] FIG. 5 depicts an exemplary embodiment of an optical add-drop multiplexer (OADM) according to the present invention. By way of example, OADM 500 comprises a WSR-S (or WSR) apparatus 510 and an optical combiner 550. An input port 520 of the WSR-S apparatus 510 transmits a multi-wavelength optical signal. The constituent spectral channels are subsequently separated and routed into a plurality of output ports, including a passthrough port 530 and one or more drop ports 540-1 through 540-N (N≥1). The pass-through port 530 may receive any number of the spectral channels (i.e., the pass-through spectral channels). Each drop port may also receive any number of the spectral channels (i.e., the drop spectral channels). The pass-through port 530 is optically coupled to the optical combiner 550, which serves to combine the pass-through spectral channels with one or more add spectral channels provided by one or more add ports 560-1

through 560-M (M $\ge$ 1). The combined optical signal is then routed into an existing port 570, providing an output multi-wavelength optical signal.

[0063] In the above embodiment, the optical combiner 550 may be a K×1 (K≥2) broadband fiber-optic coupler, wherein there are K input-ends and one output-end. The pass-through spectral channels and the add spectral channels are fed into the K input-ends (e.g., in a one-to-one correspondence) and the combined optical signal exits from the output-end of the K×1 fiber-optic coupler as the output multi-wavelength optical signal of the system. Such a multiple-input coupler also serves the purpose of multiplexing a multiplicity of add spectral channels to be coupled into the OADM 500. If the power levels of the spectral channels in the output multiwavelength optical signal are desired to be actively managed, such as being equalized at a predetermined value, two spectral monitors may be utilized. As a way of example, the first spectral monitor may receive optical signals tapped off from the pass-through port 530 and the drop ports 540-1 through 540-N (e.g., by way of fiber-optic couplers as depicted in FIG. 4A or 4B). The second spectral monitor receives optical signals tapped off from the exiting port 570. A servo-control system may be constructed accordingly for monitoring and controlling the pass-through, drop and add spectral channels. As such, the embodiment of FIG. 5 provides a versatile optical add-drop multiplexer in a simple and low-cost assembly, while providing multiple physically separate drop/add ports in a dynamically reconfigurable fashion.

[0064] FIG. 6 depicts an alternative embodiment of an optical add-drop multiplexer (OADM) according to the present invention. By way of example, OADM 600 comprises a first WSR-S apparatus 610 optically coupled to a second WSR-S apparatus 650. Each WSR-S apparatus may be in the embodiment of FIG. 4A or 4B. (AWSR apparatus of the embodiment of FIG. 1A, 2A, 2B, or 3 may be alternatively implemented.) The first WSR-S apparatus 610 includes an input port 620, a pass-through port 630, and one or more drop ports 640-1 through 640-N (N≥1). The pass-through spectral channels from the pass-through port 630 are further coupled to the second WSR-S apparatus 650, along with one or more add spectral channels emerging from add ports 660-1 through 660-M (M≥1). In this exemplary case, the pass-through port 630 and the add ports 660-1 through 660-M constitute the input ports for the second WSR-S apparatus 650. By way of its constituent wavelength-separator (e.g., a diffraction grating) and channel micromirrors (not shown in FIG. 6), the second WSR-S apparatus 650 serves to multiplex the pass-through spectral channels and the add spectral channels, and route the multiplexed optical signal into an exiting port 770 to provide an output signal of the system.

[0065] In the embodiment of FIG. 6, one WSR-S apparatus (e.g., the first WSR-S apparatus 610) effectively performs dynamic drop function, whereas the other WSR-S apparatus (e.g., the second WSR-S apparatus 650) carries out dynamic add function. And there are essentially no fundamental restrictions on the wavelengths that can be added or dropped (other than those imposed by the overall communication system). Moreover, the underlying OADM architecture thus presented is intrinsically scalable and can be readily extended to any number of cascaded WSR-S (or WSR) systems, if so desired for performing intricate add and **[0066]** Those skilled in the art will recognize that the aforementioned embodiments provide only two of many embodiments of a dynamically reconfigurable OADM according to the present invention. Those skilled in the art will also appreciate that various changes, substitutions, and alternations can be made herein without departing from the principles and the scope of the invention as defined in the appended claims. Accordingly, a skilled artisan can design invention, to best suit a given application.

**[0067]** Although the present invention and its advantages have been described in detail, it should be understood that various changes, substitutions, and alternations can be made herein without departing from the principles and the scope of the invention. Accordingly, the scope of the present invention should be determined by the following claims and their legal equivalents.

What is claimed is:

1. A wavelength-separating-routing apparatus, comprising:

- a) multiple fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots; and
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously controllable to reflect said spectral channels into selected ones of said output ports.

2. The wavelength-separating-routing apparatus of claim 1 further comprising a servo control assembly, in communication with said channel micromirrors and said output ports, for providing control of said channel micromirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

**3.** The wavelength-separating-routing apparatus of claim 2 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors.

**4**. The wavelength-separating-routing apparatus of claim 3 wherein said servo-control assembly maintains said power levels at a predetermined value.

5. The wavelength-separating-routing apparatus of claim 1 further comprising an array of collimator-alignment mirrors, in optical communication with said wavelength-separator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports. 6. The wavelength-separating-routing apparatus of claim 5 wherein each collimator-alignment mirror is rotatable about one axis.

7. The wavelength-separating-routing apparatus of claim 5 wherein each collimator-alignment mirror is rotatable about two axes.

**8**. The wavelength-separating-routing apparatus of claim 5 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimatoralignment mirrors and said fiber collimators.

 $\overline{9}$ . The wavelength-separating-routing apparatus of claim 1 wherein each channel micromirror is continuously pivotable about one axis.

10. The wavelength-separating-routing apparatus of claim 1 wherein each channel micromirror is pivotable about two axes.

11. The wavelength-separating-routing apparatus of claim 10 wherein said fiber collimators are arranged in a two-dimensional array.

12. The wavelength-separating-routing apparatus of claim 1 wherein each channel micromirror is a silicon micromachined mirror.

**13**. The wavelength-separating-routing apparatus of claim 1 wherein said fiber collimators are arranged in a one-dimensional array.

14. The wavelength-separating-routing apparatus of claim 1 wherein said beam-focuser comprises a focusing lens having first and second focal points.

15. The wavelength-separating-routing apparatus of claim 14 wherein said wavelength-separator and said channel micromirrors are placed respectively at said first and second focal points of said focusing lens.

16. The wavelength-separating-routing apparatus of claim 1 wherein said beam-focuser comprises an assembly of lenses.

17. The wavelength-separating-routing apparatus of claim 1 wherein said wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

18. The wavelength-separating-routing apparatus of claim 1 further comprising a quarter-wave plate optically interposed between said wavelength-separator and said channel micromirrors.

**19**. The wavelength-separating-routing apparatus of claim 1 wherein each output port carries a single one of said spectral channels.

**20**. The wavelength-separating-routing apparatus of claim 19 further comprising one or more optical sensors, optically coupled to said output ports.

21. A servo-based optical apparatus comprising:

- a) multiple fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being

individually controllable to reflect said spectral channels into selected ones of said output ports; and

e) a servo-control assembly, in communication with said channel micromirrors and said output ports, for maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

22. The servo-based optical apparatus of claim 21 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors.

**23**. The servo-based optical apparatus of claim 22 wherein said servo-control assembly maintains said power levels at a predetermined value.

24. The servo-based optical apparatus of claim 21 further comprising an array of collimator-alignment mirrors, in optical communication with said wavelength-separator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

**25**. The servo-based optical apparatus of claim 24 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

26. The servo-based optical apparatus of claim 24 wherein each collimator-alignment mirror is rotatable about at least one axis.

27. The servo-based optical apparatus of claim 21 wherein each channel micromirror is continuously pivotable about at least one axis.

28. The servo-based optical apparatus of claim 21 wherein each channel micromirror is a silicon micromachined mirror.

**29**. The servo-based optical apparatus of claim 21 wherein said wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

**30**. The servo-based optical apparatus of claim 21 wherein said beam-focuser comprises one or more lenses.

31. An optical apparatus comprising:

- a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually controllable to reflect said spectral channels into selected ones of said output ports; and
- e) a one-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.
  32. The optical apparatus of claim 31 further comprising a servo-control assembly, in communication with said chan-

nel micromirrors, said collimator-alignment mirrors, and said output ports, for providing control of said channel micromirrors along with said collimator-alignment mirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

**33.** The optical apparatus of claim 32 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors and said collimator-alignment mirrors.

**34**. The optical apparatus of claim 31 wherein each channel micromirror is continuously pivotable about at least one axis.

**35**. The optical apparatus of claim 31 wherein each collimator-alignment mirror is rotatable about at least one axis.

**36**. The optical apparatus of claim 31 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

37. An optical apparatus comprising:

- a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually controllable to reflect said spectral channels into selected ones of said output ports; and
- e) a two-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

**38**. The optical apparatus of claim 37 further comprising a servo-control assembly, in communication with said channel micromirrors, said collimator-alignment mirrors, and said output ports, for providing control of said channel micromirrors along with said collimator-alignment mirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

**39**. The optical apparatus of claim 38 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors and said collimator-alignment mirrors.

**40**. The optical apparatus of claim 37 wherein each collimator-alignment mirror is rotatable about at least one axis.

**41**. The optical apparatus of claim 37 wherein each channel micromirror is continuously pivotable about at least one axis.

