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# United States Patent [19] Kolpak

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- [54] MULTI-PHASE FLUID FLOW MEASUREMENT
- [75] Inventor: Miroslav M. Kolpak, Plano, Tex.
- [73] Assignee: Atlantic Richfield Company, Los Angeles, Calif.
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### Related U.S. Application Data

- [63] Continuation-in-part of Ser. No. 523,152, May 14, 1990, Pat. No. 5,090,253.
- [51] Int. Cl.<sup>5</sup> ..... G01N 33/00
- [52] U.S. Cl. .... 73/19.03; 73/19.10
- [58] Field of Search ..... 73/861.04, 861.37, 861.38, 73/19.01, 19.03, 19.05

### References Cited

#### U.S. PATENT DOCUMENTS

- 3,927,565 12/1975 Pavlin et al. .... 73/861.38 X
- 4,096,745 6/1978 Riukin et al. .... 73/861.37 X
- 5,029,482 7/1991 Liu et al. .... 73/861.04 X

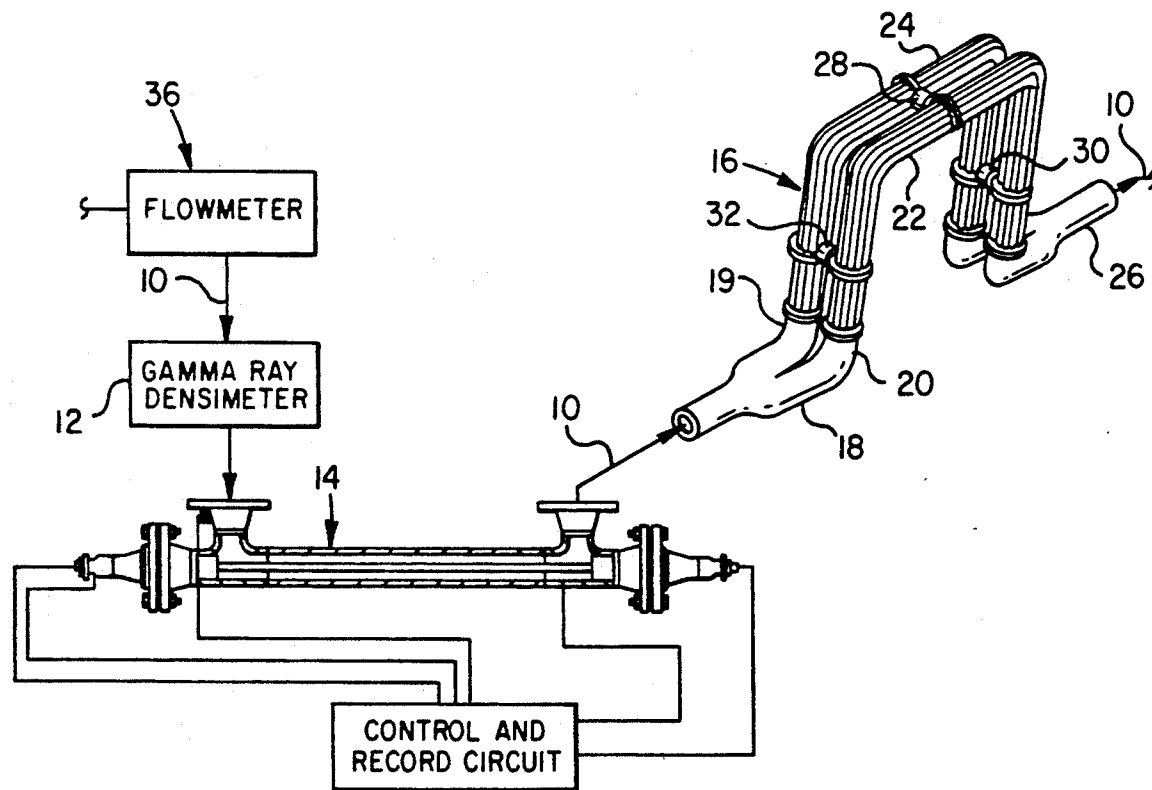
Primary Examiner—Herbert Goldstein

Attorney, Agent, or Firm—Michael E. Martin

### [57] ABSTRACT

Multiphase (gas and two liquid phases) fluid flowstreams are measured to determine the total flow rate, fluid density, the fraction of gas, and one