

United States Patent [19]

Williamson

[54] HIGH NUMERICAL APERTURE RING FIELD OPTICAL REDUCTION SYSTEM

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- G02B 23/00; G02B 5/10
- 359/729, 858, 859, 730, 731

[56] **References Cited**

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Jewell et al, Reflective Systems Design Study For Soft X–Ray Projection Lithography, Aug. 3, 1990, J. Vac. Sci. Technol B8(6), Nov./Dec. 1990;1990 American Vaccum Society; pp. 1519 to 1523.

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[57] ABSTRACT

An optical projection reduction system used in photolithography for the manufacture of semiconductor devices having a first mirror pair, a second field mirror pair, and a third mirror pair. Electromagnetic radiation from a reticle or mask is reflected by a first mirror pair to a second field mirror pair forming an intermediate image. A third mirror pair re-images the intermediate image to an image plane at a wafer. All six mirrors are spherical or aspheric and rotationally symmetrical about an optical axis. An annular ring field is obtained, a portion of which may be used in a step and scan photolithography system. In another embodiment, weak refracting elements are introduced to further reduce residual aberrations allowing a higher numerical aperture. In the catoptric embodiment of the present invention, a numerical aperture of 0.25 is obtained resulting in a working resolution of 0.03 microns with electromagnetic radiation having a wavelength of 13 nanometers. The optical projection reduction systems are intended for use at extreme ultraviolet to the soft X-ray wavelength range. The present invention, provides a relatively high numerical aperture and uses substantially all reflective elements, greatly facilitating the manufacture of semiconductor devices having feature sizes below 0.25 microns.

18 Claims, 3 Drawing Sheets





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HIGH NUMERICAL APERTURE RING FIELD OPTICAL REDUCTION SYSTEM

FIELD OF THE INVENTION

This invention relates generally to projection lithography, and more particularly to a catoptric and catadioptric optical system for use with short wavelengths in the near and extreme ultraviolet or soft X-ray region.

BACKGROUND OF THE INVENTION

In the manufacture of semiconductor devices, photolithography is often used. Projection optics are used to image a mask or reticle onto a wafer. Optical systems using refractive elements have achieved resolutions approaching 15 0.25 micrometers operating with illumination sources having wavelengths of 248 or 193 nanometers. As the element or feature size of semiconductor devices become smaller, the need for optical projection systems capable of providing a resolution less than 0.25 micrometers are needed. In order to $_{20}$ decrease the feature size which the optical projection systems used in photolithography can resolve, shorter wavelengths of electromagnetic radiation must be used to project the image of a reticle or mask onto a photosensitive substrate, such as a semiconductor wafer. Because very few 25 refractive optical materials are able to transmit significant electromagnetic radiation below a wavelength of 193 nanometers, it is necessary to reduce to a minimum or eliminate refractive elements in optical projection systems operating at wavelengths below 193 nanometers. An optical 30 system that is usable in the deep ultraviolet portion of the spectrum is disclosed in U.S. Pat. No. 4,747,678 entitled "Optical Relay System With Magnification" issuing to Shafer, et al, on May 31, 1988, which is herein incorporated by reference. However, the desire to resolve ever smaller 35 features makes necessary optical projection systems that operate at the extreme ultraviolet wavelengths, below 200 nanometers, to the soft X-ray wavelengths, around 13 nanometers. While there are several optical projection systems that operate within this wavelength region, they are 40limited to a relatively low numerical aperture of less than 0.1 at the image or wafer. Increasing the numerical aperture of these designs will result in unacceptably large residual aberrations and obscuration of the light beams by the edges of the mirrors. While these projection optical systems per-45 form adequately for their intended purpose, there is a need for optical projection systems having a higher numerical aperture for use at wavelengths in the extreme ultraviolet or soft x-ray wavelengths, or for resolutions substantially less than 0.1 micrometers or microns.

SUMMARY OF THE INVENTION

The present invention comprises three mirror pairs. The first mirror pair includes a positive power mirror imaging an entrance pupil onto a second mirror of the first mirror pair 55 providing an accessible, real aperture stop. A second mirror pair receives electromagnetic radiation from the first mirror pair and includes a positive power mirror relaying the aperture stop to a second real pupil and forming an intermediate image. A third mirror pair receives electromagnetic 60 radiation from the second mirror pair, and includes a positive power mirror relaying the second real pupil to an exit pupil at infinity and imaging the intermediate image to a real final image. A six mirror reduction system of relatively high numerical aperture is thereby obtained that provides a 65 reduced image of an object, such as a reticle or mask, onto a photosensitive substrate, such as a semiconductor wafer.

ΟΟΚΕ

The second mirror pair acts as a field mirror element providing a relatively high numerical aperture with good or acceptable image quality. All six mirrors may be aspheric to obtain the smallest possible residual aberrations.

Accordingly, it is an object of the present invention to provide a projection optical system for use with wavelengths lower than approximately 200 nanometers and having a relatively high numerical aperture.

It is a further object of the present invention to increase resolution permitting imaging of small element features as required in semiconductor manufacture.

It is an advantage of the present invention that the object and image are accessible for parallel scanning of a reticle and wafer stage as used in step and scan photolithography.

It is another advantage of the present invention that a relatively large field is obtained.

It is a feature of the present invention that an aperture stop is accessible.

It is a further feature of the present invention that a field mirror element is used.

These and other objects, advantages, and features will become readily apparent in view of the following detailed description.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic illustration of one embodiment of the present invention.

FIG. **2** is a schematic illustration of a second embodiment of the present invention.

FIG. **3** is a schematic illustration of a third embodiment of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 1 schematically illustrates a first embodiment of the present invention. The light from a reticle or mask 10 is collected by concave mirror M1. Dashed line 12 represents the extended curvature of mirror M1. Mirror M1 reflects electromagnetic radiation to concave mirror M2. An aperture stop 14 is positioned at or near mirror M2. An entrance pupil is positioned a finite distance from the reticle or mask 10 and imaged at mirror M2 by mirror M1. Electromagnetic radiation is reflected from mirror M2 to concave mirror M3. Dashed line 16 illustrates the extended curvature of concave mirror M3. Electromagnetic radiation from mirror M3 is received and reflected by concave mirror M4. Dashed line 18 illustrates the extended curvature of concave mirror M4. 50 Electromagnetic radiation is reflected from mirror M4 and received by convex mirror M5. Dashed line 20 illustrates the extended curvature of convex mirror M5. Electromagnetic radiation is reflected from mirror M5 and received by concave mirror M6, and reflected by concave mirror M6 to an image location at a wafer 22. All of the mirrors M1-M6 are substantially rotationally symmetric about the optical axis OA. An intermediate image 24 is formed between the mirrors M4 and M3 or at an off-axis location between the first mirror pair, M1 and M2, and the third mirror pair, M5 and M6. This intermediate image is re-imaged at the wafer 22 by mirrors M4, M5, and M6. The first mirror pair, M1 and M2, reflects electromagnetic radiation to a second mirror pair, M3 and M4. The second mirror pair, M3 and M4, functions as a field mirror element and takes the chief ray leaving mirror M2 diverging away from the optical axis OA, and converts it to a chief ray converging toward the optical axis OA for acceptance by a third mirror pair, M5 and M6.

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