42. The optical apparatus of claim 41 wherein each channel micromirrors is pivotable about two axes, and wherein said fiber collimators are arranged in a two-dimensional array.

**43**. The optical apparatus of claim 37 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

44. An optical system comprising a wavelength-separating-routing apparatus, wherein said wavelength-separatingrouting apparatus includes:

- a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports including a pass-through port and one or more drop ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots; and
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously pivotable to reflect said spectral channels into selected ones of said output ports, whereby said pass-through port receives a subset of said spectral channels.

**45**. The optical system of claim 44 further comprising a servo-control assembly, in communication with said channel micromirrors and said output ports, for providing control of said channel micromirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

**46**. The optical system of claim 45 wherein said servocontrol assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors.

**47**. The optical system of claim 44 further comprising an array of collimator-alignment mirrors, in optical communication with said wavelength-separator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

**48**. The optical system of claim 47 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

**49**. The optical system of claim 47 wherein each collimator-alignment mirror is rotatable about at least one axis.

**50**. The optical system of claim 44 wherein each channel micromirror is pivotable about at least one axis.

**51**. The optical system of claim 44 wherein each channel micromirror is a silicon micromachined mirror.

**52.** The optical system of claim 44 wherein said beamfocuser comprises a focusing lens having first and second focal points, and wherein said wavelength-separator and said channel micromirrors are placed respectively at said first and second focal points.

**53.** The optical system of claim 44 wherein said wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

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**54.** The optical system of claim 44 further comprising a quarter-wave plate optically interposed between said wavelength-separator and said channel micromirrors.

**55**. The optical system of claim 44 further comprising an auxiliary wavelength-separating-routing apparatus, including:

- a) multiple auxiliary fiber collimators, providing a plurality of auxiliary input ports and an exiting port;
- b) an auxiliary wavelength-separator;
- c) an auxiliary beam-focuser; and
- d) a spatial array of auxiliary channel micromirrors;
- wherein said subset of said spectral channels in said pass-through port and one or more add spectral channels are directed into said auxiliary input ports, and multiplexed into an output optical signal directed into said exiting port by way of said auxiliary wavelengthseparator, said auxiliary beam-focuser and said auxiliary channel micromirrors.

**56**. The optical system of claim 55 wherein said auxiliary channel micromirrors are individually pivotable.

**57**. The optical system of claim 55 wherein each auxiliary channel micromirror is pivotable continuously about at least one axis.

**58**. The optical system of claim 55 wherein each auxiliary channel micromirror is a silicon micromachined mirror.

**59**. The optical system of claim 55 wherein said auxiliary wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

**60**. The optical system of claim 55 wherein said passthrough port constitutes one of said auxiliary input ports.

**61**. A method of performing dynamic wavelength separating and routing, comprising:

- a) receiving a multi-wavelength optical signal from an input port;
- b) separating said multi-wavelength optical signal into multiple spectral channels;
- c) focusing said spectral channels onto a spatial array of corresponding beam-deflecting elements, whereby each beam-deflecting element receives one of said spectral channels; and
- d) dynamically and continuously controlling said beamdeflecting elements, thereby directing said spectral channels into a plurality of output ports.

**62**. The method of claim 61 further comprising the step of providing feedback control of said beam-deflecting elements, thereby maintaining a predetermining coupling of each spectral channel directed into one of said output ports.

**63**. The method of claim 62 further comprising the step of maintaining power levels of said spectral channels directed into said output ports at a predetermining value.

**64**. The method of claim 61 wherein each spectral channel is directed into a separate output port.

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**65**. The method of claim 61 wherein a subset of said spectral channels is directed into one of said output ports, thereby providing one or more pass-through spectral channels.

66. The method of claim 65 further comprising the step of multiplexing said pass-through spectral channels with one or

more add spectral channels, so as to provide an output optical signal.

67. The method of claim 61 wherein said beam-deflecting elements comprise an array of silicon micromachined mirrors.

\* \* \* \* \*



US006625346B2

# (12) United States Patent Wilde

# (54) RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES

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- (\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.
- (21) Appl. No.: 09/938,426
- (22) Filed: Aug. 23, 2001

### (65) Prior Publication Data

US 2002/0131687 A1 Sep. 19, 2002

### Related U.S. Application Data

- (60) Provisional application No. 60/277,217, filed on Mar. 19, 2001.
- (51) Int. Cl.<sup>7</sup> ...... G02B 6/28

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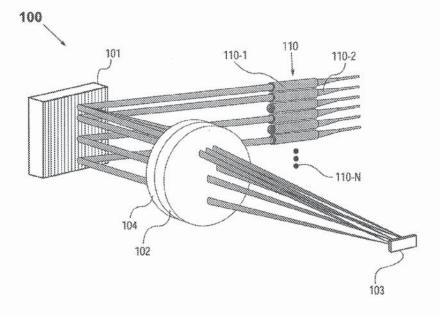
Primary Examiner-Brian Healy

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### (57) ABSTRACT

This invention provides a novel wavelength-separatingrouting (WSR) apparatus that uses a diffraction grating to separate a multi-wavelength optical signal by wavelength into multiple spectral channels, which are then focused onto an array of corresponding channel micromirrors. The channel micromirrors are individually controllable and continuously pivotable to reflect the spectral channels into selected output ports. As such, the inventive WSR apparatus is capable of routing the spectral channels on a channel-bychannel basis and coupling any spectral channel into any one of the output ports. The WSR apparatus of the present invention may be further equipped with servo-control and spectral power-management capabilities, thereby maintaining the coupling efficiencies of the spectral channels into the output ports at desired values. The WSR apparatus of the present invention can be used to construct a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs) for WDM optical networking applications.

### 67 Claims, 12 Drawing Sheets



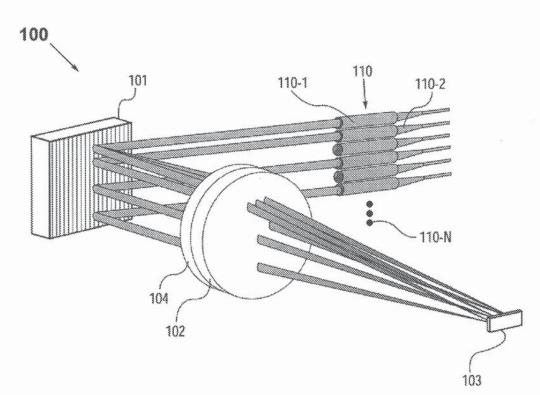
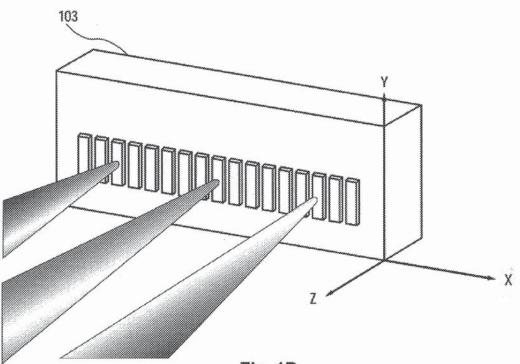
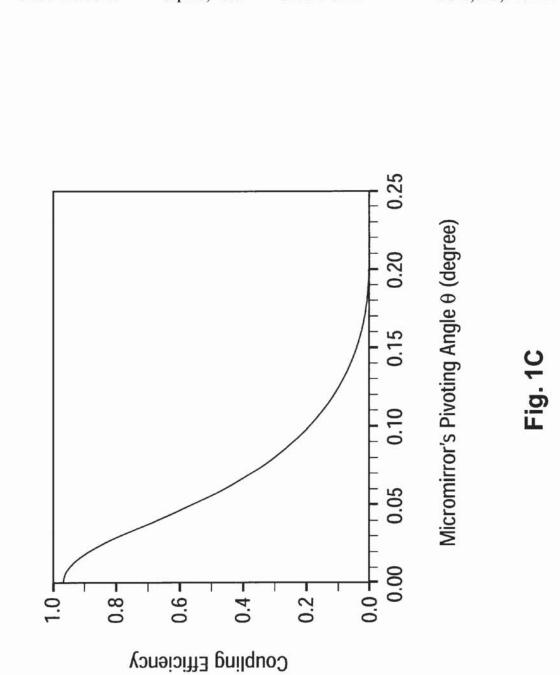


Fig. 1A







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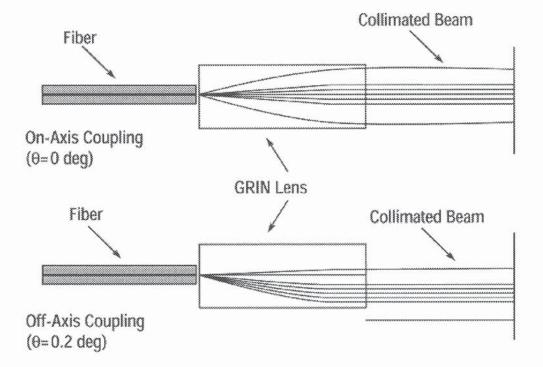