liquid in the total liquid mixture by passing the flowstream through a Ceriolis flow meter (16, 40), a densimeter (12) and a meter (14) which measures the fraction of one liquid in the two liquid mixture. The total fluid flow rate may be measured by a single tube flow meter (40) having adjacent loops which provide tube legs (49, 51) positioned adjacent each other and vibrated laterally at a predetermined frequency and amplitude while measuring pressures in the contraflowing streams in the adjacent tube legs. The density and gas fraction of the flowstream may be determined by vibrating a tube containing the flowstream over a range of frequencies and measuring the phase angle and amplitude of the fluctuating fluid pressures compared with acceleration of the tube to determine the sloshing natural frequency of the fluid mixture. The tube may be vibrated at a frequency far from the sloshing natural frequency of the fluid mixture to determine the fluid density.

12 Claims, 2 Drawing Sheets



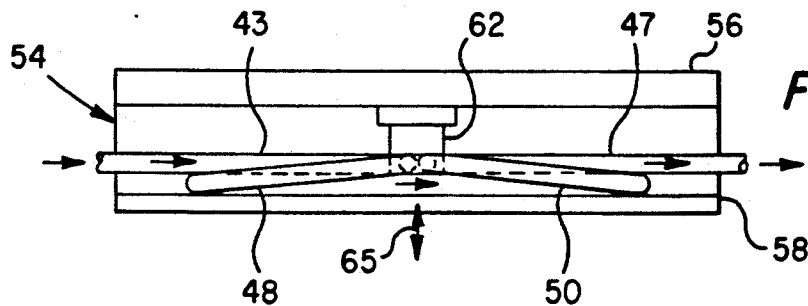
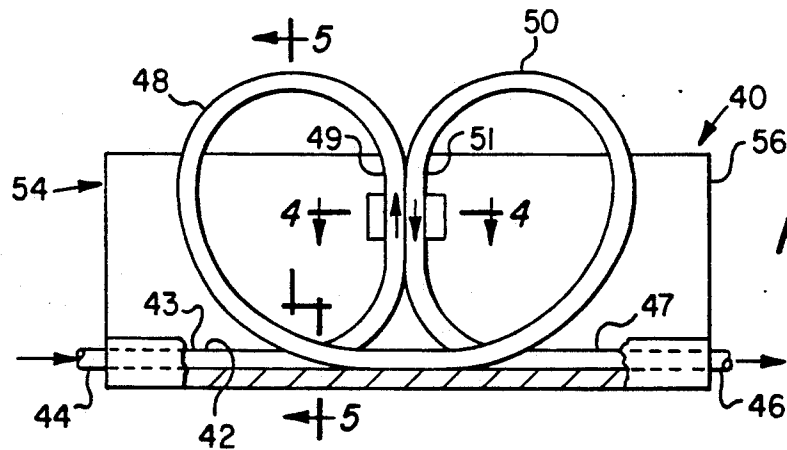
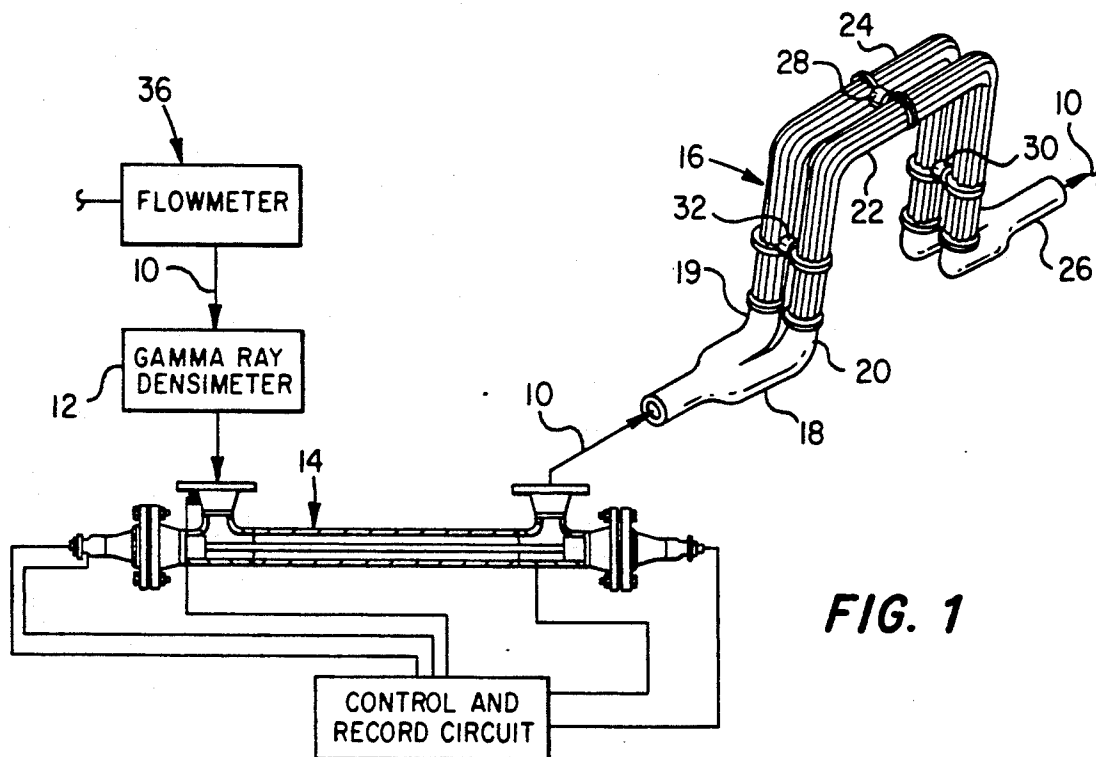