Fig. 1D

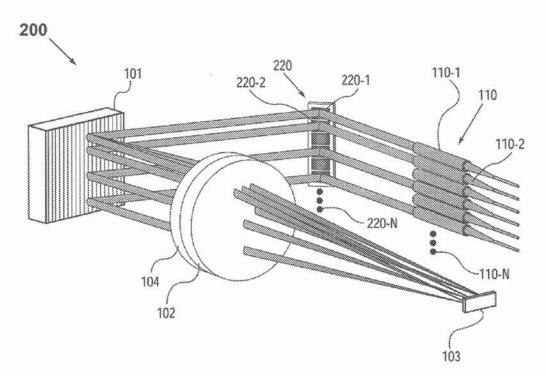


Fig. 2A

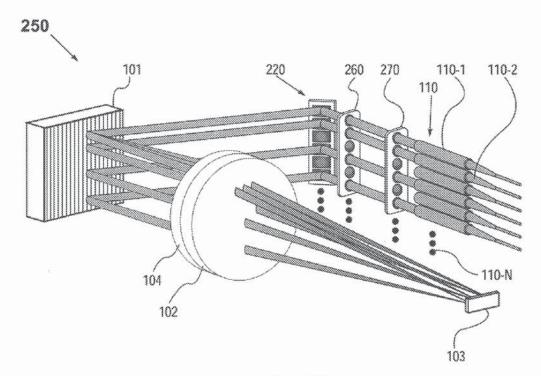


Fig. 2B



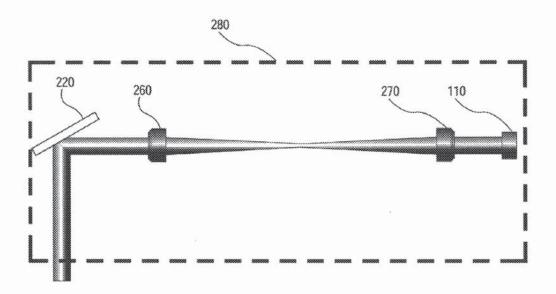


Fig. 2C

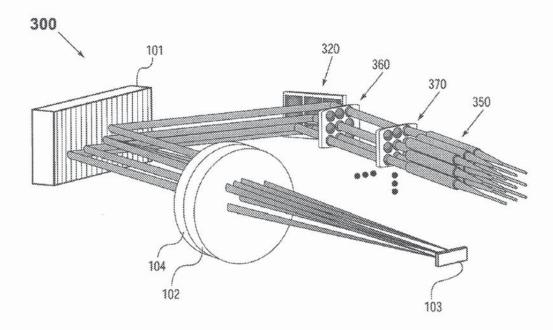


Fig. 3

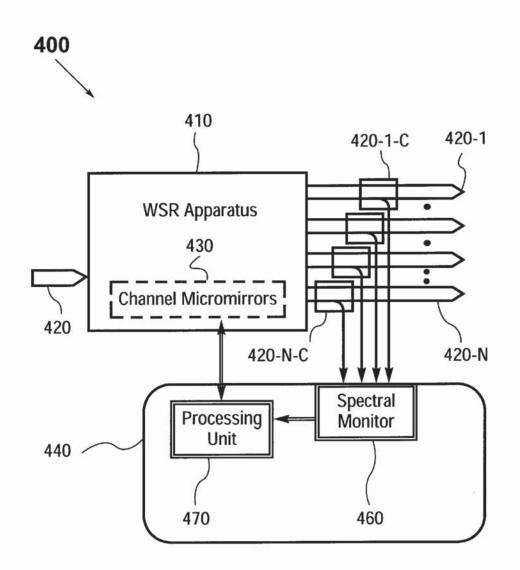


Fig. 4A

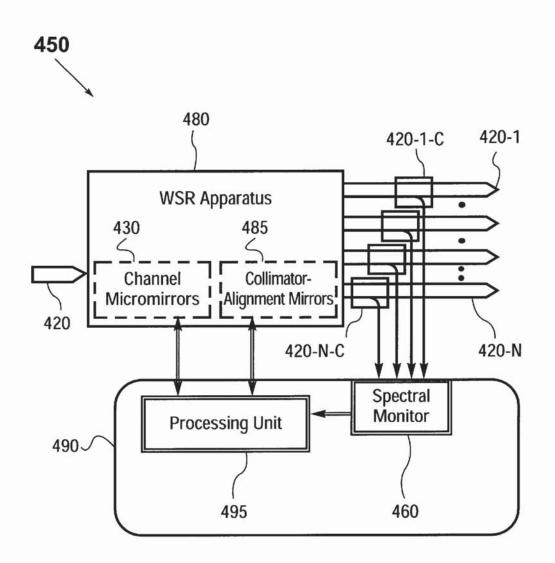
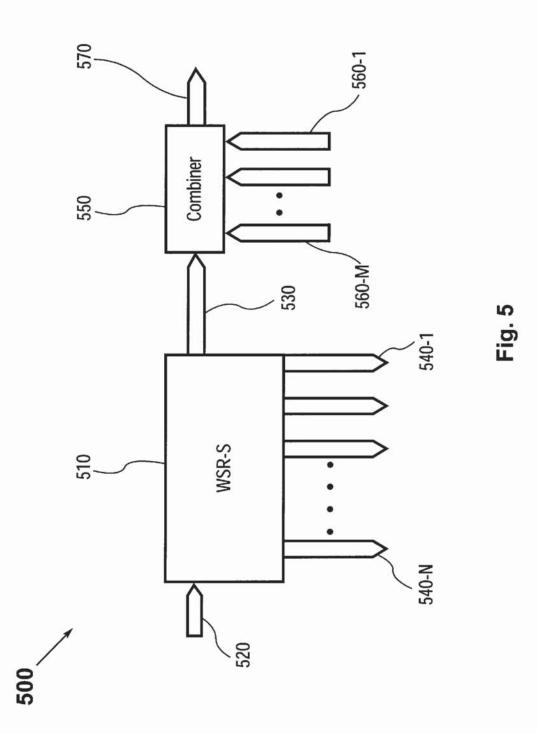
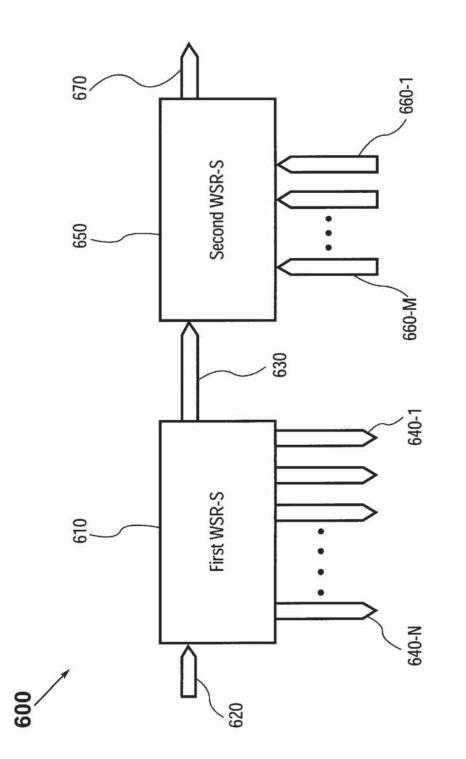


Fig. 4B







# RECONFIGURABLE OPTICAL ADD-DROP MULTIPLEXERS WITH SERVO CONTROL AND DYNAMIC SPECTRAL POWER MANAGEMENT CAPABILITIES

## CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims priority of U.S. Provisional Patent Application No. 60/277,217, filed Mar. 19, 2001 which is 10 incorporated herein by reference.

## FIELD OF THE INVENTION

This invention relates generally to optical communication systems. More specifically, it relates to a novel class of <sup>15</sup> dynamically reconfigurable optical add-drop multiplexers (OADMs) for wavelength division multiplexed optical networking applications.

### BACKGROUND

As fiber-optic communication networks rapidly spread into every walk of modern life, there is a growing demand for optical components and subsystems that enable the fiber-optic communications networks to be increasingly scalable, versatile, robust, and cost-effective.

Contemporary fiber-optic communications networks commonly employ wavelength division multiplexing (WDM), for it allows multiple information (or data) channels to be simultaneously transmitted on a single optical 30 fiber by using different wavelengths and thereby significantly enhances the information bandwidth of the fiber. The prevalence of WDM technology has made optical add-drop multiplexers indispensable building blocks of modern fiberoptic communication networks. An optical add-drop multiplexer (OADM) serves to selectively remove (or drop) one or more wavelengths from a multiplicity of wavelengths on an optical fiber, hence taking away one or more data channels from the traffic stream on the fiber. It further adds one or more wavelengths back onto the fiber, thereby 40 inserting new data channels in the same stream of traffic. As such, an OADM makes it possible to launch and retrieve multiple data channels (each characterized by a distinct wavelength) onto and from an optical fiber respectively, without disrupting the overall traffic flow along the fiber. 45 Indeed, careful placement of the OADMs can dramatically improve an optical communication network's flexibility and robustness, while providing significant cost advantages.

Conventional OADMs in the art typically employ multiplexers/demultiplexers (e.g, waveguide grating routers 50 or arrayed-waveguide gratings), tunable filters, optical switches, and optical circulators in a parallel or serial architecture to accomplish the add and drop functions. In the parallel architecture, as exemplified in U.S. Pat. No. 5,974, 207, a demultiplexer (e.g., a waveguide grating router) first 55 separates a multi-wavelength signal into its constituent spectral components. A wavelength switching/routing means (e.g., a combination of optical switches and optical circulators) then serves to drop selective wavelengths and add others. Finally, a multiplexer combines the remaining (i.e., the pass-through) wavelengths into an output multiwavelength optical signal. In the serial architecture, as exemplified in U.S. Pat. No. 6,205,269, tunable filters (e.g., Bragg fiber gratings) in combination with optical circulators are used to separate the drop wavelengths from the pass- 65 through wavelengths and subsequently launch the add channels into the pass-through path. And if multiple wavelengths

are to be added and dropped, additional multiplexers and demultiplexers are required to demultiplex the drop wavelengths and multiplex the add wavelengths, respectively. Irrespective of the underlying architecture, the OADMs currently in the art are characteristically high in cost, and prone to significant optical loss accumulation. Moreover, the designs of these OADMs are such that it is inherently difficult to reconfigure them in a dynamic fashion.