FIG. 4

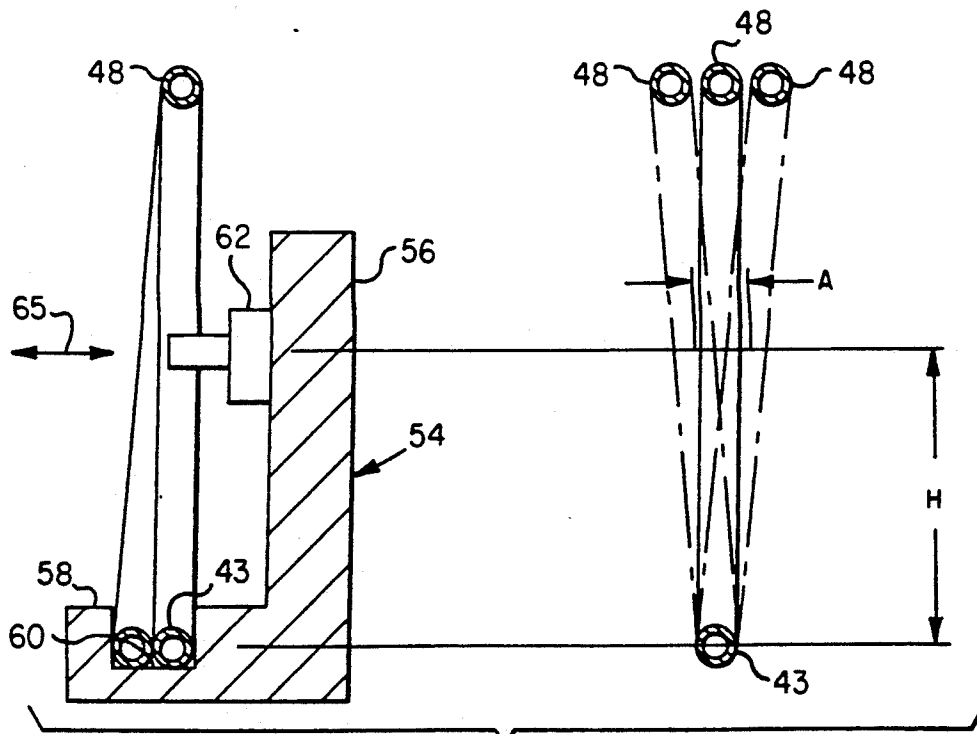
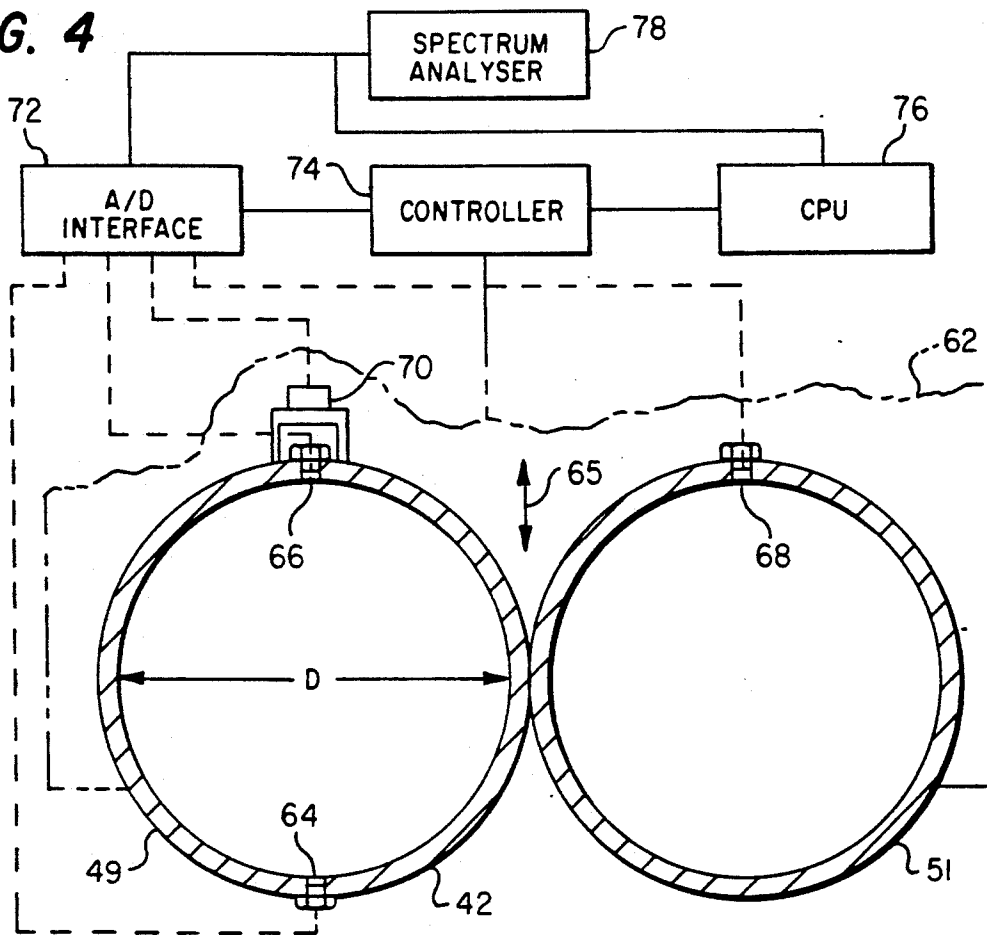