U.S. Pat. No. 6,204,946 to Askyuk et al. discloses an OADM that makes use of free-space optics in a parallel construction. In this case, a multi-wavelength optical signal emerging from an input port is incident onto a ruled diffraction grating. The constituent spectral channels thus separated are then focused by a focusing lens onto a linear array of binary micromachined mirrors. Each micromirror is configured to operate between two discrete states, such that it either retroreflects its corresponding spectral channel back into the input port as a pass-through channel, or directs its spectral channel to an output port as a drop channel. As such, the pass-through signal (i.e., the combined pass-through channels) shares the same input port as the input signal. An optical circulator is therefore coupled to the input port, to provide necessary routing of these two signals. Likewise, the drop channels share the output port with the add channels. An additional optical circulator is thereby coupled to the output port, from which the drop channels exit and the add channels are introduced into the output port. The add channels are subsequently combined with the pass-through signal by way of the diffraction grating and the binary micromirrors

Although the aforementioned OADM disclosed by Askyuk et al. has the advantage of performing wavelength separating and routing in free space and thereby incurring less optical loss, it suffers a number of limitations. First, it requires that the pass-through signal share the same port/ fiber as the input signal. An optical circulator therefore has to be implemented, to provide necessary routing of these two signals. Likewise, all the add and drop channels enter and leave the OADM through the same output port, hence the need for another optical circulator. Moreover, additional means must be provided to multiplex the add channels before entering the system and to demultiplex the drop channels after exiting the system. This additional multiplexing/demultiplexing requirement adds more cost and complexity that can restrict the versatility of the OADM thus-constructed. Second, the optical circulators implemented in this OADM for various routing purposes introduce additional optical losses, which can accumulate to a substantial amount. Third, the constituent optical components must be in a precise alignment, in order for the system to achieve its intended purpose. There are, however, no provisions provided for maintaining the requisite alignment; and no mechanisms implemented for overcoming degradation in the alignment owing to environmental effects such as thermal and mechanical disturbances over the course of operation.

U.S. Pat. No. 5,906,133 to Tomlinson discloses an OADM that makes use of a design similar to that of Aksyuk et al. There are input, output, drop and add ports implemented in this case. By positioning the four ports in a specific arrangement, each micromirror, notwithstanding switchable between two discrete positions, either reflects its corresponding channel (coming from the input port) to the output port, or concomitantly reflects its channel to the drop port and an incident add channel to the output port. As such, this OADM is able to perform both the add and drop functions without involving additional optical components

(such as optical circulators used in the system of Aksyuk et al.). However, because a single drop port is designated for all the drop channels and a single add port is designated for all the add channels, the add channels would have to be multiplexed before entering the add port and the drop 5 channels likewise need to be demutiplxed upon exiting from the drop port. Moreover, as in the case of Askyuk et al., there are no provisions provided for maintaining requisite optical alignment in the system, and no mechanisms implemented for combating degradation in the alignment due to environ-10 mental effects over the course of operation.

As such, the prevailing drawbacks suffered by the OADMs currently in the art are summarized as follows:

- The wavelength routing is intrinsically static, rendering it <sup>15</sup> difficult to dynamically reconfigure these OADMs.
- Add and/or drop channels often need to be multiplexed and/or demultiplexed, thereby imposing additional complexity and cost.
- 3) Stringent fabrication tolerance and painstaking optical <sup>20</sup> alignment are required. Moreover, the optical alignment is not actively maintained, rendering it susceptible to environmental effects such as thermal and mechanical disturbances over the course of operation.
- 4) In an optical communication network, OADMs are typi-<sup>25</sup> cally in a ring or cascaded configuration. In order to mitigate the interference amongst OADMs, which often adversely affects the overall performance of the network, it is essential that the power levels of spectral channels entering and exiting each OADM be managed in a systematic way, for instance, by introducing power (or gain) equalization at each stage. Such a power equalization capability is also needed for compensating for nonuniform gain caused by optical amplifiers (e.g., erbium doped fiber amplifiers) in the network. There lacks, <sup>35</sup> however, a systematic and dynamic management of the power levels of various spectral channels in these OADMs.
- 5) The inherent high cost and heavy optical loss further impede the wide application of these OADMs.

In view of the foregoing, there is an urgent need in the art for optical add-drop multiplexers that overcome the aforementioned shortcomings in a simple, effective, and economical construction.

#### SUMMARY

The present invention provides a wavelength-separatingrouting (WSR) apparatus and method which employ an array of fiber collimators serving as an input port and a 50 plurality of output ports; a wavelength-separator; a beamfocuser; and an array of channel micromirrors.

In operation, a multi-wavelength optical signal emerges from the input port. The wavelength-separator separates the multi-wavelength optical signal into multiple spectral 55 channels, each characterized by a distinct center wavelength and associated bandwidth. The beam-focuser focuses the spectral channels into corresponding spectral spots. The channel micromirrors are positioned such that each channel micromirror receives one of the spectral channels. The 60 channel micromirrors are individually controllable and movable, e.g., continuously pivotable (or rotatable), so as to reflect the spectral channels into selected ones of the output ports. As such, each channel micromirror is assigned to a specific spectral channel, hence the name "channel micromirror". And each output port may receive any number of the reflected spectral channels.

A distinct feature of the channel micromirrors in the present invention, in contrast to those used in the prior art, is that the motion, e.g., pivoting (or rotation), of each channel micromirror is under analog control such that its pivoting angle can be continuously adjusted. This enables each channel micromirror to scan its corresponding spectral channel across all possible output ports and thereby direct the spectral channel to any desired output port.

In the WSR apparatus of the present invention, the wavelength-separator may be provided by a ruled diffraction grating, a holographic diffraction grating, an echelle grating, a curved diffraction grating, a dispersing prism, or other wavelength-separating means known in the art. The beam-focuser may be a single lens, an assembly of lenses, or other beam-focusing means known in the art. The channel micro-mirrors may be provided by silicon micromachined mirrors, reflective ribbons (or membranes), or other types of beam-deflecting means known in the art. And each channel micro-mirror may be pivotable about one or two axes. The fiber collimators serving as the input and output ports may be arranged in a one-dimensional or two-dimensional array. In the latter case, the channel micromirrors must be pivotable biaxially.

The WSR apparatus of the present invention may further comprise an array of collimator-alignment mirrors, in optical communication with the wavelength-separator and the fiber collimators, for adjusting the alignment of the input multi-wavelength signal and directing the spectral channels into the selected output ports by way of angular control of the collimated beams. Each collimator-alignment mirror may be rotatable about one or two axes. The collimatoralignment mirrors may be arranged in a one-dimensional or two-dimensional array. First and second arrays of imaging lenses may additionally be optically interposed between the collimator-alignment mirrors and the fiber collimators in a telecentric arrangement, thereby "imaging" the collimatoralignment mirrors onto the corresponding fiber collimators to ensure an optimal alignment.

The WSR apparatus of the present invention may further include a servo-control assembly, in communication with 40 the channel micromirrors and the output ports. The servocontrol assembly serves to monitor the power levels of the spectral channels coupled into the output ports and further provide control of the channel micromirrors on an individual basis, so as to maintain a predetermined coupling efficiency 45 of each spectral channel in one of the output ports. As such, the servo-control assembly provides dynamic control of the coupling of the spectral channels into the respective output ports and actively manages the power levels of the spectral channels coupled into the output ports. (If the WSR apparatus includes an array of collimator-alignment mirrors as described above, the servo-control assembly may additionally provide dynamic control of the collimator-alignment mirrors.) Moreover, the utilization of such a servo-control assembly effectively relaxes the requisite fabrication tolerances and the precision of optical alignment during assembly of a WSR apparatus of the present invention, and further enables the system to correct for shift in optical alignment over the course of operation. A WSR apparatus incorporating a servo-control assembly thus described is termed a WSR-S apparatus, thereinafter in the present invention.

Accordingly, the WSR-S (or WSR) apparatus of the present invention may be used to construct a variety of optical devices, including a novel class of dynamically reconfigurable optical add-drop multiplexers (OADMs), as exemplified in the following embodiments.

One embodiment of an OADM of the present invention comprises an aforementioned WSR-S (or WSR) apparatus and an optical combiner. The output ports of the WSR-S apparatus include a pass-through port and one or more drop ports, each carrying any number of the spectral channels. The optical combiner is coupled to the pass-through port, serving to combine the pass-through channels with one or more add spectral channels. The combined optical signal constitutes an output signal of the system. The optical combiner may be an N×1 (N≥2) broadband fiber-optic coupler, for instance, which also serves the purpose of multiplexing a multiplicity of add spectral channels to be 10 coupled into the system.

In another embodiment of an OADM of the present invention, a first WSR-S (or WSR) apparatus is cascaded with a second WSR-S (or WSR) apparatus. The output ports of the first WSR-S (or WSR) apparatus include a pass-15 through port and one or more drop ports. The second WSR-S (or WSR) apparatus includes a plurality of input ports and an exiting port. The configuration is such that the pass-through channels from the first WSR-S apparatus and one or more add channels are directed into the input ports of the second 20 WSR-S apparatus, and consequently multiplexed into an output multi-wavelength optical signal directed into the exiting port of the second WSR-S apparatus. That is to say that in this embodiment, one WSR-S apparatus (e.g., the first one) effectively performs a dynamic drop function, whereas 25 the other WSR-S apparatus (e.g., the second one) carries out a dynamic add function. And there are essentially no fundamental restrictions on the wavelengths that can be added or dropped, other than those imposed by the overall communication system. Moreover, the underlying OADM archi-30 tecture thus presented is intrinsically scalable and can be readily extended to any number of the WSR-S (or WSR) systems, if so desired for performing intricate add and drop functions in a network environment.

Those skilled in the art will recognize that the aforemen- 35 tioned embodiments provide only two of many embodiments of a dynamically reconfigurable OADM according to the present invention. Various changes, substitutions, and alternations can be made herein, without departing from the principles and the scope of the invention. Accordingly, a 40 skilled artisan can design an OADM in accordance with the present invention, to best suit a given application.

All in all, the OADMs of the present invention provide many advantages over the prior art devices, notably:

- 1) By advantageously employing an array of channel micromirrors that are individually and continuously controllable, an OADM of the present invention is capable of routing the spectral channels on a channel-byone of the output ports. As such, its underlying operation is dynamically reconfigurable, and its underlying architecture is intrinsically scalable to a large number of channel counts.
- 2) The add and drop spectral channels need not be multi- 55 plexed and demultiplexed before entering and after leaving the OADM respectively. And there are not fundamental restrictions on the wavelengths to be added or dropped.
- 3) The coupling of the spectral channels into the output ports is dynamically controlled by a servo-control assembly, rendering the OADM less susceptible to environmental effects (such as thermal and mechanical disturbances) and therefore more robust in performance. By maintaining an optimal optical alignment, the optical losses incurred by the spectral channels are also significantly reduced.
- 4) The power levels of the spectral channels coupled into the output ports can be dynamically managed according to

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demand, or maintained at desired values (e.g., equalized at a predetermined value) by way of the servo-control assembly. This spectral power-management capability as an integral part of the OADM will be particularly desirable in WDM optical networking applications.

- 5) The use of free-space optics provides a simple, low loss, and cost-effective construction. Moreover, the utilization of the servo-control assembly effectively relaxes the requisite fabrication tolerances and the precision of optical alignment during initial assembly, enabling the OADM to be simpler and more adaptable in structure, lower in cost and optical loss.
- 6) The underlying OADM architecture allows a multiplicity of the OADMs according to the present invention to be readily assembled (e.g., cascaded) for WDM optical networking applications.

The novel features of this invention, as well as the invention itself, will be best understood from the following drawings and detailed description.

## BRIEF DESCRIPTION OF THE FIGURES

FIGS. 1A-1D show a first embodiment of a wavelengthseparating-routing (WSR) apparatus according to the present invention, and the modeling results demonstrating the performance of the WSR apparatus;

FIGS. 2A-2C depict second and third embodiments of a WSR apparatus according to the present invention;

FIG. 3 shows a fourth embodiment of a WSR apparatus according to the present invention;

FIGS. 4A-4B show schematic illustrations of two embodiments of a WSR-S apparatus comprising a WSR apparatus and a servo-control assembly, according to the present invention;

FIG. 5 depicts an exemplary embodiment of an optical add-drop multiplexer (OADM) according to the present invention; and

FIG. 6 shows an alternative embodiment of an OADM according to the present invention.

# DETAILED DESCRIPTION

In this specification and appending claims, a "spectral channel" is characterized by a distinct center wavelength 45 and associated bandwidth. Each spectral channel may carry a unique information signal, as in WDM optical networking applications.

FIG. 1A depicts a first embodiment of a wavelengthchannel basis and directing any spectral channel into any 50 separating-routing (WSR) apparatus according to the present invention. By way of example to illustrate the general principles and the topological structure of a wavelength-separating-routing (WSR) apparatus of the present invention, the WSR apparatus 100 comprises multiple input/output ports which may be in the form of an array of fiber collimators 110, providing an input port 110-1 and a plurality of output ports 110-2 through 110-N (N $\geq$ 3); a wavelength-separator which in one form may be a diffraction grating 101; a beam-focuser in the form of a focusing lens 102; and an array of channel micromirrors 103.

> In operation, a multi-wavelength optical signal emerges from the input port 110-1. The diffraction grating 101 angularly separates the multi-wavelength optical signal into multiple spectral channels, which are in turn focused by the focusing lens 102 into a spatial array of distinct spectral spots (not shown in FIG. 1A) in a one-to-one correspondence. The channel micromirrors 103 are positioned in

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accordance with the spatial array formed by the spectral spots, such that each channel micromirror receives one of the spectral channels. The channel micromirrors **103** are individually controllable and movable, e.g., pivotable (or rotatable) under analog (or continuous) control, such that, upon reflection, the spectral channels are directed into selected ones of the output ports **110-2** through **110-N** by way of the focusing lens **102** and the diffraction grating **101**. As such, each channel micromirror is assigned to a specific spectral channel, hence the name "channel micromirror". <sup>10</sup> Each output port may receive any number of the reflected spectral channels.

For purposes of illustration and clarity, only a selective few (e.g., three) of the spectral channels, along with the input multi-wavelength optical signal, are graphically illus- 15 trated in FIG. 1A and the following figures. It should be noted, however, that there can be any number of the spectral channels in a WSR apparatus of the present invention (so long as the number of spectral channels does not exceed the number of channel mirrors employed in the system). It 20 should also be noted that the optical beams representing the spectral channels shown in FIG. 1A and the following figures are provided for illustrative purpose only. That is, their sizes and shapes may not be drawn according to scale. For instance, the input beam and the corresponding dif-25 fracted beams generally have different cross-sectional shapes, so long as the angle of incidence upon the diffraction grating is not equal to the angle of diffraction, as is known to those skilled in the art.

In the embodiment of FIG. 1A, it is preferable that the 30 diffraction grating 101 and the channel micromirrors 103 are placed respectively at the first and second (i.e., the front and back) focal points (on the opposing sides) of the focusing lens 102. Such a telecentric arrangement allows the chief rays of the focused beams to be parallel to each other and 35 generally parallel to the optical axis. In this application, the telecentric configuration further allows the reflected spectral channels to be efficiently coupled into the respective output ports, thereby minimizing various translational walk-off effects that may otherwise arise. Moreover, the input multiwavelength optical signal is preferably collimated and circular in cross-section. The corresponding spectral channels diffracted from the diffraction grating 101 are generally elliptical in cross-section; they may be of the same size as the input beam in one dimension and elongated in the other 45 dimension.

It is known that the diffraction efficiency of a diffraction grating is generally polarization-dependent. That is, the diffraction efficiency of a grating in a standard mounting configuration may be considerably higher for P-polarization that is perpendicular to the groove lines on the grating than for S-polarization that is orthogonal to P-polarization, especially as the number of groove lines (per unit length) increases. To mitigate such polarization-sensitive effects, a quarter-wave plate 104 may be optically interposed between 55 the diffraction grating 101 and the channel micromirrors 103, and preferably placed between the diffraction grating 101 and the focusing lens 102 as is shown in FIG. 1A. In this way, each spectral channel experiences a total of approximately 90-degree rotation in polarization upon traversing the quarter-wave plate 104 twice. (That is, if a beam of light has P-polarization when first encountering the diffraction grating, it would have predominantly (if not all) S-polarization upon the second encountering, and vice versa.) This ensures that all the spectral channels incur 65 nearly the same amount of round-trip polarization dependent loss

In the WSR apparatus **100** of FIG. **1**A, the diffraction grating **101**, by way of example, is oriented such that the focused spots of the spectral channels fall onto the channel micromirrors **103** in a horizontal array, as illustrated in FIG. **1B**.

Depicted in FIG. 1B is a close-up view of the channel micromirrors 103 shown in the embodiment of FIG. 1A. By way of example, the channel micromirrors 103 are arranged in a one-dimensional array along the x-axis (i.e., the horizontal direction in the figure), so as to receive the focused spots of the spatially separated spectral channels in a oneto-one correspondence. (As in the case of FIG. 1A, only three spectral channels are illustrated, each represented by a converging beam.) Let the reflective surface of each channel micromirror lie in the x-y plane as defined in the figure and be movable, e.g., pivotable (or deflectable) about the x-axis in an analog (or continuous) manner. Each spectral channel, upon reflection, is deflected in the y-direction (e.g., downward) relative to its incident direction, so to be directed into one of the output ports 110-2 through 110-N shown in FIG. 1A.