FIG. 5

## MULTI-PHASE FLUID FLOW MEASUREMENT

### CROSS REFERENCE TO RELATED APPLICATION

This application is a continuation in part of application Ser. No. 07/523,152, filed May 14, 1990, now U.S. Pat. No. 5,090,253, the subject matter of which is incorporated herein by reference.

### BACKGROUND OF THE INVENTION

#### 1. Field of the Invention

The present invention pertains to methods and apparatus for measuring multi-phase fluid flow such as mixtures of oil, water and gas utilizing a densimeter, a two-phase flow meter based on microwave attenuation characteristics and a mass or volumetric flow meter such as a modified coriolis-type flow meter.

#### 2. Background of the Invention

Various techniques and systems have been developed for measuring multi-phase fluid flow, in particular, three phase fluid flow comprising a mixture of oil, water and gas. My U.S. Pat. No. 4,852,395, assigned to the assignee of the present invention describes a system for measuring multiphase fluid flow wherein gas is separated from a mixture of oil and water and the fractions of oil and water are then determined including measuring batch samples to correct for the residual gas content. Although such a system has a high degree of accuracy, it is relatively mechanically complex and requires a gas separator and gas flow meter.

Mechanically simple flow meters are sought for many applications, particularly in applications for measuring the multiphase fluid emanating from oil and gas wells wherein essentially, mixtures of water, hydrocarbon liquids, such as crude oil; and gas are continually produced in varying proportions of the total fluid flowstream. The present invention provides new and unique methods for measuring multiphase fluid flow, particularly of the type above described, as well as improved apparatus for measuring such multiphase fluid flow, which overcomes some of the problems associated with prior art methods and systems.

### SUMMARY OF THE INVENTION

The present invention provides improved methods for measuring multiphase fluid flow, such as mixtures of oil, water and gas.