As described above, a unique feature of the present invention is that the motion of each channel micromirror is individually and continuously controllable, such that its position, e.g., pivoting angle, can be continuously adjusted. This enables each channel micromirror to scan its corresponding spectral channel across all possible output ports and thereby direct the spectral channel to any desired output port. To illustrate this capability, FIG. 1C shows a plot of coupling efficiency as a function of a channel micromirror's pivoting angle  $\theta$ , provided by a ray-tracing model of a WSR apparatus in the embodiment of FIG. 1A. As used herein, the coupling efficiency for a spectral channel is defined as the ratio of the amount of optical power coupled into the fiber core in an output port to the total amount of optical power incident upon the entrance surface of the fiber (associated with the fiber collimator serving as the output port). In the ray-tracing model, the input optical signal is incident upon a diffraction grating with 700 lines per millimeter at a grazing angle of 85 degrees, where the grating is blazed to optimize the diffraction efficiency for the "-1" order. The focusing lens has a focal length of 100 mm. Each output port is provided by a quarter-pitch GRIN lens (2 mm in diameter) coupled to an optical fiber (see FIG. 1D). As displayed in FIG. 1C, the coupling efficiency varies with the pivoting angle  $\theta$ , and it requires about a 0.2-degree change in  $\theta$  for the coupling efficiency to become practically negligible in this exemplary case. As such, each spectral channel may practically acquire any coupling efficiency value by way of controlling the pivoting angle of its corresponding channel micromirror. This is also to say that variable optical attenuation at the granularity of a single wavelength can be obtained in a WSR apparatus of the present invention. FIG. 1D provides ray-tracing illustrations of two extreme points on the coupling efficiency vs.  $\theta$  curve of FIG. 1C: on-axis coupling corresponding to  $\theta=0$ , where the coupling efficiency is maximum; and off-axis coupling corresponding to  $\theta$ =0.2 degrees, where the representative collimated beam (representing an exemplary spectral channel) undergoes a significant translational walk-off and renders the coupling efficiency practically negligible. All in all, the exemplary modeling results thus described demonstrate the unique capabilities of the WSR apparatus of the present invention.

FIG. 1A provides one of many embodiments of a WSR apparatus according to the present invention. In general, the wavelength-separator is a wavelength-separating means that may be a ruled diffraction grating, a holographic diffraction

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grating, an echelle grating, a dispersing prism, or other types of spectral-separating means known in the art. The beamfocuser may be a focusing lens, an assembly of lenses, or other beam-focusing means known in the art. The focusing function may also be accomplished by using a curved diffraction grating as the wavelength-separator. The channel micromirrors may be provided by silicon micromachined mirrors, reflective ribbons (or membranes), or other types of beam-deflecting elements known in the art. And each micromirror may be pivoted about one or two axes. What is important is that the pivoting (or rotational) motion of each channel micromirror be individually controllable in an analog manner, whereby the pivoting angle can be continuously adjusted so as to enable the channel micromirror to scan a spectral channel across all possible output ports. The underlying fabrication techniques for micromachined mirrors and associated actuation mechanisms are well documented in the art, see U.S. Pat. No. 5,629,790 for example. Moreover, a fiber collimator is typically in the form of a collimating lens (such as a GRIN lens) and a ferrule-mounted fiber packaged together in a mechanically rigid stainless steel (or glass) tube. The fiber collimators serving as the input and output ports may be arranged in a one-dimensional array, a twodimensional array, or other desired spatial pattern. For instance, they may be conveniently mounted in a linear array along a V-groove fabricated on a substrate made of silicon, plastic, or ceramic, as commonly practiced in the art. It should be noted, however, that the input port and the output ports need not necessarily be in close spatial proximity with each other, such as in an array configuration (although a 30 close packing would reduce the rotational range required for each channel micromirror). Those skilled in the art will know how to design a WSR apparatus according to the present invention, to best suit a given application.

A WSR apparatus of the present invention may further 35 comprise an array of collimator-alignment mirrors, for adjusting the alignment of the input multi-wavelength optical signal and facilitating the coupling of the spectral channels into the respective output ports, as shown in FIGS. 2A-2B and 3.

Depicted in FIG. 2A is a second embodiment of a WSR apparatus according to the present invention. By way of example, WSR apparatus 200 is built upon and hence shares a number of the elements used in the embodiment of FIG. 1A, as identified by those labeled with identical numerals. 45 Moreover, a one-dimensional array 220 of collimatoralignment mirrors 220-1 through 220-N is optically interposed between the diffraction grating 101 and the fiber collimator array 110. The collimator-alignment mirror 220-1 is designated to correspond with the input port 110-1, for 50 adjusting the alignment of the input multi-wavelength optical signal and therefore ensuring that the spectral channels impinge onto the corresponding channel micromirrors. The collimator-alignment mirrors 220-2 through 220-N are designated to the output ports 110-2 through 110-N in a oneto-one correspondence, serving to provide angular control of the collimated beams of the reflected spectral channels and thereby facilitating the coupling of the spectral channels into the respective output ports according to desired coupling efficiencies. Each collimator-alignment mirror may be rotat- 60 able about one axis, or two axes.

The embodiment of FIG. 2A is attractive in applications where the fiber collimators (serving as the input and output ports) are desired to be placed in close proximity to the collimator-alignment mirror array 220. To best facilitate the 65 coupling of the spectral channels into the output ports, arrays of imaging lenses may be implemented between the

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collimator-alignment mirror array 220 and the fiber collimator array 110, as depicted in FIG. 2B. By way of example, WSR apparatus 250 of FIG. 2B is built upon and hence shares many of the elements used in the embodiment of FIG. 2A, as identified by those labeled with identical numerals. Additionally, first and second arrays 260, 270 of imaging lenses are placed in a 4-f telecentric arrangement with respect to the collimator-alignment mirror array 220 and the fiber collimator array 110. The dashed box 280 shown in FIG. 2C provides a top view of such a telecentric arrangement. In this case, the imaging lenses in the first and second arrays 260, 270 all have the same focal length f. The collimator-alignment mirrors 220-1 through 220-N are placed at the respective first (or front) focal points of the imaging lenses in the first array 260. Likewise, the fiber collimators 110-1 through 110-N are placed at the respective second (or back) focal points of the imaging lenses in the second array 270. And the separation between the first and second arrays 260, 270 of imaging lenses is 2f. In this way, the collimator-alignment mirrors 220-1 through 220-N are effectively imaged onto the respective entrance surfaces (i.e., the front focal planes) of the GRIN lenses in the corresponding fiber collimators 110-1 through 110-N. Such a telecentric imaging system substantially eliminates translational walk-off of the collimated beams at the output ports that may otherwise occur as the mirror angles change.

FIG. 3 shows a fourth embodiment of a WSR apparatus according to the present invention. By way of example, WSR apparatus 300 is built upon and hence shares a number of the elements used in the embodiment of FIG. 2B, as identified by those labeled with identical numerals. In this case, the one-dimensional fiber collimator array 110 of FIG. 2B is replaced by a two-dimensional array 350 of fiber collimators, providing for an input-port and a plurality of output ports. Accordingly, the one-dimensional collimatoralignment mirror array 220 of FIG. 2B is replaced by a two-dimensional array 320 of collimator-alignment mirrors, and first and second one-dimensional arrays 260, 270 of imaging lenses of FIG. 2B are likewise replaced by first and second two-dimensional arrays 360, 370 of imagining lenses respectively. As in the case of the embodiment of FIG. 2B, the first and second two-dimensional arrays 360, 370 of imaging lenses are placed in a 4-f telecentric arrangement with respect to the two-dimensional collimator-alignment mirror array 320 and the two-dimensional fiber collimator array 350. The channel micromirrors 103 must be pivotable biaxially in this case (in order to direct its corresponding spectral channel to any one of the output ports). As such, the WSR apparatus 300 is equipped to support a greater number of the output ports.

In addition to facilitating the coupling of the spectral channels into the respective output ports as described above, the collimator-alignment mirrors in the above embodiments also serve to compensate for misalignment (e.g., due to fabrication and assembly errors) in the fiber collimators that provide for the input and output ports. For instance, relative misalignment between the fiber cores and their respective collimating lenses in the fiber collimators can lead to pointing errors in the collimated beams, which may be corrected for by the collimator-alignment mirrors. For these reasons, the collimator-alignment mirrors are preferably rotatable about two axes. They may be silicon micromachined mirrors, for fast rotational speeds. They may also be other types of mirrors or beam-deflecting elements known in the art.

To optimize the coupling of the spectral channels into the output ports and further maintain the optimal optical alignment against environmental effects such as temperature variations and mechanical instabilities over the course of operation, a WSR apparatus of the present invention may incorporate a servo-control assembly, for providing dynamic control of the coupling of the spectral channels into the respective output ports on a channel-by-channel basis. A WSR apparatus incorporating a servo-control assembly is termed a WSR-S apparatus, thereinafter in this specification.

FIG. 4A depicts a schematic illustration of a first embodiment of a WSR-S apparatus according to the present inven- 10 tion. The WSR-S apparatus 400 comprises a WSR apparatus 410 and a servo-control assembly 440. The WSR 410 may be in the embodiment of FIG. 1A, or any other embodiment in accordance with the present invention. The servo-control assembly 440 includes a spectral monitor 460, for monitor- 15 ing the power levels of the spectral channels coupled into the output ports 420-1 through 420-N of the WSR apparatus 410. By way of example, the spectral monitor 460 is coupled to the output ports 420-1 through 420-N by way of fiberoptic couplers 420-1-C through 420-N-C, wherein each 20 fiber-optic coupler serves to tap off a predetermined fraction of the optical signal in the corresponding output port. The servo-control assembly 440 further includes a processing unit 470, in communication with the spectral monitor 460 and the channel micromirrors 430 of the WSR apparatus 25 410. The processing unit 470 uses the power measurements from the spectral monitor 460 to provide feedback control of the channel micromirrors 430 on an individual basis, so as to maintain a desired coupling efficiency for each spectral channel into a selected output port. As such, the servo- 30 control assembly 440 provides dynamic control of the coupling of the spectral channels into the respective output ports on a channel-by-channel basis and thereby manages the power levels of the spectral channels coupled into the output ports. The power levels of the spectral channels in the 35 output ports may be dynamically managed according to demand, or maintained at desired values (e.g., equalized at a predetermined value) in the present invention. Such a spectral power-management capability is essential in WDM optical networking applications, as discussed above.