In accordance with one aspect of the present invention a method is provided for measuring the oil, water and gas flow rates of a multiphase fluid flowstream without completely separating any of the fluid fractions from the flowstream. A system for practicing the method includes a meter which measures the oil and water fractions of the flowstream, a densimeter and a coriolis type flow meter. The oil-water fraction or "watercut" meter may be one of several types but is preferably one based on microwave attenuation characteristics which vary with the fraction of oil and water, respectively. The coriolis type flow meter may be of the type described in co-pending U.S. patent application Ser. No. 07/523,152.

In another system and method according to the invention, the fractional volumetric flow rates may be determined using only, in combination, the watercut meter and the modified coriolis type flow meter.

The present invention still further provides unique methods and apparatus for determining the gas fraction

and density of a multiphase fluid mixture utilizing a single continuous tube type device which is vibrated substantially at the sloshing resonant frequency of the fluid mixture, or determining the density of a fluid mixture by vibrating the device at a frequency substantially away from the sloshing resonant frequency. Still further, there is provided a method and system utilizing a single continuous tube type flow meter with tube portions wherein the fluid flow at a predetermined point is in opposite directions and wherein the difference in fluid pressures at selected locations in the tube are measured to determine mass flow rate.

Those skilled in the art will recognize the above-described advantages and superior features of the present invention together with other important aspects thereof upon reading the detailed description which follows in conjunction with the drawing.

### BRIEF DESCRIPTION OF THE DRAWING

FIG. 1 is a schematic diagram illustrating one combination of measurement devices used in conjunction with the methods of the present invention.

FIG. 2 is a side elevation of a single continuous tube type flow measuring apparatus in accordance with the present invention;

FIG. 3 is a top plan view of the apparatus shown in FIG. 2;

FIG. 4 is a section view taken along the line 4—4 of FIG. 2 illustrating an arrangement which is used in conjunction with a method of the present invention;

FIG. 5 is a section view taken along line 5—5 of FIG. 2 and including a diagram illustrating some of the dimensions used in accordance with the method of the present invention.

### DESCRIPTION OF PREFERRED EMBODIMENTS

In the description which follows like parts are marked throughout the specification and drawing with the same reference numerals, respectively. The drawing figures are not to scale and certain features are shown in schematic form in the interest of clarity and conciseness. Referring to FIG. 1, there is illustrated a conduit 10 which is operable to conduct a multiphase fluid flowstream, such as might result from the production of crude oil from a well, and which typically includes a mixture of crude oil, water and gas. The systems and methods described herein are more accurate when the gas content of the fluid flowstream is less than about twenty percent (20%) of the total. Preliminary separation of gas might be necessary in some situations in order to prepare the flowstream for measurements by the system of the present invention. In FIG. 1, four separate devices are shown interposed in the conduit 10 and which devices may be used in certain combinations or alone to make certain measurements in accordance with the present invention. A densimeter 12 is interposed in the conduit 10 which may be of the so-called gamma ray type, for example. The densimeter 12 may be of a type commercially available, such as a model S-Series "Sensor Net" manufactured by TN Technologies, Inc. of Round Rock, Tex. A second device shown interposed in the conduit 10 for receiving flow of fluid therethrough is a so-called "watercut" meter, generally designated by the numeral 14, and of the type which measures changes in microwave attenuation resulting from changes in the composition of the fluid flowing

therethrough. The meter 14 is preferably of the type disclosed and claimed in U.S. Pat. Nos. 4,862,060 issued Aug. 29, 1989 or 4,996,490 issued Feb. 26, 1991 both to Scott et al. and both assigned to the assignee of the present invention. Suffice it to say that the meter 14 is operable to measure the water fraction of an oil-water mixture which may include certain amounts of gas entrained therein.

FIG. 1 further illustrates a modified coriolis type flow meter, generally designated by the numeral 16, which may be of the type described in application Ser. No. 07/523,152. Basically, the flow meter 16 comprises an inlet conduit 18 which is split into two branch conduits 19 and 20 which are in communication with respective bundles of smaller diameter tubes 22 and 24, having a generally U-shaped configuration, and connected to an outlet manifold 26 similar to the manifold or conduit 18. The tube bundles 22 and 24 are vibrated in a generally lateral direction with respect to their longitudinal central axes by suitable vibrator means and the vibrations of the respective upstream and downstream legs of the tube bundles 22 and 24 are sensed by vibration sensors 30 and 32. Further details of the flow meter 16 may be obtained by referring to the above-referenced patent application.