FIG. 4B depicts a schematic illustration of a second embodiment of a WSR-S apparatus according to the present invention. The WSR-S apparatus 450 comprises a WSR apparatus 480 and a servo-control assembly 490. In addition to the channel micromirrors 430 (and other elements iden- 45 tified by the same numerals as those used in FIG. 4A), the WSR apparatus 480 further includes a plurality of collimator-alignment mirrors 485, and may be configured according to the embodiment of FIGS. 2A, 2B, 3, or any other embodiment in accordance with the present invention. 50 By way of example, the servo-control assembly 490 includes the spectral monitor 460 as described in the embodiment of FIG. 4A, and a processing unit 495. In this case, the processing unit 495 is in communication with the channel micromirrors 430 and the collimator-alignment mir- 55 rors 485 of the WSR apparatus 480, as well as the spectral monitor 460. The processing unit 495 uses the power measurements from the spectral monitor 460 to provide dynamic control of the channel micromirrors 430 along with the collimator-alignment mirrors 485, so to maintain the 60 coupling efficiencies of the spectral channels into the output ports at desired values.

In the embodiment of FIG. 4A or 4B, the spectral monitor 460 may be one of spectral power monitoring devices known in the art that is capable of detecting the power levels 65 of spectral components in a multi-wavelength optical signal. Such devices are typically in the form of a wavelength12

separating means (e.g., a diffraction grating) that spatially separates a multi-wavelength optical signal by wavelength into constituent spectral components, and one or more optical sensors (e.g., an array of photodiodes) that are configured such to detect the power levels of these spectral components. The processing unit 470 in FIG. 4A (or the processing unit 495 in FIG. 4B) typically includes electrical circuits and signal processing programs for processing the power measurements received from the spectral monitor 460 and generating appropriate control signals to be applied to the channel micromirrors 430 (and the collimator-alignment mirrors 485 in the case of FIG. 4B), so to maintain the coupling efficiencies of the spectral channels into the output ports at desired values. The electronic circuitry and the associated signal processing algorithm/software for such processing unit in a servo-control system are known in the art. A skilled artisan will know how to implement a suitable spectral monitor along with an appropriate processing unit to provide a servo-control assembly in a WSP-S apparatus according to the present invention, for a given application.

The incorporation of a servo-control assembly provides additional advantages of effectively relaxing the requisite fabrication tolerances and the precision of optical alignment during initial assembly of a WSR apparatus of the present invention, and further enabling the system to correct for shift in the alignment over the course of operation. By maintaining an optimal optical alignment, the optical losses incurred by the spectral channels are also significantly reduced. As such, the WSR-S apparatus thus constructed is simpler and more adaptable in structure, more robust in performance, and lower in cost and optical loss. Accordingly, the WSR-S (or WSR) apparatus of the present invention may be used to construct a variety of optical devices and utilized in many applications.

For instance, by directing the spectral channels into the output ports in a one-channel-per-port fashion and coupling the output ports of a WSR-S (or WSR) apparatus to an array of optical sensors (e.g., photodiodes), or a single optical sensor that is capable of scanning across the output ports, a dynamic and versatile spectral power monitor (or channel analyzer) is provided, which would be highly desired in WDM optical networking applications. Moreover, a novel class of optical add-drop multiplexers (OADMs) may be built upon the WSR-S (or WSR) apparatus of the present invention, as exemplified in the following embodiments.

FIG. 5 depicts an exemplary embodiment of an optical add-drop multiplexer (OADM) according to the present invention. By way of example, OADM 500 comprises a WSR-S (or WSR) apparatus 510 and an optical combiner 550. An input port 520 of the WSR-S apparatus 510 transmits a multi-wavelength optical signal. The constituent spectral channels are subsequently separated and routed into a plurality of output ports, including a pass-through port 530 and one or more drop ports 540-1 through 540-N (N $\geq$ 1). The pass-through port 530 may receive any number of the spectral channels (i.e., the pass-through spectral channels). Each drop port may also receive any number of the spectral channels (i.e., the drop spectral channels). The pass-through port 530 is optically coupled to the optical combiner 550, which serves to combine the pass-through spectral channels with one or more add spectral channels provided by one or more add ports 560-1 through 560-M (M≥1). The combined optical signal is then routed into an existing port 570, providing an output multi-wavelength optical signal.

In the above embodiment, the optical combiner 550 may be a K×1 (K $\geq$ 2) broadband fiber-optic coupler, wherein there are K input-ends and one output-end. The pass-through spectral channels and the add spectral channels are fed into the K input-ends (e.g., in a one-to-one correspondence) and the combined optical signal exits from the output-end of the K×1 fiber-optic coupler as the output multi-wavelength optical signal of the system. Such a multiple-input coupler also serves the purpose of multiplexing a multiplicity of add spectral channels to be coupled into the OADM 500. If the power levels of the spectral channels in the output multiwavelength optical signal are desired to be actively managed, such as being equalized at a predetermined value, 10 two spectral monitors may be utilized. As a way of example, the first spectral monitor may receive optical signals tapped off from the pass-through port 530 and the drop ports 540-1 through 540-N (e.g., by way of fiber-optic couplers as depicted in FIG. 4A or 4B). The second spectral monitor 15 receives optical signals tapped off from the exiting port 570. A servo-control system may be constructed accordingly for monitoring and controlling the pass-through, drop and add spectral channels. As such, the embodiment of FIG. 5 provides a versatile optical add-drop multiplexer in a simple 20 and low-cost assembly, while providing multiple physically separate drop/add ports in a dynamically reconfigurable fashion.

FIG. 6 depicts an alternative embodiment of an optical add-drop multiplexer (OADM) according to the present 25 invention. By way of example, OADM 600 comprises a first WSR-S apparatus 610 optically coupled to a second WSR-S apparatus 650. Each WSR-S apparatus may be in the embodiment of FIG. 4A or 4B. (A WSR apparatus of the embodiment of FIG. 1A, 2A, 2B, or 3 may be alternatively 30 implemented.) The first WSR-S apparatus 610 includes an input port 620, a pass-through port 630, and one or more drop ports 640-1 through 640-N (N≥1). The pass-through spectral channels from the pass-through port 630 are further coupled to the second WSR-S apparatus 650, along with one 35 or more add spectral channels emerging from add ports 660-1 through 660-M (M≥1). In this exemplary case, the pass-through port 630 and the add ports 660-1 through 660-M constitute the input ports for the second WSR-S apparatus 650. By way of its constituent wavelength-40 separator (e.g., a diffraction grating) and channel micromirrors (not shown in FIG. 6), the second WSR-S apparatus 650 serves to multiplex the pass-through spectral channels and the add spectral channels, and route the multiplexed optical signal into an exiting port 770 to provide an output signal of 45 the system.

In the embodiment of FIG. 6, one WSR-S apparatus (e.g., the first WSR-S apparatus 610) effectively performs dynamic drop function, whereas the other WSR-S apparatus (e.g., the second WSR-S apparatus 650) carries out dynamic 50 add function. And there are essentially no fundamental restrictions on the wavelengths that can be added or dropped (other than those imposed by the overall communication system). Moreover, the underlying OADM architecture thus presented is intrinsically scalable and can be readily 55 extended to any number of cascaded WSR-S (or WSR) systems, if so desired for performing intricate add and drop functions. Additionally, the OADM of FIG. 6 may be operated in reverse direction, by using the input ports as the output ports, the drop ports as the add ports, and vice versa. 60

Those skilled in the art will recognize that the aforementioned embodiments provide only two of many embodiments of a dynamically reconfigurable OADM according to the present invention. Those skilled in the art will also appreciate that various changes, substitutions, and alterna tions can be made herein without departing from the principles and the scope of the invention as defined in the

appended claims. Accordingly, a skilled artisan can design an OADM in accordance with the principles of the present invention, to best suit a given application.

Although the present invention and its advantages have been described in detail, it should be understood that various changes, substitutions, and alternations can be made herein without departing from the principles and the scope of the invention. Accordingly, the scope of the present invention should be determined by the following claims and their legal equivalents.

What is claimed is:

1. A wavelength-separating-routing apparatus, comprising:

- a) multiple fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots; and
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously controllable to reflect said spectral channels into selected ones of said output ports.

2. The wavelength-separating-routing apparatus of claim 1 further comprising a servo-control assembly, in communication with said channel micromirrors and said output ports, for providing control of said channel micromirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

3. The wavelength-separating-routing apparatus of claim 2 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors.

4. The wavelength-separating-routing apparatus of claim 3 wherein said servo-control assembly maintains said power levels at a predetermined value.

5. The wavelength-separating-routing apparatus of claim 1 further comprising an array of collimator-alignment mirrors, in optical communication with said wavelengthseparator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

 The wavelength-separating-routing apparatus of claim
 wherein each collimator-alignment mirror is rotatable about one axis.

7. The wavelength-separating-routing apparatus of claim 5 wherein each collimator-alignment mirror is rotatable about two axes.

8. The wavelength-separating-routing apparatus of claim 5 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimatoralignment mirrors and said fiber collimators.

9. The wavelength-separating-routing apparatus of claim 1 wherein each channel micromirror is continuously pivotable about one axis.

10. The wavelength-separating-routing apparatus of claim 1 wherein each channel micromirror is pivotable about two axes.

11. The wavelength-separating-routing apparatus of claim 10 wherein said fiber collimators are arranged in a twodimensional array.

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12. The wavelength-separating-routing apparatus of claim 1 wherein each channel micromirror is a silicon micromachined mirror.

13. The wavelength-separating-routing apparatus of claim 1 wherein said fiber collimators are arranged in a one-dimensional array.

14. The wavelength-separating-routing apparatus of claim 1 wherein said beam-focuser comprises a focusing lens having first and second focal points.

15. The wavelength-separating-routing apparatus of claim 14 wherein said wavelength-separator and said channel micromirrors are placed respectively at said first and second focal points of said focusing lens.

16. The wavelength-separating-routing apparatus of claim 1 wherein said beam-focuser comprises an assembly of lenses.

17. The wavelength-separating-routing apparatus of claim 1 wherein said wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

18. The wavelength-separating-routing apparatus of claim 1 further comprising a quarter-wave plate optically interposed between said wavelength-separator and said channel micromirrors.

The wavelength-separating-routing apparatus of claim
 wherein each output port carries a single one of said spectral channels.

**20**. The wavelength-separating-routing apparatus of claim **19** further comprising one or more optical sensors, optically coupled to said output ports.

21. A servo-based optical apparatus comprising:

- a) multiple fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually controllable to reflect said spectral channels into selected ones of said output ports; and
- e) a servo-control assembly, in communication with said channel micromirrors and said output ports, for maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

22. The servo-based optical apparatus of claim 21 wherein 50 said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors. 55

23. The servo-based optical apparatus of claim 22 wherein said servo-control assembly maintains said power levels at a predetermined value.

24. The servo-based optical apparatus of claim 21 further comprising an array of collimator-alignment mirrors, in 60 optical communication with said wavelength-separator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports. 65

25. The servo-based optical apparatus of claim 24 further comprising first and second arrays of imaging lenses, in a

telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

26. The servo-based optical apparatus of claim 24 wherein each collimator-alignment mirror is rotatable about at least one axis.

27. The servo-based optical apparatus of claim 21 wherein each channel micromirror is continuously pivotable about at least one axis.

 ${\bf 28}.$  The servo-based optical apparatus of claim  ${\bf 21}$  wherein each channel micromirror is a silicon micromachined mirror.

29. The servo-based optical apparatus of claim 21 wherein said wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

**30**. The servo-based optical apparatus of claim **21** wherein said beam-focuser comprises one or more lenses.

31. An optical apparatus comprising:

- a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously controllable to reflect said spectral channels into selected ones of said output ports; and
- a one-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multiwavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

32. The optical apparatus of claim 31 further comprising a servo-control assembly, in communication with said chanand nel micromirrors, said collimator-alignment mirrors, and said output ports, for providing control of said channel micromirrors along with said collimator-alignment mirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

33. The optical apparatus of claim 32 wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors and said collimator-alignment mirrors.

34. The optical apparatus of claim 31 wherein each channel micromirror is continuously pivotable about at least one axis.

**35**. The optical apparatus of claim **31** wherein each <sup>55</sup> collimator-alignment mirror is rotatable about at least one axis.

36. The optical apparatus of claim 31 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

37. An optical apparatus comprising:

- a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;

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- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots;
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being individually and continuously controllable to reflect said spectral channels into selected ones of said output ports; and
- e) a two-dimensional array of collimator-alignment mirrors, for adjusting an alignment of said multiwavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

**38**. The optical apparatus of claim **37** further comprising a servo-control assembly, in communication with said channel micromirrors, said collimator-alignment mirrors, and said output ports, for providing control of said channel micromirrors along with said collimator-alignment mirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports.

**39**. The optical apparatus of claim **38** wherein said servo-control assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors and said collimator-alignment mirrors.

40. The optical apparatus of claim 37 wherein each collimator-alignment mirror is rotatable about at least one axis.

**41**. The optical apparatus of claim **37** wherein each  $_{30}$  channel micromirror is continuously pivotable about at least one axis.

42. The optical apparatus of claim 41 wherein each channel micromirrors is pivotable about two axes, and wherein said fiber collimators are arranged in a two- $_{35}$  dimensional array.

43. The optical apparatus of claim 37 further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

44. An optical system comprising a wavelengthseparating-routing apparatus, wherein said wavelengthseparating-routing apparatus includes:

- a) an array of fiber collimators, providing an input port for a multi-wavelength optical signal and a plurality of output ports including a pass-through port and one or more drop ports;
- b) a wavelength-separator, for separating said multiwavelength optical signal from said input port into multiple spectral channels;
- c) a beam-focuser, for focusing said spectral channels into corresponding spectral spots; and
- d) a spatial array of channel micromirrors positioned such that each channel micromirror receives one of said spectral channels, said channel micromirrors being 55 individually and continuously pivotable to reflect said spectral channels into selected ones of said output ports, whereby said pass-through port receives a subset of said spectral channels.

**45**. The optical system of claim **44** further comprising a 60 servo-control assembly, in communication with said channel micromirrors and said output ports, for providing control of said channel micromirrors and thereby maintaining a predetermined coupling of each reflected spectral channel into one of said output ports. 65

46. The optical system of claim 45 wherein said servocontrol assembly comprises a spectral monitor for monitoring power levels of said spectral channels coupled into said output ports, and a processing unit responsive to said power levels for providing control of said channel micromirrors.

47. The optical system of claim 44 further comprising an array of collimator-alignment mirrors, in optical communication with said wavelength-separator and said fiber collimators, for adjusting an alignment of said multi-wavelength optical signal from said input port and directing said reflected spectral channels into said output ports.

**48**. The optical system of claim **47** further comprising first and second arrays of imaging lenses, in a telecentric arrangement with said collimator-alignment mirrors and said fiber collimators.

**49**. The optical system of claim **47** wherein each 15 collimator-alignment mirror is rotatable about at least one axis.

**50**. The optical system of claim **44** wherein each channel micromirror is pivotable about at least one axis.

**51**. The optical system of claim **44** wherein each channel <sup>20</sup> micromirror is a silicon micromachined mirror.

52. The optical system of claim 44 wherein said beamfocuser comprises a focusing lens having first and second focal points, and wherein said wavelength-separator and said channel micromirrors are placed respectively at said 25 first and second focal points.

**53**. The optical system of claim **44** wherein said wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

54. The optical system of claim 44 further comprising a quarter-wave plate optically interposed between said wavelength-separator and said channel micromirrors.

55. The optical system of claim 44 further comprising an auxiliary wavelength-separating-routing apparatus, including:

a) multiple auxiliary fiber collimators, providing a plurality of auxiliary input ports and an exiting port;

b) an auxiliary wavelength-separator;

c) an auxiliary beam-focuser; and

- d) a spatial array of auxiliary channel micromirrors;
- wherein said subset of said spectral channels in said pass-through port and one or more add spectral channels are directed into said auxiliary input ports, and multiplexed into an output optical signal directed into said exiting port by way of said auxiliary wavelengthseparator, said auxiliary beam-focuser and said auxiliary channel micromirrors.

**56**. The optical system of claim **55** wherein said auxiliary channel micromirrors are individually pivotable.

57. The optical system of claim 55 wherein each auxiliary channel micromirror is pivotable continuously about at least one axis.

**58**. The optical system of claim **55** wherein each auxiliary channel micromirror is a silicon micromachined mirror.

**59**. The optical system of claim **55** wherein said auxiliary wavelength-separator comprises an element selected from the group consisting of ruled diffraction gratings, holographic diffraction gratings, echelle gratings, curved diffraction gratings, and dispersing prisms.

60. The optical system of claim 55 wherein said passthrough port constitutes one of said auxiliary input ports.

**61**. A method of performing dynamic wavelength sepa-65 rating and routing, comprising:

 a) receiving a multi-wavelength optical signal from an input port;

- b) separating said multi-wavelength optical signal into multiple spectral channels;
- c) focusing said spectral channels onto a spatial array of corresponding beam-deflecting elements, whereby each beam-deflecting element receives one of said 5 spectral channels; and
- d) dynamically and continuously controlling said beamdeflecting elements, thereby directing said spectral

providing feedback control of said beam-deflecting elements, thereby maintaining a predetermining coupling of each spectral channel directed into one of said output ports.

63. The method of claim 62 further comprising the step of maintaining power levels of said spectral channels directed <sup>15</sup> into said output ports at a predetermining value.

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64. The method of claim 61 wherein each spectral channel is directed into a separate output port.

65. The method of claim 61 wherein a subset of said spectral channels is directed into one of said output ports, thereby providing one or more pass-through spectral channels.

66. The method of claim 65 further comprising the step of multiplexing said pass-through spectral channels with one or 62. The method of claim 61 further comprising the step of 10 more add spectral channels, so as to provide an output optical signal.

> 67. The method of claim 61 wherein said beam-deflecting elements comprise an array of silicon micromachined mirrors.

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