In accordance with a first method the gas, water and oil flow rates in a multi-phase fluid flowstream flowing through the conduit 10 may be determined utilizing the densimeter 12, a meter such as the meter 14, and the coriolis flow meter 16, for example. The densimeter 12 provides measurement of the total fluid mixture density,  $dm$ , and the coriolis flow meter 16 provides measurement of the apparent mixture density,  $dma$ , which is related to the true mixture density,  $dm$ , by the equation:

$$dm = dma(1 + A2 * fg + A3 * fg^2) \quad (1)$$

where  $A2$  and  $A3$  are coefficients which may be determined earlier by calibration of the meter 16 in gassy liquid flow wherein small uniformly distributed gas bubbles are present in the range of zero percent (0%) to twenty percent (20%) by volume in the liquid, and  $fg$  is the gas fraction of the multi-phase fluid flowstream. Equation (1) may be solved for the gas fraction,  $fg$ , which then takes the form:

$$fg = \frac{\sqrt{A2^2 - 4A3(1 - dm/dma)}}{2A3} \quad (2)$$

The coriolis type flow meter 16, is operable to provide a measurement of the apparent mass flow rate of the fluid flowstream,  $Ma$ , which is related to the true mass flow rate,  $M$ , by the equation:

$$M = Ma(1 + A4 * fg + A5 * fg^2 + \dots) \quad (3)$$

where  $A4$ ,  $A5$ , ... are coefficients which are also determined earlier by calibration of the coriolis meter 16 in gassy liquid flow wherein small uniformly distributed gas bubbles are present in the range of zero percent (0%) to twenty percent (20%) by volume, in the liquid.

The oil, water and gas volumetric flow rates  $Qo$ ,  $Qw$ , and  $Qg$  are computed by:

$$Qo = Qm(1 - fg)(1 - wc) \quad (4)$$

$$Qw = Qm(1 - fg) * wc \quad (5)$$

$$Qg = Qm * fg \quad (6)$$

where  $Qm$  is the volumetric flow rate of the fluid mixture determined by:

$$Qm = M/dm \quad (7)$$

where  $dm$  and  $M$  are computed by equations (1) and (3) substituting the value of the gas fraction,  $fg$ , determined in equation (2) and the value of the water fraction,  $wc$ , as determined by the meter 14. The method just described above provides volumetric flow rates for the oil fraction, the water fraction and the gas fraction without the need of knowing the density of each of these components.

On the other hand, in situations where the water density, the oil density and the gas density are known or are easily measured and are relatively stable from time to time over the period where flow measurement is desired, the flow rates of each of the fractions of gas, water and oil in the multi-phase flowstream may be determined by a second method using a watercut meter and a modified coriolis type meter such as the meters 14 and 16, respectively. The coriolis meter 16 will provide a measurement of the apparent density of the mixture,  $dma$ , which may be used to determine the true density,  $dm$ , from equation (1). The gas fraction,  $fg$ , is related to the density values and the water fraction (on a volumetric basis) by the following equation:

$$fg = \frac{wc(dw - do) + (do - dm)}{(do - dg)} \quad (8)$$

where  $fg$  is the gas fraction,  $wc$  is the water fraction measured by the meter 14,  $do$  is the oil density,  $dw$  is the water density and  $dg$  is the gas density.

Simultaneous solution of equations (1) and (8) yields

$$fg = \frac{\sqrt{b^2 - 4ac}}{2a}$$

where

$$a = dma * A3 \quad (9)$$

$$b = dma * A2 + wc(dw - do) + (do - dg) \quad (10)$$

$$c = dma - wc(dw - do) - do \quad (11)$$

$wc$  = measured by meter 14

$dma$  = measured by coriolis meter 16

$do, dw, dg$  = known (measured) densities of oil, water and gas

The oil, water and gas flow rates  $Qo$ ,  $Qw$ , and  $Qg$  may then be computed using equations (4) through (6). Accordingly, a method utilizing only two meters, namely the meters 14 and 16 may be used if the densities of the fluid fractions can be measured and remain relatively constant. Inaccuracies caused by imprecise knowledge of the oil density and the water density when oil gravity is low (API gravity approaches about 10) do not occur.

In accordance with a third method of the present invention, the flow rates of the fractional fluid components of a multi-phase fluid flowstream flowing through the conduit 10 may be determined utilizing a watercut

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